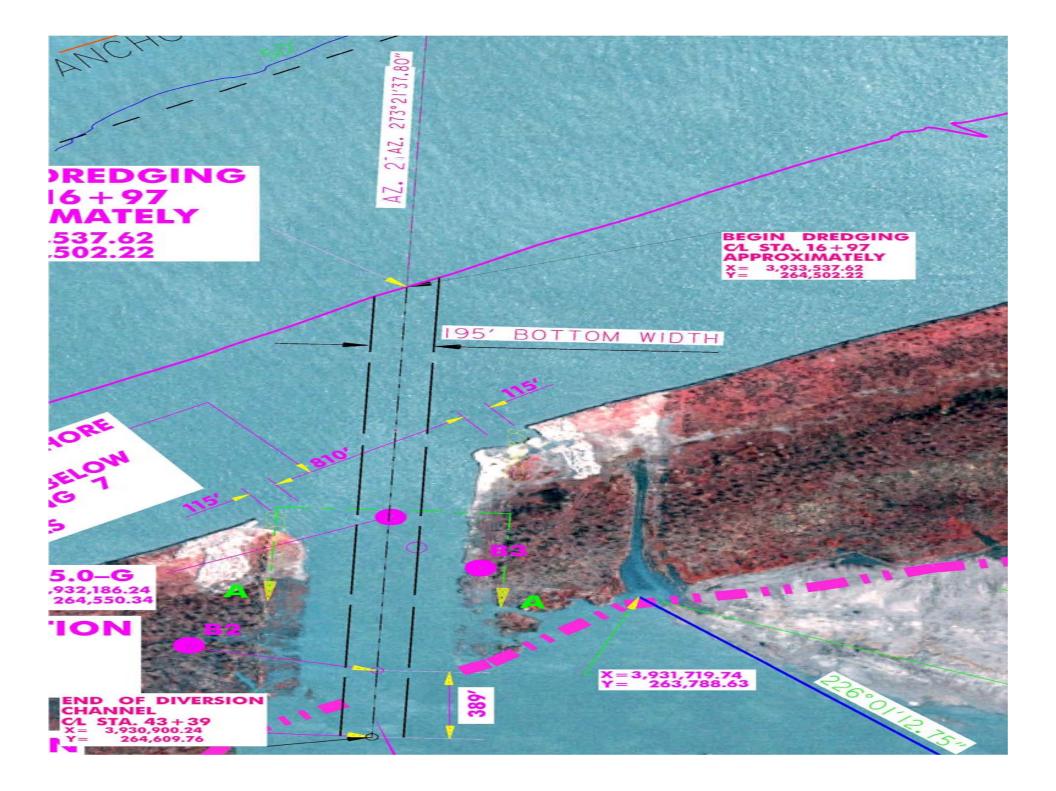
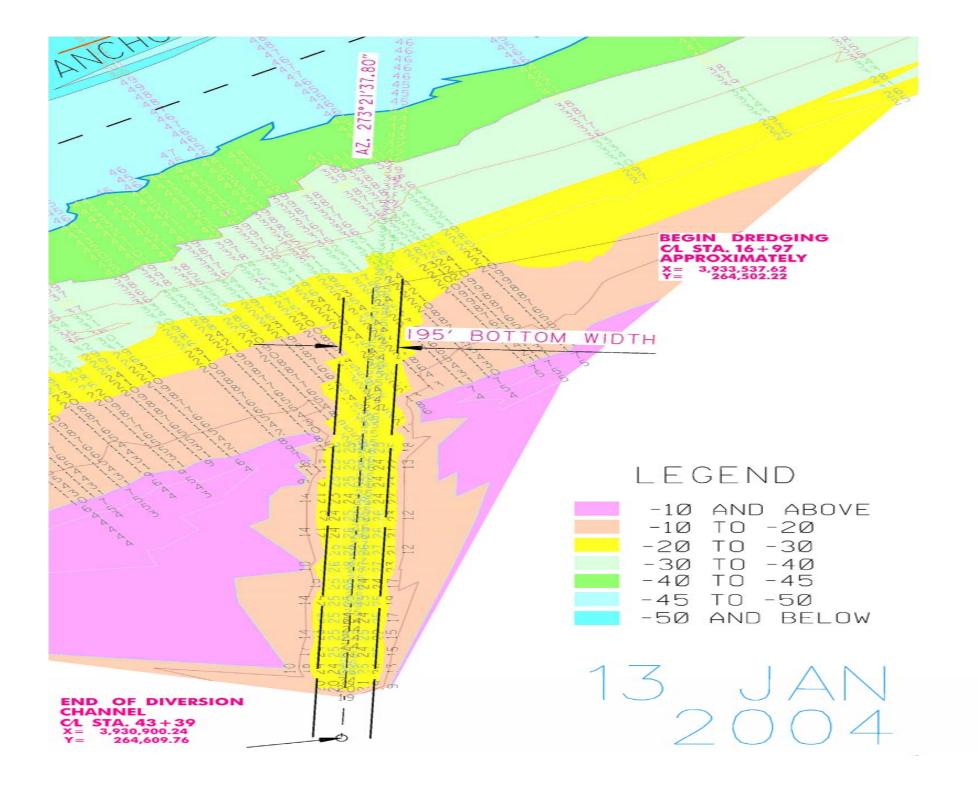
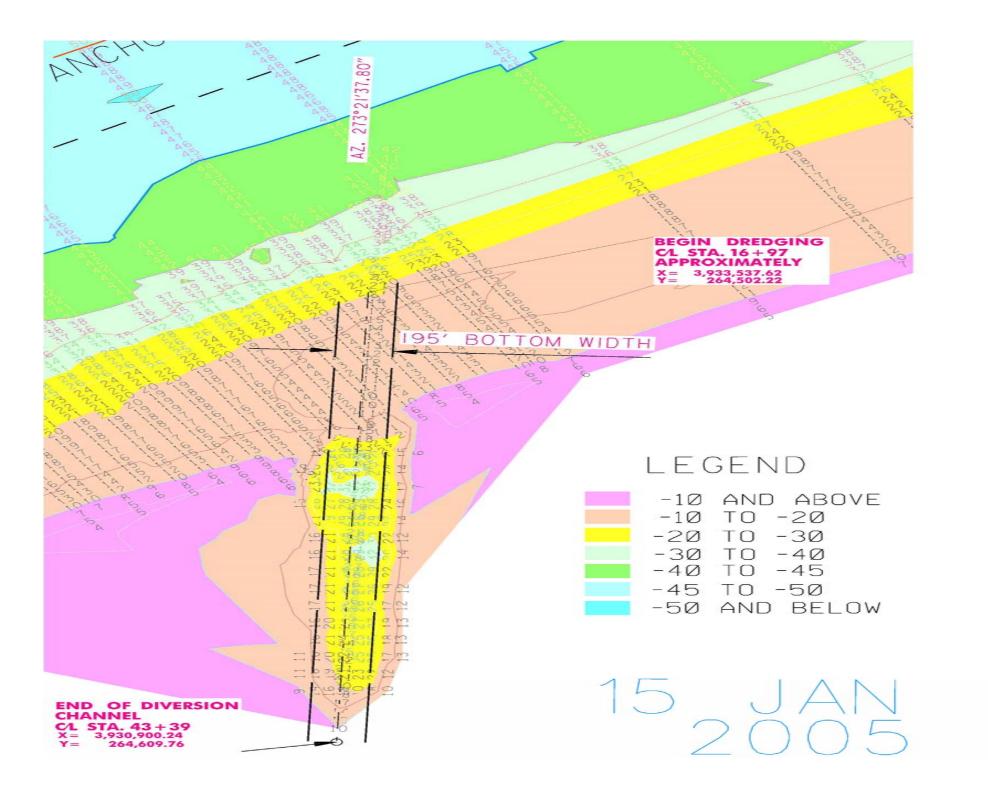
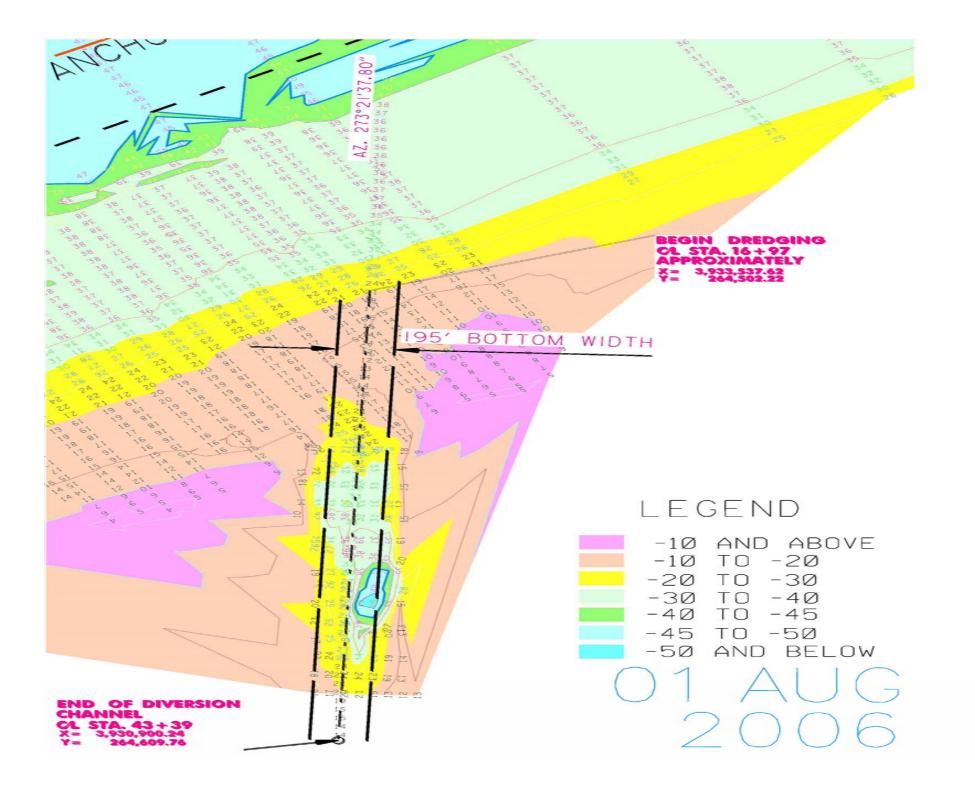
West Bay 20,000 CFS Diversion

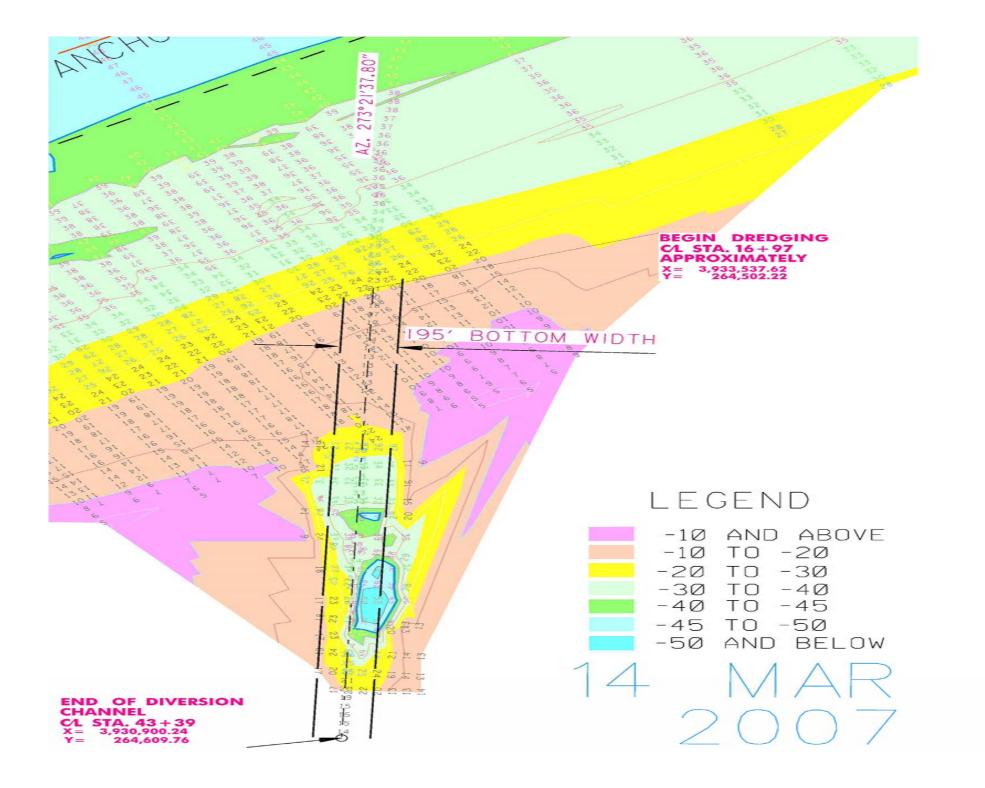
Diversion Channel Development

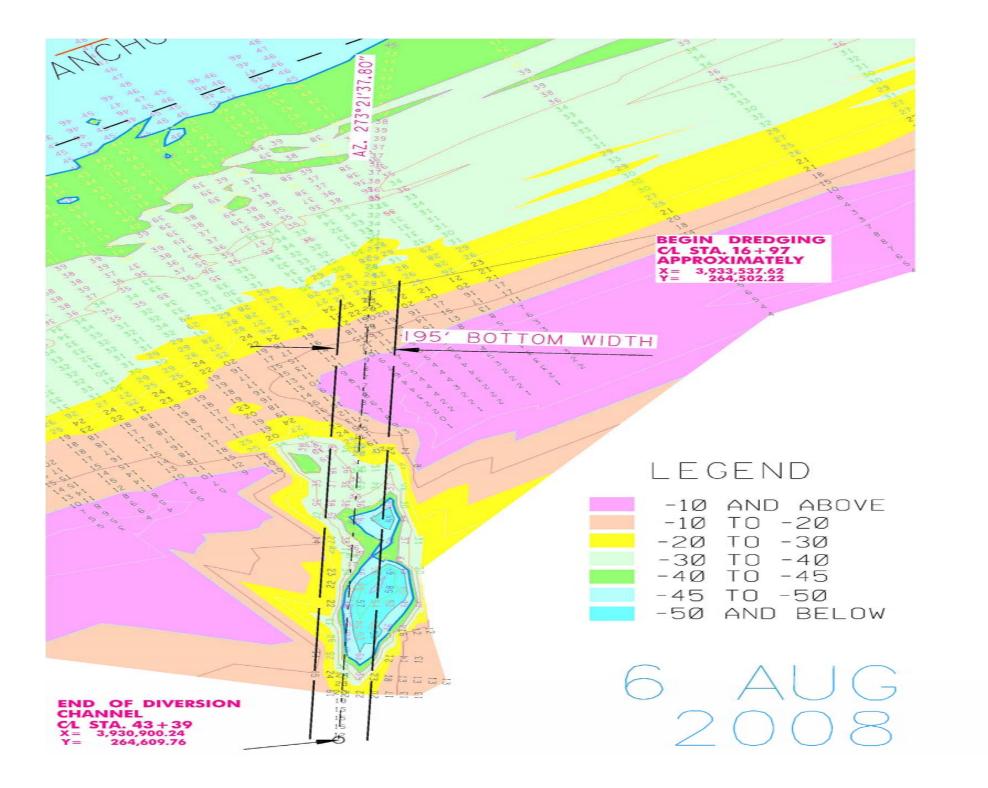


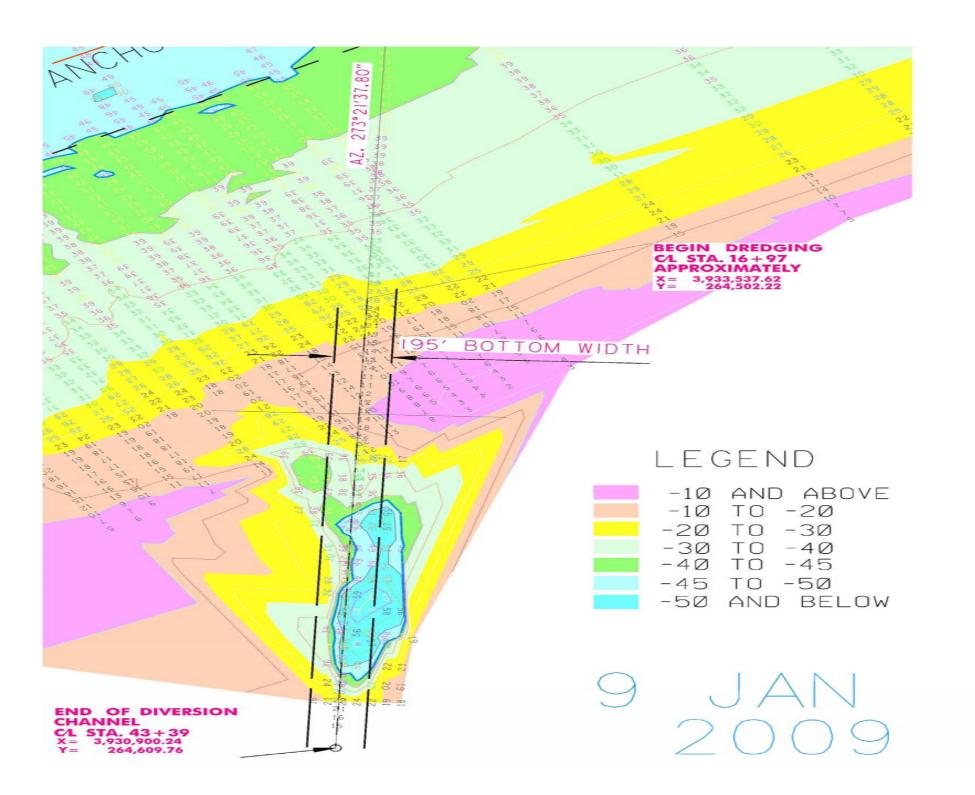


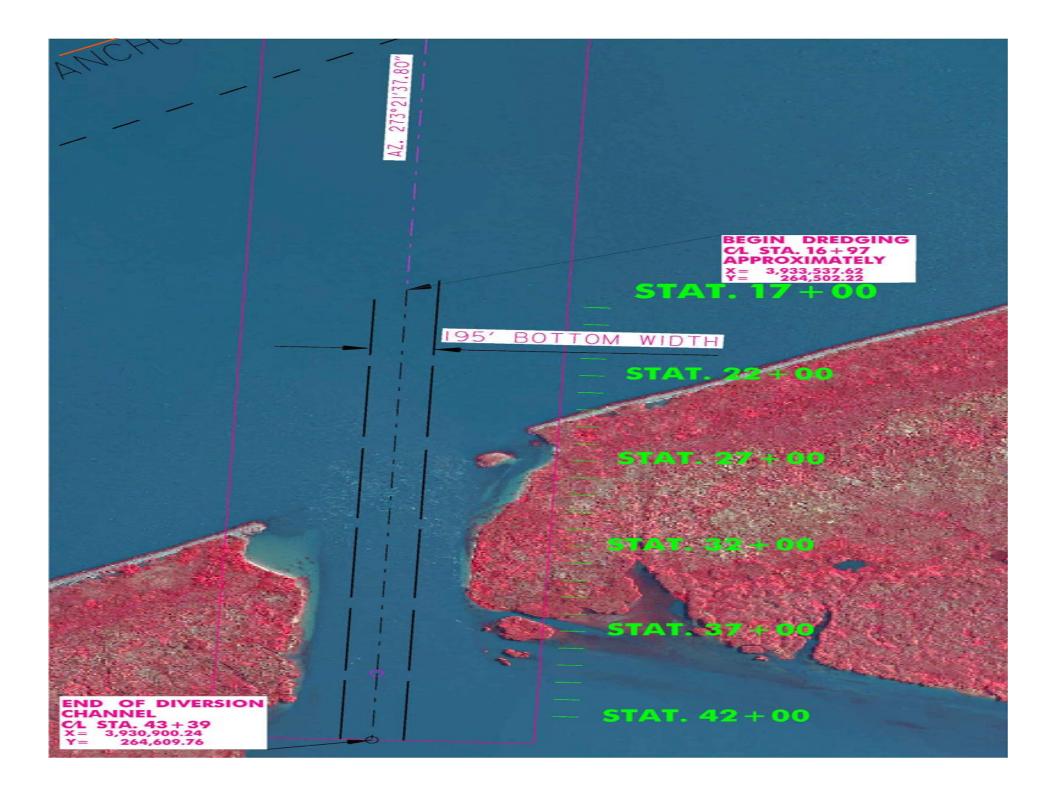


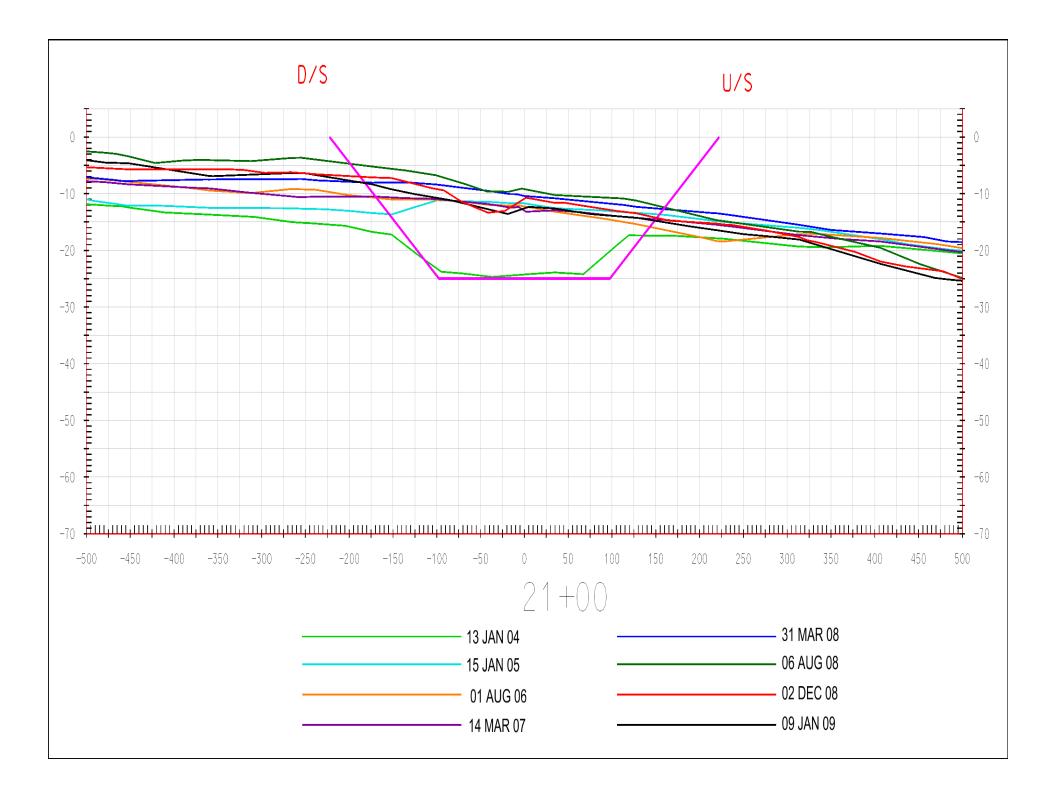


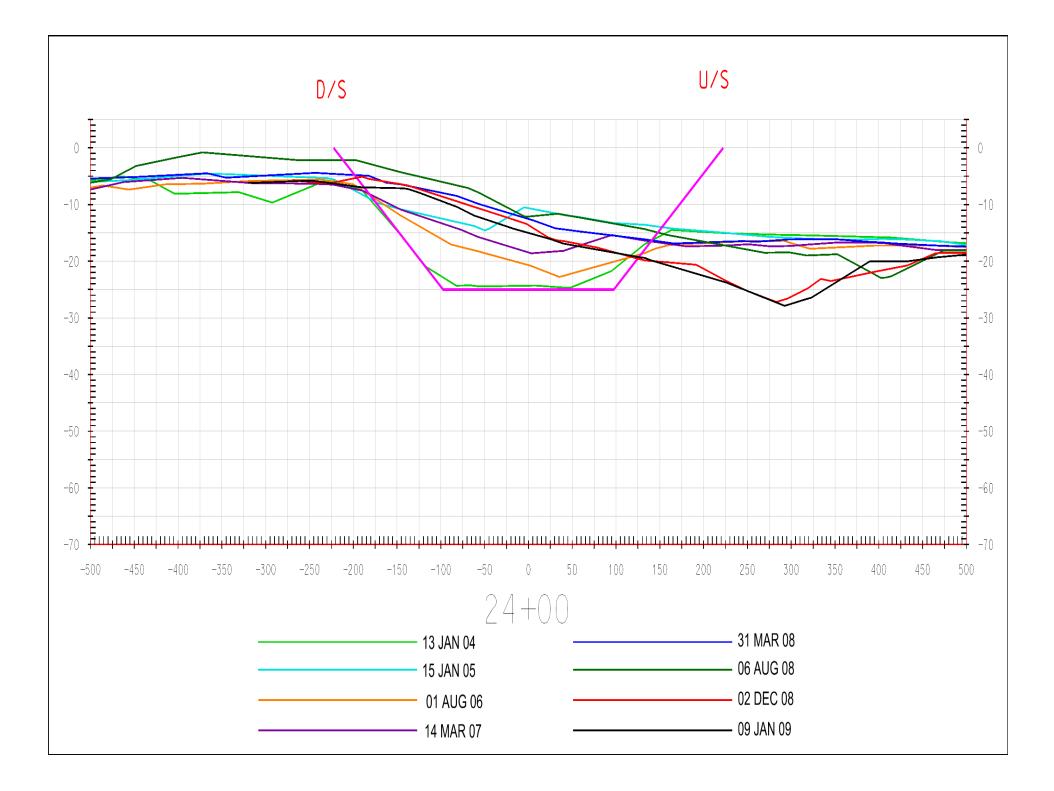


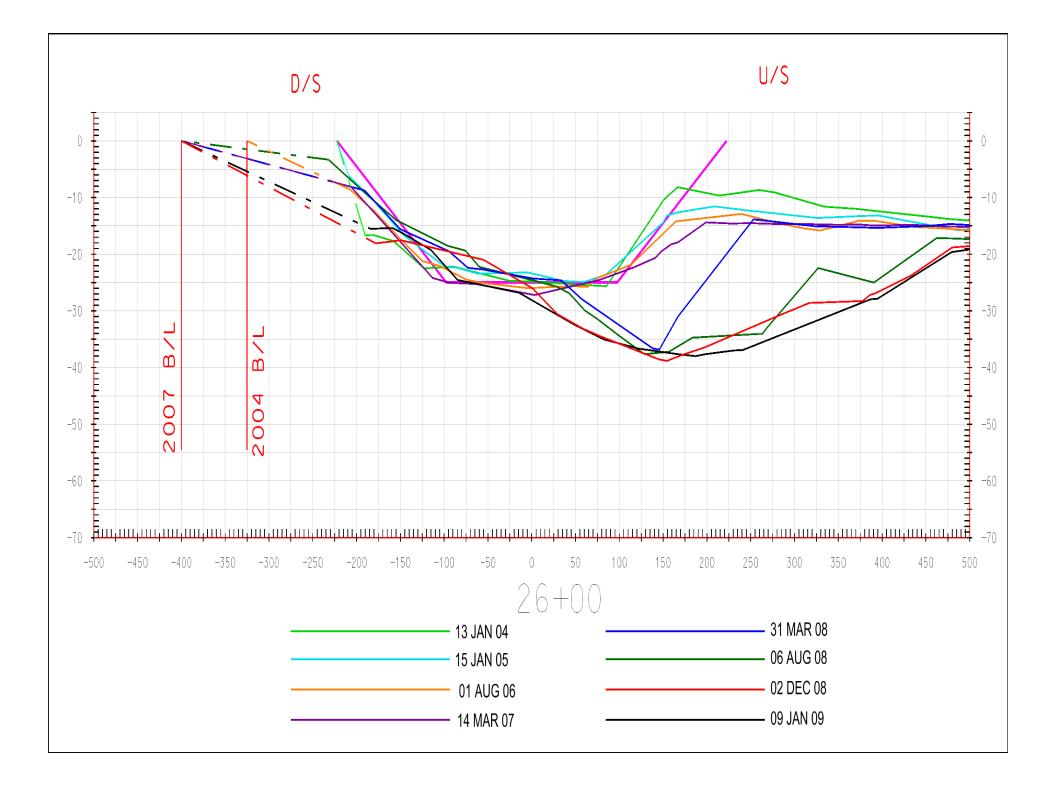


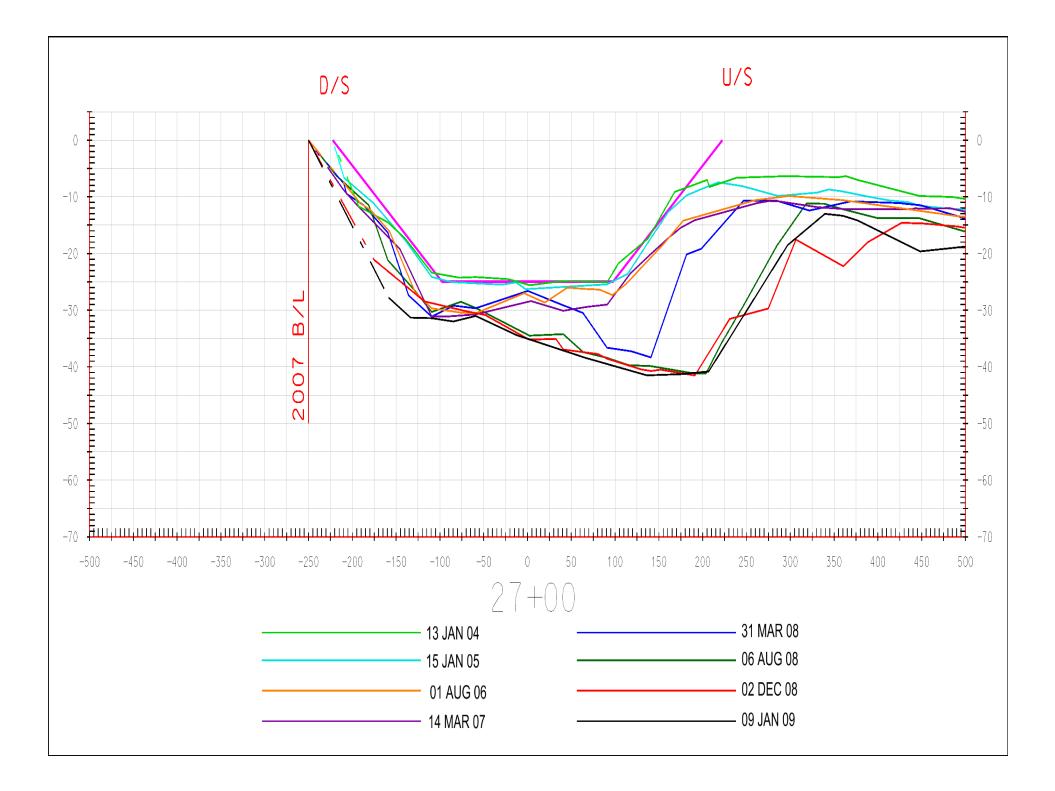


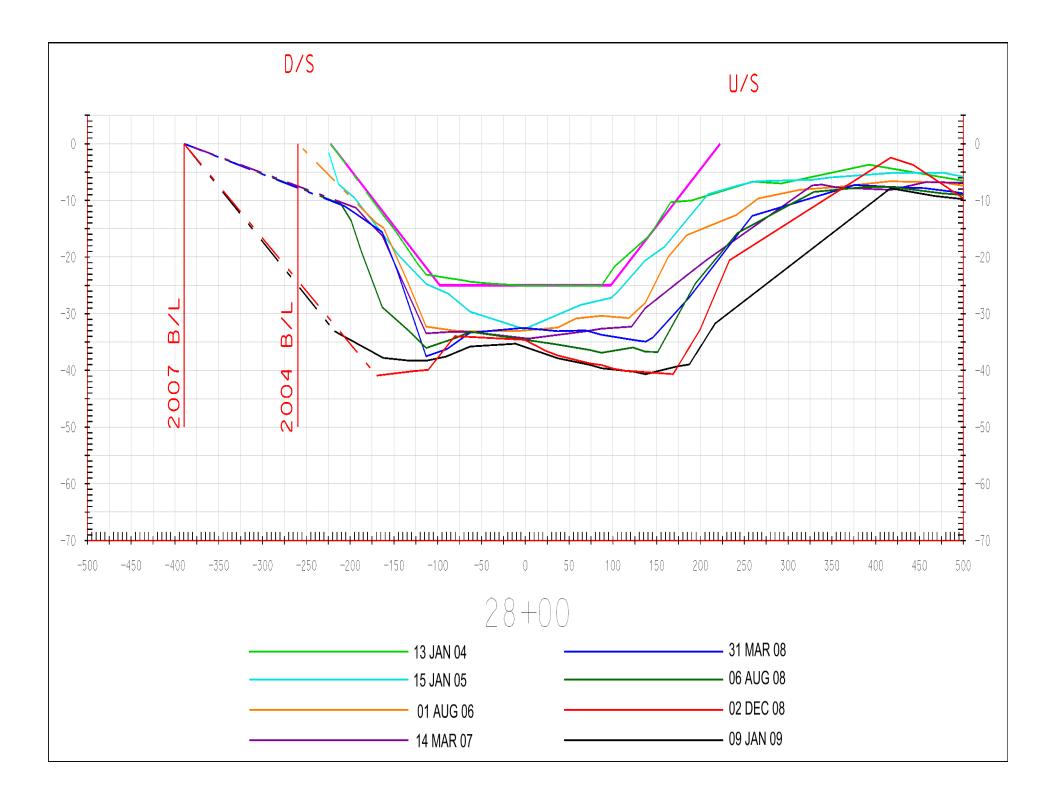


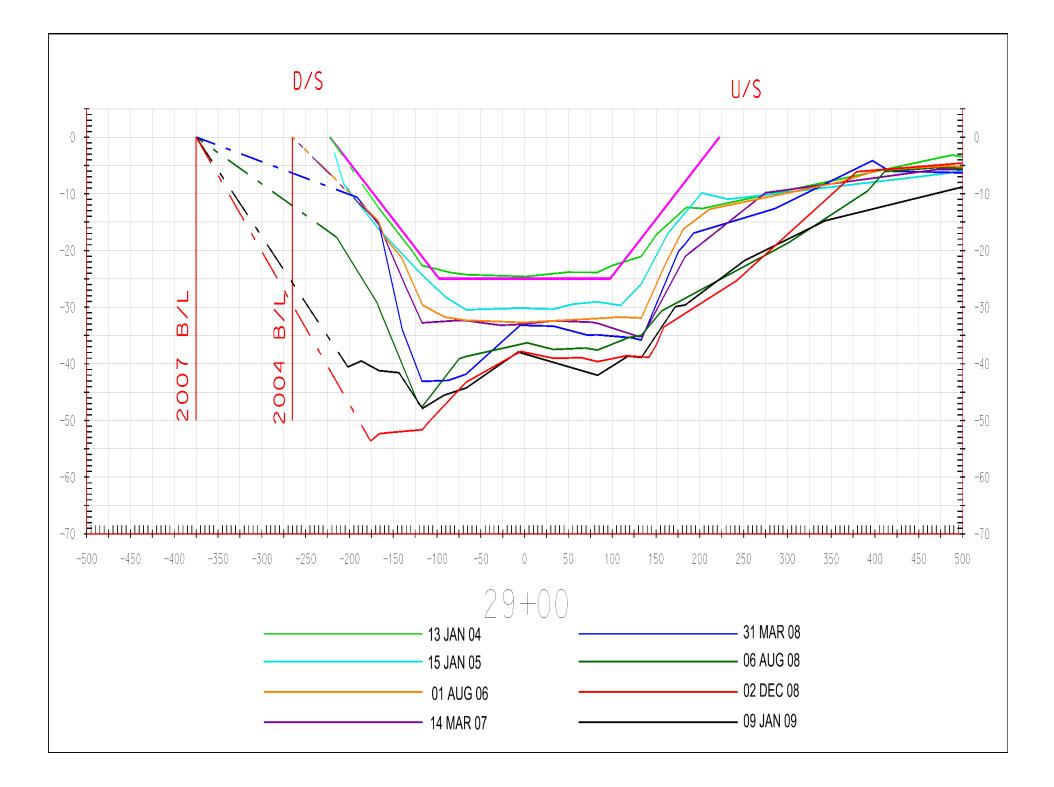


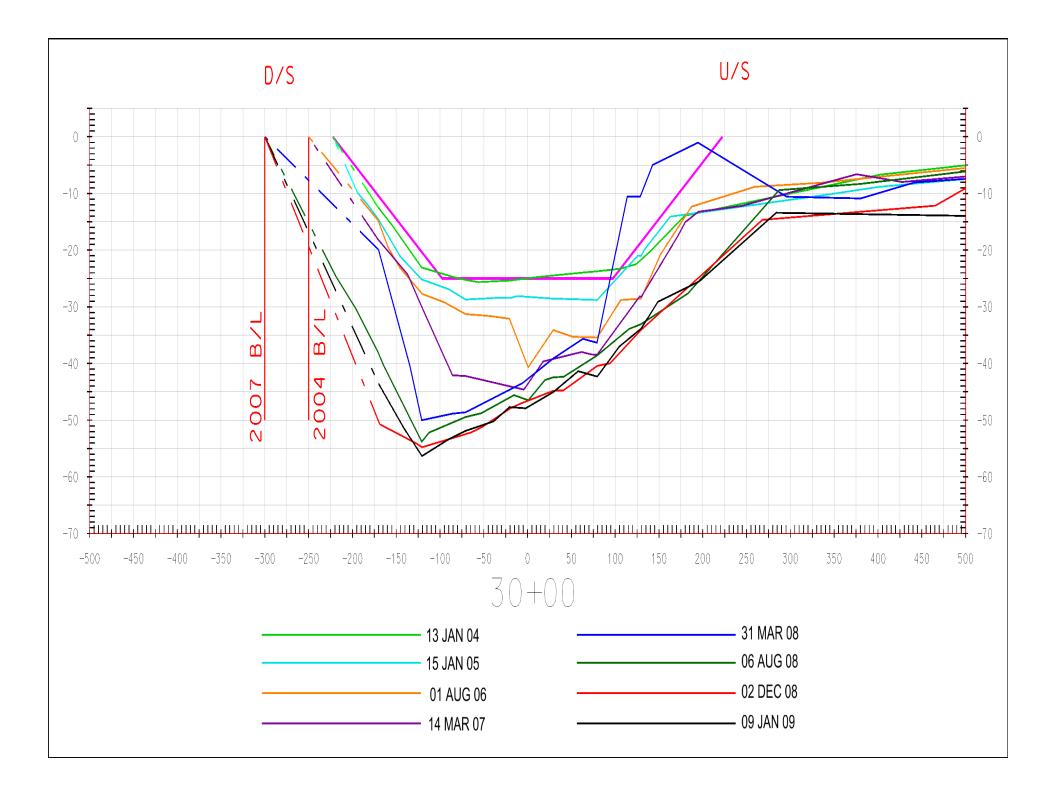


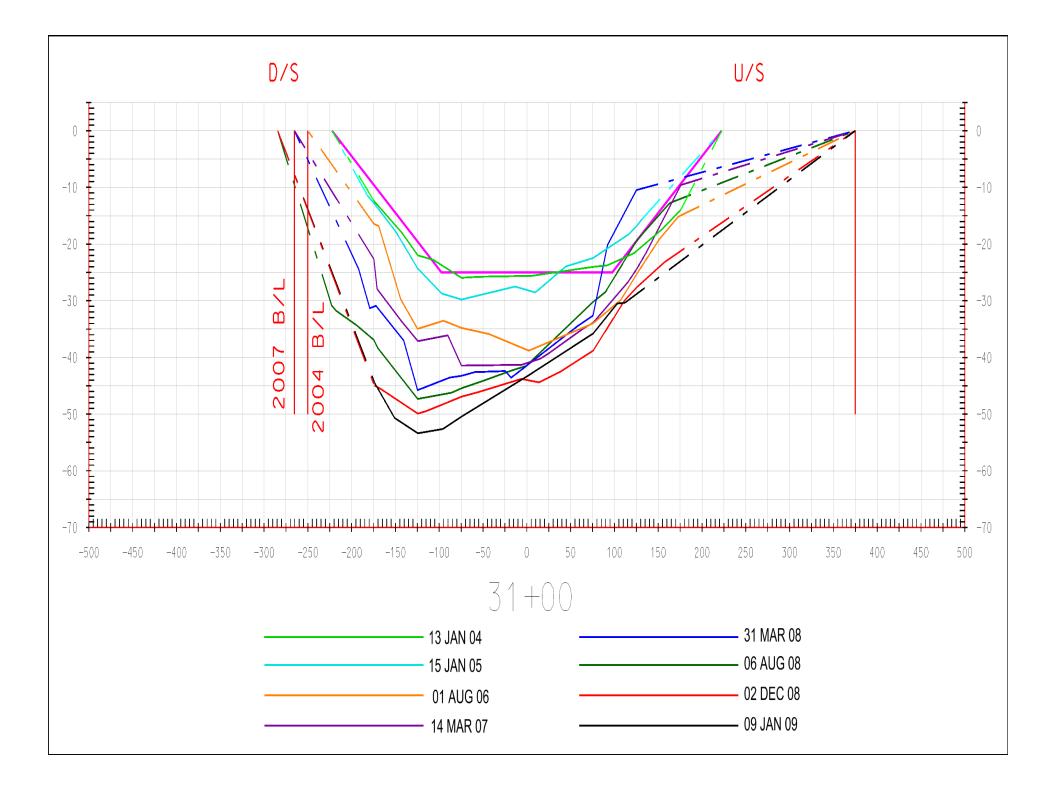


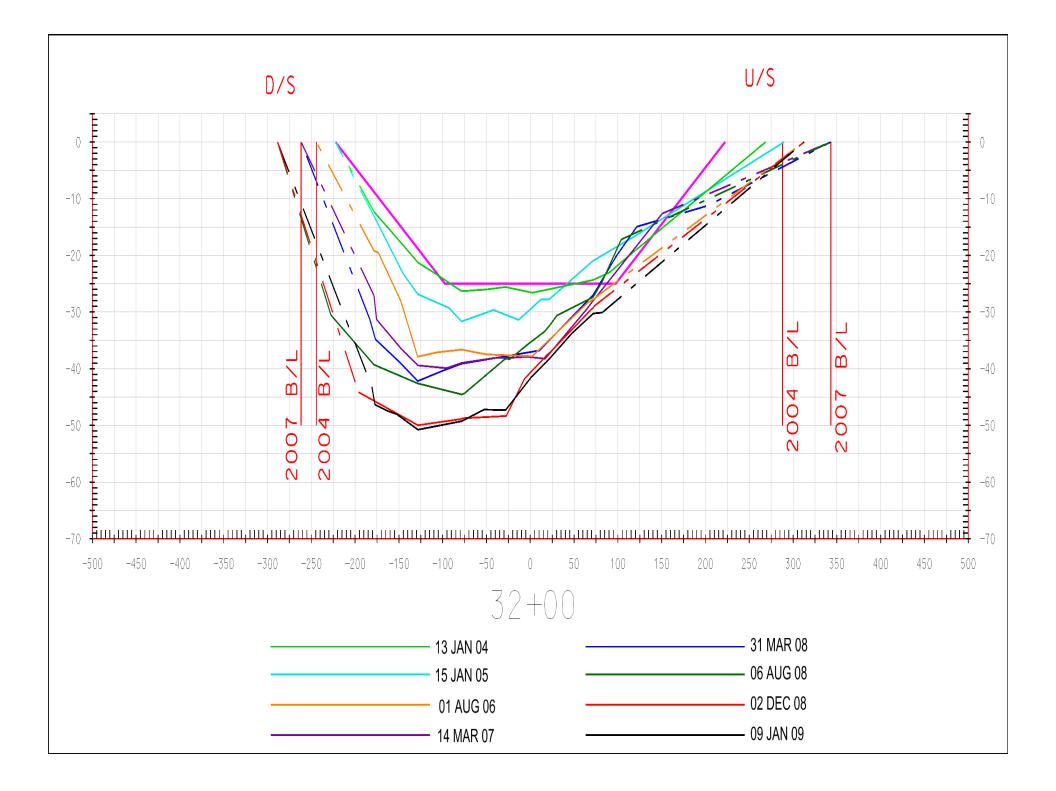


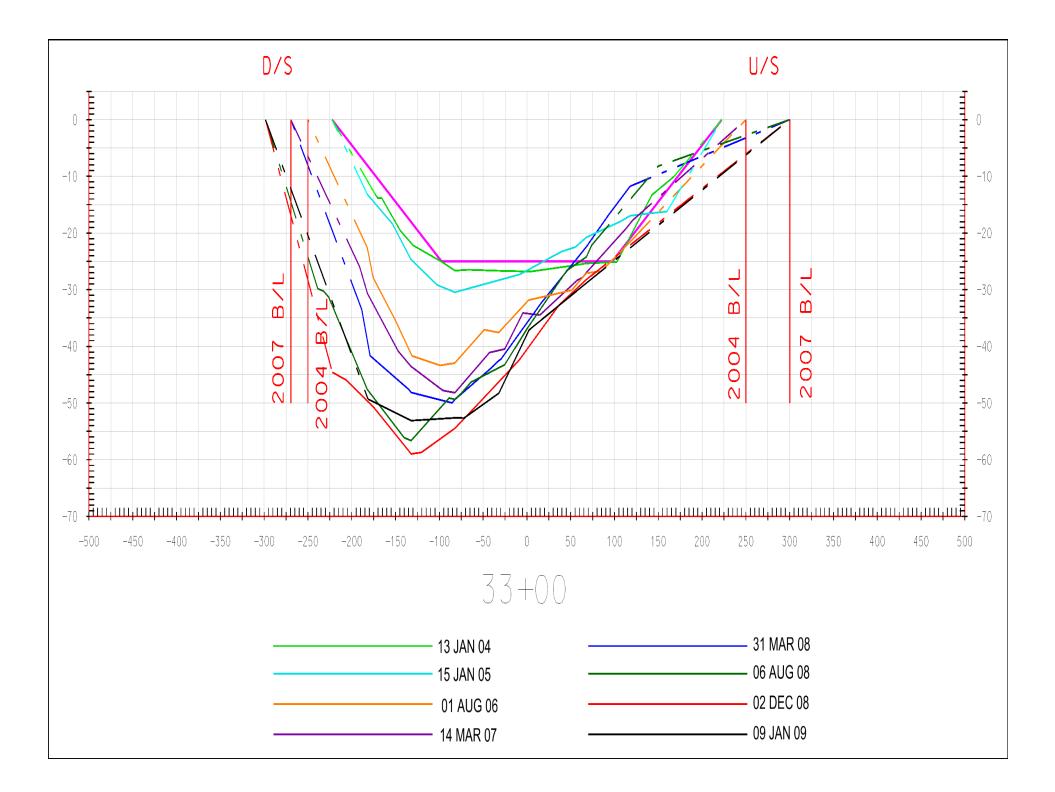


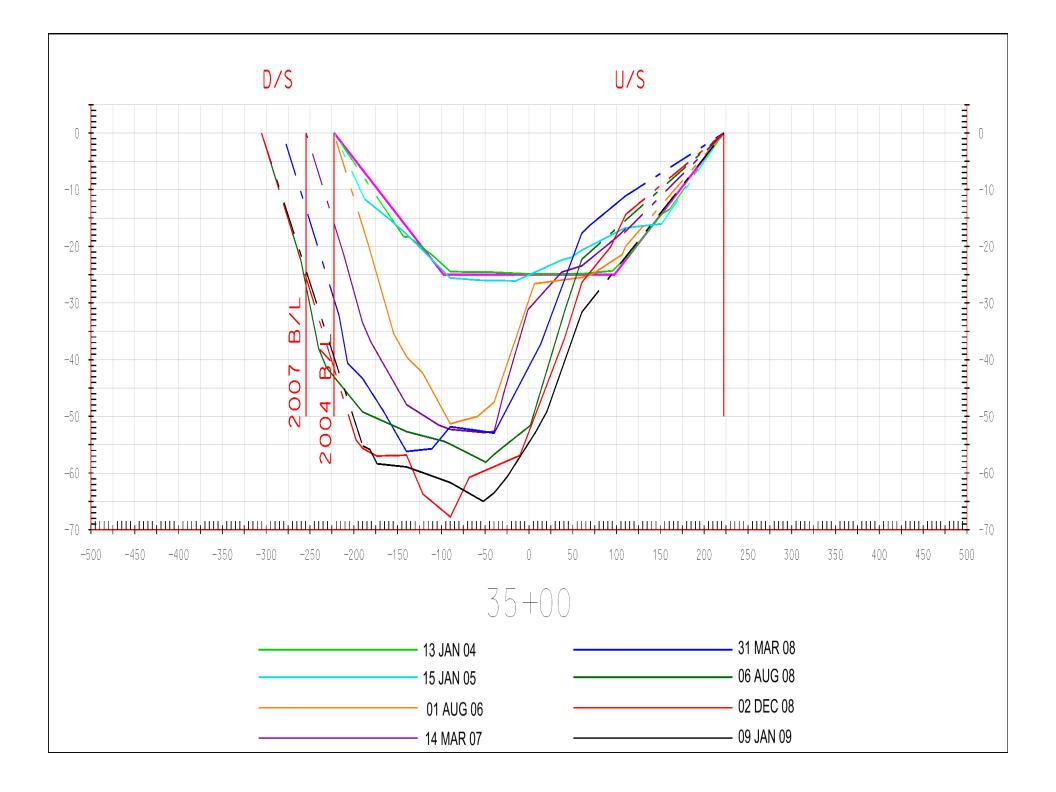


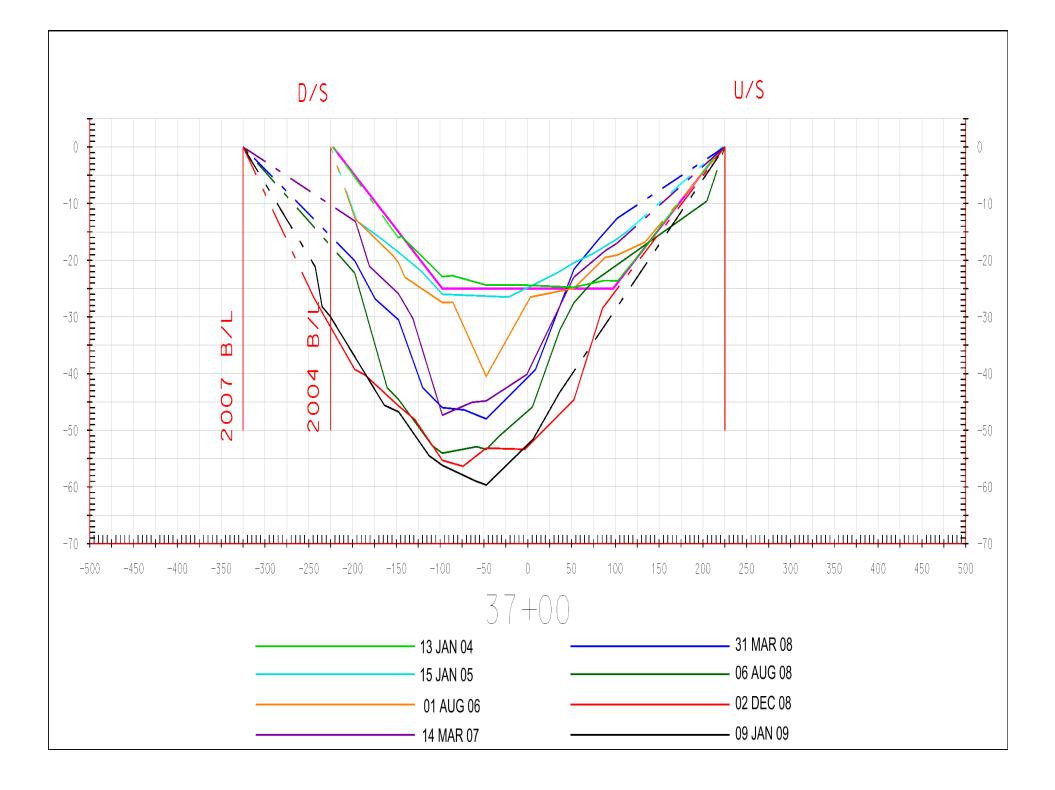


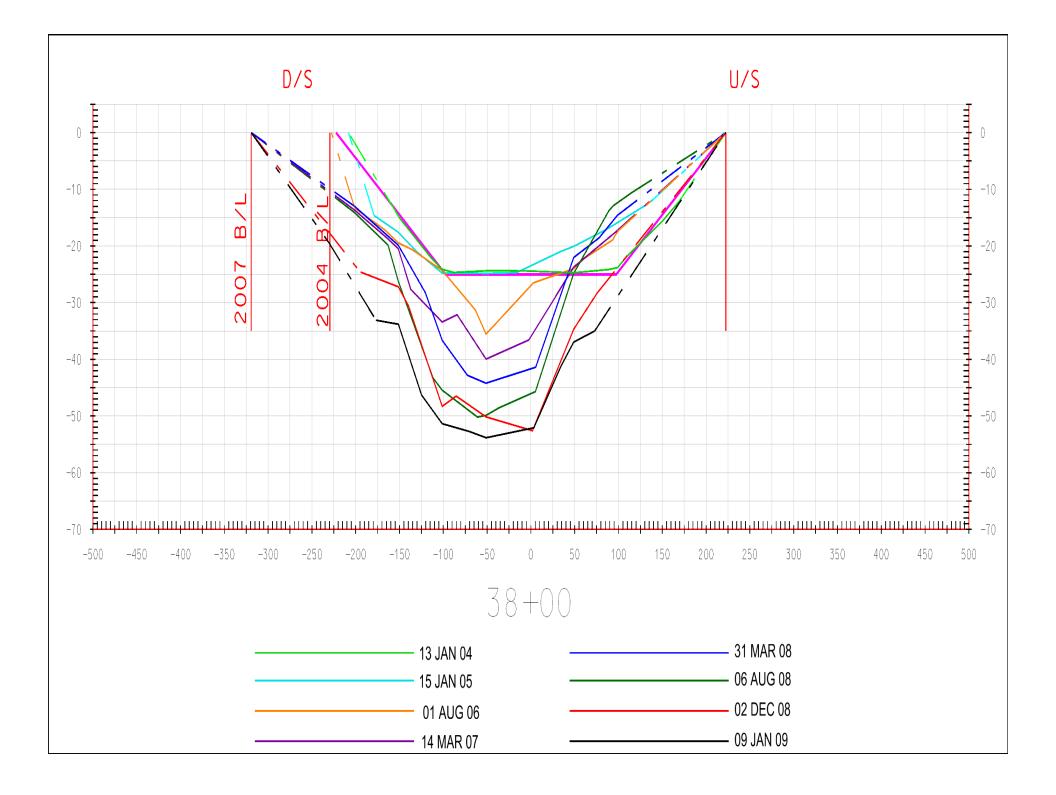


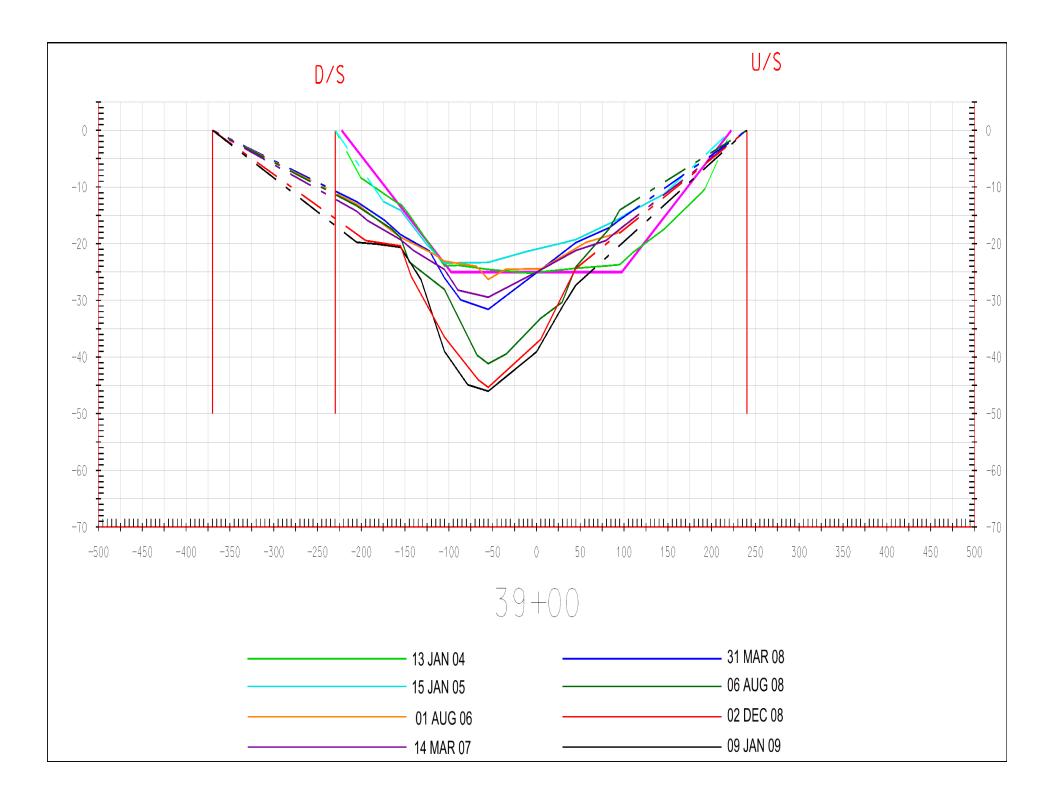


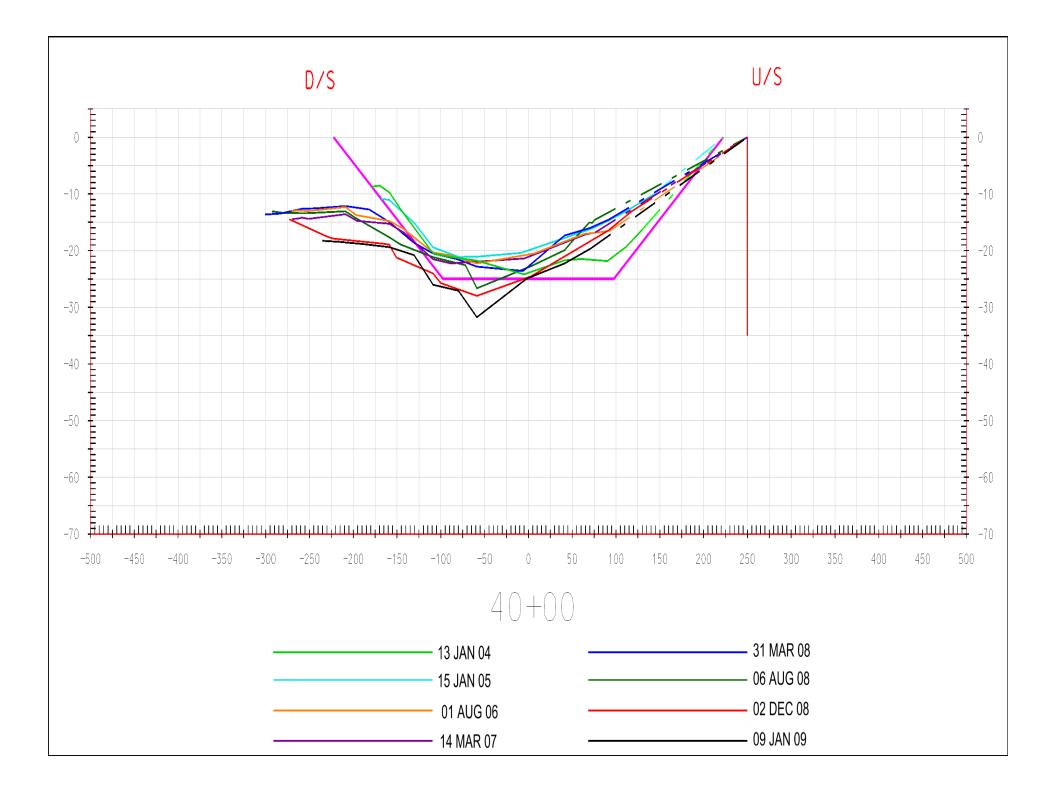


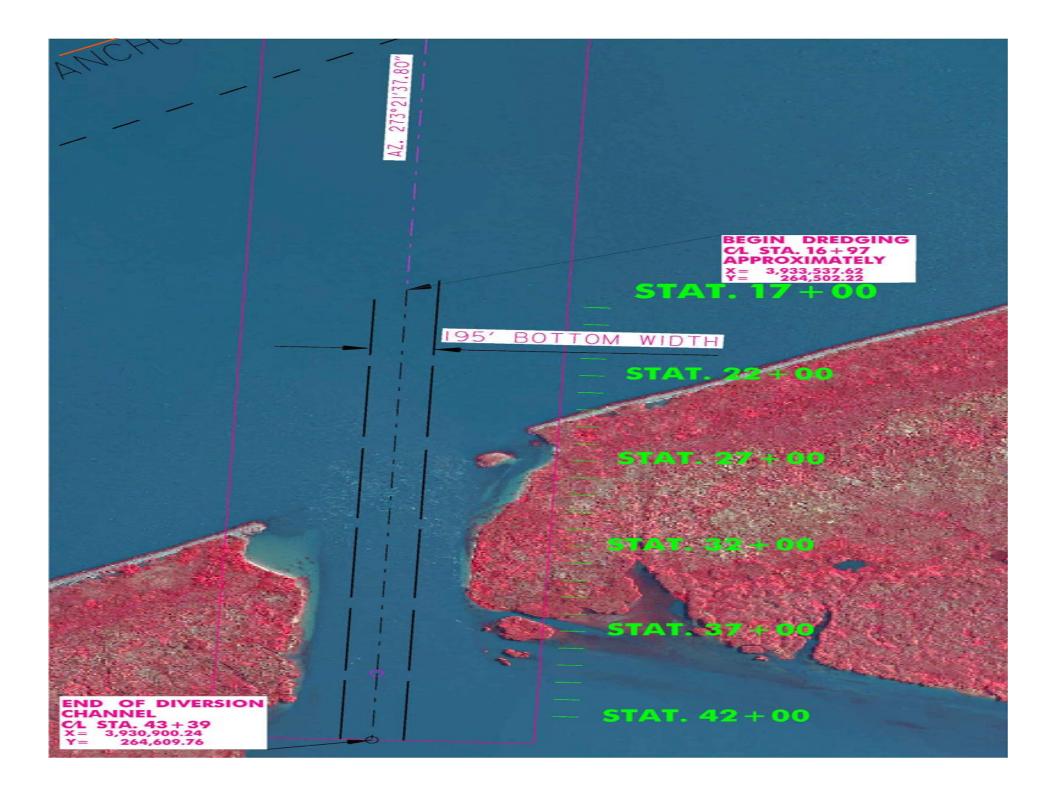












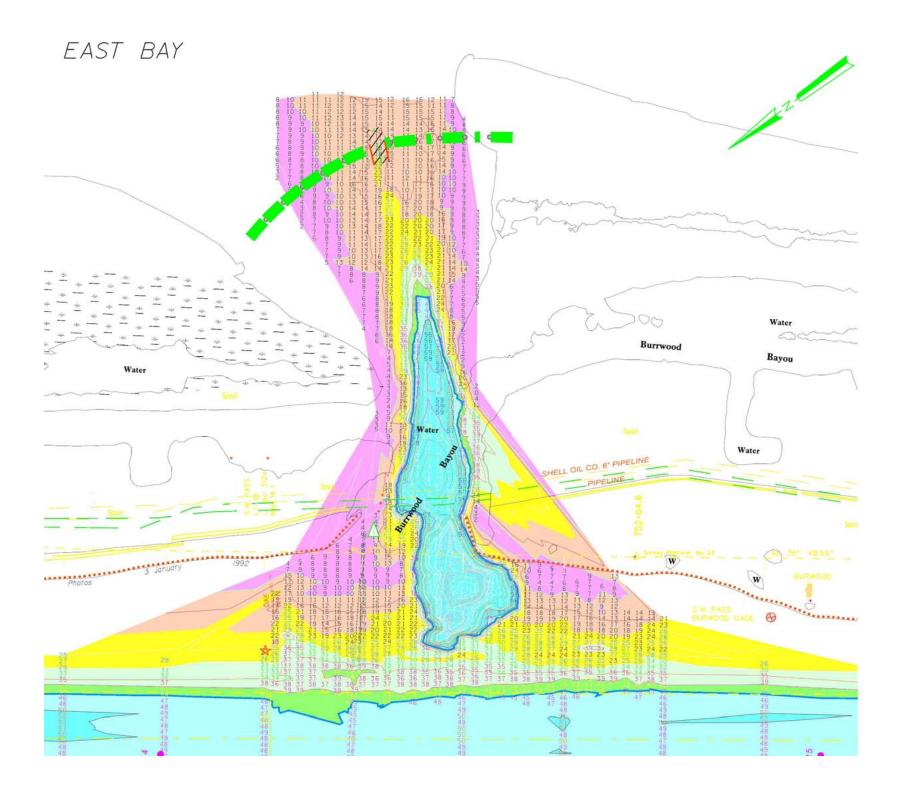
| Survey | January | January | % |
|---------|---------|---------|----------|
| Date: | 2004 | 2009 | Increase |
| Station | Area | Area | |
| 30+00 | 9,253 | 17,876 | 93% |
| 31+00 | 8,494 | 19,207 | 126% |
| 32+00 | 8,663 | 17,375 | 101% |
| 33+00 | 8,429 | 17,578 | 109% |
| 34+00 | 7,941 | 18,068 | 128% |
| 35+00 | 8,059 | 19,873 | 147% |
| 36+00 | 8,082 | 19,285 | 139% |
| 37+00 | 7,807 | 18,422 | 136% |
| 38+00 | 7,888 | 16,377 | 108% |

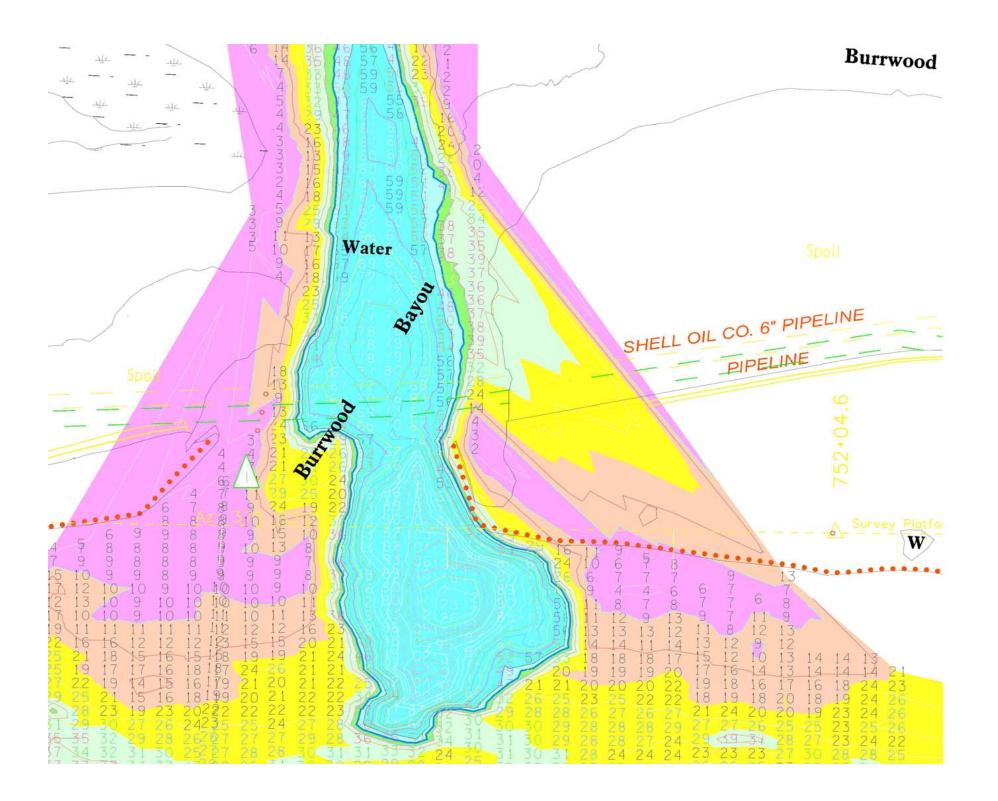
| - 30 | | | | | 30 | |
|----------------|---|---|--|--|---|---------|
| _ | | | | | - | |
| - | | | | | - | |
| - | | | | | - | |
| - | <u>B-1</u> | | B-2 | B-3 | - | |
| 0 | | | WATER | WATER | ° | |
| - | 50 6 510. W 0.51 VS0 6 8.10. W 0.51 | | 4 LE8 4 α 111111 1375 1 LV7 | VSD G SICL W/ SISA LDN: SI LAY VSD B CL V/ SI LAY. | - | |
| - | чэр са, ман за мс с эк51 м са, sa (дл. мс - sas) мс с эк31 | C G CLSI W/ FEM LEN. TR MD HST G SICL W/ SI | a | LO G CLSI W SICL ULLUL 250 | - | |
| - | MC 6 5A51 | VSD G D, W/ ST L CONC | LEN. 145 | ST 6 STCL W K0 <u>Y50 6 STCL V ST LAT</u> 135 | - | |
| - | VSD C & BR CL W/ S1 | | | HST G & BR CL W/ ALT ST LAY & LEN | - | |
| -30 | | SO BE & D CL W SO BE & C CL W | / 51 | VSD 88 A C CL V/ S1 4 180 | -30 | |
| - | VSO G CL W/ SISA LAY A LEN 165 | NST G SICL W/ SI | 1 LEN | 0 G CL N7 ALT SI LEN (18) | - | |
| _ | ST © CL W/ SISA LAY & | | | (9) | 16 | |
| - | 50 G CL W SE LAY & LEN | SD G CL W/ SI LE POC | | NO G FISA | | |
| | 50 6 C. W/ 515A LAY 8 | 3 L0 G H+FI SA | (48) | | | |
| | - ///// | NO G SISA K/ TR | (34) R DM 11111111111111111111111111111111111 | MD G CLSA | -60 | |
| - | MST 6 SICL W/ CLSI | NC G SASI W/ CL | LAY 115 | (125) | E E - E E - E E - | |
| | | | (15) | D G SISA W/ CLSA LAY | | |
| | LO G SISA WY CL LEN. LEN. 1.1.1.385 OK LO GCISA WY SASI LAY. TR ON | LD G SASI W/ SI Lay, TR DM | siel - | MD C SISA W/ SACL LAY | - 2 | |
| | LAY. THION NC C SAST K/ CL LEN | | | | | |
| | MC G CLSI W/ SA LEN | MC C CLSI W/ S | SA 990 | D G FISA | | |
| | | 5 | | | | |
| | MD G SISA W/TRION | VLO G CLSI W/ S Len. TR om | sisa | x0 G CLSA (29) | | |
| | | LEN. TR OM | | 10 G FISA | - | |
| -120 | NO G SISA W/ TR ON | NC 6 SASI W/ CLS | SI LAY (22) | | -120 | |
| - | | MC G SASI W/ CLS | | WC G CLSI W/ SISA LAY | 120 | |
| _ | | D G \$154 | (28) | | | |
| - | ST G (L K/ SI LEN & 1415 POC. (FISS) | | | C 6 (LSI W/ SISA LAY | | |
| _ | - ///// | ST G CL #/ SI | PCC 1260 | C G CLSI W/ SISA LAY | _ | |
| -150 | LO G SASJ W/ TR CL 455 | 6 - | POC 1260 POC 1350 | | -150 | |
| _ | | ST G CL W/ SI I | POC 1350 | NC C DLSI W/ SISA LAY | _ | |
| _ | | | | | _ | |
| _ | | | | | _ | |
| - | <u>Strata symbols</u> | 770 blab plasticity | Poorly graded sand | Clayey sand | _ | |
| -180 | | high plasticity clay | Poorly graded sand | 8333 | -180 | |
| | Silty low plasticity clay | Clayey silt | Silty sand | Sandy silt | | |
| | | | ROF | (RER) | | |
| CTDATU | | | | | | |
| STRATUM NO. | | LEGEND | | | EUSTIS ENGINEERING | C COMPA |
| ① VE | RY SOFT TO STIFF GRAY OR GRAY AND BROWN | CLAY AND SILTY CLAY | | | | |
| | OSE TO COMPACT GRAY SANDY SILT AND CLAYE | | STIFF GRAY OR GRAY AND BROWN SIL | TY CLAY | 3011 28TH STREET | M |
| | RY SOFT TO MEDIUM STIFF GRAY OR GRAY AND | | | | | |
| | RY LOOSE TO MEDIUM DENSE GRAY SAND AND S | SILTY SAND | | | SUBSOIL PRO | |
| | DSE TO DENSE GRAY SAND, SILTY SAND AND (| CLAYEY SAND INTERSPERSED WITH VE | ERY LODSE TO MEDILUM COMPACT GRAY | SANDY STIT AND CLAYEY STIT | CHEVRONTE) DIRECTIONAL DR MISSISSIPPI RIVER VICINITY OF VENICE | XACO |

DRAWN BY: D. LAFONT PLOT DATE: 19 JUNE 02 CADD FILE: FIGURE 2.00N CHECKED BY: J.R.E. JOB NO.: 17413 FIGURE 2

NOTE: NUMBER TO RIGHT OF BORING LOG INDICATES COHESION IN PSF. NUMBERS IN PARENTHESES INDICATE RESULTS OF STANDARD PENETRATION TEST.

Closure ?





BURRWOOD BAYOU FLOW IN CFS

| Date | Mississippi River | SW Pass | SW Pass | Burrwood | Percent | |
|-------------------|--------------------|----------------|----------------|----------|---------|----------|
| | at Tarbert Landing | above Burrwood | below Burrwood | Bayou | SW Pass | |
| | (2 day lag) | Bayou | Bayou | (C - D) | (E/C) | |
| March 15, 2003 | 950,000 | 223,000 | 139,000 | 84,000 | 37.7% | |
| April 15, 2003 | 456,000 | 118,000 | 73,500 | 44,500 | 37.7% | |
| May 13, 2003 | 524,000 | 156,000 | 95,800 | 60,200 | 38.6% | |
| June 21, 2003 | 614,000 | 190,000 | 95,800 | 94,200 | 49.6% | |
| July 19, 2003 | 367,000 | 81,400 | 51,300 | 30,100 | 37.0% | |
| September 9, 2003 | 236,000 | 85,100 | 58,700 | 26,400 | 31.0% | note 1 |
| January 16, 2004 | 574,000 | 93,700 | 48,000 | 45,700 | 48.8% | note 2 |
| April 16, 2004 | 575,000 | 176,000 | 110,000 | 66,000 | 37.5% | note 3 |
| May 12, 2004 | 700,000 | 120,000 | 99,600 | 24,900 | 20.8% | note 4 |
| June 23, 2004 | 835,000 | 154,000 | 137,000 | 18,500 | 12.0% | note 4/5 |
| August 4, 2004 | 383,000 | 83,000 | 64,300 | 14,600 | 17.6% | note 4 |

note 1 - falling tide

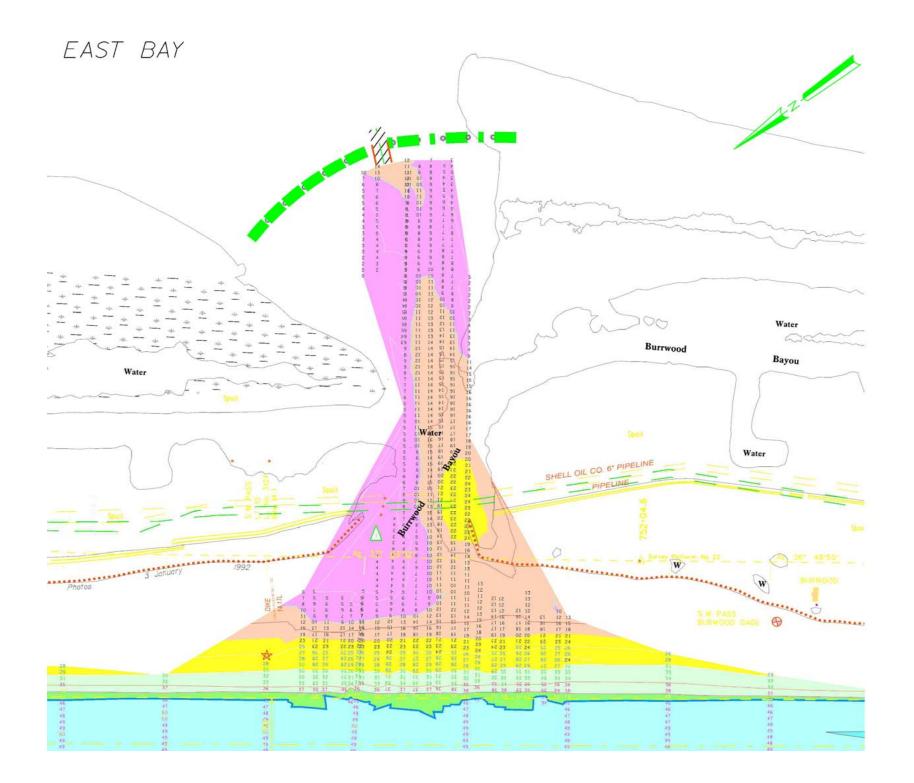
note 2 - GPS problems, bottom tracking used, measurements may be affected

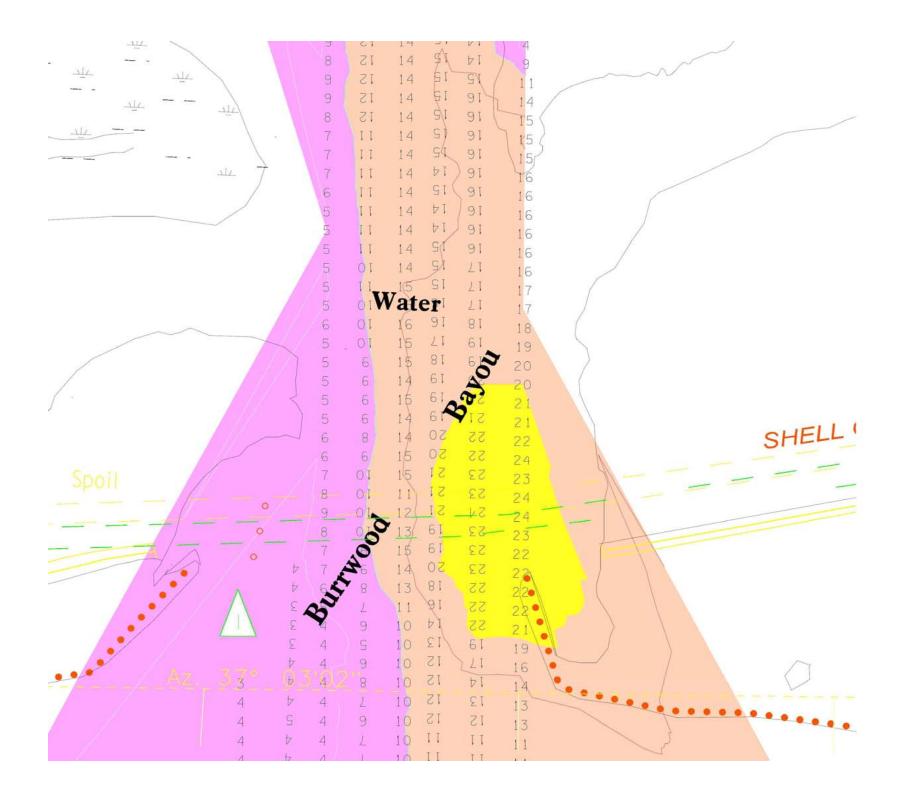
note 3 - Placement of Stone Commenced 15 April 2004

note 4 - actual measurement in Burrwood Bayou

note 5 - Stone closure dike contract completed 29 May 2004







| and the second se | | | | | | | | | |
|--|-------|----|----|-----|-----|----|---|---------------------|--|
| and the second s | | 14 | | /10 | | 9 | | 3 | |
| | 15 | 5 | 11 | 11 | 10 | 9 | 6 | 3 | |
| 10 | 14 | 15 | 11 | 11 | 10 | 9 | 6 | 3 | |
| 9 | 12 | 14 | 11 | 10 | 10 | 9 | 6 | 3 | |
| 8 | 11 | 13 | 11 | 10 | 10 | 10 | 6 | 3 | |
| 8 | 10 | 11 | 11 | 10 | 10 | 9 | 6 | 6 | |
| 8 | 8 | 10 | 10 | 10 | 10 | 9 | 5 | 5 | |
| 7 | 7 | 10 | 10 | 10 | 10 | 10 | 6 | 5 | |
| 6 | 7 | 10 | 10 | 10 | 8 | 9 | 6 | 5 | |
| 5 | 7 | 9 | 10 | 9 | 9 | 9 | 6 | $\langle 4 \rangle$ | |
| 5 | 7 | 9 | 10 | 9 | 9 | 9 | 7 | 4 | |
| | 7 | 9 | 10 | 9 | 9 | 9 | 7 | 5 | |
| 4 | 7 | 8 | 11 | 9 | 9 | 9 | 7 | 4 | |
| 4 | 6 | 8 | 12 | 9 | 10 | 9 | 7 | 4 | |
| 4 | 6 | 8 | 12 | 11 | 710 | 8 | 7 | 4 | |
| 3 | 6 | 8 | 12 | 11 | 9 | 8 | 8 | 4 | |
| 3 | 6 | 8 | 12 | 12 | 10 | 8 | 8 | 4 | |
| 3 | 6 | 8 | 13 | 13 | 12 | 8 | 8 | 5 | |
| 3 | 6 | 8 | 12 | 14 | 12 | 8 | 8 | 4 | |
| 3 | | 8 | 12 | 13 | 13 | 9 | 7 | 3 | |
| 3 | 5 5 4 | 8 | 12 | 14 | 13 | 9 | 7 | 3 | |
| 3 | A | 7 | 13 | 14 | 14 | 10 | 6 | | |

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