

Geotechnical Engineering Report

South Grand Chenier—Baker Marsh Creation (ME-32)
Cameron Parish, Louisiana

for

ECM + MRD Joint Venture

May 10, 2023

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File No. 10883-026-00

May 10, 2023

Prepared for:

ECM + MRD Joint Venture
1301 Clearview Parkway, Suite 200
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1.0 INTRODUCTION AND PROJECT UNDERSTANDING

GeoEngineers, Inc. (GeoEngineers) is pleased to present this geotechnical engineering report to the ECM + MRD Joint Venture (ECM + MRD) and the U.S. Department of Agriculture, Natural Resources Conservation Service (NRCS) in support of the South Grand Chenier – Baker Marsh Creation Project ME-32 (Project) located in Cameron Parish, Louisiana. Our services were completed under an Agreement between Consultant and Subconsultant dated August 18, 2022, between ECM + MRD and GeoEngineers.

Our understanding of the project is based on the information provided by NRCS and our July 26, 2022, proposal. The objective of the Project is to create and nourish approximately 420 acres of marsh using hydraulically dredged fill from an offshore borrow source located in the Gulf of Mexico. This fill material will be placed in a designated marsh creation area formed by constructing earthen containment dikes around the perimeter. The project site is shown in the Vicinity Map, Figure 1.

All elevations described in this report, including figures and appendices, are referenced to the North American Vertical Datum of 1988 (NAVD88), Geoid 12A. Report figures are located at the end of the report text. Appendices are organized as shown in the Table of Contents.

2.0 SITE CONDITIONS

2.1. Surface Conditions

2.1.1. Marsh Creation Area

The marsh creation area is primarily open water with some fragmented marsh as shown in Marsh Creation Area Boring and CPT Locations, Figure 2a. Based on Coastwide Reference Monitoring System (CRMS) station 614-H01, the mean water level in the area is approximately elevation 0.7 feet (El. 0.7 ft.). Based on survey information collected by Fugro, we calculated an average mudline of El. -0.93 ft. with a standard deviation of 0.566 ft. Water depths will vary based on the time of year, the direction of wind and tidal fluctuations.

2.1.2. Borrow Area

The planned borrow area is located approximately 2 miles offshore in the Gulf of Mexico (Figure 2b) approximately south of the marsh creation area as shown in Figure 1. Mudline elevations were not taken for the borrow area, but the water depth at the time of sample collection was approximately 23 feet.

2.2. Subsurface Conditions

Subsurface conditions discussed below are based on six soil borings and 13 cone penetration test (CPT) soundings in the marsh creation area, and six vibracores in the borrow area. Soil borings and CPTs were completed between October 12 and 15, 2022, and vibracores were completed on November 2, 2022. Field reports of sampling events are included in Appendix A. No artifacts or material other than that noted on the logs included in Appendices B, C and D were observed by GeoEngineers during our field investigation or during laboratory testing; however, GeoEngineers personnel are not trained in recognition of such items. Detailed laboratory test results are included in Appendix E.

Subsurface cross-sections based on the investigations are shown in Figures 3a through 3c. Although undetected anomalies (sand layers, wood debris, etc.) beyond the locations of our explorations may exist, the generalized subsurface conditions can be described as given in the following sections.

2.2.1. Marsh Creation Area

Site soil conditions were fairly uniform. Very soft gray clay was present from the mudline to approximately El. -19 ft. to El. -26 ft.. Below the very soft clay, stiff to very stiff clay was present, which appears to be consistent with Pleistocene Age overconsolidated deposits. Figures 3a and 3b present subsurface soil cross-sections through the marsh fill area.

2.2.2. Borrow Area

In the borrow area, very soft gray clay with a moisture content greater than 70 percent was typically encountered from the mudline to a depth of 9 to 12 feet below the mudline. Below this, stiff tan and gray clay, typically with ferrous or calcareous nodules and a significantly lower moisture content was present. We believe this underlying stiffer clay is Pleistocene Age overconsolidated deposits. Shell was observed in soil samples at the transition from overlying very soft clay to stiffer Pleistocene Age clay. Figure 3c shows a subsurface cross section through the borrow area.

3.0 CONCLUSIONS AND RECOMMENDATIONS

GeoEngineers evaluated various geotechnical data to develop engineering recommendations for the project. Our analyses focused on stability and bearing capacity of earthen containment dikes and settlement of the project features. Our results, conclusions and recommendations are described in the following sections.

3.1. Design Parameters

Design moisture content, unit weight and shear strength parameters were developed for the marsh creation area based on the borings and CPTs as shown in Marsh Creation Area Design Profile, Figure 4. Elevations and other information used in our calculations are summarized below, and sources are identified in Appendix F. Design settlement parameters are included in Appendix H.

- Design mudline elevation = El. -0.93 ft.
- Target long-term marsh elevation = El. 0.8 ft.
- Mean high water = El. 1.09 ft.
- Mean water = El. 0.74 ft.
- Mean low water = El. 0.3 ft.
- Sea level rise = 0.026 ft/year
- Subsidence = 4.3 mm/year
- Accretion = 2.5 mm/year (starting year 6)
- Min. mudline for 95% confidence interval range = El. -2.06 ft.
- Max. mudline for 95% confidence interval range = El +0.21 ft.
- Hydraulic fill placement duration = 25 days.

3.2. Earthen Containment Dikes

Our analyses for the earthen containment dikes (ECDs) included evaluating slope stability, bearing capacity, settlement and cut-to-fill. Our containment dike analysis results are presented below and discussed further in Appendices G and H. The recommended ECD design section is shown in Figure 5.

3.2.1. Recommended Dike Sections

ECD geometry included a 5-foot-wide crown at El. +4 ft., and side slopes of 4 horizontal to 1 vertical (4H:1V) were evaluated for stability of the ECD. A bench width of 35 feet between the toe of the ECD and the edge of the borrow channel is required. The preferential failure for ECDs at this site is from the dike through soft soil 5 to 15 feet below the mudline into the borrow channel. Shortening of the bench width or steepening the 2H:1V side slopes assumed for the borrow channel will likely cause the ECD to fail into the borrow channel.

The designer and contractor must understand that ECD constructability is a function of construction methods. The construction considerations section of this report must be followed to provide the best chance for ECD stability. Even so, soil conditions are variable and localized problems are always a possibility.

We understand a marsh creation area was constructed adjacent to the southern edge of this proposed project, and south of CPT location C-6, there were some ECD stability issues. Interestingly enough, as shown in Figure 4, C-6 appears to show a shear strength profile that is consistently weaker than the rest of the soil borings and CPTs. Construction sequencing to address construction considerations are recommended in this area.

3.2.2. Slope Stability and Bearing Capacity

Stability of the containment dikes was evaluated assuming mean low water conditions (El. +0.3 ft.). It was assumed the material for the dikes would be dredged from an adjacent borrow channel within the marsh creation cells. The critical case for this project was failure of the ECD into the borrow channel, and we increased the bench width to 35 feet to maintain an adequate factor of safety. The borrow channel was assumed to extend to El. -10 feet and be dredged with side slopes of 2H:1V (Case 2 in Table 3-1). We also evaluated a borrow channel excavated to El. -15 ft. (Case 2a in Table 3-1) and found the factor of safety to be very similar. It will be important for the contractor to maintain the required bench width and borrow channel slope to maintain ECD stability.

The results of our slope stability and bearing capacity analyses for the recommended containment dike sections are summarized below in Table 3-1. A discussion of our slope stability and bearing capacity evaluations is provided in Appendix G. Figures of the critical failure surfaces for each case presented in Table 3-1 below are also included in Appendix G.

TABLE 3-1. CONTAINMENT DIKE SLOPE STABILITY AND BEARING

Design Mudline El. (ft)	Critical Slope Safety Factor					Bearing
	Case 1	Case 2	Case 2a	Case 3	Case 4	
-0.93	1.38	1.23	1.22	1.35	1.37	1.56

Notes:

Case 1 = Internal failure of the containment dike, no marsh fill placed.

Case 2 = Global failure of the containment dike into the borrow channel, no marsh fill placed.

Case 2a = Global failure of the containment dike into a deeper borrow channel, no marsh fill placed.

Case 3 = Failure of the borrow channel, no marsh fill placed, construction equipment modeled.

Case 4 = Failure of the containment dike, marsh fill placed.

The critical factors of safety presented in Table 3-1 meet or exceed the acceptable factor of safety of 1.2 for slope stability and 1.3 for bearing based on the assumed conditions.

3.2.3. Containment Dike Settlement

Containment dike settlement typically includes four components.

1. Elastic compression (construction settlement);
2. Soil displacement, or mudwaving of softer material under loading (during construction);
3. Foundation soil consolidation settlement below the containment dike (during and after construction);
and
4. Settlement within the fill itself, which is a combination of compaction due to the weight of the fill and desiccation-induced shrinkage settlement (during and after construction).

Construction settlement and mudwaving will occur as fill materials are placed resulting in more fill being required than the volume of the dike section above existing grade. Consolidation of the fill/underlying soil and shrinkage will mostly occur after fill materials have been placed and combined with wind, rain and wave erosion, will degrade the containment dikes over time. As such, regular maintenance of the containment dikes will be required through construction of the marsh fill platform.

For this project we estimate about 3 to 9 inches of settlement from construction settlement and mudwaving while the dike is being built. Since this will occur during construction, it will result in additional fill volume being placed.

Post construction, we recommend allowing for 12 to 18 inches of settlement within the first six months due to consolidation of the underlying soils and desiccation and compression of the ECD fill. As described below, the exact calculation was 13 inches (7 inches consolidation + 6 inches shrinkage); however, this can vary based on construction methods, seasons, weather and other factors, so a wider range is recommended. With regular maintenance, this will likely be addressed as several smaller maintenance lifts.

We do not believe it is appropriate to show this settlement as a curve, since half or more of the settlement is dependent on construction methods and desiccation which will vary with seasons. Details of our settlement analyses are included in Appendix H.

3.2.3.1. Construction Settlement

Construction settlement is often taken as a percentage of the longer-term consolidation settlement. For this project, we expect approximately 3 inches of construction settlement will occur; however, since this occurs as the ECD is being built, it is not readily evident.

3.2.3.2. Mudwaving

We generally did not encounter significant organic soil (peat or organic clay) in our soil borings, and site soils are relatively competent compared to many other marsh creation project sites we have worked on. We expect mudwaving may be up to 6 inches; however, this also occurs as the ECD is being built, and is not readily evident post construction.

We believe building ECDs on existing marsh significantly reduces mudwaving. The marsh platform acts as a natural load distribution and soil reinforcement system (like a geogrid or geotextile) spreading the ECD load over a broader area and reducing load concentrations that produce mudwaving. Additionally, if there is an existing marsh, the mudline elevation is typically higher than open water areas, resulting in less fill to reach the target dike elevation.

3.2.3.3. Consolidation Settlement of Foundation Soils

The upper 25 feet of native soil is predominantly a very soft high plasticity gray clay with little to no presence of silt or sand seams or layers to improve drainage. Therefore, settlement of subgrade soils is expected to be very slow. In addition, the underlying stiffer Pleistocene clays are expected to have virtually no settlement.

Long-term we estimate approximately 14 inches of settlement; **however**, due to the lack of drainage layers, we expect about 7 inches will be realized during project construction (assuming about 6 months construction).

3.2.3.4. Shrinkage and Self-Weight Settlement of Fill Soils

ECD settlement will be influenced by desiccation of exposed soil above the average water level and compression of fill after it is placed, especially when fill is excavated from a submerged (buoyant) condition and placed above water (total stress). Research conducted by GeoEngineers indicates inorganic high-plasticity clays experience moderate shrinkage (about 15 to 20 percent exposed soil volume loss). For the high plasticity inorganic clays that will be used to construct ECDs at this site, we estimate post-construction shrinkage settlement will be about 15 percent of the fill height above the mean water level (about 6 inches), in addition to foundation settlement. We expect this settlement to occur within 6 months after construction.

Settlement within the ECD fill due to disturbance during construction and the weight of the fill upon itself, is a function of many different factors, including the type of fill, consistency of the fill, type of construction equipment and rate of placement.

3.2.4. Mechanical Dredging Cut-to-Fill

Earthen containment dike construction commonly involves removing material from a submerged condition within excavator reach of the dike alignment, placing it in the dike footprint, then shaping it to meet containment dike geometry specifications. At the project site, material in the top 10 feet of the in-place borrow soil profile generally consists of high plasticity clay. Material losses during construction, mudwaving, compaction, and water drainage as the fill is placed and shaped, soil shrinkage, and foundation settlement

during construction results in more than 1 cubic yard of material excavated from the in-place borrow soil for every cubic yard in the fill template. Due to the number of variables involved, calculating the cut-to-fill ratio for the containment dikes is very difficult. To allow for adequate material quantities in project design and cost estimating, GeoEngineers recommends a cut-to-fill ratio of about 2 to 1 to account for material losses, construction settlement, mudwave displacement, and compression settlement and shrinkage.

3.3. Marsh Creation Areas

Our analyses for the marsh creation areas included evaluating hydraulic fill settlement, marsh foundation soil settlement and cut-to-fill ratio. The results of our analyses are presented below and discussed further in Appendix I.

3.3.1. Marsh Hydraulic Fill Settlement

Freshly created marsh platforms created by pumping hydraulically dredged fill into a contained area settle over time. Elevation changes in the marsh fill are driven by self-weight consolidation, water drainage, water evaporation, plant-induced evapotranspiration and foundation soil settlement due to the weight of the marsh fill.

As GeoEngineers understands, a successful marsh creation project establishes a marsh platform that remains within the intertidal range (between mean high water and mean low water levels for fresh and intermediate marsh) for as long as practical during the project life.

3.3.1.1. Fill Testing

Based on a review of the vibracore logs during extrusion and initial moisture contents, we recommended that we prepare a composite sample of the top 10 feet of each core, then composite those into a single site composite. Results of some individual vibracore sample intervals and the site composite are summarized below in Table 3-2. As can be seen in the table, the soil properties in the top 10 feet of the borrow area are generally uniform.

TABLE 3-2. BORROW AREA COMPOSITE TESTING SUMMARY

Sample Location	Depth Below Mudline (ft)	LL	PI	Actual Moisture (%)	Finer than No. 200 Sieve (%)	Specific Gravity
V-1	0-1	108	81	106.3	99.7	
V-2	0.6-2.6	95	69	94.9	99.7	
V-3	2-4	96	69	96.1	99.8	
V-4	4-6	104	75	87.8	99.3	
V-5	0-0.8	107	79	124.8	96.9	
V-6	6-8	95	67	92.0	99.7	
V-1 through V-6 Composite	0-10	99	74	93.9	99.6	2.667

There are a couple of items worth noting regarding the borrow area. First, shell was noted in several

vibracores at the transition from the soft gray clay present in the upper 9 to 10 feet to the stiffer underlying clay. Shell typically stacks up at the dredge discharge outfall and requires spreading with equipment. Also, the underlying Pleistocene clays are typically stiff fat clay. This material tends to break into little chunks, or “clay balls” during dredging, which like shell, tend to stack up at the dredge discharge outfall. Neither of these materials (shell or stiff clay/clay balls) are represented by the hydraulic fill analyses and settlement predictions completed for this project. For conditions best suited to spreading hydraulic fill without the need to use additional equipment, dredging depths should be maintained above the depth of shell and/or stiff clay.

The scope of services requested low-stress consolidation tests on samples prepared at concentrations of 161 grams per liter (g/L) (584% moisture) and 483 g/L (170% moisture). Standard procedure for a low-stress consolidation test is to mix the samples at 3 to 4 times the liquid limit (LL), or about 300% to 400% for this borrow site. The consistency of the slurry for this test needs to have enough solids to support the test apparatus applying the load, but not so much that it cannot flow into the sample ring. We tried testing a sample at 460% moisture, and it could not support the initial load. After discussions with NRCS, we ended up running tests at moistures/concentrations summarized in Table 3-3. Test results are presented in Appendix E.

TABLE 3-3. LOW STRESS CONSOLIDATION TEST SLURRY CONCENTRATIONS

Target Moisture (%)	Actual Moisture (%)	Corresponding Solids Concentration (g solids/L slurry)
330	344.2	262
350	373.3	243
400	409.2	224

3.3.1.2. Settlement Evaluation

Based on a discussion with NRCS, we used a fill time of 25 days, which was thought to be a reasonable time to continuously discharge fill in a location before having to move the discharge pipe. GeoEngineers modeled fill placement as several lifts of approximately 1 to 1.5 feet each over this period to allow for settlement during filling.

We modeled the stiffer Pleistocene age soils encountered approximately 25 feet below the existing mudline as incompressible. The top 10 to 15 feet of the existing site soil was overconsolidated and combined with the relatively low stresses created by the hydraulic fill, there was not much settlement in existing site soil as a result of fill placement (about 0.2 to 0.3 feet expected over the 20-year design life).

Most of the expected settlement is coming from within the hydraulic fill after placement. NRCS asked for a number of evaluations, and results are presented as described below.

- Figures 6a and 7a. Hydraulic fill settlement vs. time (linear scale) with no subsidence or accretion starting at the end of construction for two starting slurry concentrations. These figures also show fill elevation from near the start of construction on a log scale.

- Figures 6b and 7b. Hydraulic fill settlement vs. time (linear scale) with subsidence starting at the end of construction for two starting slurry concentrations. These figures also show fill elevation from near the start of construction on a log scale.
- Figures 6c and 7c. Hydraulic fill settlement vs. time (linear scale) with subsidence and accretion starting at the end of construction for two starting slurry concentrations. These figures also show fill elevation from near the start of construction on a log scale.
- Figures 6d and 7d. We used the curve from Figures 6a and 7a that ended up closest to El. +0.8 ft. at 20 years, then based on the variability of the mudline elevations within the fill area, used the same starting fill elevation but a mudline representing two standard deviations above (mudline El. +0.21 ft.) and below (mudline El. -2.06 ft.) the mean elevation to estimate a 95 percent confidence interval above and below the mean elevation scenario.

Based on the results of our analyses, it appears a constructed marsh fill elevation (CMFE) of El. +2.5 feet to +3.0 feet is likely to achieve project goals. Summaries of our calculation approach and our analyses are provided in Appendix I.

3.3.2. Hydraulic Dredging Cut-to-Fill

Hydraulically dredged material cut-to-fill ratios have been reported between 1.0 (1-yard cut from the borrow for every 1 yard placed in the fill area) and 1.5 for marsh creation projects in Louisiana, depending on material type, containment scheme and dredge/pipe/containment efficiencies. The material exiting the dredge pipe will initially be less dense than the in-place borrow material; however, it is expected to return to its pre-dredge density with time. GeoEngineers recommends a cut-to-fill ratio of 1.2 for this site. This number is based on a fill volume calculated using the long-term total consolidated fill thickness and associated settlement. In other words, the volume should be calculated including the volume needed to fill to the target long-term elevation (El. 0.8 ft.) and account for subgrade settlement (El. -0.93 ft. less 0.2 feet settlement).

As can be seen in Figures 6d and 7d, variation in the mudline can significantly affect the resulting 20-year fill elevation. Given the variability of the mudline and modern survey and drafting technology, some designers prefer to work with surfaces representing the mudline. In this case, the designer can add a percentage to the difference between the target long-term elevation and the existing mudline to account for subgrade settlement. For example, in this particular case, there is approximately 0.2 feet of settlement for 1.73 feet of consolidated fill thickness above El. -0.93 ft. at year 20, or about a 12 percent increase in the volume due to subgrade settlement. The designer could use CAD to determine the volume between the target design elevation (El. 0.8 ft.) and the existing variable mudline based on survey data, then multiply by 1.12 to estimate the total volume, including subgrade settlement, then multiply this number by 1.2 for dredging losses to determine the in-place borrow area volume required to be cut.

4.0 CONSTRUCTION CONSIDERATIONS

4.1. General Considerations

Based on the expected site construction activities and evaluations completed for this project, the following construction considerations are offered:

- Our evaluations are based on a limited number of investigations over a wide area. Our evaluations indicate generally similar conditions across the site. However, NRCS should expect localized areas during construction to require location-specific remedies. GeoEngineers offers our services during construction to address issues that may arise.
- For pipelines in close proximity to the marsh creation cells and borrow area, we recommend taking precautions to mitigate impact to pipelines prior to construction. The project design and construction teams should work closely with the companies that have pipelines in the area and conduct a pre-construction geophysical survey to confirm pipeline and other obstruction locations.
- Water depth in the marsh creation areas is variable.
- We did not encounter significant organic soil layers such as peat; however, should such layers be encountered, the design and construction teams should be aware of the following:
 - Peat used in constructing containment dikes may compress significantly under loading, requiring more fill; however, it can be utilized and should not be wasted.
 - Energy diffusers or other such precautions are recommended to reduce scouring of organic deposits during hydraulic fill placement. We understand scoured floating blocks of peat have blocked discharge weir boxes at sites with similar conditions. At these sites, wire mesh fences placed in a wide arc in front of the discharge point were used to screen out floating organic material blocks.
 - Peat is a weak, light-weight material. Mudwaves and lateral displacement should be expected while placing fill in areas with peat.
- Dewatering structures (weirs, drainage culverts) should be designed to allow retention of as much soil fill as practical. In general, placement of such structures away from the dredge discharge point is preferred.

4.2. Construction Sequencing

- The contractor should plan to place fill in low areas first, then move to higher ground, both for the containment dikes and hydraulic marsh fill. Lower areas will require more fill and are expected to settle more. Filling these low areas first will allow some additional settlement to be realized and then potentially mitigated by placing additional fill in these areas during construction.
- Please be advised that the predominant soil in the borrow area is high moisture, high plasticity clay. High plasticity clay will typically settle slowly. The slurry will also be using Gulf of Mexico water, which will be saline. Saline water will have two effects on clay: (1) it acts as a dispersant; and (2) saline water is denser which will also slow settling. The contractor must consider this when determining fill rates and/or sequencing to allow settlement of solids within the fill area.
- As discussed earlier, the dredge discharge outfall will likely have to be moved during construction to distribute fill throughout the marsh creation area. The distance between discharge locations and number of outfall moves required to best fill the marsh creation area will be a judgement call by the contractor based on their equipment, slurry mixture and other factors. A construction monitoring tool that may be useful to monitor how well hydraulic fill is spreading throughout the fill area is an instrumented settlement plate. These plates measure the solids as they accumulate above the base of the plate and allow the contractor to evaluate how well the fill is spreading.

4.3. Containment Dike Construction

- **Containment dike construction can be challenging if not performed correctly.** Lift construction is recommended. The best strategy to achieve stable ECDs is to allow time for fill material to settle, consolidate and gain strength between lifts. We recommend a minimum of 14 days; however, additional time between lifts will improve stability. Open water areas and areas with lower mudlines (thicker fill) **and the ECD section between C-5 and C-7 should be filled first to allow additional time for the fill material to set-up. The second lift for these potentially critical areas should be added last to allow the maximum time for ECD fill to settle and re-gain strength.** With large fill volumes, the contractor should consider equipment reach and excavation sequencing to ensure sufficient fill is available for ECD construction.
- **Contractors are likely to excavate deeper for “better” soil to build earthen containment dikes, often plunging through the top few feet of weak soil. This will result in borrow channels that are deeper than designed and/or ECD borrow material that is heavier than assumed in our analyses. Contractors should adhere to the depth guidelines presented in this report. For this project, the lowest borrow channel elevation evaluated was El. -15 ft.**
- Do not direct dredge discharge streams at ECDs or other critical containment structures. Moving slurry has momentum that if directed towards ECDs can cause failure.
- Instrumentation, combined with lateral displacement survey monitoring may be beneficial to monitor ECD construction. Push-in piezometers can be used to monitor excess pore water pressure in subgrade soil beneath the ECD. Surveyed monitoring points set a fixed distance from the ECD centerline near the toe of the ECD can be monitored to check for lateral soil displacement during filling. Excessive lateral displacement, or mudwaving, is an indication of potential failure and will result in additional fill volume to replace displaced soil. Managing fill to limit lateral displacement will reduce fill volumes but may require a longer construction time.
- ECD maintenance will be required throughout construction. ECDs should not be built above the design elevation as a measure to reduce maintenance.
- Where permissible, the contractor should build containment dikes on emergent marsh. This provides a higher base elevation, and the marsh vegetation is a natural reinforcement, resulting in less fill and generally lower failure potential. From an engineering perspective, the contractor may use the top layer of marsh for dike fill (i.e., it is okay to use marsh grass and roots for containment dike fill).
- When building earthen containment dikes, sound construction practice includes excavating and placing soil as gently as practical in as intact a mass as practical. Double-handling fill, tracking over fill material, dropping fill so that it free-falls, and other activities that disturb fill and reduce soil strength must be prevented.
- Closing all but one small opening for the marsh creation area will force the tidal flow through the open location and potentially scour a channel. Careful consideration should be given to ECD construction sequencing and tidal patterns to minimize the potential for tidal channel scour.
- ECD fill should be maintained about 1 foot above the level of the hydraulic marsh fill, plus any free water ponded on top of the marsh fill.
- Containment structure design recommendations are based on hydraulic fill retention during normal weather conditions. Exceptional weather, such as hurricane winds or storm surge, were not considered.

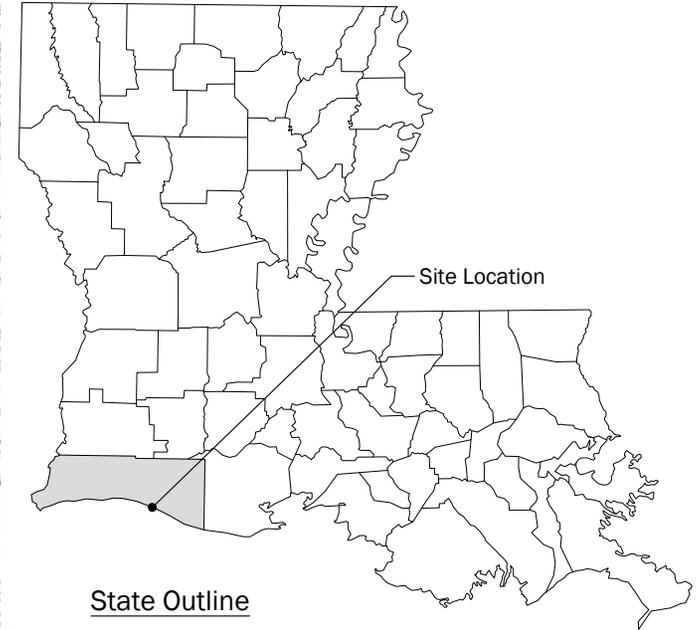
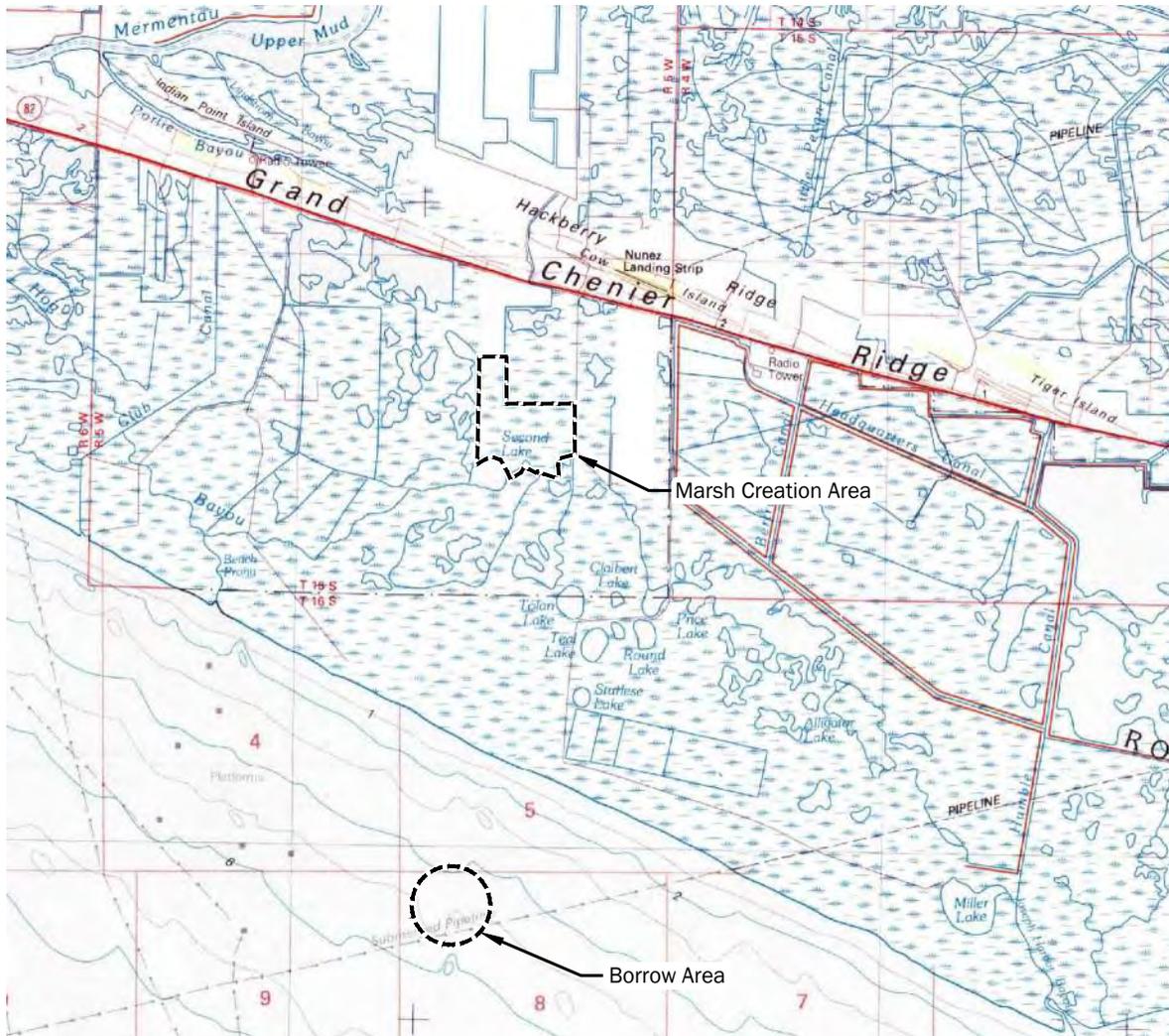
- Unless otherwise specified, we recommend the marsh buggy excavators stay at least 2 feet away from the containment dike toe and at least 5 feet away from the borrow slope crest.

5.0 LIMITATIONS

This report has been prepared exclusively for ECM + MRD Joint Venture and NRCS in support of the South Grand Chenier—Baker Marsh Creation (ME-32) project located in Cameron Parish, Louisiana.

Within the limitations of scope, schedule and budget, our services have been executed in accordance with generally accepted practices in the field of geotechnical engineering in this area at the time this report was prepared. No warranty or other conditions, expressed or implied, should be understood.

Please refer to Appendix J, Report Limitations and Guidelines for Use, for additional information pertaining to use of this report.

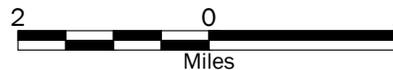


Notes:

1. The locations of all features shown are approximate.
2. This drawing is for information purposes. It is intended to assist in showing features discussed in an attached document. GeoEngineers, Inc. cannot guarantee the accuracy and content of electronic files. The master file is stored by GeoEngineers, Inc. and will serve as the official record of this communication.

Data Source: Topographic Image was taken from USGS,
Quads: White Lake (1983)

Projection: Louisiana State Plane, Southern Zone, NAD83, US Foot



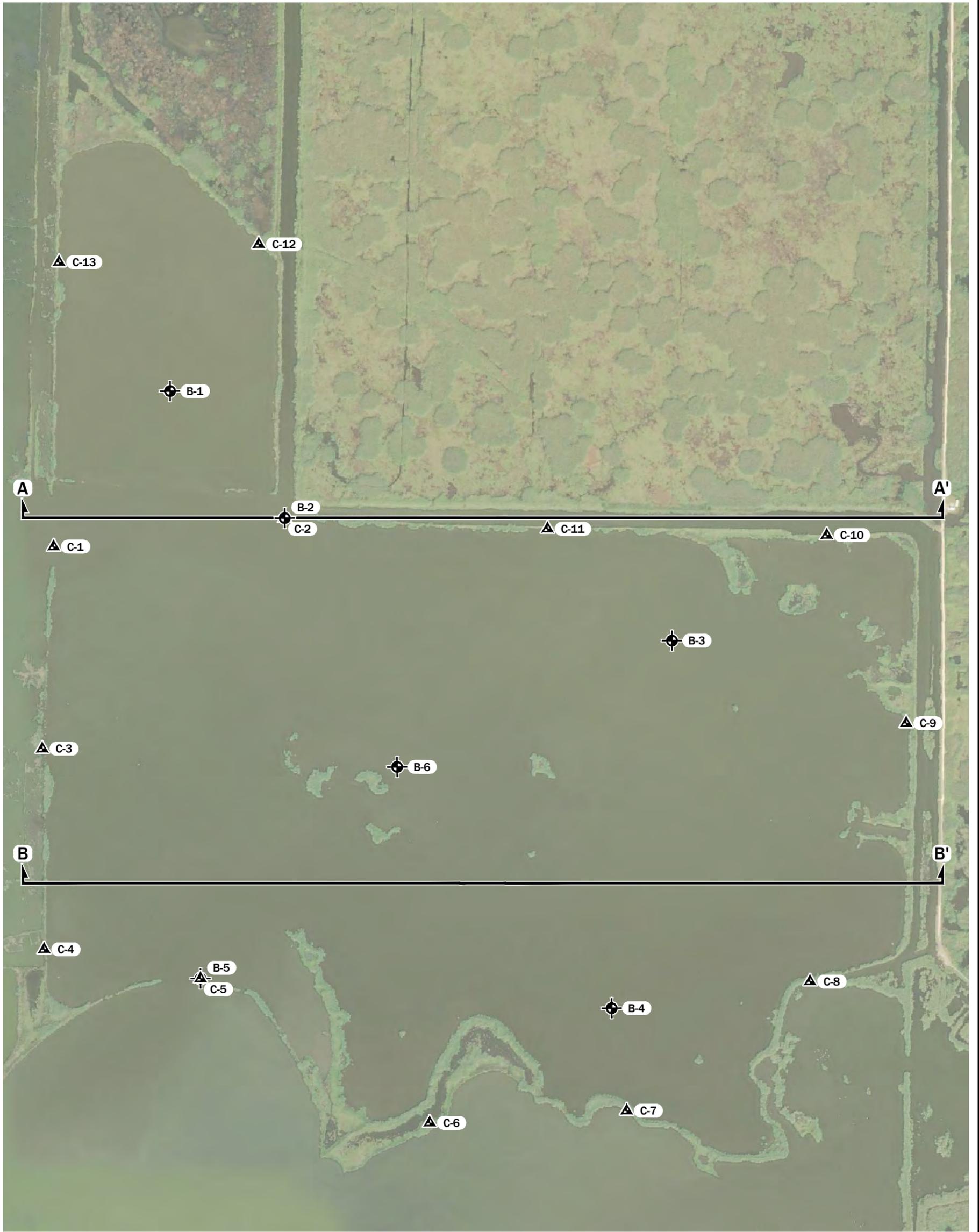
Vicinity Map

South Grand Chenier
Baker Marsh Creation (ME-32)
Cameron Parish, Louisiana



Figure 1

P:\10_10883026\CAD\00\Geotech - Final\1088302600_F02a_Boring and CPT Locations.dwg F01 Date Exported: 2/14/2023 3:50 PM - by Kyle M. Cook

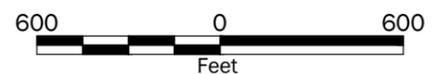


Legend

B-1  Boring by GeoEngineers, Inc., 2022

C-1  Cone Penetration Test, 2022

A A'  Cross Section Location



Marsh Creation Area Boring and CPT Locations

South Grand Chenier
Baker Marsh Creation (ME-32)
Cameron Parish, Louisiana



Figure 2a

Notes:

1. The locations of all features shown are approximate.
2. This drawing is for information purposes. It is intended to assist in showing features discussed in an attached document. GeoEngineers, Inc. cannot guarantee the accuracy and content of electronic files. The master file is stored by GeoEngineers, Inc. and will serve as the official record of this communication.

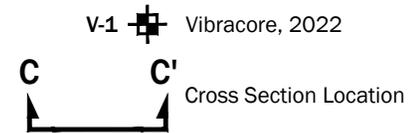
Data Source: Aerial from Microsoft Bing.

Projection: LA State Plane, South Zone, NAD83, US Foot



Vibracore Details			
Location ID	Latitude	Longitude	Depth (ft)
V-1	N029.643673	W092.873329	20
V-2	N029.644501	W092.869153	20
V-3	N029.645377	W092.864944	20
V-4	N029.641403	W092.872703	20
V-5	N029.642312	W092.868546	20
V-6	N029.643300	W092.864434	20

Legend

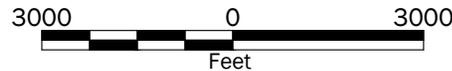


Notes:

1. The locations of all features shown are approximate.
2. This drawing is for information purposes. It is intended to assist in showing features discussed in an attached document. GeoEngineers, Inc. cannot guarantee the accuracy and content of electronic files. The master file is stored by GeoEngineers, Inc. and will serve as the official record of this communication.

Data Source: Aerial from MicroSoft Bing

Projection: Louisiana State Plane, Southern Zone, NAD83, US Foot



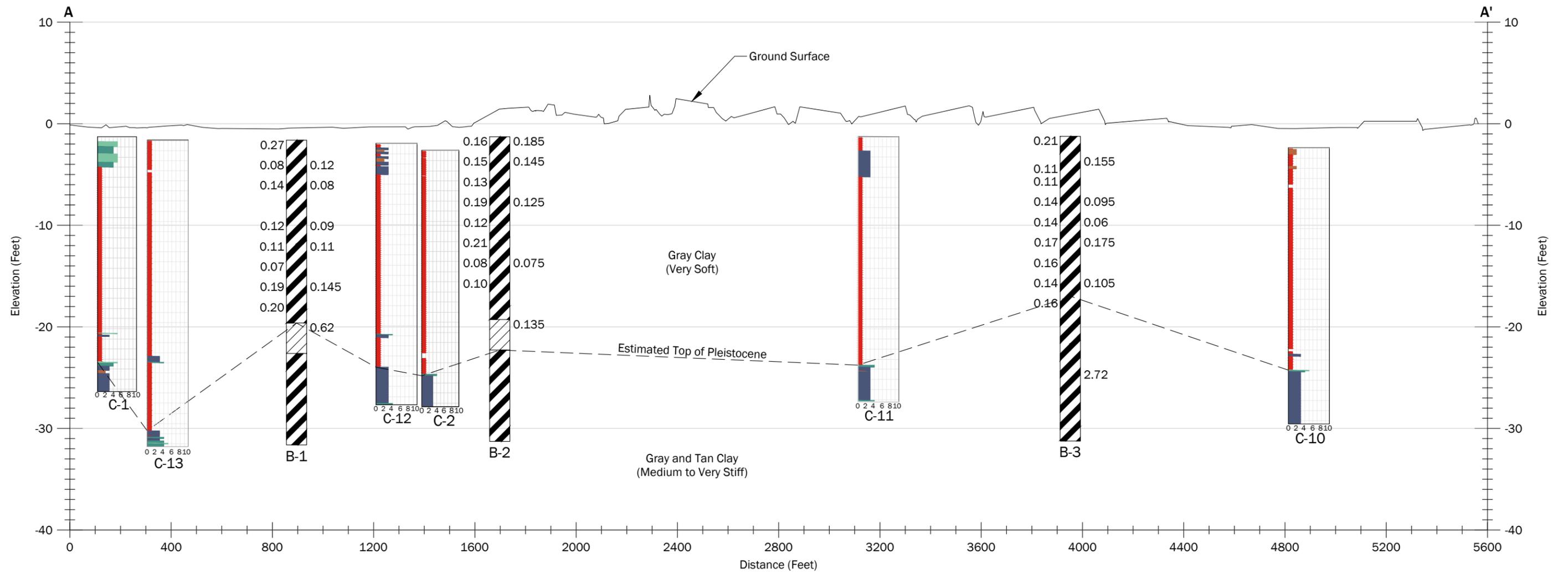
Borrow Area Vibracore Locations

South Grand Chenier
Baker Marsh Creation (ME-32)
Cameron Parish, Louisiana



Figure 2b

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Notes:

1. The subsurface conditions shown are based on interpolation between widely spaced explorations and should be considered approximate; actual subsurface conditions may vary from those shown.
2. This figure is for informational purposes only. It is intended to assist in the identification of features discussed in a related document. Data were compiled from sources as listed in this figure. The data sources do not guarantee these data are accurate or complete. There may have been updates to the data since the publication of this figure. This figure is a copy of a master document. The hard copy is stored by GeoEngineers, Inc. and will serve as the official document of record.

Data Source: Elevation data was provided by USDA, Dated 12/21
Datum: NAVD 88, unless otherwise noted.

CPT Legend

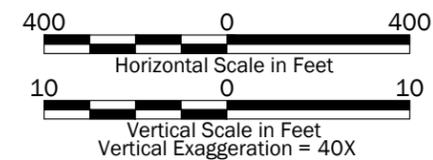
- 1. Sensitive fine grained
- 2. Organic material
- 3. Clay to silty clay
- 4. Clayey silt to silty clay
- 5. Silty sand to sandy silt
- 6. Clean sand to silty sand
- 7. Gravely sand to sand
- 8. Very stiff sand to clayey sand
- 9. Very stiff fine grained

Soil Classification

- CL - Silty Clay
- CH - Clay

Boring Legend

- Minivane (KSF)
- Shear Strength (KSF)



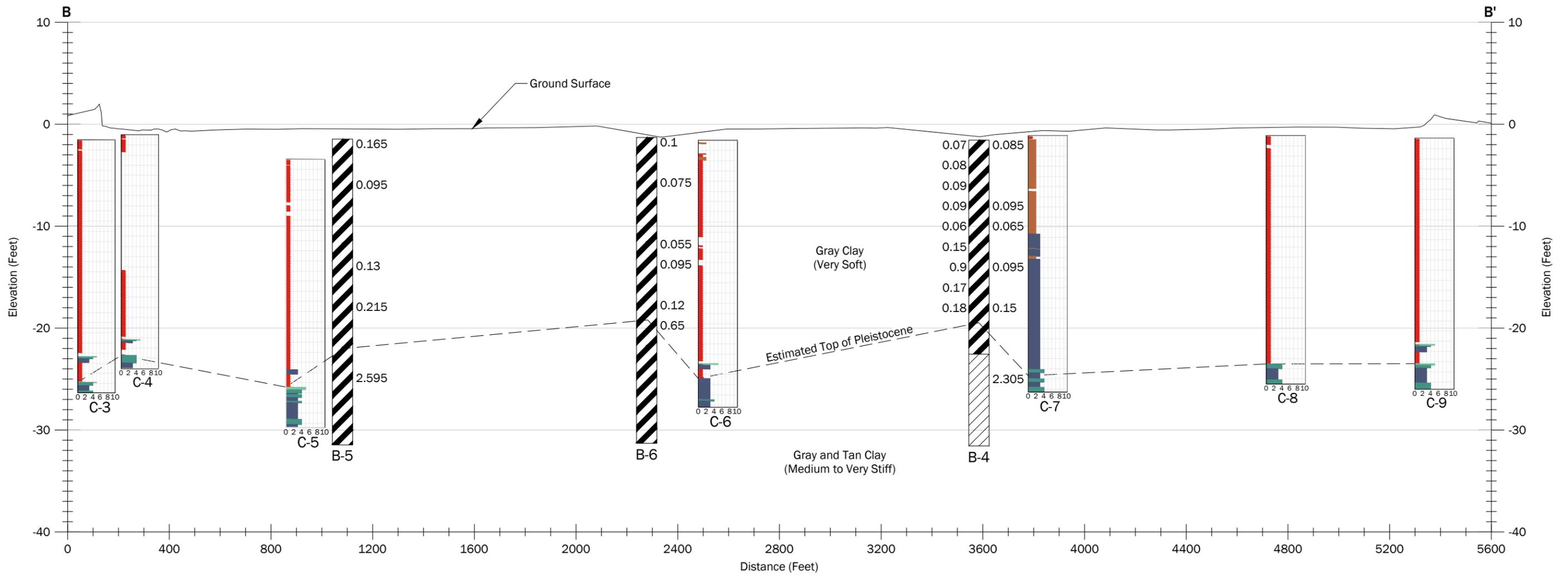
Subsurface Profile A-A'

South Grand Chenier
Baker Marsh Creation (ME-32)
Cameron Parish, Louisiana

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Figure 3a

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Notes:

1. The subsurface conditions shown are based on interpolation between widely spaced explorations and should be considered approximate; actual subsurface conditions may vary from those shown.
2. This figure is for informational purposes only. It is intended to assist in the identification of features discussed in a related document. Data were compiled from sources as listed in this figure. The data sources do not guarantee these data are accurate or complete. There may have been updates to the data since the publication of this figure. This figure is a copy of a master document. The hard copy is stored by GeoEngineers, Inc. and will serve as the official document of record.

Data Source: Elevation data was provided by USDA, Dated 12/21
Datum: NAVD 88, unless otherwise noted.

CPT Legend

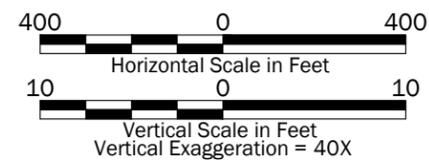
- 1. Sensitive fine grained
- 2. Organic material
- 3. Clay to silty clay
- 4. Clayey silt to silty clay
- 5. Silty sand to sandy silt
- 6. Clean sand to silty sand
- 7. Gravely sand to sand
- 8. Very stiff sand to clayey sand
- 9. Very stiff fine grained

Soil Classification

- CL - Silty Clay
- CH - Clay

Boring Legend

- Minivane (KSF)
- Shear Strength (KSF)



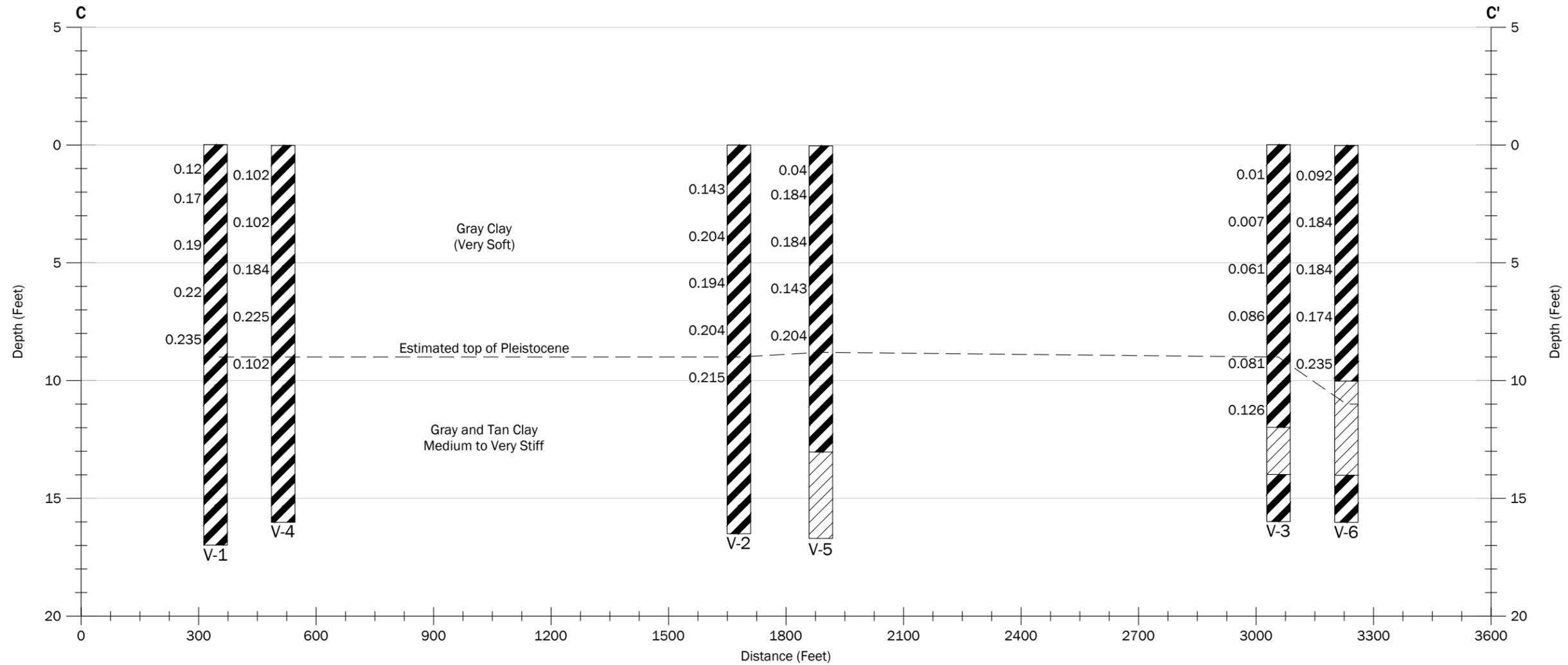
Subsurface Profile B-B'

South Grand Chenier
Baker Marsh Creation (ME-32)
Cameron Parish, Louisiana

GEOENGINEERS

Figure 3b

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Notes:

1. The subsurface conditions shown are based on interpolation between widely spaced explorations and should be considered approximate; actual subsurface conditions may vary from those shown.
2. This figure is for informational purposes only. It is intended to assist in the identification of features discussed in a related document. Data were compiled from sources as listed in this figure. The data sources do not guarantee these data are accurate or complete. There may have been updates to the data since the publication of this figure. This figure is a copy of a master document. The hard copy is stored by GeoEngineers, Inc. and will serve as the official document of record.

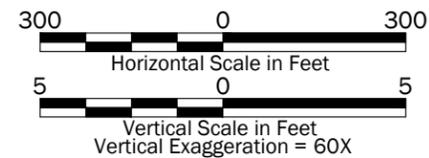
Data Source: Elevation data was provided by USDA, Dated 12/21
Datum: NAVD 88, unless otherwise noted.

Soil Classification

- CL - Silty Clay
- CH - Clay

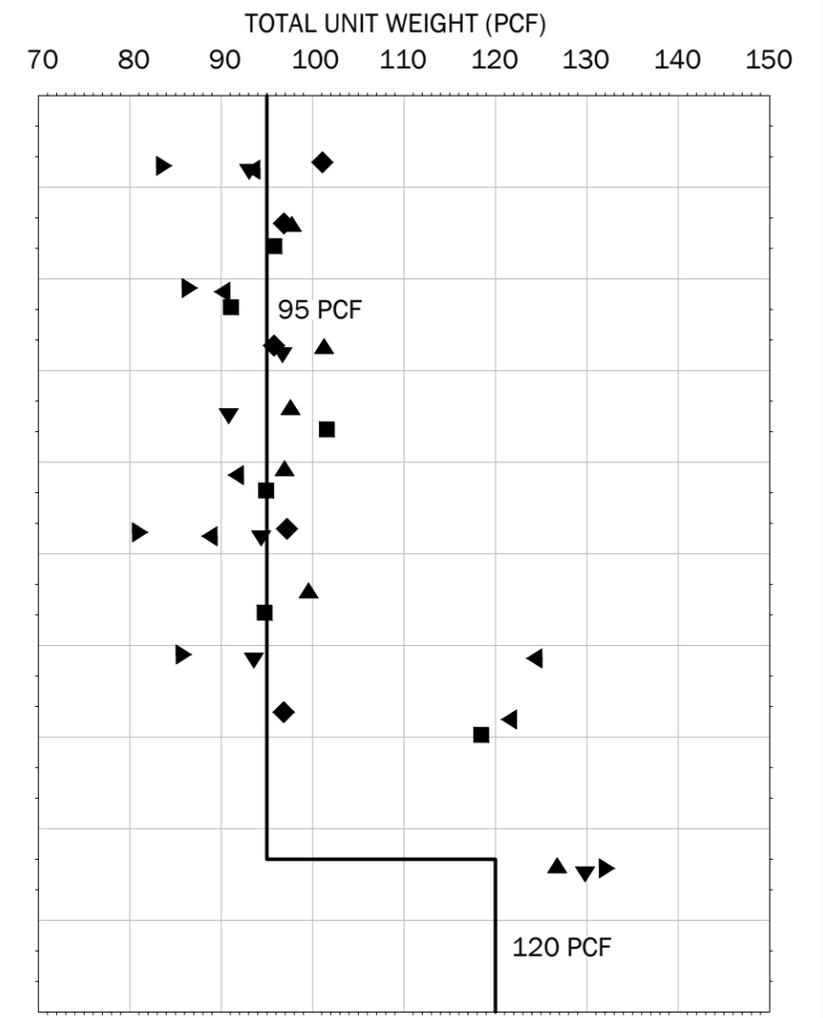
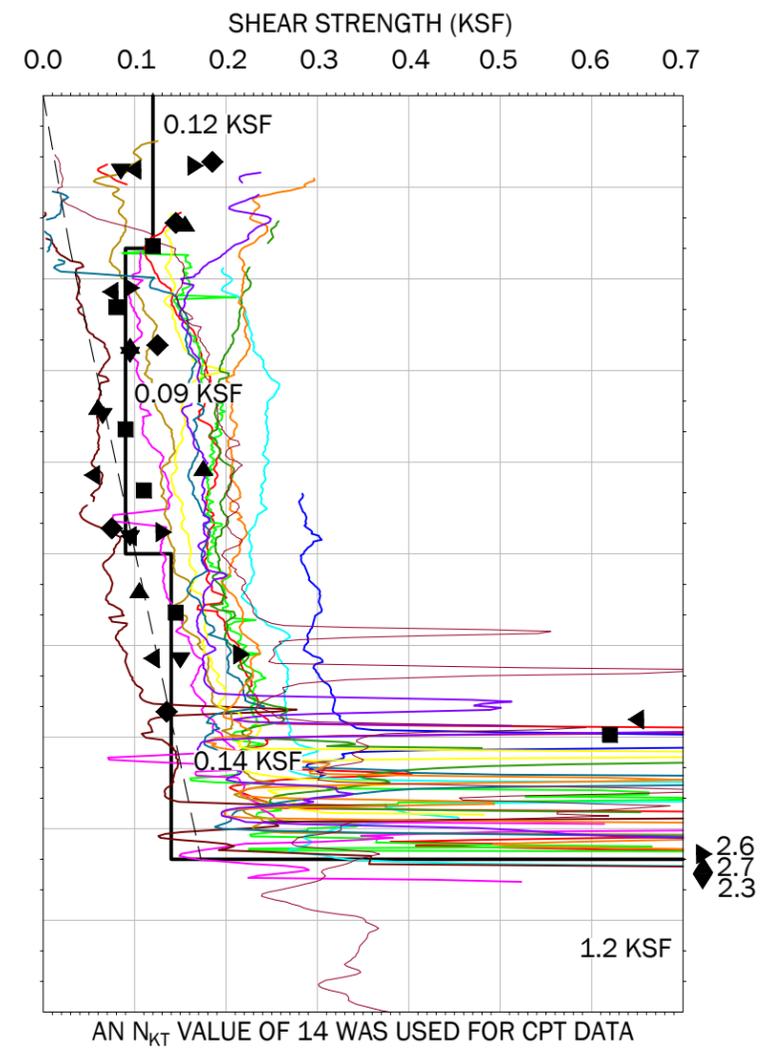
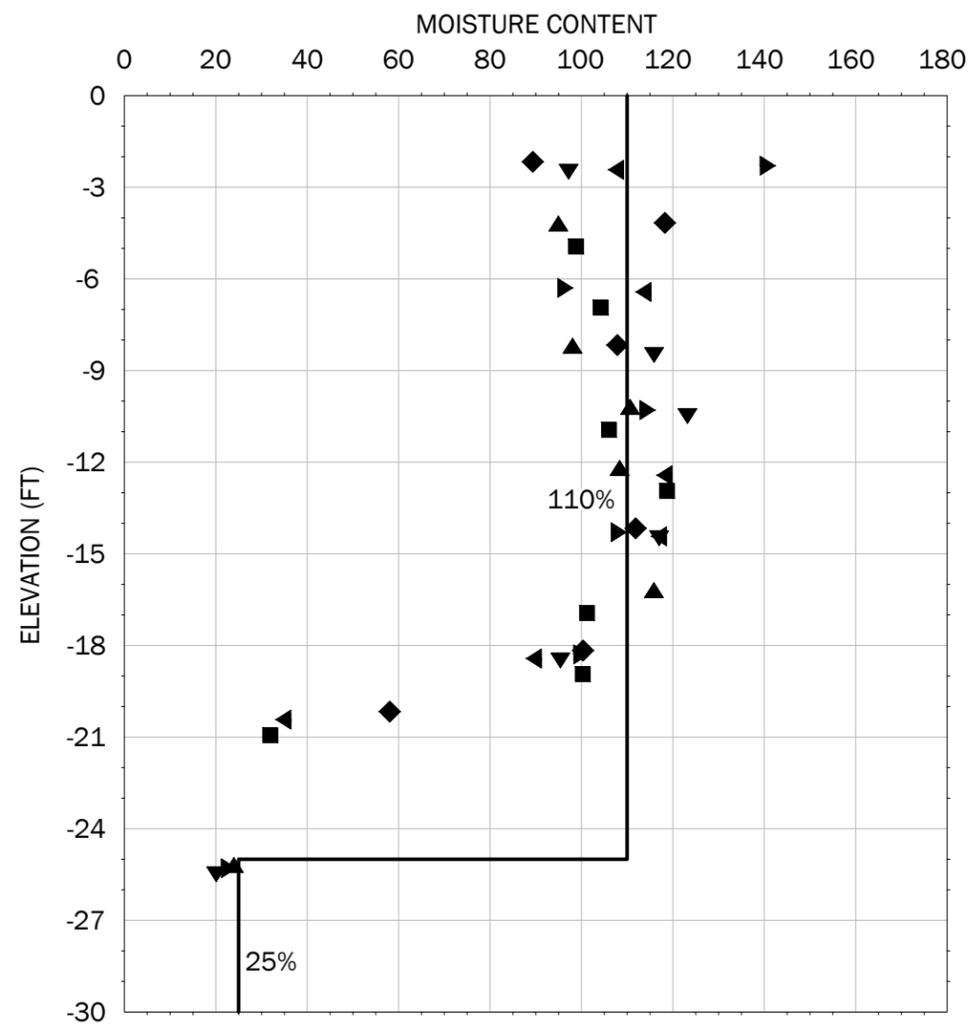
Boring Legend

Torvane Shear Strength (KSF)



Subsurface Profile C-C'	
South Grand Chenier Baker Marsh Creation (ME-32) Cameron Parish, Louisiana	
	Figure 3c

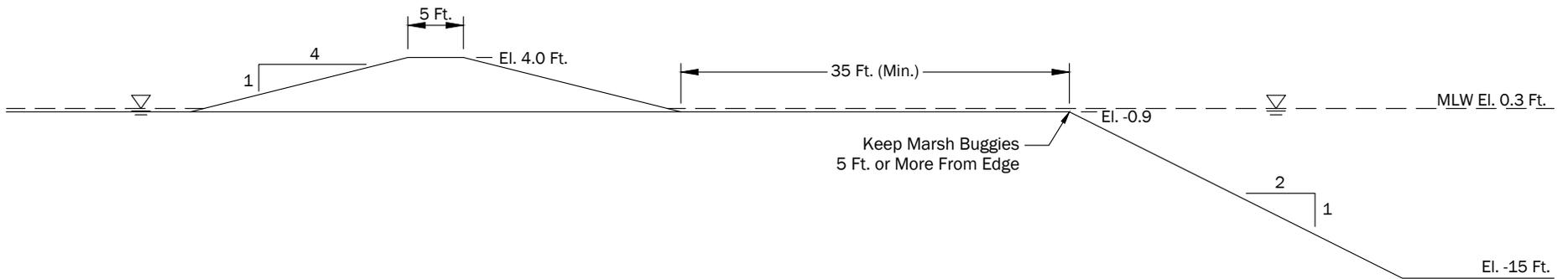
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- Legend**
- B-1
 - ◆ B-2
 - ▲ B-3
 - ▼ B-4
 - ▶ B-5
 - ◀ B-6
 - Design Profile
 - - - 0.22σ_v

- CPT Legend**
- C-1
 - C-2
 - C-3
 - C-4
 - C-5
 - C-6
 - C-7
 - C-8
 - C-9
 - C-10
 - C-11
 - C-12
 - C-13

Marsh Creation Area Design Profile	
South Grand Chenier Baker Marsh Creation (ME-32) Cameron Parish, Louisiana	
	Figure 4

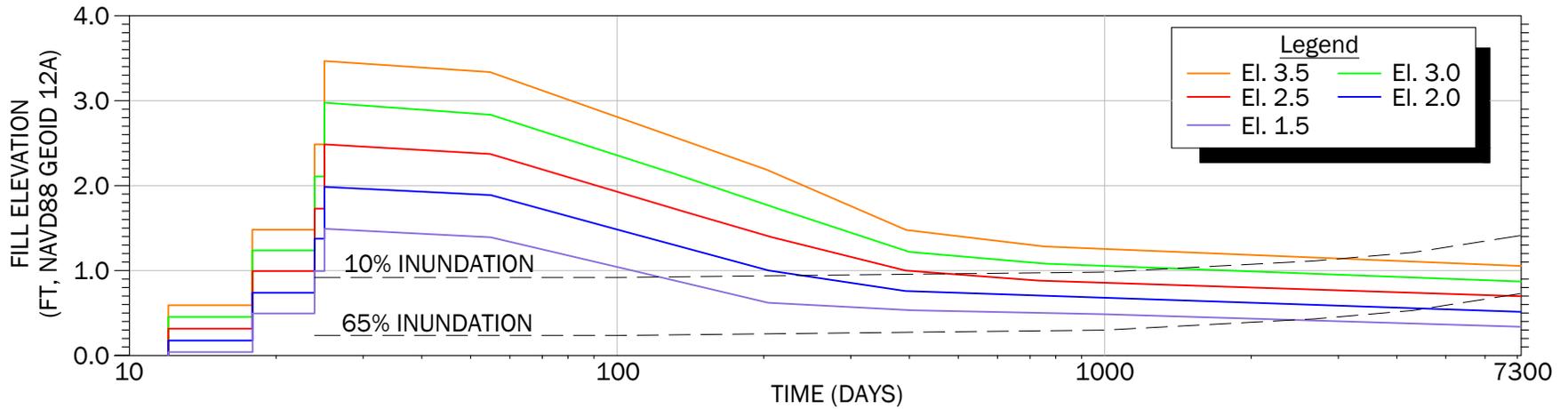
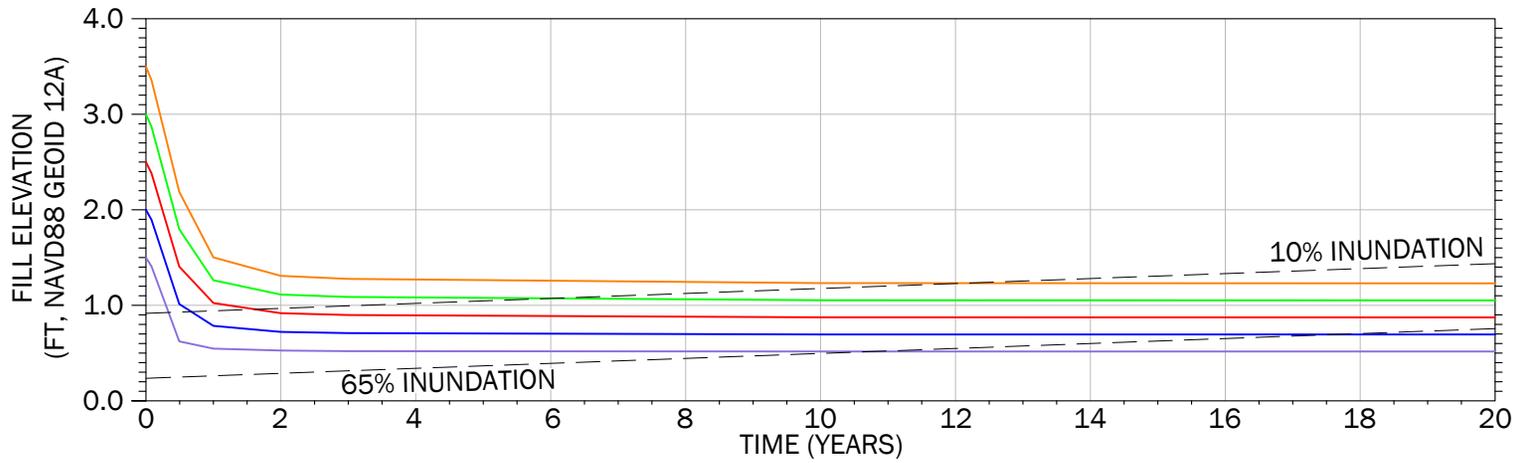


Earthen Containment Dike Section

South Grand Chenier
Baker Marsh Creation (ME-32)
Cameron Parish, Louisiana



Figure 5



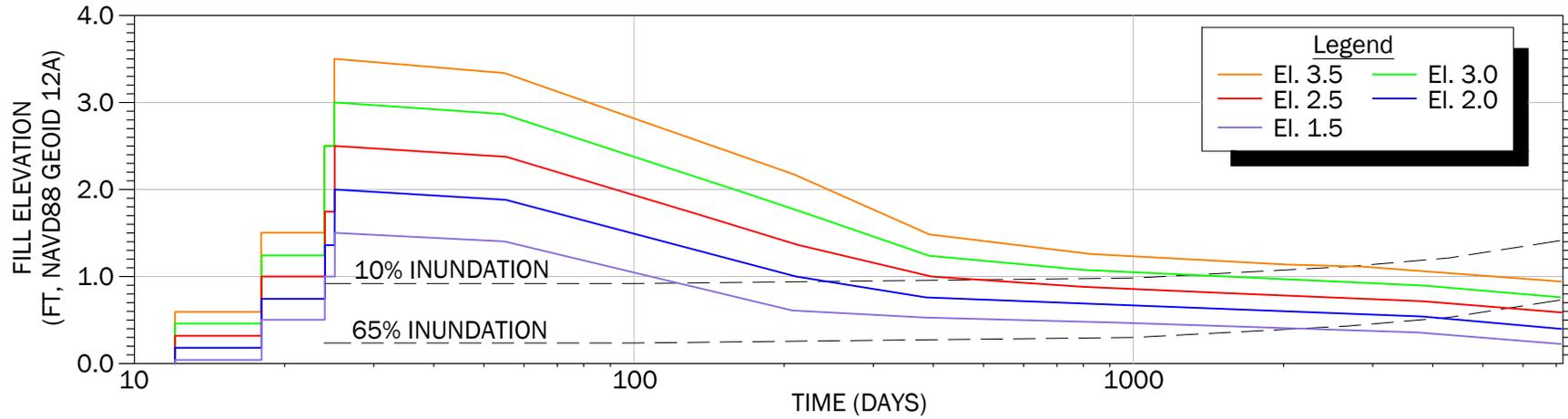
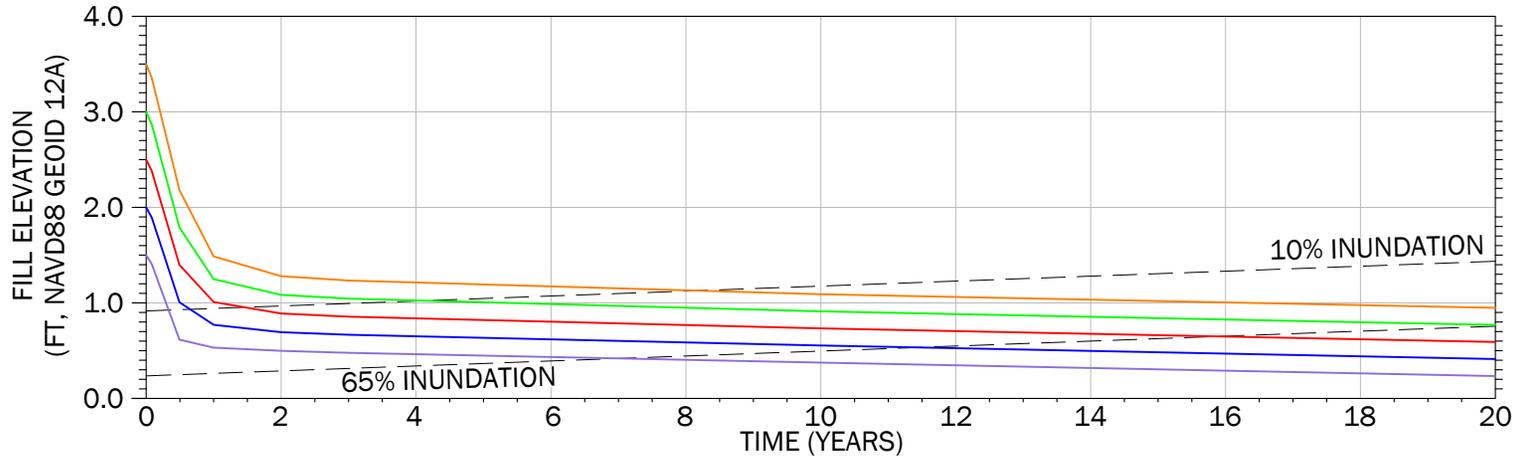
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	1 MONTH	6 MONTHS	1 YEAR	2 YEARS	3 YEARS	10 YEARS	20 YEARS	0 YEARS	20 YEARS
3.5	3.4	2.2	1.5	1.3	1.3	1.2	1.2	-0.9	-1.2
3.0	2.9	1.8	1.3	1.1	1.1	1.1	1.1	-0.9	-1.2
2.5	2.4	1.4	1.0	0.9	0.9	0.9	0.9	-0.9	-1.1
2.0	1.9	1.0	0.8	0.7	0.7	0.7	0.7	-0.9	-1.1
1.5	1.4	0.6	0.5	0.5	0.5	0.5	0.5	-0.9	-1.0

Marsh Settlement
344.2% Moisture Slurry (262 g/L)

South Grand Chenier
 Baker Marsh Creation (ME-32)
 Cameron Parish, Louisiana

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Figure 6a



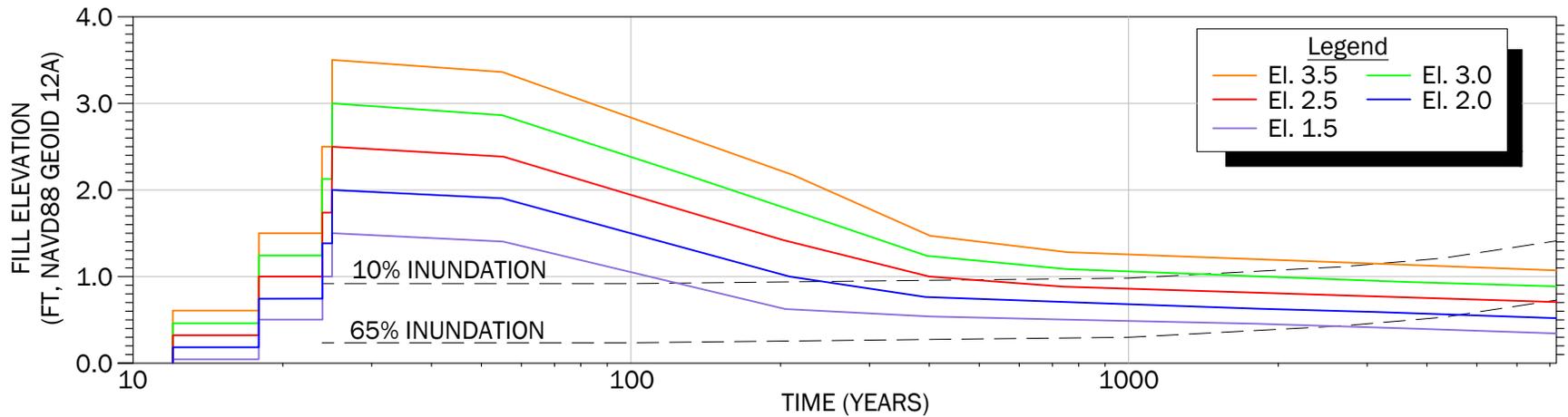
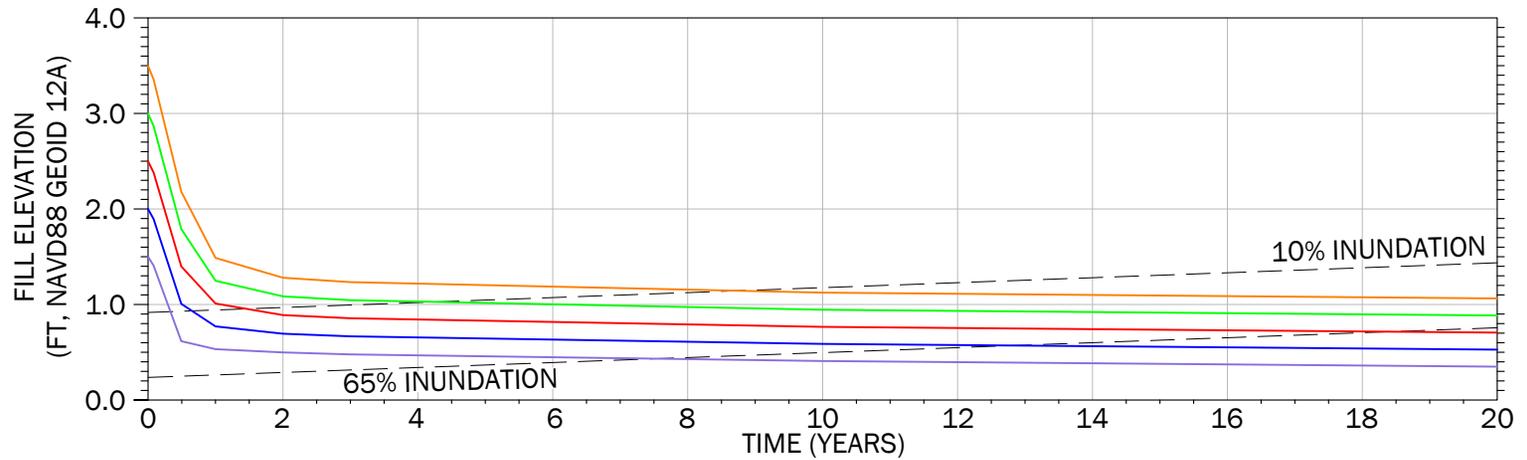
END OF CONSTRUCTION	FILL ELEVATION (FEET NAVD88)							MUDLINE ELEVATION (FEET NAVD88)	
	1 MONTH	6 MONTHS	1 YEAR	2 YEARS	3 YEARS	10 YEARS	20 YEARS	0 YEARS	20 YEARS
3.5	3.4	2.2	1.5	1.3	1.2	1.1	0.9	-0.9	-1.5
3.0	2.9	1.8	1.2	1.1	1.0	0.9	0.8	-0.9	-1.4
2.5	2.4	1.4	1.0	0.9	0.9	0.7	0.6	-0.9	-1.4
2.0	1.9	1.0	0.8	0.7	0.7	0.6	0.4	-0.9	-1.3
1.5	1.4	0.6	0.5	0.5	0.5	0.4	0.2	-0.9	-1.3

Marsh Settlement
344.2% Moisture Slurry (262 g/L)
w/ Subsidence

South Grand Chenier
 Baker Marsh Creation (ME-32)
 Cameron Parish, Louisiana

GEOENGINEERS 

Figure 6b



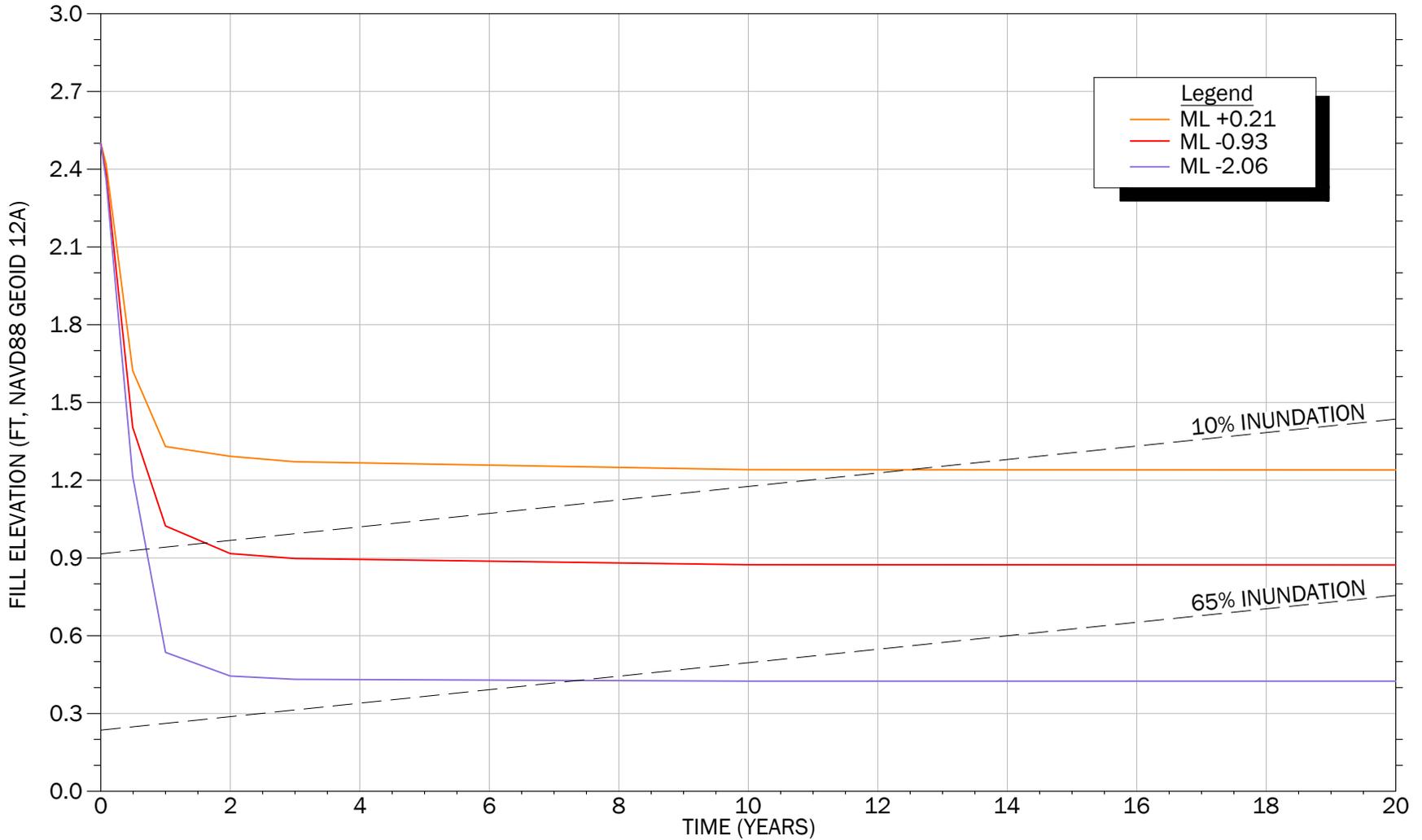
END OF CONSTRUCTION	FILL ELEVATION (FEET NAVD88)							MUDLINE ELEVATION (FEET NAVD88)	
	1 MONTH	6 MONTHS	1 YEAR	2 YEARS	3 YEARS	10 YEARS	20 YEARS	0 YEARS	20 YEARS
3.5	3.4	2.2	1.5	1.3	1.2	1.1	1.1	-0.9	-1.5
3.0	2.9	1.8	1.2	1.1	1.0	0.9	0.9	-0.9	-1.4
2.5	2.4	1.4	1.0	0.9	0.9	0.8	0.7	-0.9	-1.4
2.0	1.9	1.0	0.8	0.7	0.7	0.6	0.5	-0.9	-1.3
1.5	1.4	0.6	0.5	0.5	0.5	0.4	0.3	-0.9	-1.3

Marsh Settlement
344.2% Moisture Slurry (262 g/L)
w/ Subsidence & Accretion

South Grand Chenier
 Baker Marsh Creation (ME-32)
 Cameron Parish, Louisiana

GEOENGINEERS 

Figure 6c



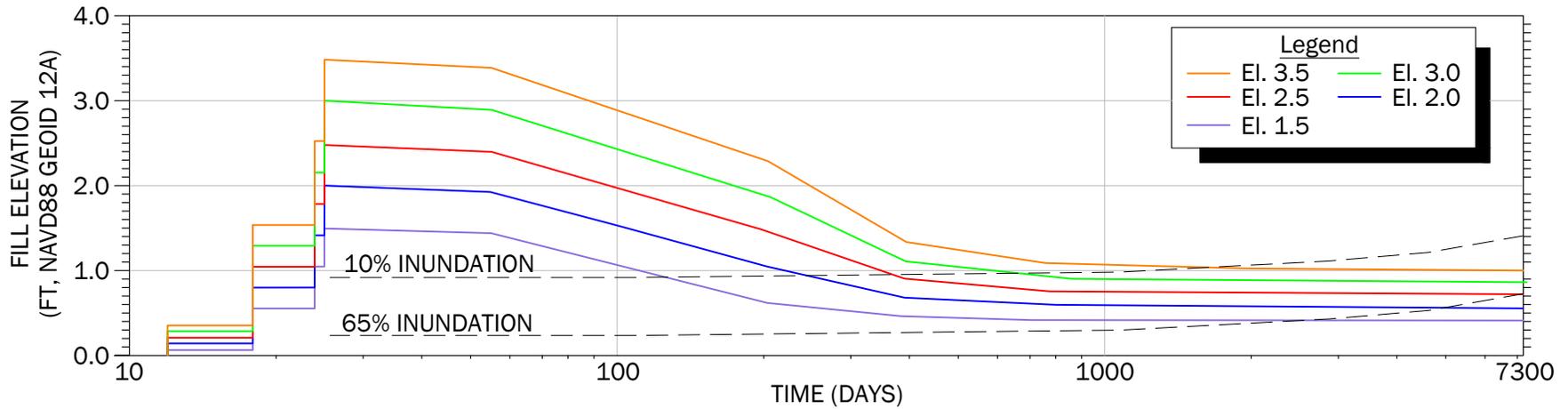
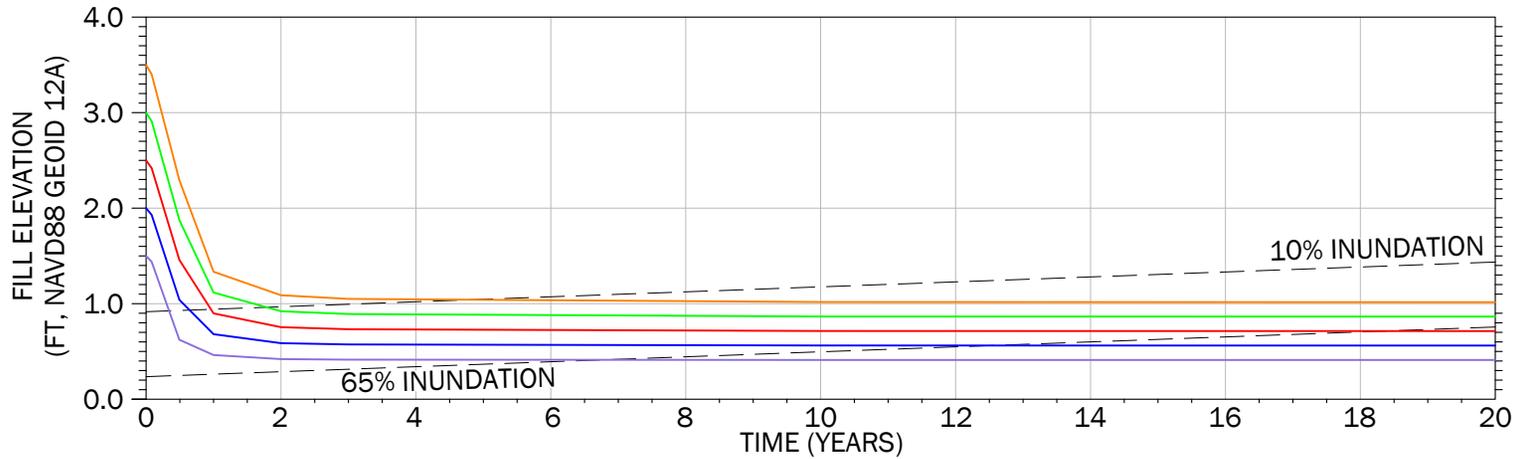
FILL ELEVATION (FEET NAVD88)								MUDLINE ELEVATION (FEET NAVD88)	
END OF CONSTRUCTION	1 MONTH	6 MONTHS	1 YEAR	2 YEARS	3 YEARS	10 YEARS	20 YEARS	0 YEARS	20 YEARS
2.5	2.4	1.6	1.3	1.3	1.3	1.2	1.2	0.2	0.0
2.5	2.4	1.4	1.0	0.9	0.9	0.9	0.9	-0.9	-1.1
2.5	2.4	1.2	0.5	0.4	0.4	0.4	0.4	-2.1	-2.2

Marsh Settlement
344.2% Moisture Slurry (262 g/L)
w/ Confidence Intervals

South Grand Chenier
 Baker Marsh Creation (ME-32)
 Cameron Parish, Louisiana

GEOENGINEERS 

Figure 6d



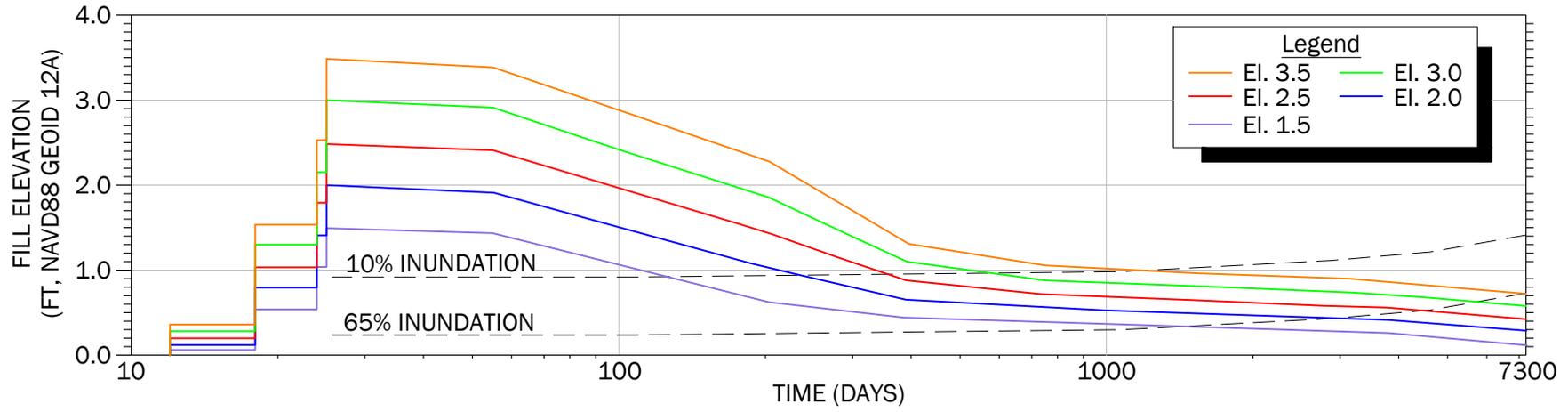
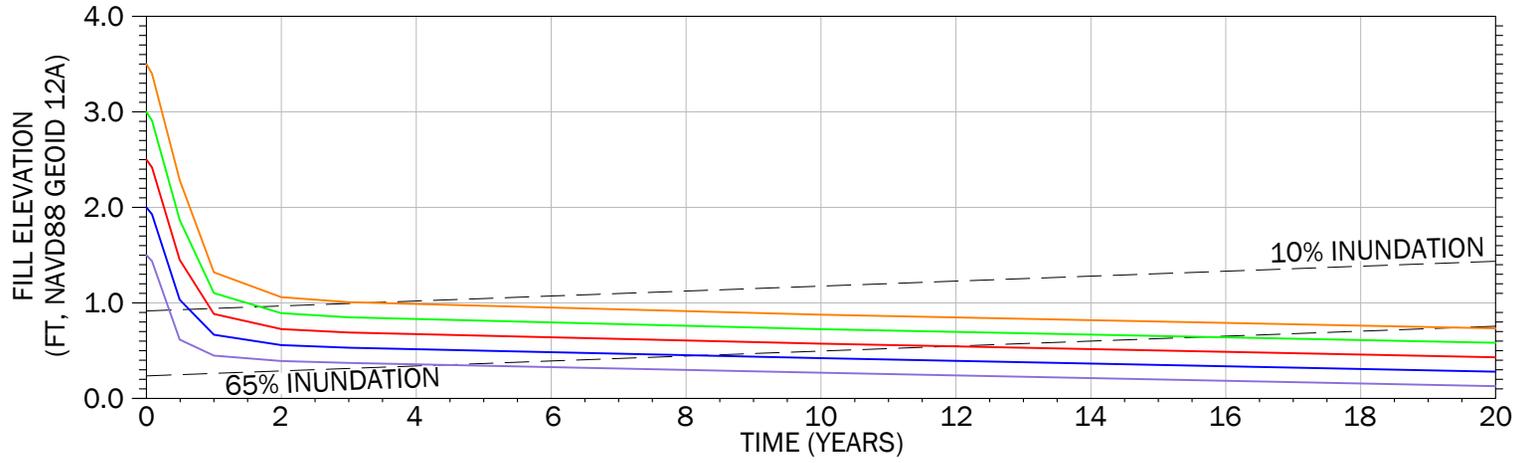
END OF CONSTRUCTION	FILL ELEVATION (FEET NAVD88)							MUDLINE ELEVATION (FEET NAVD88)	
	1 MONTH	6 MONTHS	1 YEAR	2 YEARS	3 YEARS	10 YEARS	20 YEARS	0 YEARS	20 YEARS
3.5	3.4	2.3	1.3	1.1	1.1	1.0	1.0	-0.9	-1.2
3.0	2.9	1.9	1.1	0.9	0.9	0.9	0.9	-0.9	-1.1
2.5	2.4	1.5	0.9	0.8	0.7	0.7	0.7	-0.9	-1.1
2.0	1.9	1.0	0.7	0.6	0.6	0.6	0.6	-0.9	-1.1
1.5	1.4	0.6	0.5	0.4	0.4	0.4	0.4	-0.9	-1.0

Marsh Settlement
409.2% Moisture Slurry (224 g/L)

South Grand Chenier
 Baker Marsh Creation (ME-32)
 Cameron Parish, Louisiana

GEOENGINEERS 

Figure 7a



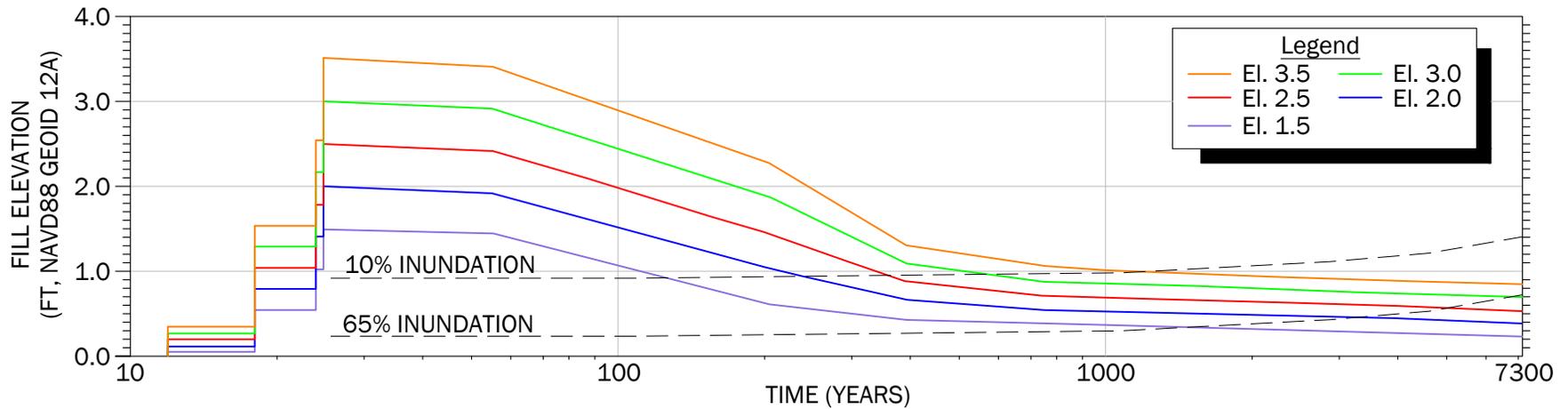
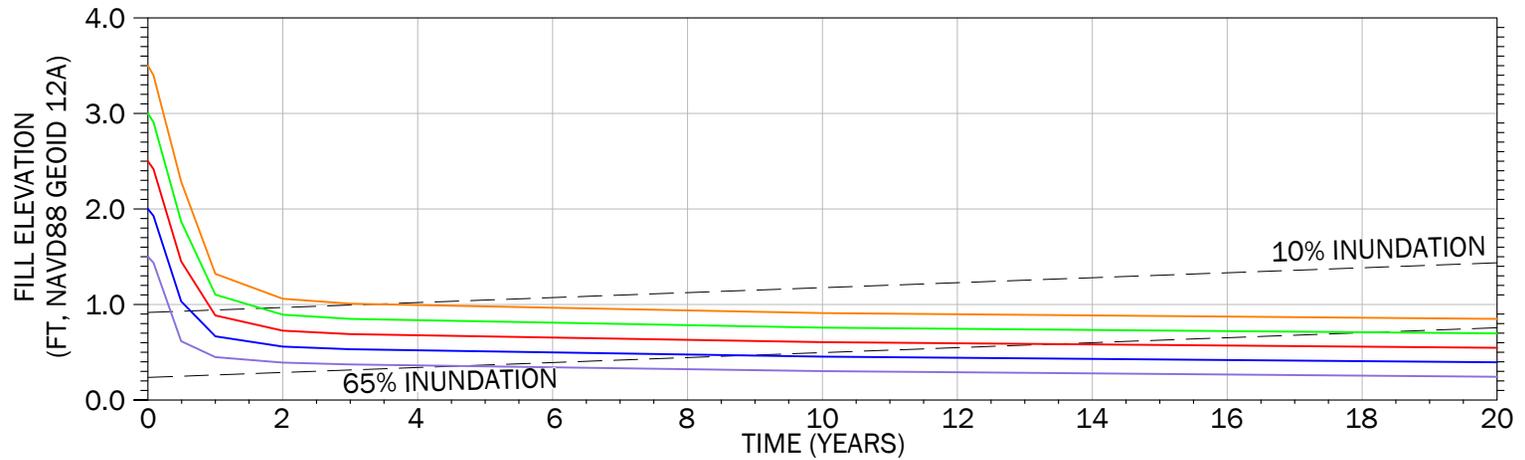
END OF CONSTRUCTION	FILL ELEVATION (FEET NAVD88)							MUDLINE ELEVATION (FEET NAVD88)	
	1 MONTH	6 MONTHS	1 YEAR	2 YEARS	3 YEARS	10 YEARS	20 YEARS	0 YEARS	20 YEARS
3.5	3.4	2.3	1.3	1.1	1.0	0.9	0.7	-0.9	-1.4
3.0	2.9	1.9	1.1	0.9	0.8	0.7	0.6	-0.9	-1.4
2.5	2.4	1.5	0.9	0.7	0.7	0.6	0.4	-0.9	-1.4
2.0	1.9	1.0	0.7	0.6	0.5	0.4	0.3	-0.9	-1.3
1.5	1.4	0.6	0.4	0.4	0.4	0.3	0.1	-0.9	-1.3

Marsh Settlement
409.2% Moisture Slurry (224 g/L)
w/ Subsidence

South Grand Chenier
 Baker Marsh Creation (ME-32)
 Cameron Parish, Louisiana

GEOENGINEERS

Figure 7b



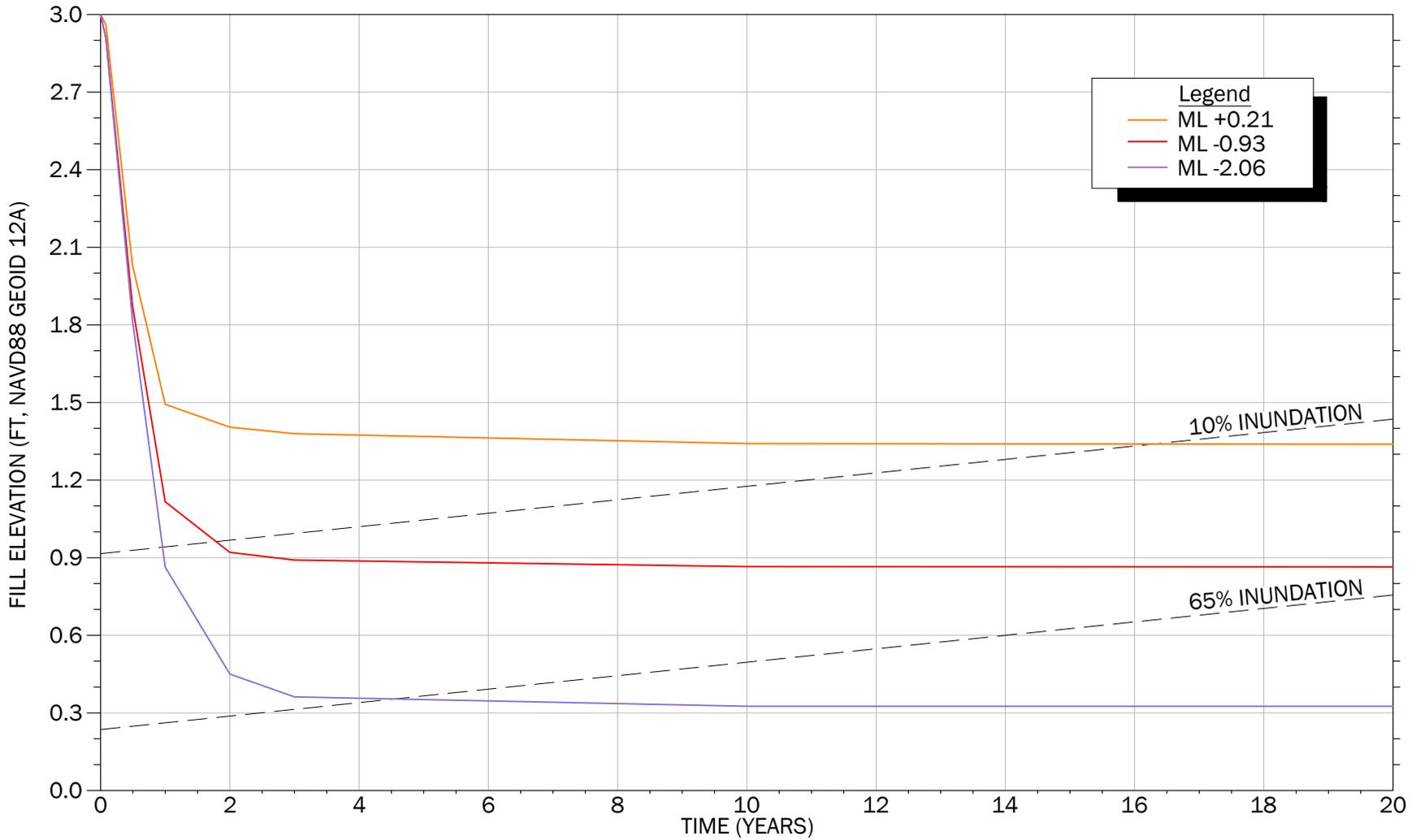
END OF CONSTRUCTION	FILL ELEVATION (FEET NAVD88)								MUDLINE ELEVATION (FEET NAVD88)	
	1 MONTH	6 MONTHS	1 YEAR	2 YEARS	3 YEARS	10 YEARS	20 YEARS	0 YEARS	20 YEARS	
3.5	3.4	2.3	1.3	1.1	1.0	0.9	0.8	-0.9	-1.4	
3.0	2.9	1.9	1.1	0.9	0.8	0.8	0.7	-0.9	-1.4	
2.5	2.4	1.5	0.9	0.7	0.7	0.6	0.5	-0.9	-1.4	
2.0	1.9	1.0	0.7	0.6	0.5	0.5	0.4	-0.9	-1.3	
1.5	1.4	0.6	0.4	0.4	0.4	0.3	0.2	-0.9	-1.3	

Marsh Settlement
409.2% Moisture Slurry (224 g/L)
w/ Subsidence & Accretion

South Grand Chenier
 Baker Marsh Creation (ME-32)
 Cameron Parish, Louisiana

GEOENGINEERS 

Figure 7c



END OF CONSTRUCTION	FILL ELEVATION (FEET NAVD88)							MUDLINE ELEVATION (FEET NAVD88)	
	1 MONTH	6 MONTHS	1 YEAR	2 YEARS	3 YEARS	10 YEARS	20 YEARS	0 YEARS	20 YEARS
3.0	3.0	2.0	1.5	1.4	1.4	1.3	1.3	0.2	-0.1
3.0	2.9	1.9	1.1	0.9	0.9	0.9	0.9	-0.9	-1.1
3.0	2.9	1.8	0.9	0.5	0.4	0.3	0.3	-2.1	-2.2

Marsh Settlement
409.2% Moisture Slurry (224 g/L)
w/ Confidence Intervals

South Grand Chenier
 Baker Marsh Creation (ME-32)
 Cameron Parish, Louisiana

GEOENGINEERS 

Figure 7d

APPENDIX A

Details of Field Exploration

APPENDIX A DETAILS OF FIELD EXPLORATION

This appendix provides additional information regarding the field exploration completed for the South Grand Chenier—Baker Marsh Creation project (ME-32).

General Field Exploration Information

GeoEngineers' field exploration took place between October 12 and November 2, 2021. Three separate rigs were used to complete our field exploration. Their use is summarized in the table below:

TABLE A-1. EXPLORATION EQUIPMENT SUMMARY

Rig Type	Start Date	End Date	Explorations Completed
Airboat-Mounted Drill Rig	October 12, 2022	October 13, 2022	6 Soil Borings
Airboat-Mounted CPT Rig	October 14, 2021	October 15, 2022	13 CPT Soundings
Boat-Based Vibracore Rig	November 2, 2022	November 2, 2022	6 Vibracores

Note:

CPT = cone penetration test

Daily field reports for this work are included in this Appendix.

Exploration Coordination

GeoEngineers contacted Louisiana “One-Call” to locate utilities prior to performing the field exploration. Exploration locations in the marsh were surveyed in the field by Fugro under a separate contract, including a magnetometer sweep around each proposed location. In addition, Fugro placed polyvinyl chloride (PVC) poles with flagging to mark the locations of the soil borings and CPT soundings. GeoEngineers used a handheld GPS receiver and the PVC poles set by Fugro to locate the exploration locations. Some locations were set on what appeared to be remnants of an old dike and were not accessible to our boat-mounted rigs. In these instances, we positioned the rig as close as possible to the marked location, but still in water accessible by boat.

Soil Borings

Six soil borings were advanced using wet rotary drilling methods with a top-drive, chain-mounted drill rig mounted on an airboat. Soil boring termination depths were 30 feet below mudline (bml) in the marsh creation area (MCA). Samples were mostly collected using an Osterberg-style fixed piston sampler and 3-inch outside diameter (O.D.), thin-wall, steel Shelby tubes in general accordance with applicable ASTM International (ASTM) standards.

Immediately upon retrieval from the subsurface, each sample was examined by our field representative and visually classified. Samples collected with Shelby tubes were examined at the bottom end of the sample for classification in the field. The tubes were then capped, labeled and stored upright to reduce the likelihood of sample disturbance during transport to a soil mechanics laboratory.

Soil borings were grouted upon completion. Soil boring logs are included in Appendix B.

CPT Soundings

Thirteen CPT soundings were completed within the proposed marsh creation area to provide supplementary soil type and shear strength information between soil borings. CPT soundings were pushed by an airboat-mounted GeoProbe 540M rig and were completed by pushing a Geotech AB 5-ton capacity CPT cone at approximately 2 centimeters per second from the mudline until refusal (generally defined for our purposes as encountering a layer hard enough to start to lift the airboat during pushing and cause the drill stem to start bending between the boat deck and the rig's hydraulic piston).

CPT data was delivered to the GeoEngineers Baton Rouge office for processing after completion of CPT sounding services. A cone factor of 0.8 was assumed during the data processing. Sounding operations were conducted in general accordance with applicable ASTM standards.

During the processing of CPT sounding data, the data was compared to the soil boring field and laboratory data to select the closest model for the soil behavior type (SBT). Multiple SBT models were evaluated; however, the model that appeared to closest fit the soil boring data was the normalized Q_t vs. B_q model (after Robertson, 1990¹) which accounts for a normalized pore pressure parameter, B_q . CPT logs developed using the normalized (Q_t vs. B_q) SBT model are presented in Appendix C.

Water Surface Elevation

The water surface elevation for the duration of the fieldwork in the marsh was obtained from a water level gauge set for the project and read each morning. Additional information regarding water levels is included in Appendix F. The nearest gage CRMS 0614 was used to validate the readings, confirming that water levels were between elevation of +0.30 ft. and +0.45 ft. (North American Vertical Datum of 1988 [NAVD88] Geoid 12A) during our field investigation.

Vibracores

Six vibracores were completed within the borrow area on November 2, 2022, using equipment deployed from an 85-foot vessel operated by American Vibracore Services, a division of Amdrill, Inc. The cores were advanced 20 feet below mudline in one continuous vibration/push inside a 3 $\frac{5}{8}$ -inch diameter polycarbonate tube. The samples were considered acceptable if a minimum of 80 percent of the core push was recovered. Upon recovery, the cores were cut into 4-foot lengths, capped, sealed, labeled and transported to GeoEngineers lab.

At the lab, the cores were weighed and measured for length to calculate density. The cores were then split longitudinally, tested for strength using a torvane in soft soil, classified/logged, photographed, and samples were collected. Vibracore logs, as well as density and strength measurements are included in Appendix D.

¹ Robertson, P.K., 1990. Soil Classification Using the Cone Penetration Test. *Canadian Geotechnical Journal*, 27(1): 151-158.



FIELD REPORT

File Number:
10883-026-0011955 Lakeland Park Blvd., Suite 100
Baton Rouge, LA 70809
225.293.2460Project:
Grand Chenier Marsh Creation ProjectDate:
10/12/2022Client:
ECM Consultants Inc.Time of Arrival:
8:30Report Number:
DFR-1Prepared by:
Neil L. TrahanLocation:
New Orleans, LouisianaTime of Departure:
17:30Page:
1 of 6Purpose of visit:
Geotechnical ExplorationWeather:
Partly Cloudy; 80-90 °FTravel Time:
3.0 hours

Permit Number:

Please refer to attached safety documentation.

Personnel and Equipment

GeoEngineers, Inc. Field Representative: Neil Trahan

Drilling Company: Specialized Environmental Resources (SER)

Drilling Personnel: Drake Blanchard (Driller), Everette Segura (Roughneck) & Jayce Hulin (Roughneck)

Drilling Equipment: Airboat-mounted Drill Rig

Support Equipment: SER Support Boat (2), SER Pickup Truck (3), GeoEngineers' Pickup Truck

GEOTECHNICAL BORINGS STATUS TABLE

BORING NAME	WATER DEPTH	BORING DEPTH	TODAY (FEET)	TO DATE (FEET)	% COMPLETE
B-1	2'4"	30	30	30	100%
B-2	1'7"	30	30	30	100%
B-3		30	0	0	0%
B-4		30	0	0	0%
B-5	1'10"	30	30	30	100%
B-6		30	0	0	0%
C-1		40	0	0	0%
C-2		40	0	0	0%
C-3		40	0	0	0%
C-4		40	0	0	0%
C-5		40	0	0	0%
C-6		40	0	0	0%
C-7		40	0	0	0%
C-8		40	0	0	0%
C-9		40	0	0	0%
C-10		40	0	0	0%

THIS FIELD REPORT IS PRELIMINARY
A preliminary report is provided solely as evidence that field observation was performed. Observations and/or conclusions and/or recommendations conveyed in the final report may vary from and shall take precedence over those indicated in a preliminary report.

FIELD REPRESENTATIVE
Neil L. Trahan

DATE
10/12/2022

THIS FIELD REPORT IS FINAL
A final report is an instrument of professional service. Any conclusions drawn from this report should be discussed with and evaluated by the professional involved.

REVIEWED BY
Nafi Haque, PE

DATE
10/13/2022

This report presents opinions formed as a result of our observation of activities relating to our services only. We rely on the contractor to comply with the plans and specification throughout the duration of the project irrespective of the presence of our representative. Our work does not include supervision or direction of the work of others. Our firm will not be responsible for job or site safety of others on this project. **DISCLAIMER:** Any electronic form, facsimile or hard copy of the original document (email, text, table, and/or figure), if provided, and any attachments are only a copy of the original document. The original document is stored by GeoEngineers, Inc. and will serve as the official document of record.

Attachments: None

C-11		40	0	0	0%
C-12		40	0	0	0%
C-13		40	0	0	0%

Observations and Activities:

- 06:30 I (Neil Trahan of GeoEngineers, Inc. [GeoEngineers]) leave my residence and mobilize to the Grand Chenier Marsh Creation Project boat launch, located in Grand Chenier, Louisiana.
- 08:30 I arrive at the boat launch and meet with the SER Drilling Personnel; I begin conducting a tailgate safety meeting.
- 08:45 The tailgate safety meeting concludes; all parties have reviewed and signed the GeoEngineers' Job Hazard Analysis (JHA). SER begin launching the drilling equipment and preparing for mobilization.
- 10:00 SER has finished launching the drilling equipment, and we mobilize to an area north of C-8 to install a survey stake.
- 10:05 We arrive at the area north of C-8, located at approximately 29° 42' 40" N, 92° 51' 02" W, and install the survey stake. The survey stake measures 5-foot 3 inches from the top of the stake to the water line.
- 10:15 We begin mobilization to Geotechnical Boring B-1.
- 10:30 We arrive at Geotechnical Boring B-1 and begin preparing for drilling and sampling operations. Worksite conditions before drilling and sampling operations can be seen in the photograph below.



**PRE-DRILL CONDITION OF GEOTECHNICAL BORING B-1
(LOOKING NORTHWARD)**

- 10:45 Subsurface exploration of Geotechnical Boring B-1 begins.
- 11:45 We suspend drilling and sampling operations and begin a lunch break.
- 12:15 We resume drilling and sampling operations.

- 12:35 We complete drilling and sampling Geotechnical Boring B-1 and SER begin grouting the bore hole. We have drilled Geotechnical Boring B-1 to a depth of 30 feet below the mudline (bml); drilling and sampling continuously from the mudline to 20 feet bml, and on five (5) foot centers from 20 feet bml to 30 feet bml.
- 12:50 SER has finished grouting Geotechnical Boring B-1 and we begin mobilization to Geotechnical Boring B-2. Worksite conditions after drilling and sampling operations can be seen in the photograph below.



**POST-DRILL CONDITION OF GEOTECHNICAL BORING B-1
(LOOKING NORTHWARD)**

- 13:00 We arrive at Geotechnical Boring B-2; SER begins spudding the drilling equipment and we prepare for drilling and sampling operations. Worksite conditions before drilling and sampling operations can be seen in the photograph below.



**PRE-DRILL CONDITION OF GEOTECHNICAL BORING B-2
(LOOKING SOUTHWARD)**

- 13:10 Subsurface exploration of Geotechnical Boring B-2 begins.
- 14:50 We complete drilling and sampling Geotechnical Boring B-2 and SER begin grouting the bore hole. We have drilled Geotechnical Boring B-2 to a depth of 30 feet below the mudline (bml); drilling and sampling continuously from the mudline to 20 feet bml, and on five (5) foot centers from 20 feet bml to 30 feet bml.
- 15:10 SER has finished grouting Geotechnical Boring B-2 and we begin mobilization to Geotechnical Boring B-5. Worksite conditions after drilling and sampling operations can be seen in the photograph below.



**POST-DRILL CONDITION OF GEOTECHNICAL BORING B-2
(LOOKING SOUTHWARD)**

15:20 We arrive at Geotechnical Boring B-5; SER begins spudding the drilling equipment and we prepare for drilling and sampling operations. Worksite conditions before drilling and sampling operations can be seen in the photograph below.



**PRE-DRILL CONDITION OF GEOTECHNICAL BORING B-5
(LOOKING SOUTHWARD)**

15:30 Subsurface exploration of Geotechnical Boring B-5 begins.

17:10 We complete drilling and sampling Geotechnical Boring B-5 and SER begin grouting the bore hole. We have drilled Geotechnical Boring B-5 to a depth of 30 feet below the mudline (bml); drilling and sampling continuously from the mudline to 20 feet bml, and on five (5) foot centers from 20 feet bml to 30 feet bml.

17:30 SER has finished grouting Geotechnical Boring B-5 and we begin mobilization to the boat launch. Worksite conditions after drilling and sampling operations can be seen in the photograph below.



**POST-DRILL CONDITION OF GEOTECHNICAL BORING B-5
(LOOKING SOUTHWARD)**

17:45 We arrive at the boat launch and begin transferring samples onto the pickup truck.

17:50 We have finished transferring samples onto the pickup truck and I mobilize to the hotel, located in Lake Charles, Louisiana.

18:50 I arrive at the hotel.



FIELD REPORT

File Number:
10883-026-0011955 Lakeland Park Blvd., Suite 100
Baton Rouge, LA 70809
225.293.2460Project:
Grand Chenier Marsh Creation ProjectDate:
10/13/2022Client:
ECM Consultants Inc.Time of Arrival:
7:30Report Number:
DFR-2Prepared by:
Neil L. TrahanLocation:
New Orleans, LouisianaTime of Departure:
15:45Page:
1 of 6Purpose of visit:
Geotechnical ExplorationWeather:
Sunny; 70-85 °FTravel Time:
5.75 hours

Permit Number:

Please refer to attached safety documentation.

Personnel and Equipment

GeoEngineers, Inc. Field Representative: Neil Trahan

Drilling Company: Specialized Environmental Resources (SER)

Drilling Personnel: Drake Blanchard (Driller), Everette Segura (Roughneck) & Jayce Hulin (Roughneck)

Drilling Equipment: Airboat-mounted CPT Rig

Support Equipment: SER Support Boat, SER Pickup Truck (2), GeoEngineers' Pickup Truck

GEOTECHNICAL BORINGS STATUS TABLE

BORING NAME	WATER DEPTH	BORING DEPTH	TODAY (FEET)	TO DATE (FEET)	% COMPLETE
B-1	2'4"	30	0	30	100%
B-2	1'7"	30	0	30	100%
B-3	1'8"	30	30	30	100%
B-4	1'10"	30	30	30	100%
B-5	1'10"	30	0	30	100%
B-6	1'10"	30	30	30	100%
C-1		40	0	0	0%
C-2		40	0	0	0%
C-3		40	0	0	0%
C-4		40	0	0	0%
C-5		40	0	0	0%
C-6		40	0	0	0%
C-7		40	0	0	0%
C-8		40	0	0	0%
C-9		40	0	0	0%
C-10		40	0	0	0%

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FIELD REPRESENTATIVE
Neil L. Trahan

DATE
10/13/2022

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A final report is an instrument of professional service. Any conclusions drawn from this report should be discussed with and evaluated by the professional involved.

REVIEWED BY
Nafi Haque, PE

DATE
10/14/2022

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Attachments: None

C-11	40	0	0	0%
C-12	40	0	0	0%
C-13	40	0	0	0%

Observations and Activities:

- 06:30 I (Neil Trahan of GeoEngineers, Inc. [GeoEngineers]) leave the hotel and mobilize to the Grand Chenier Marsh Creation Project boat launch, located in Grand Chenier, Louisiana.
- 07:30 I arrive at the boat launch and meet with the SER Drilling Personnel; I begin conducting a tailgate safety meeting.
- 07:45 The tailgate safety meeting concludes; all parties have reviewed and signed the GeoEngineers' Job Hazard Analysis (JHA). We standby for inclement weather to pass overhead.
- 08:30 The weather has cleared, we begin mobilizing to the survey stake, located north of C-8.
- 08:35 We arrive at the survey stake and take a measurement from the top of the survey stake to the water line, which measures 5-foot 2-inches. We mobilize to the CPT rig.
- 08:45 We arrive at the drilling equipment and begin preparing for mobilization to Geotechnical Boring B-6.
- 09:00 We begin mobilization to Geotechnical Boring B-6.
- 09:10 We arrive at Geotechnical Boring B-6 and begin preparing for drilling and sampling operations. Worksite conditions before drilling and sampling operations can be seen in the photograph below.



**PRE-DRILL CONDITION OF GEOTECHNICAL BORING B-6
(LOOKING NORTHEASTWARD)**

- 09:15 Subsurface exploration of Geotechnical Boring B-6 begins.
- 11:15 We complete drilling and sampling Geotechnical Boring B-6 and SER begin grouting the bore hole. We have drilled Geotechnical Boring B-6 to a depth of 30 feet below the mudline (bml); drilling and sampling continuously from the mudline to 20 feet bml, and on five (5) foot centers from 20 feet bml to 30 feet bml.

11:30 SER has finished grouting Geotechnical Boring B-6 and we begin mobilization to Geotechnical Boring B-3. Worksite conditions after drilling and sampling operations can be seen in the photograph below.



**POST-DRILL CONDITION OF GEOTECHNICAL BORING B-6
(LOOKING NORTHEASTWARD)**

11:40 We arrive at Geotechnical Boring B-3; SER begins spudding the drilling equipment and we prepare for drilling and sampling operations. Worksite conditions before drilling and sampling operations can be seen in the photograph below.



**PRE-DRILL CONDITION OF GEOTECHNICAL BORING B-3
(LOOKING NORTHEASTWARD)**

- 11:45 Subsurface exploration of Geotechnical Boring B-3 begins.
- 12:00 We suspend drilling and sampling operations and begin a lunch break.
- 12:30 We resume drilling and sampling operations.
- 13:00 We complete drilling and sampling Geotechnical Boring B-3 and SER begin grouting the bore hole. We have drilled Geotechnical Boring B-3 to a depth of 30 feet below the mudline (bml); drilling and sampling continuously from the mudline to 20 feet bml, and on five (5) foot centers from 20 feet bml to 30 feet bml.
- 13:15 SER has finished grouting Geotechnical Boring B-3 and we begin mobilization to Geotechnical Boring B-4. Worksite conditions after drilling and sampling operations can be seen in the photograph below.



**POST-DRILL CONDITION OF GEOTECHNICAL BORING B-3
(LOOKING NORTHEASTWARD)**

13:20 We arrive at Geotechnical Boring B-4; SER begins spudding the drilling equipment and we prepare for drilling and sampling operations. Worksite conditions before drilling and sampling operations can be seen in the photograph below.



**PRE-DRILL CONDITION OF GEOTECHNICAL BORING B-4
(LOOKING NORTHEASTWARD)**

13:25 Subsurface exploration of Geotechnical Boring B-4 begins.

- 15:00 We complete drilling and sampling Geotechnical Boring B-4 and SER begin grouting the bore hole. We have drilled Geotechnical Boring B-4 to a depth of 30 feet below the mudline (bml); drilling and sampling continuously from the mudline to 20 feet bml, and on five (5) foot centers from 20 feet bml to 30 feet bml.
- 15:15 SER has finished grouting Geotechnical Boring B-4 and we begin mobilization to the boat launch. Worksite conditions after drilling and sampling operations can be seen in the photograph below.



**POST-DRILL CONDITION OF GEOTECHNICAL BORING B-4
(LOOKING NORTHEASTWARD)**

- 15:30 We arrive at the boat launch and begin transferring samples onto the pickup truck.
- 15:45 We have finished transferring samples onto the pickup truck and I mobilize to the GeoEngineers' Offices, located in Baton Rouge, Louisiana.
- 18:45 I arrive at the GeoEngineers' Offices and begin to unload the samples and check them in.
- 19:15 I have finished unloading the samples and I mobilize to the hotel, located in Lake Charles, Louisiana.
- 21:15 I arrive at the hotel.



FIELD REPORT

File Number:
10883-026-0011955 Lakeland Park Blvd., Suite 100
Baton Rouge, LA 70809
225.293.2460Project:
Grand Chenier Marsh Creation ProjectDate:
10/14/2022Client:
ECM Consultants Inc.Time of Arrival:
7:30Report Number:
DFR-3Prepared by:
Neil L. TrahanLocation:
Grand Chenier, LouisianaTime of Departure:
15:00Page:
1 of 7Purpose of visit:
Geotechnical ExplorationWeather:
Sunny; 70-85 °FTravel Time:
2 hours

Permit Number:

Please refer to attached safety documentation.

Personnel and Equipment

GeoEngineers, Inc. Field Representative: Neil Trahan

Drilling Company: Specialized Environmental Resources (SER)

Drilling Personnel: Drake Blanchard (Driller), Everette Segura (Roughneck) & Jayce Hulin (Roughneck)

Drilling Equipment: Airboat-mounted CPT Rig

Support Equipment: SER Support Boat, SER Pickup Truck (2), GeoEngineers' Pickup Truck

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B-4	1'10"	30	0	30	100%
B-5	1'10"	30	0	30	100%
B-6	1'10"	30	0	30	100%
C-1		40	0	0	0%
C-2		40	0	0	0%
C-3		40	0	0	0%
C-4		40	0	0	0%
C-5	3'10"	26.3	26.3	26.3	100%
C-6	2'0"	26.1	26.1	26.1	100%
C-7	1'6"	25.2	25.2	25.2	100%
C-8		40	0	0	0%
C-9		40	0	0	0%
C-10		40	0	0	0%

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FIELD REPRESENTATIVE
 Neil L. Trahan **DATE**
 10/14/2022

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REVIEWED BY
 Nafi Haque, PE **DATE**
 10/15/2022

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Attachments: None

C-11		40	0	0	0%
C-12		40	0	0	0%
C-13		40	0	0	0%

Observations and Activities:

- 06:30 I (Neil Trahan of GeoEngineers, Inc. [GeoEngineers]) leave the hotel and mobilize to the Grand Chenier Marsh Creation Project boat launch, located in Grand Chenier, Louisiana.
- 07:30 I arrive at the boat launch and meet with the SER Drilling Personnel; I begin conducting a tailgate safety meeting.
- 07:45 The tailgate safety meeting concludes; all parties have reviewed and signed the GeoEngineers' Job Hazard Analysis (JHA). We begin setting up the CPT equipment on the CPT rig.
- 10:30 We have finished setting up the CPT equipment and SER begin launching the CPT rig.
- 11:30 SER has finished launching the CPT rig and we mobilize to the survey stake, located north of C-8.
- 11:40 We arrive at the survey stake and take a measurement from the top of the survey stake to the water line, which measures 5-foot 2-inches. We mobilize to C-8.
- 11:45 We arrive at C-8 and begin preparing for sounding operations. Worksite conditions before drilling and sampling operations can be seen in the photograph below.



PRE-SOUNDING CONDITION OF C-8 (LOOKING SOUTHWESTWARD)

- 12:00 We begin CPT operations at C-8.
- 12:40 We complete CPT operations at C-8, terminating the sounding at a depth of 25.9 feet below the mudline (bml). SER grout C-8 and we prepare to mobilize to the location of C-7.
- 12:50 SER has finished grouting C-8 and we begin mobilization to C-7. Worksite conditions after drilling and sampling operations can be seen in the photograph below.



POST-SOUNDING CONDITION OF C-8 (LOOKING SOUTHWESTWARD)

13:00 We arrive at C-7 and begin preparing for sounding operations. Worksite conditions before drilling and sampling operations can be seen in the photograph below.



PRE-SOUNDING CONDITION OF C-7 (LOOKING SOUTHWESTWARD)

13:10 We halt CPT operations and begin changing the cone sensor due to the friction values not recording properly.

14:15 I have finished changing the cone sensor on the CPT equipment, and we begin sounding operations at C-7.

14:40 We complete CPT operations at C-7, terminating the sounding at a depth of 25.2 feet below the mudline (bml). SER grout C-7 and we prepare to mobilize to the location of C-6.

14:55 SER has finished grouting C-7 and we begin mobilization to C-6. Worksite conditions after drilling and sampling operations can be seen in the photograph below.



POST-SOUNDING CONDITION OF C-7 (LOOKING SOUTHWESTWARD)

15:00 We arrive at C-6 and begin preparing for sounding operations. Worksite conditions before drilling and sampling operations can be seen in the photograph below.



PRE-SOUNDING CONDITION OF C-6 (LOOKING NORTHWARD)

15:10 We begin CPT operations at C-6.

15:35 We complete CPT operations at C-6, terminating the sounding at a depth of 26.1 feet below the mudline (bml). SER grout C-6 and we prepare to mobilize to the location of C-5.

15:45 SER has finished grouting C-6 and we begin mobilization to C-5. Worksite conditions after drilling and sampling operations can be seen in the photograph below.



POST-SOUNDING CONDITION OF C-6 (LOOKING NORTHWARD)

15:50 We arrive at C-5 and begin preparing for sounding operations. Worksite conditions before drilling and sampling operations can be seen in the photograph below.



PRE-SOUNDING CONDITION OF C-5 (LOOKING NORTHWARD)

15:55 We begin CPT operations at C-5.

16:15 We complete CPT operations at C-5, terminating the sounding at a depth of 26.3 feet below the mudline (bml). SER grout C-5 and we prepare to mobilize to the boat launch.

16:25 SER has finished grouting C-5 and we begin mobilization to the boat launch. Worksite conditions after drilling and sampling operations can be seen in the photograph below.



POST-SOUNDING CONDITION OF C-5 (LOOKING NORTHWARD)

16:45 We arrive at the boat launch and begin securing the CPT equipment.

17:00 We have finished securing the CPT equipment; all parties depart the worksite. I travel to the hotel.

18:00 I arrive at the hotel.



FIELD REPORT

File Number:
10883-026-0011955 Lakeland Park Blvd., Suite 100
Baton Rouge, LA 70809
225.293.2460Project:
Grand Chenier Marsh Creation ProjectDate:
10/15/2022Client:
ECM Consultants Inc.Time of Arrival:
7:30Report Number:
DFR-4Prepared by:
Neil L. TrahanLocation:
Grand Chenier, LouisianaTime of Departure:
15:10Page:
1 of 13Purpose of visit:
Geotechnical ExplorationWeather:
Sunny; 70-85 °FTravel Time:
2.75 hours

Permit Number:

Please refer to attached safety documentation.

Personnel and Equipment

GeoEngineers, Inc. Field Representative: Neil Trahan

Drilling Company: Specialized Environmental Resources (SER)

Drilling Personnel: Drake Blanchard (Driller), Everette Segura (Roughneck) & Jayce Hulin (Roughneck)

Drilling Equipment: Airboat-mounted CPT Rig

Support Equipment: SER Support Boat, SER Pickup Truck (2), GeoEngineers' Pickup Truck

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B-2	1'7"	30	0	30	100%
B-3	1'8"	30	0	30	100%
B-4	1'10"	30	0	30	100%
B-5	1'10"	30	0	30	100%
B-6	1'10"	30	0	30	100%
C-1	1'8"	25.1	25.1	25.1	100%
C-2	3'0"	25.3	25.3	25.3	100%
C-3	1'11"	24.8	24.8	24.8	100%
C-4	1'5"	23	23	23	100%
C-5	3'10"	26.3	0	26.3	100%
C-6	2'0"	26.1	0	26.1	100%
C-7	1'6"	25.2	0	25.2	100%
C-8	1'6"	24.4	24.4	24.4	100%
C-9	1'9"	24.6	24.6	24.6	100%
C-10	2'9"	27.2	27.2	27.2	100%

 THIS FIELD REPORT IS PRELIMINARY

A preliminary report is provided solely as evidence that field observation was performed. Observations and/or conclusions and/or recommendations conveyed in the final report may vary from and shall take precedence over those indicated in a preliminary report.

FIELD REPRESENTATIVE

Neil L. Trahan

DATE

10/15/2022

 THIS FIELD REPORT IS FINAL

A final report is an instrument of professional service. Any conclusions drawn from this report should be discussed with and evaluated by the professional involved.

REVIEWED BY

Nafi Haque, PE

DATE

10/16/2022

This report presents opinions formed as a result of our observation of activities relating to our services only. We rely on the contractor to comply with the plans and specification throughout the duration of the project irrespective of the presence of our representative. Our work does not include supervision or direction of the work of others. Our firm will not be responsible for job or site safety of others on this project. **DISCLAIMER:** Any electronic form, facsimile or hard copy of the original document (email, text, table, and/or figure), if provided, and any attachments are only a copy of the original document. The original document is stored by GeoEngineers, Inc. and will serve as the official document of record.

Attachments: None

C-11	1'8"	26.1	26.1	26.1	100%
C-12	2'4"	25.7	25.7	25.7	100%
C-13	2'0"	30.2	30.2	30.2	100%

Observations and Activities:

- 06:30 I (Neil Trahan of GeoEngineers, Inc. [GeoEngineers]) leave the hotel and mobilize to the Grand Chenier Marsh Creation Project boat launch, located in Grand Chenier, Louisiana.
- 07:30 I arrive at the boat launch and meet with the SER Drilling Personnel; I begin conducting a tailgate safety meeting.
- 07:45 The tailgate safety meeting concludes; all parties have reviewed and signed the GeoEngineers' Job Hazard Analysis (JHA). We begin mobilizing to the survey stake, located north of C-8.
- 07:50 We arrive at the survey stake and take a measurement from the top of the survey stake to the water line, which measures 5-foot 3-inches. We mobilize to the CPT rig.
- 08:00 We arrive at the CPT rig and begin preparing for mobilization to C-4.
- 08:05 We arrive at C-4 and begin preparing for sounding operations. Worksite conditions before drilling and sampling operations can be seen in the photograph below.



PRE-SOUNDING CONDITION OF C-4 (LOOKING SOUTHWESTWARD)

- 08:10 We begin CPT operations at C-4.
- 08:35 We complete CPT operations at C-4, terminating the sounding at a depth of 23 feet below the mudline (bml). SER grout C-4 and we prepare to mobilize to the location of C-3.
- 08:45 SER has finished grouting C-4 and we begin mobilization to C-3. Worksite conditions after drilling and sampling operations can be seen in the photograph below.



POST-SOUNDING CONDITION OF C-4 (LOOKING SOUTHWESTWARD)

08:50 We arrive at C-3 and begin preparing for sounding operations. Worksite conditions before drilling and sampling operations can be seen in the photograph below.



PRE-SOUNDING CONDITION OF C-3 (LOOKING WESTWARD)

08:55 We begin sounding operations at C-3.

09:25 We complete CPT operations at C-3, terminating the sounding at a depth of 24.8 feet below the mudline (bml). SER grout C-3 and we prepare to mobilize to the location of C-1.

09:35 SER has finished grouting C-3 and we begin mobilization to C-1. Worksite conditions after drilling and sampling operations can be seen in the photograph below.



POST-SOUNDING CONDITION OF C-3 (LOOKING WESTWARD)

09:40 We arrive at C-1 and begin preparing for sounding operations. Worksite conditions before drilling and sampling operations can be seen in the photograph below.



PRE-SOUNDING CONDITION OF C-1 (LOOKING NORTHWESTWARD)

09:45 We begin CPT operations at C-1.

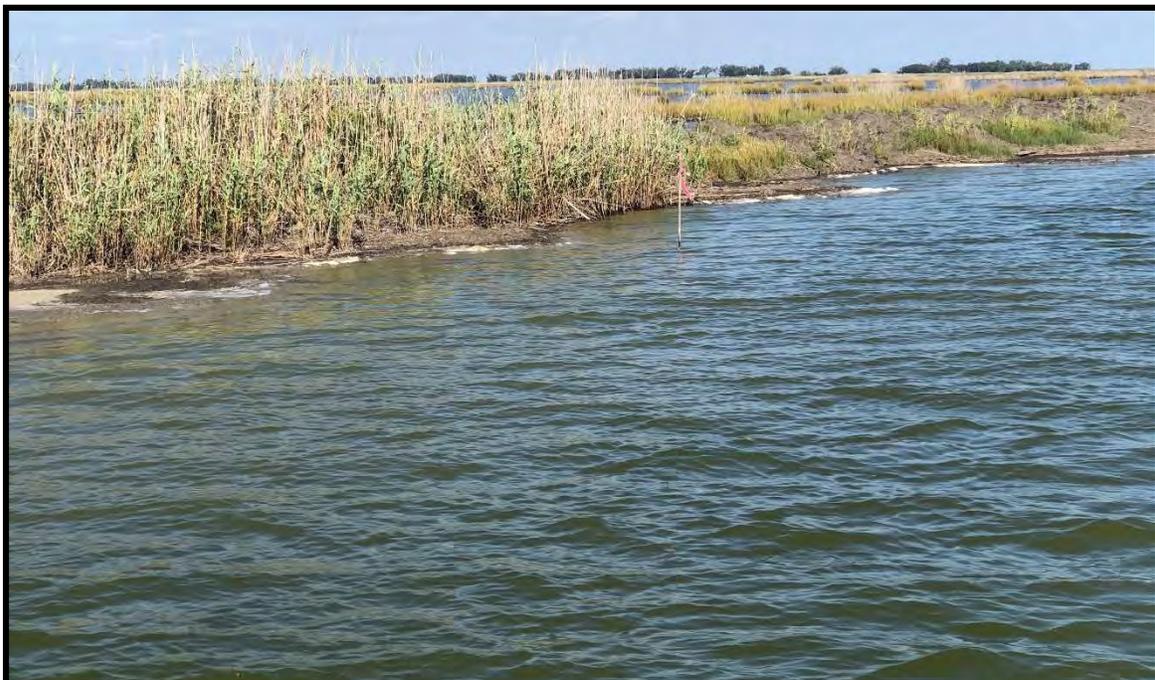
10:15 We complete CPT operations at C-1, terminating the sounding at a depth of 25.1 feet below the mudline (bml). SER grout C-1 and we prepare to mobilize to the location of C-13.

10:25 SER has finished grouting C-1 and we begin mobilization to C-13. Worksite conditions after drilling and sampling operations can be seen in the photograph below.



POST-SOUNDING CONDITION OF C-1 (LOOKING NORTHWESTWARD)

10:30 We arrive at C-13 and begin preparing for sounding operations. Worksite conditions before drilling and sampling operations can be seen in the photograph below.



PRE-SOUNDING CONDITION OF C-13 (LOOKING NORTHWESTWARD)

10:35 We begin CPT operations at C-13.

11:05 We complete CPT operations at C-13, terminating the sounding at a depth of 30.2 feet below the mudline (bml). SER grout C-13 and we prepare to mobilize to C-12.



POST-SOUNDING CONDITION OF C-13 (LOOKING NORTHWESTWARD)

11:10 We arrive at C-12 and begin preparing for sounding operations. Worksite conditions before drilling and sampling operations can be seen in the photograph below.



PRE-SOUNDING CONDITION OF C-12 (LOOKING SOUTHEASTWARD)

11:15 We begin CPT operations at C-12.

11:45 We complete CPT operations at C-12, terminating the sounding at a depth of 25.7 feet below the mudline (bml). SER grout C-12 and we prepare to mobilize to the location of C-2.

11:55 SER has finished grouting C-12 and we begin mobilization to C-2. Worksite conditions after drilling and sampling operations can be seen in the photograph below.



POST-SOUNDING CONDITION OF C-12 (LOOKING SOUTHEASTWARD)

12:00 We arrive at C-2 and begin preparing for sounding operations. Worksite conditions before drilling and sampling operations can be seen in the photograph below.



PRE-SOUNDING CONDITION OF C-2 (LOOKING SOUTHEASTWARD)

12:05 We begin sounding operations at C-2.

12:35 We complete CPT operations at C-2, terminating the sounding at a depth of 25.3 feet below the mudline (bml). SER grout C-2 and we prepare to mobilize to the location of C-11.

12:45 SER has finished grouting C-2 and we begin mobilization to C-11. Worksite conditions after drilling and sampling operations can be seen in the photograph below.



POST-SOUNDING CONDITION OF C-2 (LOOKING SOUTHEASTWARD)

12:55 We arrive at C-11 and begin a lunch break.

13:25 We begin preparing for sounding operations. Worksite conditions before drilling and sampling operations can be seen in the photograph below.



PRE-SOUNDING CONDITION OF C-11 (LOOKING NORTHEASTWARD)

13:30 We begin CPT operations at C-11.

14:00 We complete CPT operations at C-11, terminating the sounding at a depth of 26.1 feet below the mudline (bml). SER grout C-11 and we prepare to mobilize to the location of C-10.

14:10 SER has finished grouting C-11 and we begin mobilization to C-10. Worksite conditions after drilling and sampling operations can be seen in the photograph below.



POST-SOUNDING CONDITION OF C-11 (LOOKING NORTHEASTWARD)

14:25 We arrive at C-10 and begin preparing for sounding operations. Worksite conditions before drilling and sampling operations can be seen in the photograph below.



PRE-SOUNDING CONDITION OF C-10 (LOOKING SOUTHEASTWARD)

14:30 We begin CPT operations at C-10.

15:00 We complete CPT operations at C-10, terminating the sounding at a depth of 27.2 feet below the mudline (bml). SER grout C-10 and we prepare to mobilize to C-9.

15:10 SER has finished grouting C-10 and we mobilize to C-9. Worksite conditions after sounding operations can be seen in the photograph below.



POST-SOUNDING CONDITION OF C-10 (LOOKING SOUTHEASTWARD)

15:15 We arrive at C-9 and begin preparing for sounding operations. Worksite conditions before drilling and sampling operations can be seen in the photograph below.



PRE-SOUNDING CONDITION OF C-9 (LOOKING NORTHEASTWARD)

15:20 We begin CPT operations at C-9.

15:50 We complete CPT operations at C-9, terminating the sounding at a depth of 24.6 feet below the mudline (bml). SER grout C-9 and we prepare to mobilize to the location of C-8.

16:00 SER has finished grouting C-9 and we begin mobilization to C-8. Worksite conditions after drilling and sampling operations can be seen in the photograph below.



POST-SOUNDING CONDITION OF C-9 (LOOKING NORTHEASTWARD)

16:05 We arrive at C-8 and begin preparing for sounding operations. Worksite conditions before drilling and sampling operations can be seen in the photograph below.



PRE-SOUNDING CONDITION OF C-8 (LOOKING SOUTHWARD)

16:10 We begin sounding operations at C-8.

16:30 We complete CPT operations at C-8, terminating the sounding at a depth of 24.4 feet below the mudline (bml). SER grout C-8 and we prepare to mobilize to the boat launch.

16:40 SER has finished grouting C-8 and we begin mobilization to the boat launch. Worksite conditions after drilling and sampling operations can be seen in the photograph below.



POST-SOUNDING CONDITION OF C-8 (LOOKING SOUTHWARD)

16:50 We arrive at the boat launch and begin offloading the CPT equipment and loading the airboats onto the trailers.

17:10 We have finished offloading the CPT equipment and loading the airboats onto the trailers; all parties depart the worksite. I travel to my residence, located in Lafayette, Louisiana.

18:55 I arrive at my residence.



FIELD REPORT

File Number:
10883-026-0011955 Lakeland Park Blvd., Suite 100
Baton Rouge, LA 70809
225.293.2460Project:
Grand Chenier Marsh Creation ProjectDate:
11/02/2022Client:
ECM Consultants Inc.Time of Arrival:
7:30Report Number:
DFR-5Prepared by:
Neil L. TrahanLocation:
Grand Chenier, LouisianaTime of Departure:
15:10Page:
1 of 2Purpose of visit:
Geotechnical ExplorationWeather:
Partly Cloudy; 70-85 °FTravel Time:
4.25 hours

Permit Number:

Please refer to attached safety documentation.

Personnel and Equipment

GeoEngineers, Inc. Field Representative: Neil Trahan

Sampling Company: American Vibracore Services (AVS)

Sampling Personnel: Brian Simmons (Captain), Caleb Simmons (Deckhand), Michael Knight Jr. (Deckhand), Myles Nagy (Deckhand) & Kenneth Neeley (Deckhand)

Sampling Equipment: 85-foot Vessel ("Thunderforce")

Support Equipment: AVS Pickup Truck (1), GeoEngineers' Pickup Truck (1)

GEOTECHNICAL BORINGS STATUS TABLE

BORING NAME	BORING DEPTH	WATER DEPTH	TODAY (FEET)	RECOVERY (FEET)	TO DATE (FEET)	% COMPLETE
V-1	20	23	20	17	20	100%
V-2	20	23	20	16.6	20	100%
V-3	20	23	20	16	20	100%
V-4	20	23	20	16	20	100%
V-5	20	23	20	16.8	20	100%
V-6	20	23	20	16	20	100%

Observations and Activities:

05:45 I (Neil Trahan of GeoEngineers, Inc. [GeoEngineers]) leave my residence in Lafayette, Louisiana, and mobilize to the Grand Chenier Marsh Creation Project boat dock, located in Creole, Louisiana.

07:30 I arrive at the boat dock and meet with Captain Brian Simmons and the AVS Personnel; I begin conducting a tailgate safety meeting.

07:45 The tailgate safety meeting concludes; all parties have reviewed and signed the GeoEngineers' Job Hazard Analysis (JHA). We begin preparing for mobilization to V-1.

08:45 AVS has finished preparing for mobilization, and we mobilize to the location of V-1.

 THIS FIELD REPORT IS PRELIMINARY

A preliminary report is provided solely as evidence that field observation was performed. Observations and/or conclusions and/or recommendations conveyed in the final report may vary from and shall take precedence over those indicated in a preliminary report.

FIELD REPRESENTATIVE

Neil L. Trahan

DATE

11/02/2022

 THIS FIELD REPORT IS FINAL

A final report is an instrument of professional service. Any conclusions drawn from this report should be discussed with and evaluated by the professional involved.

REVIEWED BY

Nafi Haque, PE

DATE

11/03/2022

This report presents opinions formed as a result of our observation of activities relating to our services only. We rely on the contractor to comply with the plans and specification throughout the duration of the project irrespective of the presence of our representative. Our work does not include supervision or direction of the work of others. Our firm will not be responsible for job or site safety of others on this project. **DISCLAIMER:** Any electronic form, facsimile or hard copy of the original document (email, text, table, and/or figure), if provided, and any attachments are only a copy of the original document. The original document is stored by GeoEngineers, Inc. and will serve as the official document of record.

Attachments: None

- 10:30 We arrive at V-1 and AVS begin preparing for vibracore sampling.
- 10:34 AVS begins vibracore sampling at V-1.
- 10:37 AVS has completed vibracore sampling at V-1, terminating at a depth of 20 feet below the mudline (bml). AVS Personnel begin cutting and sealing the sampling tube into 4-foot sections while Captain Brian Simmons begins mobilization to the location of V-4.
- 10:50 We arrive at V-4 and AVS begin preparing for vibracore sampling.
- 10:56 AVS begins vibracore sampling at V-4.
- 10:58 AVS has completed vibracore sampling at V-4, terminating at a depth of 20 feet below the mudline (bml). AVS Personnel begin cutting and sealing the sampling tube into 4-foot sections while Captain Brian Simmons begins mobilization to the location of V-5.
- 11:30 We arrive at V-5 and AVS begin preparing for vibracore sampling.
- 11:34 AVS begins vibracore sampling at V-5.
- 11:36 AVS has completed vibracore sampling at V-5, terminating at a depth of 20 feet below the mudline (bml). AVS Personnel begin cutting and sealing the sampling tube into 4-foot sections while Captain Brian Simmons begins mobilization to the location of V-2.
- 11:55 We arrive at V-2 and AVS begin preparing for vibracore sampling.
- 11:58 AVS begins vibracore sampling at V-2.
- 12:01 AVS has completed vibracore sampling at V-2, terminating at a depth of 20 feet below the mudline (bml). AVS Personnel begin cutting and sealing the sampling tube into 4-foot sections while Captain Brian Simmons begins mobilization to the location of V-6.
- 12:10 We arrive at V-6 and AVS begin preparing for vibracore sampling.
- 12:16 AVS begins vibracore sampling at V-6.
- 12:18 AVS has completed vibracore sampling at V-6, terminating at a depth of 20 feet below the mudline (bml). AVS Personnel begin cutting and sealing the sampling tube into 4-foot sections while Captain Brian Simmons begins mobilization to the location of V-3.
- 12:30 We arrive at V-3 and AVS begin preparing for vibracore sampling.
- 12:33 AVS begins vibracore sampling at V-3.
- 12:35 AVS has completed vibracore sampling at V-3, terminating at a depth of 20 feet below the mudline (bml). AVS Personnel begin cutting and sealing the sampling tube into 4-foot sections while Captain Brian Simmons begins mobilization to the boat dock.
- 14:45 We arrive at the boat dock and we begin offloading the vibracore samples and preparing them for transportation.
- 15:10 We have finished offloading the vibracore samples and preparing them for transportation. I begin mobilization to the GeoEngineers Offices, located in Baton Rouge, Louisiana.
- 17:40 I arrive at the GeoEngineers Offices and offload the vibracore samples.

APPENDIX B
Marsh Creation Area Soil Boring Logs

SOIL CLASSIFICATION CHART

MAJOR DIVISIONS			SYMBOLS		TYPICAL DESCRIPTIONS
			GRAPH	LETTER	
COARSE GRAINED SOILS	GRAVEL AND GRAVELLY SOILS	CLEAN GRAVELS <small>(LITTLE OR NO FINES)</small>		GW	WELL-GRADED GRAVELS, GRAVEL - SAND MIXTURES
		GRAVELS WITH FINES <small>(APPRECIABLE AMOUNT OF FINES)</small>		GP	POORLY-GRADED GRAVELS, GRAVEL - SAND MIXTURES
		GRAVELS WITH FINES <small>(APPRECIABLE AMOUNT OF FINES)</small>		GM	SILTY GRAVELS, GRAVEL - SAND - SILT MIXTURES
	SAND AND SANDY SOILS	CLEAN SANDS <small>(LITTLE OR NO FINES)</small>		SW	WELL-GRADED SANDS, GRAVELLY SANDS
		SANDS WITH FINES <small>(APPRECIABLE AMOUNT OF FINES)</small>		SP	POORLY-GRADED SANDS, GRAVELLY SAND
		SANDS WITH FINES <small>(APPRECIABLE AMOUNT OF FINES)</small>		SM	SILTY SANDS, SAND - SILT MIXTURES
FINE GRAINED SOILS	SILTS AND CLAYS	LIQUID LIMIT LESS THAN 50		ML	INORGANIC SILTS, ROCK FLOUR, CLAYEY SILTS WITH SLIGHT PLASTICITY
		LIQUID LIMIT LESS THAN 50		CL	INORGANIC CLAYS OF LOW TO MEDIUM PLASTICITY, GRAVELLY CLAYS, SANDY CLAYS, SILTY CLAYS, LEAN CLAYS
		LIQUID LIMIT LESS THAN 50		OL	ORGANIC SILTS AND ORGANIC SILTY CLAYS OF LOW PLASTICITY
	SILTS AND CLAYS	LIQUID LIMIT GREATER THAN 50		MH	INORGANIC SILTS, MICACEOUS OR DIATOMACEOUS SILTY SOILS
		LIQUID LIMIT GREATER THAN 50		CH	INORGANIC CLAYS OF HIGH PLASTICITY
		LIQUID LIMIT GREATER THAN 50		OH	ORGANIC CLAYS AND SILTS OF MEDIUM TO HIGH PLASTICITY
HIGHLY ORGANIC SOILS				PT	PEAT, HUMUS, SWAMP SOILS WITH HIGH ORGANIC CONTENTS

NOTE: Multiple symbols are used to indicate borderline or dual soil classifications

Sampler Symbol Descriptions

	2.4-inch I.D. split barrel / Dames & Moore (D&M)
	Standard Penetration Test (SPT)
	Shelby tube
	Piston
	Direct-Push
	Bulk or grab
	Continuous Coring

Blowcount is recorded for driven samplers as the number of blows required to advance sampler 12 inches (or distance noted). See exploration log for hammer weight and drop.

"P" indicates sampler pushed using the weight of the drill rig.

"WOH" indicates sampler pushed using the weight of the hammer.

NOTE: The reader must refer to the discussion in the report text and the logs of explorations for a proper understanding of subsurface conditions. Descriptions on the logs apply only at the specific exploration locations and at the time the explorations were made; they are not warranted to be representative of subsurface conditions at other locations or times.

ADDITIONAL MATERIAL SYMBOLS

SYMBOLS		TYPICAL DESCRIPTIONS
GRAPH	LETTER	
	AC	Asphalt Concrete
	CC	Cement Concrete
	CR	Crushed Rock/ Quarry Spalls
	SOD	Sod/Forest Duff
	TS	Topsoil

Groundwater Contact



Measured groundwater level in exploration, well, or piezometer



Water level observed at time of exploration

Graphic Log Contact

Distinct contact between soil strata

Approximate contact between soil strata

Material Description Contact

Contact between geologic units

Contact between soil of the same geologic unit

Laboratory / Field Tests

%F	Percent fines
%G	Percent gravel
AL	Atterberg limits
CA	Chemical analysis
CP	Laboratory compaction test
CS	Consolidation test
DD	Dry density
DS	Direct shear
HA	Hydrometer analysis
MC	Water content
MD	Water content and dry density
Mohs	Mohs hardness scale
OC	Organic content
PM	Permeability or hydraulic conductivity
PI	Plasticity index
PL	Plastic load test
PP	Pocket penetrometer
SA	Sieve analysis
TX	Triaxial compression
UC	Unconfined compression
UU	Unconsolidated undrained triaxial compression
VS	Vane shear

Sheen Classification

NS	No Visible Sheen
SS	Slight Sheen
MS	Moderate Sheen
HS	Heavy Sheen

Key to Exploration Logs



Figure B-1

Start Drilled	10/12/2022	End	10/12/2022	Total Depth (ft)	30	Logged By	NLT	Checked By	NH	Driller	Specialized Environmental Resources, LLC	Drilling Method	Wet Rotary
Surface Elevation (ft) Vertical Datum	-1.61 NAVD88			Hammer Data	Cathead Hammer 140 (lbs) / 30 (in) Drop			Drilling Equipment		Airboat Drill Rig			
Latitude Longitude	29.721574 -92.8631024			System Datum	Decimal Degrees Geographic NAD83 (ft)			Water depth approximately 2.3 ft at time of exploration.					
Notes: Cement-bentonite grout full depth.													

Elevation (feet)	Depth (feet)	FIELD DATA					Graphic Log	Group Classification	MATERIAL DESCRIPTION	LABORATORY DATA						
		Interval	Recovered (in)	Blows/foot or Pocket Pen (TSF)	Collected Sample	Sample Name				Water Content, %	Dry Density, (pcf)	Shear Strength, (KSF)	Confining Pressure, (PSI)	Strain, %	Liquid Limit (LL), %	Plasticity Index (PI), %
0	15	0.0	S-1		CH	Very soft gray clay with organic materials	95						134	97		0.27
	18	0.0	S-2			Gray clay (very soft)	99	48	0.12	0.05	9					0.08
	17	0.0	S-3			Gray clay (very soft)	104	44.6	0.08	1.47	8					0.14
	27	0.75	S-4			Gray clay with 3/2-inch sand and shell fragment layer at bottom (very soft)										
	28	0.0	S-5			Gray clay with sand and shell fragment layer (very soft)	106	49.3	0.09	2.41	20					0.12
	27	0.0	S-6			Gray clay (very soft)	119	43.4	0.11	2.89	5					0.11
	28	0.0	S-7			Gray clay (very soft)										0.07
	28	0.0	S-8			Gray clay (very soft)	101	47	0.145	3.88	12					0.19
	28	0.0	S-9			Gray clay (very soft)	100					115	90			0.20
	28	1.50	S-10		CL	Gray silty clay with ferrous nodules (medium) Estimated top of Pleistocene	32	89.8	0.62	4.89	10					
					CH											
	28	.75	S-11			Gray clay with ferrous nodules (stiff)										
	28	2	S-12			Gray and tan clay with ferrous nodules and shell fragments (stiff)										

Note: See Figure B-1 for explanation of symbols.
Coordinates Data Source: Horizontal approximated based on GPS (Survey), Vertical approximated based on (undetermined)
*Indicates a remold was used for strength testing.

Log of Boring B-1



Project: Grand Chenier Marsh Creation
Project Location: Cameron Parish, Louisiana
Project Number: 10883-026-00

Figure B-2
Sheet 1 of 1

Date: 2/22/23 Path: P:\10_10883026\GINT_1088302600.GPJ DBLibrary\Library\GEOENGINEERS_DF_STD_US_JUNE_2017\GLB\GERB_GEOTECH_LAB_NO_GW

Start Drilled	10/12/2022	End	10/12/2022	Total Depth (ft)	30	Logged By	NLT	Checked By	NH	Driller	Specialized Environmental Resources, LLC	Drilling Method	Wet Rotary
Surface Elevation (ft) Vertical Datum	-1.284 NAVD88			Hammer Data	Cathead Hammer 140 (lbs) / 30 (in) Drop			Drilling Equipment	Airboat Drill Rig				
Latitude	29.719469			System Datum	Decimal Degrees Geographic NAD83 (ft)			Water depth approximately 1.6 ft at time of exploration.					
Longitude	-92.860791			Notes: Cement-bentonite grout full depth.									

Elevation (feet)	Depth (feet)	FIELD DATA					Graphic Log	Group Classification	MATERIAL DESCRIPTION	LABORATORY DATA							
		Interval	Recovered (in)	Blows/foot or Pocket Pen (TSF)	Collected Sample	Sample Name				Water Content, %	Dry Density, (pcf)	Shear Strength, (KSF)	Confining Pressure, (PSI)	Strain, %	Liquid Limit (LL), %	Plasticity Index (PI), %	Passing No. 200 Sieve, %
0	20	0.0			S-1		CH	Gray clay with organic matter (very soft) (OC = 6.4%)	89	53.4	0.185	0.56	8				0.16
	17	0.0			S-2			Gray clay with organic matter (very soft)	118	44.4	0.145	1.2	16	117	91		0.15
5	22	0.0			S-3			Gray clay (very soft)									0.13
	28	0.0			S-4			Gray clay (very soft)	108	46.1	0.125	1.87	8				0.19
10	27	0.0			S-5			Gray clay (very soft)									0.12
	27	0.0			S-6			Gray clay (very soft)									0.21
15	27	0.0			S-7			Gray clay (very soft)	112	45.9	0.075	3.52	20				0.08
	27	0.0			S-8			Gray clay with shell fragments (very soft)	100								0.10
20	16	0.0			S-9			Gray clay (very soft)									
	28	.75			S-10		CL	Gray clay with silty sand (very soft)	58	61.3	0.135	4.98	12				
25							CH	Estimated top of Pleistocene									
	27	1.5			S-11			Gray and tan clay with ferrous nodules (stiff)									
30	28	2.5			S-12			Gray and tan clay with ferrous nodules, calcareous nodules and silt seams (very stiff)									

Note: See Figure B-1 for explanation of symbols.
Coordinates Data Source: Horizontal approximated based on GPS (Survey), Vertical approximated based on (undetermined)
*Indicates a remold was used for strength testing.

Log of Boring B-2



Project: Grand Chenier Marsh Creation
Project Location: Cameron Parish, Louisiana
Project Number: 10883-026-00

Figure B-3
Sheet 1 of 1

Date: 2/22/23 Path: P:\10_10883026\GINT_1088302600.GPJ DBLibrary\Library\GEOENGINEERS_DF_STD_US_JUNE_2017\GLB\GEB_GOTECH_LAB_NO_GW

Start Drilled	10/13/2022	End	10/13/2022	Total Depth (ft)	30	Logged By	NLT	Checked By	NH	Driller	Specialized Environmental Resources, LLC	Drilling Method	Wet Rotary
Surface Elevation (ft) Vertical Datum	-1.235 NAVD88			Hammer Data	Cathead Hammer 140 (lbs) / 30 (in) Drop			Drilling Equipment		Airboat Drill Rig			
Latitude Longitude	29.717499 -92.853332			System Datum	Decimal Degrees Geographic NAD83 (ft)			Water depth approximately 1.7 ft at time of exploration.					
Notes: Cement-bentonite grout full depth.													

Elevation (feet)	Depth (feet)	FIELD DATA				Graphic Log	Group Classification	MATERIAL DESCRIPTION	LABORATORY DATA								
		Interval	Recovered (in)	Blows/foot or Pocket Pen (TSF)	Collected Sample				Sample Name	Water Content, %	Dry Density, (pcf)	Shear Strength, (KSF)	Confining Pressure, (PSI)	Strain, %	Liquid Limit (LL), %	Plasticity Index (PI), %	Passing No. 200 Sieve, %
0	0	20	0.0		S-1		CH	Gray clay with organic matter (very soft) (OC = 13.5%)									0.21
	5	17	0.25		S-2		Gray clay (very soft)	95	50.1	0.155	0.79	10					0.11
	5	27	0.25		S-3		Gray clay (very soft)										0.11
	5	27	0.25		S-4		Gray clay (very soft)	98	51.1	0.095	1.85	20					0.14
	10	28	0.25		S-5		Gray clay (very soft)	111	46.3	0.06	2.5	20	120	87			0.14
	10	28	0.25		S-6		Gray clay (very soft)	108	46.5	0.175	2.93	20					0.17
	15	28	0.25		S-7		Gray clay (very soft)										0.16
	15	28	0.25		S-8		Gray clay (very soft)	116	46.14	0.105	2.93	20					0.14
	20	27	1.5		S-9		CH	Gray clay with silt (stiff) Estimated top of Pleistocene									0.16
	20	28	4.5		S-10		Gray silty clay with shell fragments and 3/2-inch tan and gray clay with ferrous nodules layer (very stiff)										
	25	28	4.5		S-11		Gray and tan clay with ferrous nodules, calcareous nodules and silt seams (very stiff)	24	102.2	2.72	6.28	11					
	30	28	4.5		S-12		Gray and tan clay with ferrous nodules (very stiff)										

Note: See Figure B-1 for explanation of symbols.
Coordinates Data Source: Horizontal approximated based on GPS (Survey), Vertical approximated based on (undetermined)
*Indicates a remold was used for strength testing.

Log of Boring B-3



Project: Grand Chenier Marsh Creation
Project Location: Cameron Parish, Louisiana
Project Number: 10883-026-00

Figure B-4
Sheet 1 of 1

Date: 2/22/23 Path: P:\10_10883026\GINT_1088302600.GPJ DBLibrary\Library\GEOENGINEERS_DF_STD_US_JUNE_2017\GLB\GERB_GTECH_LAB_NO_GW

Start Drilled	10/13/2022	End	10/13/2022	Total Depth (ft)	30	Logged By	NLT	Checked By	NH	Driller	Specialized Environmental Resources, LLC	Drilling Method	Wet Rotary
Surface Elevation (ft) Vertical Datum	-1.553 NAVD88			Hammer Data	Cathead Hammer 140 (lbs) / 30 (in) Drop			Drilling Equipment		Airboat Drill Rig			
Latitude	29.711318			System Datum	Decimal Degrees Geographic NAD83 (ft)			Water depth approximately 1.8 ft at time of exploration.					
Longitude	-92.854395			Notes: Cement-bentonite grout full depth.									

Elevation (feet)	Depth (feet)	FIELD DATA					Graphic Log	Group Classification	MATERIAL DESCRIPTION	LABORATORY DATA						
		Interval	Recovered (in)	Blows/foot or Pocket Pen (TSF)	Collected Sample	Sample Name				Water Content, %	Dry Density, (pcf)	Shear Strength, (KSF)	Confining Pressure, (PSI)	Strain, %	Liquid Limit (LL), %	Plasticity Index (PI), %
0	20	0.25		S-1		CH	Gray clay with organic matter (very soft) (OC = 7.9%)	97	47.2	0.085	0.32	20				0.07
	17	0.0		S-2			Gray clay with organic matter (very soft)	107.6	40.3	0.03	5	8				0.08
	27	0.0		S-3			Gray clay (very soft)									0.09
	27	0.25		S-4			Gray clay (very soft)	116	44.8	0.095	1.71	11				0.09
	27	0.0		S-5			Gray clay (very soft)	123.2	40.7	0.065	2.4	20				0.06
	16	0.25		S-6			Gray clay (very soft)									0.15
	28	0.25		S-7			Gray clay (very soft)	117	43.5	0.095	3.39	9				0.9
	27	0.25		S-8			Gray clay with sand pockets (very soft)	108.6					84	80		0.17
	20	0.5		S-9			Gray clay with shells (very soft)	95	47.9	0.15	4.41	10				0.18
	27	4.5		S-10		CH	Gray clay with 1-inch shell layer (soft)/3-inch layer gray and tan clay (hard) Estimated top of Pleistocene									
						CL										
	27	4.5		S-11			Gray and tan clay with silt and ferrous nodules (very stiff)	20	108.1	2.305	6.32	20				
	28	4.5		S-12			Gray and tan clay with silt and ferrous nodules (hard)									

Note: See Figure B-1 for explanation of symbols.
Coordinates Data Source: Horizontal approximated based on GPS (Survey), Vertical approximated based on (undetermined)
*Indicates a remold was used for strength testing.

Log of Boring B-4



Project: Grand Chenier Marsh Creation
Project Location: Cameron Parish, Louisiana
Project Number: 10883-026-00

Date: 2/22/23 Path: P:\10_10883026\GINT_1088302600.GPJ DBLibrary\Library\GEOENGINEERS_DF_STD_US_JUNE_2017\GLB\GER_GEO TECH_LAB_NO_GW

Start Drilled	10/12/2022	End	10/12/2022	Total Depth (ft)	30	Logged By	NLT	Checked By	NH	Driller	Specialized Environmental Resources, LLC	Drilling Method	Wet Rotary
Surface Elevation (ft) Vertical Datum	-1.463 NAVD88			Hammer Data	Cathead Hammer 140 (lbs) / 30 (in) Drop			Drilling Equipment		Airboat Drill Rig			
Latitude	29.711723			System Datum	Decimal Degrees Geographic NAD83 (ft)			Water depth approximately 1.8 ft at time of exploration.					
Longitude	-92.862289			Notes: Cement-bentonite grout full depth.									

Elevation (feet)	Depth (feet)	FIELD DATA					Graphic Log	Group Classification	MATERIAL DESCRIPTION	LABORATORY DATA							
		Interval	Recovered (in)	Blows/foot or Pocket Pen (TSF)	Collected Sample	Sample Name				Water Content, %	Dry Density, (pcf)	Shear Strength, (KSF)	Confining Pressure, (PSI)	Strain, %	Liquid Limit (LL), %	Plasticity Index (PI), %	Passing No. 200 Sieve, %
0	14	0.0		S-1		CH	Gray and brown clay with organic matter (peat) (very soft)	140	34.8	0.165	0.36	16					
	15	0.0		S-2			Gray and brown clay with organic matter (very soft) (OC = 11.8%)										
5	17	0.0		S-3			Gray clay (very soft)	96	44.1	0.095	1.41	14	124	88			
	28	0.0		S-4			Gray clay (very soft)										
10	28	0.0		S-5			Gray clay with silt lenses (very soft)	114									
	28	0.0		S-6			Gray clay with silt lenses (very soft)										
15	28	0.0		S-7			Gray clay (very soft)	108	39	0.13	3.48	20					
	27	0.25		S-8			Gray clay (very soft)										
	27	0.25		S-9			Gray clay (very soft)	100	43	0.215	4.47	6					
20	15	0.25		S-10			Gray clay with 2-inch shell layer and 2-inch gray and tan clay layer (soft)										
						CH	Estimated top of Pleistocene										
25	28	2.0		S-11			Gray and tan clay with silt and ferrous nodules (very stiff)	22	107.9	2.595	6.29	12					
30	14	2.5		S-12			Gray and tan clay with ferrous nodules (very stiff)										

Note: See Figure B-1 for explanation of symbols.
Coordinates Data Source: Horizontal approximated based on GPS (Survey), Vertical approximated based on (undetermined)
*Indicates a remold was used for strength testing.

Log of Boring B-5



Project: Grand Chenier Marsh Creation
Project Location: Cameron Parish, Louisiana
Project Number: 10883-026-00

Figure B-6
Sheet 1 of 1

Date: 2/22/23 Path: P:\10_10883026\GINT_1088302600.GPJ DBLibrary\Library\GEOENGINEERS_DF_STD_US_JUNE_2017\GLB\GER_GEOTECH_LAB_NO_GW

Start Drilled	10/13/2022	End	10/13/2022	Total Depth (ft)	30	Logged By	NLT	Checked By	NH	Driller	Specialized Environmental Resources, LLC	Drilling Method	Wet Rotary
Surface Elevation (ft) Vertical Datum	-1.3 NAVD88			Hammer Data	Cathead Hammer 140 (lbs) / 30 (in) Drop			Drilling Equipment	Airboat Drill Rig				
Latitude	29.715319			System Datum	Decimal Degrees Geographic NAD83 (ft)			Water depth approximately 1.8 ft at time of exploration.					
Longitude	-92.858571			Notes: Cement-bentonite grout full depth.									

Elevation (feet)	Depth (feet)	FIELD DATA					Graphic Log	Group Classification	MATERIAL DESCRIPTION	LABORATORY DATA							
		Interval	Recovered (in)	Blows/foot or Pocket Pen (TSF)	Collected Sample	Sample Name				Water Content, %	Dry Density, (pcf)	Shear Strength, (KSF)	Confining Pressure, (PSI)	Strain, %	Liquid Limit (LL), %	Plasticity Index (PI), %	Passing No. 200 Sieve, %
0	28	0.0			S-1	[Hatched Pattern]	CH	Gray clay with roots (very soft)	108	45	0.1	0.38	20				
5	20	0.0			S-2		Gray clay with roots (very soft)										
5	22	0.0			S-3		Gray clay with organic matter (very soft) (OC = 10.4%)	114	42.2	0.075	1.34	20					
10	21	0.0			S-4		Gray clay (very soft)	110.4				134	98				
10	27	0.25			S-5		Gray clay (very soft)										
15	28	0.25			S-6		Gray clay (very soft)	119	42	0.055	2.88	20					
15	28	0.25			S-7		Gray clay (very soft)	117	40.9	0.095	3.43	20					
15	27	0.25			S-8		Gray clay (very soft)										
20	27	0.25			S-9		Gray clay (very soft)	90	65.5	0.12	4.38	20	128	86			
20	28	2.5			S-10		CH	Gray silty sandy clay with shell fragments and silty clay layer (medium) (silt lenses) Estimated top of Pleistocene	35	90	0.65	4.99	20				
25	28	3.0			S-11		Gray clay with ferrous nodules (very stiff)										
30	28	3.75			S-12		Gray and tan clay with silt and ferrous nodules (very stiff)										

Note: See Figure B-1 for explanation of symbols.
Coordinates Data Source: Horizontal approximated based on GPS (Survey), Vertical approximated based on (undetermined)
*Indicates a remold was used for strength testing.

Log of Boring B-6



Project: Grand Chenier Marsh Creation
Project Location: Cameron Parish, Louisiana
Project Number: 10883-026-00

Date: 2/22/23 Path: P:\10_10883026\GINT_1088302600.GPJ DBLibrary\Library\GEOENGINEERS_DF_STD_US_JUNE_2017.GLB\GEBB_GTECH_LAB_NO_GW

APPENDIX C
Marsh Creation Area CPT Logs

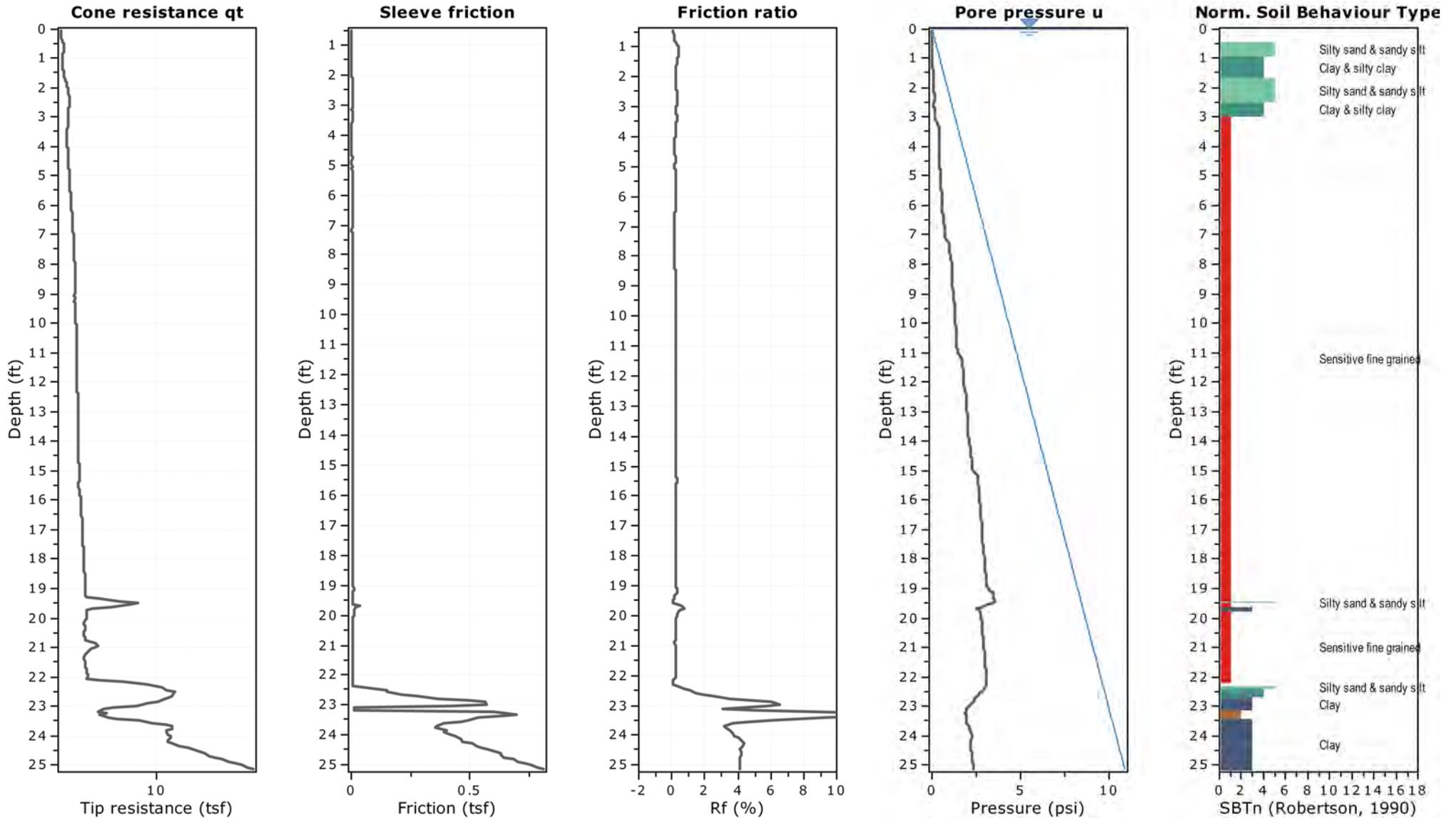
Project: South Grand Chenier - Baker Marsh Creation (ME-32)

Location: Cameron parish, Louisiana

Total depth: 25.13 ft, Date: 12/6/2022

Surface Elevation: -1.27 ft

Coords: 29°43'7.985" N 92°51'54.932" E



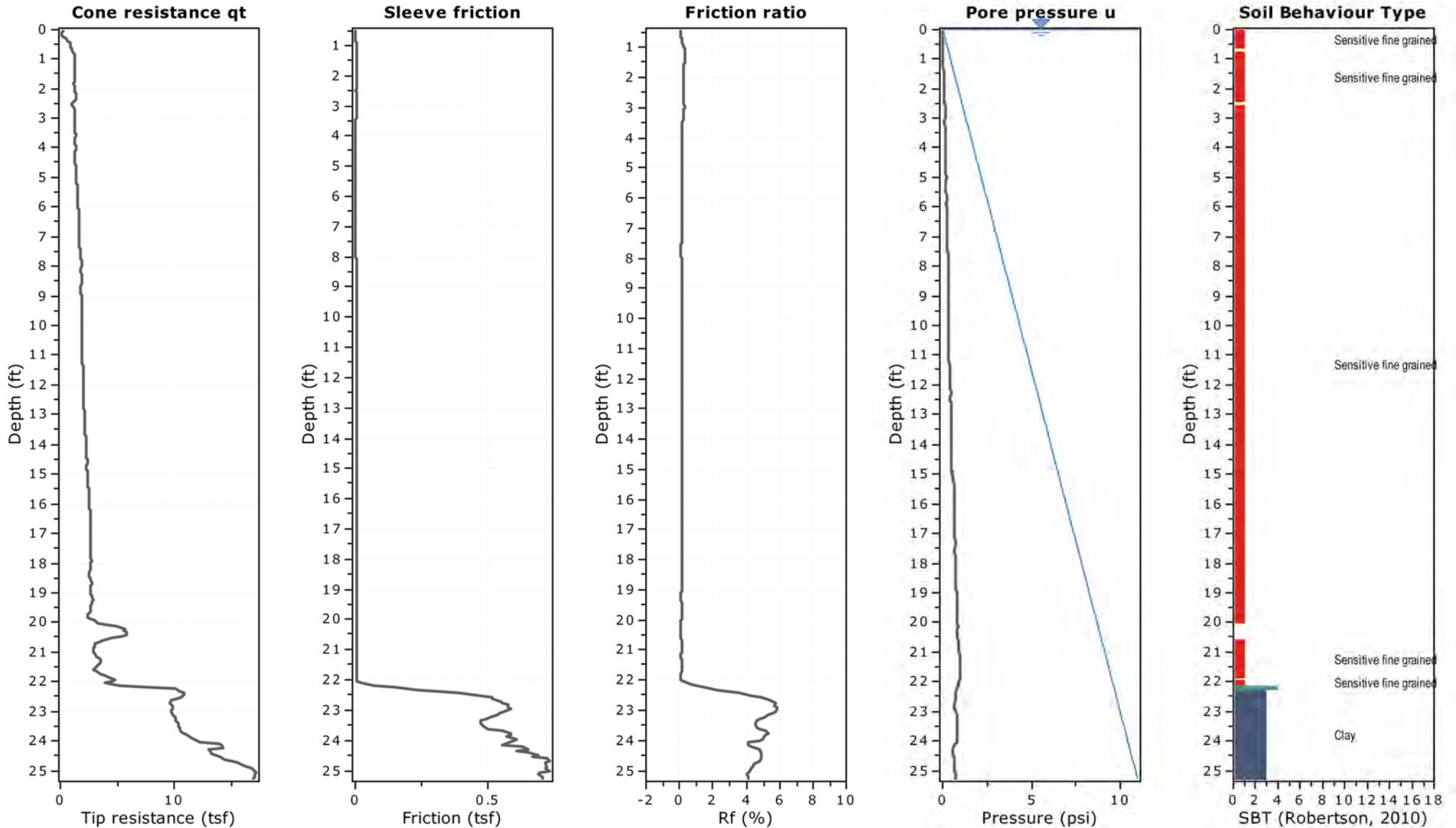
Project: South Grand Chenier - Baker Marsh Creation (ME-32)

Location: Cameron parish, Louisiana

Total depth: 25.26 ft, Date: 12/6/2022

Surface Elevation: -2.60 ft

Coords: 29°43'10.084" N 92°51'38.845" E



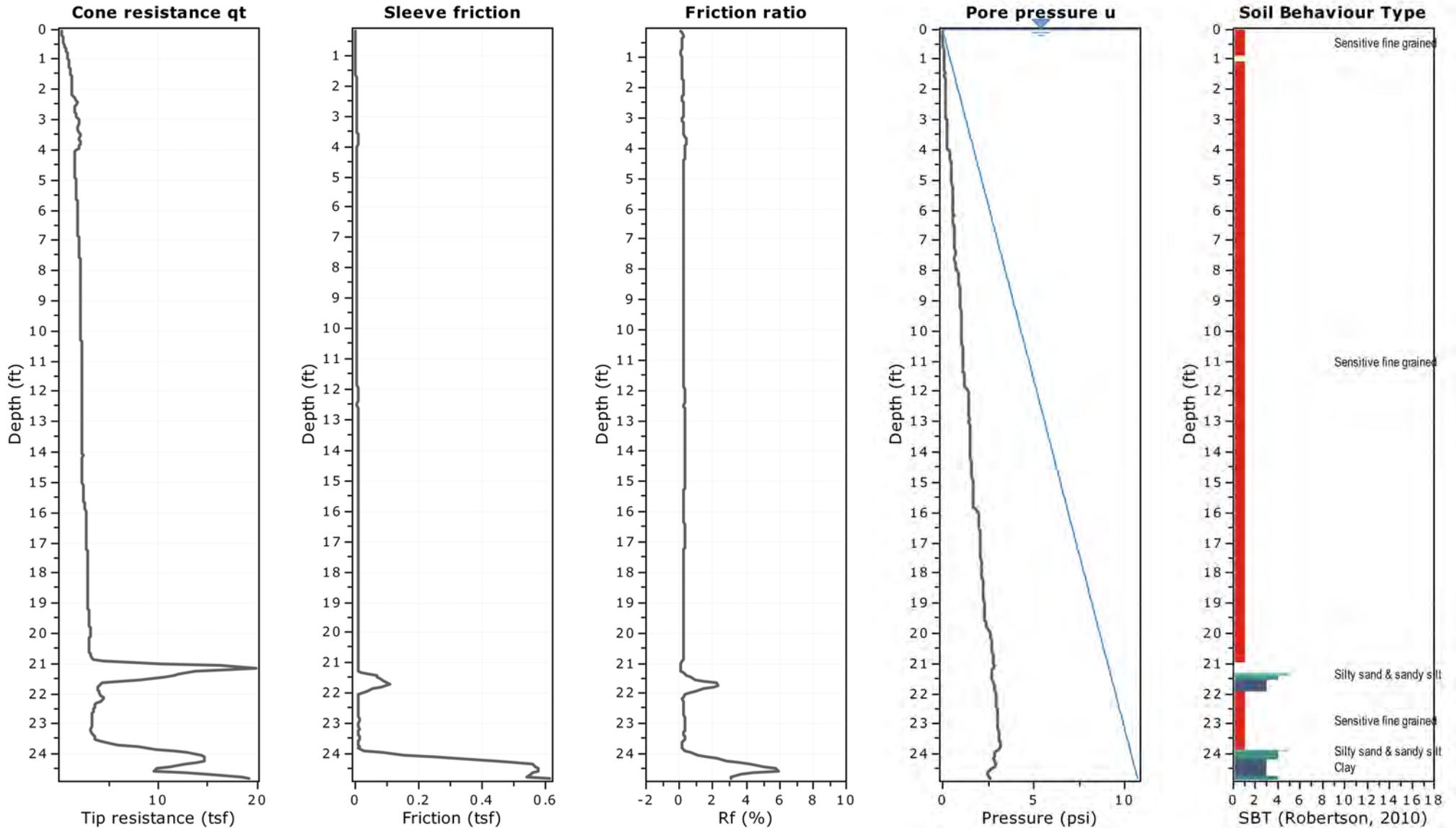
Project: South Grand Chenier - Baker Marsh Creation (ME-32)

Location: Cameron parish, Louisiana

Total depth: 24.80 ft, Date: 12/6/2022

Surface Elevation: -1.52 ft

Coords: 29°42'56.122" N 92°51'55.281" E





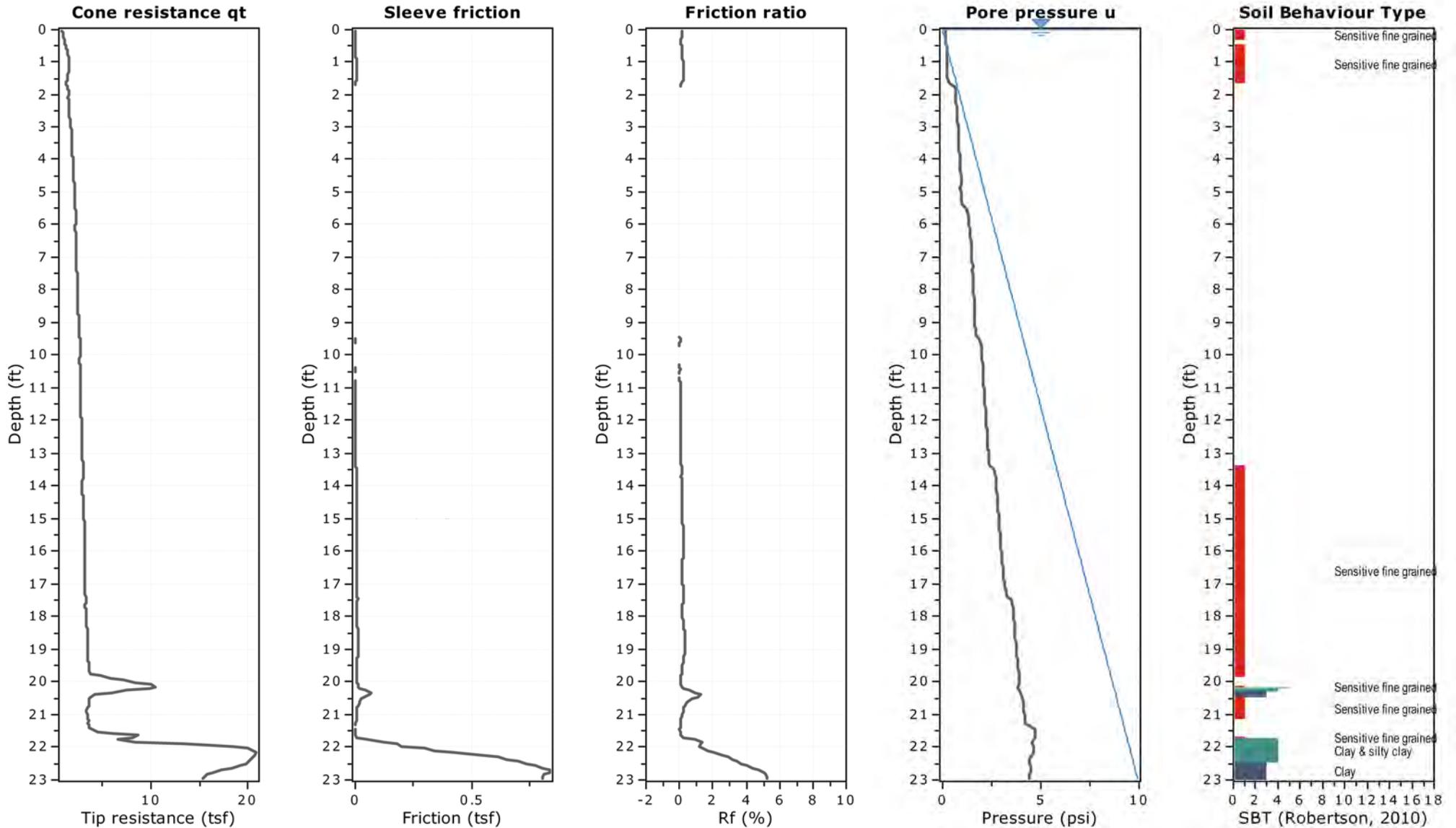
Project: South Grand Chenier - Baker Marsh Creation (ME-32)

Location: Cameron parish, Louisiana

Total depth: 22.97 ft, Date: 12/6/2022

Surface Elevation: -1.02 ft

Coords: 29°42'43.79" N 92°51'54.99" E



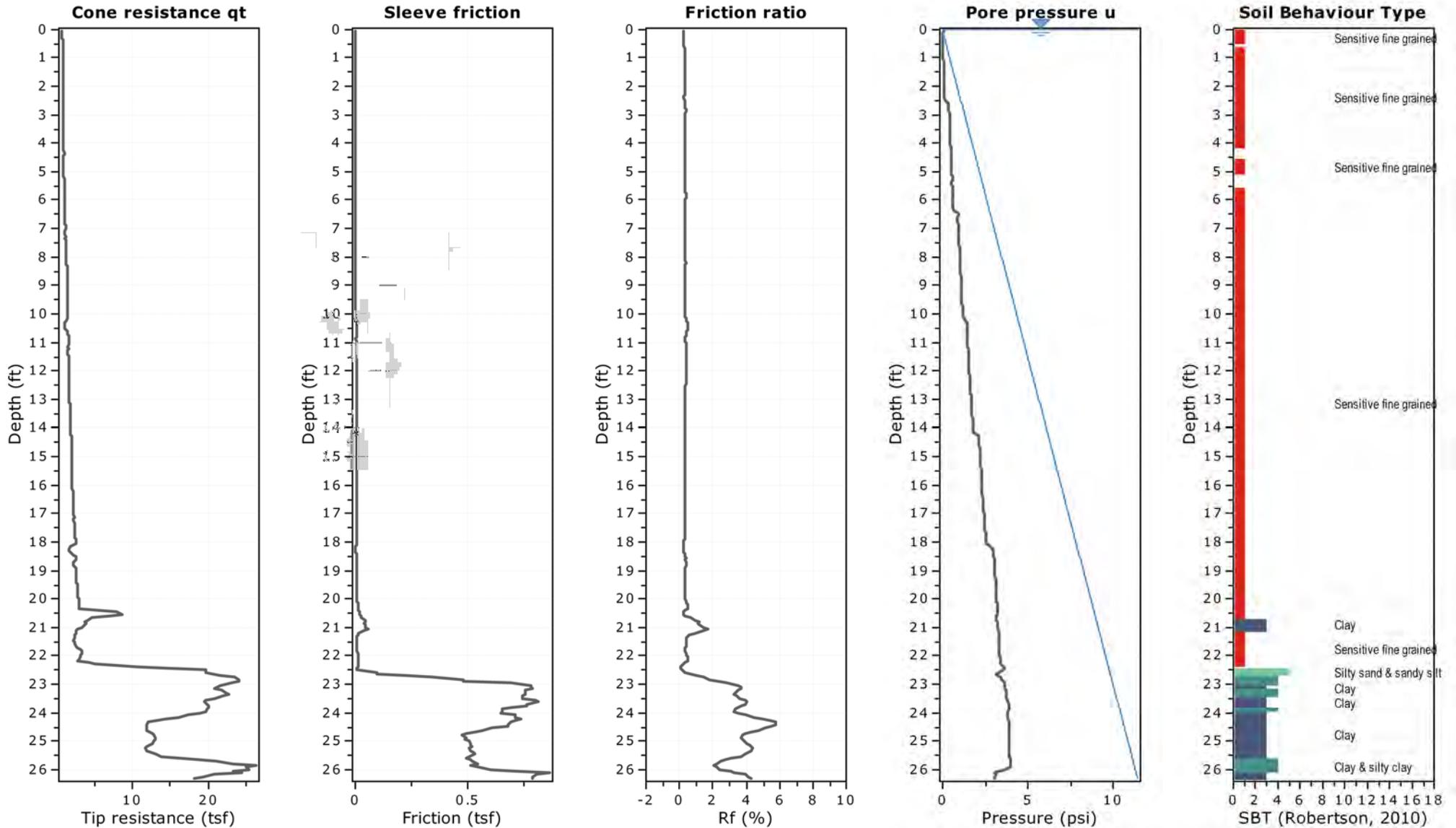
Project: South Grand Chenier - Baker Marsh Creation (ME-32)

Location: Cameron parish, Louisiana

Total depth: 26.31 ft, Date: 12/6/2022

Surface Elevation: -3.43 ft

Coords: 29°42'42.32" N 92°51'44.18" E



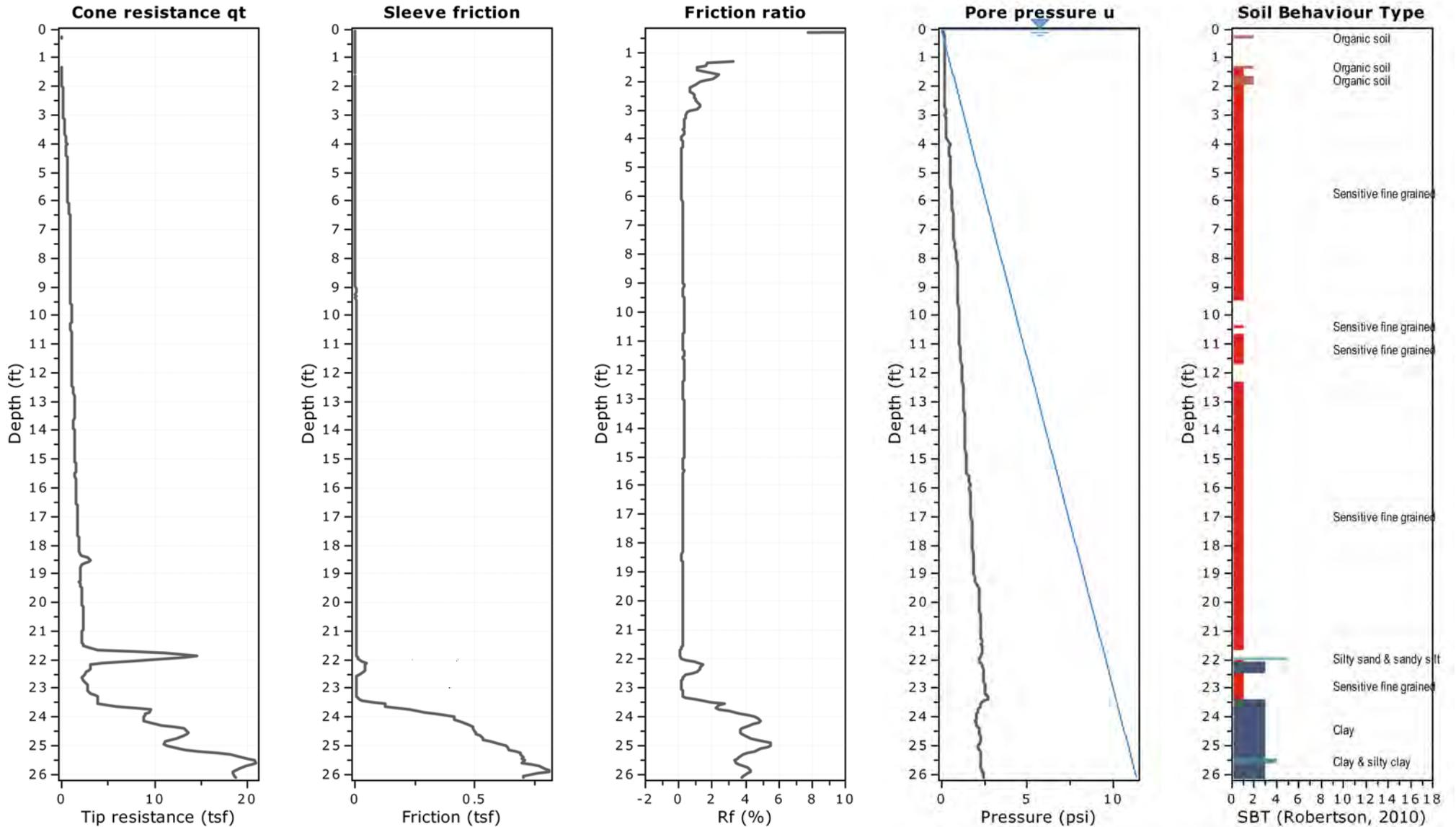
Project: South Grand Chenier - Baker Marsh Creation (ME-32)

Location: Cameron parish, Louisiana

Total depth: 26.12 ft, Date: 12/6/2022

Surface Elevation: -1.60 ft

Coords: 29°42'62.74" N 92°51'28.31" E



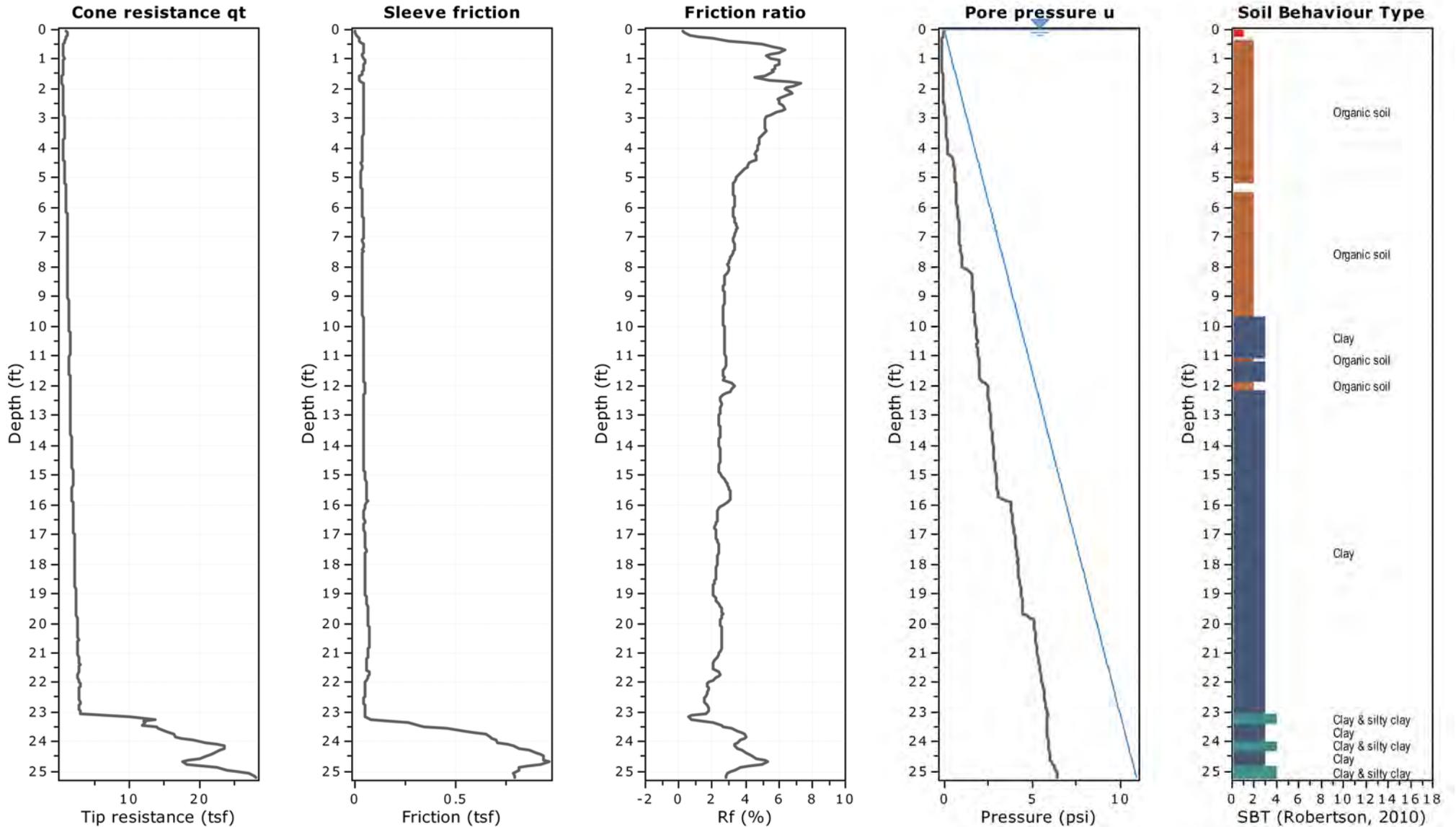
Project: South Grand Chenier - Baker Marsh Creation (ME-32)

Location: Cameron parish, Louisiana

Total depth: 25.20 ft, Date: 12/6/2022

Surface Elevation: -1.10 ft

Coords: 29°42'34.785" N 92°51'14.61" E





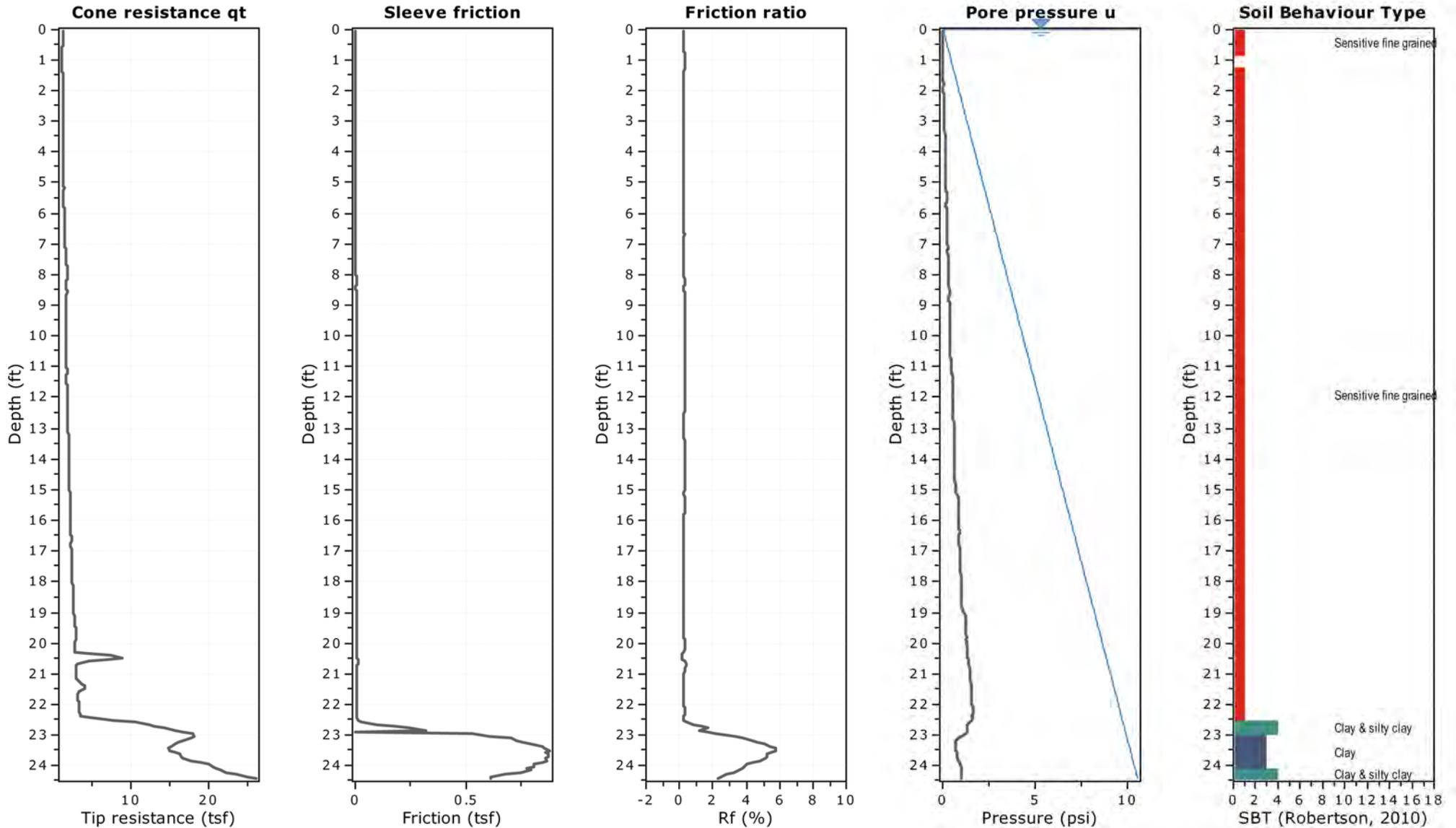
Project: South Grand Chenier - Baker Marsh Creation (ME-32)

Location: Cameron parish, Louisiana

Total depth: 24.41 ft, Date: 12/6/2022

Surface Elevation: -1.10 ft

Coords: 29°42'42.71" N 92°51'2.91" E



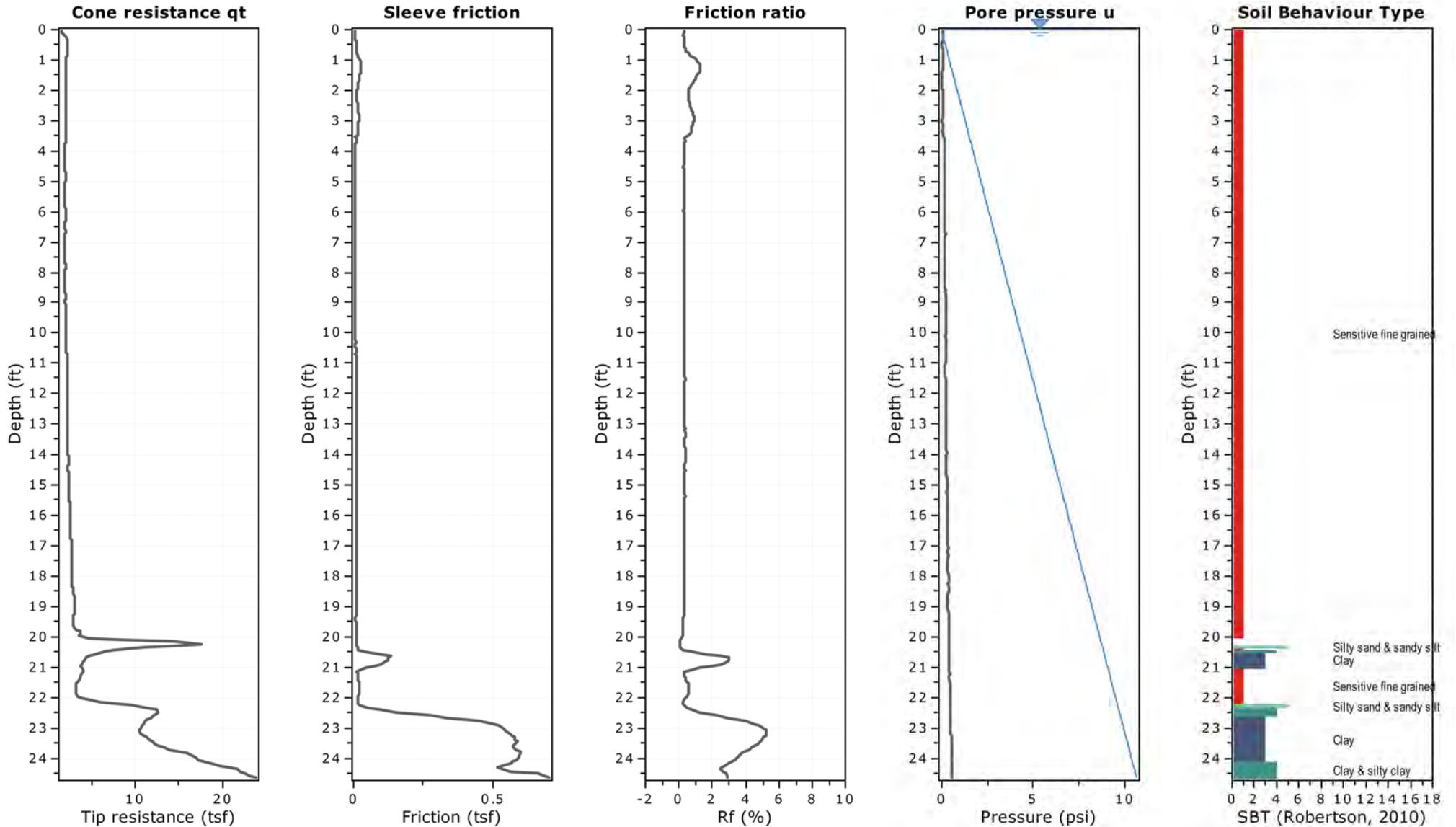
Project: South Grand Chenier - Baker Marsh Creation (ME-32)

Location: Cameron parish, Louisiana

Total depth: 24.61 ft, Date: 12/6/2022

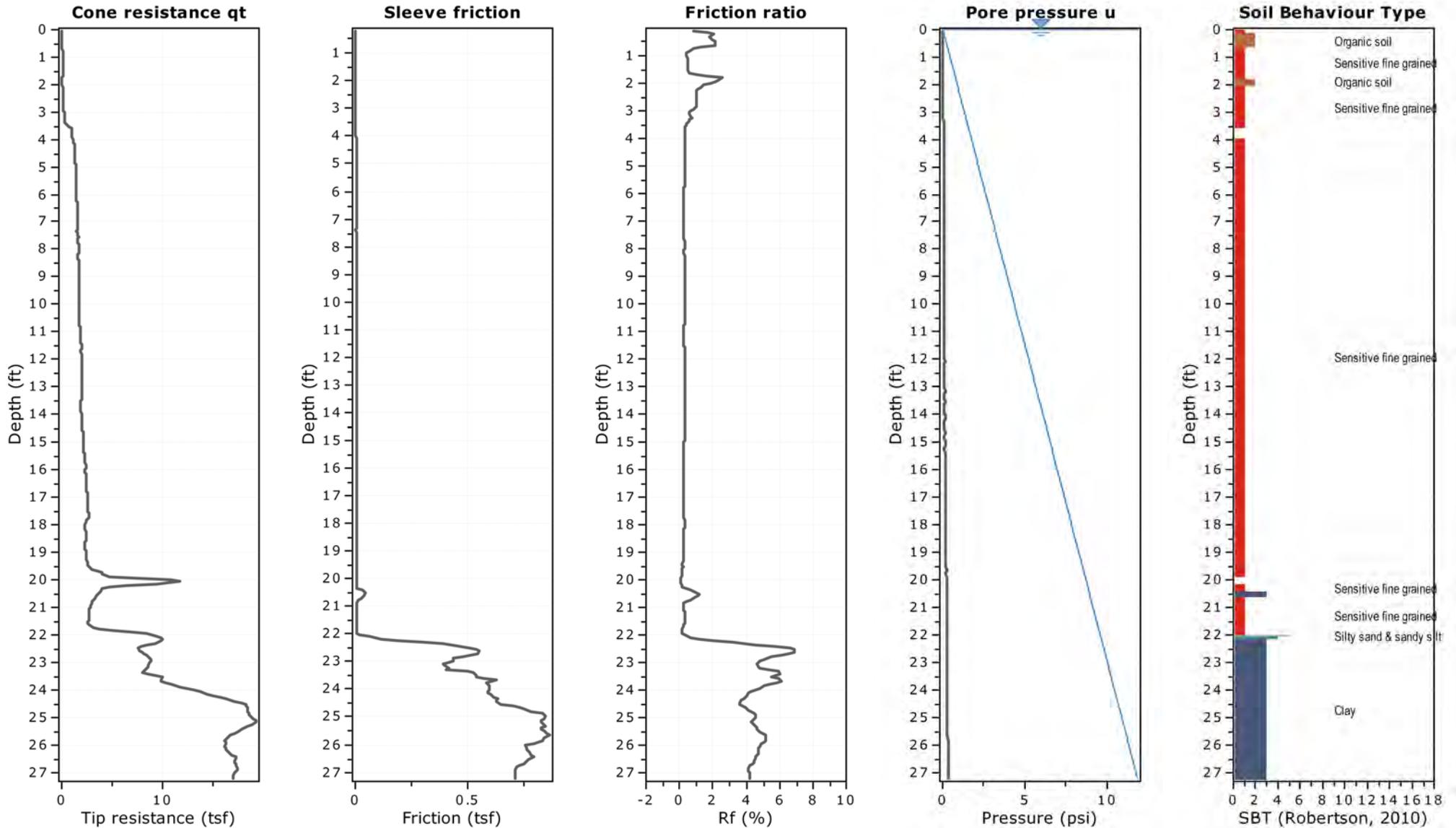
Surface Elevation: -1.35 ft

Coords: 29°42'58.24" N 92°50'55.35" E



Project: South Grand Chenier - Baker Marsh Creation (ME-32)
 Location: Cameron parish, Louisiana

Total depth: 27.23 ft, Date: 12/6/2022
 Surface Elevation: -2.35 ft
 Coords: 29°43'9.64" N 92°51'20.68" E



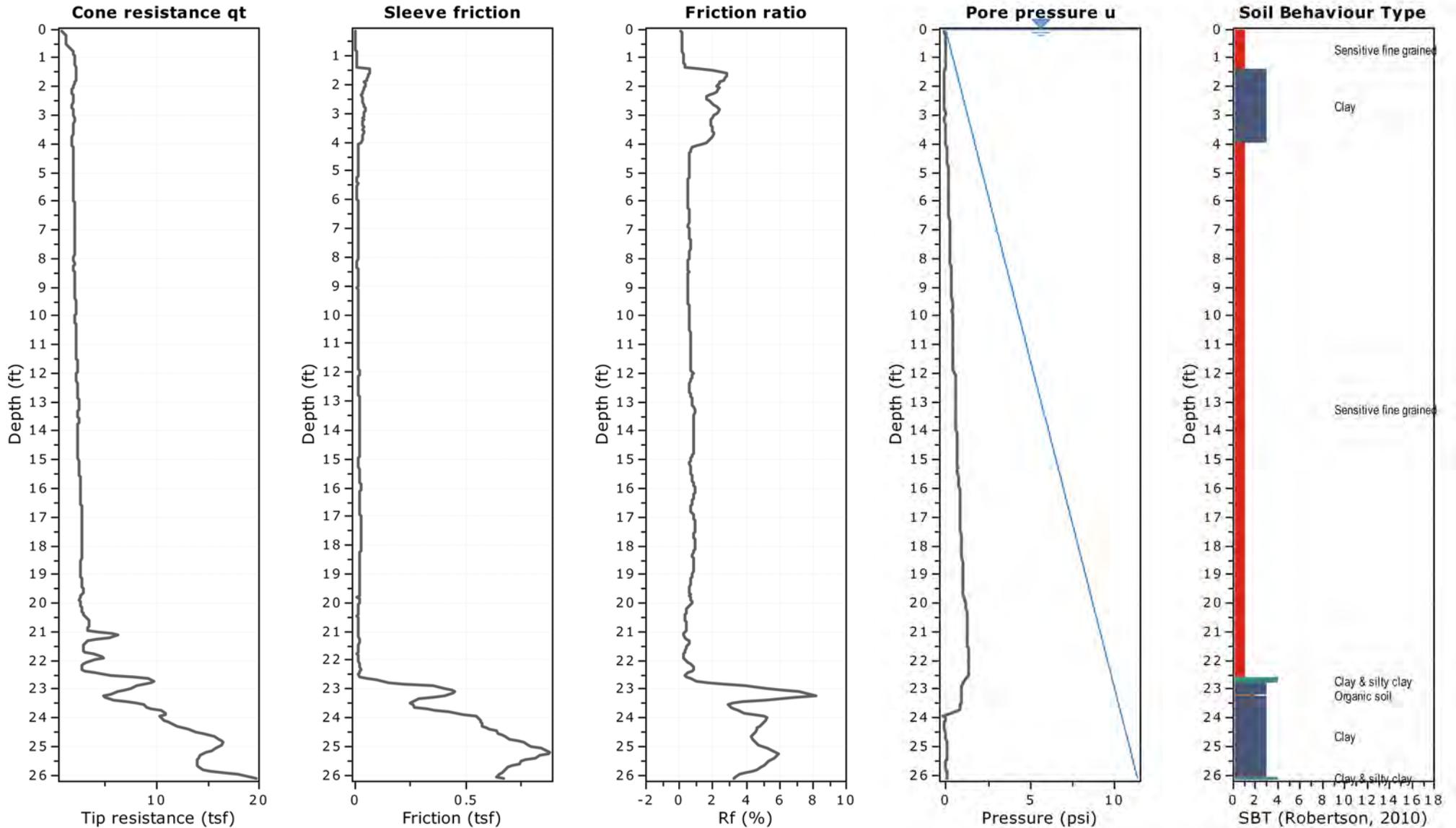
Project: South Grand Chenier - Baker Marsh Creation (ME-32)

Location: Cameron parish, Louisiana

Total depth: 26.12 ft, Date: 12/6/2022

Surface Elevation: -1.27 ft

Coords: 29°43'9.64" N 92°51'20.68" E





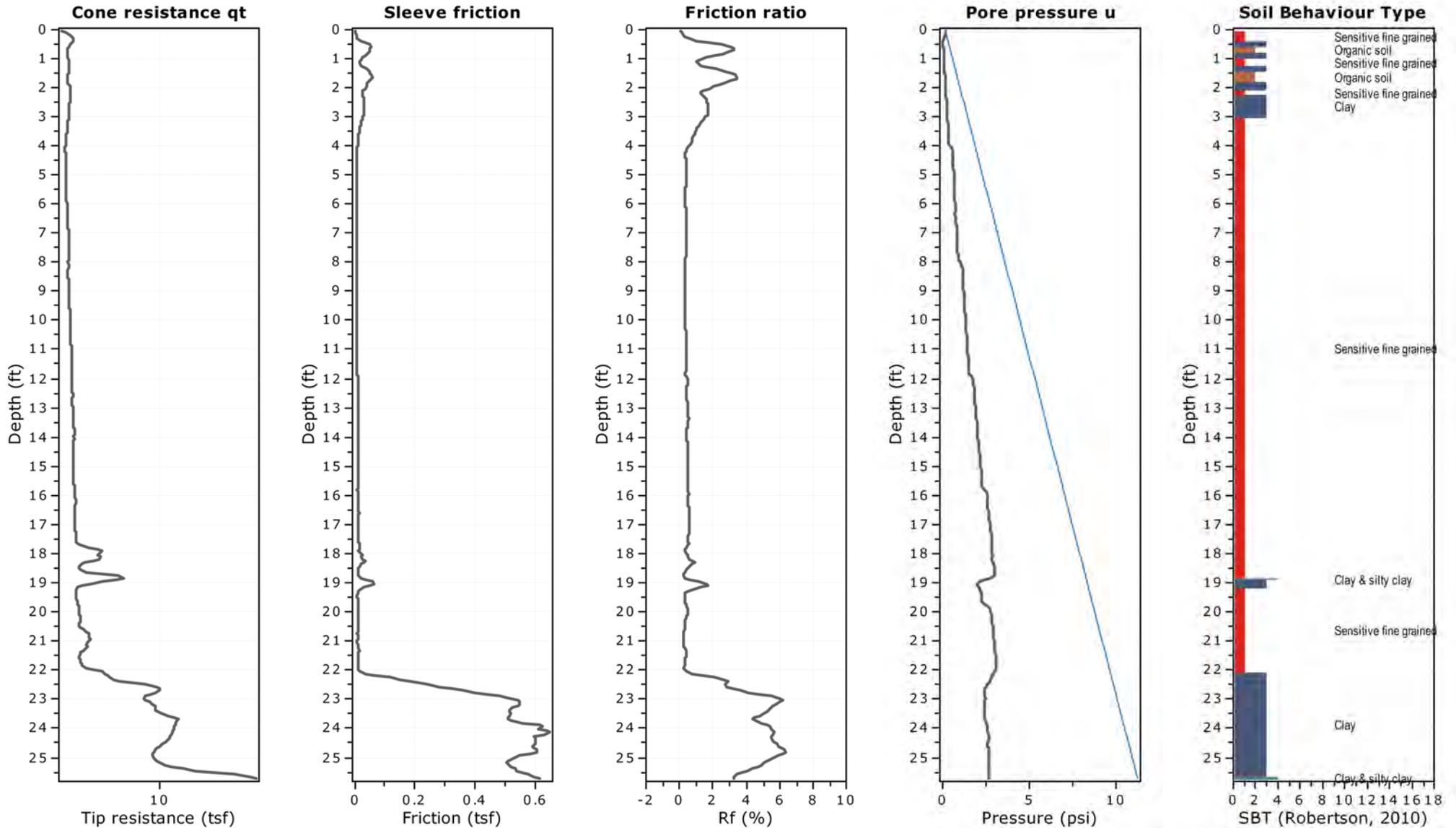
Project: South Grand Chenier - Baker Marsh Creation (ME-32)

Location: Cameron parish, Louisiana

Total depth: 25.72 ft, Date: 12/6/2022

Surface Elevation: -1.93 ft

Coords: 29°43'26.38" N 92°51'40.48" E



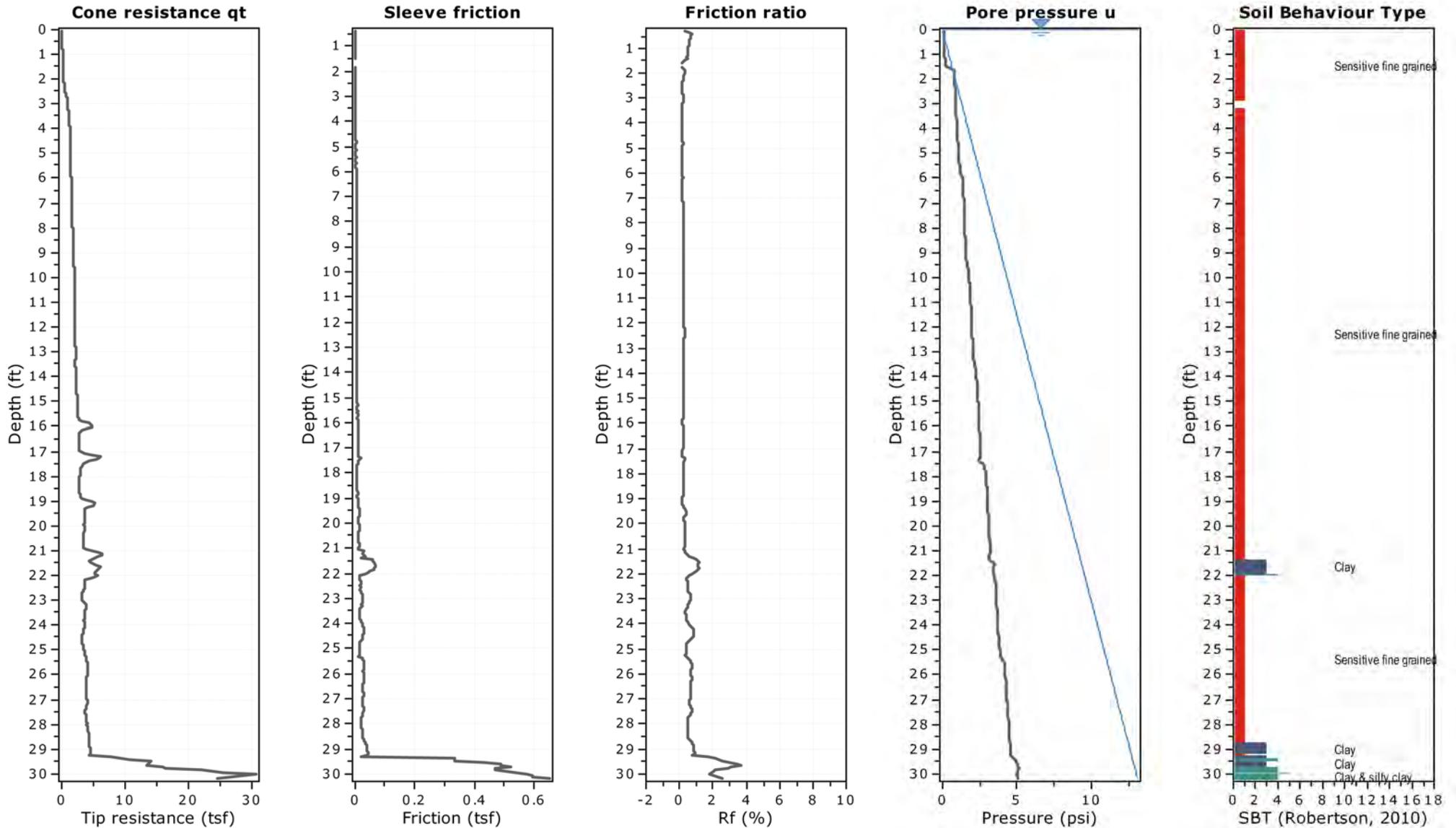
Project: South Grand Chenier - Baker Marsh Creation (ME-32)

Location: Cameron parish, Louisiana

Total depth: 30.18 ft, Date: 12/6/2022

Surface Elevation: -1.60 ft

Coords: 29°43'25.37" N 92°51'54.67" E



APPENDIX D
Borrow Area Vibracore Logs

SOIL CLASSIFICATION CHART

MAJOR DIVISIONS			SYMBOLS		TYPICAL DESCRIPTIONS
			GRAPH	LETTER	
COARSE GRAINED SOILS	GRAVEL AND GRAVELLY SOILS	CLEAN GRAVELS <small>(LITTLE OR NO FINES)</small>		GW	WELL-GRADED GRAVELS, GRAVEL - SAND MIXTURES
		GRAVELS WITH FINES <small>(APPRECIABLE AMOUNT OF FINES)</small>		GP	POORLY-GRADED GRAVELS, GRAVEL - SAND MIXTURES
		GRAVELS WITH FINES <small>(APPRECIABLE AMOUNT OF FINES)</small>		GM	SILTY GRAVELS, GRAVEL - SAND - SILT MIXTURES
	SAND AND SANDY SOILS	CLEAN SANDS <small>(LITTLE OR NO FINES)</small>		SW	WELL-GRADED SANDS, GRAVELLY SANDS
		SANDS WITH FINES <small>(APPRECIABLE AMOUNT OF FINES)</small>		SP	POORLY-GRADED SANDS, GRAVELLY SAND
		SANDS WITH FINES <small>(APPRECIABLE AMOUNT OF FINES)</small>		SM	SILTY SANDS, SAND - SILT MIXTURES
FINE GRAINED SOILS	SILTS AND CLAYS	LIQUID LIMIT LESS THAN 50		ML	INORGANIC SILTS, ROCK FLOUR, CLAYEY SILTS WITH SLIGHT PLASTICITY
		LIQUID LIMIT LESS THAN 50		CL	INORGANIC CLAYS OF LOW TO MEDIUM PLASTICITY, GRAVELLY CLAYS, SANDY CLAYS, SILTY CLAYS, LEAN CLAYS
		LIQUID LIMIT LESS THAN 50		OL	ORGANIC SILTS AND ORGANIC SILTY CLAYS OF LOW PLASTICITY
	SILTS AND CLAYS	LIQUID LIMIT GREATER THAN 50		MH	INORGANIC SILTS, MICACEOUS OR DIATOMACEOUS SILTY SOILS
		LIQUID LIMIT GREATER THAN 50		CH	INORGANIC CLAYS OF HIGH PLASTICITY
		LIQUID LIMIT GREATER THAN 50		OH	ORGANIC CLAYS AND SILTS OF MEDIUM TO HIGH PLASTICITY
HIGHLY ORGANIC SOILS				PT	PEAT, HUMUS, SWAMP SOILS WITH HIGH ORGANIC CONTENTS

NOTE: Multiple symbols are used to indicate borderline or dual soil classifications

Sampler Symbol Descriptions

	2.4-inch I.D. split barrel / Dames & Moore (D&M)
	Standard Penetration Test (SPT)
	Shelby tube
	Piston
	Direct-Push
	Bulk or grab
	Continuous Coring

Blowcount is recorded for driven samplers as the number of blows required to advance sampler 12 inches (or distance noted). See exploration log for hammer weight and drop.

"P" indicates sampler pushed using the weight of the drill rig.

"WOH" indicates sampler pushed using the weight of the hammer.

NOTE: The reader must refer to the discussion in the report text and the logs of explorations for a proper understanding of subsurface conditions. Descriptions on the logs apply only at the specific exploration locations and at the time the explorations were made; they are not warranted to be representative of subsurface conditions at other locations or times.

ADDITIONAL MATERIAL SYMBOLS

SYMBOLS		TYPICAL DESCRIPTIONS
GRAPH	LETTER	
	AC	Asphalt Concrete
	CC	Cement Concrete
	CR	Crushed Rock/ Quarry Spalls
	SOD	Sod/Forest Duff
	TS	Topsoil

Groundwater Contact



Measured groundwater level in exploration, well, or piezometer



Water level observed at time of exploration

Graphic Log Contact

Distinct contact between soil strata

Approximate contact between soil strata

Material Description Contact

Contact between geologic units

Contact between soil of the same geologic unit

Laboratory / Field Tests

%F	Percent fines
%G	Percent gravel
AL	Atterberg limits
CA	Chemical analysis
CP	Laboratory compaction test
CS	Consolidation test
DD	Dry density
DS	Direct shear
HA	Hydrometer analysis
MC	Water content
MD	Water content and dry density
Mohs	Mohs hardness scale
OC	Organic content
PM	Permeability or hydraulic conductivity
PI	Plasticity index
PL	Plastic load test
PP	Pocket penetrometer
SA	Sieve analysis
TX	Triaxial compression
UC	Unconfined compression
UU	Unconsolidated undrained triaxial compression
VS	Vane shear

Sheen Classification

NS	No Visible Sheen
SS	Slight Sheen
MS	Moderate Sheen
HS	Heavy Sheen

Key to Exploration Logs



Figure D-1

Start Drilled	10/17/2022	End	10/17/2022	Total Depth (ft)	17	Logged By	NLT	Checked By	NH	Driller	AM Drilling	Drilling Method	Vibracore
Surface Elevation (ft) Vertical Datum	Undetermined NAVD88			Hammer Data	Cathead Hammer 140 (lbs) / 30 (in) Drop			Drilling Equipment Vibracore					
Latitude	29.64367			System Datum	Decimal Degrees Geographic NAD83 (ft)			Water depth approximately 23 ft at time of exploration					
Longitude	-92.873323												
Notes:													

Elevation (feet)	Depth (feet)	FIELD DATA					Graphic Log	Group Classification	MATERIAL DESCRIPTION	LABORATORY DATA									
		Interval	Recovered (in)	Blows/foot or Pocket Pen (TSF)	Collected Sample	Sample Name				Water Content, %	Dry Density, (pcf)	Shear Strength, (KSF)	Confining Pressure, (PSI)	Strain, %	Liquid Limit (LL), %	Plasticity Index (PI), %	Passing No. 200 Sieve, %	Tonvane Shear Strength (KSF)	
	0	11				S-1		CH	Gray clay (very soft)	106.3					108	81	99.7	0.12	
	20					S-2		CH	Gray clay (very soft)	88.8									0.17
	21					S-3		CH	Gray clay (very soft)	86.8									0.19
5	26					S-4		CH	Gray clay (very soft)	91.6					99	70			0.23
	26					S-5		CH	Gray clay (very soft)	82.2									0.23
	10	24				S-6	CH	Estimated top of Pleistocene											
		25				S-7	CH	Gray clay at top 7.5 inches, with 1-inch shell layer, gray and tan clay with ferrous nodules and shells at bottom (medium to stiff)	32.3										
		25				S-8	CH	Gray and tan clay with shells and ferrous nodules, tan and gray clay with ferrous nodules at bottom 9 inches (medium to stiff)	24.2										
	15	25				S-8	CH	Gray and tan clay with ferrous nodules and calcareous nodules (medium to stiff)	36.4										
		12				S-9	CH	Tan and gray clay with calcareous nodules and ferrous nodules (medium to stiff)	26.6										

Note: See Figure B-1 for explanation of symbols.
Coordinates Data Source: Horizontal approximated based on GPS (Survey), Vertical approximated based on (undetermined)
*Indicates a remold was used for strength testing.

Log of Boring V-1



Project: Grand Chenier Marsh Creation
Project Location: Cameron Parish, Louisiana
Project Number: 10883-026-00

Figure D-2
Sheet 1 of 1

Date: 2/1/23 Path: \\10.10883026\GINT\10883026\GINT\10883026\GIB\GIB_2017\GIB\GIB_GEO TECH_LAB_NO_GW

Start Drilled	10/17/2022	End	10/17/2022	Total Depth (ft)	16.5	Logged By	NLT	Checked By	NH	Driller	AM Drilling	Drilling Method	Vibracore
Surface Elevation (ft) Vertical Datum	Undetermined NAVD88			Hammer Data	Cathead Hammer 140 (lbs) / 30 (in) Drop			Drilling Equipment Vibracore					
Latitude	29.6445			System Datum	Decimal Degrees Geographic NAD83 (ft)			Water depth approximately 23 ft at time of exploration					
Longitude	-92.869142												
Notes:													

Elevation (feet)	Depth (feet)	FIELD DATA					Graphic Log	Group Classification	MATERIAL DESCRIPTION	LABORATORY DATA								
		Interval Recovered (in)	Blows/foot or Pocket Pen (TSF)	Collected Sample	Sample Name	Water Content, %				Dry Density, (pcf)	Shear Strength, (KSF)	Confining Pressure, (PSI)	Strain, %	Liquid Limit (LL), %	Plasticity Index (PI), %	Passing No. 200 Sieve, %	Tonvane Shear Strength (KSF)	
	0	20			S-1		CH	Gray clay (very soft)	116.8								0.06	
	17				S-2		CH	Gray clay (very soft)	94.9				95	69	99.7			0.14
	20				S-3		CH	Gray clay (very soft)	96.2									0.20
5	26				S-4		CH	Gray clay (very soft)	88.5				108	78				0.19
	25				S-5		CH	Gray clay (very soft)	81.7									0.20
10	26				S-6		CH	Estimated top of Pleistocene										0.22
	26				S-7		CH	Gray clay at top 18", 1" shell layer, gray and tan clay with ferrous nodules and shells at bottom 5" (very soft)	87.5									
	22				S-8		CH	Gray and tan clay with ferrous nodules and calcareous nodules (very soft)	31.2									
15	6				S-9		CH	Tan and gray clay with ferrous nodules and calcareous nodules (very soft)	25.9									
							Tan and gray clay with calcareous nodules and ferrous nodules	28.1										

Note: See Figure B-1 for explanation of symbols.
Coordinates Data Source: Horizontal approximated based on GPS (Survey), Vertical approximated based on (undetermined)
*Indicates a remold was used for strength testing.

Log of Boring V-2



Project: Grand Chenier Marsh Creation
Project Location: Cameron Parish, Louisiana
Project Number: 10883-026-00

Figure D-3
Sheet 1 of 1

Date: 2/21/23 Path: \\10.10883026\GINT\10883026\GINT\10883026\GIP\DLLibrary\Library\GEOENGINEERS_DF_STD_US_JUNE_2017\GLB\GERB_GEO TECH_LAB_NO_GW

Start Drilled	10/18/2022	End	10/18/2022	Total Depth (ft)	16	Logged By	NLT	Checked By	NH	Driller	AM Drilling	Drilling Method	Vibracore
Surface Elevation (ft) Vertical Datum	Undetermined NAVD88			Hammer Data	Cathead Hammer 140 (lbs) / 30 (in) Drop			Drilling Equipment Vibracore					
Latitude	29.641394			System Datum	Decimal Degrees Geographic NAD83 (ft)			Water depth approximately 23 ft at time of exploration					
Longitude	-92.872699												
Notes:													

Elevation (feet)	Depth (feet)	FIELD DATA					Graphic Log	Group Classification	MATERIAL DESCRIPTION	LABORATORY DATA									
		Interval	Recovered (in)	Blows/foot or Pocket Pen (TSF)	Collected Sample	Sample Name				Water Content, %	Dry Density, (pcf)	Shear Strength, (KSF)	Confining Pressure, (PSI)	Strain, %	Liquid Limit (LL), %	Plasticity Index (PI), %	Passing No. 200 Sieve, %	Tonvane Shear Strength (KSF)	
0	22					S-1	[Hatched Pattern]	CH	Gray clay (very soft)	103.6									0.10
	25					S-2		CH	Gray clay (very soft)	94.5									0.10
	26					S-3		CH	Gray clay (very soft)	87.8				104	75	99.3			0.18
5	24					S-4		CH	Gray clay (very soft)	95.2				100	73				0.23
	26					S-5		CH	Gray clay (very soft)	79.5									0.10
10	17					S-6	CH	Estimated top of Pleistocene											
	25					S-7	CH	Gray clay at top 4", 2" shell layer, gray and tan clay with ferrous nodules at bottom 18" (medium to stiff)	31.5										
	28					S-8	CH	Gray and tan clay with calcareous nodules and ferrous nodules (medium to stiff)	32.8										
15							CH	Tan and gray clay with calcareous nodules and ferrous nodules (medium to stiff)	25.8										

Note: See Figure B-1 for explanation of symbols.
Coordinates Data Source: Horizontal approximated based on GPS (Survey), Vertical approximated based on (undetermined)
*Indicates a remold was used for strength testing.

Log of Boring V-4



Project: Grand Chenier Marsh Creation
Project Location: Cameron Parish, Louisiana
Project Number: 10883-026-00

Date: 2/21/23 Path: \\ID_10883026\GINT\088302600.GPJ DBLibrary\Library\GEOENGINEERS_DF_STD_US_JUNE_2017\GLB\GERB_GEO TECH_LAB_NO_GW

Start Drilled	10/20/2022	End	10/20/2022	Total Depth (ft)	16	Logged By	NLT	Checked By	NH	Driller	AM Drilling	Drilling Method	Vibracore
Surface Elevation (ft) Vertical Datum	Undetermined NAVD88			Hammer Data	Cathead Hammer 140 (lbs) / 30 (in) Drop			Drilling Equipment Vibracore					
Latitude	29.643302			System Datum	Decimal Degrees Geographic NAD83 (ft)			Water depth approximately 23 ft at time of exploration					
Longitude	-92.864426												
Notes:													

Elevation (feet)	Depth (feet)	FIELD DATA					Graphic Log	Group Classification	MATERIAL DESCRIPTION	LABORATORY DATA									
		Interval	Recovered (in)	Blows/foot or Pocket Pen (TSF)	Collected Sample	Sample Name				Water Content, %	Dry Density, (pcf)	Shear Strength, (KSF)	Confining Pressure, (PSI)	Strain, %	Liquid Limit (LL), %	Plasticity Index (PI), %	Passing No. 200 Sieve, %	Tonvane Shear Strength (KSF)	
	0	22				S-1		CH	Gray clay (very soft)	120.7									0.09
	21					S-2		CH	Gray clay (very soft)	89.9				104	78				0.18
	20					S-3		CH	Gray clay (very soft)	88.1									0.18
5	19					S-4		CH	Gray clay (very soft)	92				95	67	99.7			0.17
	22					S-5		CH	Gray clay with 2" shell layer at bottom (very soft)	87.5									0.23
10	24					S-6		CL	Gray and tan clay with silt, calcareous nodules and ferrous nodules (medium to stiff)	28.3									
	22					S-7		CL	Estimated top of Pleistocene										
	24					S-8		CH	Tan and gray clay with ferrous nodules and calcareous nodules and 4" layer of gray silty clay with shells (medium to stiff)	23.6									

Note: See Figure B-1 for explanation of symbols.
Coordinates Data Source: Horizontal approximated based on GPS (Survey), Vertical approximated based on (undetermined)
*Indicates a remold was used for strength testing.

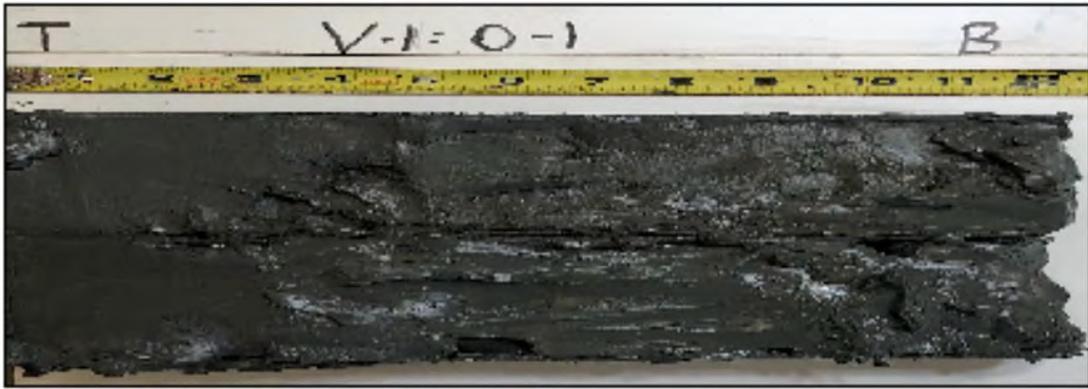
Log of Boring V-6



Project: Grand Chenier Marsh Creation
Project Location: Cameron Parish, Louisiana
Project Number: 10883-026-00

Figure D-7
Sheet 1 of 1

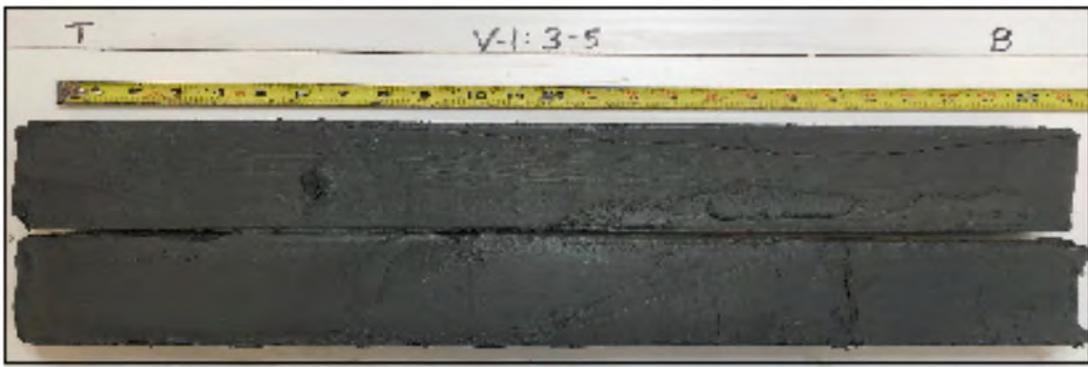
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V-1
Depth Below Mudline 0'-1'



V-1
Depth Below Mudline 1'-3'



V-1
Depth Below Mudline 3'-5'

Top

Bottom

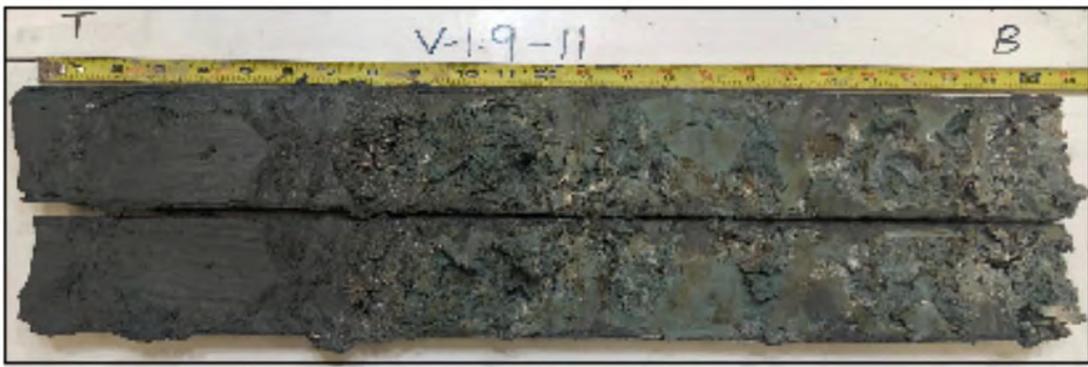
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V-1
Depth Below Mudline 5'-7'



V-1
Depth Below Mudline 7'-9'



V-1
Depth Below Mudline 9'-11'

Top

Bottom

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V-1
Depth Below Mudline 11'-13'



V-1
Depth Below Mudline 13'-15'



V-1
Depth Below Mudline 15'-17'

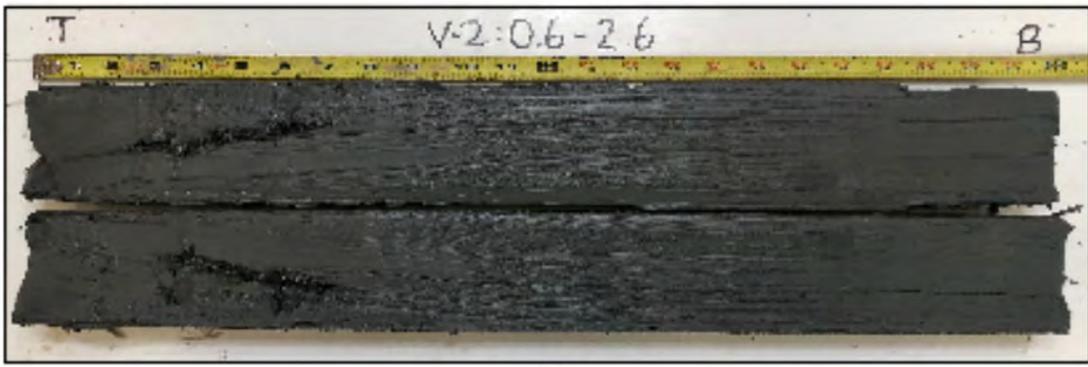
Top

Bottom

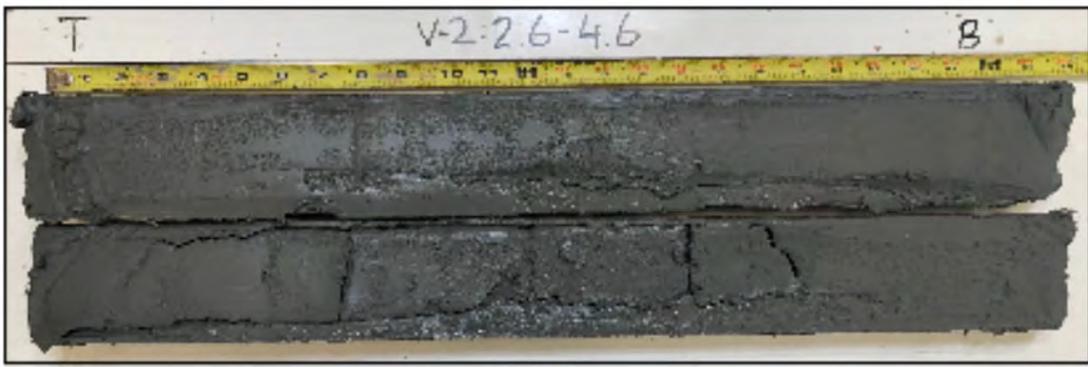
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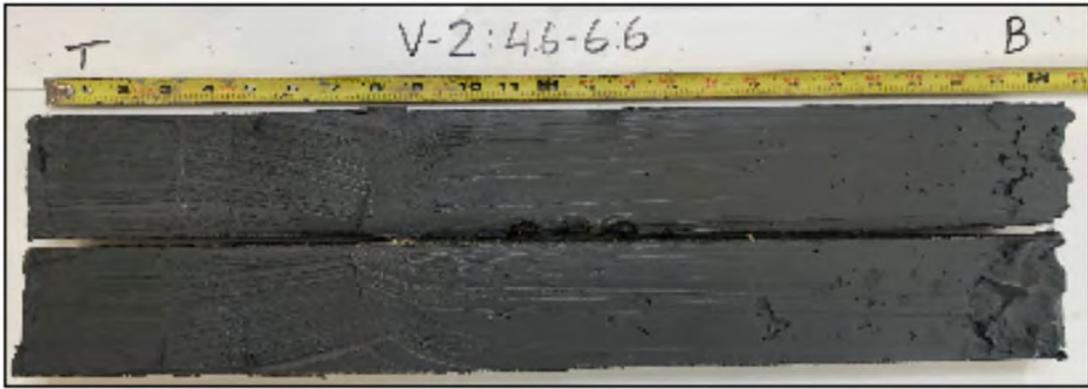
V-2
Depth Below Mudline 0'-0.6'



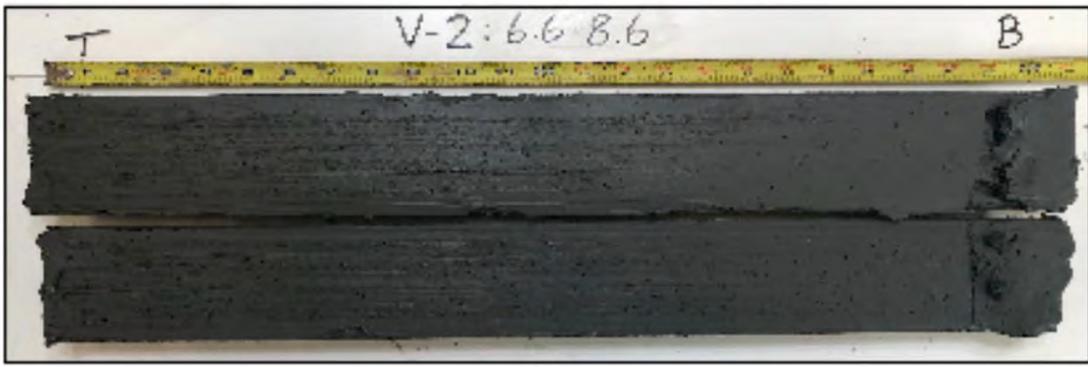
V-2
Depth Below Mudline 0.6'-2.6'



V-2
Depth Below Mudline 2.6'-4.6'



V-2
Depth Below Mudline 4.6'-6.6'



V-2
Depth Below Mudline 6.6'-8.6'



V-2
Depth Below Mudline 8.6'-10.6'

Top

Bottom

PA1310108310261001Photo

Photo Log
V-2

USDA-NRCS - S Grand Chenier Marsh Creation Baker
Grand Chenier, Louisiana



Figure D-9b



V-2
Depth Below Mudline 10.6'-12.6'

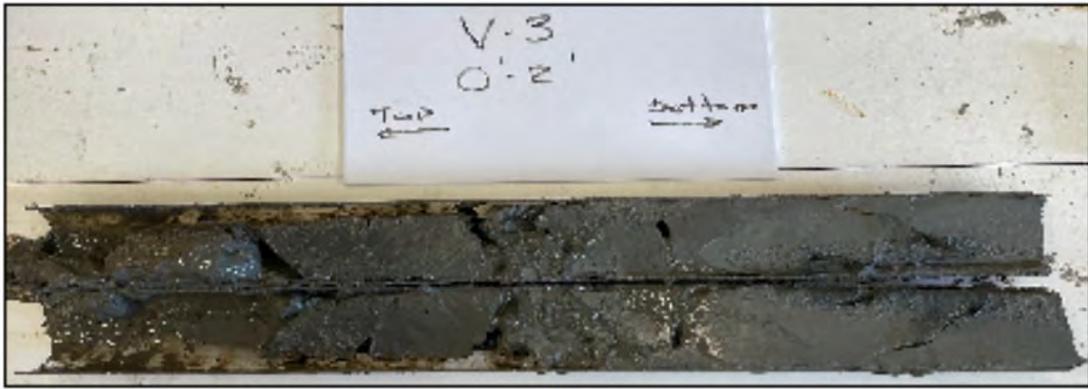


V-2
Depth Below Mudline 12.6'-14.6'

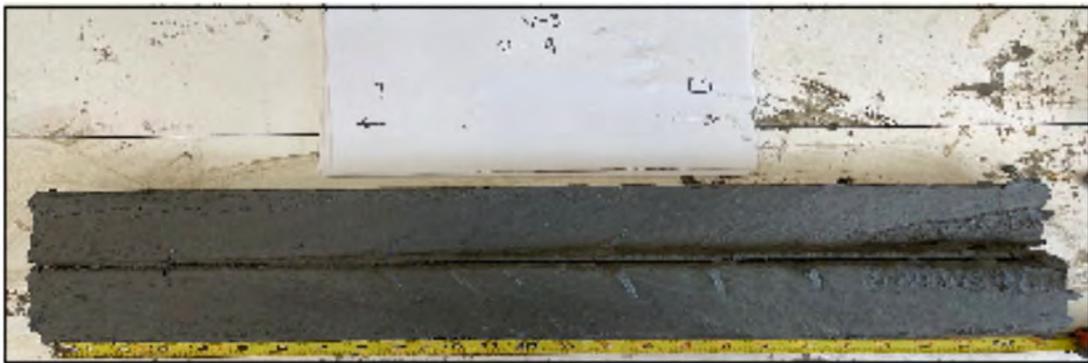


V-2
Depth Below Mudline 14.6'-16.6'

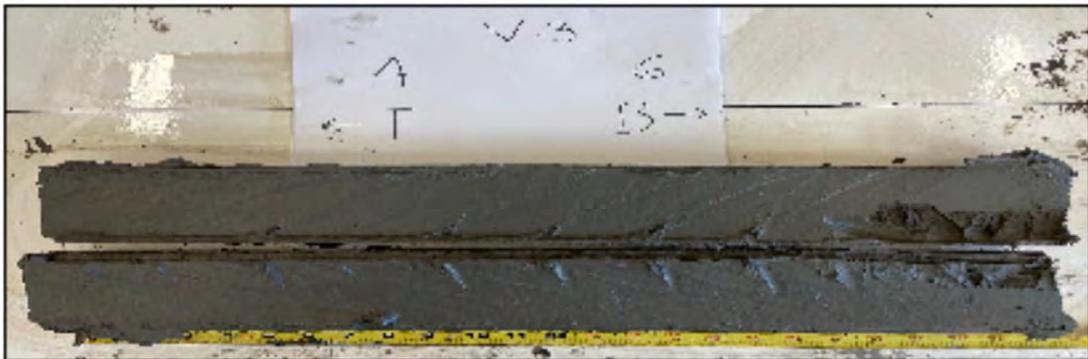
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V-3
Depth Below Mudline 0'-2'



V-3
Depth Below Mudline 2'-4'

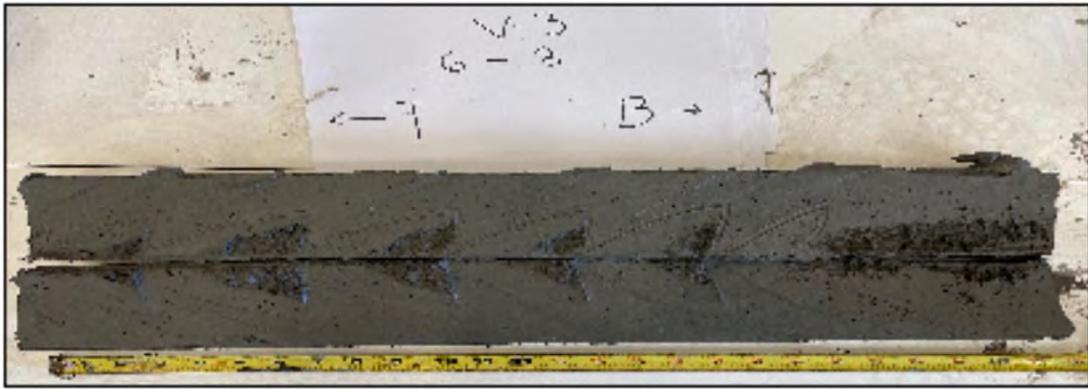


V-3
Depth Below Mudline 4'-6'

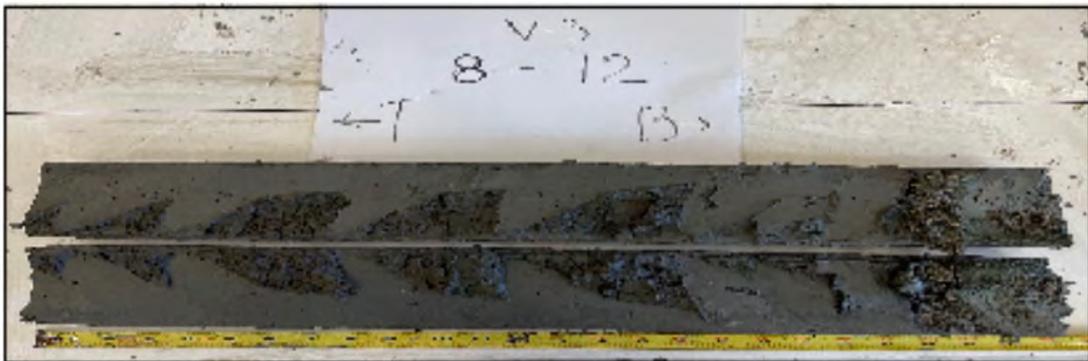
Top

Bottom

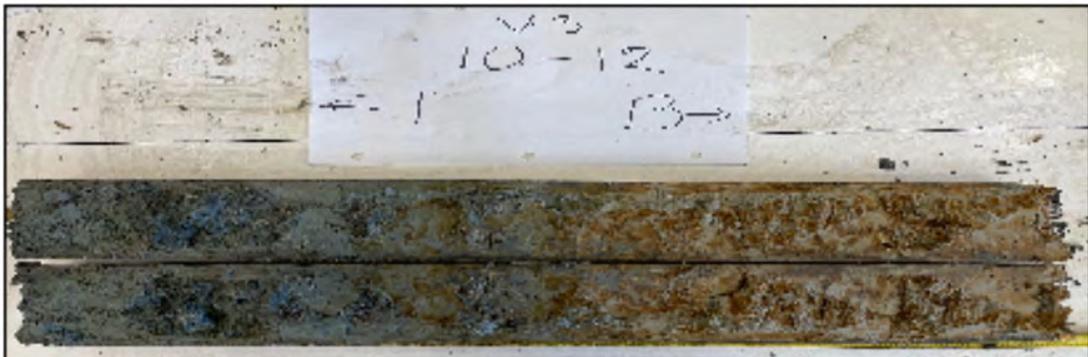
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V-3
Depth Below Mudline 6'-8'



V-3
Depth Below Mudline 8'-10'



V-3
Depth Below Mudline 10'-12'

Top

Bottom

PA10100830261001Photo

Photo Log
V-3

USDA-NRCS - S Grand Chenier Marsh Creation Baker
Grand Chenier, Louisiana



Figure D-10b



V-3
Depth Below Mudline 12'-14'



V-3
Depth Below Mudline 14'-16'

Top

Bottom

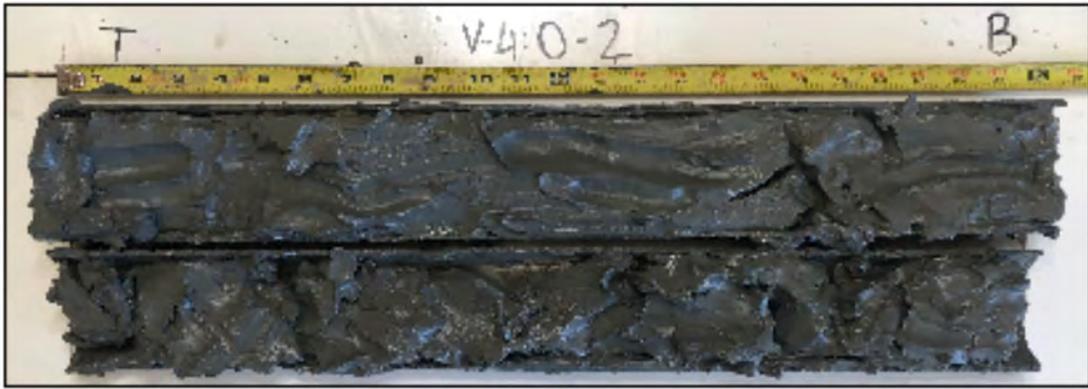
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Photo Log
V-3

USDA-NRCS - 8 Grand Chenier Marsh Creation Baker
Grand Chenier, Louisiana



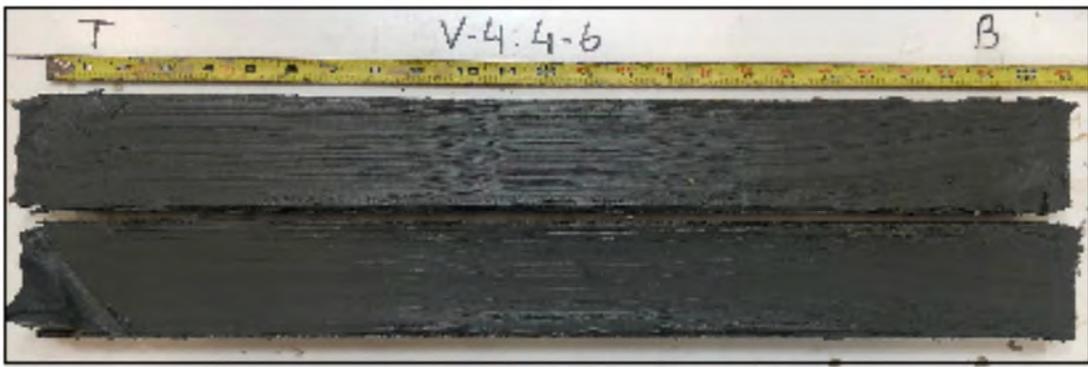
Figure D-10c



V-4
Depth Below Mudline 0'-2'



V-4
Depth Below Mudline 2'-4'



V-4
Depth Below Mudline 4'-6'

Top

Bottom

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V-4
Depth Below Mudline 6'-8'



V-4
Depth Below Mudline 8'-10'



V-4
Depth Below Mudline 10'-12'

Photo Log
V-4

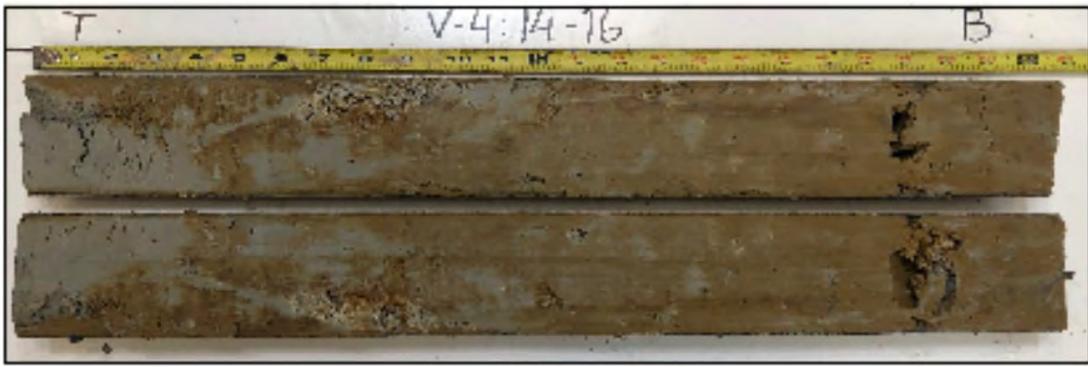
USDA-NRCS - 8 Grand Chenier Marsh Creation Baker
Grand Chenier, Louisiana

GEOENGINEERS 

Figure D-11b



V-4
Depth Below Mudline 12'-14'



V-4
Depth Below Mudline 14'-16'

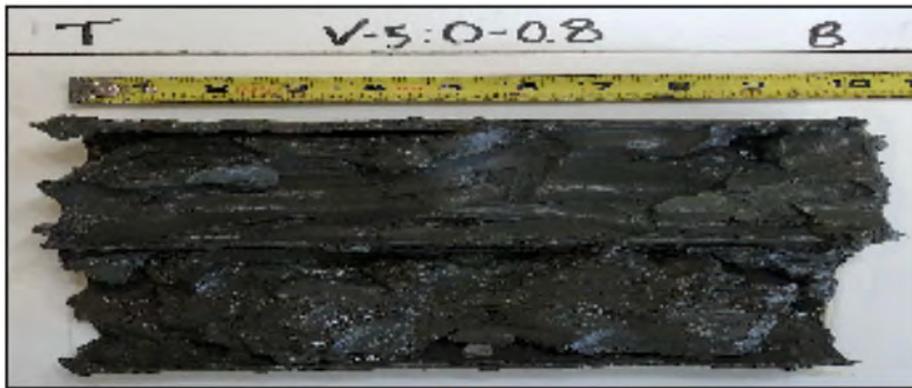
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Photo Log
V-4

USDA-NRCS - S Grand Chenier Marsh Creation Baker
Grand Chenier, Louisiana



Figure D-11c



V-5
Depth Below Mudline 0'-0.8'



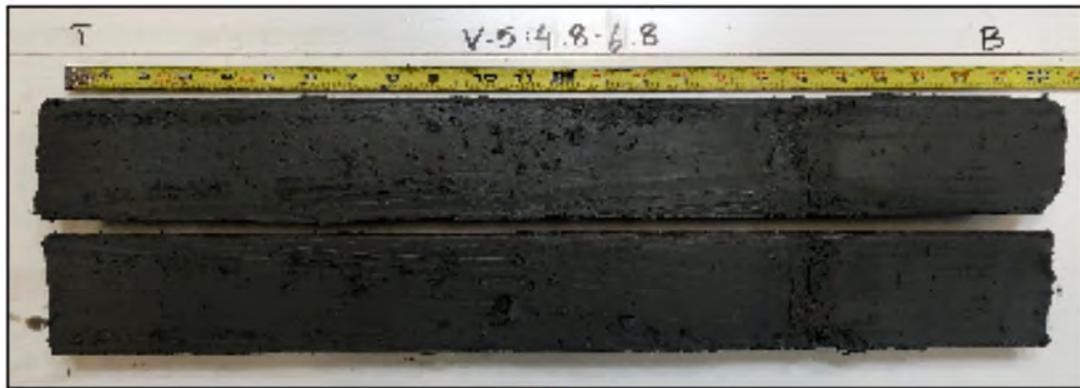
V-5
Depth Below Mudline 0.8'-2.8'



V-5
Depth Below Mudline 2.8'-4.8'

Top

Bottom



V-5
Depth Below Mudline 4.8'-6.8'



V-5
Depth Below Mudline 6.8'-8.8'



V-5
Depth Below Mudline 8.8'-10.8'

Top

Bottom

PA110100830261001Photo

Photo Log
V-5

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Grand Chenier, Louisiana



Figure D-12b



V-5
Depth Below Mudline 10.8'-12.8'



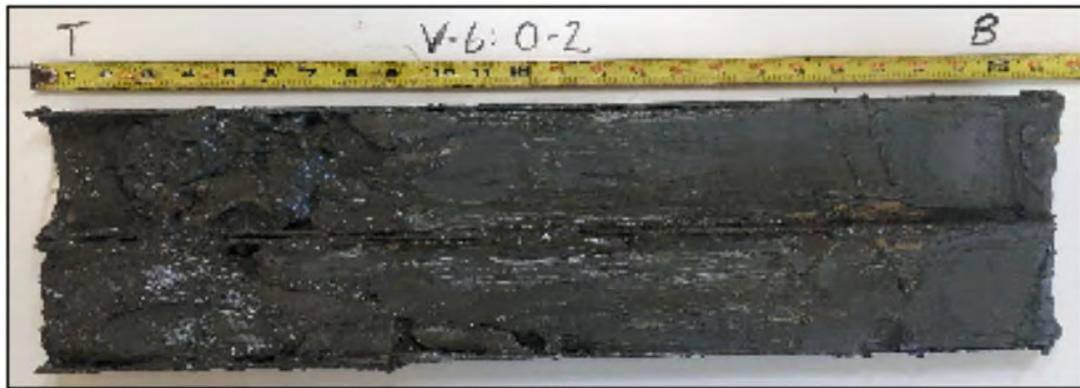
V-5
Depth Below Mudline 12.8'-14.8'



V-5
Depth Below Mudline 14.8'-16.8'

Top

Bottom



V-6
Depth Below Mudline 0'-2'



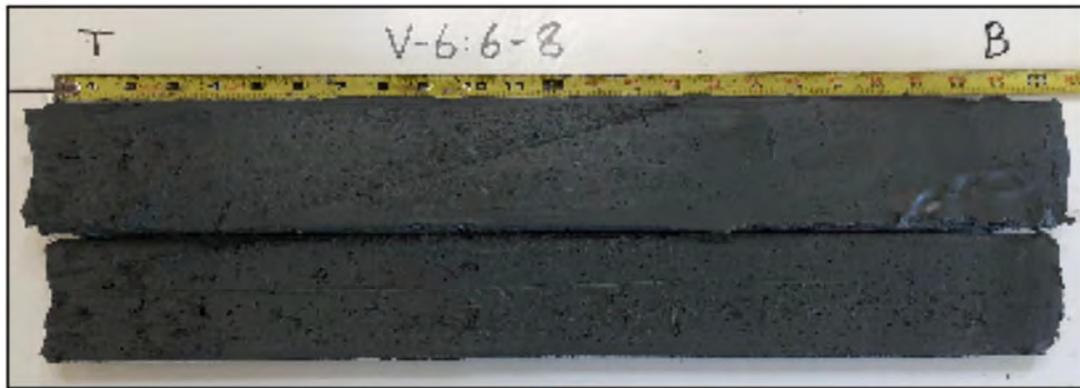
V-6
Depth Below Mudline 2'-4'



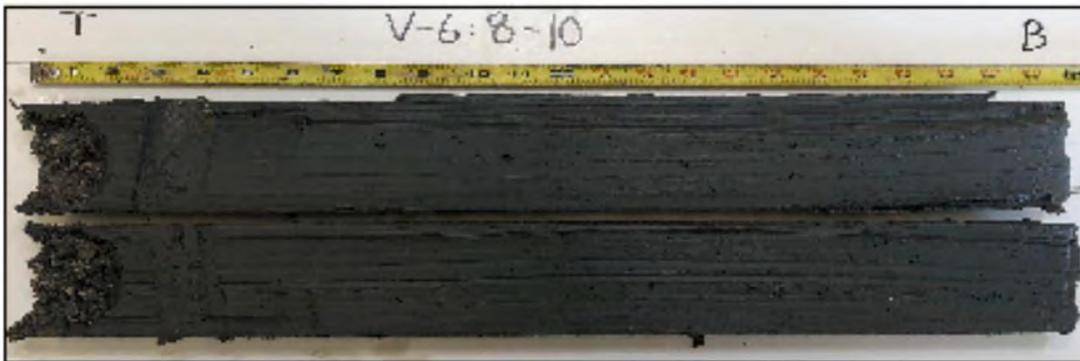
V-6
Depth Below Mudline 4'-6'

Top

Bottom



V-6
Depth Below Mudline 6'-8'



V-6
Depth Below Mudline 8'-10'



V-6
Depth Below Mudline 10'-12'



V-6
Depth Below Mudline 12'-14'



V-6
Depth Below Mudline 14'-16'

Top

Bottom

Table D-1

Boring ID	Depth: FROM	Depth: TO	Shear Strength (ksf)	Unit weight (pcf)
V-1	0	1	0.12	72.39
	1	3	0.17	82.74
	3	5	0.19	
	5	7	0.23	84.73
	7	9	0.24	
	9	11	-	108.68
	11	13	-	
	13	15	-	108.37
15	17	-		
V-2	0	0.6	0.06	51.60
	0.6	2.6	0.14	81.00
	2.6	4.6	0.20	
	4.6	6.6	0.19	81.87
	6.6	8.6	0.20	
	8.6	10.6	0.22	100.10
	10.6	12.6	-	
	12.6	14.6	-	111.89
	14.6	16.6	-	
V-3	0	2	0.01	74.00
	2	4	0.01	89.77
	4	6	0.06	88.33
	6	8	0.09	90.62
	8	10	0.08	96.41
	10	12	0.13	116.60
	12	14	-	113.28
	14	16	-	
V-4	0	2	0.10	66.81
	2	4	0.10	
	4	6	0.18	95.75
	6	8	0.23	
	8	10	0.10	95.71
	10	12	-	
	12	14	-	107.64
14	16	-		
V-5	0	0.8	0.04	59.62
	0.8	2.8	0.18	82.43
	2.8	4.8	0.18	
	4.8	6.8	0.14	84.73
	6.8	8.8	0.20	
	8.8	10.8	-	108.30
	10.8	12.8	-	
	12.8	14.8	-	109.69
14.8	16.8	-		
V-6	0	2	0.10	78.63
	2	4	0.18	
	4	6	0.18	82.74
	6	8	0.17	
	8	10	0.24	98.99
	10	12	-	
	12	14	-	111.61
14	16	-		

APPENDIX E
Laboratory Testing Results

LABORATORY TEST RESULTS

Boring No. B-1

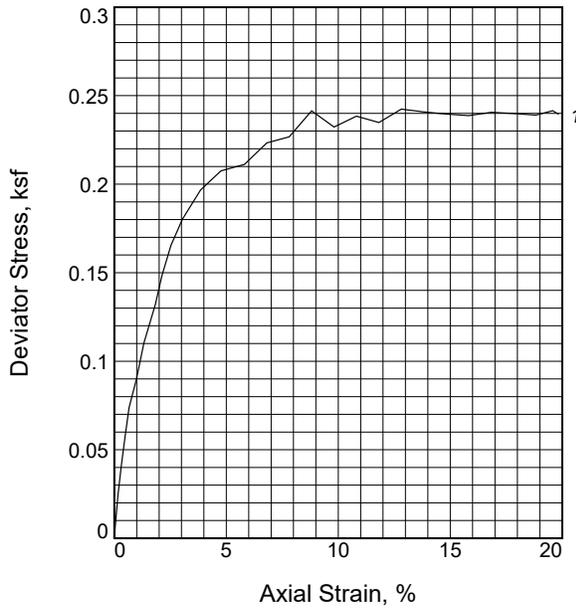
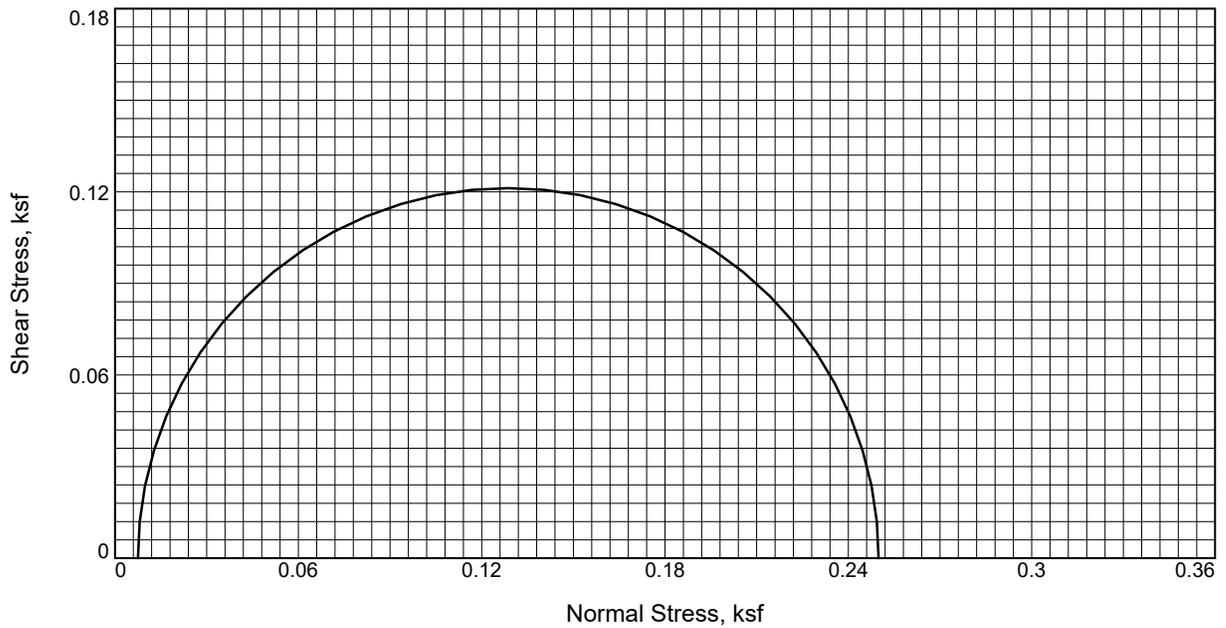
Date Tested	Depth (ft)	ASTM D2216	ASTM D2937	ASTM D2850	ASTM D4318			ASTM D2974	ASTM D2488
		Moisture Content (%)	Dry Density (pcf)	Shear Strength (ksf)	Atterberg Limits			Organic Content (%)	Classification
					LL	PL	PI		
11/16/22	0-2				134	37	97		Gray Fat Clay (CH)
11/14/22	2-4	98.8	48.2	0.120					Gray Fat Clay (CH)
11/14/22	4-6	104.2	44.6	0.080					Gray Fat Clay (CH)
11/14/22	8-10	106.0	49.3	0.090					Gray Fat Clay w/ Sand & Shell Fragment Layer (CH)
11/14/22	10-12	118.7	43.4	0.110					Gray Fat Clay (CH)
	12-14								Gray Fat Clay (CH)
11/14/22	14-16	101.2	47.1	0.145					Gray Fat Clay (CH)
11/15/22	16-18	100.3			115	25	90		Gray Fat Clay (CH)
11/14/22	18-20	31.9	89.8	0.620					Gray Silty Clay w/ Ferrous Nodules (CL)

Notes:

Project: S. Grand Chenier Marsh Creation Baker Tract
 Client: GeoEngineers, Inc.



Project Number: L-GEI-020
 Date: 02/10/23



Sample No.		1
Initial	Water Content, %	98.8
	Dry Density, pcf	48.2
	Saturation, %	107.5
	Void Ratio	2.4342
	Diameter, in.	2.78
At Test	Height, in.	5.65
	Water Content, %	97.5
	Dry Density, pcf	48.2
	Saturation, %	106.1
	Void Ratio	2.4342
Diameter, in.		2.78
Height, in.		5.65
Strain rate, in./min.		1.000
Back Pressure, psi		0.00
Cell Pressure, psi		0.05
Fail. Stress, ksf		0.24
Ult. Stress, ksf		
σ_1 Failure, ksf		0.25
σ_3 Failure, ksf		0.01

Type of Test:
Unconsolidated Undrained

Sample Type: Undisturbed

Description: Gray Fat Clay

Assumed Specific Gravity= 2.65

Remarks:

Client: GeoEngineers, Inc.

Project: S Grand Chenier Marsh Creation Baker Tract

Source of Sample: B-1 **Depth:** 2-4

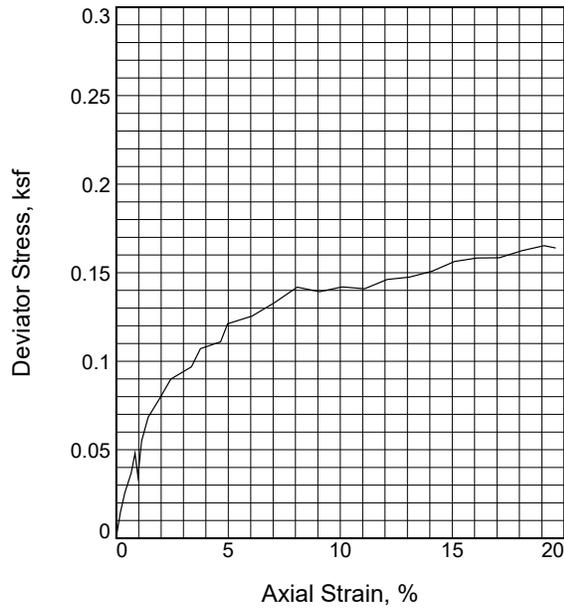
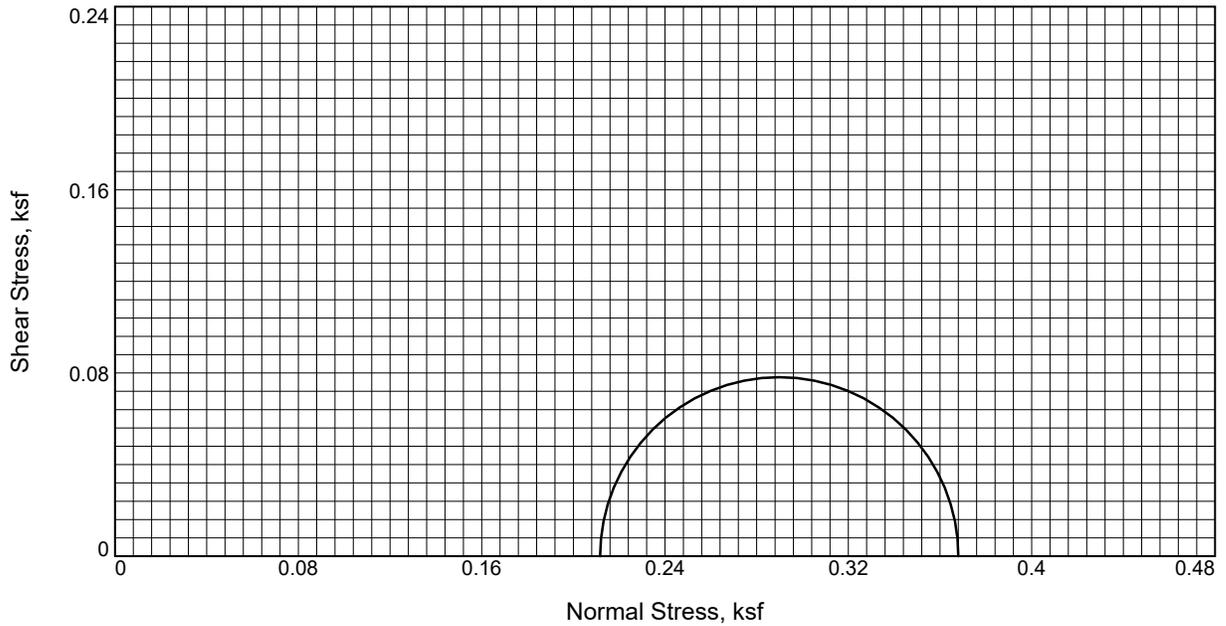
Sample Number: B-1

Proj. No.: L-GEI-020

Date Sampled:

TRIAXIAL SHEAR TEST REPORT
 Fourier & de Abreu Engineers, LLC
 Baton Rouge, Louisiana

Figure _____



Sample No.		1
Initial	Water Content, %	104.2
	Dry Density, pcf	44.6
	Saturation, %	101.9
	Void Ratio	2.7101
	Diameter, in.	2.80
At Test	Height, in.	5.68
	Water Content, %	122.4
	Dry Density, pcf	44.6
	Saturation, %	119.6
	Void Ratio	2.7101
Diameter, in.		2.80
Height, in.		5.68
Strain rate, in./min.		1.000
Back Pressure, psi		0.00
Cell Pressure, psi		1.47
Fail. Stress, ksf		0.16
Ult. Stress, ksf		
σ_1 Failure, ksf		0.37
σ_3 Failure, ksf		0.21

Type of Test:
Unconsolidated Undrained

Sample Type: Undisturbed
Description: Gray Fat Clay

Assumed Specific Gravity= 2.65

Remarks:

Figure _____

Client: GeoEngineers, Inc.

Project: S Grand Chenier Marsh Creation Baker Tract

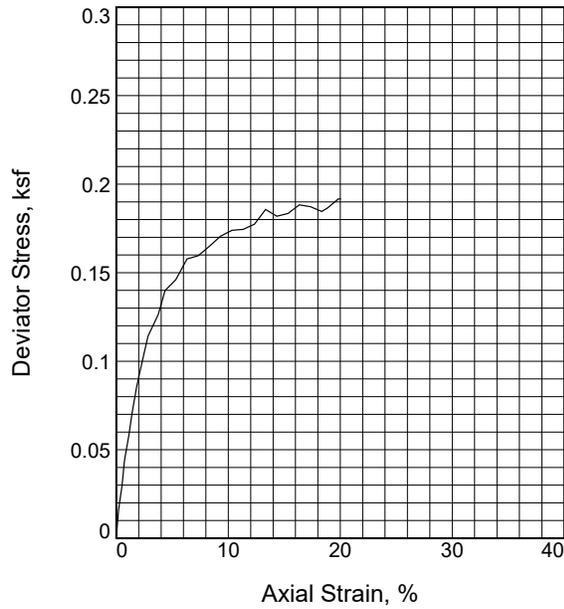
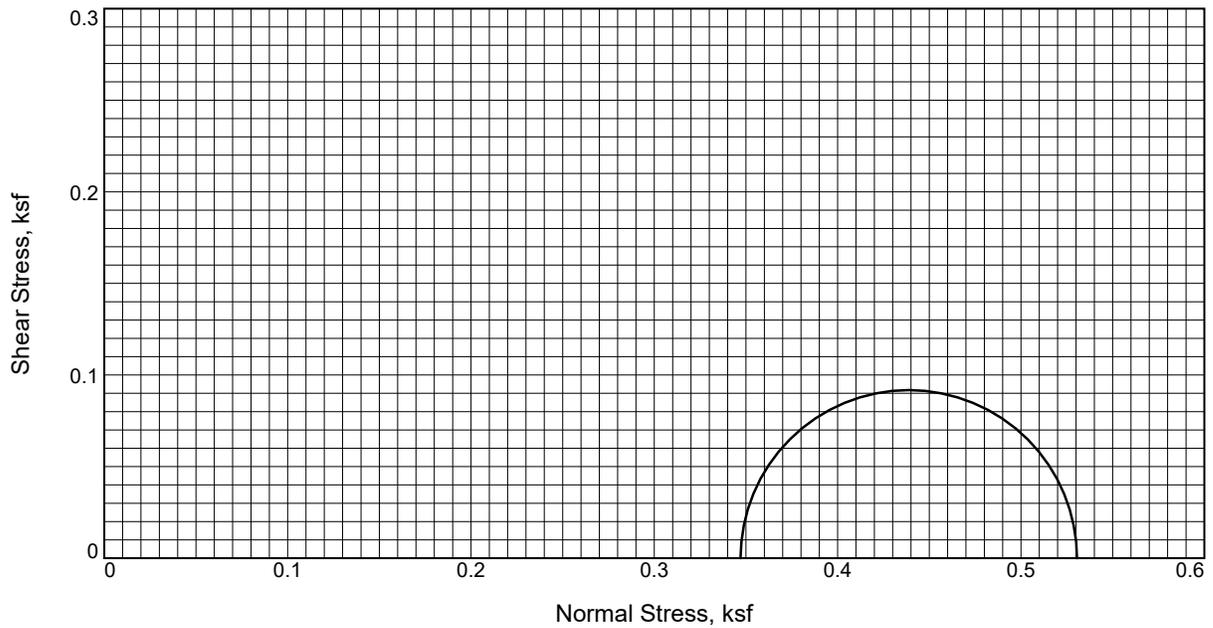
Source of Sample: B-1 **Depth:** 4-6

Sample Number: B-1

Proj. No.: L-GEI-020

Date Sampled:

TRIAXIAL SHEAR TEST REPORT
Fourrier & de Abreu Engineers, LLC
Baton Rouge, Louisiana



Sample No.		1
Initial	Water Content, %	106.0
	Dry Density, pcf	49.3
	Saturation, %	119.2
	Void Ratio	2.3562
	Diameter, in.	2.72
At Test	Height, in.	5.61
	Water Content, %	104.5
	Dry Density, pcf	49.3
	Saturation, %	117.6
	Void Ratio	2.3562
Diameter, in.		2.72
Height, in.		5.61
Strain rate, in./min.		1.000
Back Pressure, psi		0.00
Cell Pressure, psi		2.41
Fail. Stress, ksf		0.18
Ult. Stress, ksf		
σ_1 Failure, ksf		0.53
σ_3 Failure, ksf		0.35

Type of Test:
Unconsolidated Undrained

Sample Type: Undisturbed

Description: Gray Fat Clay w/ Sand & Shell
Fragment Layer

Assumed Specific Gravity= 2.65

Remarks:

Client: GeoEngineers, Inc.

Project: S Grand Chenier Marsh Creation Baker Tract

Source of Sample: B-1 **Depth:** 8-10

Sample Number: B-1

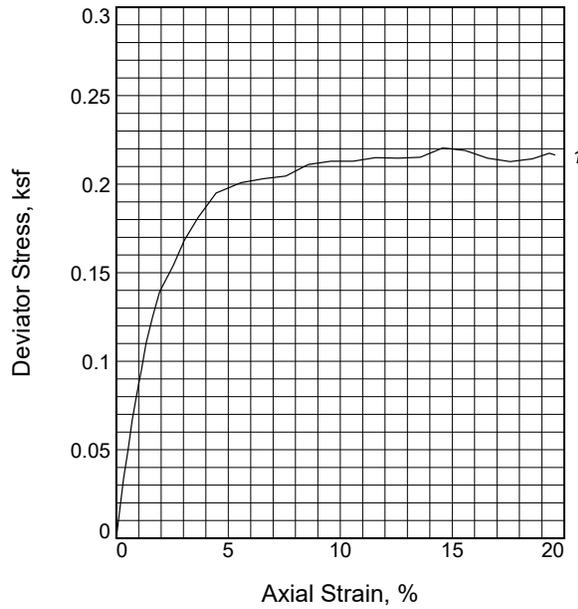
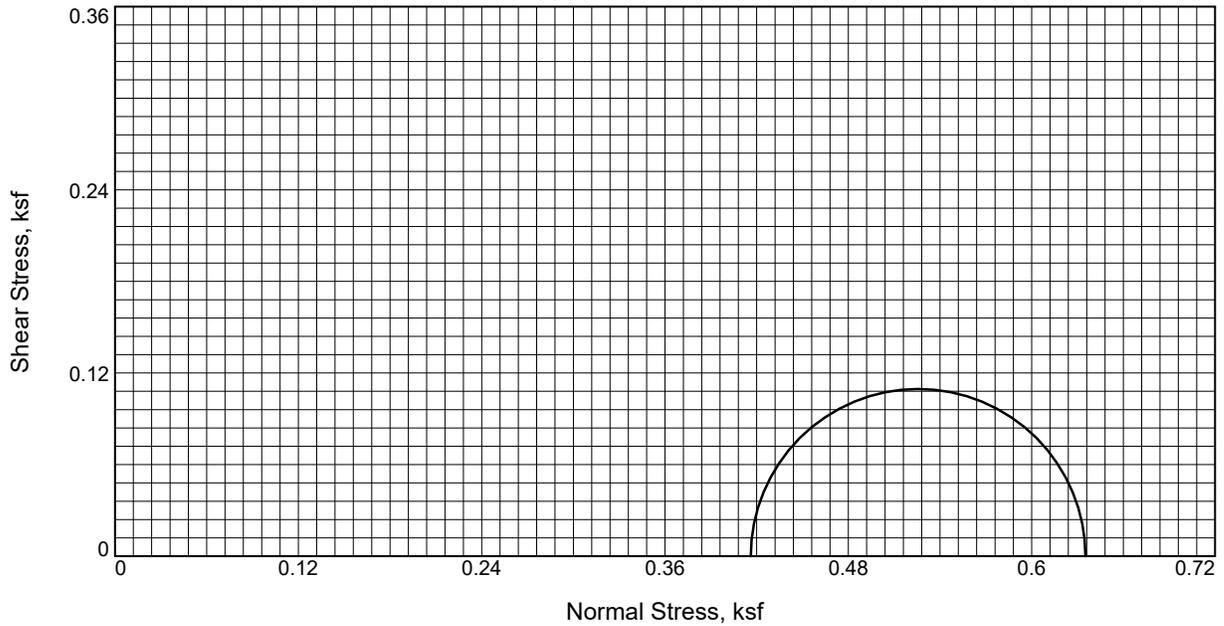
Proj. No.: L-GEI-020

Date Sampled:

TRIAXIAL SHEAR TEST REPORT
Fourrier & de Abreu Engineers, LLC
Baton Rouge, Louisiana

Figure _____

Tested By: CM **Checked By:** JOF



Sample No.		1
Initial	Water Content, %	118.7
	Dry Density, pcf	43.4
	Saturation, %	111.8
	Void Ratio	2.8139
	Diameter, in.	2.75
	Height, in.	5.68
At Test	Water Content, %	108.1
	Dry Density, pcf	43.4
	Saturation, %	101.8
	Void Ratio	2.8139
	Diameter, in.	2.75
	Height, in.	5.68
Strain rate, in./min.		1.000
Back Pressure, psi		0.00
Cell Pressure, psi		2.89
Fail. Stress, ksf		0.22
Ult. Stress, ksf		
σ_1 Failure, ksf		0.64
σ_3 Failure, ksf		0.42

Type of Test:
Unconsolidated Undrained

Sample Type: Undisturbed
Description: Gray Fat Clay

Assumed Specific Gravity= 2.65

Remarks:

Figure _____

Client: GeoEngineers, Inc.

Project: S Grand Chenier Marsh Creation Baker Tract

Source of Sample: B-1 **Depth:** 10-12

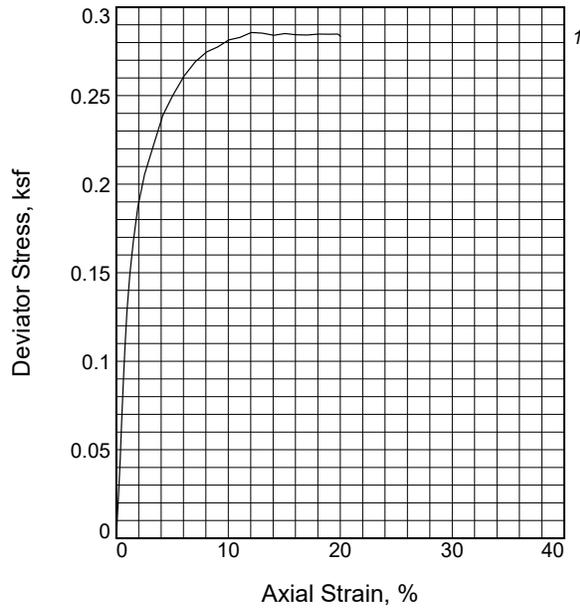
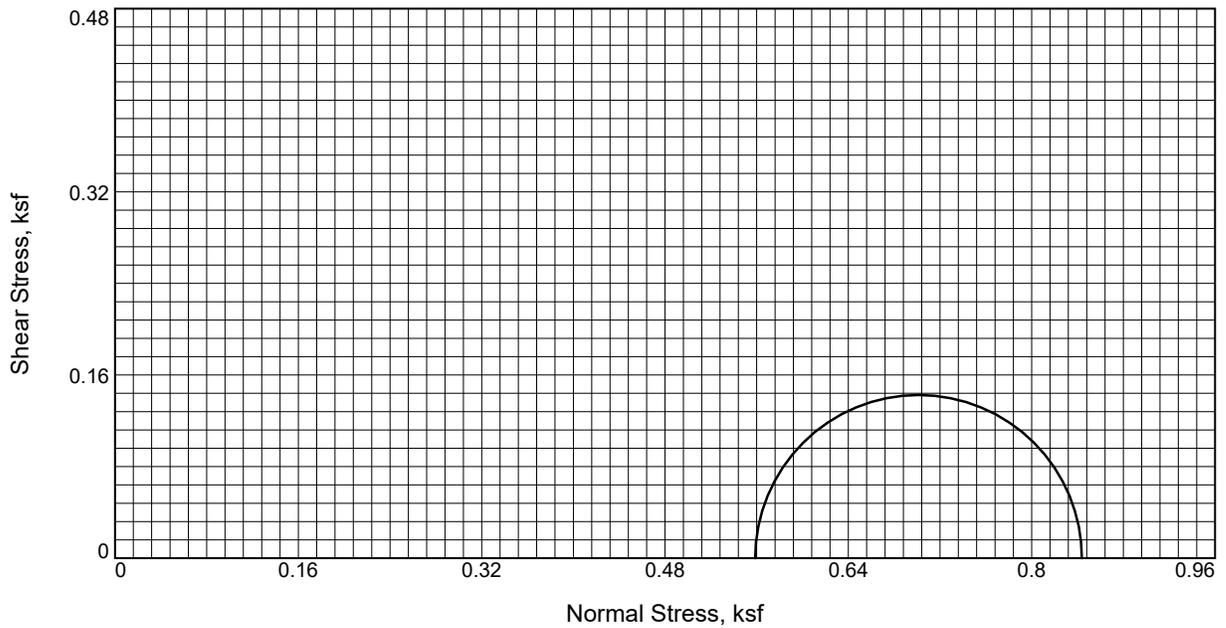
Sample Number: B-1

Proj. No.: L-GEI-020

Date Sampled:

TRIAXIAL SHEAR TEST REPORT
Fourrier & de Abreu Engineers, LLC
Baton Rouge, Louisiana

Tested By: CM **Checked By:** JOF



Sample No.		1
Initial	Water Content, %	101.2
	Dry Density, pcf	47.1
	Saturation, %	106.9
	Void Ratio	2.5087
	Diameter, in.	2.83
At Test	Height, in.	5.65
	Water Content, %	93.3
	Dry Density, pcf	47.1
	Saturation, %	98.6
	Void Ratio	2.5087
Diameter, in.		2.83
Height, in.		5.65
Strain rate, in./min.		1.000
Back Pressure, psi		0.00
Cell Pressure, psi		3.88
Fail. Stress, ksf		0.29
Ult. Stress, ksf		
σ_1 Failure, ksf		0.84
σ_3 Failure, ksf		0.56

Type of Test:

Unconsolidated Undrained

Sample Type: Undisturbed

Description: Gray Fat Clay

Assumed Specific Gravity= 2.65

Remarks:

Figure _____

Client: GeoEngineers, Inc.

Project: S Grand Chenier Marsh Creation Baker Tract

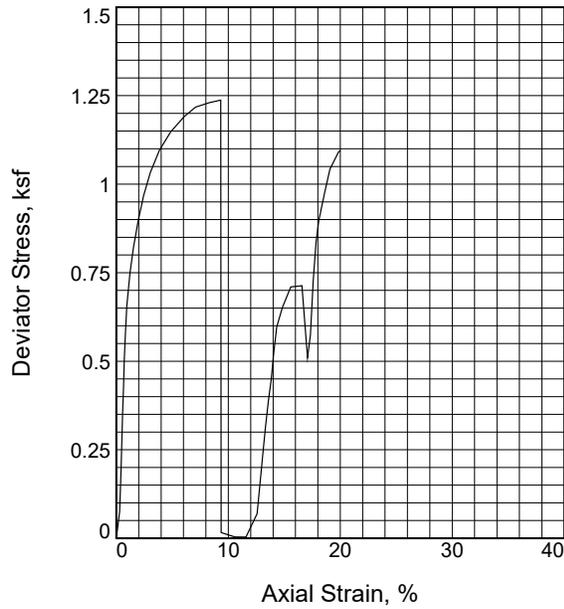
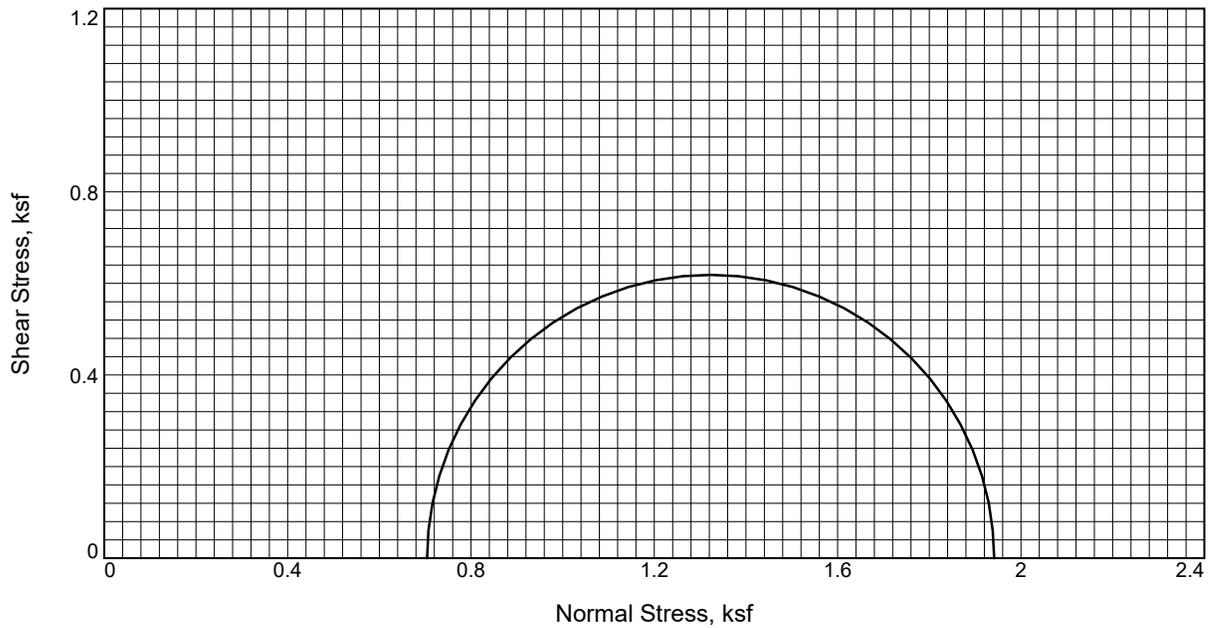
Source of Sample: B-1 **Depth:** 14-16

Sample Number: B-1

Proj. No.: L-GEI-020

Date Sampled:

TRIAXIAL SHEAR TEST REPORT
 Fourier & de Abreu Engineers, LLC
 Baton Rouge, Louisiana



Sample No.		1
Initial	Water Content, %	31.9
	Dry Density, pcf	89.8
	Saturation, %	100.4
	Void Ratio	0.8419
	Diameter, in.	2.83
	Height, in.	5.02
At Test	Water Content, %	34.3
	Dry Density, pcf	89.8
	Saturation, %	108.0
	Void Ratio	0.8419
	Diameter, in.	2.83
	Height, in.	5.02
Strain rate, in./min.		1.000
Back Pressure, psi		0.00
Cell Pressure, psi		4.89
Fail. Stress, ksf		1.24
Ult. Stress, ksf		
σ_1 Failure, ksf		1.94
σ_3 Failure, ksf		0.70

Type of Test:
Unconsolidated Undrained
Sample Type: Undisturbed
Description: Gray Silty Clay w/ Ferrous Nodules

Assumed Specific Gravity= 2.65
Remarks:

Client: GeoEngineers, Inc.

Project: S Grand Chenier Marsh Creation Baker Tract

Source of Sample: B-1 **Depth:** 18-20

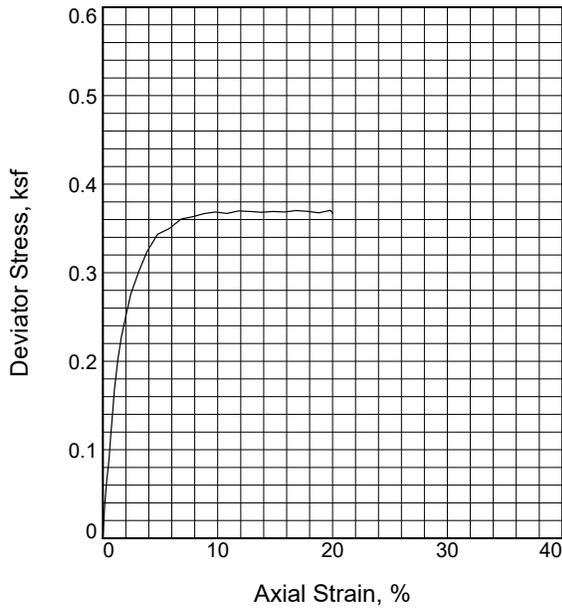
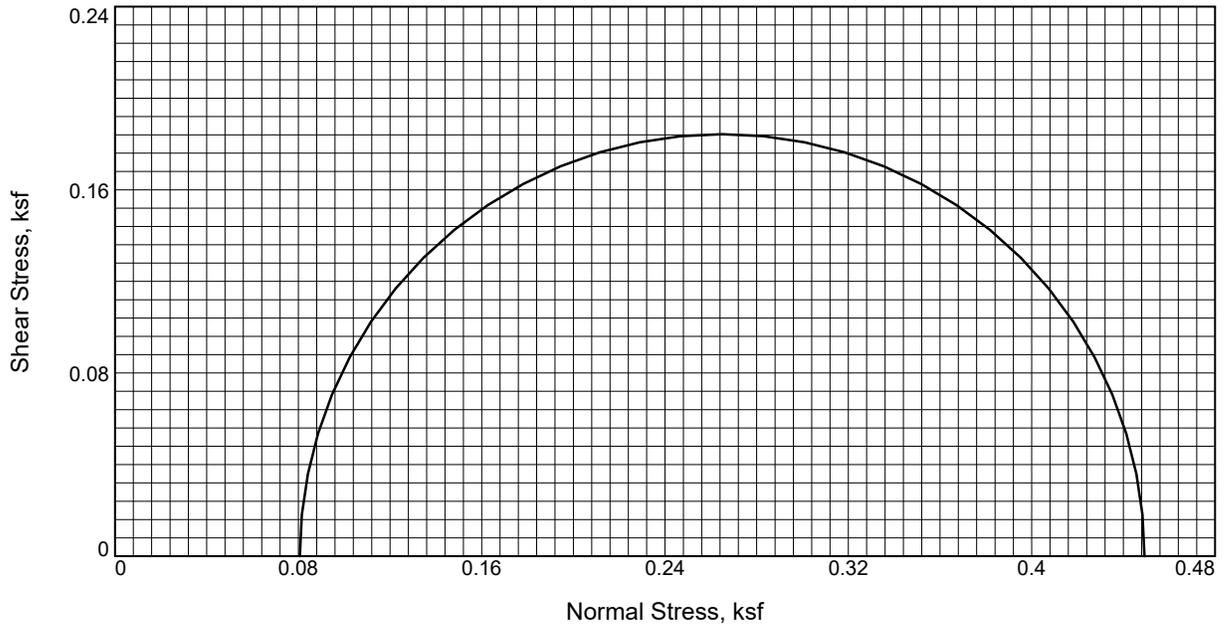
Sample Number: B-1

Proj. No.: L-GEI-020

Date Sampled:

TRIAXIAL SHEAR TEST REPORT
Fourrier & de Abreu Engineers, LLC
Baton Rouge, Louisiana

Figure _____



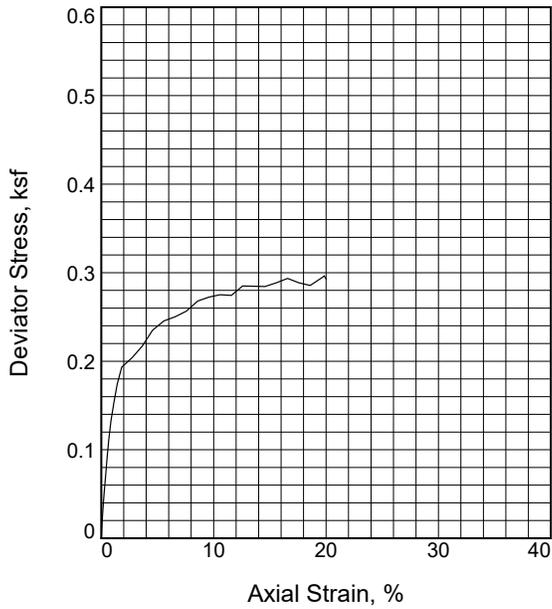
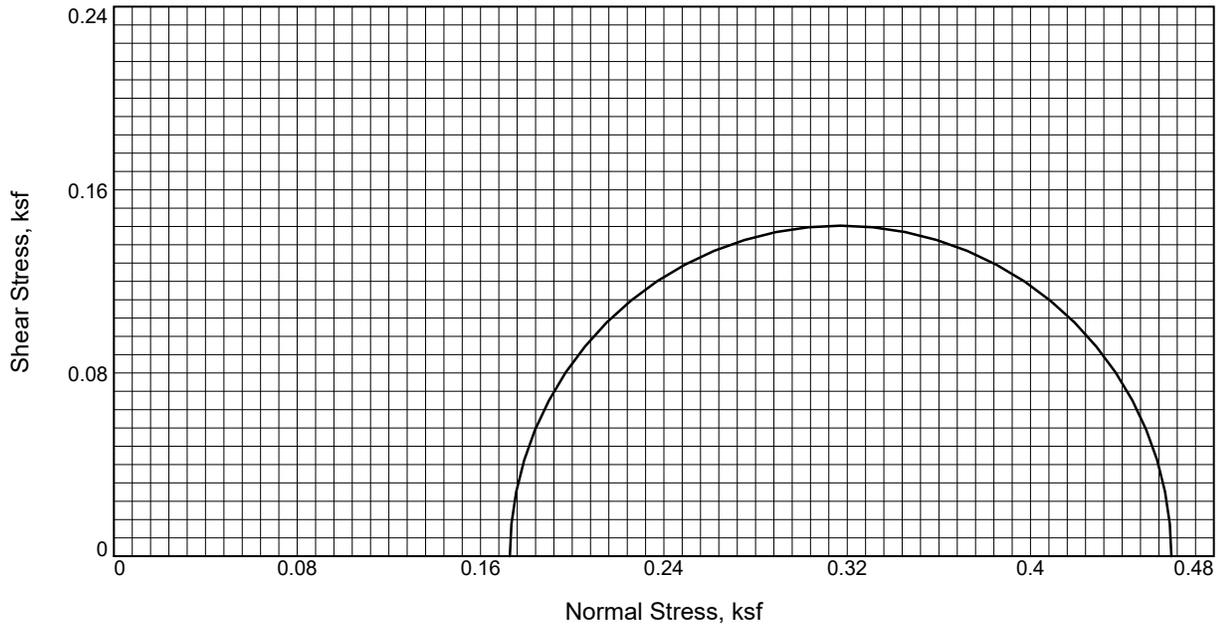
Sample No.		1
Initial	Water Content, %	89.3
	Dry Density, pcf	53.4
	Saturation, %	112.6
	Void Ratio	2.1006
	Diameter, in.	2.74
At Test	Height, in.	5.56
	Water Content, %	95.0
	Dry Density, pcf	53.4
	Saturation, %	119.9
	Void Ratio	2.1006
Diameter, in.		2.74
Height, in.		5.56
Strain rate, in./min.		0.999
Back Pressure, psi		0.00
Cell Pressure, psi		0.56
Fail. Stress, ksf		0.37
Ult. Stress, ksf		
σ_1 Failure, ksf		0.45
σ_3 Failure, ksf		0.08

Type of Test:
Unconsolidated Undrained
Sample Type: Undisturbed
Description: Gray Fat Clay w/ Organics

Assumed Specific Gravity= 2.65
Remarks:

Figure _____

Client: GeoEngineers, Inc.
Project: S Grand Chenier Marsh Creation Baker Tract
Source of Sample: B-2 **Depth:** 0-2
Sample Number: B-2
Proj. No.: L-GEI-020 **Date Sampled:**
 TRIAXIAL SHEAR TEST REPORT
 Fourier & de Abreu Engineers, LLC
 Baton Rouge, Louisiana



Sample No.	1	
Initial	Water Content, %	118.2
	Dry Density, pcf	44.4
	Saturation, %	114.9
	Void Ratio	2.7270
	Diameter, in.	2.74
At Test	Height, in.	5.63
	Water Content, %	99.5
	Dry Density, pcf	44.4
	Saturation, %	96.7
	Void Ratio	2.7270
Diameter, in.	2.74	
Height, in.	5.63	
Strain rate, in./min.	1.000	
Back Pressure, psi	0.00	
Cell Pressure, psi	1.20	
Fail. Stress, ksf	0.29	
Ult. Stress, ksf		
σ_1 Failure, ksf	0.46	
σ_3 Failure, ksf	0.17	

Type of Test:

Unconsolidated Undrained

Sample Type: Undisturbed

Description: Gray Fat Clay w/ Organics

LL= 117

PL= 26

PI= 91

Assumed Specific Gravity= 2.65

Remarks:

Figure _____

Client: GeoEngineers, Inc.

Project: S Grand Chenier Marsh Creation Baker Tract

Source of Sample: B-2

Depth: 2-4

Sample Number: B-2

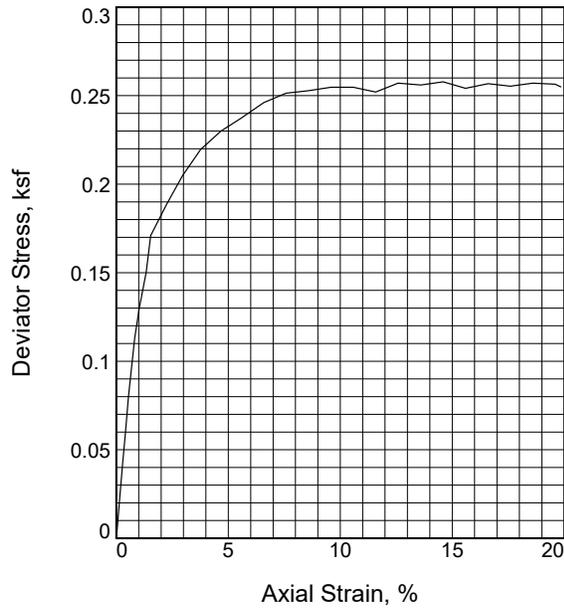
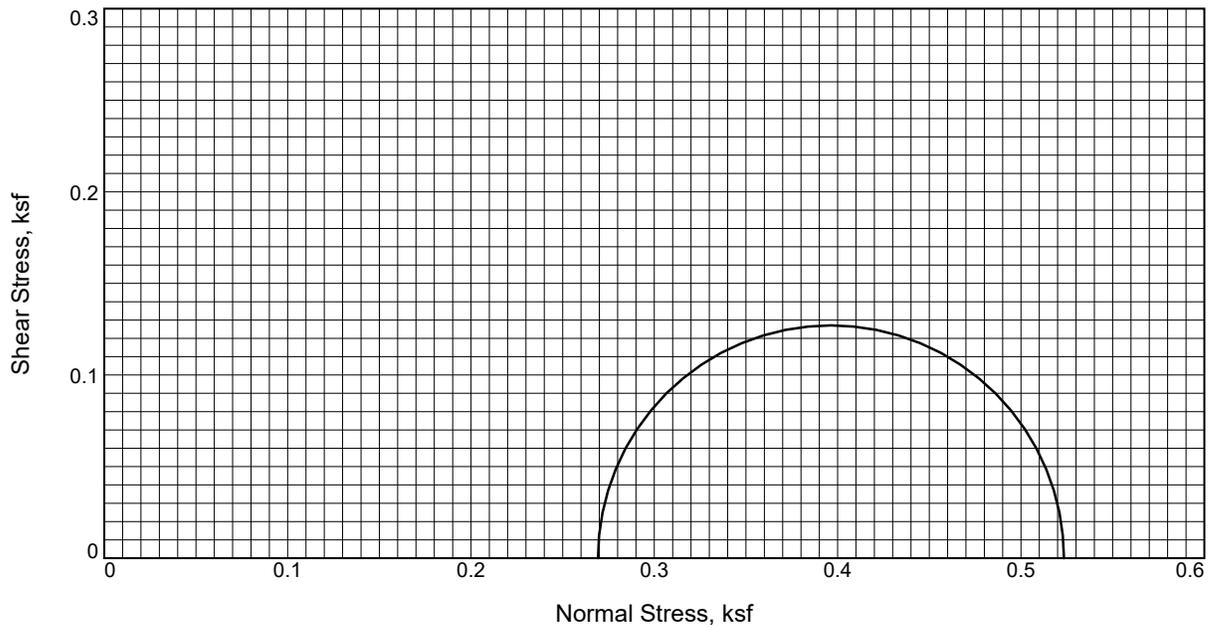
Proj. No.: L-GEI-020

Date Sampled:

TRIAXIAL SHEAR TEST REPORT
 Fourrier & de Abreu Engineers, LLC
 Baton Rouge, Louisiana

Tested By: CM

Checked By: JOF



Sample No.		1
Initial	Water Content, %	107.8
	Dry Density, pcf	46.1
	Saturation, %	110.3
	Void Ratio	2.5898
	Diameter, in.	2.75
At Test	Height, in.	5.68
	Water Content, %	110.2
	Dry Density, pcf	46.1
	Saturation, %	112.8
	Void Ratio	2.5898
Diameter, in.		2.75
Height, in.		5.68
Strain rate, in./min.		1.000
Back Pressure, psi		0.00
Cell Pressure, psi		1.87
Fail. Stress, ksf		0.25
Ult. Stress, ksf		
σ_1 Failure, ksf		0.52
σ_3 Failure, ksf		0.27

Type of Test:
Unconsolidated Undrained

Sample Type: Undisturbed

Description: Gray Fat Clay

Assumed Specific Gravity= 2.65

Remarks:

Client: GeoEngineers, Inc.

Project: S Grand Chenier Marsh Creation Baker Tract

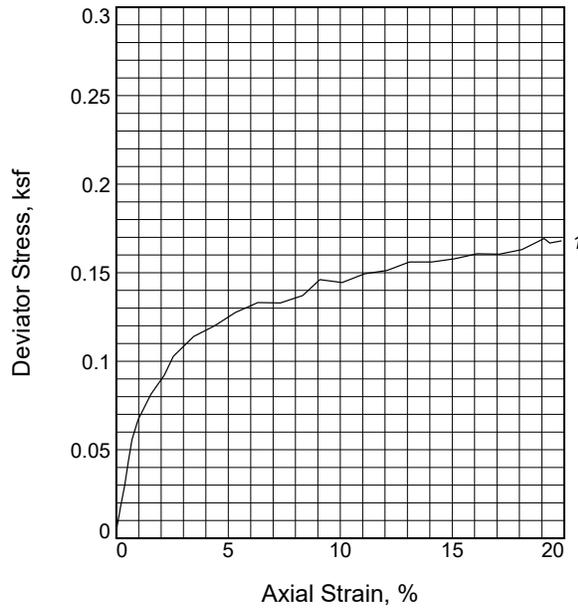
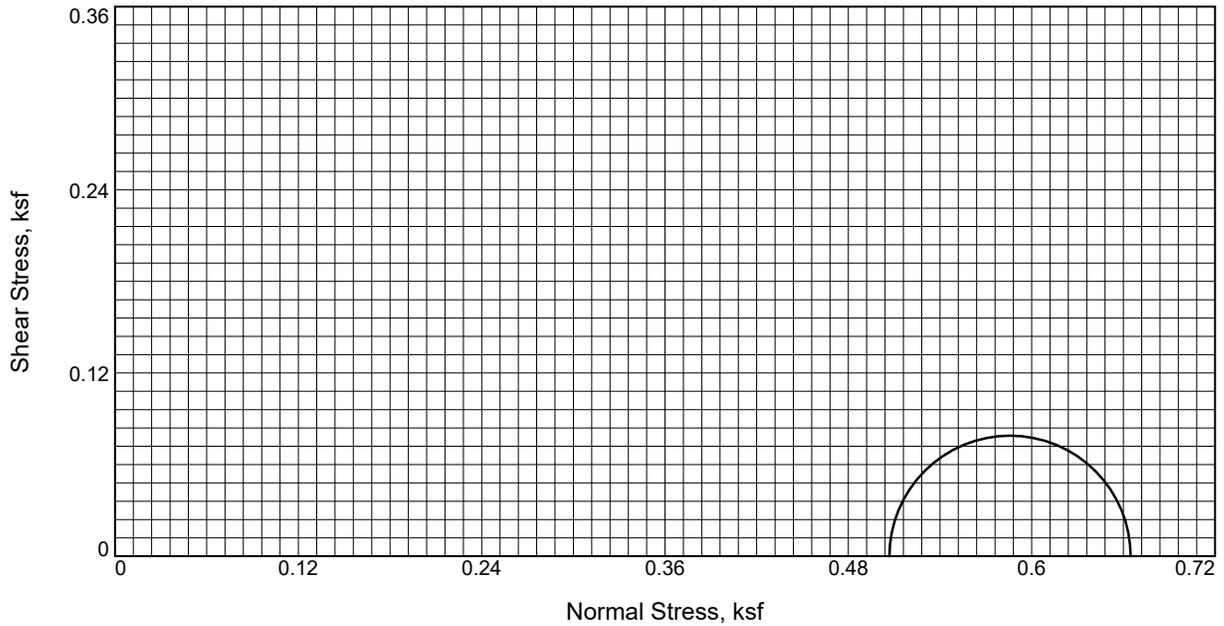
Source of Sample: B-2 **Depth:** 6-8

Sample Number: B-2

Proj. No.: L-GEI-020 **Date Sampled:**

TRIAXIAL SHEAR TEST REPORT
 Fourier & de Abreu Engineers, LLC
 Baton Rouge, Louisiana

Figure _____



Sample No.		1
Initial	Water Content, %	111.8
	Dry Density, pcf	45.9
	Saturation, %	113.8
	Void Ratio	2.6040
	Diameter, in.	2.75
At Test	Height, in.	5.64
	Water Content, %	103.5
	Dry Density, pcf	45.9
	Saturation, %	105.3
	Void Ratio	2.6040
Diameter, in.		2.75
Height, in.		5.64
Strain rate, in./min.		1.000
Back Pressure, psi		0.00
Cell Pressure, psi		3.52
Fail. Stress, ksf		0.16
Ult. Stress, ksf		
σ_1 Failure, ksf		0.66
σ_3 Failure, ksf		0.51

Type of Test:
Unconsolidated Undrained

Sample Type: Undisturbed
Description: Gray Fat Clay

Assumed Specific Gravity= 2.65

Remarks:

Figure _____

Client: GeoEngineers, Inc.

Project: S Grand Chenier Marsh Creation Baker Tract

Source of Sample: B-2 **Depth:** 12-14

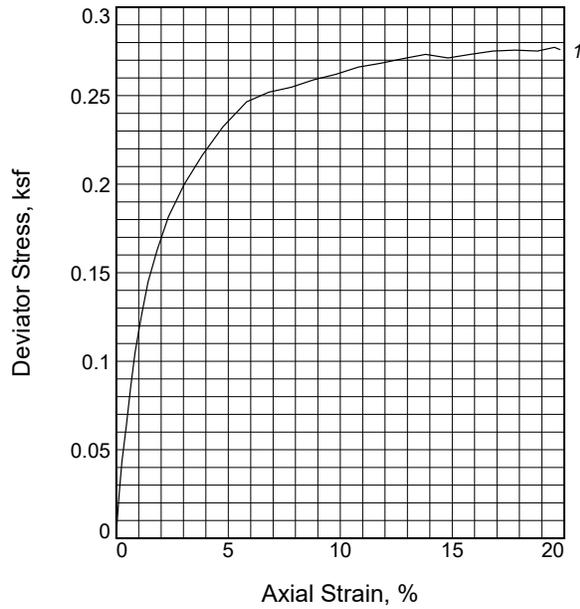
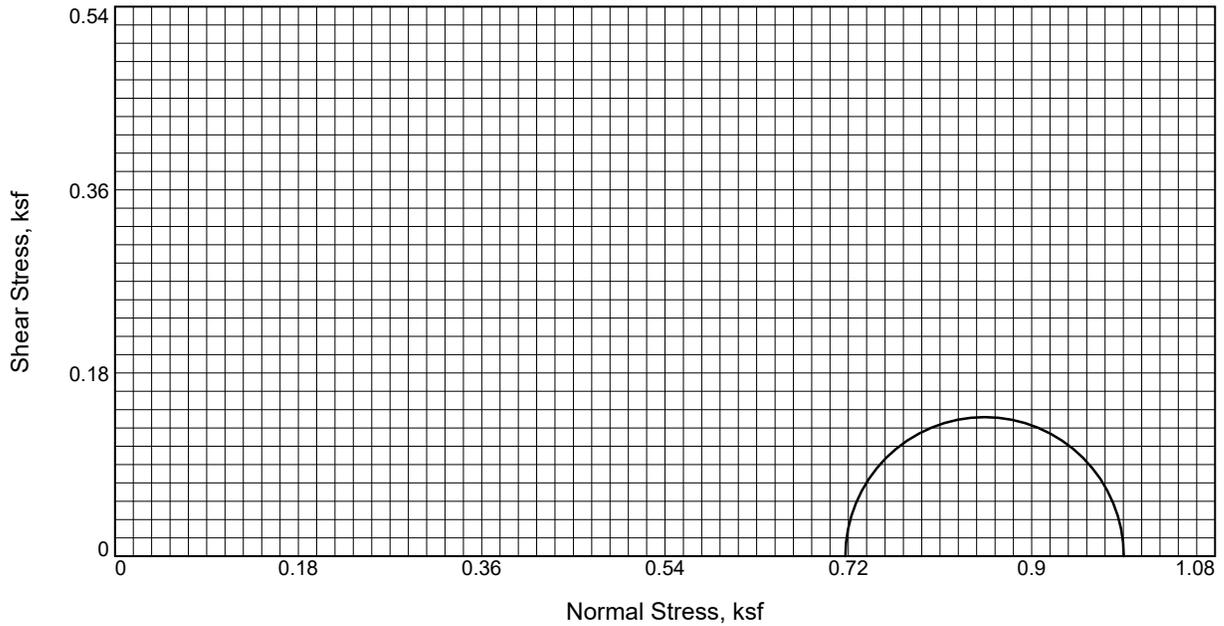
Sample Number: B-2

Proj. No.: L-GEI-020

Date Sampled:

TRIAXIAL SHEAR TEST REPORT
Fourrier & de Abreu Engineers, LLC
Baton Rouge, Louisiana

Tested By: CM **Checked By:** JOF



Sample No.		1
Initial	Water Content, %	58.0
	Dry Density, pcf	61.3
	Saturation, %	90.4
	Void Ratio	1.7003
	Diameter, in.	2.77
At Test	Height, in.	5.65
	Water Content, %	55.6
	Dry Density, pcf	61.3
	Saturation, %	86.7
	Void Ratio	1.7003
Diameter, in.		2.77
Height, in.		5.65
Strain rate, in./min.		0.999
Back Pressure, psi		0.00
Cell Pressure, psi		4.98
Fail. Stress, ksf		0.27
Ult. Stress, ksf		
σ_1 Failure, ksf		0.99
σ_3 Failure, ksf		0.72

Type of Test:

Unconsolidated Undrained

Sample Type: Undisturbed

Description: Gray Lean Clay w/ Silty Sand

Assumed Specific Gravity= 2.65

Remarks:

Figure _____

Client: GeoEngineers, Inc.

Project: S Grand Chenier Marsh Creation Baker Tract

Source of Sample: B-2 **Depth:** 18-20

Sample Number: B-2

Proj. No.: L-GEI-020

Date Sampled:

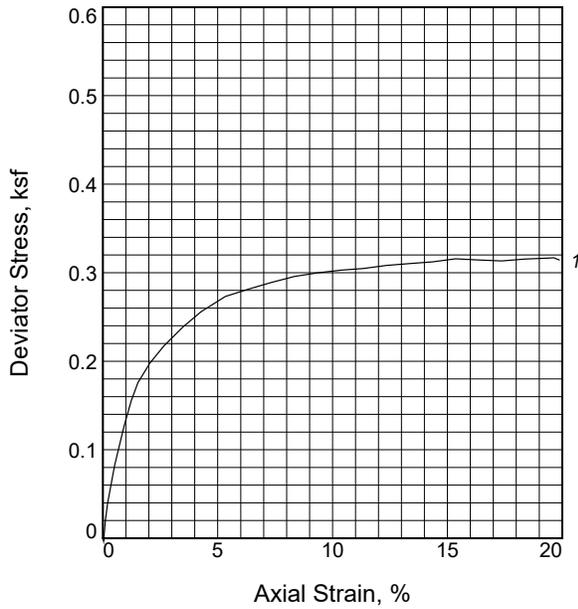
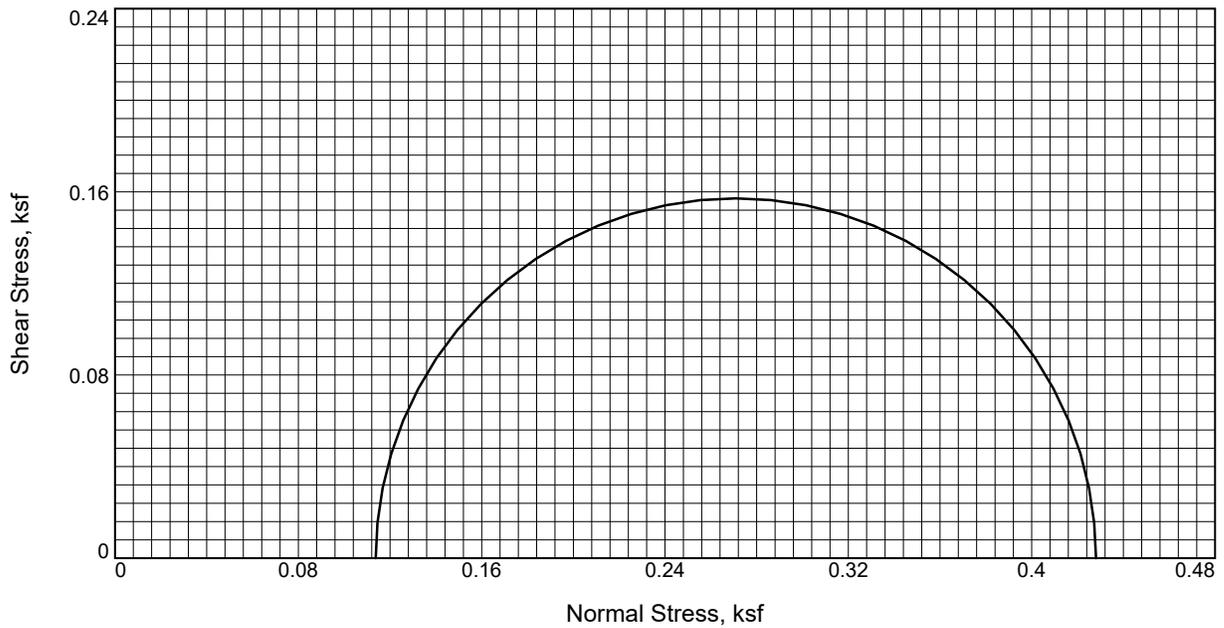
TRIAXIAL SHEAR TEST REPORT
 Fourrier & de Abreu Engineers, LLC
 Baton Rouge, Louisiana

LABORATORY TEST RESULTS

Boring No. B-3

		ASTM D2216	ASTM D2937	ASTM D2850	ASTM D4318			ASTM D2974	ASTM D2488
Date Tested	Depth (ft)	Moisture Content (%)	Dry Density (pcf)	Shear Strength (ksf)	Atterberg Limits			Organic Content (%)	Classification
					LL	PL	PI		
11/17/22	0-2							13.5	Gray Fat Clay w/ Organics (CH)
11/15/22	2-4	95.0	50.1	0.155					Gray Fat Clay (CH)
	4-6								Gray Fat Clay (CH)
11/15/22	6-8	98.1	51.1	0.095	120	33	87		Gray Fat Clay (CH)
11/15/22	8-10	110.7	46.3	0.060					Gray Fat Clay (CH)
11/15/22	10-12	108.4	46.5	0.175					Gray Fat Clay (CH)
11/15/22	14-16	115.9	46.1	0.105					Gray Fat Clay (CH)
11/15/22	23-25	24.0	102.2	2.720					Gray & Tan Fat Clay w/ Ferrous Nodules, Calcareous Nodules & Silt Seams (CH)

Notes:



Sample No.		1
Initial	Water Content, %	95.0
	Dry Density, pcf	50.1
	Saturation, %	109.5
	Void Ratio	2.2999
	Diameter, in.	2.71
	Height, in.	5.62
At Test	Water Content, %	89.9
	Dry Density, pcf	50.1
	Saturation, %	103.5
	Void Ratio	2.2999
	Diameter, in.	2.71
	Height, in.	5.62
Strain rate, in./min.		0.999
Back Pressure, psi		0.00
Cell Pressure, psi		0.79
Fail. Stress, ksf		0.31
Ult. Stress, ksf		
σ_1 Failure, ksf		0.43
σ_3 Failure, ksf		0.11

Type of Test:
Unconsolidated Undrained

Sample Type: Undisturbed

Description: Gray Fat Clay

Assumed Specific Gravity= 2.65

Remarks:

Figure _____

Client: GeoEngineers, Inc.

Project: S Grand Chenier Marsh Creation Baker Tract

Source of Sample: B-3 **Depth:** 2-4

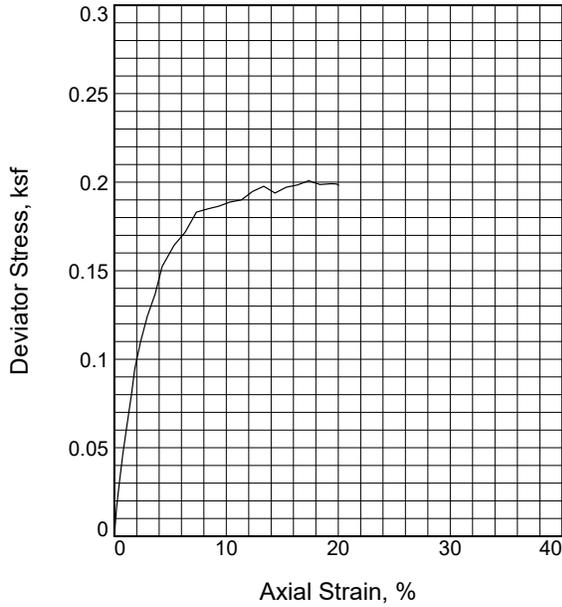
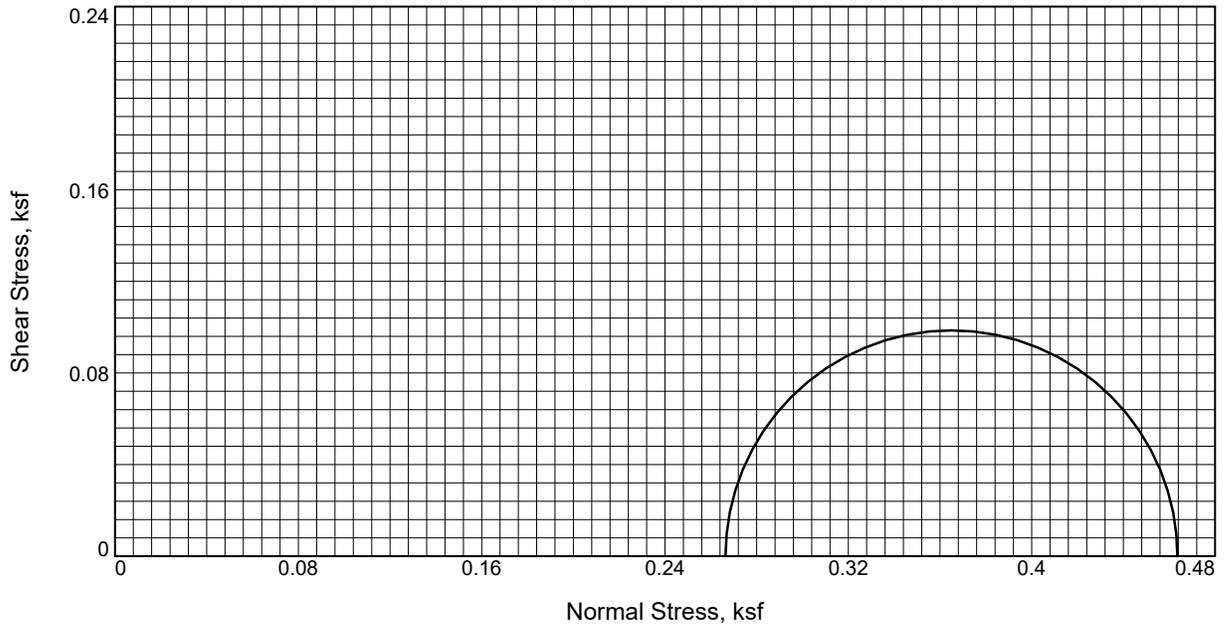
Sample Number: B-3

Proj. No.: L-GEI-020

Date Sampled:

TRIAXIAL SHEAR TEST REPORT
Fourrier & de Abreu Engineers, LLC
Baton Rouge, Louisiana

Tested By: CM _____ **Checked By:** JOF _____



Sample No.		1
Initial	Water Content, %	98.1
	Dry Density, pcf	51.1
	Saturation, %	116.1
	Void Ratio	2.2404
	Diameter, in.	2.69
At Test	Height, in.	5.58
	Water Content, %	106.1
	Dry Density, pcf	51.1
	Saturation, %	125.5
	Void Ratio	2.2404
Diameter, in.		2.69
Height, in.		5.58
Strain rate, in./min.		1.000
Back Pressure, psi		0.00
Cell Pressure, psi		1.85
Fail. Stress, ksf		0.20
Ult. Stress, ksf		
σ_1 Failure, ksf		0.46
σ_3 Failure, ksf		0.27

Type of Test:
Unconsolidated Undrained

Sample Type: Undisturbed
Description: Gray Fat Clay

Assumed Specific Gravity= 2.65

Remarks:

Figure _____

Client: GeoEngineers, Inc.

Project: S Grand Chenier Marsh Creation Baker Tract

Source of Sample: B-3 **Depth:** 6-8

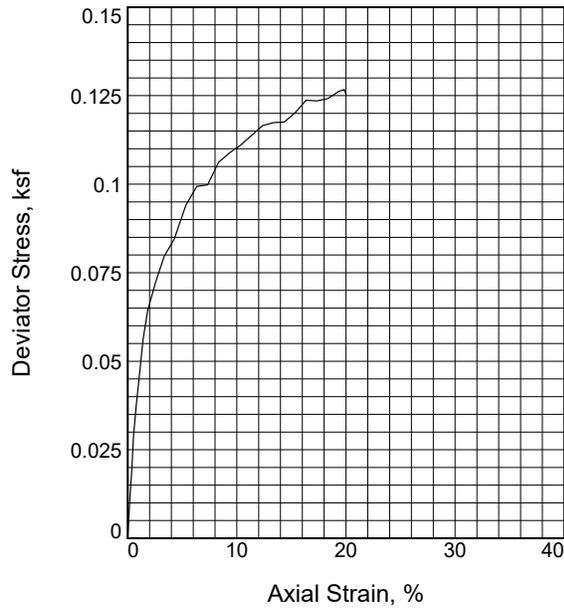
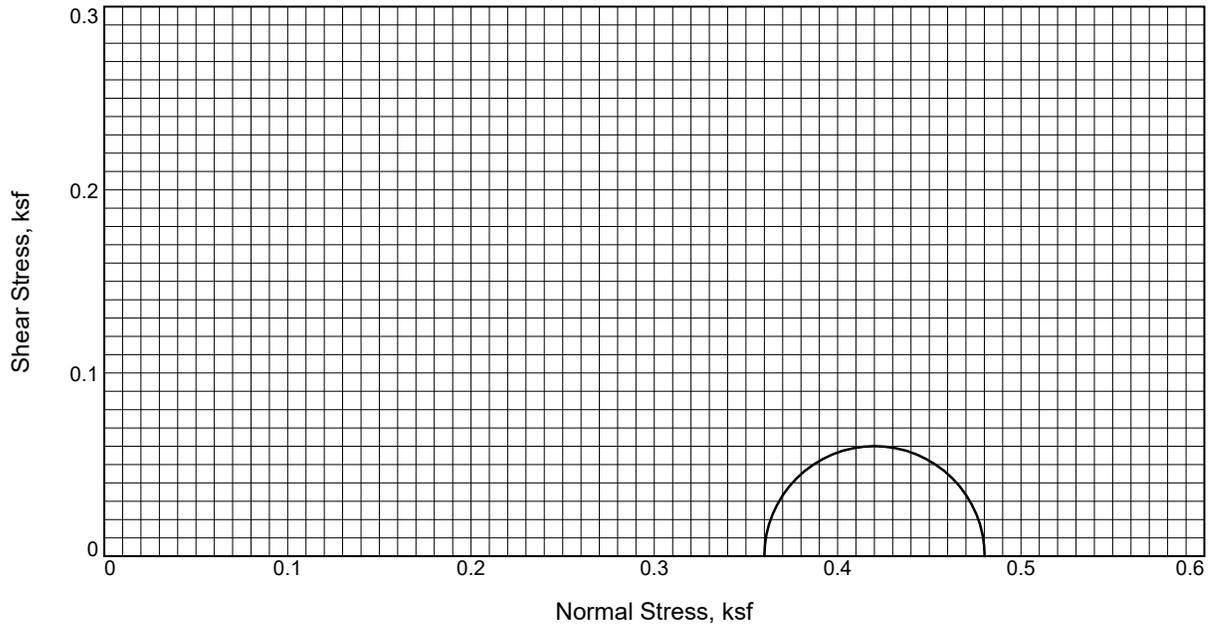
Sample Number: B-3

Proj. No.: L-GEI-020

Date Sampled:

TRIAXIAL SHEAR TEST REPORT
Fourrier & de Abreu Engineers, LLC
Baton Rouge, Louisiana

Tested By: CM **Checked By:** JOF



Sample No.		1
Initial	Water Content, %	110.7
	Dry Density, pcf	46.3
	Saturation, %	114.1
	Void Ratio	2.5705
	Diameter, in.	2.70
	Height, in.	5.61
At Test	Water Content, %	113.2
	Dry Density, pcf	46.3
	Saturation, %	116.7
	Void Ratio	2.5705
	Diameter, in.	2.70
	Height, in.	5.61
Strain rate, in./min.		0.999
Back Pressure, psi		0.00
Cell Pressure, psi		2.50
Fail. Stress, ksf		0.12
Ult. Stress, ksf		
σ_1 Failure, ksf		0.48
σ_3 Failure, ksf		0.36

Type of Test:

Unconsolidated Undrained

Sample Type: Undisturbed

Description: Gray Fat Clay

Assumed Specific Gravity= 2.65

Remarks:

Figure _____

Client: GeoEngineers, Inc.

Project: S Grand Chenier Marsh Creation Baker Tract

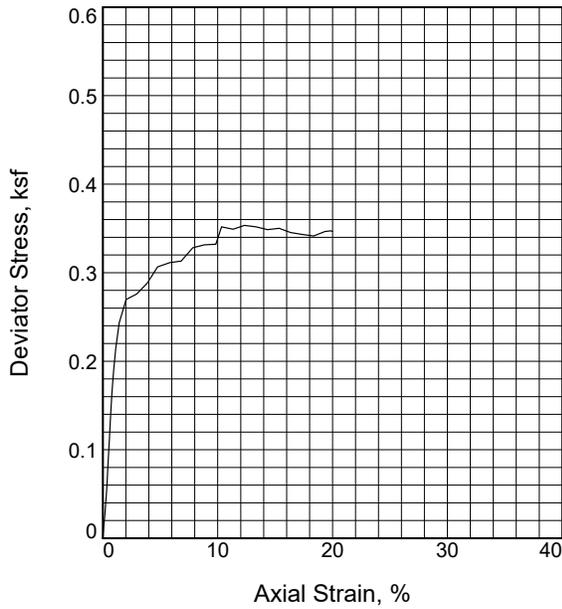
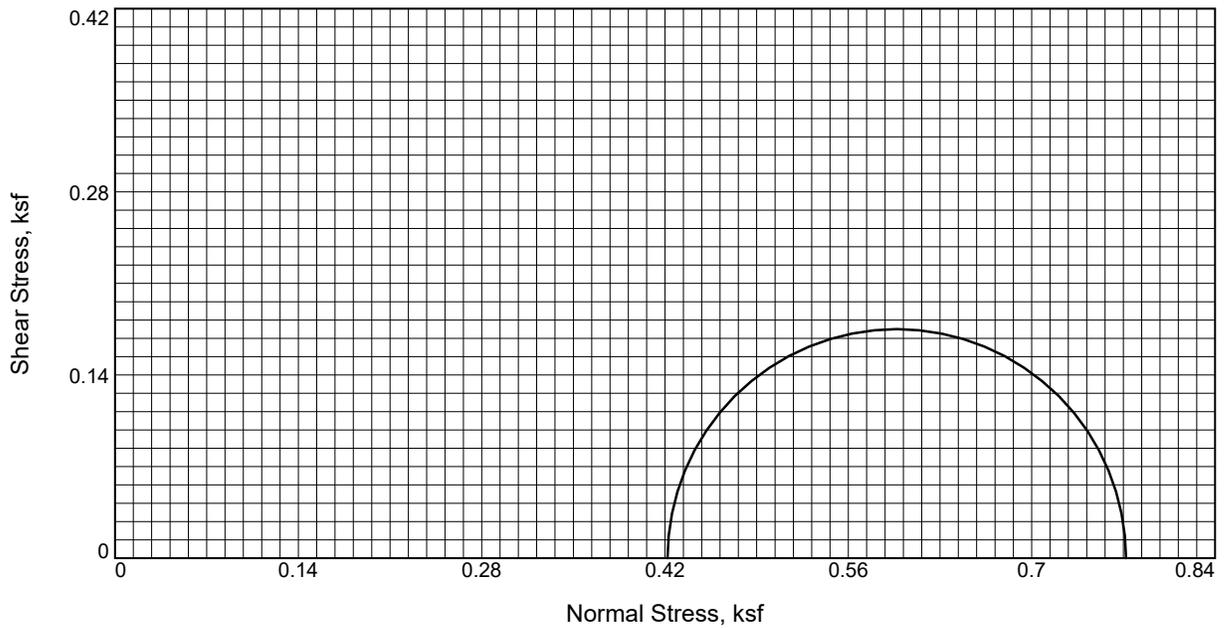
Source of Sample: B-3 **Depth:** 8-10

Sample Number: B-3

Proj. No.: L-GEI-020

Date Sampled:

TRIAXIAL SHEAR TEST REPORT
 Fourrier & de Abreu Engineers, LLC
 Baton Rouge, Louisiana



Sample No.		1
Initial	Water Content, %	108.4
	Dry Density, pcf	46.5
	Saturation, %	112.2
	Void Ratio	2.5604
	Diameter, in.	2.72
	Height, in.	5.72
At Test	Water Content, %	109.7
	Dry Density, pcf	46.5
	Saturation, %	113.6
	Void Ratio	2.5604
	Diameter, in.	2.72
	Height, in.	5.72
Strain rate, in./min.		0.999
Back Pressure, psi		0.00
Cell Pressure, psi		2.93
Fail. Stress, ksf		0.35
Ult. Stress, ksf		
σ_1 Failure, ksf		0.77
σ_3 Failure, ksf		0.42

Type of Test:
Unconsolidated Undrained

Sample Type: Undisturbed

Description: Gray Fat Clay

Assumed Specific Gravity= 2.65

Remarks:

Figure _____

Client: GeoEngineers, Inc.

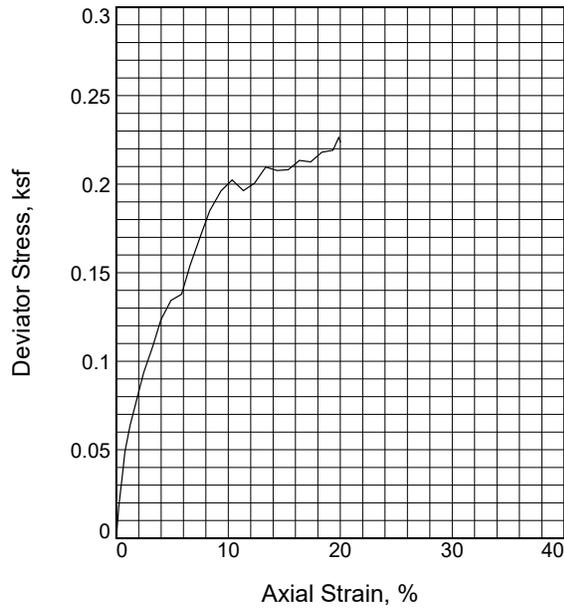
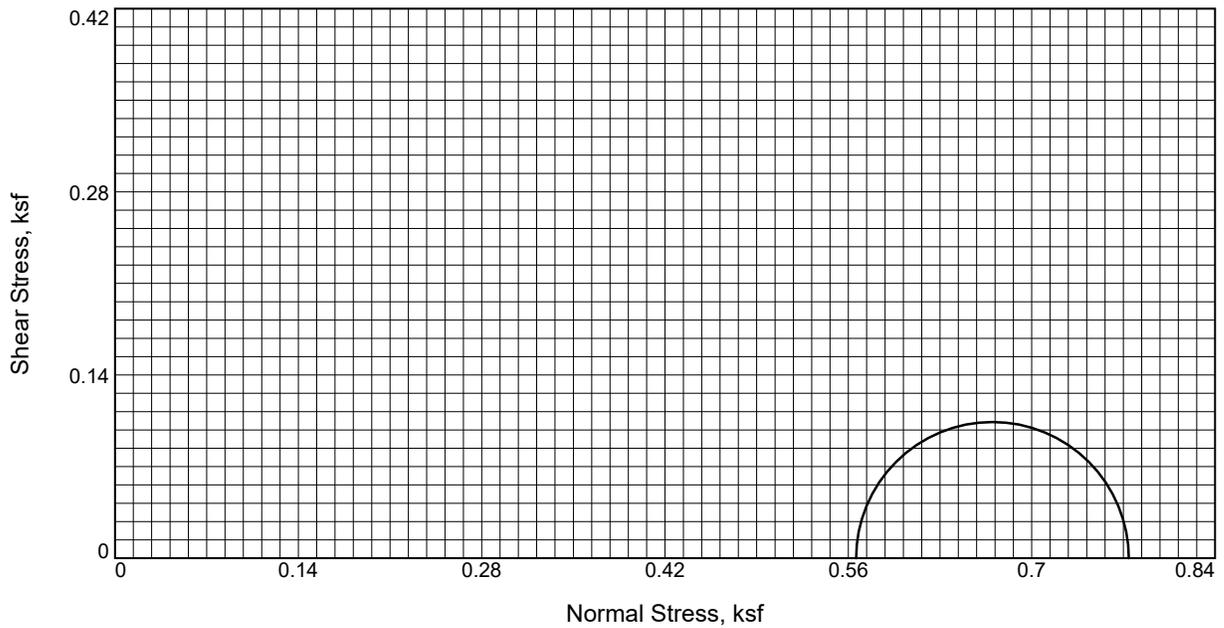
Project: S Grand Chenier Marsh Creation Baker Tract

Source of Sample: B-3 **Depth:** 10-12

Sample Number: B-3

Proj. No.: L-GEI-020 **Date Sampled:**

TRIAXIAL SHEAR TEST REPORT
 Fourrier & de Abreu Engineers, LLC
 Baton Rouge, Louisiana



Sample No.		1
Initial	Water Content, %	115.9
	Dry Density, pcf	46.1
	Saturation, %	118.6
	Void Ratio	2.5887
	Diameter, in.	2.70
At Test	Height, in.	5.61
	Water Content, %	110.4
	Dry Density, pcf	46.1
	Saturation, %	113.0
	Void Ratio	2.5887
Diameter, in.		2.70
Height, in.		5.61
Strain rate, in./min.		1.000
Back Pressure, psi		0.00
Cell Pressure, psi		3.93
Fail. Stress, ksf		0.21
Ult. Stress, ksf		
σ_1 Failure, ksf		0.77
σ_3 Failure, ksf		0.57

Type of Test:
Unconsolidated Undrained

Sample Type: Undisturbed

Description: Gray Fat Clay

Assumed Specific Gravity= 2.65

Remarks:

Figure _____

Client: GeoEngineers, Inc.

Project: S Grand Chenier Marsh Creation Baker Tract

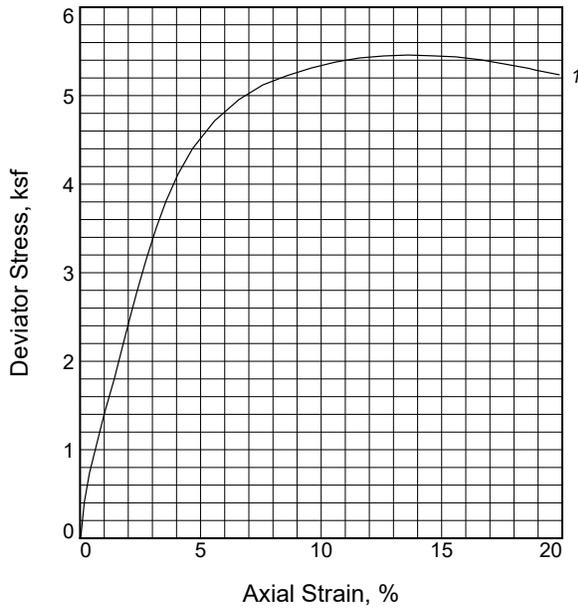
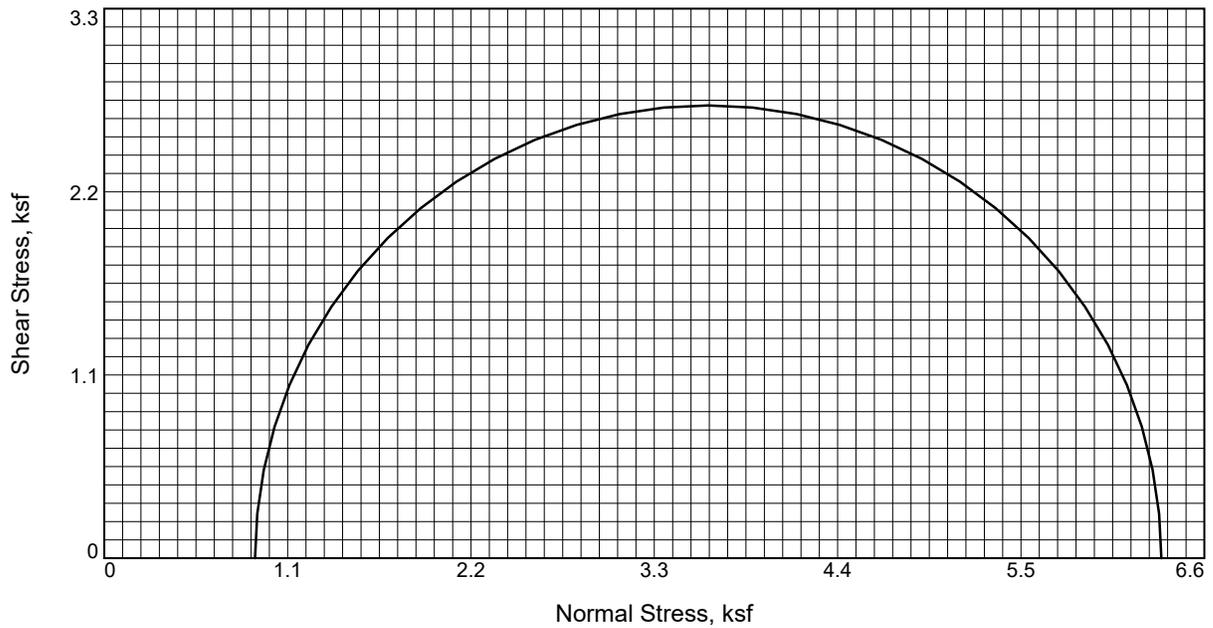
Source of Sample: B-3 **Depth:** 14-16

Sample Number: B-3

Proj. No.: L-GEI-020 **Date Sampled:**

TRIAXIAL SHEAR TEST REPORT
 Fourrier & de Abreu Engineers, LLC
 Baton Rouge, Louisiana

Tested By: CM _____ **Checked By:** JOF _____



Sample No.		1
Initial	Water Content, %	24.0
	Dry Density, pcf	102.2
	Saturation, %	102.9
	Void Ratio	0.6183
	Diameter, in.	2.88
	Height, in.	5.72
At Test	Water Content, %	19.7
	Dry Density, pcf	102.2
	Saturation, %	84.4
	Void Ratio	0.6183
	Diameter, in.	2.88
	Height, in.	5.72
Strain rate, in./min.		1.000
Back Pressure, psi		0.00
Cell Pressure, psi		6.28
Fail. Stress, ksf		5.44
Ult. Stress, ksf		
σ_1 Failure, ksf		6.34
σ_3 Failure, ksf		0.90

Type of Test:
Unconsolidated Undrained

Sample Type: Undisturbed

Description: Gray & Tan Fat Clay w/ Ferrous Nodules, Calareous Nodules & Silt Seams

Assumed Specific Gravity= 2.65

Remarks:

Client: GeoEngineers, Inc.

Project: S Grand Chenier Marsh Creation Baker Tract

Source of Sample: B-3 **Depth:** 23-25

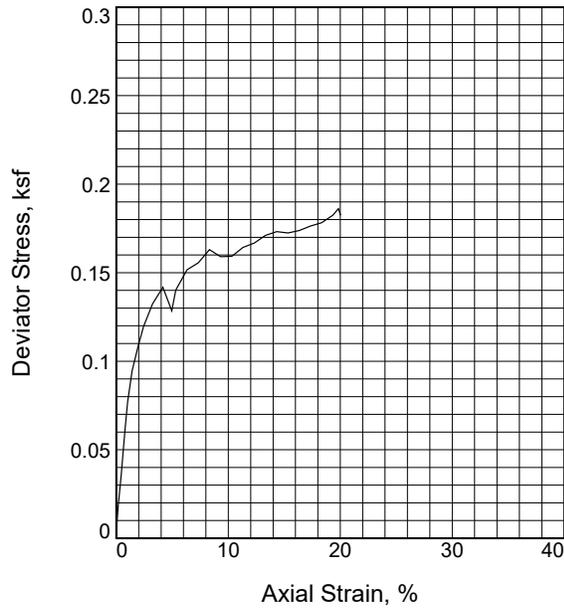
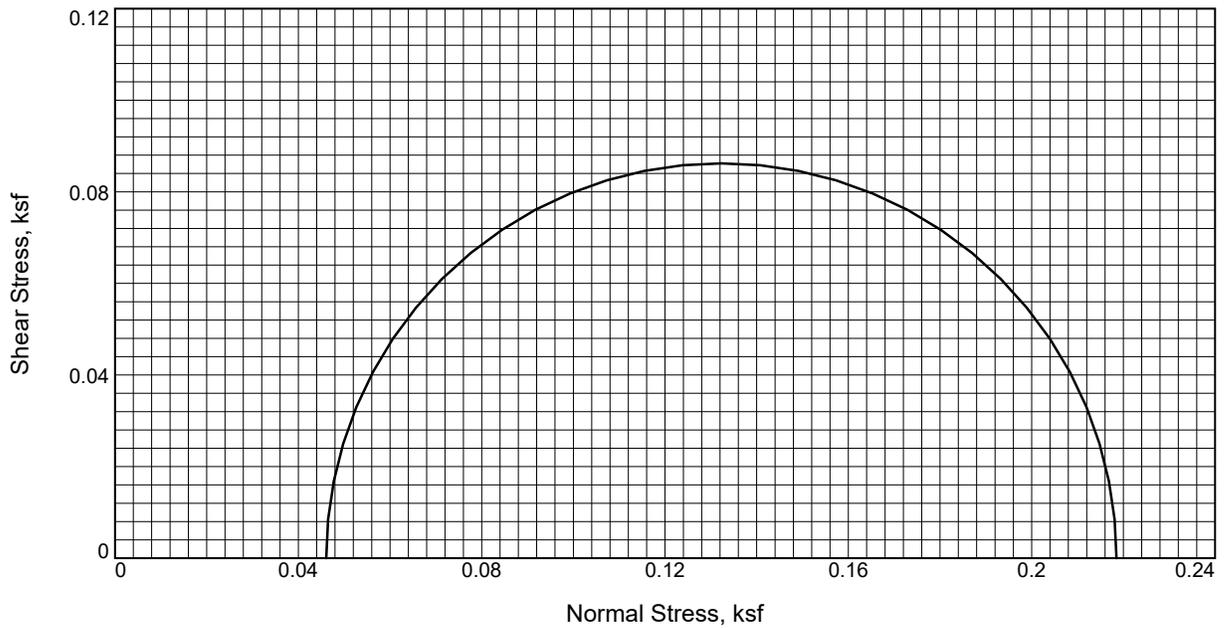
Sample Number: B-3

Proj. No.: L-GEI-020 **Date Sampled:**

TRIAXIAL SHEAR TEST REPORT
 Fourier & de Abreu Engineers, LLC
 Baton Rouge, Louisiana

Figure _____

Tested By: CM Checked By: JOF



Sample No.		1
Initial	Water Content, %	97.2
	Dry Density, pcf	47.2
	Saturation, %	102.8
	Void Ratio	2.5044
	Diameter, in.	2.77
At Test	Height, in.	5.65
	Water Content, %	52.3
	Dry Density, pcf	47.2
	Saturation, %	55.3
	Void Ratio	2.5044
Diameter, in.		2.77
Height, in.		5.65
Strain rate, in./min.		1.000
Back Pressure, psi		0.00
Cell Pressure, psi		0.32
Fail. Stress, ksf		0.17
Ult. Stress, ksf		
σ_1 Failure, ksf		0.22
σ_3 Failure, ksf		0.05

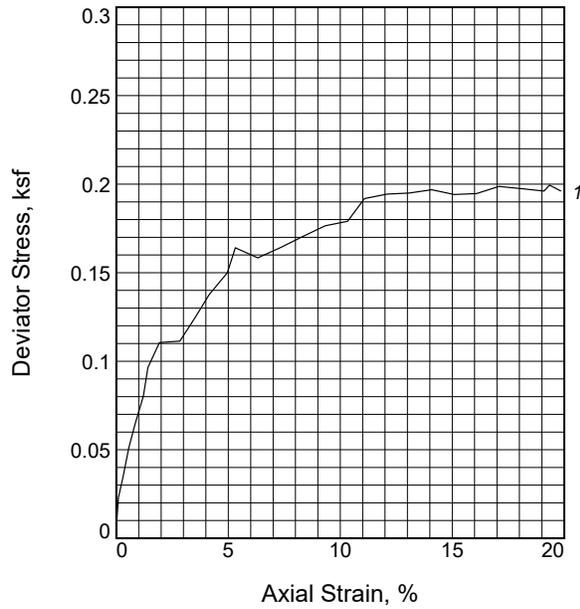
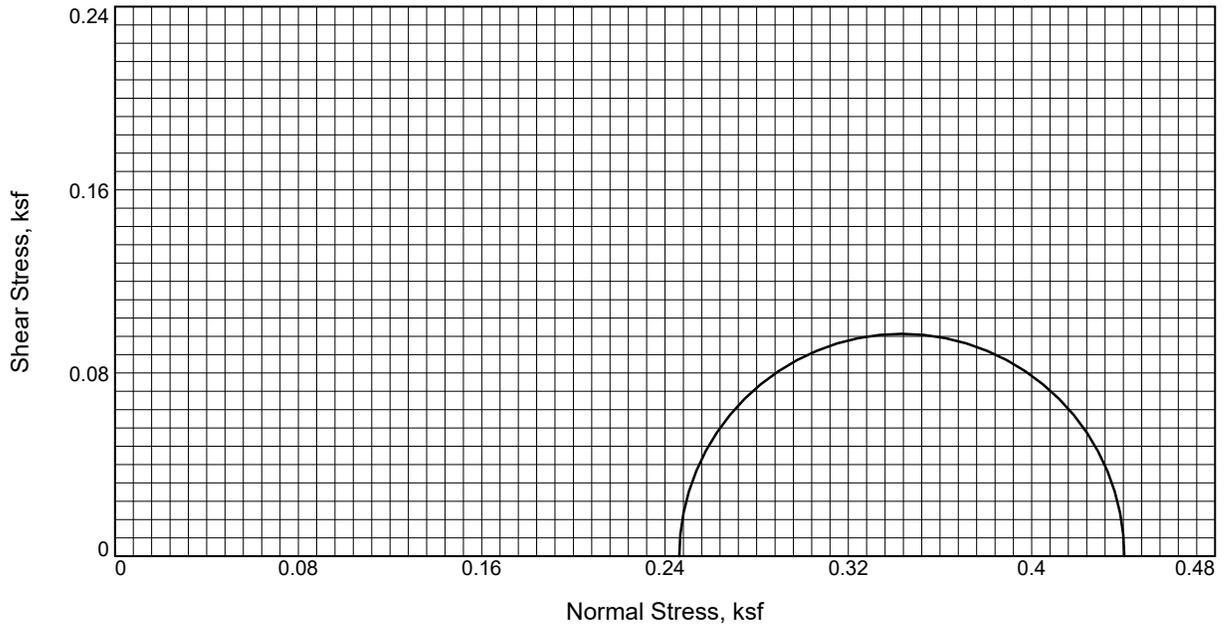
Type of Test:
Unconsolidated Undrained
Sample Type: Undisturbed
Description: Gray Fat Clay w/ Organics

Assumed Specific Gravity= 2.65
Remarks:

Client: GeoEngineers, Inc.
Project: S Grand Chenier Marsh Creation Baker Tract
Source of Sample: B-4 **Depth:** 0-2
Sample Number: B-4
Proj. No.: L-GEI-020 **Date Sampled:**

TRIAXIAL SHEAR TEST REPORT
Fourrier & de Abreu Engineers, LLC
Baton Rouge, Louisiana

Figure _____



Sample No.		1
Initial	Water Content, %	115.9
	Dry Density, pcf	44.8
	Saturation, %	114.0
	Void Ratio	2.6946
	Diameter, in.	2.68
At Test	Height, in.	5.54
	Water Content, %	119.6
	Dry Density, pcf	44.8
	Saturation, %	117.6
	Void Ratio	2.6946
Diameter, in.		2.68
Height, in.		5.54
Strain rate, in./min.		1.000
Back Pressure, psi		0.00
Cell Pressure, psi		1.71
Fail. Stress, ksf		0.19
Ult. Stress, ksf		
σ_1 Failure, ksf		0.44
σ_3 Failure, ksf		0.25

Type of Test:
Unconsolidated Undrained

Sample Type: Undisturbed
Description: Gray Fat Clay

Assumed Specific Gravity= 2.65

Remarks:

Figure _____

Client: GeoEngineers, Inc.

Project: S Grand Chenier Marsh Creation Baker Tract

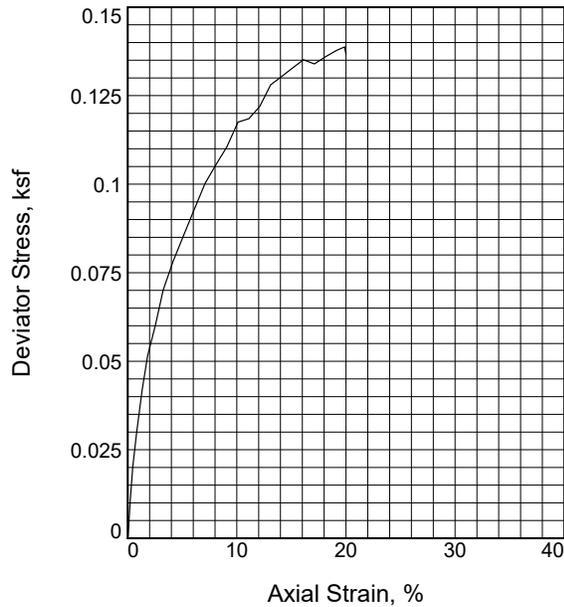
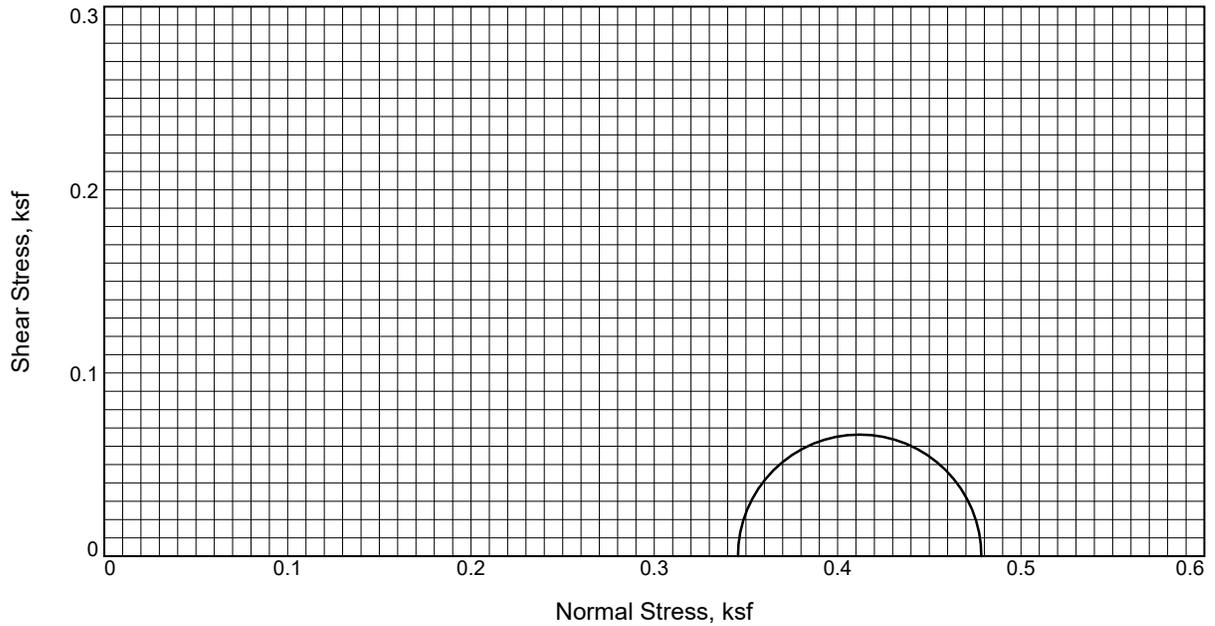
Source of Sample: B-4 **Depth:** 6-8

Sample Number: B-4

Proj. No.: L-GEI-020

Date Sampled:

TRIAXIAL SHEAR TEST REPORT
Fourrier & de Abreu Engineers, LLC
Baton Rouge, Louisiana



Sample No.		1
Initial	Water Content, %	123.2
	Dry Density, pcf	40.7
	Saturation, %	106.5
	Void Ratio	3.0658
	Diameter, in.	2.79
At Test	Height, in.	5.75
	Water Content, %	117.7
	Dry Density, pcf	40.7
	Saturation, %	101.7
	Void Ratio	3.0658
Diameter, in.		2.79
Height, in.		5.75
Strain rate, in./min.		1.000
Back Pressure, psi		0.00
Cell Pressure, psi		2.40
Fail. Stress, ksf		0.13
Ult. Stress, ksf		
σ_1 Failure, ksf		0.48
σ_3 Failure, ksf		0.35

Type of Test:
Unconsolidated Undrained

Sample Type: Undisturbed
Description: Gray Fat Clay

Assumed Specific Gravity= 2.65

Remarks:

Client: GeoEngineers, Inc.

Project: S Grand Chenier Marsh Creation Baker Tract

Source of Sample: B-4 **Depth:** 8-10

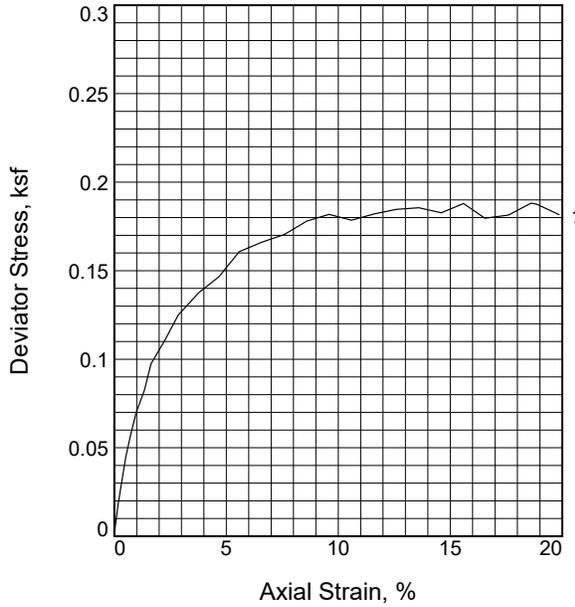
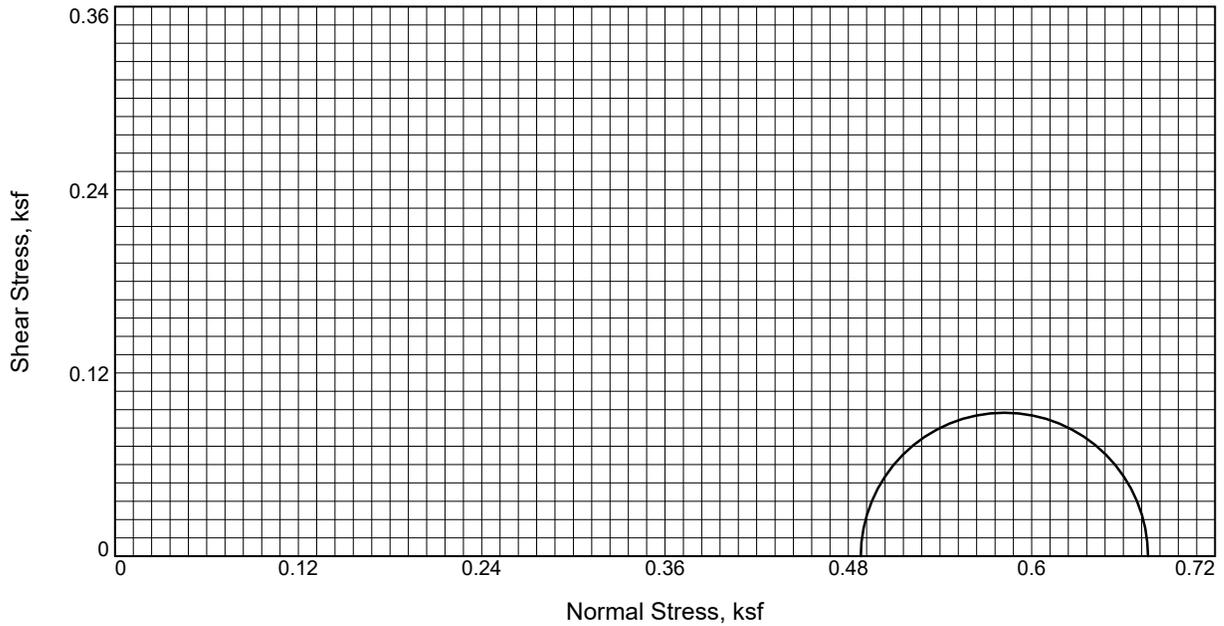
Sample Number: B-4

Proj. No.: L-GEI-020

Date Sampled:

TRIAXIAL SHEAR TEST REPORT
 Fourier & de Abreu Engineers, LLC
 Baton Rouge, Louisiana

Figure _____



Sample No.		1
Initial	Water Content, %	117.0
	Dry Density, pcf	43.5
	Saturation, %	110.5
	Void Ratio	2.8070
	Diameter, in.	2.80
At Test	Height, in.	5.72
	Water Content, %	114.4
	Dry Density, pcf	43.5
	Saturation, %	108.0
	Void Ratio	2.8070
Diameter, in.		2.80
Height, in.		5.72
Strain rate, in./min.		1.000
Back Pressure, psi		0.00
Cell Pressure, psi		3.39
Fail. Stress, ksf		0.19
Ult. Stress, ksf		
σ_1 Failure, ksf		0.68
σ_3 Failure, ksf		0.49

Type of Test:

Unconsolidated Undrained

Sample Type: Undisturbed

Description: Gray Fat Clay

Assumed Specific Gravity= 2.65

Remarks:

Figure _____

Client: GeoEngineers, Inc.

Project: S Grand Chenier Marsh Creation Baker Tract

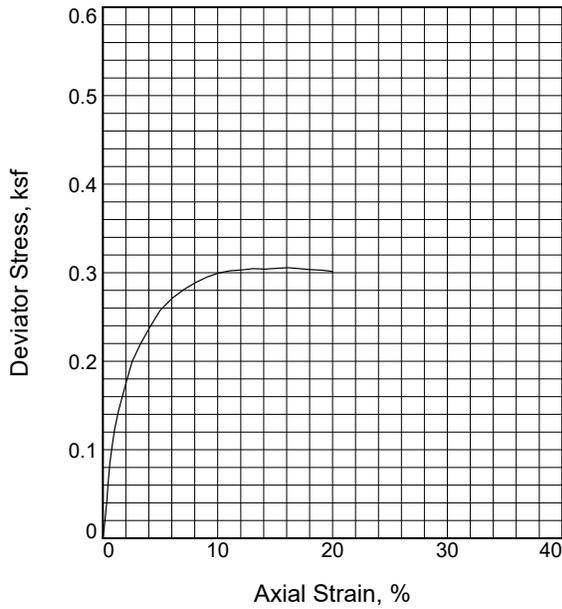
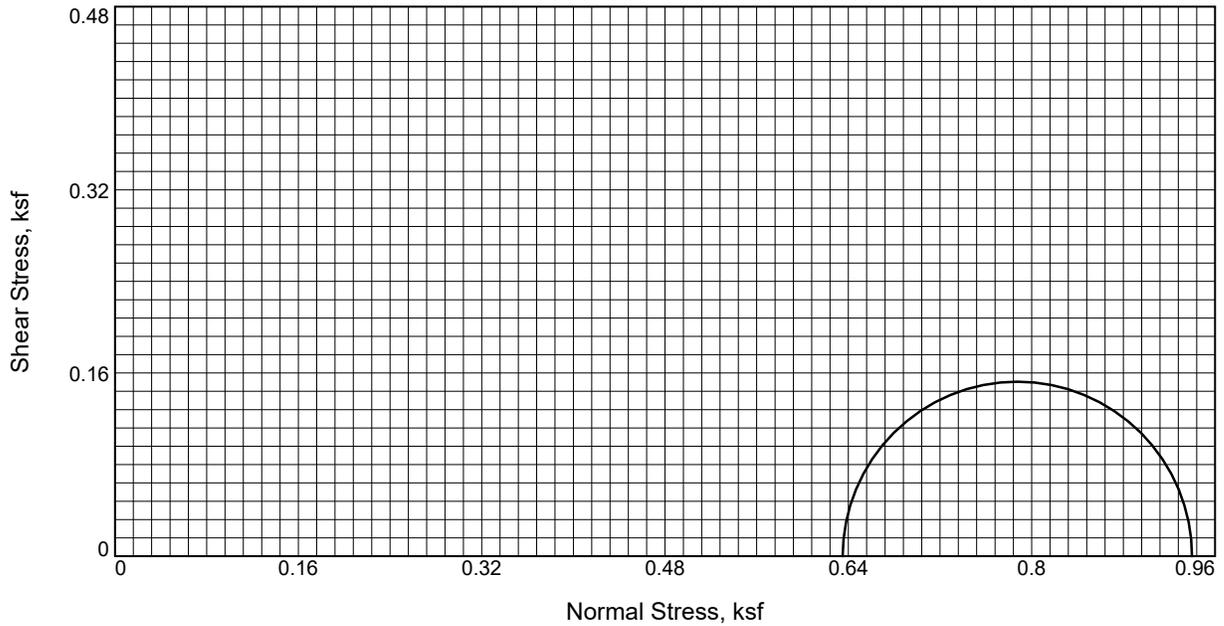
Source of Sample: B-4 **Depth:** 12-14

Sample Number: B-4

Proj. No.: L-GEI-020

Date Sampled:

TRIAXIAL SHEAR TEST REPORT
 Fourrier & de Abreu Engineers, LLC
 Baton Rouge, Louisiana



Sample No.		1
Initial	Water Content, %	95.4
	Dry Density, pcf	47.9
	Saturation, %	103.0
	Void Ratio	2.4524
	Diameter, in.	2.80
	Height, in.	5.73
At Test	Water Content, %	99.3
	Dry Density, pcf	47.9
	Saturation, %	107.3
	Void Ratio	2.4524
	Diameter, in.	2.80
	Height, in.	5.73
Strain rate, in./min.		1.000
Back Pressure, psi		0.00
Cell Pressure, psi		4.41
Fail. Stress, ksf		0.30
Ult. Stress, ksf		
σ_1 Failure, ksf		0.94
σ_3 Failure, ksf		0.64

Type of Test:

Unconsolidated Undrained

Sample Type: Undisturbed

Description: Gray Fat Clay w/ Shells

Assumed Specific Gravity= 2.65

Remarks:

Figure _____

Client: GeoEngineers, Inc.

Project: S Grand Chenier Marsh Creation Baker Tract

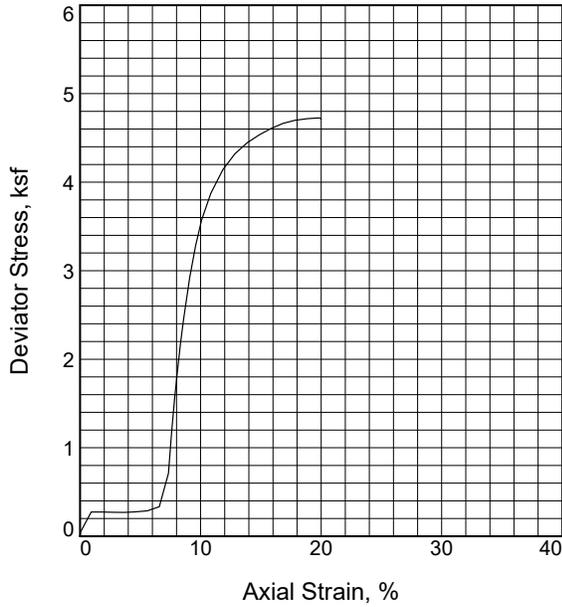
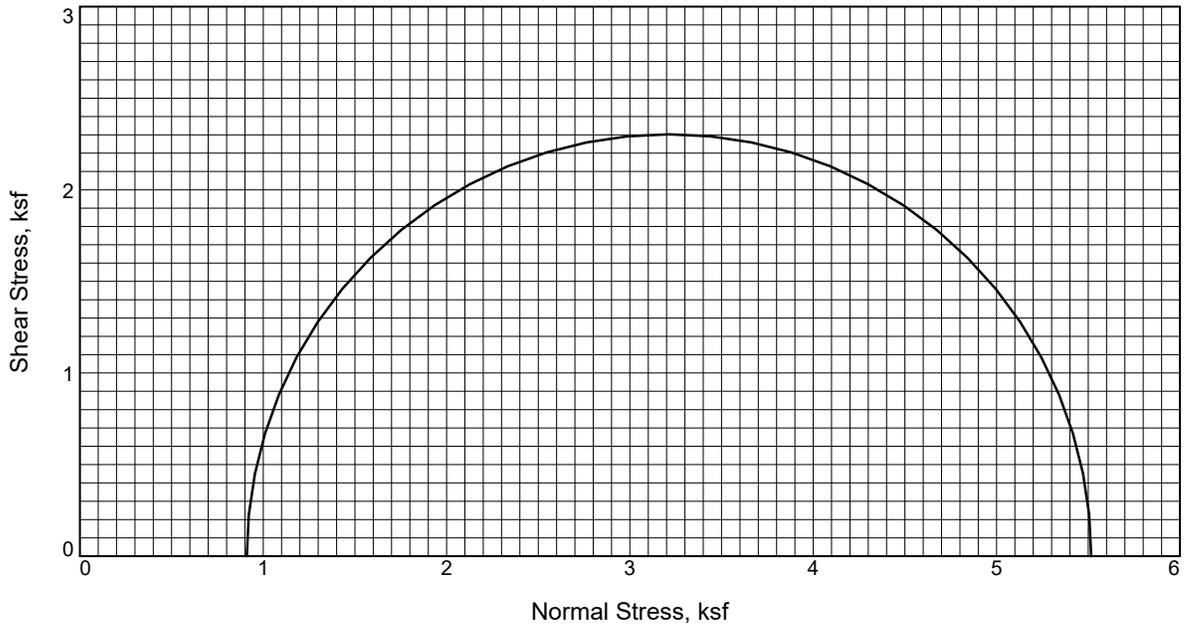
Source of Sample: B-4 **Depth:** 16-18

Sample Number: B-4

Proj. No.: L-GEI-020

Date Sampled:

TRIAXIAL SHEAR TEST REPORT
 Fourrier & de Abreu Engineers, LLC
 Baton Rouge, Louisiana



Sample No.		1
Initial	Water Content, %	20.1
	Dry Density, pcf	108.1
	Saturation, %	100.3
	Void Ratio	0.5305
	Diameter, in.	2.84
	Height, in.	5.75
At Test	Water Content, %	20.8
	Dry Density, pcf	108.1
	Saturation, %	104.0
	Void Ratio	0.5305
	Diameter, in.	2.84
	Height, in.	5.75
Strain rate, in./min.		1.000
Back Pressure, psi		0.00
Cell Pressure, psi		6.32
Fail. Stress, ksf		4.61
Ult. Stress, ksf		
σ_1 Failure, ksf		5.52
σ_3 Failure, ksf		0.91

Type of Test:

Unconsolidated Undrained

Sample Type: Undisturbed

Description: Gray & Tan Lean Clay w/ Silt & Ferrous Nodules

Assumed Specific Gravity= 2.65

Remarks:

Figure _____

Client: GeoEngineers, Inc.

Project: S Grand Chenier Marsh Creation Baker Tract

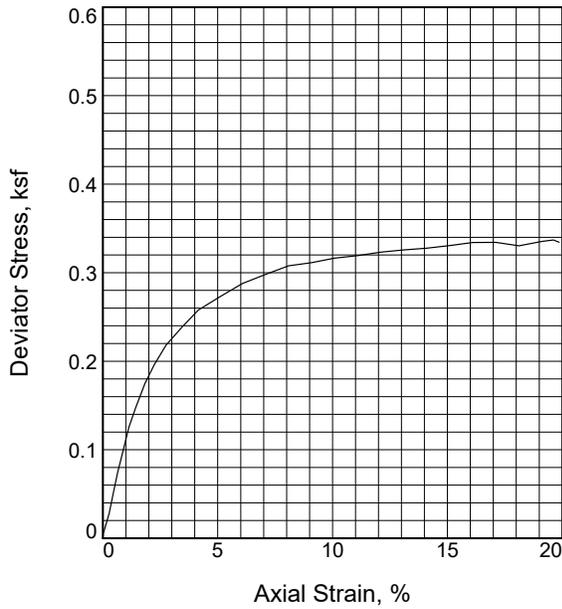
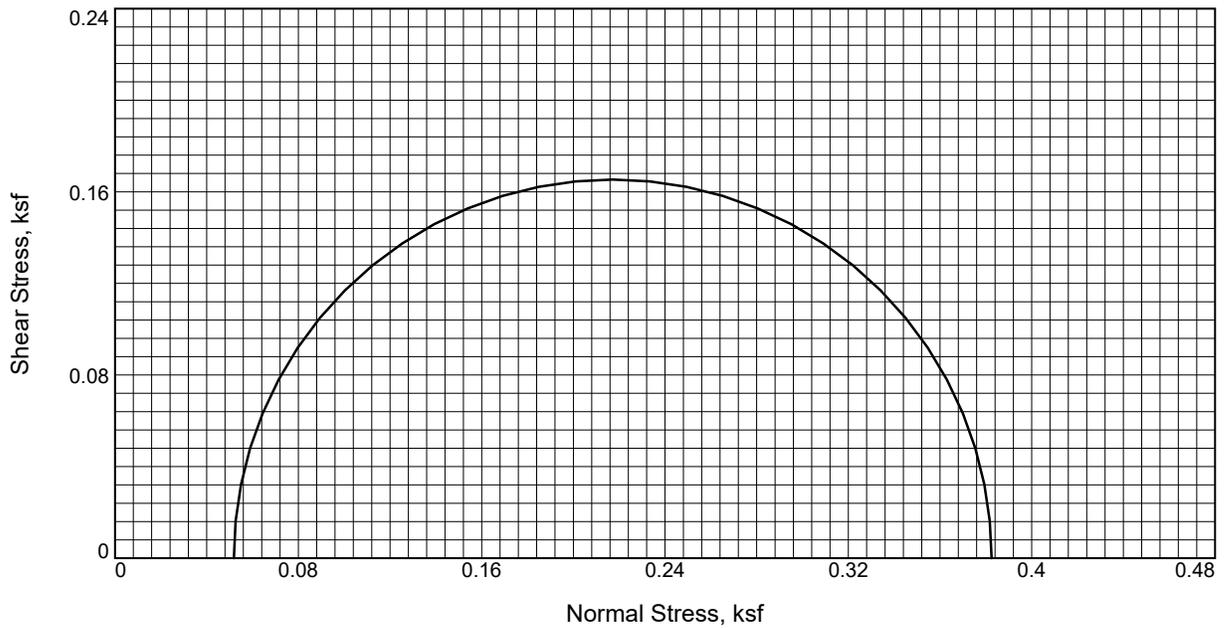
Source of Sample: B-4 **Depth:** 23-25

Sample Number: B-4

Proj. No.: L-GEI-020

Date Sampled:

TRIAXIAL SHEAR TEST REPORT
 Fourier & de Abreu Engineers, LLC
 Baton Rouge, Louisiana



Sample No.		1
Initial	Water Content, %	140.3
	Dry Density, pcf	34.8
	Saturation, %	99.0
	Void Ratio	3.7551
	Diameter, in.	2.80
	Height, in.	5.69
At Test	Water Content, %	154.8
	Dry Density, pcf	34.8
	Saturation, %	109.2
	Void Ratio	3.7551
	Diameter, in.	2.80
	Height, in.	5.69
Strain rate, in./min.		1.000
Back Pressure, psi		0.00
Cell Pressure, psi		0.36
Fail. Stress, ksf		0.33
Ult. Stress, ksf		
σ_1 Failure, ksf		0.38
σ_3 Failure, ksf		0.05

Type of Test:
Unconsolidated Undrained
Sample Type: Undisturbed
Description: Dark Gray Fat Clay w/ Organics

Assumed Specific Gravity= 2.65
Remarks:

Figure _____

Client: GeoEngineers, Inc.

Project: S Grand Chenier Marsh Creation Baker Tract

Source of Sample: B-5 **Depth:** 0-2

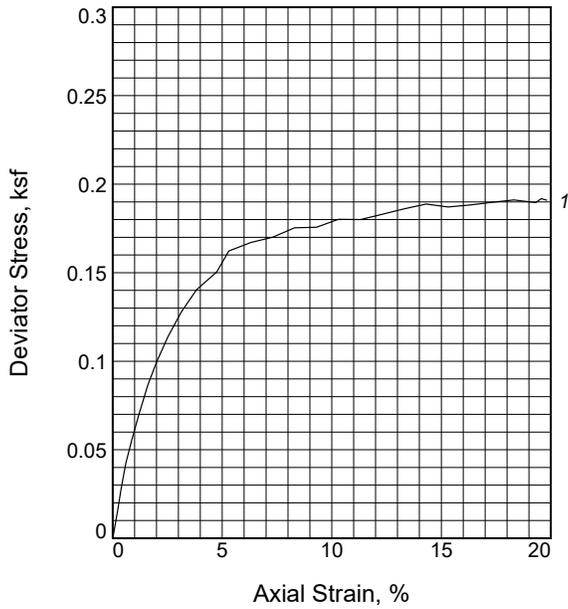
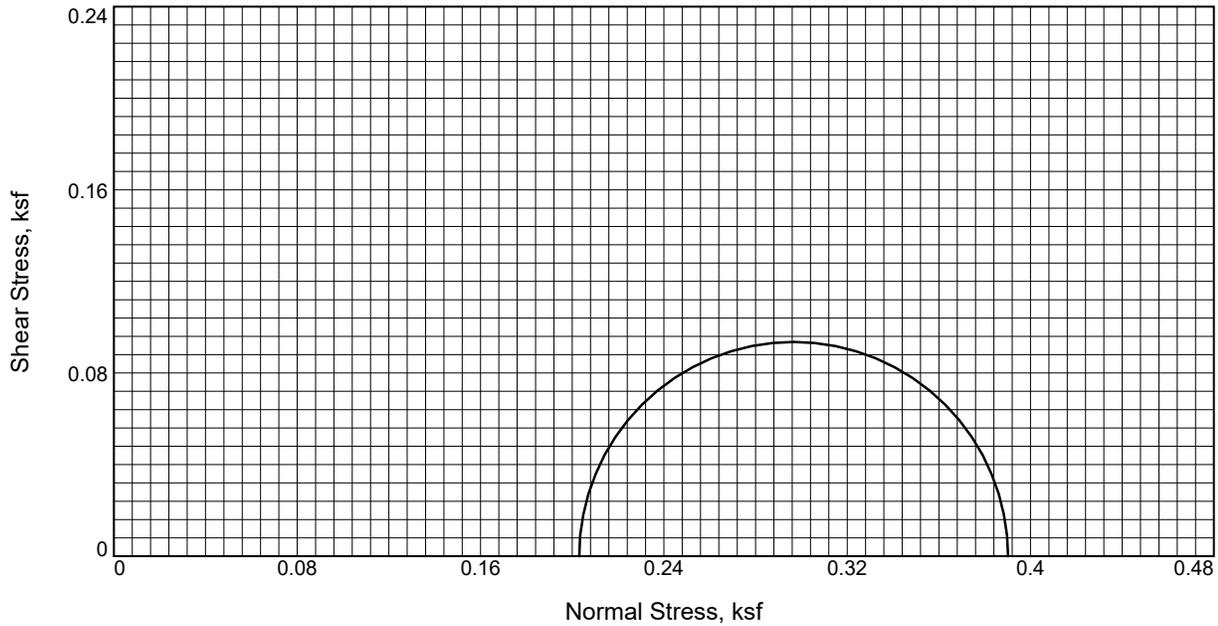
Sample Number: B-5

Proj. No.: L-GEI-020

Date Sampled:

TRIAXIAL SHEAR TEST REPORT
 Fourrier & de Abreu Engineers, LLC
 Baton Rouge, Louisiana

Tested By: CM _____ **Checked By:** JOF _____



Sample No.	1	
Initial	Water Content, %	96.1
	Dry Density, pcf	44.1
	Saturation, %	92.4
	Void Ratio	2.7550
	Diameter, in.	2.75
At Test	Height, in.	5.71
	Water Content, %	95.0
	Dry Density, pcf	44.1
	Saturation, %	91.4
	Void Ratio	2.7550
Strain rate, in./min.	0.999	
Back Pressure, psi	0.00	
Cell Pressure, psi	1.41	
Fail. Stress, ksf	0.19	
Ult. Stress, ksf		
σ_1 Failure, ksf	0.39	
σ_3 Failure, ksf	0.20	

Type of Test:

Unconsolidated Undrained

Sample Type: Undisturbed

Description: Gray Fat Clay

LL= 124

PL= 36

PI= 88

Assumed Specific Gravity= 2.65

Remarks:

Figure _____

Client: GeoEngineers, Inc.

Project: S Grand Chenier Marsh Creation Baker Tract

Source of Sample: B-5

Depth: 4-6

Sample Number: B-5

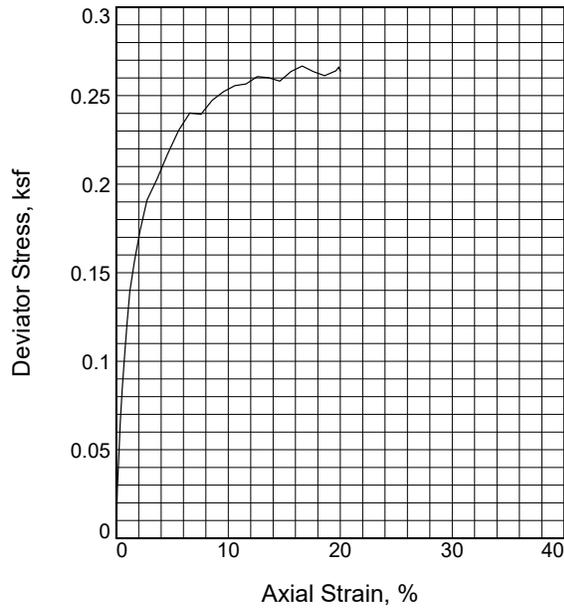
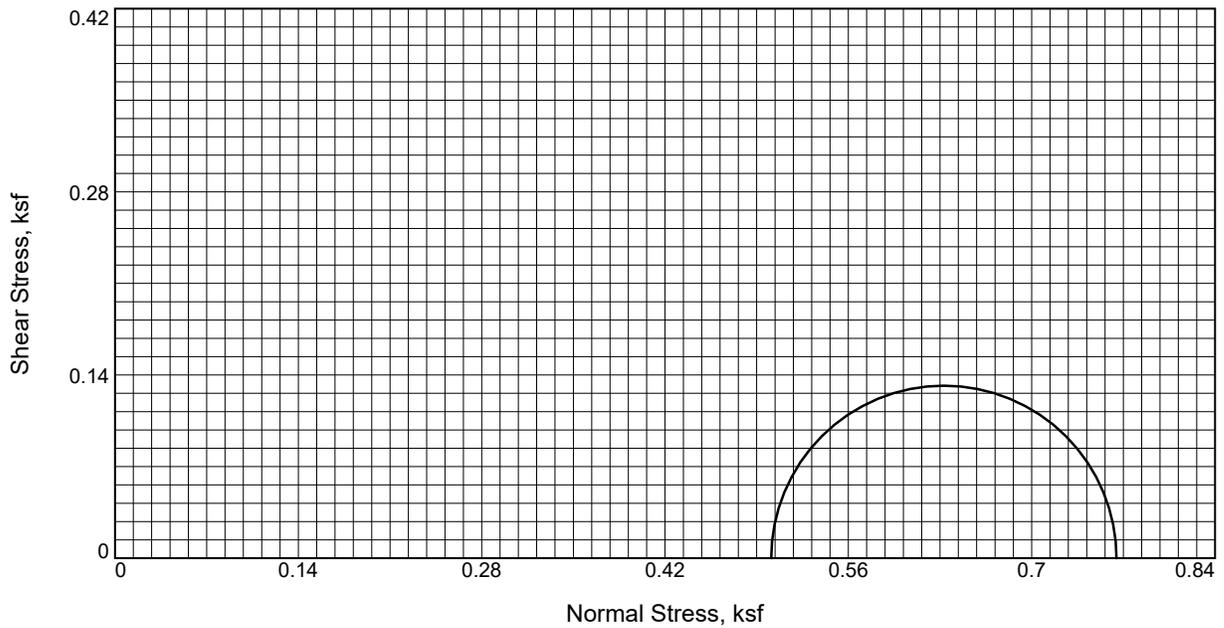
Proj. No.: L-GEI-020

Date Sampled:

TRIAXIAL SHEAR TEST REPORT
 Fourrier & de Abreu Engineers, LLC
 Baton Rouge, Louisiana

Tested By: CM

Checked By: JOF



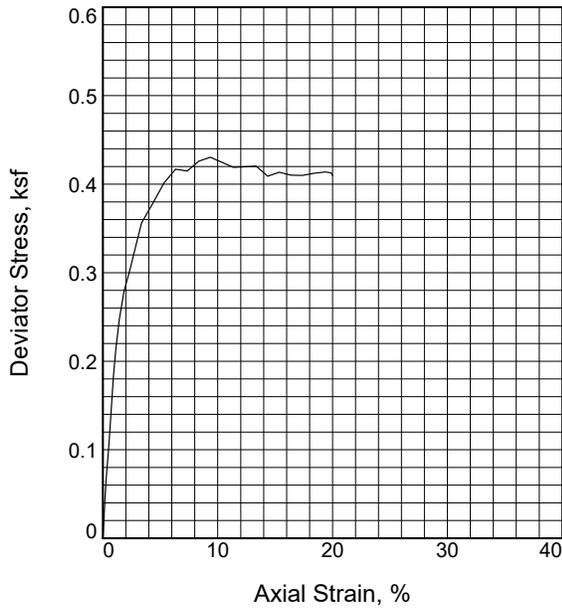
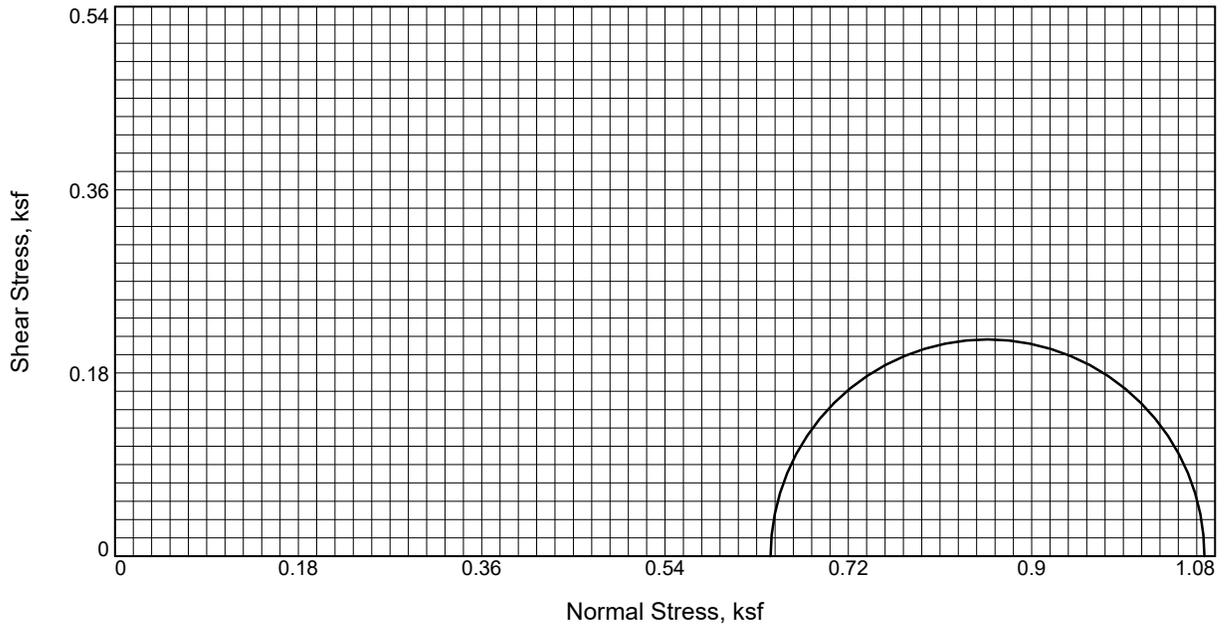
Sample No.		1
Initial	Water Content, %	107.7
	Dry Density, pcf	39.0
	Saturation, %	88.0
	Void Ratio	3.2437
	Diameter, in.	2.78
	Height, in.	5.69
At Test	Water Content, %	100.1
	Dry Density, pcf	39.0
	Saturation, %	81.8
	Void Ratio	3.2437
	Diameter, in.	2.78
	Height, in.	5.69
Strain rate, in./min.		0.999
Back Pressure, psi		0.00
Cell Pressure, psi		3.48
Fail. Stress, ksf		0.26
Ult. Stress, ksf		
σ_1 Failure, ksf		0.76
σ_3 Failure, ksf		0.50

Type of Test:
Unconsolidated Undrained
Sample Type: Undisturbed
Description: Gray Fat Clay

Assumed Specific Gravity= 2.65
Remarks:

Client: GeoEngineers, Inc.
Project: S Grand Chenier Marsh Creation Baker Tract
Source of Sample: B-5 **Depth:** 12-14
Sample Number: B-5
Proj. No.: L-GEI-020 **Date Sampled:**
 TRIAXIAL SHEAR TEST REPORT
 Fourrier & de Abreu Engineers, LLC
 Baton Rouge, Louisiana

Figure _____



Sample No.		1
Initial	Water Content, %	99.5
	Dry Density, pcf	43.0
	Saturation, %	92.6
	Void Ratio	2.8467
	Diameter, in.	2.79
	Height, in.	5.73
At Test	Water Content, %	86.0
	Dry Density, pcf	43.0
	Saturation, %	80.0
	Void Ratio	2.8467
	Diameter, in.	2.79
	Height, in.	5.73
Strain rate, in./min.		1.000
Back Pressure, psi		0.00
Cell Pressure, psi		4.47
Fail. Stress, ksf		0.43
Ult. Stress, ksf		
σ_1 Failure, ksf		1.07
σ_3 Failure, ksf		0.64

Type of Test:
Unconsolidated Undrained

Sample Type: Undisturbed

Description: Gray Fat Clay

Assumed Specific Gravity= 2.65

Remarks:

Figure _____

Client: GeoEngineers, Inc.

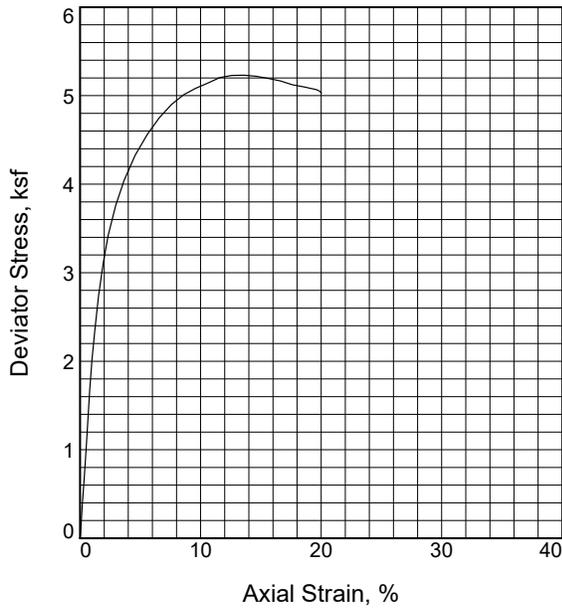
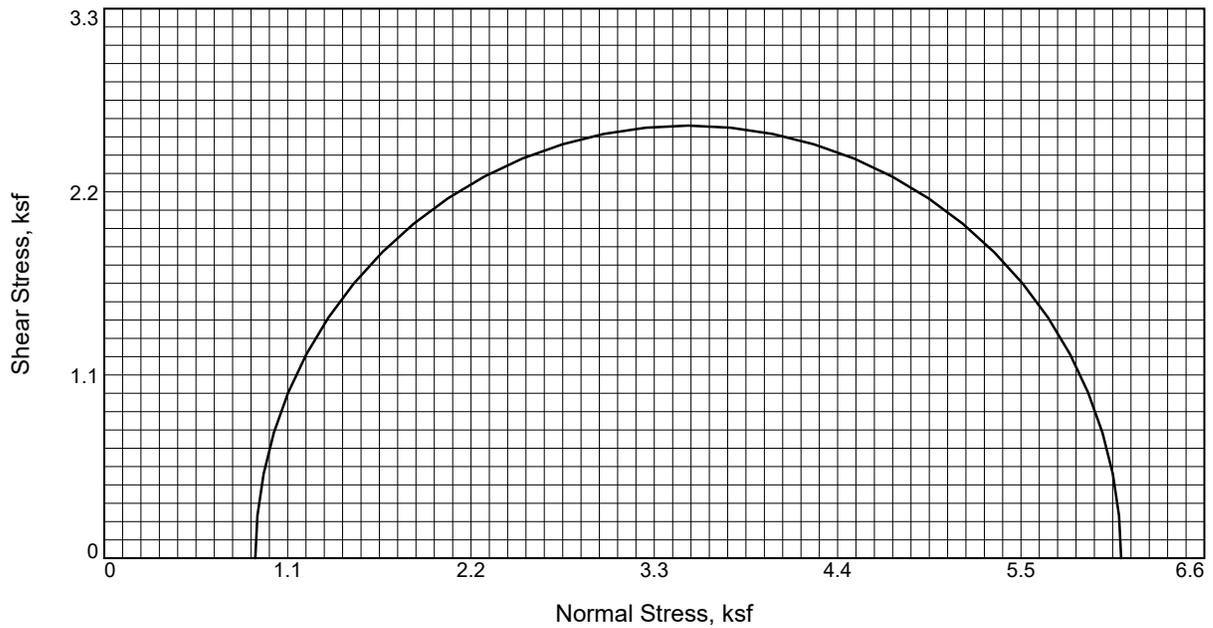
Project: S Grand Chenier Marsh Creation Baker Tract

Source of Sample: B-5 **Depth:** 16-18

Sample Number: B-5

Proj. No.: L-GEI-020 **Date Sampled:**

TRIAXIAL SHEAR TEST REPORT
 Fourrier & de Abreu Engineers, LLC
 Baton Rouge, Louisiana



Sample No.		1
Initial	Water Content, %	22.4
	Dry Density, pcf	107.9
	Saturation, %	111.1
	Void Ratio	0.5339
	Diameter, in.	2.83
	Height, in.	5.74
At Test	Water Content, %	22.2
	Dry Density, pcf	107.9
	Saturation, %	110.3
	Void Ratio	0.5339
	Diameter, in.	2.83
	Height, in.	5.74
Strain rate, in./min.		0.999
Back Pressure, psi		0.00
Cell Pressure, psi		6.29
Fail. Stress, ksf		5.20
Ult. Stress, ksf		
σ_1 Failure, ksf		6.10
σ_3 Failure, ksf		0.91

Type of Test:
Unconsolidated Undrained
Sample Type: Undisturbed
Description: Gray & Tan Fat Clay

Assumed Specific Gravity= 2.65
Remarks:

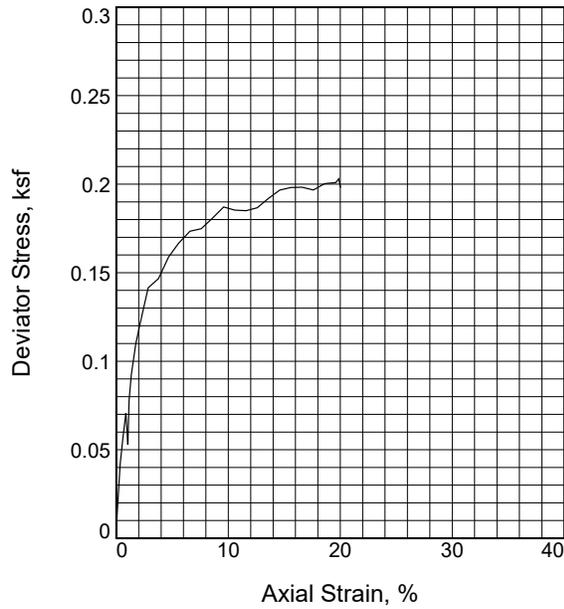
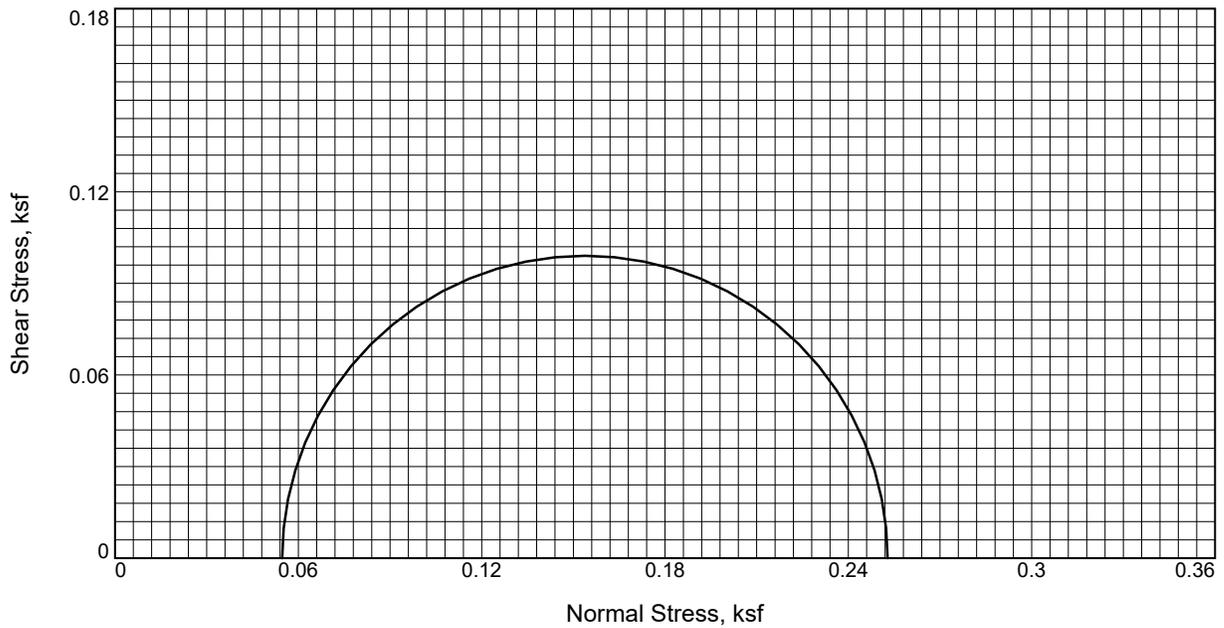
Client: GeoEngineers, Inc.
Project: S Grand Chenier Marsh Creation Baker Tract

Source of Sample: B-5 **Depth:** 23-25
Sample Number: B-5
Proj. No.: L-GEI-020 **Date Sampled:**

TRIAXIAL SHEAR TEST REPORT
Fourrier & de Abreu Engineers, LLC
Baton Rouge, Louisiana

Figure _____

Tested By: CM Checked By: JOF



Sample No.		1
Initial	Water Content, %	108.0
	Dry Density, pcf	45.0
	Saturation, %	106.8
	Void Ratio	2.6795
	Diameter, in.	2.72
At Test	Height, in.	5.70
	Water Content, %	103.8
	Dry Density, pcf	45.0
	Saturation, %	102.7
	Void Ratio	2.6795
Diameter, in.		2.72
Height, in.		5.70
Strain rate, in./min.		0.999
Back Pressure, psi		0.00
Cell Pressure, psi		0.38
Fail. Stress, ksf		0.20
Ult. Stress, ksf		
σ_1 Failure, ksf		0.25
σ_3 Failure, ksf		0.05

Type of Test:
Unconsolidated Undrained

Sample Type: Undisturbed

Description: Gray Fat Clay w/ Roots

Assumed Specific Gravity= 2.65

Remarks:

Client: GeoEngineers, Inc.

Project: S Grand Chenier Marsh Creation Baker Tract

Source of Sample: B-6 **Depth:** 0-2

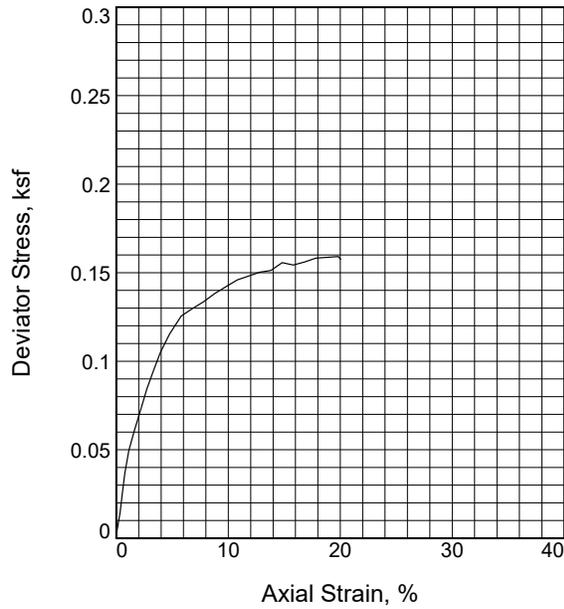
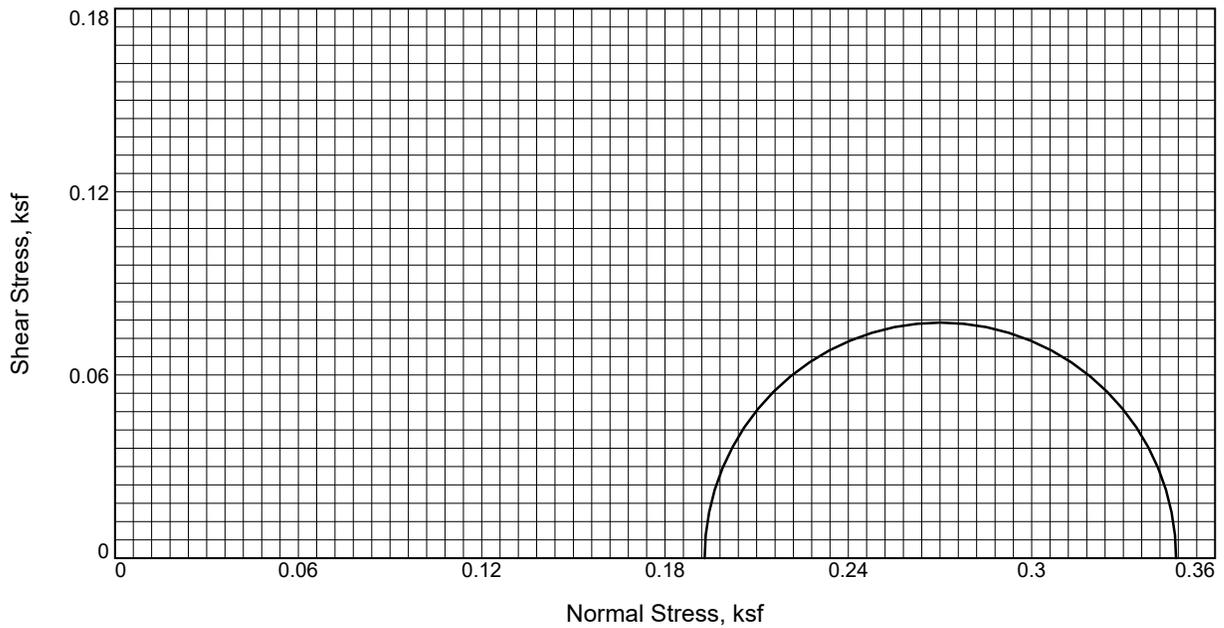
Sample Number: B-6

Proj. No.: L-GEI-020 **Date Sampled:**

TRIAXIAL SHEAR TEST REPORT
 Fourrier & de Abreu Engineers, LLC
 Baton Rouge, Louisiana

Figure _____

Tested By: CM _____ **Checked By:** JOF _____



Sample No.		1
Initial	Water Content, %	114.0
	Dry Density, pcf	42.2
	Saturation, %	103.3
	Void Ratio	2.9237
	Diameter, in.	2.72
At Test	Height, in.	5.69
	Water Content, %	103.1
	Dry Density, pcf	42.2
	Saturation, %	93.4
	Void Ratio	2.9237
Diameter, in.		2.72
Height, in.		5.69
Strain rate, in./min.		0.999
Back Pressure, psi		0.00
Cell Pressure, psi		1.34
Fail. Stress, ksf		0.15
Ult. Stress, ksf		
σ_1 Failure, ksf		0.35
σ_3 Failure, ksf		0.19

Type of Test:

Unconsolidated Undrained

Sample Type: Undisturbed

Description: Gray Fat Clay with Organics

Assumed Specific Gravity= 2.65

Remarks:

Figure _____

Client: GeoEngineers, Inc.

Project: S Grand Chenier Marsh Creation Baker Tract

Source of Sample: B-6 **Depth:** 4-6

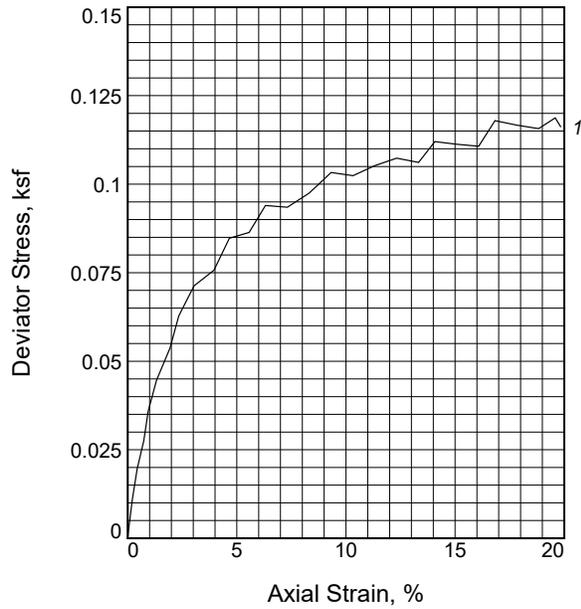
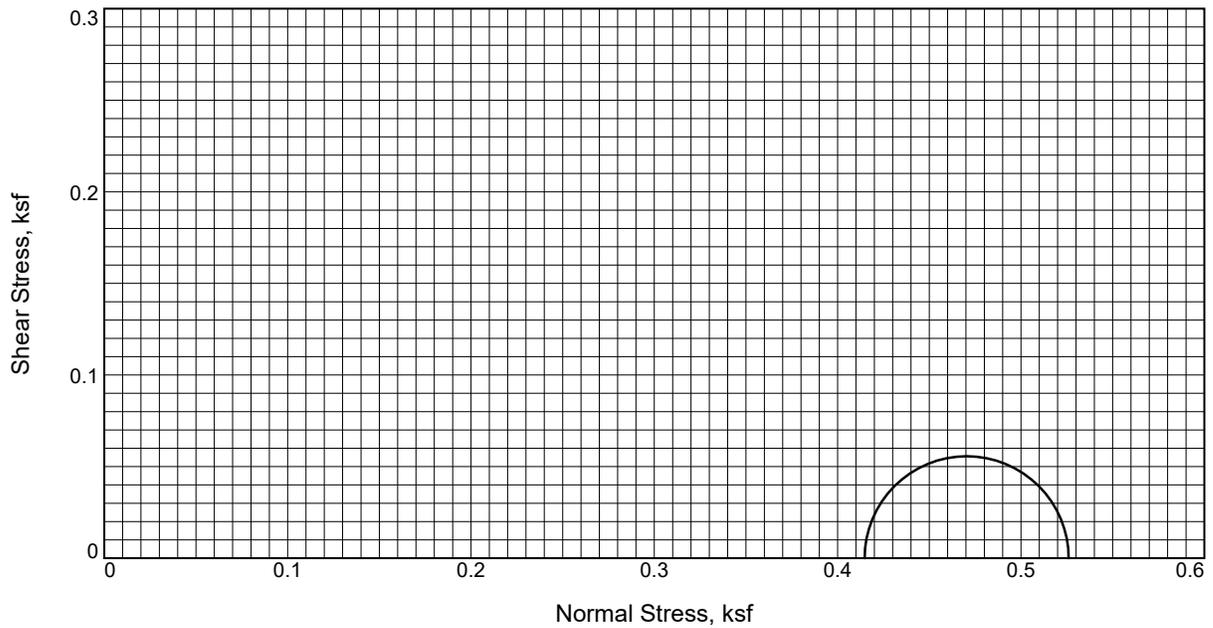
Sample Number: B-6

Proj. No.: L-GEI-020

Date Sampled:

TRIAXIAL SHEAR TEST REPORT
 Fourrier & de Abreu Engineers, LLC
 Baton Rouge, Louisiana

Tested By: CM _____ **Checked By:** JOF _____



Sample No.		1
Initial	Water Content, %	118.6
	Dry Density, pcf	42.0
	Saturation, %	107.1
	Void Ratio	2.9351
	Diameter, in.	2.73
At Test	Height, in.	5.70
	Water Content, %	109.5
	Dry Density, pcf	42.0
	Saturation, %	98.8
	Void Ratio	2.9351
Diameter, in.		2.73
Height, in.		5.70
Strain rate, in./min.		1.000
Back Pressure, psi		0.00
Cell Pressure, psi		2.88
Fail. Stress, ksf		0.11
Ult. Stress, ksf		
σ_1 Failure, ksf		0.53
σ_3 Failure, ksf		0.41

Type of Test:
Unconsolidated Undrained

Sample Type: Undisturbed
Description: Gray Fat Clay

Assumed Specific Gravity= 2.65

Remarks:

Figure _____

Client: GeoEngineers, Inc.

Project: S Grand Chenier Marsh Creation Baker Tract

Source of Sample: B-6 **Depth:** 10-12

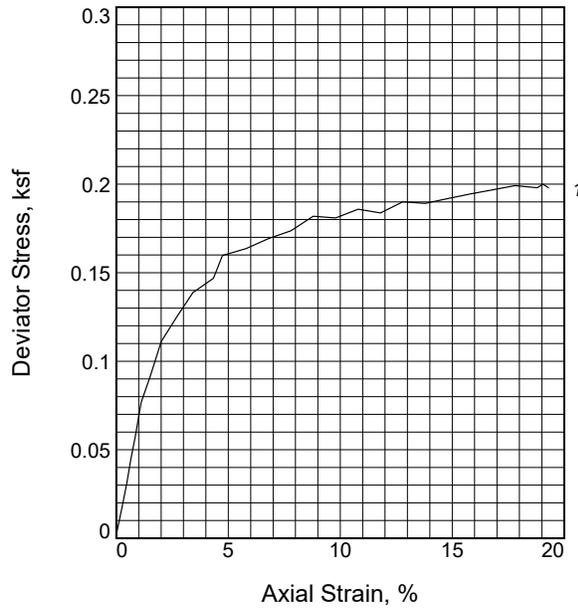
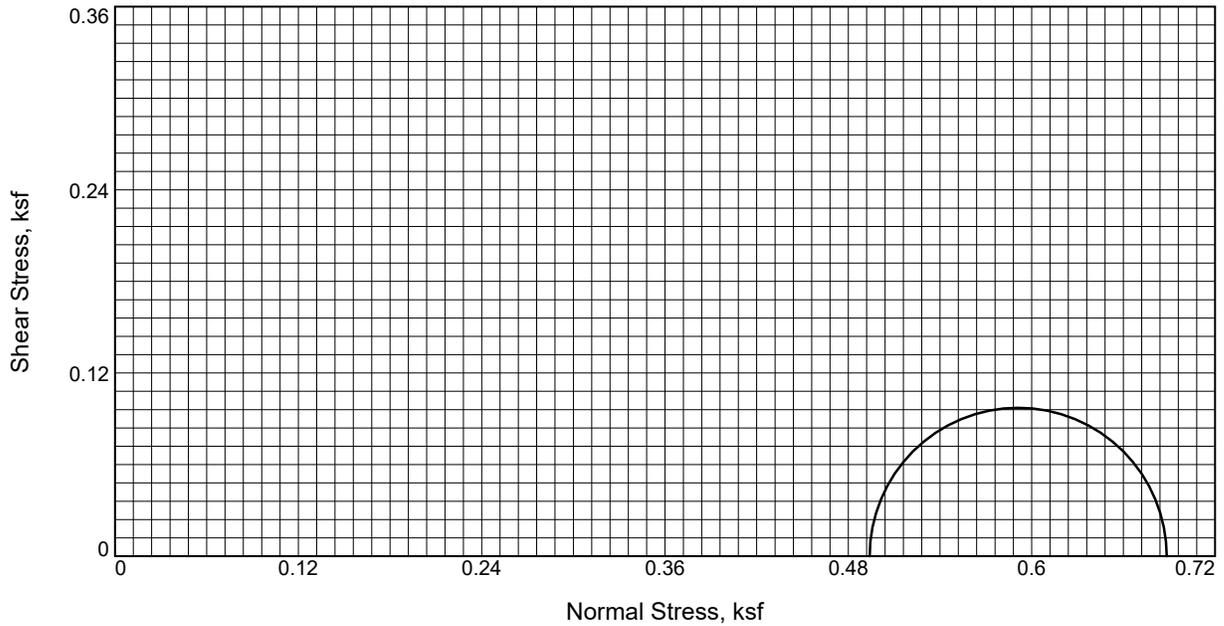
Sample Number: B-6

Proj. No.: L-GEI-020

Date Sampled:

TRIAXIAL SHEAR TEST REPORT
Fourrier & de Abreu Engineers, LLC
Baton Rouge, Louisiana

Tested By: CM **Checked By:** JOF



Sample No.		1
Initial	Water Content, %	117.4
	Dry Density, pcf	40.9
	Saturation, %	102.2
	Void Ratio	3.0452
	Diameter, in.	2.74
At Test	Height, in.	5.69
	Water Content, %	96.6
	Dry Density, pcf	40.9
	Saturation, %	84.0
	Void Ratio	3.0452
Diameter, in.		2.74
Height, in.		5.69
Strain rate, in./min.		1.000
Back Pressure, psi		0.00
Cell Pressure, psi		3.43
Fail. Stress, ksf		0.19
Ult. Stress, ksf		
σ_1 Failure, ksf		0.69
σ_3 Failure, ksf		0.49

Type of Test:
Unconsolidated Undrained

Sample Type: Undisturbed

Description: Gray Fat Clay

Assumed Specific Gravity= 2.65

Remarks:

Figure _____

Client: GeoEngineers, Inc.

Project: S Grand Chenier Marsh Creation Baker Tract

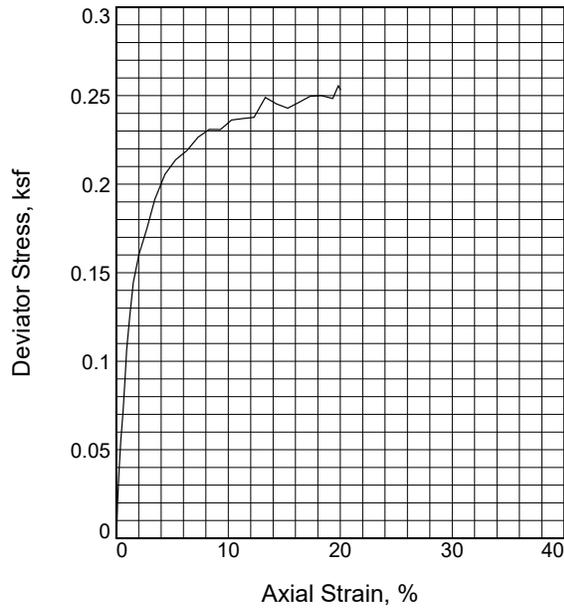
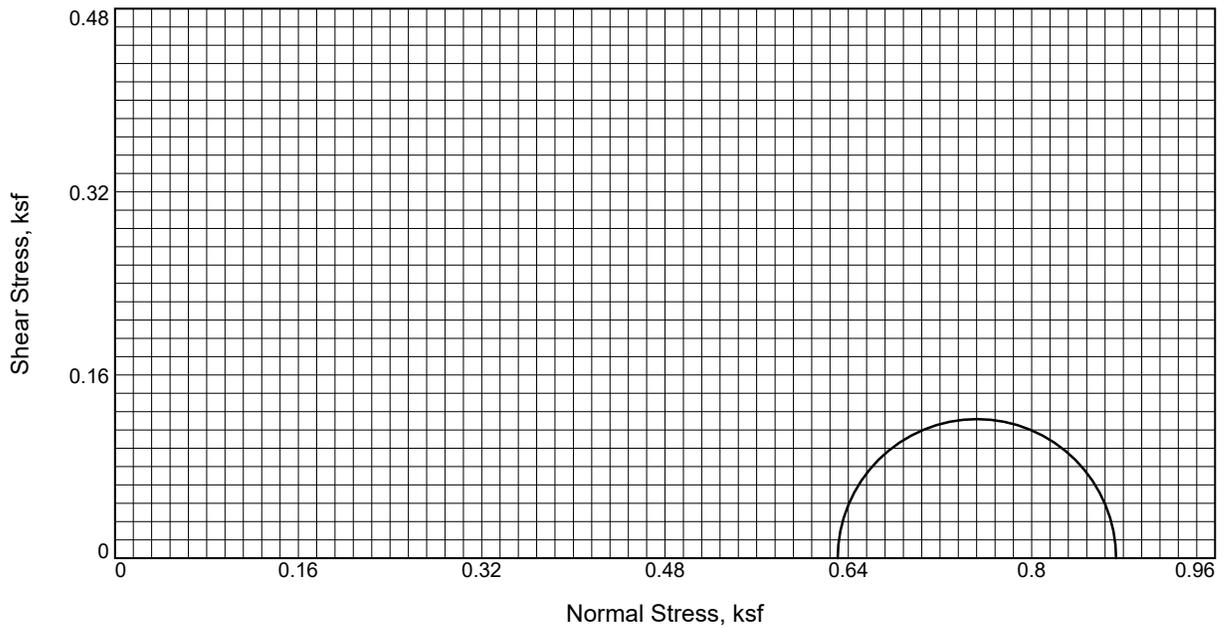
Source of Sample: B-6 **Depth:** 12-14

Sample Number: B-6

Proj. No.: L-GEI-020 **Date Sampled:**

TRIAXIAL SHEAR TEST REPORT
 Fourier & de Abreu Engineers, LLC
 Baton Rouge, Louisiana

Tested By: CM _____ **Checked By:** JOF _____



Sample No.		1
Initial	Water Content, %	37.3
	Dry Density, pcf	65.5
	Saturation, %	64.9
	Void Ratio	1.5242
	Diameter, in.	2.81
At Test	Height, in.	5.72
	Water Content, %	90.0
	Dry Density, pcf	65.5
	Saturation, %	156.5
	Void Ratio	1.5242
Diameter, in.		2.81
Height, in.		5.72
Strain rate, in./min.		1.000
Back Pressure, psi		0.00
Cell Pressure, psi		4.38
Fail. Stress, ksf		0.24
Ult. Stress, ksf		
σ_1 Failure, ksf		0.87
σ_3 Failure, ksf		0.63

Type of Test:

Unconsolidated Undrained

Sample Type: Undisturbed

Description: Gray Fat Clay

LL= 128 PL= 42 PI= 86

Assumed Specific Gravity= 2.65

Remarks:

Figure _____

Client: GeoEngineers, Inc.

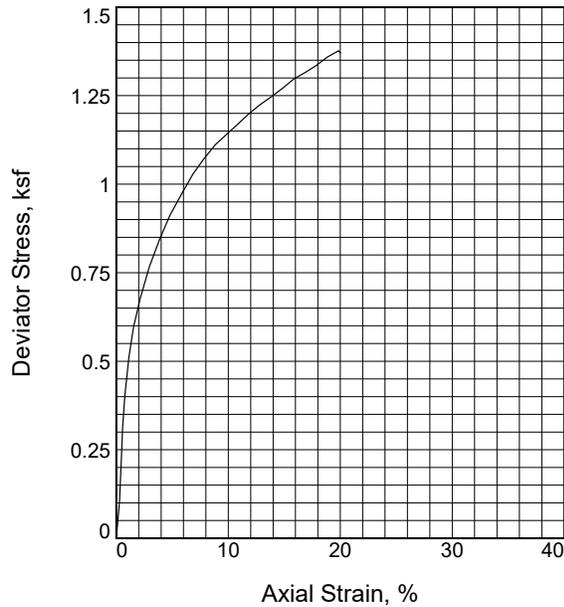
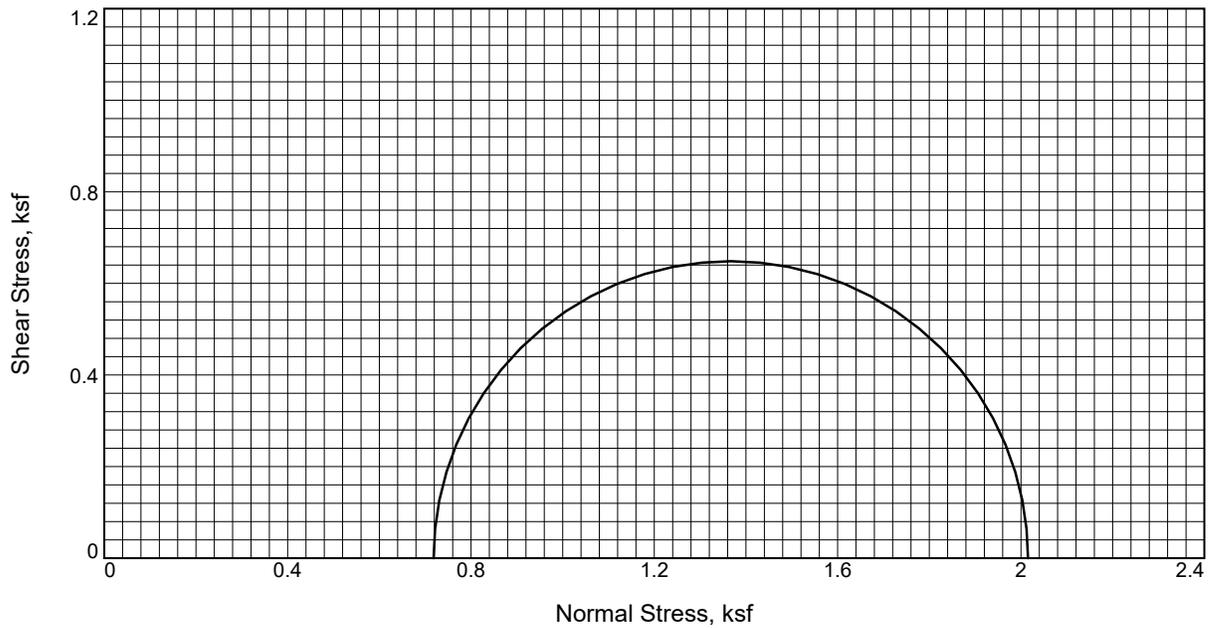
Project: S Grand Chenier Marsh Creation Baker Tract

Source of Sample: B-6 **Depth:** 16-18

Sample Number: B-6

Proj. No.: L-GEI-020 **Date Sampled:**

TRIAXIAL SHEAR TEST REPORT
 Fourrier & de Abreu Engineers, LLC
 Baton Rouge, Louisiana



Sample No.		1
Initial	Water Content, %	35.2
	Dry Density, pcf	90.0
	Saturation, %	111.2
	Void Ratio	0.8379
	Diameter, in.	2.83
At Test	Height, in.	5.73
	Water Content, %	26.9
	Dry Density, pcf	90.0
	Saturation, %	85.1
	Void Ratio	0.8379
Diameter, in.		2.83
Height, in.		5.73
Strain rate, in./min.		1.000
Back Pressure, psi		0.00
Cell Pressure, psi		4.99
Fail. Stress, ksf		1.30
Ult. Stress, ksf		
σ_1 Failure, ksf		2.02
σ_3 Failure, ksf		0.72

Type of Test:
Unconsolidated Undrained

Sample Type: Undisturbed

Description: Gray Fat Clay w/ Silt Lenses

Assumed Specific Gravity= 2.65

Remarks:

Client: GeoEngineers, Inc.

Project: S Grand Chenier Marsh Creation Baker Tract

Source of Sample: B-6 **Depth:** 18-20

Sample Number: B-6

Proj. No.: L-GEI-020 **Date Sampled:**

TRIAXIAL SHEAR TEST REPORT
 Fourrier & de Abreu Engineers, LLC
 Baton Rouge, Louisiana

Figure _____

Tested By: CM Checked By: JOF

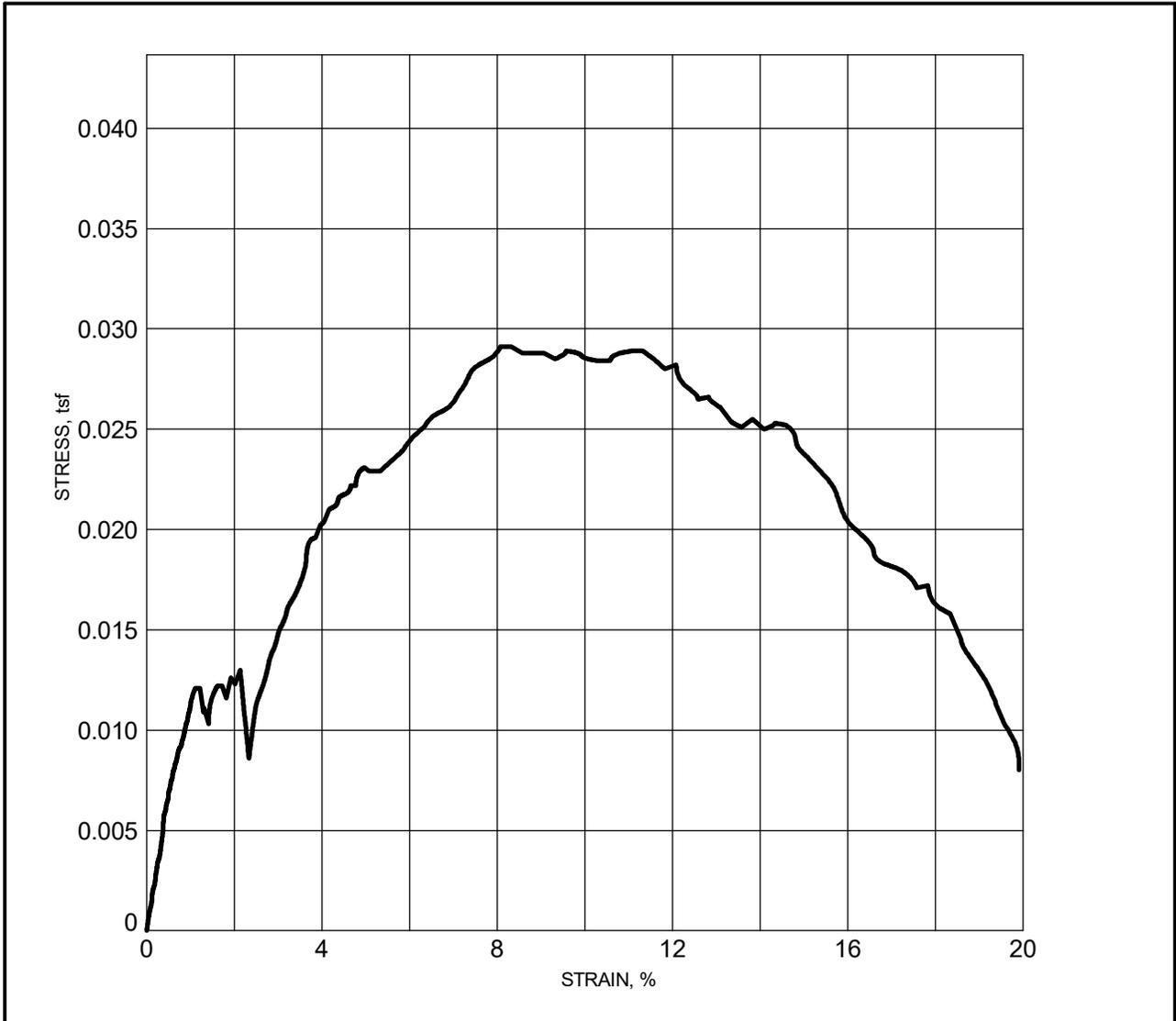
Soil Boring ID	Depth Interval (ft)	D2488	Test Type	D2216	D2166/D2850		D4318			D422/D1140 /D6913	D2166/D2850					D4648	Comments
		Visual Description		Moisture (%)	Unit Weight (PCF)		Atterberg Limits			%<#200 Sieve	Shear Strength (KSF)	Remolded Strength (KSF)	Failure Strain (%)	Confining Pressure (PSI)	Failure Type	Mini Vane Shear Strength (KSF)	
					Wet	Dry	LL	PL	PI								
B-4	2.0 - 4.0	Very soft gray clay with organic matter (CH)	UU	107.6	83.6	40.3					0.03		8.1	5.0	B		
B-4	14.0 - 16.0	Very soft gray clay with sand pockets (CH)	MC	108.6													

Disclaimer: The results presented relate only to those samples tested.
 Note: ASTM standard identification numbers shown above each test description.

Multiple Shear = MS Vertical Shear = VS Angle Shear = AS
 Slickensided = SLS Bulge = B Crumble = C

 Technical Responsibility: <u>Anthony Ju</u> Title: <u>QOM</u> Date: <u>5/2/2023</u>	Summary of Lab Results Project No.: 10883-026-00	USDA-NRCS-5 Grand Chenier Marsh Creation Baker Tract	
			

GEI\UNCONSOLIDATED UNDRAINED GRAPH - GEO TEMPLATE WITH LAB.GDT - 5/2/23 15:44 - P:\1010883026\00\LAB\10883-026-00 BR LAB - NEW ASSIGNED.GPJ



Boring ID	B-4
Depth (ft)	2-4
Water Content, %	107.6
Wet Density, pcf	83.6
Dry Density, pcf	40.3
Saturation, %	90.8
Void Ratio	3.25
Specimen Diameter	2.897
Specimen Height	5.877
Height/diameter ratio	2.03
Deviator Stress, tsf	0.029
Strain, %	8.1
Confining Pressure (psi)	5.0

Bulge

Failure Sketch

LL = PL = PI =

% 200= % Organic= Assumed Gs=2.74

Description: Very soft gray clay with organic matter (CH)

Note: This report may not be reproduced, except in full, without written approval of GeoEngineers, Inc. Test results are applicable only to the specific sample on which they were performed, and should not be interpreted as representative of any other samples obtained at other times, depths or locations, or generated by separate operations or processes.

Tested By: Raven Roberts	Date Tested: 2/8/2023	UNCONSOLIDATED UNDRAINED COMPRESSION TEST ASTM D2850 Project No.: 10883-026-00	USDA-NRCS-5 Grand Chenier Marsh Creation Baker Tract	
Reviewed By: Anthony Ju	Date Reviewed: 2/9/2023		GEOENGINEERS	

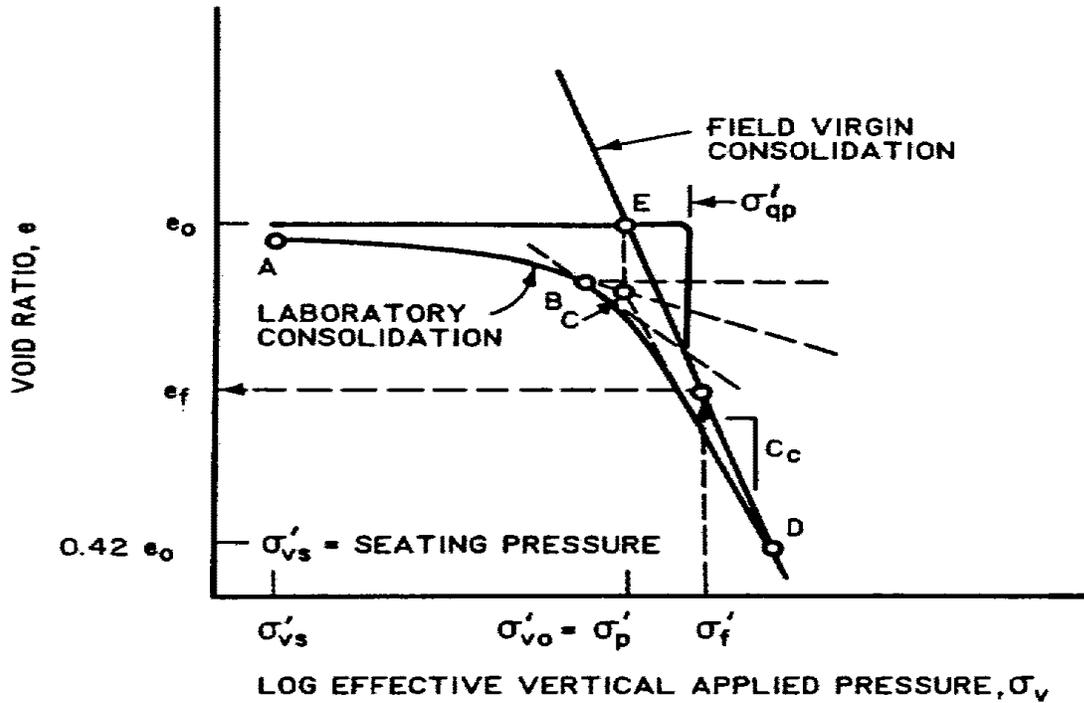
Soil Boring ID	Depth Interval (ft)	D2488	Test Type	D2216	D2166/D2850		D4318			D422/D1140 /D6913	D2166/D2850					D4648	Comments
		Visual Description		Moisture (%)	Unit Weight (PCF)		Atterberg Limits			%<#200 Sieve	Shear Strength (KSF)	Remolded Strength (KSF)	Failure Strain (%)	Confining Pressure (PSI)	Failure Type	Mini Vane Shear Strength (KSF)	
					Wet	Dry	LL	PL	PI								
B-6	6.0 - 8.0	Gray clay (CH)	MC	110.4													

Disclaimer: The results presented relate only to those samples tested.
 Note: ASTM standard identification numbers shown above each test description.

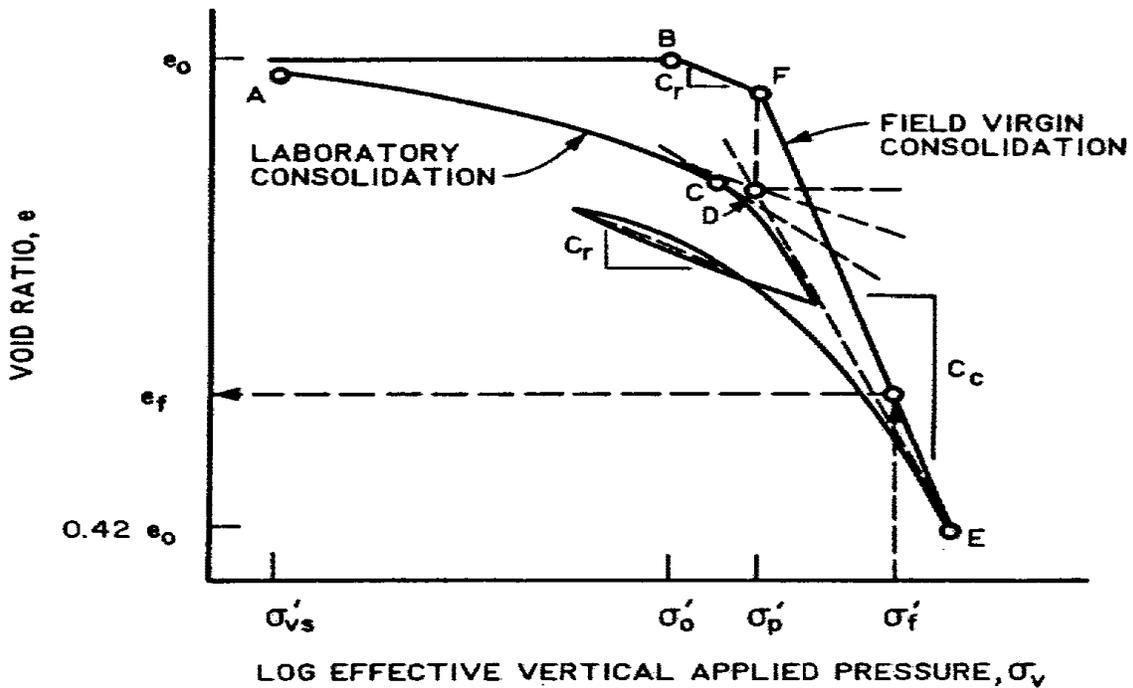
Multiple Shear = MS Vertical Shear = VS Angle Shear = AS
 Slickensided = SLS Bulge = B Crumble = C

 Technical Responsibility: <u>Anthony Ju</u> Title: <u>QOM</u> Date: <u>5/2/2023</u>	Summary of Lab Results Project No.: 10883-026-00	USDA-NRCS-5 Grand Chenier Marsh Creation Baker Tract	
			

Consolidation Reconstruction
Including Procedure Description



a. NORMALLY CONSOLIDATED SOIL



b. OVERCONSOLIDATED SOIL

Figure 3-12. Construction of field virgin consolidation relationships

Table 3-6

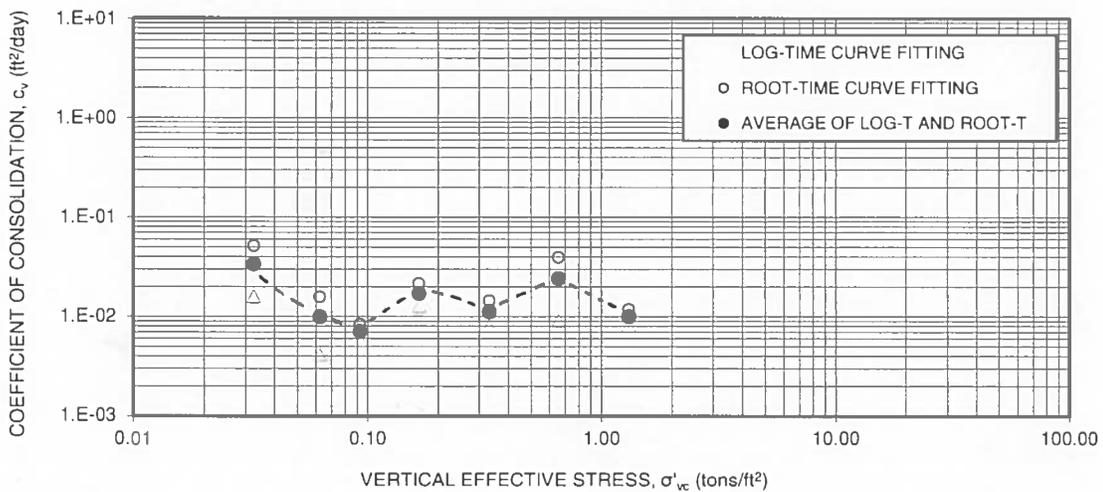
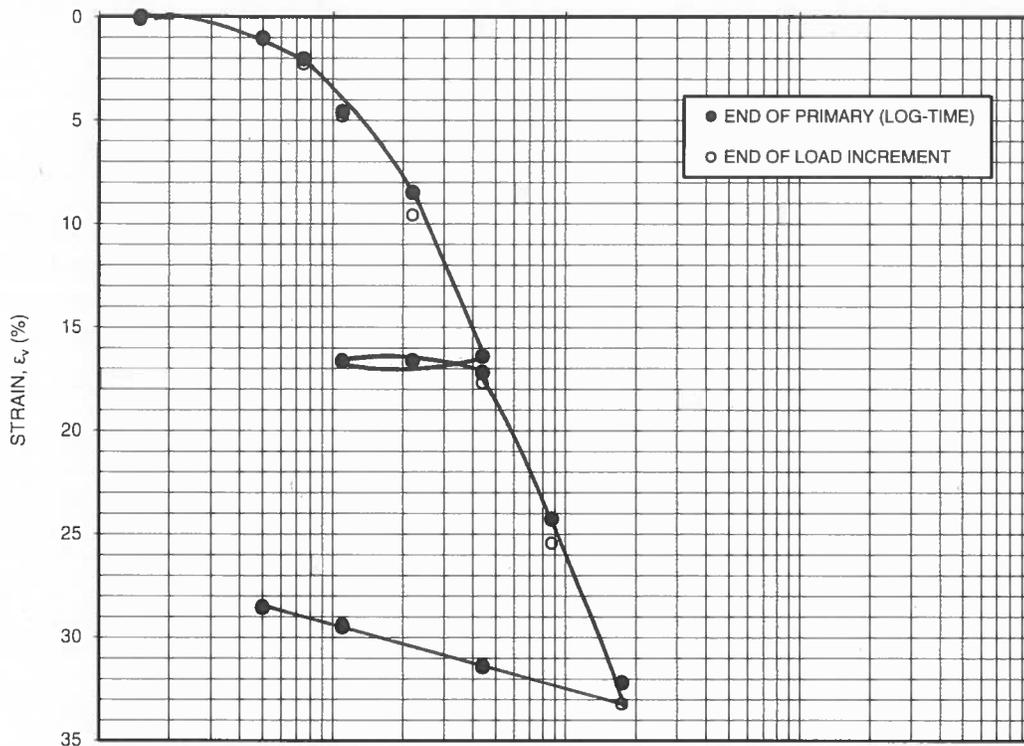
Reconstruction of Virgin Field Consolidation (Data from Item 54)

a. Normally Consolidated Soil (Figure 3-12a)

Step	Description
1	Plot point B at the point of maximum radius of curvature of the laboratory consolidation curve.
2	Plot point C by the Casagrande construction procedure: (1) Draw a horizontal line from B ; (2) Draw a line tangent to the laboratory consolidation curve through B ; and (3) Draw the bisector between horizontal and tangent lines. Point C is the intersection of the straight portion of the laboratory curve with the bisector. Point C indicates the maximum past pressure σ'_p .
3	Plot point E at the intersection e_o and σ'_p . e_o is given as the initial void ratio prior to testing in the consolidometer and σ'_p is found from step 2.
4	Plot point D at the intersection of the laboratory virgin consolidation curve with void ratio $e = 0.42e_o$.
5	The field virgin consolidation curve is the straight line determined by points E and D.

b. Overconsolidated Soil (Figure 3-12b)

Step	Description
1	Plot point B at the intersection of the given e_o and the initial estimated in situ effective overburden pressure σ'_o .
2	Draw a line through B parallel to the mean slope C_r of the rebound laboratory curve.
3	Plot point D using step 2 in Table 3-6a above for normally consolidated soil.
4	Plot point F by extending a vertical line through D up through the intersection of the line of slope C_r extending through B.
5	Plot point E at the intersection of the laboratory virgin consolidation curve with void ratio $e = 0.42e_o$.
6	The field virgin consolidation curve is the straight line through points F and E.



SAMPLE DATA

BORING NO.:	B-6
SAMPLE DEPTH (ft):	2-4
DESCRIPTION:	Gray Clay CH

SPECIMEN CONDITIONS

	INITIAL	FINAL
MOISTURE CONTENT (%):	122.3	74.1
DRY DENSITY (lb/ft³):	40.0	58.8
VOID RATIO:	3.281	1.917

INDEX PROPERTIES

LIQUID LIMIT (%):	105
PLASTIC LIMIT (%):	26
PLASTICITY INDEX (%):	79
SPECIFIC GRAVITY:	2.745 (Assumed)
-200 (%):	99.8

CONSOLIDATION PARAMETERS

VIRGIN COMPRESSION RATIO, CR:	0.264
RECOMPRESSION RATIO, RR:	0.009
PRECONSOLIDATION PRESSURE, σ'_p :	0.16 TSF

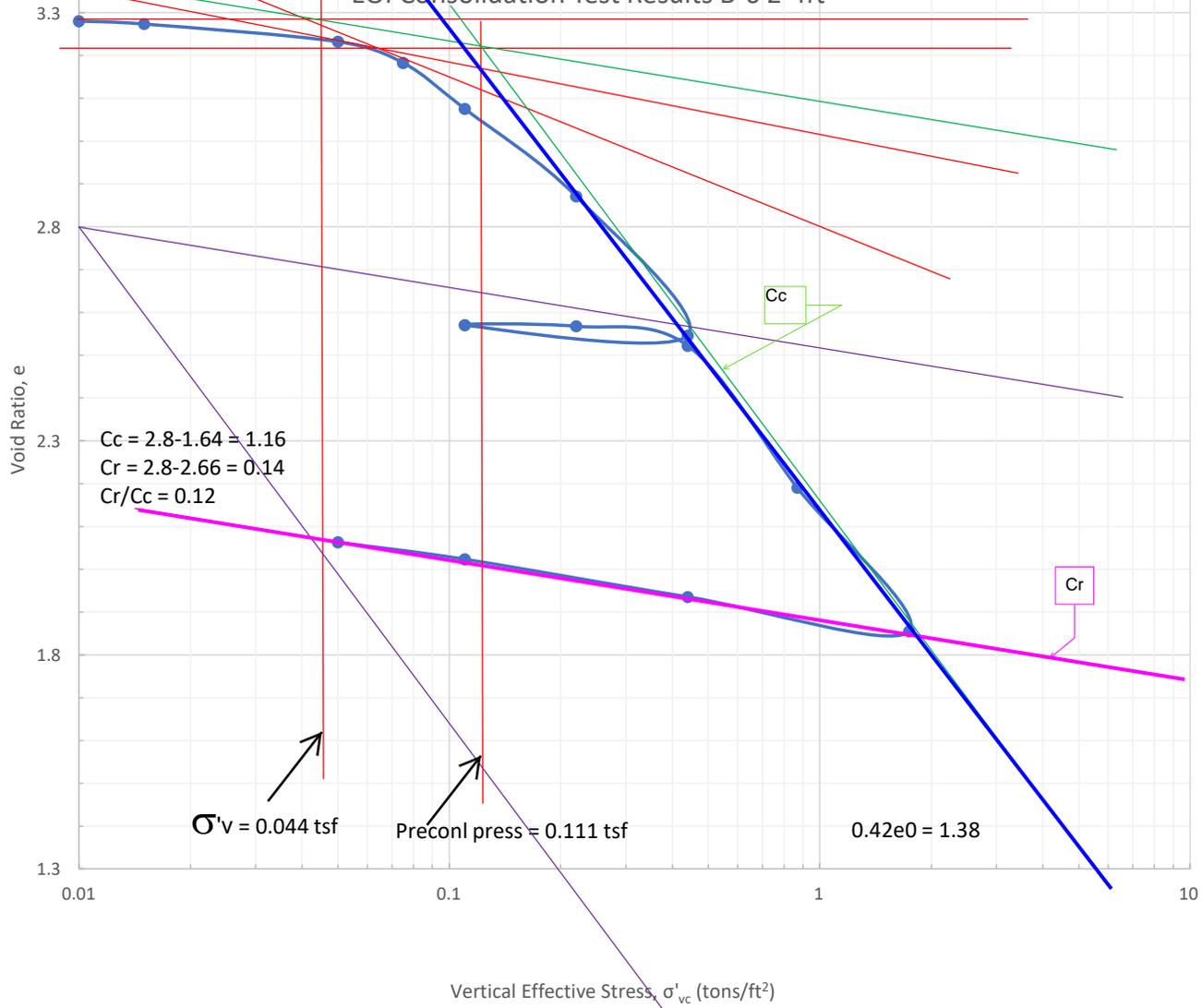
INCREMENTAL CONSOLIDATION TEST RESULTS

Ardaman & Associates, Inc.
 Geotechnical, Environmental and Materials Consultants

Grand Chenier

DRAWN BY CMW	CHECKED BY AYA	DATE 11-16-22
FILE NO. 22-83-3874	APPROVED BY MB	FIGURE 1

EOI Consolidation Test Results B-6 2-4ft



ARDAMAN & ASSOCIATES, INC
GEOTECHNICAL TESTING LABORATORY
ONE-DIMENSIONAL INCREMENTAL LOADING CONSOLIDATION TEST SUMMARY SHEET

Effective Stress (tsf)	Dial Readings (inch)			Time, t_{50} (sec)	Method (L=log, S=sq rt)	Cv (ft ² /day)	Average Effective Stress (tsf)	Height at EOP (inch)	Height at EOI (inch)	Void Ratio at EOP	Void Ratio at EOI	Strain at EOP (%)	Strain at EOI (%)	C _{ave}
	Initial	EOP	EOI											
0.00	0.1760	0.1760	0.1760		-	-	-	0.7500	0.7500	3.2806	3.2806	0.00	0.00	-----
0.015	0.1760	0.1760	0.1772				0.008	0.7500	0.7488	3.2806	3.2737	0.00	0.16	-----
0.05	0.1772	0.1838	0.1844	1020	L	1.62E-02	0.033	0.7422	0.7416	3.2361	3.2327	1.04	1.12	-----
0.075	0.1843	0.1913	0.1931	3900	L	4.14E-03	0.063	0.7346	0.7328	3.1927	3.1824	2.05	2.29	-----
0.11	0.1935	0.2108	0.2124	2640	L	5.89E-03	0.093	0.7155	0.7139	3.0837	3.0746	4.60	4.81	-----
0.22	0.2125	0.2402	0.2484	1140	L	1.27E-02	0.165	0.6862	0.6780	2.9165	2.8697	8.51	9.60	-----
0.44	0.2489	0.3000	0.3054	1560	L	8.09E-03	0.330	0.6269	0.6215	2.5780	2.5472	16.41	17.13	-----
0.11	0.3046	0.3011	0.3005	216	L	5.33E-02	0.275	0.6250	0.6256	2.5672	2.5706	16.67	16.59	-----
0.22	0.3005	0.3008	0.3009				0.165	0.6253	0.6252	2.5689	2.5683	16.63	16.64	-----
0.44	0.3014	0.3057	0.3094	168	L	6.85E-02	0.330	0.6209	0.6172	2.5436	2.5226	17.22	17.71	-----
0.87	0.3102	0.3595	0.3683	1140	L	9.13E-03	0.655	0.5679	0.5591	2.2413	2.1910	24.28	25.45	-----
1.74	0.3695	0.4200	0.4278	1020	L	8.28E-03	1.305	0.5086	0.5008	1.9028	1.8583	32.19	33.23	-----
0.44	0.4272	0.4137	0.4128	372	L	2.05E-02	1.090	0.5143	0.5152	1.9353	1.9405	31.43	31.31	-----
0.11	0.4121	0.3985	0.3975	1620	L	4.99E-03	0.275	0.5288	0.5298	2.0181	2.0238	29.49	29.36	-----
0.05	0.3971	0.3912	0.3905	4200	L	2.00E-03	0.080	0.5357	0.5364	2.0575	2.0615	28.57	28.48	-----

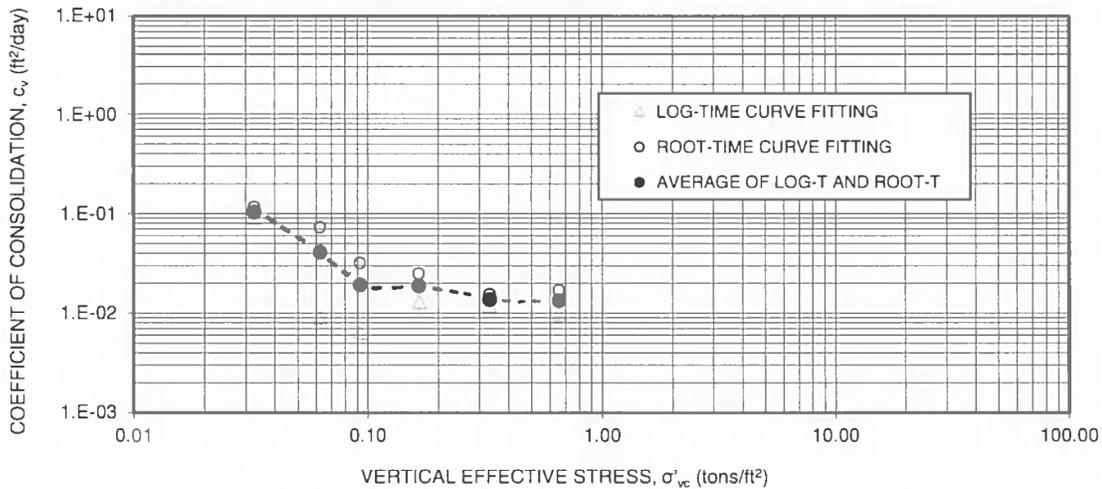
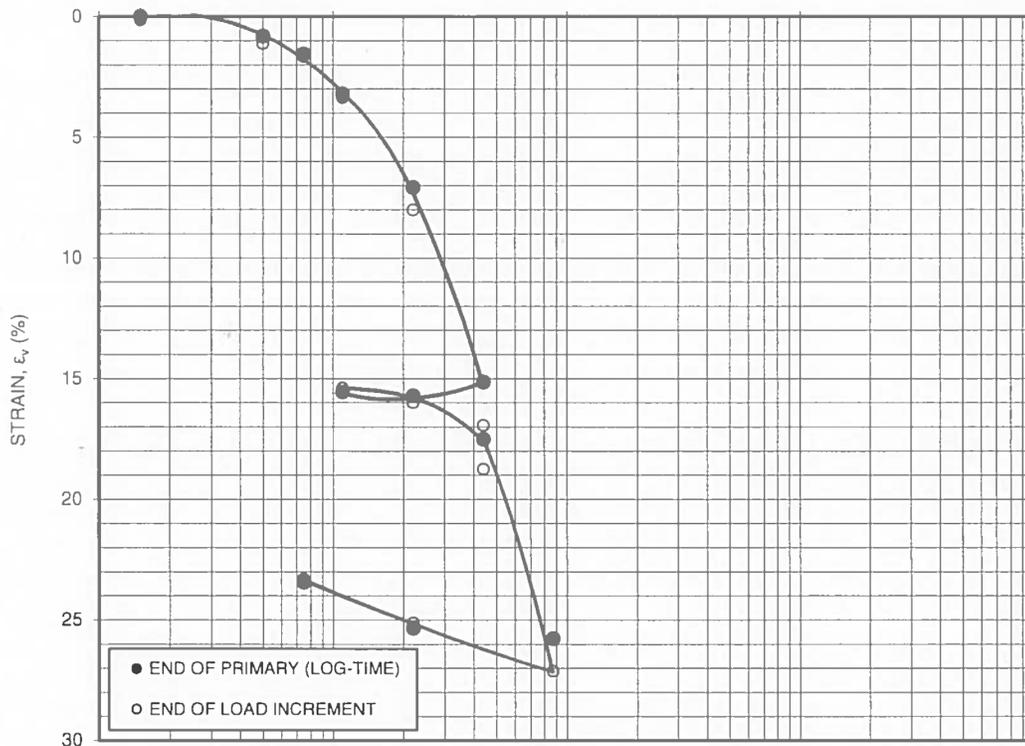
Project Name:	Grand Chenier	Initial Conditions	Final Conditions	EOP= End of Primary Consolidation
File Number:	22-83-3874	Height (in)	0.7500	0.5110
Boring Number:	B-6	w _c (%)	122.3	74.1
Depth:	2-4	γ _t (pcf)	89.0	102.3
		γ _d (pcf)	40.0	58.8
LL = 105	-200 = 99.8	Saturation (%)	102.4	106.1
PI = 79	OC = --	Void ratio, e	3.2806	1.9165
				Specific Gravity 2.745
				Ring Diameter (in) 2.0000
				Ring weight (g) 62.56
				Height of Solids (in) 0.1752
				Weight of Dry Soil (g) 24.76

ARDAMAN & ASSOCIATES, INC
GEOTECHNICAL TESTING LABORATORY

ONE-DIMENSIONAL INCREMENTAL LOADING CONSOLIDATION TEST SUMMARY SHEET

Effective Stress (tsf)	Dial Readings (inch)			Time, t_{90} (sec)	Method (L=log, S=sq rt)	Cv (ft ² /day)	Average Effective Stress (tsf)	Height at EOP (inch)	Height at EOI (inch)	Void Ratio at EOP	Void Ratio at EOI	Strain at EOP (%)	Strain at EOI (%)	C _v /e
	Initial	EOP	EOI											
0.00	0.1760	0.1760	0.1760		-	-	-	0.7500	0.7500	3.2806	3.2806	0.00	0.00	-----
0.015	0.1760	0.1760	0.1772				0.008	0.7500	0.7488	3.2806	3.2737	0.00	0.16	-----
0.05	0.1772	0.1814	0.1844	1382	S	5.15E-02	0.033	0.7446	0.7416	3.2498	3.2327	0.72	1.12	-----
0.075	0.1844	0.1884	0.1931	4438	S	1.57E-02	0.063	0.7376	0.7329	3.2098	3.1830	1.65	2.28	-----
0.11	0.1936	0.2078	0.2124	8074	S	8.33E-03	0.093	0.7187	0.7141	3.1020	3.0757	4.17	4.79	-----
0.22	0.2125	0.2347	0.2484	2940	S	2.15E-02	0.165	0.6919	0.6782	2.9490	2.8708	7.75	9.57	-----
0.44	0.2485	0.2891	0.3054	3840	S	1.44E-02	0.330	0.6376	0.6213	2.6391	2.5460	14.99	17.16	-----
0.11	0.3047	0.3007	0.3005	694	S	7.14E-02	0.275	0.6253	0.6255	2.5689	2.5700	16.63	16.60	-----
0.22	0.3005	0.3008	0.3009				0.165	0.6252	0.6251	2.5683	2.5677	16.64	16.65	-----
0.44	0.3014	0.3053	0.3094	540	S	9.18E-02	0.330	0.6212	0.6171	2.5455	2.5221	17.17	17.72	-----
0.87	0.3102	0.3595	0.3683	1140	S	3.93E-02	0.655	0.5678	0.5590	2.2407	2.1905	24.29	25.47	-----
1.74	0.3690	0.4146	0.4278	3110	S	1.18E-02	1.305	0.5134	0.5002	1.9302	1.8549	31.55	33.31	-----
0.44	0.4269	0.4170	0.4128	913	S	3.57E-02	1.090	0.5101	0.5143	1.9114	1.9353	31.99	31.43	-----
0.11	0.4129	0.4010	0.3975	4034	S	8.56E-03	0.275	0.5262	0.5297	2.0033	2.0232	29.84	29.37	-----
0.05	0.3975	0.3930	0.3905	7393	S	4.88E-03	0.080	0.5342	0.5367	2.0489	2.0632	28.77	28.44	-----

Project Name:	Grand Chenier	Initial Conditions	Final Conditions	EOP= End of Primary Consolidation
File Number:	22-83-3874	Height (in)	0.7500	EOI= End of load increment (typically 24 hrs +/-)
Boring Number:	B-6	w _c (%)	122.3	Specific Gravity
Depth:	2-4	γ _t (pcf)	89.0	74.1
		γ _d (pcf)	40.0	102.3
		Saturation (%)	102.4	58.8
LL = 105	-200 = 99.8	Void ratio, e	3.2806	106.1
PI = 79	OC = --			1.9165
				Ring Diameter (in)
				2.0000
				Ring weight (g)
				62.56
				Height of Solids (in)
				0.1752
				Weight of Dry Soil (g)
				24.76



SAMPLE DATA

BORING NO.:	B-4
SAMPLE DEPTH (ft):	10-12
DESCRIPTION:	Gray Clay CH

SPECIMEN CONDITIONS

	INITIAL	FINAL
MOISTURE CONTENT (%):	128.7	91.7
DRY DENSITY (lb/ft³):	38.3	50.9
VOID RATIO:	3.439	2.344

INDEX PROPERTIES

LIQUID LIMIT (%):	117
PLASTIC LIMIT (%):	26
PLASTICITY INDEX (%):	91
SPECIFIC GRAVITY:	2.725 (Assumed)
-200 (%):	100

CONSOLIDATION PARAMETERS

VIRGIN COMPRESSION RATIO, CR:	0.313
RECOMPRESSION RATIO, RR:	0.033
PRECONSOLIDATION PRESSURE, σ'_p :	0.21 TSF

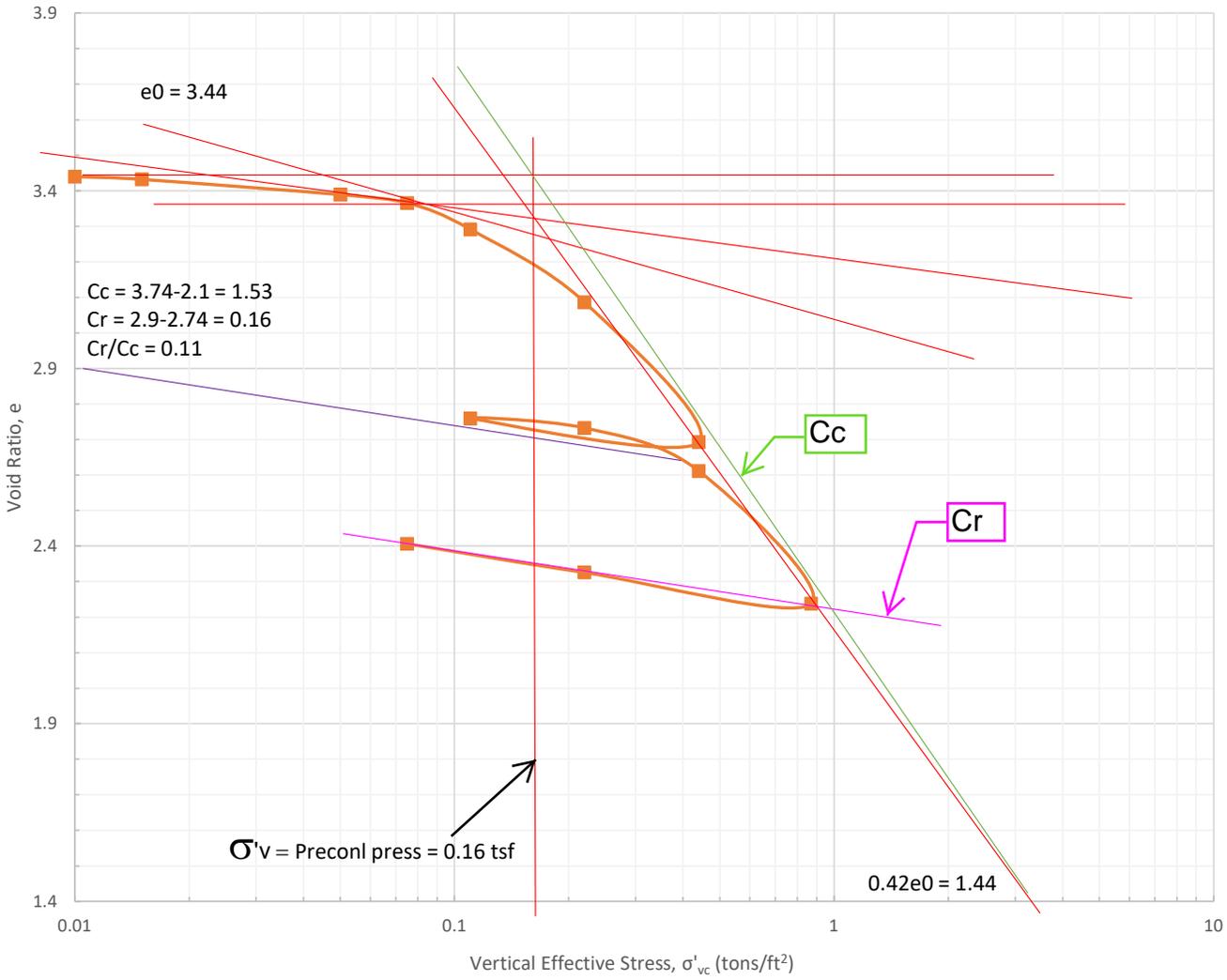
INCREMENTAL CONSOLIDATION TEST RESULTS

Ardaman & Associates, Inc.
Geotechnical, Environmental and Materials Consultants

Grand Chenier

DRAWN BY	CWV	CHECKED BY	AYA	DATE	11-16-22
FILE NO.	22-83-3874	APPROVED BY	MB	FIGURE	1

EOI Consolidation Test Results B-4 10-12ft



ARDAMAN & ASSOCIATES, INC
GEOTECHNICAL TESTING LABORATORY

ONE-DIMENSIONAL INCREMENTAL LOADING CONSOLIDATION TEST SUMMARY SHEET

Effective Stress (tsf)	Dial Readings (inch)			Time, t_{50} (sec)	Method (L=log, S=sq rt)	Cv (ft ² /day)	Average Effective Stress (tsf)	Height at EOP (inch)	Height at EOI (inch)	Void Ratio at EOP	Void Ratio at EOI	Strain at EOP (%)	Strain at EOI (%)	C _{αε}
	Initial	EOP	EOI											
0.00	0.0648	0.0648	0.0648		-	-	-	0.7500	0.7500	3.4395	3.4395	0.00	0.00	-----
0.015	0.0648	0.0648	0.0660				0.008	0.7500	0.7488	3.4395	3.4324	0.00	0.16	-----
0.05	0.0660	0.0710	0.0733	180	L	9.17E-02	0.033	0.7438	0.7415	3.4028	3.3891	0.83	1.13	0.00167
0.075	0.0733	0.0766	0.0773	1800	L	9.02E-03	0.063	0.7383	0.7375	3.3699	3.3655	1.57	1.67	0.00152
0.11	0.0773	0.0889	0.0901	2460	L	6.45E-03	0.093	0.7259	0.7247	3.2968	3.2897	3.21	3.37	0.00547
0.22	0.0901	0.1180	0.1250	1170	L	1.28E-02	0.165	0.6968	0.6898	3.1246	3.0831	7.09	8.03	0.01093
0.44	0.1246	0.1780	0.1915	1080	L	1.21E-02	0.330	0.6364	0.6229	2.7670	2.6871	15.15	16.95	0.01667
0.11	0.1910	0.1806	0.1794	246	L	4.75E-02	0.275	0.6333	0.6345	2.7487	2.7558	15.56	15.40	-----
0.22	0.1795	0.1819	0.1841	90	L	1.32E-01	0.165	0.6321	0.6299	2.7416	2.7286	15.72	16.01	-----
0.44	0.1844	0.1957	0.2050	198	L	5.84E-02	0.330	0.6186	0.6093	2.6617	2.6066	17.52	18.76	-----
0.87	0.2053	0.2580	0.2681	1020	L	9.88E-03	0.655	0.5566	0.5465	2.2947	2.2349	25.79	27.13	0.01333
0.22	0.2674	0.2540	0.2524	306	L	2.97E-02	0.545	0.5599	0.5615	2.3142	2.3237	25.35	25.13	-----
0.075	0.2519	0.2392	0.2383	1620	L	5.90E-03	0.148	0.5742	0.5751	2.3989	2.4042	23.44	23.32	-----

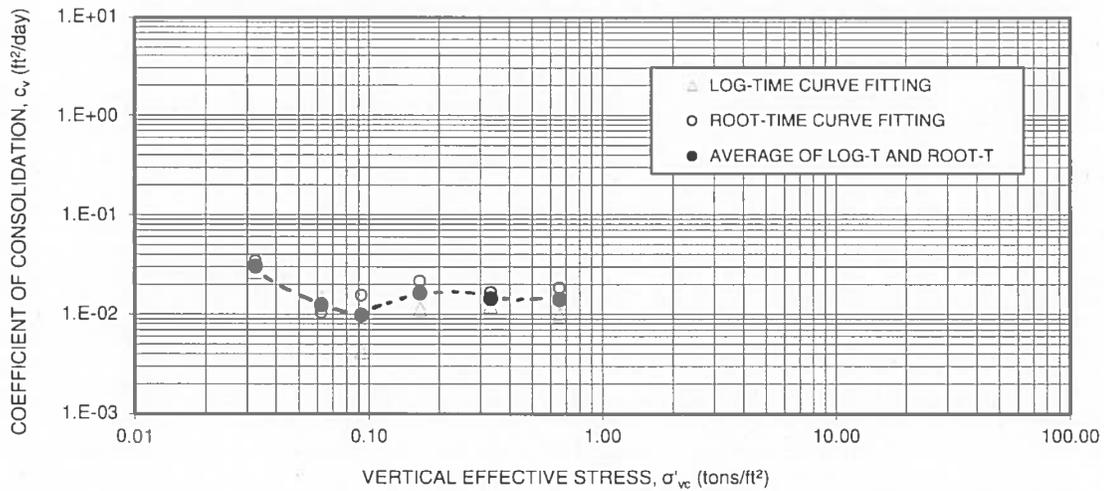
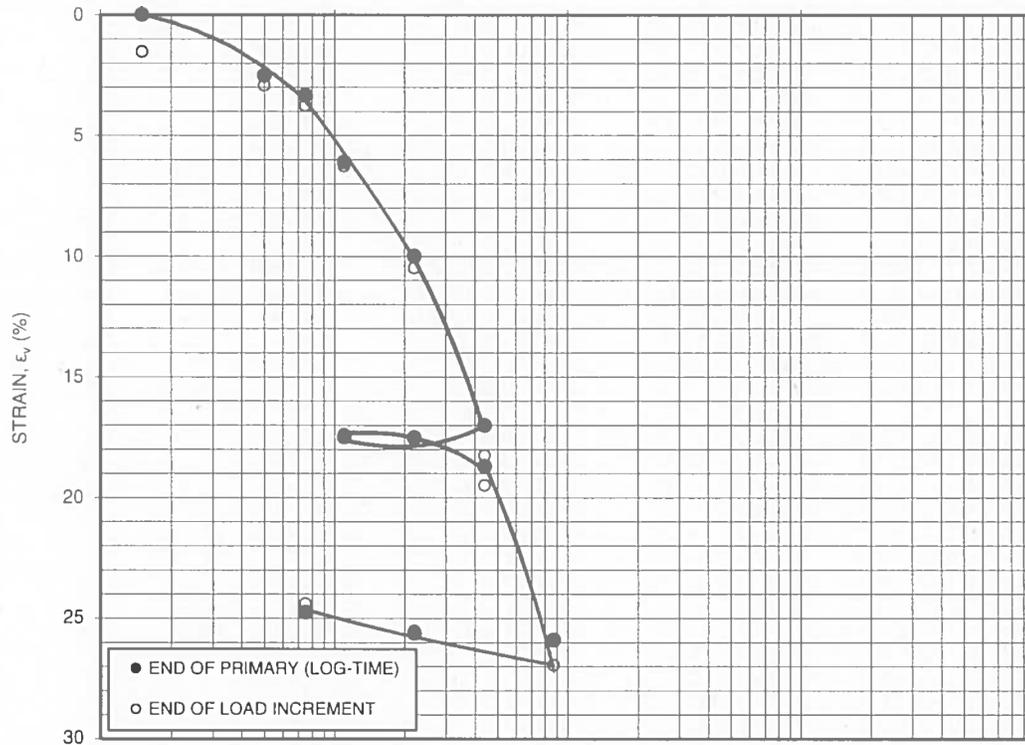
Project Name:	Grand Chenier	Initial Conditions	Final Conditions	EOP= End of Primary Consolidation
File Number:	22-83-3874	Height (in)	0.7500	EOI= End of load increment (typically 24 hrs +/-)
Boring Number:	B-4	w _c (%)	128.7	Specific Gravity
Depth:	10-12	γ _t (pcf)	87.6	Ring Diameter (in)
		γ _d (pcf)	38.3	Ring weight (g)
LL = 117	-200 = 100	Saturation (%)	102.0	Height of Solids (in)
PI = 91	OC = --	Void ratio, e	3.4395	Weight of Dry Soil (g)
			2.3444	2.725
				2.0000
				62.54
				0.1689
				23.70

ARDAMAN & ASSOCIATES, INC
GEOTECHNICAL TESTING LABORATORY

ONE-DIMENSIONAL INCREMENTAL LOADING CONSOLIDATION TEST SUMMARY SHEET

Effective Stress (tsf)	Dial Readings (inch)			Time, t_{90} (sec)	Method (L=log, S=sq rt)	Cv (ft ² /day)	Average Effective Stress (tsf)	Height at EOP (inch)	Height at EOI (inch)	Void Ratio at EOP	Void Ratio at EOI	Strain at EOP (%)	Strain at EOI (%)	C _{ve}
	Initial	EOP	EOI											
0.00	0.0648	0.0648	0.0648		-	-	-	0.7500	0.7500	3.4395	3.4395	0.00	0.00	-----
0.015	0.0648	0.0648	0.0660				0.008	0.7500	0.7488	3.4395	3.4324	0.00	0.16	-----
0.05	0.0660	0.0703	0.0733	614	S	1.16E-01	0.033	0.7445	0.7415	3.4069	3.3891	0.73	1.13	0.00167
0.075	0.0733	0.0748	0.0773	960	S	7.29E-02	0.063	0.7400	0.7375	3.3803	3.3655	1.33	1.67	0.00152
0.11	0.0776	0.0834	0.0901	2160	S	3.19E-02	0.093	0.7317	0.7250	3.3311	3.2915	2.44	3.33	0.00547
0.22	0.0903	0.1111	0.1250	2614	S	2.49E-02	0.165	0.7042	0.6903	3.1684	3.0861	6.11	7.96	0.01093
0.44	0.1250	0.1728	0.1915	3650	S	1.55E-02	0.330	0.6425	0.6238	2.8031	2.6924	14.33	16.83	0.01667
0.11	0.1907	0.1825	0.1794	735	S	6.85E-02	0.275	0.6320	0.6351	2.7410	2.7593	15.73	15.32	-----
0.22	0.1796	0.1816	0.1841	290	S	1.77E-01	0.165	0.6331	0.6306	2.7475	2.7327	15.59	15.92	-----
0.44	0.1845	0.1945	0.2050	694	S	7.20E-02	0.330	0.6206	0.6101	2.6735	2.6114	17.25	18.65	-----
0.87	0.2050	0.2483	0.2681	2614	S	1.69E-02	0.655	0.5668	0.5470	2.3551	2.2378	24.43	27.07	0.01333
0.22	0.2672	0.2570	0.2524	778	S	5.00E-02	0.545	0.5572	0.5618	2.2982	2.3255	25.71	25.09	-----
0.075	0.2520	0.2436	0.2383	2535	S	1.61E-02	0.148	0.5702	0.5755	2.3752	2.4065	23.97	23.27	-----

Project Name:	Grand Chenier	Initial Conditions	Final Conditions	EOP= End of Primary Consolidation
File Number:	22-83-3874	Height (in)	0.7500	EOI= End of load increment (typically 24 hrs +/-)
Boring Number:	B-4	w _c (%)	128.7	Specific Gravity
Depth:	10-12	γ _t (pcf)	87.6	Ring Diameter (in)
		γ _d (pcf)	38.3	Ring weight (g)
LL =	117	Saturation (%)	102.0	Height of Solids (in)
PI =	91	Void ratio, e	3.4395	Weight of Dry Soil (g)
	-200 = 100			
	OC = --			



SAMPLE DATA

BORING NO.:	B-5
SAMPLE DEPTH (ft):	6-8
DESCRIPTION:	Gray Clay CH

SPECIMEN CONDITIONS

	INITIAL	FINAL
MOISTURE CONTENT (%):	122.1	83.7
DRY DENSITY (lb/ft³):	39.9	53.4
VOID RATIO:	3.261	2.187

INDEX PROPERTIES

LIQUID LIMIT (%):	98
PLASTIC LIMIT (%):	25
PLASTICITY INDEX (%):	73
SPECIFIC GRAVITY:	2.726 (Assumed)
-200 (%):	99.6

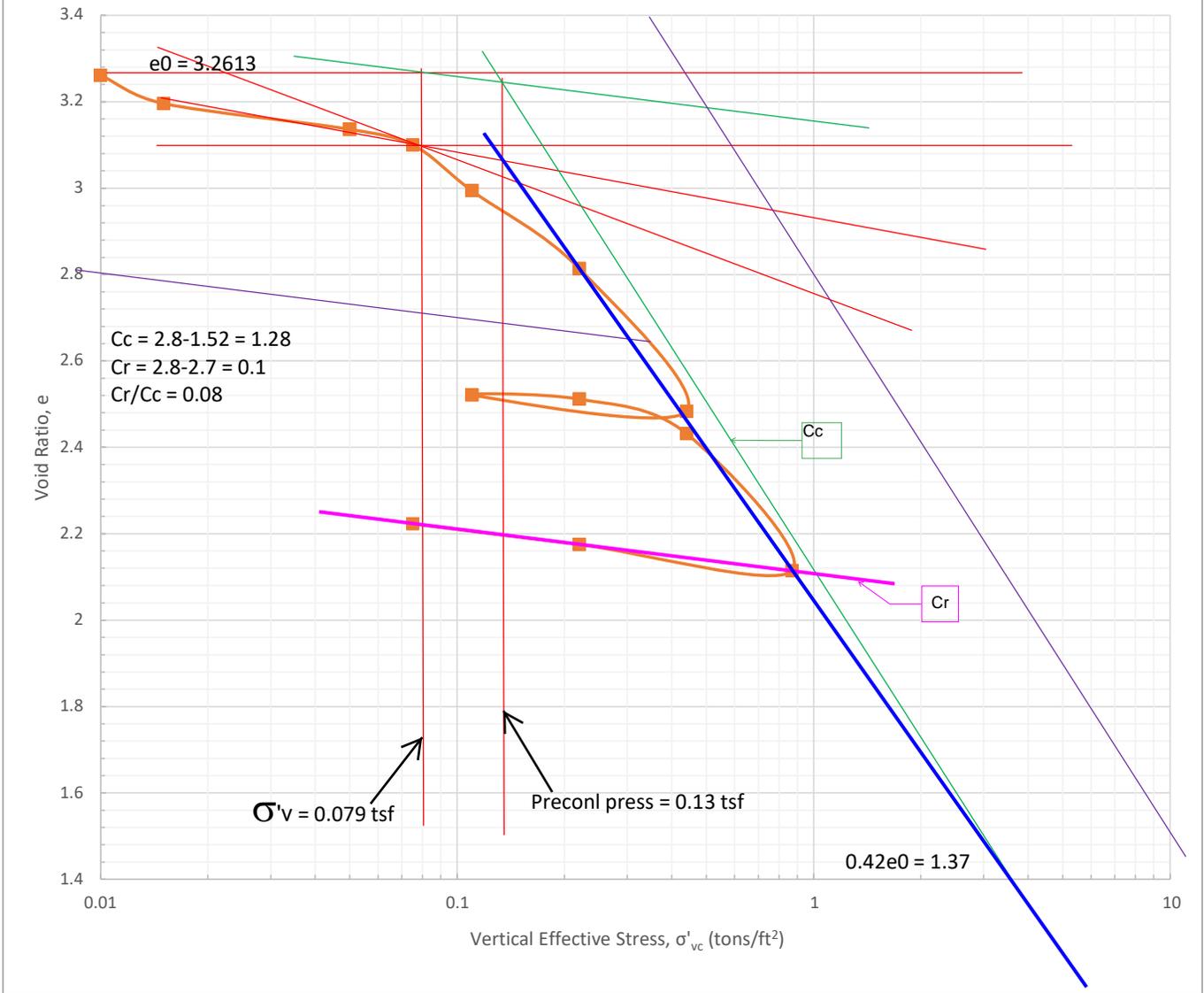
CONSOLIDATION PARAMETERS

VIRGIN COMPRESSION RATIO, CR:	0.266
RECOMPRESSION RATIO, RR:	0.02
PRECONSOLIDATION PRESSURE, σ'_p :	0.18 TSF

INCREMENTAL CONSOLIDATION TEST RESULTS

 Ardaman & Associates, Inc. Geotechnical, Environmental and Materials Consultants		
Grand Chenier		
DRAWN BY CMW	CHECKED BY AYA	DATE 11-18-22
FILE NO. 22-83-3874	APPROVED BY MB	FIGURE 1

EOI Consolidation Test Results B-5 6-8ft



ARDAMAN & ASSOCIATES, INC
GEOTECHNICAL TESTING LABORATORY

ONE-DIMENSIONAL INCREMENTAL LOADING CONSOLIDATION TEST SUMMARY SHEET

Effective Stress (tsf)	Dial Readings (inch)			Time, t_{50} (sec)	Method (L=log, S=sq rt)	Cv (ft ² /day)	Average Effective Stress (tsf)	Height at EOP (inch)	Height at EOI (inch)	Void Ratio at EOP	Void Ratio at EOI	Strain at EOP (%)	Strain at EOI (%)	C _{αE}
	Initial	EOP	EOI											
0.00	0.0610	0.0610	0.0610		-	-	-	0.7500	0.7500	3.2613	3.2613	0.00	0.00	-----
0.015	0.0610	0.0610	0.0725				0.008	0.7500	0.7385	3.2613	3.1960	0.00	1.53	-----
0.05	0.0725	0.0799	0.0830	600	L	2.67E-02	0.033	0.7311	0.7280	3.1539	3.1363	2.52	2.93	0.00213
0.075	0.0830	0.0860	0.0893	1080	L	1.45E-02	0.063	0.7250	0.7217	3.1192	3.1005	3.33	3.77	0.00227
0.11	0.0895	0.1070	0.1083	3600	L	4.19E-03	0.093	0.7042	0.7029	3.0011	2.9937	6.11	6.28	0.00587
0.22	0.1085	0.1364	0.1401	1260	L	1.12E-02	0.165	0.6750	0.6713	2.8352	2.8141	10.00	10.49	0.00600
0.44	0.1401	0.1890	0.1983	1020	L	1.22E-02	0.330	0.6224	0.6131	2.5363	2.4835	17.01	18.25	0.01200
0.11	0.1977	0.1920	0.1912	174	L	6.46E-02	0.275	0.6188	0.6196	2.5158	2.5204	17.49	17.39	-----
0.22	0.1913	0.1923	0.1929	72	L	1.58E-01	0.165	0.6186	0.6180	2.5147	2.5113	17.52	17.60	-----
0.44	0.1933	0.2016	0.2076	234	L	4.77E-02	0.330	0.6097	0.6037	2.4641	2.4301	18.71	19.51	-----
0.87	0.2080	0.2560	0.2638	1020	L	9.77E-03	0.655	0.5557	0.5479	2.1573	2.1130	25.91	26.95	0.01067
0.22	0.2633	0.2534	0.2527	246	L	3.68E-02	0.545	0.5578	0.5585	2.1693	2.1732	25.63	25.53	-----
0.075	0.2523	0.2464	0.2439	594	L	1.57E-02	0.148	0.5644	0.5669	2.2068	2.2210	24.75	24.41	-----

Project Name:	Grand Chenier	Initial Conditions	Final Conditions	EOP= End of Primary Consolidation
File Number:	22-83-3874	Height (in)	0.7500	0.5610
Boring Number:	B-5	w _c (%)	122.1	83.7
Depth:	6-8	γ _t (pcf)	88.7	98.1
		γ _d (pcf)	39.9	53.4
LL = 98	-200 = 99.6	Saturation (%)	102.1	104.3
PI = 73	OC = --	Void ratio, e	3.2613	2.1874
				Specific Gravity 2.726
				Ring Diameter (in) 2.0000
				Ring weight (g) 62.58
				Height of Solids (in) 0.1760
				Weight of Dry Soil (g) 24.70

ARDAMAN & ASSOCIATES, INC
GEOTECHNICAL TESTING LABORATORY

ONE-DIMENSIONAL INCREMENTAL LOADING CONSOLIDATION TEST SUMMARY SHEET

Effective Stress (tsf)	Dial Readings (inch)			Time, t_{90} (sec)	Method (L=log, S=sq rt)	Cv (ft ² /day)	Average Effective Stress (tsf)	Height at EOP (inch)	Height at EOI (inch)	Void Ratio at EOP	Void Ratio at EOI	Strain at EOP (%)	Strain at EOI (%)	C _{αE}
	Initial	EOP	EOI											
0.00	0.0610	0.0610	0.0610		-	-	-	0.7500	0.7500	3.2613	3.2613	0.00	0.00	-----
0.015	0.0610	0.0610	0.0725				0.008	0.7500	0.7385	3.2613	3.1960	0.00	1.53	-----
0.05	0.0725	0.0789	0.0830	2018	S	3.42E-02	0.033	0.7321	0.7280	3.1596	3.1363	2.39	2.93	0.00213
0.075	0.0830	0.0865	0.0893	6490	S	1.04E-02	0.063	0.7245	0.7217	3.1164	3.1005	3.40	3.77	0.00227
0.11	0.0896	0.0996	0.1083	4234	S	1.55E-02	0.093	0.7117	0.7030	3.0437	2.9943	5.11	6.27	0.00587
0.22	0.1084	0.1291	0.1401	2857	S	2.14E-02	0.165	0.6823	0.6713	2.8766	2.8141	9.03	10.49	0.00600
0.44	0.1401	0.1822	0.1983	3286	S	1.64E-02	0.330	0.6292	0.6131	2.5749	2.4835	16.11	18.25	0.01200
0.11	0.1978	0.1929	0.1912	540	S	8.96E-02	0.275	0.6180	0.6197	2.5113	2.5210	17.60	17.37	-----
0.22	0.1913	0.1920	0.1929	217	S	2.26E-01	0.165	0.6190	0.6181	2.5170	2.5119	17.47	17.59	-----
0.44	0.1935	0.1996	0.2076	540	S	8.94E-02	0.330	0.6120	0.6040	2.4772	2.4318	18.40	19.47	-----
0.87	0.2080	0.2453	0.2638	2381	S	1.84E-02	0.655	0.5667	0.5482	2.2198	2.1147	24.44	26.91	0.01067
0.22	0.2633	0.2534	0.2527	246	S	1.59E-01	0.545	0.5581	0.5588	2.1710	2.1749	25.59	25.49	-----
0.075	0.2524	0.2477	0.2439	1382	S	2.91E-02	0.148	0.5635	0.5673	2.2014	2.2230	24.87	24.37	-----

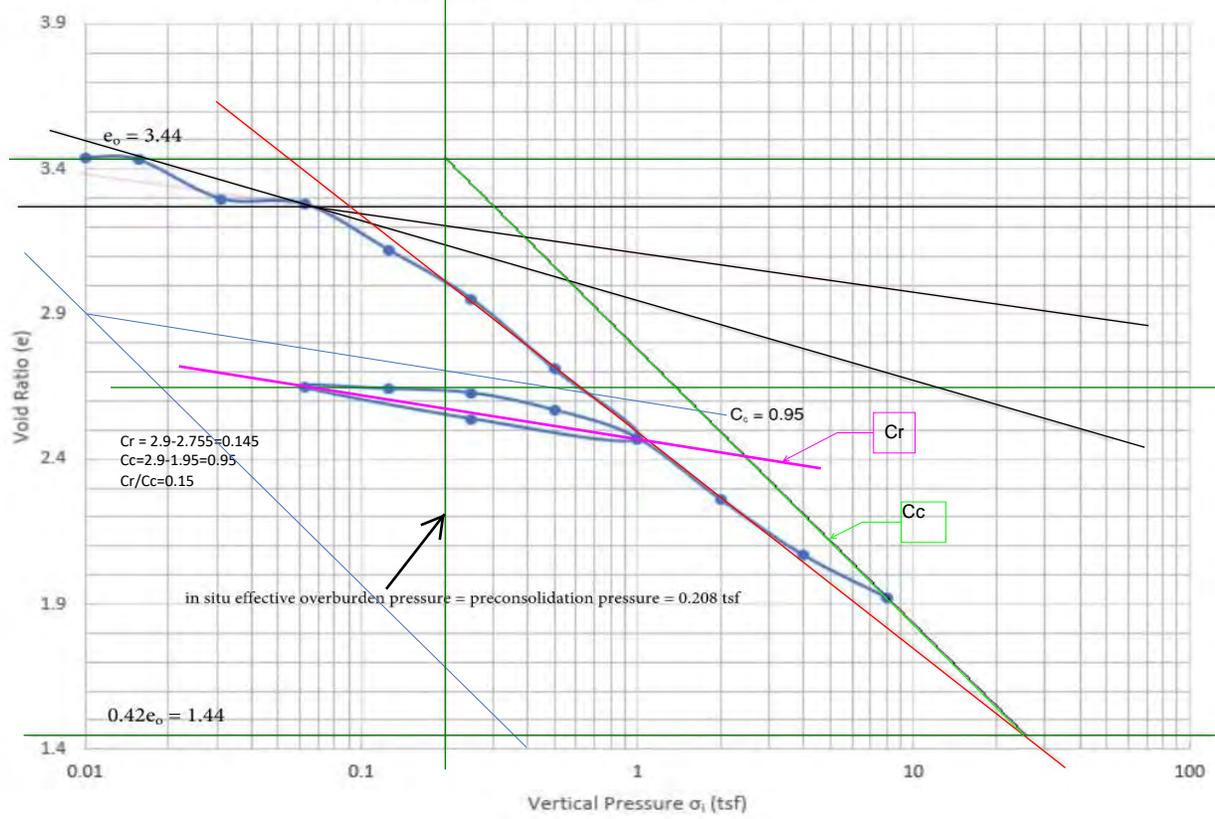
Project Name:	Grand Chenier	Initial Conditions	Final Conditions	EOP= End of Primary Consolidation
File Number:	22-83-3874	Height (in)	0.7500	EOI= End of load increment (typically 24 hrs +/-)
Boring Number:	B-5	w _c (%)	122.1	Specific Gravity
Depth:	6-8	γ _t (pcf)	88.7	83.7
		γ _d (pcf)	39.9	98.1
		Saturation (%)	102.1	53.4
LL = 98	-200 = 99.6	Void ratio, e	3.2613	104.3
PI = 73	OC = --			2.1874
				Ring Diameter (in)
				2.0000
				Ring weight (g)
				62.58
				Height of Solids (in)
				0.1760
				Weight of Dry Soil (g)
				24.70

Setup/Import

Standard Test Method for One Dimensional Consolidation Properties of Soil (ASTM D 2435)

Project Number: 02541395		Liquid Limit: 116	Torvane: 0.025 tsf	MOISTURE DATA		BEFORE	AFTER										
Project Name: Laboratory Test, GeoEngineers		Plastic Limit: 32	% Passing No 200: NA	Tare Weight, gms:		31.45	337.08										
Boring No.: B-1		Plasticity Index: 84	Sample Trimmed by Cutting Shoe, Test Method B	Wet Weight+Tare Weight., gms:		81.80	422.08										
Sample ID, Depth: 12-14'		Sample Classification: Gray; Fat Clay		Dry Weight +Tare Weight., gms:		54.58	387.06										
SAMPLE DATA		Before	After	Assumed Specific Gravity (G):		2.750	Weight of Dry Soil, gms:										
Diameter of Specimen, in.:		2.498	2.498	Mass of Dry Solids Md =(Mf/(1+wf), gms):		49.71	Weight of Water, gms:										
Height of Specimen (Ho, Hf), in.:		0.9990	0.6579	Initial Moisture, Wo = (Mo -Md)/Md:		124.6%	Moisture Content (W'o, W'f), %:										
Height of Specimen (Ho, Hf), cm.:		2.5375	1.6711	Final Moisture, Wf = (Mf - Md)/Md:		70.1%	UNIT WEIGHT										
Area of Specimen, cm ² :		31.619	31.619	Initial Dry Density (Md/Vo), pcf:		38.7	BEFORE										
Volume of Specimen (Vo, Vf), cm ³ :		80.231	52.839	Final Dry Density (Md/Vf), pcf:		58.7	AFTER										
Volume of Specimen, in ³ :		4.896	3.224	Initial Void Ratio, eo = (Ho-Hs)/Hs:		3.4385	Wet Wt. Soil+Ring/Tare, gms:										
Volume of Solids, Vs = Md/(G), cm ³ :		18.076		Final Void Ratio, eo = (Hf-Hs)/Hs:		1.9231	Wt of Ring/Tare, gms:										
Height of Solids, Hs = Vs/A, cm:		0.5717		Initial Degree of Saturation So = (Mo-Md)/(A* (Ho- Hs)), %:		1.00	Wet Mass of Soil (Mo, Mf) ,gms:										
Height of Solids, (Hs), inches:		0.2251		Final Degree of Saturation So = (Mf-Md)/(A* (Hf- Hs)), %:		1.00	Dry Mass of Soil, gms:										
Total Number of Loads (Increments + Decrements)		Average Sample Depth: 13 feet		Remarks: Machine Flexibility Deformation was less than 5% of the Measured Deformation under each load and is not taken into account.													
16		Ground Water Depth: 0 feet															
		Over Burden Pressure: 0.39 tsf															
Description	Vertical Pressure σ _i (tsf)	Machine Flexibility (δ _{mi}) (in.)	Change in Height (δ _{hi}) (in.)	Corrected Change (δ _{hi} -δ _{mi})	Cumulative Change (ΔH) (in.)	Final Sample Height (in.) (H _i =Ho-ΔH)	Height of Voids (in.) (V _v =H _i - Hs)	Void Ratio (e) (V _v /V _s)	Strain ε =ΔH/Ho %	Average Height (in.)	Incremental Strain ε _i %	Incremental Work (tsf) (σ _i +σ _{i+1})*ε _i /2	Work Done per Unit Vol. tsf	t50 (min.)	Cv for t50 (in ² /day)	t90 (min.)	Cv for t90 (in ² /day)
LOADING	0.0100	0.0000	0.0000	0.0000	0.0000	0.9990	0.7739	3.4385	0.0000	-	0.0000	0.0000	0.0000	-	-	-	-
LOADING	0.0156	0.0000	0.0018	0.0018	0.0018	0.9972	0.7722	3.4306	0.0018	0.9981	0.0018	0.0000	0.0000	-	-	-	-
LOADING	0.0312	0.0002	0.0306	0.0304	0.0321	0.9669	0.7418	3.2957	0.0322	0.9821	0.0304	0.0007	0.0007	-	-	-	-
LOADING	0.0625	0.0004	0.0043	0.0039	0.0361	0.9629	0.7379	3.2783	0.0361	0.9649	0.0041	0.0002	0.0009	-	-	-	-
LOADING	0.1250	0.0008	0.0360	0.0353	0.0713	0.9277	0.7026	3.1216	0.0714	0.9453	0.0366	0.0034	0.0044	-	-	-	-
LOADING	0.2500	0.0015	0.0396	0.0381	0.1094	0.8896	0.6645	2.9523	0.1095	0.9086	0.0411	0.0077	0.0121	-	-	-	-
LOADING	0.5000	0.0030	0.0575	0.0545	0.1639	0.8351	0.6100	2.7103	0.1641	0.8623	0.0612	0.0230	0.0350	-	-	-	-
LOADING	1.0000	0.0047	0.0592	0.0546	0.2184	0.7806	0.5555	2.4679	0.2187	0.8078	0.0653	0.0490	0.0840	-	-	-	-
UNLOADING	0.2500	-0.0045	-0.0205	-0.0159	0.2025	0.7965	0.5714	2.5388	0.2027	0.7885	-0.0204	-0.0128	0.0712	-	-	-	-
UNLOADING	0.0625	-0.0027	-0.0272	-0.0245	0.1780	0.8210	0.5959	2.6474	0.1782	0.8087	-0.0307	-0.0048	0.0664	-	-	-	-
LOADING	0.1250	0.0017	0.0030	0.0013	0.1793	0.8197	0.5946	2.6418	0.1795	0.8203	0.0015	0.0001	0.0666	-	-	-	-
LOADING	0.2500	0.0024	0.0056	0.0031	0.1824	0.8166	0.5915	2.6279	0.1826	0.8181	0.0038	0.0007	0.0673	-	-	-	-
LOADING	0.5000	0.0038	0.0169	0.0132	0.1956	0.8034	0.5783	2.5694	0.1958	0.8100	0.0161	0.0061	0.0734	-	-	-	-
LOADING	1.0000	0.0049	0.0265	0.0216	0.2172	0.7818	0.5567	2.4734	0.2174	0.7926	0.0269	0.0202	0.0935	-	-	-	-
LOADING	2.0000	0.0064	0.0540	0.0476	0.2648	0.7342	0.5091	2.2618	0.2651	0.7580	0.0609	0.0914	0.1849	-	-	-	-
LOADING	4.0000	0.0100	0.0535	0.0435	0.3083	0.6907	0.4656	2.0687	0.3086	0.7124	0.0592	0.1776	0.3625	-	-	-	-
LOADING	8.0000	0.0166	0.0494	0.0328	0.3411	0.6579	0.4329	1.9231	0.3414	0.6743	0.0474	0.2846	0.6471	-	-	-	-

Consolidation Test Results B-1 12-14

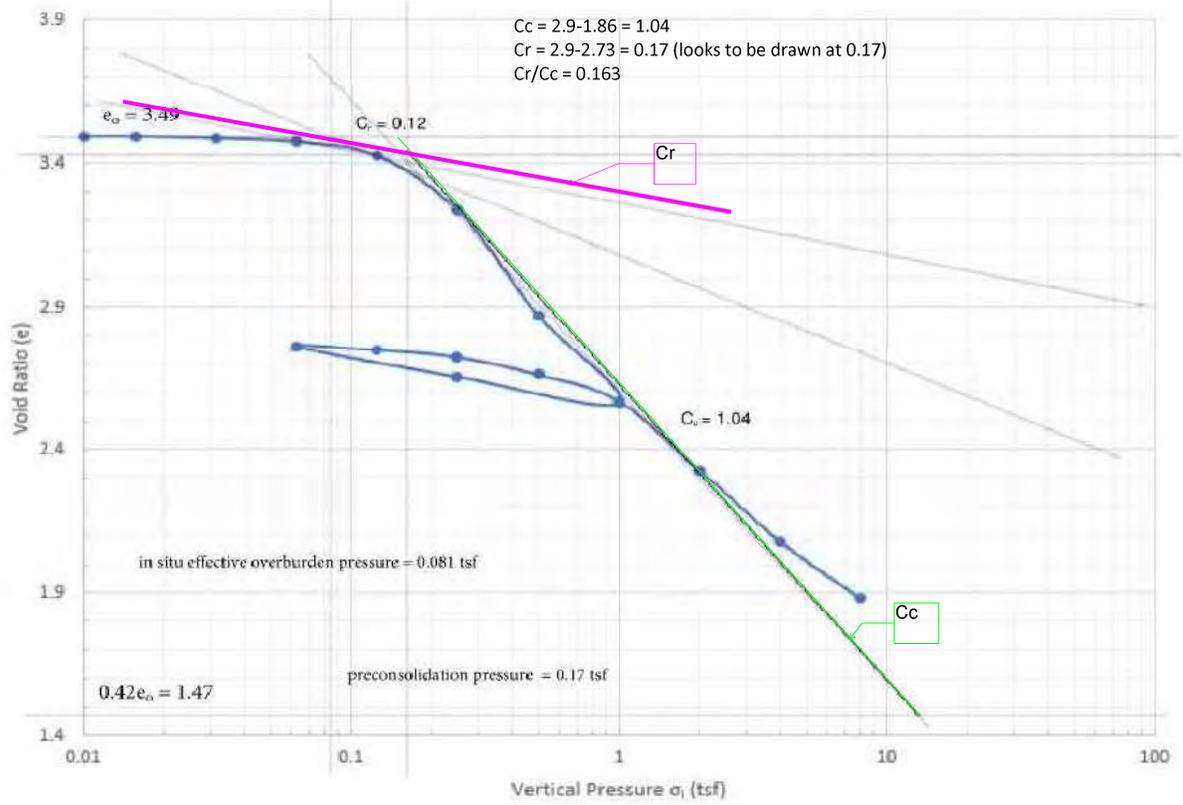


Setup/Import

Standard Test Method for One Dimensional Consolidation Properties of Soil (ASTM D 2435)

Project Number: 02541395		Liquid Limit: 111	Torvane: 0.05 tsf	MOISTURE DATA		BEFORE	AFTER										
Project Name: Laboratory Test, GeoEngineers		Plastic Limit: 31	% Passing No 200: NA	Tare Weight, gms:		31.42	337.50										
Boring No.: B-3		Plasticity Index: 80	Sample Trimmed by Cutting Shoe, Test Method B	Wet Weight+Tare Weight., gms:		83.52	420.12										
Sample ID, Depth: 4-6'		Sample Classification: Gray; Fat Clay		Dry Weight +Tare Weight., gms:		55.90	386.57										
SAMPLE DATA		Before	After	Assumed Specific Gravity (G):		2.750	Weight of Dry Soil, gms:										
Diameter of Specimen, in.:		2.499	2.499	Mass of Dry Solids Md =(Mf/(1+wf), gms):		49.09	Weight of Water, gms:										
Height of Specimen (Ho, Hf), in.:		0.9980	0.6397	Initial Moisture, Wo = (Mo -Md)/Md:		121.8%	Moisture Content (W'o, W'f), %:										
Height of Specimen (Ho, Hf), cm.:		2.5349	1.6248	Final Moisture, Wf = (Mf - Md)/Md:		68.4%	UNIT WEIGHT										
Area of Specimen, cm ² :		31.644	31.644	Initial Dry Density (Md/Vo), pcf:		38.2	BEFORE										
Volume of Specimen (Vo, Vf), cm ³ :		80.215	51.415	Final Dry Density (Md/Vf), pcf:		59.6	AFTER										
Volume of Specimen, in ³ :		4.895	3.138	Initial Void Ratio, eo = (Ho-Hs)/Hs:		3.4938	Wet Wt. Soil+Ring/Tare, gms:										
Volume of Solids, Vs = Md/(G), cm ³ :		17.850		Final Void Ratio, eo = (Hf-Hs)/Hs:		1.8803	Wt of Ring/Tare, gms:										
Height of Solids, Hs = Vs/A, cm:		0.5641		Initial Degree of Saturation So = (Mo-Md)/(A* (Ho- Hs)), %:		0.96	Wet Mass of Soil (Mo, Mf) ,gms:										
Height of Solids, (Hs), inches:		0.2221		Final Degree of Saturation So = (Mf-Md)/(A* (Hf- Hs)), %:		1.00	Dry Mass of Soil, gms:										
Total Number of Loads (Increments + Decrements)		Average Sample Depth: 5 feet		Remarks: Machine Flexibility Deformation was less than 5% of the Measured Deformation under each load and is not taken into account.													
16		Ground Water Depth: 0 feet															
		Over Burden Pressure: 0.15 tsf															
Description	Vertical Pressure σ _i (tsf)	Machine Flexibility (δ _{mi}) (in.)	Change in Height (δ _{hi}) (in.)	Corrected Change (δ _{hi} -δ _{mi})	Cumulative Change (ΔH) (in.)	Final Sample Height (H _i =Ho-ΔH)	Height of Voids (in.) (V _v =H _i - Hs)	Void Ratio (e) (V _v /V _s)	Strain ε =ΔH/Ho %	Average Height (in.)	Incremental Strain ε _i ,%	Incremental Work (tsf) (σ _i +σ _{i+1})*ε _i /2	Work Done per Unit Vol. tsf	t50 (min.)	Cv for t50 (in ² /day)	t90 (min.)	Cv for t90 (in ² /day)
LOADING	0.0100	0.0000	0.0000	0.0000	0.0000	0.9980	0.7759	3.4938	0.0000	-	0.0000	0.0000	0.0000	-	-	-	-
LOADING	0.0156	0.0000	0.0000	0.0000	0.0000	0.9980	0.7759	3.4938	0.0000	0.9980	0.0000	0.0000	0.0000	-	-	-	-
LOADING	0.0312	0.0000	0.0016	0.0015	0.0015	0.9965	0.7744	3.4869	0.0015	0.9972	0.0015	0.0000	0.0000	-	-	-	-
LOADING	0.0625	0.0000	0.0028	0.0028	0.0043	0.9937	0.7716	3.4743	0.0043	0.9951	0.0028	0.0001	0.0002	-	-	-	-
LOADING	0.1250	0.0000	0.0104	0.0104	0.0147	0.9833	0.7612	3.4274	0.0148	0.9885	0.0105	0.0010	0.0012	-	-	-	-
LOADING	0.2500	0.0006	0.0432	0.0426	0.0573	0.9407	0.7186	3.2358	0.0574	0.9620	0.0433	0.0081	0.0093	-	-	-	-
LOADING	0.5000	0.0007	0.0821	0.0814	0.1387	0.8593	0.6372	2.8692	0.1390	0.9000	0.0865	0.0325	0.0417	-	-	-	-
LOADING	1.0000	0.0017	0.0696	0.0679	0.2066	0.7914	0.5693	2.5634	0.2070	0.8253	0.0790	0.0593	0.1010	-	-	-	-
UNLOADING	0.2500	-0.0018	-0.0219	-0.0201	0.1865	0.8115	0.5894	2.6538	0.1869	0.8014	-0.0254	-0.0159	0.0851	-	-	-	-
UNLOADING	0.0625	-0.0006	-0.0241	-0.0236	0.1630	0.8350	0.6129	2.7600	0.1633	0.8232	-0.0291	-0.0045	0.0806	-	-	-	-
LOADING	0.1250	0.0000	0.0027	0.0027	0.1657	0.8323	0.6102	2.7477	0.1660	0.8337	0.0033	0.0003	0.0809	-	-	-	-
LOADING	0.2500	0.0002	0.0059	0.0057	0.1714	0.8266	0.6045	2.7220	0.1718	0.8294	0.0069	0.0013	0.0822	-	-	-	-
LOADING	0.5000	0.0007	0.0143	0.0136	0.1850	0.8130	0.5909	2.6607	0.1854	0.8198	0.0165	0.0062	0.0884	-	-	-	-
LOADING	1.0000	0.0016	0.0219	0.0203	0.2053	0.7927	0.5706	2.5693	0.2057	0.8028	0.0250	0.0187	0.1071	-	-	-	-
LOADING	2.0000	0.0011	0.0545	0.0535	0.2588	0.7392	0.5171	2.3285	0.2593	0.7660	0.0675	0.1012	0.2083	-	-	-	-
LOADING	4.0000	0.0020	0.0576	0.0556	0.3144	0.6836	0.4615	2.0781	0.3150	0.7114	0.0752	0.2257	0.4340	-	-	-	-
LOADING	8.0000	0.0037	0.0476	0.0439	0.3583	0.6397	0.4176	1.8803	0.3590	0.6616	0.0642	0.3855	0.8195	-	-	-	-

Consolidation Test Results B-3 4-6



V1-V6 Composite Low Stress Consolidation Tests Summary

Low stress consolidation tests were performed for V1-V6 Composite sample following the method in the U.S. Army Corps of Engineers Manual No. 1110-2-5027 (USACE, 1987) and the University of Texas Method (Pederson, 2001). To simplify sample preparation, each composite sample was diluted to a moisture content approximately three times its liquid limit to allow free flow of the soil. Per CPRA's request, we used three different moistures contents; 340 percent, 370 percent and 400 percent. One-dimensional incremental loading was used to consolidate the samples, with stresses ranging from about 1 pound per square foot (psf) to 640 psf, with stress doubling between each load increment. The coefficient of consolidation was determined using the square root of time method, and hydraulic conductivity was determined at t_{90} .

The results of each low-stress consolidation test are summarized below in the tables and charts. The charts presented in this document include best-fit logarithmic trend lines with correlation equations and correlation strength indicated on the plot.

Table 1. Definition of Symbols

Symbol	Definition
$\sigma'v$	Vertical effective stress
δ_{100}	Deformation at t_{100}
e_0	Initial void ratio
e_{100}	Void ratio at t_{100}
ϵ_{100}	Strain at t_{100}
C_c	Virgin compression index
$\Delta e(C_\alpha)$	Change in void ratio based on Secondary Compression
t_{90}	Time for 90% consolidation
t_{100}	Time for 100% consolidation
Hdr	Vertical drainage distance
C_v	Coefficient of consolidation (vertical)
K	Permeability

TABLE 2. MC TARGET 340% RESULTS

σ'_v (psf)	δ_{100} (in)	e_{100}	ϵ_{100} (%)	$\Delta e(C_\alpha)$	t90 (min)	Hdr (in)	Cv (ft ² /day)	K (ft/day)
0.93	0.215	8.133	21.35	0.58	961	0.444	0.0017	0.0279
1.83	0.245	7.783	24.37	0.09	1225	0.381	0.0010	0.0027
5.01	0.346	6.622	34.36	0.42	967	0.346	0.0010	0.0029
10.01	0.406	5.928	40.34	0.18	529	0.306	0.0015	0.0018
20.03	0.472	5.170	46.87	0.13	784	0.276	0.0008	0.0006
30	0.491	4.953	48.74	0.04	462	0.256	0.0012	0.0001
40	0.506	4.780	50.22	0.05	484	0.250	0.0011	0.0002
80	0.557	4.189	55.32	0.07	169	0.233	0.0027	0.0005
160	0.602	3.674	59.75	0.06	144	0.209	0.0026	0.0002
320	0.638	3.261	63.31	0.05	81	0.188	0.0037	0.0001
640	0.671	2.876	66.62	0.04	49	0.171	0.0051	0.0001

Note: $e_0 = 10.613$ and $C_c = 1.927$

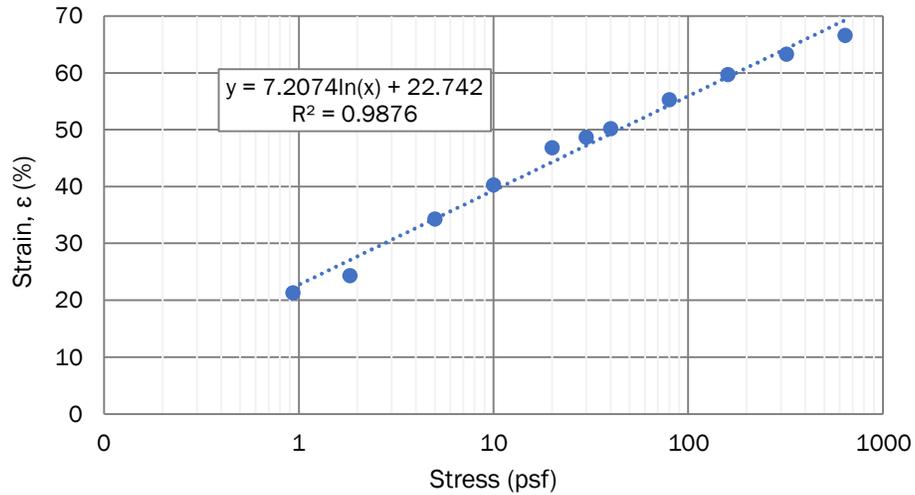


Figure F-1a. Target 340% Axial Strain vs. Stress

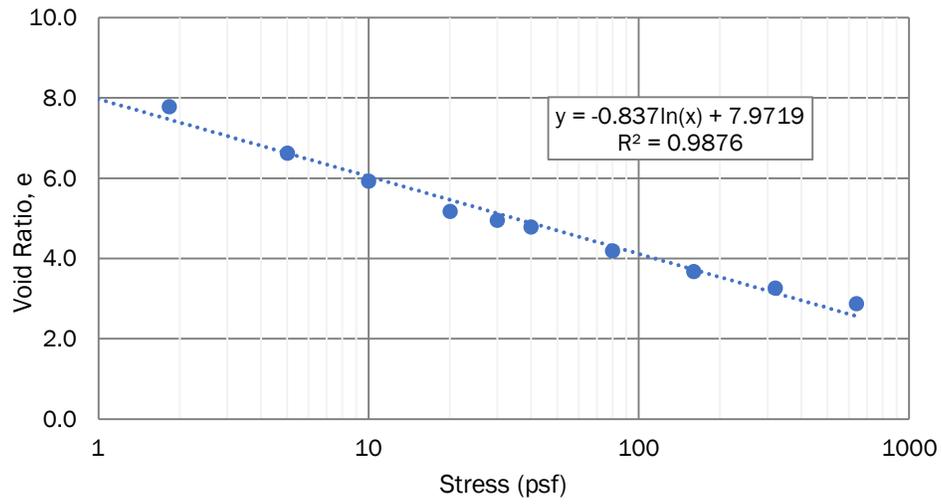


Figure F-1b. Target 340% Void Ratio vs. Stress

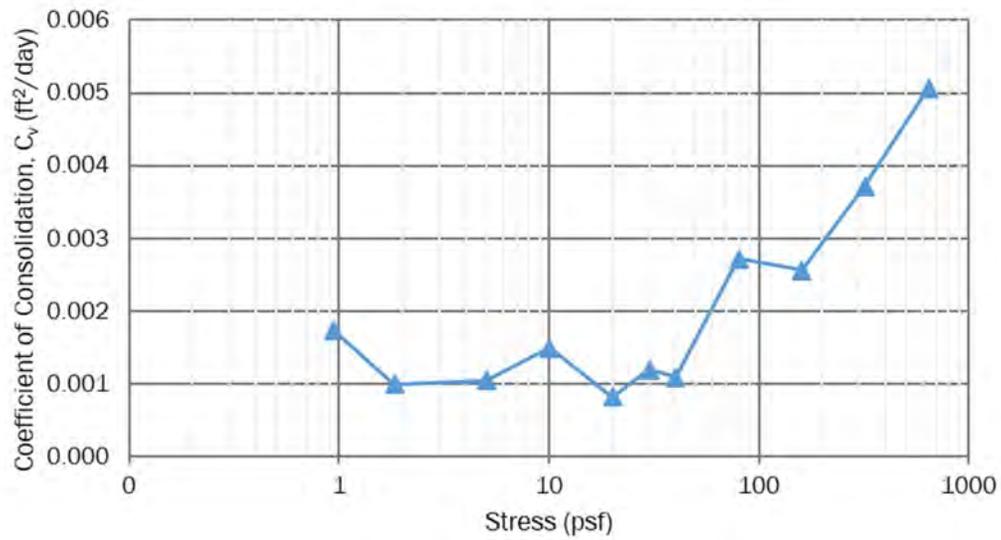


Figure F-1c. Target 340% Coefficient of Consolidation vs. Stress

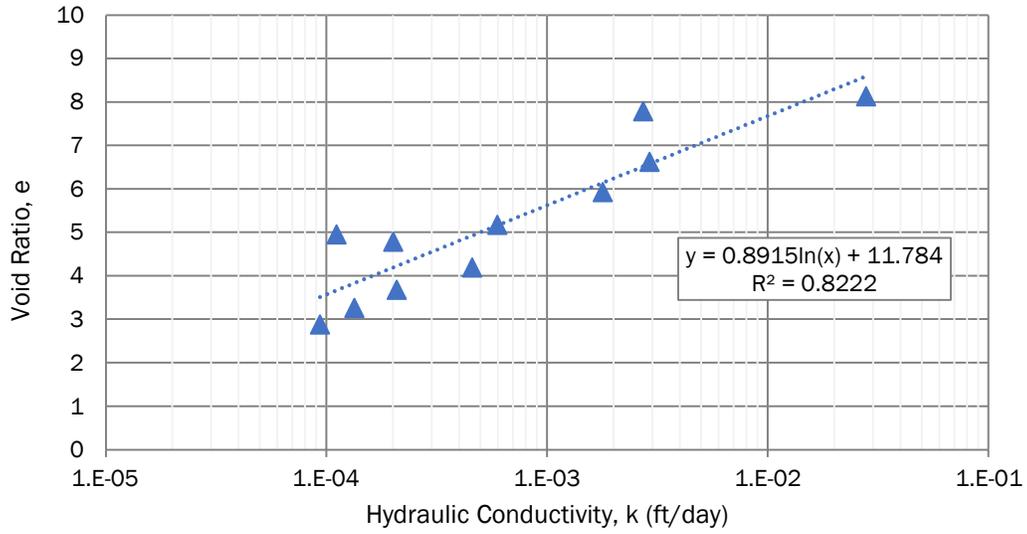


Figure F-1d. Target 340% Void Ratio vs. Hydraulic Conductivity

TABLE 3. MC TARGET 370% RESULTS

$\sigma'v$ (psf)	$\delta 100$ (in)	$e 100$	$\epsilon 100$ (%)	$\Delta e(C_\alpha)$	$t 90$ (min)	Hdr (in)	C_v (ft ² /day)	K (ft/day)
2.00	0.321	6.226	32.07	0.68	1444	0.420	0.0010	0.0123
5.00	0.430	5.068	42.96	0.28	729	0.312	0.0011	0.0041
10.00	0.500	4.320	49.99	0.21	484	0.268	0.0013	0.0021
20.00	0.552	3.764	55.21	0.08	462	0.237	0.0010	0.0007
50.00	0.619	3.056	61.88	0.07	196	0.207	0.0019	0.0006
100	0.662	2.597	66.19	0.04	169	0.180	0.0016	0.0002
500	0.761	1.542	76.10	0.01	49	0.133	0.0031	0.0001
1000	0.799	1.143	79.86	0.02	30	0.110	0.0034	0.0001

Note: $e_0 = 9.638$ and $C_c = 1.817$

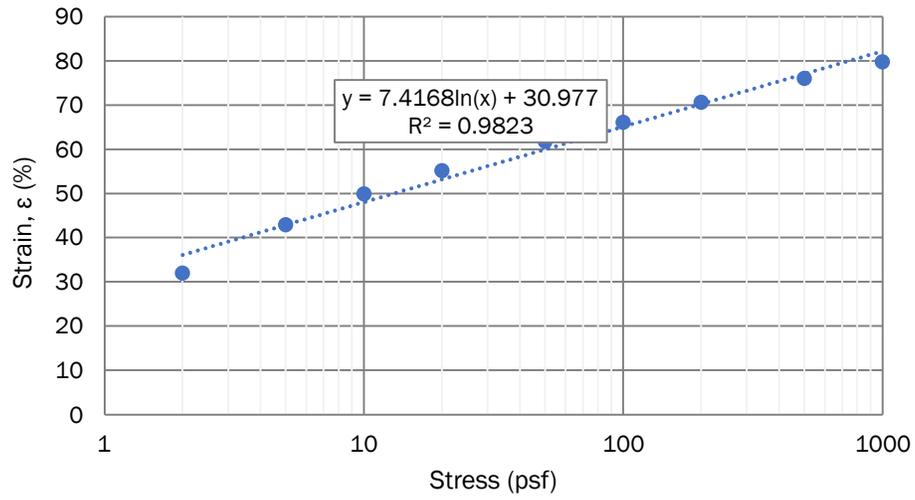


Figure F-2a. Target 370% Axial Strain vs. Stress

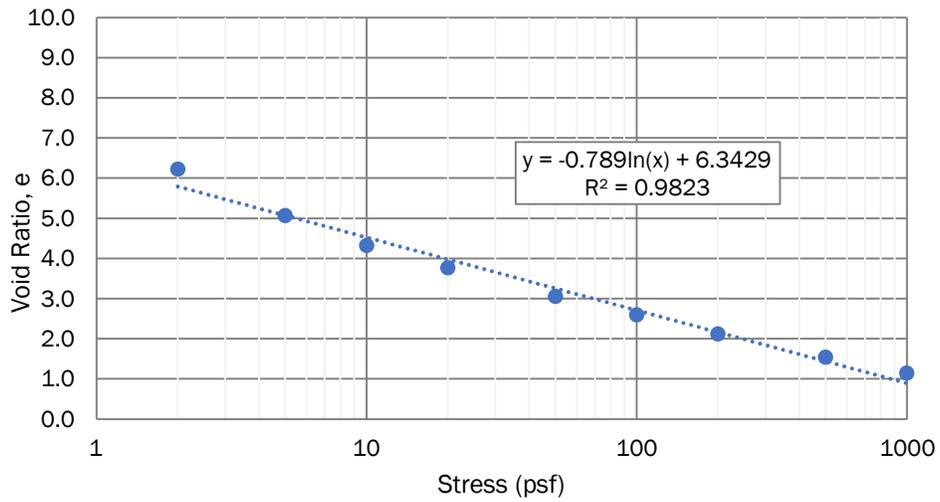


Figure F-2b. Target 370% Void Ratio vs. Stress

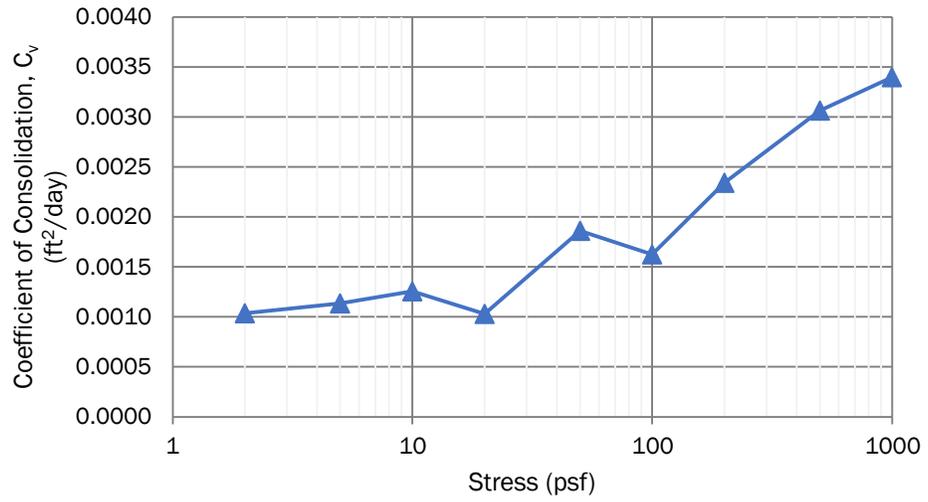


Figure F-2c. Target 370% Coefficient of Consolidation vs. Stress

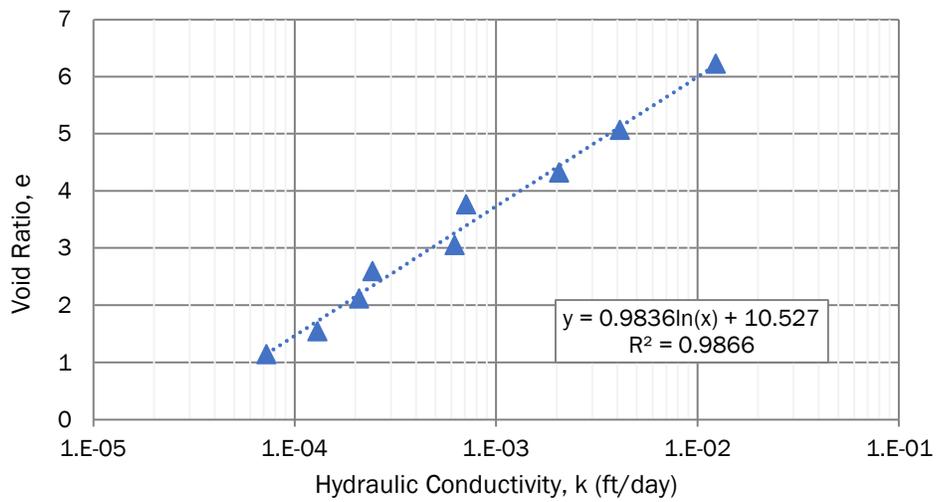


Figure F-2d. Target 370% Void Ratio vs. Hydraulic Conductivity

TABLE 4. MC TARGET 400% RESULTS

$\sigma'v$ (psf)	$\delta 100$ (in)	$e100$	$\epsilon 100$ (%)	$\Delta e(C\alpha)$	t90 (min)	Hdr (in)	Cv (ft ² /day)	K (ft/day)
0.97	0.180	9.121	18.00	0.68	2025	0.446	0.0008	0.0111
2.01	0.265	8.072	26.50	0.37	2209	0.370	0.0005	0.0034
5.00	0.416	6.203	41.64	0.72	1681	0.316	0.0005	0.0024
10.00	0.482	5.397	48.17	0.16	1156	0.264	0.0005	0.0008
20	0.589	4.073	58.90	0.28	625	0.222	0.0007	0.0010
30	0.622	3.663	62.22	0.02	400	0.188	0.0008	0.0001
40	0.649	3.327	64.94	0.10	317	0.180	0.0009	0.0004
80	0.700	2.699	70.03	0.07	225	0.161	0.0010	0.0002
160	0.748	2.108	74.82	0.07	121	0.136	0.0013	0.0002
320	0.785	1.659	78.46	0.03	81	0.115	0.0014	0.0001
640	0.802	1.438	80.25	0.01	25	0.103	0.0036	0.0001

Note: $e_0 = 11.343$ and $C_c = 2.811$

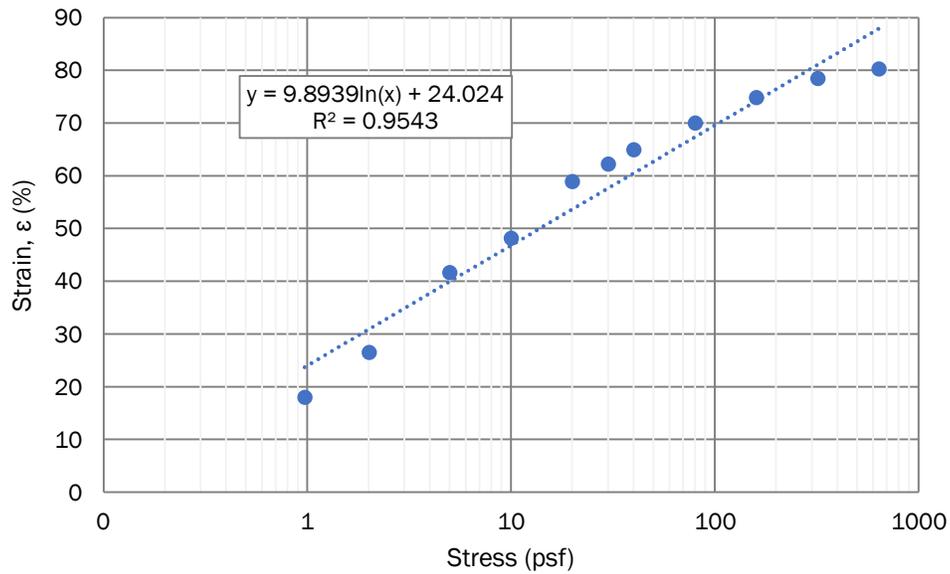


Figure F-3a. Target 400% Axial Strain vs. Stress

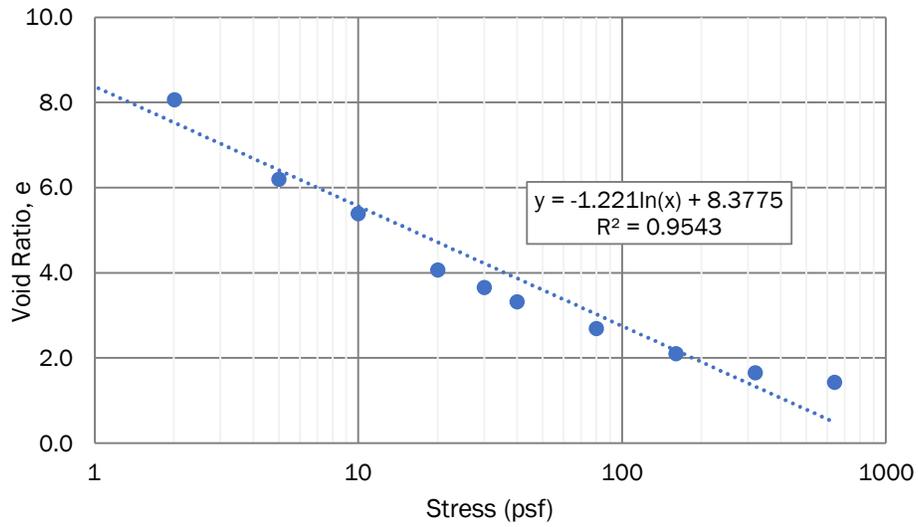


Figure F-3b. Target 400% Void Ratio vs. Stress

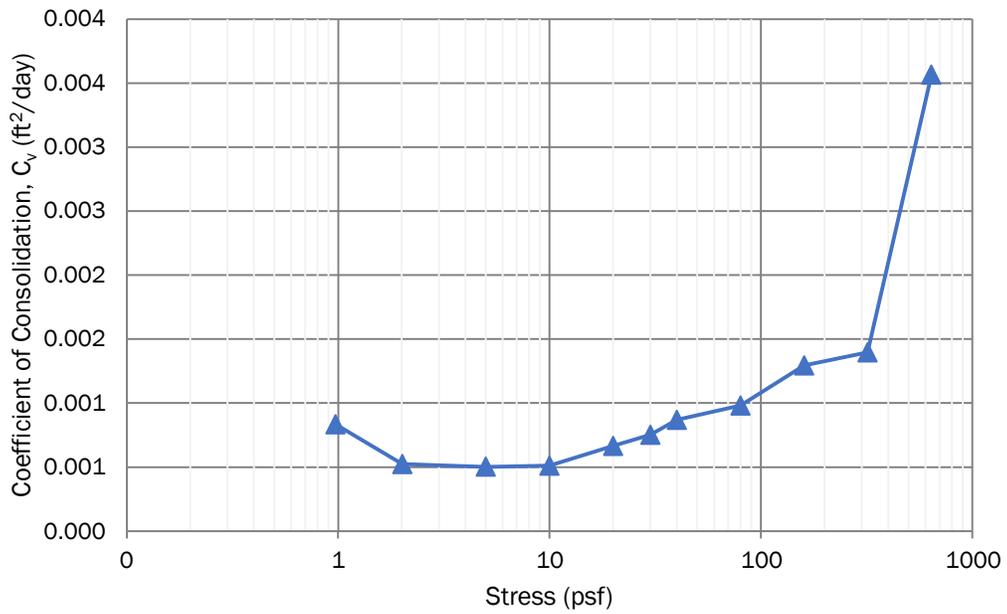


Figure F-3c. Target 400% Coefficient of Consolidation vs. Stress

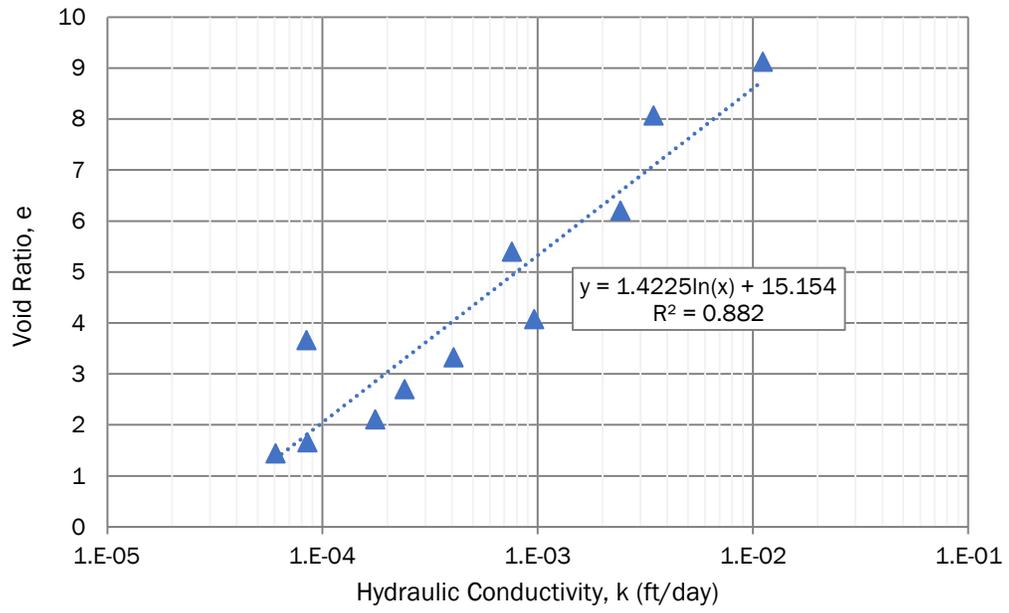
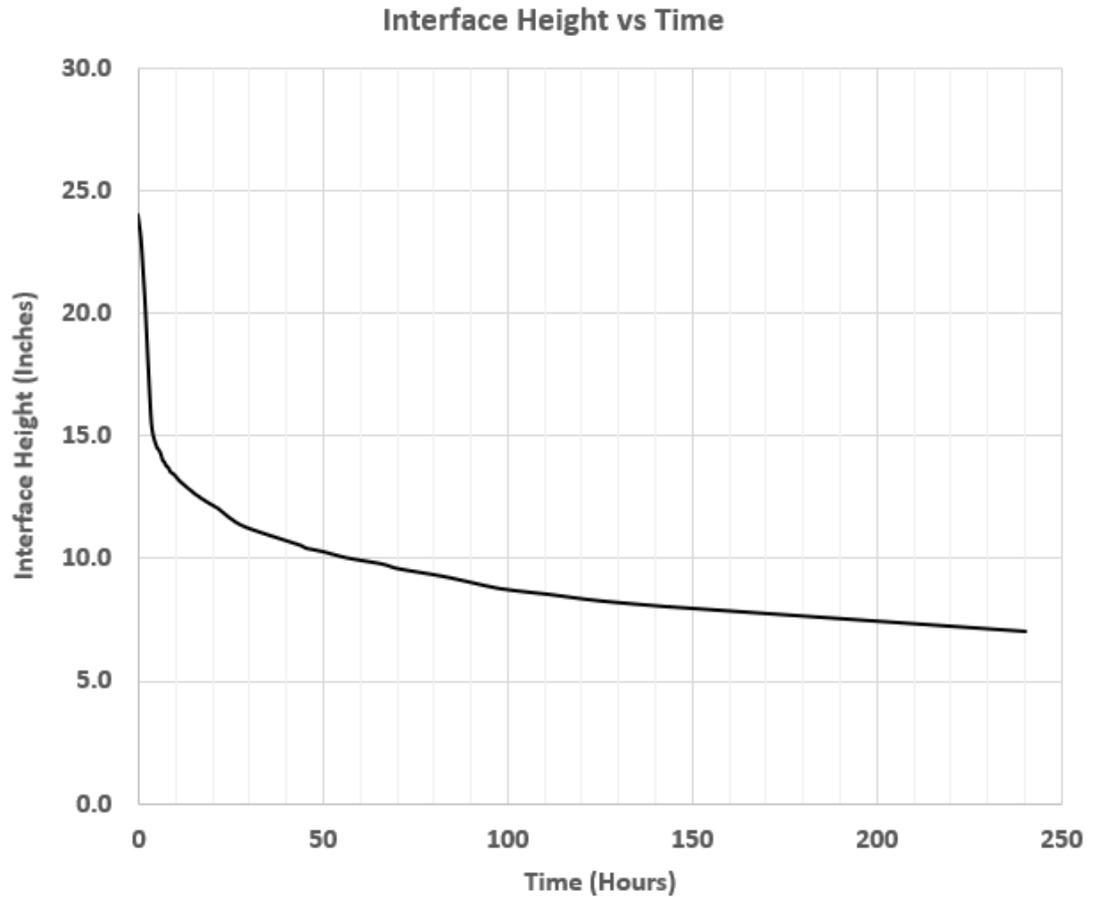


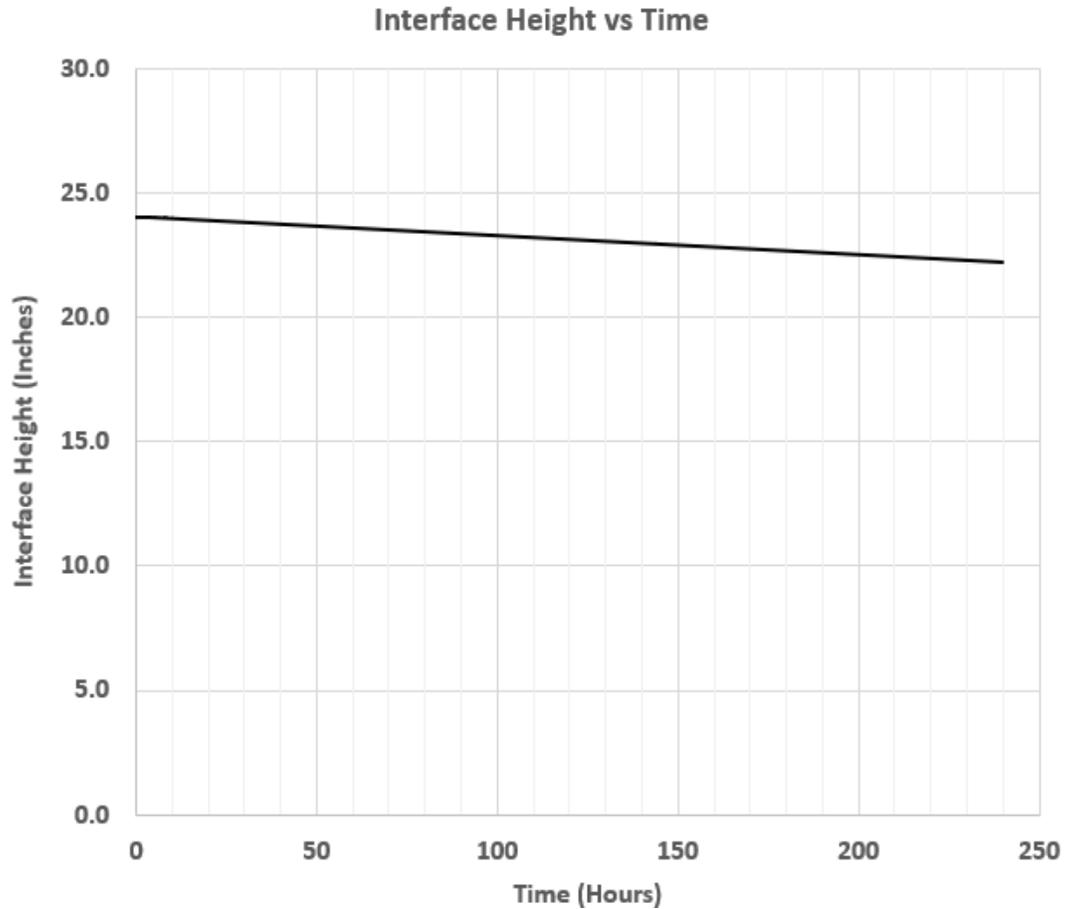
Figure F-3d. Target 400% Void Ratio vs. Hydraulic Conductivity

Time (hours)	Interface Height (inches)
0.0	24.0
0.8	23.0
1.5	21.5
2.0	20.3
3.2	16.8
3.8	15.3
5.2	14.5
5.7	14.4
6.2	14.3
6.7	14.0
7.2	13.9
7.5	13.8
7.8	13.8
8.0	13.7
8.3	13.7
8.5	13.6
8.8	13.5
9.8	13.4
10.3	13.3
11.2	13.2
12.3	13.0
15.5	12.6
19.0	12.3
21.8	12.0
24.7	11.7
29.2	11.3
44.2	10.5
45.3	10.4
50.2	10.3
56.5	10.0
66.0	9.8
69.2	9.6
72.5	9.5
82	9.3
90	9.0
98	8.8
106	8.6
112	8.5
125	8.3
144	8.0
144	8.0
192	7.5
240	7.0



Initial Slurry % Solids: 9.5
Testing Method: Settling without Dessication
Composite Depth Range: 0-10 feet
Sample Description: Gray Fat Clay
Percent Sand Fraction: 0.3
Percent Clay Fraction: 82.7
Percent Silt Fraction: 16.9
Liquid Limit: 92
Plastic Limit: 30
Plasticity Index: 62
Specific Gravity: N/A
Organic Content: N/A
Diameter of Cylinder (in.): 7.5
Initial Slurry Height (in.): 24.0
Final Interface Height (in.): 7.0
Final Water Height (in.): 24
Desiccation Crust Thickness (in.): No Dessication
Zone Settling Velocity (feet/day): 5.4
Solids Concentration in Compression Settling: $y = -2.099\ln(x) + 18.451$
Note: Where y is solids concentration in grams per liter and x is time in hours

Time (hours)	Interface Height (inches)
0.0	24.0
0.8	24.0
1.5	24.0
2.0	24.0
3.2	24.0
3.8	24.0
5.2	24.0
5.7	24.0
6.2	24.0
6.7	24.0
7.2	24.0
7.5	24.0
7.8	24.0
8.0	24.0
8.3	24.0
8.5	24.0
8.8	24.0
9.8	24.0
10.3	24.0
11.2	23.9
12.3	23.9
15.5	23.9
19.0	23.9
21.8	23.9
24.7	23.8
29.2	23.8
44.2	23.7
45.3	23.7
50.2	23.6
56.5	23.6
66.0	23.5
69.2	23.5
72.5	23.5
82	23.4
90	23.3
98	23.3
106	23.2
112	23.2
125	23.1
144	22.9
144	22.9
192	22.6
240	22.2



Initial Slurry % Solids: 25.2
Testing Method: Settling without Dessication
Composite Depth Range: 0-10 feet
Sample Description: Gray Fat Clay
Percent Sand Fraction: 0.3
Percent Clay Fraction: 82.7
Percent Silt Fraction: 16.9
Liquid Limit: 92
Plastic Limit: 30
Plasticity Index: 62
Specific Gravity: N/A
Organic Content: N/A
Diameter of Cylinder (in.): 7.5
Initial Slurry Height (in.): 24.0
Final Interface Height (in.): 22.2
Final Water Height (in.): 24
Desiccation Crust Thickness (in.): No Dessication
Zone Settling Velocity (feet/day): N/A
Solids Concentration in Compression Settling: $y = -0.274\ln(x) + 24.592$
Note: Where y is solids concentration in grams per liter and x is time in hours

APPENDIX F
Elevation Documentation

Project Name:	South Grand Chenier - Baker Marsh Creation (ME-32)			
Survey data reduction				
Completed by	DSE	Date	2/8/2023	
Checked by	Nafi	Date	2/8/2023	

From Fugro survey, the top of the PVC water gauge pole was set at El. 5.609 ft

From CRMS Sta. 0614-H01, during period of our soil borings, the water elevation range was from 0.3 to 0.45 ft. (about 0.15' variance max)

From field report, the distance from the top of the PVC pole to the water surface was taken each morning (no afternoon measurements recorded)

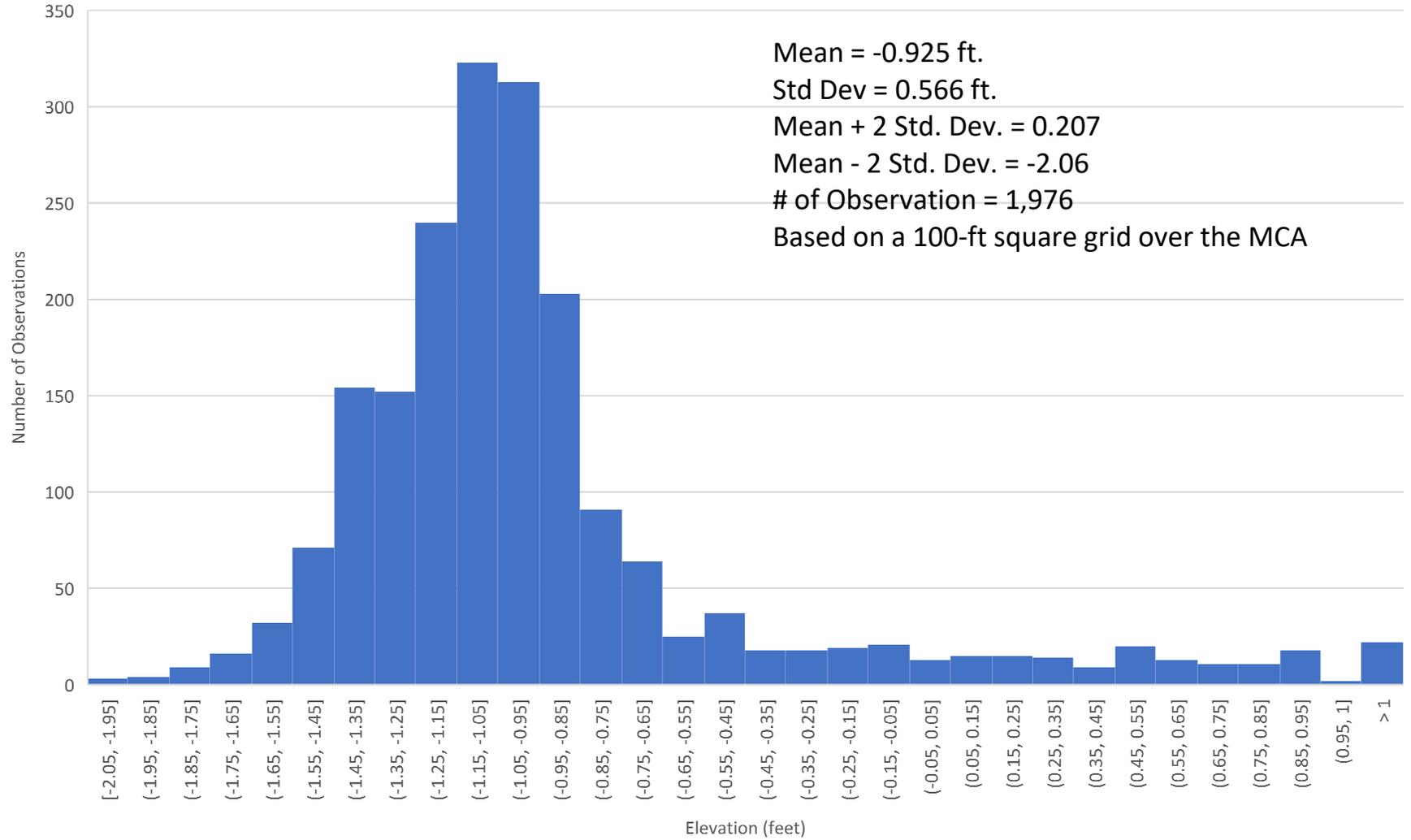
Date	Time	Dist. From top of PVC to water (ft)	Top of PVC pole El (ft)	Water El Ft
12-Oct	10:05	5.25	5.609	0.359
13-Oct	8:35	5.17	5.609	0.439
14-Oct	11:40	5.17	5.609	0.439
15-Oct	7:50	5.25	5.609	0.359

average water elevation of 0.4 ft seems appropriate

check mudline elevations against survey

Borehole/ CPT No	Elevation reported by Fugro	Measured water depth at location (ft)	Water ele (ft)	Mudline El (ft)
B-1	-1.61	2.33	0.4	-1.93
B-2/C-2	-1.28	1.58	0.4	-1.18
B-3	-1.24	1.67	0.4	-1.27
B-4	-1.3	1.83	0.4	-1.43
B-5/C-5	-1.55	1.83	0.4	-1.43
B-6	-1.46	1.83	0.4	-1.43
C-1 (47)	0.71	1.67	0.4	-1.27
C-2	-1.28	3	0.4	-2.6
C-3 (41)	0.71	1.92	0.4	-1.52
C-4 (40)	0.77	1.42	0.4	-1.02
C-5	-1.55	3.83	0.4	-3.43
C-6 (46)	0.05	2	0.4	-1.6
C-7 (45)	0.12	1.5	0.4	-1.1
C-8 (44)	-0.39	1.5	0.4	-1.1
C-9 (48)	2.76	1.75	0.4	-1.35
C-10 (43)	-0.33	2.75	0.4	-2.35
C-11 (42)	-0.49	1.67	0.4	-1.27
C-12 (49)	-0.27	2.33	0.4	-1.93
C-13 (50)	0.09	2	0.4	-1.6

Elevation Histogram



Water Surface Elevation



CRMS0614-H01 GEOID12A

September 25 2022 - October 24 2022
Data Source: Continuous Hourly Observations



David S. Eley

From: Barnes, Breese - FPAC-NRCS, Alexandria, LA <Breese.Barnes@usda.gov>
Sent: Wednesday, January 25, 2023 9:11 AM
To: Dale Garber
Cc: McCoy, Nicholas - FPAC-NRCS, Lafayette, LA; David S. Eley; Boustany, Ron - NRCS, Lafayette, LA
Subject: RE: [External Email]FW: marsh fill question
Attachments: ME-32 Topographic Survey Data - GEOID 12A.dwg

[EXTERNAL]

Gentlemen,

Following up on the meeting this morning, attached are the survey points converted to Geoid 12A as well as an updated containment dike profile. Mean elevation of the marsh creation area in this geoid is -0.929'.

Additionally, on the set of settlement curves with the 95% confidence interval the target elevation at Year 20 should be 0.80', not 1.80'.

Let me know if you have any more questions or concerns.

Thanks,
Breese

From: Dale Garber <dgarber@ecmconsultants.com>
Sent: Monday, January 23, 2023 2:27 PM
To: Barnes, Breese - FPAC-NRCS, Alexandria, LA <Breese.Barnes@usda.gov>
Cc: McCoy, Nicholas - FPAC-NRCS, Lafayette, LA <Nicholas.McCoy@usda.gov>; David S. Eley <deley@geoengineers.com>
Subject: RE: [External Email]FW: marsh fill question

Breese,

Can we do the meeting at about 8:30 am on Wednesday?

Dale J. Garber

Project Manager

ECM Consultants, Inc.

120 Rue Beauregard, Suite 120

Lafayette, LA 70508

(504) 885-4080 (ext. 402)

(337)581-9078 CELL

Email: dgarber@ecmconsultants.com

web: www.ecmconsultants.com



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From: David S. Eley <deley@geoengineers.com>
Sent: Monday, January 23, 2023 1:39 PM

David S. Eley

From: Barnes, Breese - FPAC-NRCS, Alexandria, LA <Breese.Barnes@usda.gov>
Sent: Tuesday, January 31, 2023 5:07 PM
To: David S. Eley; Dale Garber; McCoy, Nicholas - FPAC-NRCS, Lafayette, LA
Cc: Boustany, Ron - NRCS, Lafayette, LA; Kennedy, Natasha - FPAC-FBC, Fort Worth, TX; Nafi Haque; Denzel N. Flores Cubillas
Subject: RE: [External Email]RE: ME-32 Geotech Lab Discussion

[EXTERNAL]

Dave,

Yes those numbers for Y20 target elevation, Sea Level Rise, Subsidence, and Accretion listed below are correct. Thank you for double checking.

Thanks,
Breese

From: David S. Eley <deley@geoengineers.com>
Sent: Tuesday, January 31, 2023 4:52 PM
To: Barnes, Breese - FPAC-NRCS, Alexandria, LA <Breese.Barnes@usda.gov>; Dale Garber <dgarber@ecmconsultants.com>; McCoy, Nicholas - FPAC-NRCS, Lafayette, LA <Nicholas.McCoy@usda.gov>
Cc: Boustany, Ron - NRCS, Lafayette, LA <ron.boustany@usda.gov>; Kennedy, Natasha - FPAC-FBC, Fort Worth, TX <Natasha.Kennedy@usda.gov>; Nafi Haque <nhaque@geoengineers.com>; Denzel N. Flores Cubillas <dflores@geoengineers.com>
Subject: RE: [External Email]RE: ME-32 Geotech Lab Discussion

Breese & Dale,

Below is an email we received on 12/13/2022. I noticed the highlighted values are different from those in the 4-48-2022 SOS. We will use the numbers below, unless notified otherwise.

The elevation information is outdated, but I'm assuming the Sea Level Rise, Subsidence and Accretion are still correct.

Thanks,
Dave

From: Barnes, Breese - FPAC-NRCS, Alexandria, LA <Breese.Barnes@usda.gov>
Sent: Tuesday, December 13, 2022 8:19 AM
To: Dale Garber <dgarber@ecmconsultants.com>; McCoy, Nicholas - FPAC-NRCS, Lafayette, LA <Nicholas.McCoy@usda.gov>
Cc: Boustany, Ron - NRCS, Lafayette, LA <ron.boustany@usda.gov>; Kennedy, Natasha - FPAC-FBC, Fort Worth, TX <Natasha.Kennedy@usda.gov>; David S. Eley <deley@geoengineers.com>; Nafi Haque <nhaque@geoengineers.com>
Subject: RE: [External Email]RE: ME-32 Geotech Lab Discussion

[EXTERNAL]

Dale,

Attached is a CAD file containing the topographic survey data for ME-32. Included is a preliminary profile of the containment dike alignment. One thing to note is that these surveys were performed before the landowners constructed a levee on the entire western border of the project. This levee is currently built to an elevation of approximately +2.0 feet.

The average elevation in the MCA is slightly higher, but -0.5 feet is probably safe to use for the existing mudline elevation of the fill area. Target elevation at Y20 is the 10% inundation level, which in this area is +0.756 feet.

With regards to subsidence and accretion we would like to have three different scenarios run for the settlement analysis if possible. One would include no subsidence or accretion, one would include subsidence over the entire project life, and the last would include subsidence over the entire project life as well as accretion applied beginning Year 6 of the project life. Values for these parameters are listed below.

- Sea Level Rise: 0.026 feet/year
- Subsidence: 4.3 mm/year
- Accretion: 2.5 mm/year

If you have any questions please let me know.

Thanks,
Breese

From: Dale Garber <dgarber@ecmconsultants.com>

Sent: Wednesday, December 7, 2022 9:29 AM

To: Barnes, Breese - FPAC-NRCS, Alexandria, LA <Breese.Barnes@usda.gov>; McCoy, Nicholas - FPAC-NRCS, Lafayette, LA <Nicholas.McCoy@usda.gov>

Cc: Boustany, Ron - NRCS, Lafayette, LA <ron.boustany@usda.gov>; Kennedy, Natasha - FPAC-FBC, Fort Worth, TX <Natasha.Kennedy@usda.gov>; David S. Eley <deley@geoengineers.com>; Nafi Haque <nhaque@geoengineers.com>

Subject: [External Email]RE: ME-32 Geotech Lab Discussion

[External Email]

If this message comes from an **unexpected sender** or references a **vague/unexpected topic**;

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Breese,

As a follow-up to the email with the video Dave Eley sent on Monday, there are a couple options that we could pursue on the Low Stress Consolidation test:

1. Try at a lower moisture – say 400%
2. Try at same moisture, but let the sample sit for a day before we try to place screen and LVDT

It does take some effort/time to mix a sample and set up the test. Each failed attempt delays us 3-4 days

Let us know how NRCS would like us to proceed with this test.

Also, is it possible to get some of the Topographic survey data of the Marsh Creation Area (MCA) to assist in the analysis of the Earthen Containment Dikes?

We would need the following information:

1. Existing mudline elevation for design of containment dikes.
2. Existing mudline elevation for design of the marsh fill area

APPENDIX G
Earthen Containment Dike Slope Stability and
Bearing Capacity Evaluations

APPENDIX G

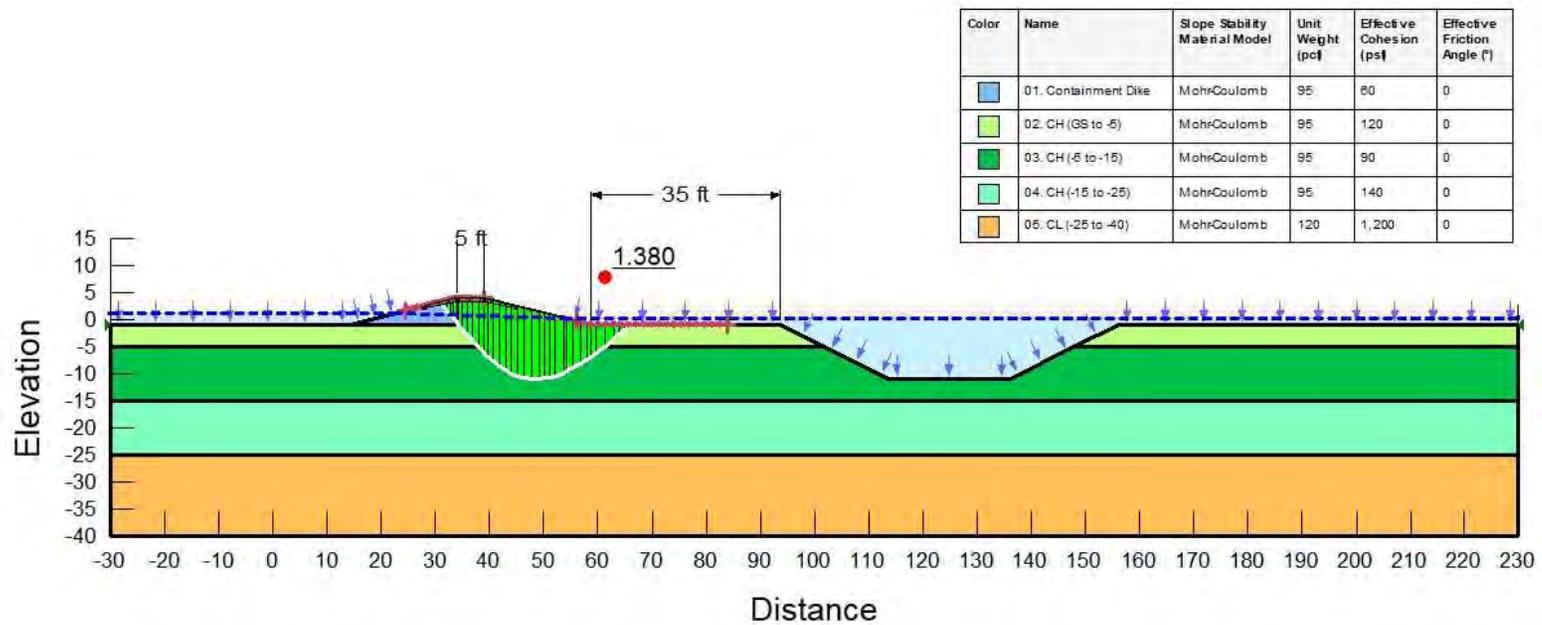
EARTHEN CONTAINMENT DIKE SLOPE STABILITY AND BEARING CAPACITY EVALUATIONS

Calculation Approach

Containment dike slope stability was evaluated using optimized circular search parameters with Spencer's method in the GEO-SLOPE International Limited computer program SLOPE/W (GeoStudio 2021.3). Bearing capacity of the containment dikes was also evaluated using traditional bearing capacity theory. Design considerations for the slope stability and bearing capacity evaluations are described below.

1. The design profile shown in Marsh Creation Area Design Profile, Figure 4, was used in our stability and bearing analyses.
2. A mean low water elevation of +0.3 feet, and a mean high water elevation of +1.09 feet were used in our stability and bearing capacity analyses.
3. A mudline elevation of -0.93 was used as provided by Natural Resources Conservation Services (NRCS).
4. A required factor of safety for slope stability for this project of 1.2.
5. A required factor of safety for bearing capacity for this project of 1.3.
6. Slope stability evaluations for the following cases:
 - a. Case 1: Internal failure of the containment dike; no marsh fill placed;
 - b. Case 2: Global failure of the containment dike into the borrow channel (elevation -10 feet); no marsh fill placed;
 - c. Case 2a: Global failure of the containment dike into the borrow channel (elevation -15 feet); no marsh fill placed;
 - d. Case 3: Failure of the borrow channel; no marsh fill placed, construction equipment modeled; and
 - e. Case 4: Failure of the containment dike; marsh fill placed.
7. For Case 3, the load of marsh excavation equipment on the bench between the containment dike toe and the top of the borrow channel was applied to the mudline. A load of 260 pounds per square foot (psf) minus the depth of water (to account for buoyancy), was applied at the mudline for each track width (4 feet).
8. The values for unit weight within the containment dike material were based on average unit weight of the material within the depth of the proposed borrow channel. An assumed initial cohesion of 60 psf was used for the containment dike material based on our experience with similar projects.
9. A unit weight of 86 pounds per cubic foot (pcf) was used for the fill with no strength (cohesion = 0) for evaluation of Case 4. Marsh fill was modeled to El. +3.0 feet in our stability analyses.
10. The bearing capacity of the containment dikes was evaluated using the method for bearing on a two-layer cohesive soil as outlined in Figure 11-5 of the Naval Facilities Engineering Command Design Manual 7.02 *Foundations and Earth Structures*.
11. For bearing capacity, the width over which the load was applied was based on the effective width which we calculated as the sum of the crown width plus the width of one side slope based on the original mudline elevation.

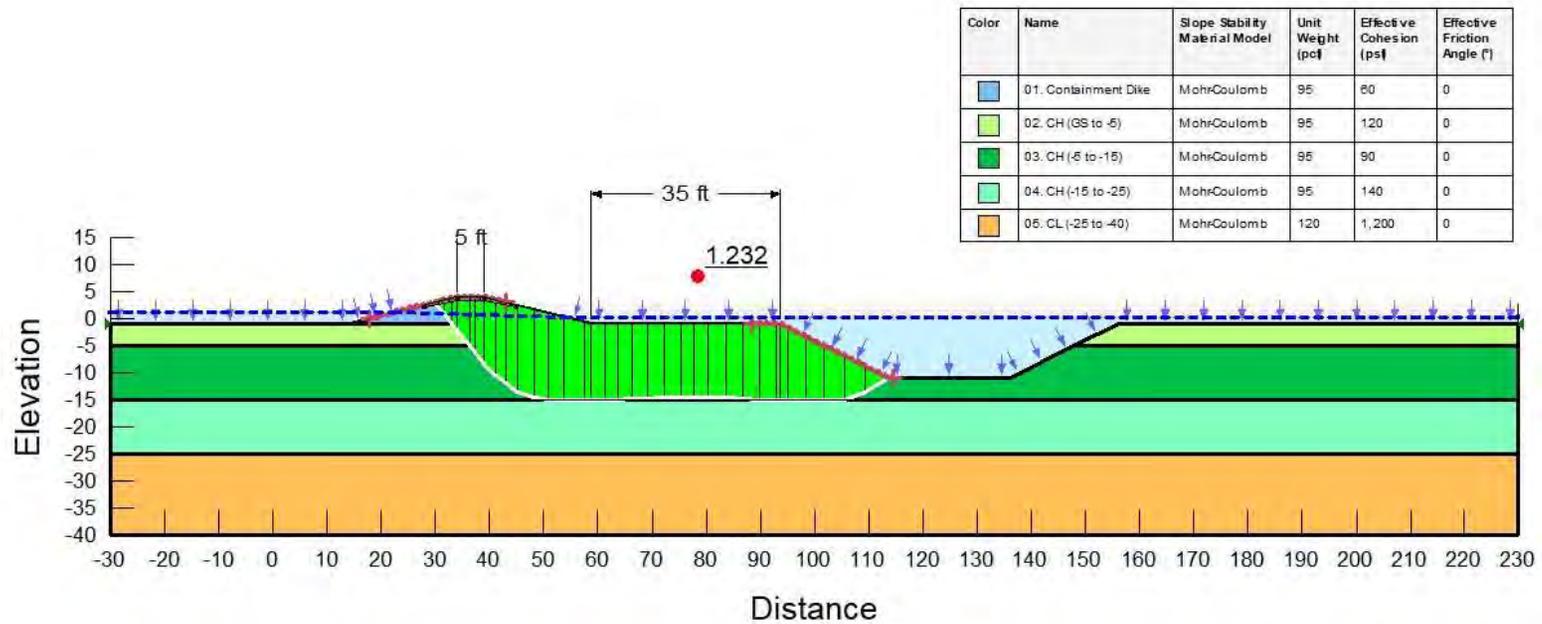
The results of our analyses are shown in the following figures and calculations.



Notes:

1. The locations of all features shown are approximate.
2. This drawing is for information purposes. It is intended to assist in showing features discussed in an attached document. GeoEngineers, Inc. cannot guarantee the accuracy and content of electronic files. The master file is stored by GeoEngineers, Inc. and will serve as the official record of this communication.
3. Failure surfaces are optimized.

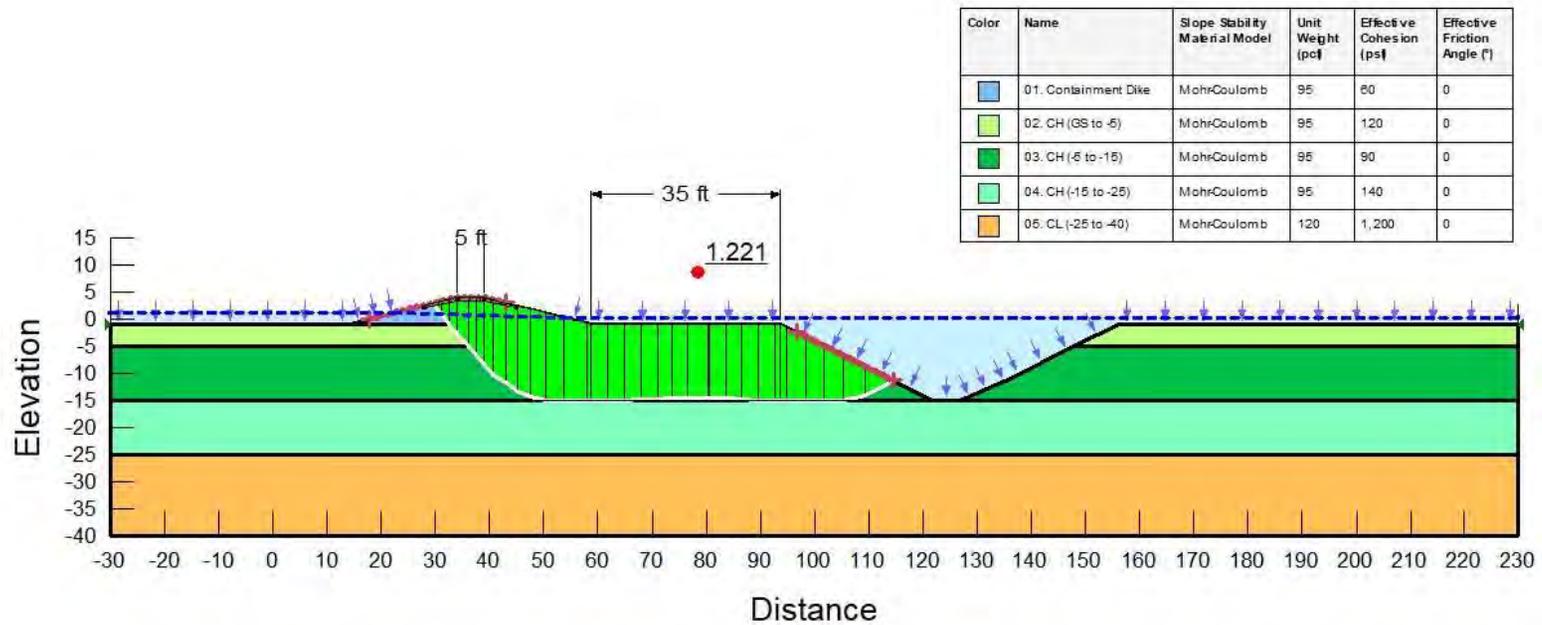
Case 1 Slope Stability	
South Grand Chenier Baker marsh Creation (ME-32) Cameron Parish, Louisiana	
	Figure G-1



Notes:

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3. Failure surfaces are optimized.

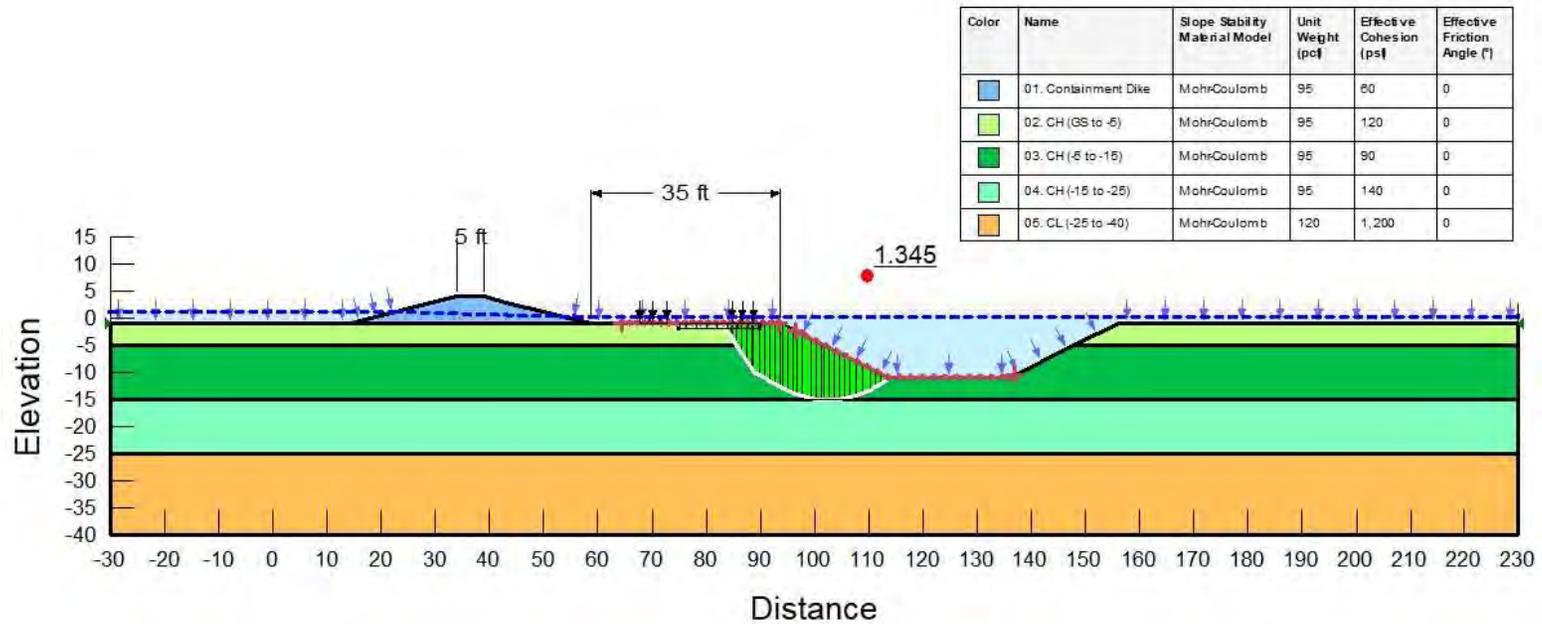
Case 2 Slope Stability	
South Grand Chenier Baker marsh Creation (ME-32) Cameron Parish, Louisiana	
	Figure G-2



Notes:

1. The locations of all features shown are approximate.
2. This drawing is for information purposes. It is intended to assist in showing features discussed in an attached document. GeoEngineers, Inc. cannot guarantee the accuracy and content of electronic files. The master file is stored by GeoEngineers, Inc. and will serve as the official record of this communication.
3. Failure surfaces are optimized.

Case 2a Slope Stability	
South Grand Chenier Baker marsh Creation (ME-32) Cameron Parish, Louisiana	
	Figure G-3

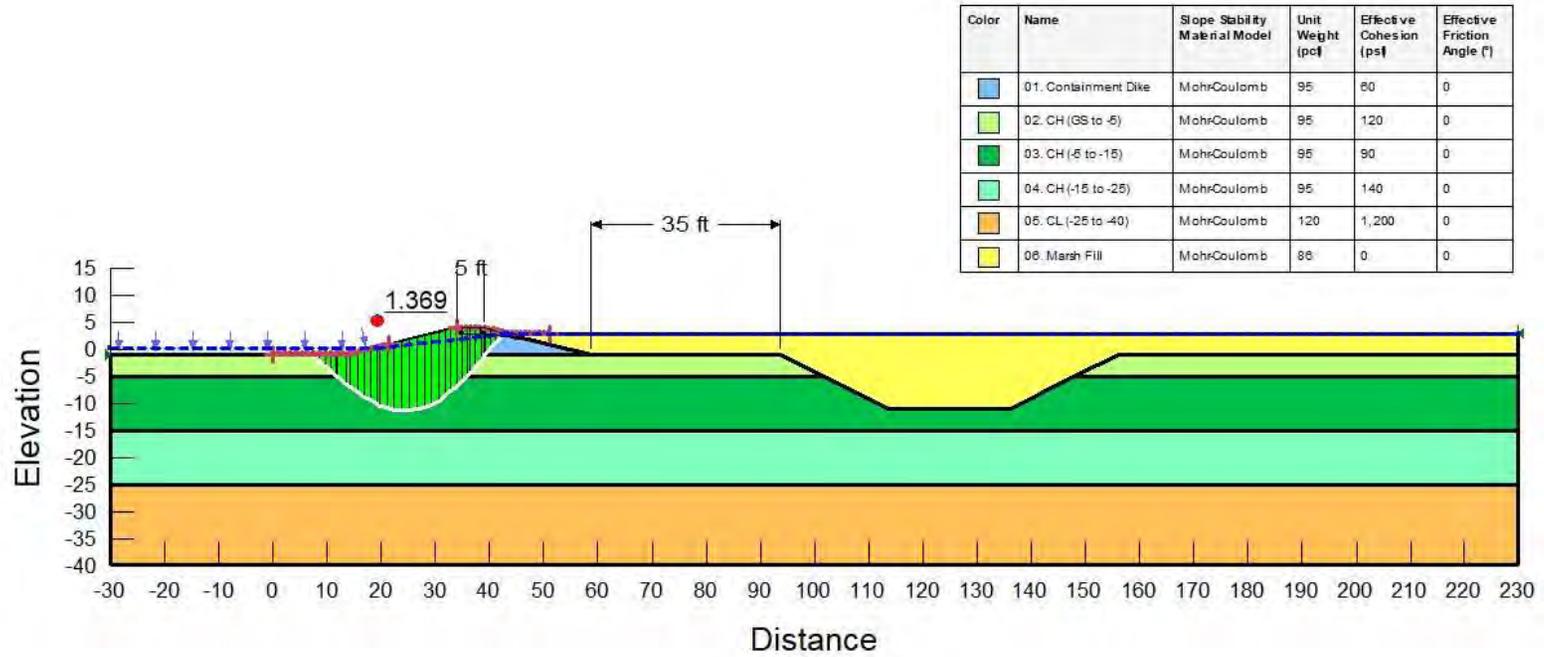


Notes:

1. The locations of all features shown are approximate.
2. This drawing is for information purposes. It is intended to assist in showing features discussed in an attached document. GeoEngineers, Inc. cannot guarantee the accuracy and content of electronic files. The master file is stored by GeoEngineers, Inc. and will serve as the official record of this communication.
3. Failure surfaces are optimized.

Case 3 Slope Stability	
South Grand Chenier Baker marsh Creation (ME-32) Cameron Parish, Louisiana	
	Figure G-4

1:08854:02-16-2023 Date Exported: 02/16/2023



Notes:

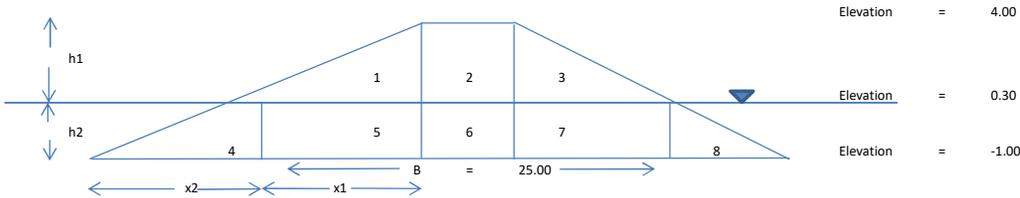
1. The locations of all features shown are approximate.
2. This drawing is for information purposes. It is intended to assist in showing features discussed in an attached document. GeoEngineers, Inc. cannot guarantee the accuracy and content of electronic files. The master file is stored by GeoEngineers, Inc. and will serve as the official record of this communication.
3. Failure surfaces are optimized.

Case 4 Slope Stability	
South Grand Chenier Baker marsh Creation (ME-32) Cameron Parish, Louisiana	
	Figure G-5

USDA-NRCS - S Grand Chenier Marsh Creation Baker

Elevation at Bottom of Dike (ft.)	Elevation at Top of Dike (ft.)	Height of Dike (ft.)	Slope Inclination (H:V)		Width at Top of Dike (ft.)	Elevation of Water (ft.)	Full Width at Bottom of Dike (ft.)	h1 (ft.)	h2 (ft.)	x1 (ft.)	x2 (ft.)
-1.00	4.00	5.00	4.00	1.00	5.00	0.30	45.00	3.70	1.30	14.80	5.20

*1.3 ft mudwave (surface layer C<50 psf)



Assumptions:

1. Unit weight of dike = 95 pcf
2. Water at EL. +0.3 feet
3. Mudline at EL -1 feet
4. The effective width of the dike is equal to the width of the crown plus the width of one sloped side.
5. The factor of safety for bearing capacity must be greater or equal to 1.3.

APPLIED STRESS

Total Unit Weight of Dike (pcf)	Buoyant Unit Weight of Dike (pcf)	Effective Width of Dike (B) (ft.)	Applied Stress (psf)
95.00	32.60	25.00	346

Zone	1	2	3	4	5	6	7	8	Total
Area (ft ²)	27	19	27	3	19	7	19	3	125
Applied Load (lb./ft.)	2601	1758	2601	110	627	212	627	110	8646

SUBSURFACE CONDITIONS

Soil Description	Elevation (ft.)			Cohesion		Thickness (ft.)
				(ksf)	(psf)	
CH (-1 to -5)	-1.00	-	-5.00	0.120	120.00	4.00
CH (-5 to -15)	-5.00	-	-15.00	0.090	90.00	10.00
CH (-15 to -25)	-15.00	-	-25.00	0.140	140.00	10.00
CL (-25 to -40)	-25.00	-	-40.00	1.200	1200.00	15.00

T	B	T/B	C1	C2	C2/C1
4.00	25.00	0.16	120.00	90.00	0.8

BEARING CAPACITY RESULTS

Effective Width of Dike (B) (ft.)	Nc Factor From NAVFAC DM-7 Figure 11-5	C1	Ultimate Bearing Capacity (psf)	Applied Stress (psf)	Factor of Safety
25.00	4.50	120	540	346	1.56

APPENDIX H
Earthen Containment Dike Settlement

APPENDIX H EARTHEN CONTAINMENT DIKE SETTLEMENT

Calculation Approach

1. The following descriptions explain how the settlement parameters were developed.
 - a. Because the site subgrade soils were uniform, we used one representative settlement profile with the following characteristics.

Depth (feet)	Unit Weight (pcf)	OCR	C _c	C _r	C _v (ft ² /day)
0-5	95	3.3	1.19	0.13	0.013
5-15	95	1.5	1.19	0.13	0.013
15-25	95	1.0	1.19	0.13	0.013
25+	120	Incompressible			

Notes:

OCR = over-consolidation ratio, C_c = compression coefficients
 C_r = recompression coefficients, C_v = vertical consolidation coefficients
 ft²/day = square feet per day, pcf = pounds per cubic foot

- b. Graphs for each consolidation test were reconstructed to determine C_c, C_r, C_v, initial void ratios (e₀) and maximum past pressures (P_c). These results were compared to several correlations, and we found the site data suggested a lower soil compressibility, so we used the site-specific data. Due to the consistency of the very soft gray clay in the top 25 feet of the soil profile, C_c was taken as an average of the six tests. Stiff Pleistocene Age soils below 25 feet were assumed to be incompressible. A summary of consolidation test results is presented in this appendix in Table H-1.
 - c. The maximum past pressure (P_c) was obtained from the consolidation test curves for the soil layers with a representative consolidation test. P_c values were also back-calculated based on shear strength. The values for P_c were also back-calculated using the OCR for soil layers at the site. Based on this evaluation, soils above approximately El. -15 ft. are overconsolidated, and soils below approximately El. -15 ft. are normally consolidated.
2. There were not clear drainage paths within the top 25 feet of very soft clay. Although the long-term settlement is expected to be substantial, we do not expect it to occur quickly and only expect about 7 of the estimated 14 inches of settlement to occur within a 6-month construction period.
3. Based on our stability analysis for the earthen containment dikes, the recommended design geometry shown in Earthen Containment Dike Section, Figure 5, was used for the settlement analysis. Water was assumed to be at the mean water level of El. +0.74 feet.
4. Primary consolidation settlement was calculated using one-dimensional consolidation theory and Boussinesq stress distribution in the Rocscience Settle3 (Version 5.001) computer program. For foundation settlement purposes, dike fill was assumed to have been placed instantaneously. The total long-term settlement expected by foundation soils due to the application of earthen containment dike (ECD) fill is 14 inches. Given the limited drainage in the very soft gray clay, we expect to only observe about 7 inches of this settlement during construction (building the dikes and placing hydraulic fill).

Our Settle3 results are included in this appendix and files were also provided electronically.

TABLE H-1. CONSOLIDATION TEST SUMMARY

Boring	Depth Below Mudline (feet)	Mudline Elevation (feet, NAVD 88)	Sample Elevation (feet, NAVD 88)	MC (%)	LL	PI	SG	dry den (pcf)	wet den (pcf)	Descrip.	C _c	C _r	e ₀	C _r /C _c	C _v for t50 (ft ² /day)	C _v for t90 (ft ² /day)	P ₀ (tsf)	P _c (tsf)	OCR	C _c = 0.0054*((S.G.*M.C.)-35) (NAVFAC)	C _c =0.021w-0.4235 (CH/CL)	C _c = 24.245e-0.059*dry den
B-6	3	-1.30	-4.3	122.3	105	79	2.745	40	88.9	CH	1.16	0.14	3.28	0.12	4.67E-03	1.57E-02	0.045	0.147	3.30	1.62	2.14	2.29
B-4	11	-1.55	-12.5	128.7	117	91	2.725	38.3	87.6	CH	1.50	0.16	3.44	0.11	1.28E-02	2.49E-02	0.16	0.16	1.00	1.70	2.28	2.53
B-5	7	-1.46	-8.5	122.1	98	73	2.726	39.9	88.6	CH	1.28	0.10	3.26	0.08	4.19E-03	1.55E-02	0.08	0.125	1.58	1.61	2.14	2.30
B-1	13	-1.28	-14.3	124.6	116	84	2.75	38.7	86.9	CH	0.95	0.15	3.44	0.15	4.07E-04	4.38E-04	0.21	0.21	1.00	1.66	2.19	2.47
B-3	5	-1.24	-6.2	121.8	111	80	2.75	38.2	84.7	CH	1.04	0.12	3.49	0.12	2.41E-03	6.48E-03	0.08	0.17	2.10	1.62	2.13	2.55
avg.				123.9					87.36		1.19	0.13	3.38	0.11	0.005	0.0126	*from Recommended Practice for Estimating Foundation Soil Consolidation Parameters from Index Properties for Louisiana Marsh Creation (Draft), Degroot, Pirouzi and Zhang, April 2018					



Grand Chenier Marsh Creation
GeoEngineers, Inc.

Report Creation Date: 2023/02/24, 09:40:32

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Settle3 Analysis Information

Grand Chenier Marsh Creation

Project Settings

Document Name	Grand Chenier_ML-1 -v2
Project Title	Grand Chenier Marsh Creation
Analysis	ML -1.5 , 4H1V
Author	Nafi Haque
Company	GeoEngineers, Inc.
Date Created	1/17/2023
Last saved with Settle3 version	5.018
Stress Computation Method	Boussinesq
Stress Units	Imperial, stress as ksf
Settlement Units	inches
Time-dependent Consolidation Analysis	
Time Units	days
Permeability Units	inches/year

Advanced Settings

Start of secondary consolidation (% of primary)	95
Min. stress for secondary consolidation (% of initial)	1
Reset time when load changes for secondary consolidation	No
Use settlement cutoff	
Load/Insitu vertical stress ratio	0.1
Minimum settlement ratio for subgrade modulus	0.9
Use average poisson's ratio to calculate layered stresses	
Ignore negative effective stresses in settlement calculations	
Add field points to load edges	

Soil Profile

Layer Option	Horizontal Soil Layers
Vertical Axis	Depth below ground surface

Stage Settings

Stage #	Name	Time [days]
1	Stage 1	0
2	Stage 2	14
3	Stage 3	30
4	Stage 4	60
5	Stage 5	90
6	Stage 6	120
7	Stage 7	150
8	Stage 8	180
9	Stage 9	300
10	Stage 10	365
11	Stage 11	730
12	Stage 12	1095
13	Stage 13	7300

Results

Time taken to compute: 0 seconds

Stage: Stage 1 = 0 d

Data Type	Minimum	Maximum
Total Settlement [in]	0	0
Total Consolidation Settlement [in]	0	0
Virgin Consolidation Settlement [in]	0	0
Recompression Consolidation Settlement [in]	0	0
Immediate Settlement [in]	0	0
Secondary Settlement [in]	0	0
Loading Stress ZZ [ksf]	0.122129	0.35931
Loading Stress XX [ksf]	0.200019	0.338251
Loading Stress YY [ksf]	0.364709	0.583309
Effective Stress ZZ [ksf]	0	1.679
Effective Stress XX [ksf]	0.200019	1.98847
Effective Stress YY [ksf]	0.364709	2.20105
Total Stress ZZ [ksf]	0.35931	4.29713
Total Stress XX [ksf]	0.559329	4.6066
Total Stress YY [ksf]	0.724019	4.81918
Modulus of Subgrade Reaction (Total) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Immediate) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Consolidation) [ksf/ft]	0	0
Total Strain	0	0
Pore Water Pressure [ksf]	0.35931	2.61813
Excess Pore Water Pressure [ksf]	0.122129	0.35931
Degree of Consolidation [%]	0	0
Pre-consolidation Stress [ksf]	0.005379	1.67814
Over-consolidation Ratio	1	3.3
Void Ratio	0	3.38
Permeability [in/y]	0	249.546
Coefficient of Consolidation [in ² /y]	0	78840
Hydroconsolidation Settlement [in]	0	0
Average Degree of Consolidation [%]	0	0
Undrained Shear Strength	-1.38778e-17	0

Stage: Stage 2 = 14 d

Data Type	Minimum	Maximum
Total Settlement [in]	-0.00156675	2.87441
Total Consolidation Settlement [in]	-0.00156675	2.87441
Virgin Consolidation Settlement [in]	0	2.53346
Recompression Consolidation Settlement [in]	-0.00156675	0.340951
Immediate Settlement [in]	0	0
Secondary Settlement [in]	0	0
Loading Stress ZZ [ksf]	0.136693	0.467446
Loading Stress XX [ksf]	0.308396	0.471692
Loading Stress YY [ksf]	0.55947	0.759356
Effective Stress ZZ [ksf]	0.0776296	1.61181
Effective Stress XX [ksf]	0.435398	2.04957
Effective Stress YY [ksf]	0.710964	2.28977
Total Stress ZZ [ksf]	0.467446	4.31169
Total Stress XX [ksf]	0.775842	4.74945
Total Stress YY [ksf]	1.02692	4.98965
Modulus of Subgrade Reaction (Total) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Immediate) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Consolidation) [ksf/ft]	0	0
Total Strain	-7.52735e-05	0.510797
Pore Water Pressure [ksf]	0.108136	2.69988
Excess Pore Water Pressure [ksf]	0.108136	0.438699
Degree of Consolidation [%]	0	15.9312
Pre-consolidation Stress [ksf]	0.199757	1.67814
Over-consolidation Ratio	1	3.30633
Void Ratio	0	3.38033
Permeability [in/y]	0	249.546
Coefficient of Consolidation [in ² /y]	0	78840
Hydroconsolidation Settlement [in]	0	0
Average Degree of Consolidation [%]	0	0
Undrained Shear Strength	-1.38778e-17	0.0063173

Stage: Stage 3 = 30 d

Data Type	Minimum	Maximum
Total Settlement [in]	-0.00275587	4.15653
Total Consolidation Settlement [in]	-0.00275587	4.15653
Virgin Consolidation Settlement [in]	0	3.61371
Recompression Consolidation Settlement [in]	-0.00501521	0.54282
Immediate Settlement [in]	0	0
Secondary Settlement [in]	0	0
Loading Stress ZZ [ksf]	0.136693	0.467446
Loading Stress XX [ksf]	0.308396	0.471692
Loading Stress YY [ksf]	0.55947	0.759356
Effective Stress ZZ [ksf]	0.137496	1.60113
Effective Stress XX [ksf]	0.495265	2.03889
Effective Stress YY [ksf]	0.77083	2.27908
Total Stress ZZ [ksf]	0.467446	4.31169
Total Stress XX [ksf]	0.775842	4.74945
Total Stress YY [ksf]	1.02692	4.98965
Modulus of Subgrade Reaction (Total) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Immediate) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Consolidation) [ksf/ft]	0	0
Total Strain	-7.79776e-05	0.542127
Pore Water Pressure [ksf]	0	2.71057
Excess Pore Water Pressure [ksf]	0	0.398016
Degree of Consolidation [%]	0	23.0372
Pre-consolidation Stress [ksf]	0.2456	1.67814
Over-consolidation Ratio	1	2.78106
Void Ratio	0	3.38034
Permeability [in/y]	0	249.546
Coefficient of Consolidation [in ² /y]	0	78840
Hydroconsolidation Settlement [in]	0	0
Average Degree of Consolidation [%]	0	0
Undrained Shear Strength	-5.84285e-06	0.00771013

Stage: Stage 4 = 60 d

Data Type	Minimum	Maximum
Total Settlement [in]	-0.00190828	5.07639
Total Consolidation Settlement [in]	-0.00190828	5.07639
Virgin Consolidation Settlement [in]	0	4.21986
Recompression Consolidation Settlement [in]	-0.00489061	0.856523
Immediate Settlement [in]	0	0
Secondary Settlement [in]	0	0
Loading Stress ZZ [ksf]	0.136693	0.467446
Loading Stress XX [ksf]	0.308396	0.471692
Loading Stress YY [ksf]	0.55947	0.759356
Effective Stress ZZ [ksf]	0.23383	1.59903
Effective Stress XX [ksf]	0.602883	2.03678
Effective Stress YY [ksf]	0.878449	2.27698
Total Stress ZZ [ksf]	0.467446	4.31169
Total Stress XX [ksf]	0.775842	4.74945
Total Stress YY [ksf]	1.02692	4.98965
Modulus of Subgrade Reaction (Total) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Immediate) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Consolidation) [ksf/ft]	0	0
Total Strain	-0.000101294	0.542373
Pore Water Pressure [ksf]	0	2.71267
Excess Pore Water Pressure [ksf]	0	0.372119
Degree of Consolidation [%]	0	28.1354
Pre-consolidation Stress [ksf]	0.276596	1.67814
Over-consolidation Ratio	1	1.77594
Void Ratio	0	3.38045
Permeability [in/y]	0	249.546
Coefficient of Consolidation [in ² /y]	0	78840
Hydroconsolidation Settlement [in]	0	0
Average Degree of Consolidation [%]	0	0
Undrained Shear Strength	-1.29653e-05	0.0109503

Stage: Stage 5 = 90 d

Data Type	Minimum	Maximum
Total Settlement [in]	-0.00278206	6.06962
Total Consolidation Settlement [in]	-0.00278206	6.06962
Virgin Consolidation Settlement [in]	0	5.07112
Recompression Consolidation Settlement [in]	-0.00458529	0.998506
Immediate Settlement [in]	0	0
Secondary Settlement [in]	0	0
Loading Stress ZZ [ksf]	0.136693	0.467446
Loading Stress XX [ksf]	0.308396	0.471692
Loading Stress YY [ksf]	0.55947	0.759356
Effective Stress ZZ [ksf]	0.274485	1.59742
Effective Stress XX [ksf]	0.679328	2.03518
Effective Stress YY [ksf]	0.954894	2.27538
Total Stress ZZ [ksf]	0.467446	4.31169
Total Stress XX [ksf]	0.775842	4.74945
Total Stress YY [ksf]	1.02692	4.98965
Modulus of Subgrade Reaction (Total) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Immediate) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Consolidation) [ksf/ft]	0	0
Total Strain	-0.000126935	0.542415
Pore Water Pressure [ksf]	0	2.71427
Excess Pore Water Pressure [ksf]	0	0.358837
Degree of Consolidation [%]	0	33.6403
Pre-consolidation Stress [ksf]	0.311713	1.67814
Over-consolidation Ratio	1	1.5074
Void Ratio	0	3.38056
Permeability [in/y]	0	249.546
Coefficient of Consolidation [in ² /y]	0	78840
Hydroconsolidation Settlement [in]	0	0
Average Degree of Consolidation [%]	0	0
Undrained Shear Strength	-2.87816e-06	0.0147511

Stage: Stage 6 = 120 d

Data Type	Minimum	Maximum
Total Settlement [in]	-0.00360524	6.89764
Total Consolidation Settlement [in]	-0.00360524	6.89764
Virgin Consolidation Settlement [in]	0	5.81413
Recompression Consolidation Settlement [in]	-0.00360524	1.08351
Immediate Settlement [in]	0	0
Secondary Settlement [in]	0	0
Loading Stress ZZ [ksf]	0.136693	0.467446
Loading Stress XX [ksf]	0.308396	0.471692
Loading Stress YY [ksf]	0.55947	0.759356
Effective Stress ZZ [ksf]	0.296927	1.59606
Effective Stress XX [ksf]	0.732522	2.03381
Effective Stress YY [ksf]	1.00809	2.27401
Total Stress ZZ [ksf]	0.467446	4.31169
Total Stress XX [ksf]	0.775842	4.74945
Total Stress YY [ksf]	1.02692	4.98965
Modulus of Subgrade Reaction (Total) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Immediate) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Consolidation) [ksf/ft]	0	0
Total Strain	-0.000148766	0.54244
Pore Water Pressure [ksf]	0	2.71564
Excess Pore Water Pressure [ksf]	0	0.344975
Degree of Consolidation [%]	0	38.2295
Pre-consolidation Stress [ksf]	0.348007	1.67814
Over-consolidation Ratio	1	1.50162
Void Ratio	0	3.38066
Permeability [in/y]	0	249.546
Coefficient of Consolidation [in ² /y]	0	78840
Hydroconsolidation Settlement [in]	0	0
Average Degree of Consolidation [%]	0	0
Undrained Shear Strength	0	0.0168148

Stage: Stage 7 = 150 d

Data Type	Minimum	Maximum
Total Settlement [in]	-0.00439551	7.6018
Total Consolidation Settlement [in]	-0.00439551	7.6018
Virgin Consolidation Settlement [in]	0	6.46371
Recompression Consolidation Settlement [in]	-0.00439551	1.13808
Immediate Settlement [in]	0	0
Secondary Settlement [in]	0	0
Loading Stress ZZ [ksf]	0.136693	0.467446
Loading Stress XX [ksf]	0.308396	0.471692
Loading Stress YY [ksf]	0.55947	0.759356
Effective Stress ZZ [ksf]	0.323449	1.59483
Effective Stress XX [ksf]	0.769722	2.03259
Effective Stress YY [ksf]	1.02692	2.27279
Total Stress ZZ [ksf]	0.467446	4.31169
Total Stress XX [ksf]	0.775842	4.74945
Total Stress YY [ksf]	1.02692	4.98965
Modulus of Subgrade Reaction (Total) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Immediate) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Consolidation) [ksf/ft]	0	0
Total Strain	-0.000168368	0.542457
Pore Water Pressure [ksf]	0	2.71686
Excess Pore Water Pressure [ksf]	0	0.33639
Degree of Consolidation [%]	0	42.1322
Pre-consolidation Stress [ksf]	0.369278	1.67814
Over-consolidation Ratio	1	1.4981
Void Ratio	0	3.38074
Permeability [in/y]	0	249.546
Coefficient of Consolidation [in ² /y]	0	78840
Hydroconsolidation Settlement [in]	0	0
Average Degree of Consolidation [%]	0	0
Undrained Shear Strength	0	0.0196573

Stage: Stage 8 = 180 d

Data Type	Minimum	Maximum
Total Settlement [in]	-0.00516113	8.2224
Total Consolidation Settlement [in]	-0.00516113	8.2224
Virgin Consolidation Settlement [in]	0	7.0495
Recompression Consolidation Settlement [in]	-0.00516113	1.17291
Immediate Settlement [in]	0	0
Secondary Settlement [in]	0	0
Loading Stress ZZ [ksf]	0.136693	0.467446
Loading Stress XX [ksf]	0.308396	0.471692
Loading Stress YY [ksf]	0.55947	0.759356
Effective Stress ZZ [ksf]	0.349368	1.59371
Effective Stress XX [ksf]	0.775842	2.03146
Effective Stress YY [ksf]	1.02692	2.27166
Total Stress ZZ [ksf]	0.467446	4.31169
Total Stress XX [ksf]	0.775842	4.74945
Total Stress YY [ksf]	1.02692	4.98965
Modulus of Subgrade Reaction (Total) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Immediate) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Consolidation) [ksf/ft]	0	0
Total Strain	-0.00018648	0.542469
Pore Water Pressure [ksf]	0	2.71799
Excess Pore Water Pressure [ksf]	0	0.324714
Degree of Consolidation [%]	0	45.5719
Pre-consolidation Stress [ksf]	0.39813	1.67814
Over-consolidation Ratio	1	1.49143
Void Ratio	0	3.38082
Permeability [in/y]	0	249.546
Coefficient of Consolidation [in ² /y]	0	78840
Hydroconsolidation Settlement [in]	0	0
Average Degree of Consolidation [%]	0	0
Undrained Shear Strength	0	0.0207682

Stage: Stage 9 = 300 d

Data Type	Minimum	Maximum
Total Settlement [in]	-0.00816633	9.63032
Total Consolidation Settlement [in]	-0.00816633	9.63032
Virgin Consolidation Settlement [in]	0	8.34945
Recompression Consolidation Settlement [in]	-0.00816633	1.28087
Immediate Settlement [in]	0	0
Secondary Settlement [in]	0	0
Loading Stress ZZ [ksf]	0.136693	0.467446
Loading Stress XX [ksf]	0.308396	0.471692
Loading Stress YY [ksf]	0.55947	0.759356
Effective Stress ZZ [ksf]	0.407542	1.58977
Effective Stress XX [ksf]	0.775842	2.02753
Effective Stress YY [ksf]	1.02692	2.26772
Total Stress ZZ [ksf]	0.467446	4.31169
Total Stress XX [ksf]	0.775842	4.74945
Total Stress YY [ksf]	1.02692	4.98965
Modulus of Subgrade Reaction (Total) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Immediate) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Consolidation) [ksf/ft]	0	0
Total Strain	-0.000249851	0.542492
Pore Water Pressure [ksf]	0	2.72192
Excess Pore Water Pressure [ksf]	0	0.293224
Degree of Consolidation [%]	0	53.3751
Pre-consolidation Stress [ksf]	0.452446	1.67814
Over-consolidation Ratio	1	1.46939
Void Ratio	0	3.3811
Permeability [in/y]	0	249.546
Coefficient of Consolidation [in ² /y]	0	78840
Hydroconsolidation Settlement [in]	0	0
Average Degree of Consolidation [%]	0	0
Undrained Shear Strength	-5.18035e-05	0.0231778

Stage: Stage 10 = 365 d

Data Type	Minimum	Maximum
Total Settlement [in]	-0.00970362	10.0644
Total Consolidation Settlement [in]	-0.00970362	10.0644
Virgin Consolidation Settlement [in]	0	8.74398
Recompression Consolidation Settlement [in]	-0.00970362	1.32038
Immediate Settlement [in]	0	0
Secondary Settlement [in]	0	0
Loading Stress ZZ [ksf]	0.136693	0.467446
Loading Stress XX [ksf]	0.308396	0.471692
Loading Stress YY [ksf]	0.55947	0.759356
Effective Stress ZZ [ksf]	0.437297	1.58789
Effective Stress XX [ksf]	0.775842	2.02565
Effective Stress YY [ksf]	1.02692	2.26585
Total Stress ZZ [ksf]	0.467446	4.31169
Total Stress XX [ksf]	0.775842	4.74945
Total Stress YY [ksf]	1.02692	4.98965
Modulus of Subgrade Reaction (Total) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Immediate) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Consolidation) [ksf/ft]	0	0
Total Strain	-0.000280172	0.542496
Pore Water Pressure [ksf]	0	2.7238
Excess Pore Water Pressure [ksf]	0	0.281924
Degree of Consolidation [%]	0	55.7807
Pre-consolidation Stress [ksf]	0.468604	1.67814
Over-consolidation Ratio	1	1.46093
Void Ratio	0	3.38123
Permeability [in/y]	0	249.546
Coefficient of Consolidation [in ² /y]	0	78840
Hydroconsolidation Settlement [in]	0	0
Average Degree of Consolidation [%]	0	0
Undrained Shear Strength	-4.69936e-05	0.0235479

Stage: Stage 11 = 730 d

Data Type	Minimum	Maximum
Total Settlement [in]	-0.0157282	11.2509
Total Consolidation Settlement [in]	-0.0157282	11.2509
Virgin Consolidation Settlement [in]	0	9.82931
Recompression Consolidation Settlement [in]	-0.0157282	1.42154
Immediate Settlement [in]	0	0
Secondary Settlement [in]	0	0
Loading Stress ZZ [ksf]	0.136693	0.467446
Loading Stress XX [ksf]	0.308396	0.471692
Loading Stress YY [ksf]	0.55947	0.759356
Effective Stress ZZ [ksf]	0.467446	1.5793
Effective Stress XX [ksf]	0.775842	2.01706
Effective Stress YY [ksf]	1.02692	2.25725
Total Stress ZZ [ksf]	0.467446	4.31169
Total Stress XX [ksf]	0.775842	4.74945
Total Stress YY [ksf]	1.02692	4.98965
Modulus of Subgrade Reaction (Total) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Immediate) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Consolidation) [ksf/ft]	0	0
Total Strain	-0.000419934	0.5425
Pore Water Pressure [ksf]	0	2.73239
Excess Pore Water Pressure [ksf]	0	0.263446
Degree of Consolidation [%]	0	62.3568
Pre-consolidation Stress [ksf]	0.468621	1.67814
Over-consolidation Ratio	1	1.40024
Void Ratio	0	3.38184
Permeability [in/y]	0	249.546
Coefficient of Consolidation [in ² /y]	0	78840
Hydroconsolidation Settlement [in]	0	0
Average Degree of Consolidation [%]	0	0
Undrained Shear Strength	0	0.0239707

Stage: Stage 12 = 1095 d

Data Type	Minimum	Maximum
Total Settlement [in]	-0.0185372	11.7614
Total Consolidation Settlement [in]	-0.0185372	11.7614
Virgin Consolidation Settlement [in]	0	10.3137
Recompression Consolidation Settlement [in]	-0.0185372	1.4477
Immediate Settlement [in]	0	0
Secondary Settlement [in]	0	0
Loading Stress ZZ [ksf]	0.136693	0.467446
Loading Stress XX [ksf]	0.308396	0.471692
Loading Stress YY [ksf]	0.55947	0.759356
Effective Stress ZZ [ksf]	0.467446	1.57343
Effective Stress XX [ksf]	0.775842	2.01119
Effective Stress YY [ksf]	1.02692	2.25138
Total Stress ZZ [ksf]	0.467446	4.31169
Total Stress XX [ksf]	0.775842	4.74945
Total Stress YY [ksf]	1.02692	4.98965
Modulus of Subgrade Reaction (Total) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Immediate) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Consolidation) [ksf/ft]	0	0
Total Strain	-0.000516289	0.5425
Pore Water Pressure [ksf]	0	2.73826
Excess Pore Water Pressure [ksf]	0	0.252938
Degree of Consolidation [%]	0	65.1865
Pre-consolidation Stress [ksf]	0.468623	1.67814
Over-consolidation Ratio	1	1.35193
Void Ratio	0	3.38227
Permeability [in/y]	0	249.546
Coefficient of Consolidation [in ² /y]	0	78840
Hydroconsolidation Settlement [in]	0	0
Average Degree of Consolidation [%]	0	0
Undrained Shear Strength	-0.000163988	0.0240166

Stage: Stage 13 = 7300 d

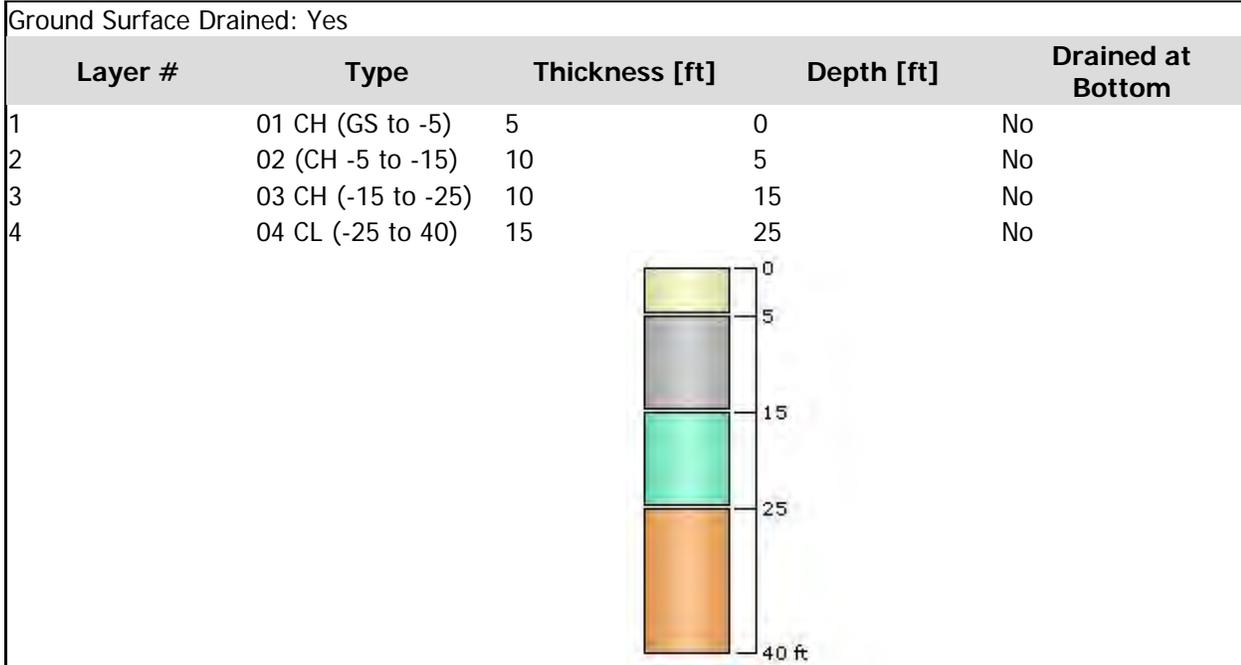
Data Type	Minimum	Maximum
Total Settlement [in]	0	13.9038
Total Consolidation Settlement [in]	0	13.9038
Virgin Consolidation Settlement [in]	0	12.3752
Recompression Consolidation Settlement [in]	0	1.52856
Immediate Settlement [in]	0	0
Secondary Settlement [in]	0	0
Loading Stress ZZ [ksf]	0.136693	0.467446
Loading Stress XX [ksf]	0.308396	0.471692
Loading Stress YY [ksf]	0.55947	0.759356
Effective Stress ZZ [ksf]	0.467446	1.63185
Effective Stress XX [ksf]	0.775842	2.06961
Effective Stress YY [ksf]	1.02692	2.3098
Total Stress ZZ [ksf]	0.467446	4.31169
Total Stress XX [ksf]	0.775842	4.74945
Total Stress YY [ksf]	1.02692	4.98965
Modulus of Subgrade Reaction (Total) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Immediate) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Consolidation) [ksf/ft]	0	0
Total Strain	0	0.542501
Pore Water Pressure [ksf]	0	2.67984
Excess Pore Water Pressure [ksf]	0	0.183843
Degree of Consolidation [%]	0	77.0602
Pre-consolidation Stress [ksf]	0.468624	1.67814
Over-consolidation Ratio	1	1.15355
Void Ratio	0	3.36517
Permeability [in/y]	0	249.546
Coefficient of Consolidation [in ² /y]	0	78840
Hydroconsolidation Settlement [in]	0	0
Average Degree of Consolidation [%]	0	0
Undrained Shear Strength	-2.28645e-05	0.0240602

Embankments

1. Embankment: "Containment Dike "

Label	Containment Dike						
Center Line	(0, 0) to (0, 100)						
Near End Angle	90 degrees						
Far End Angle	90 degrees						
Number of Layers	3						
Base Width	37						
Layer	Stage	Left Bench Width (ft)	Left Angle (deg)	Height (ft)	Unit Weight (kips/ft3)	Right Angle (deg)	Right Bench Width (ft)
1	Stage 1 = 0 d	0	14.0362	2	0.12	14.0362	0
2	Stage 1 = 0 d	0	14.0362	1	0.12	14.0362	0
3	Stage 2 = 14 d	0	14.0362	1	0.12	14.0362	0

Soil Layers



Soil Properties

Property	01 CH (GS to - 5)	02 (CH -5 to - 15)	03 CH (-15 to - 25)	04 CL (-25 to 40)
Color				
Unit Weight [kips/ft3]	0.095	0.095	0.095	0.12
Saturated Unit Weight [kips/ft3]	0.095	0.095	0.095	0.12
K0	1	1	1	1
Primary Consolidation	Enabled	Enabled	Enabled	Disabled
Material Type	Non-Linear	Non-Linear	Non-Linear	
Cc	1.19	1.19	1.19	-
Cr	0.13	0.13	0.13	-
e0	3.38	3.38	3.38	-
OCR	3.3	1.5	1	-
Cv [in2/y]	662.2	662.2	662.2	-
Cvr [in2/y]	78840	1840	6098	-
B-bar	1	1	1	-
Undrained Su A [kips/ft2]	0	0	0	0
Undrained Su S	0.2	0.2	0.2	0.2
Undrained Su m	0.8	0.8	0.8	0.8
Piezo Line ID	1	1	1	1

Groundwater

Groundwater method
Water Unit Weight

Piezometric Lines
0.0624 kips/ft³

Piezometric Line Entities

ID	Depth (ft)
1	0 ft

Query

Query Points

Point #	Query Point Name	(X,Y) Location	Number of Divisions
1	Query Point 1	0.078, 51.111	Auto: 65

APPENDIX I
Marsh Creation Area Settlement

APPENDIX I MARSH CREATION AREA SETTLEMENT

Calculation Approach Subgrade Soil

For the subsurface soil profile, the same parameters used for the earthen containment dike (ECD) settlement evaluation described in Appendix H were used for the marsh fill subgrade soil settlement. To determine the applied load, GeoEngineers looked at the point in time when the hydraulic fill completed most of its consolidation and became relatively stable. This point occurred at about 3 years after construction. We used this fill elevation and corresponding density at 3 years to determine the applied load on the subgrade soil. The resulting settlement was relatively small, ranging from 1 to 3 inches depending on the fill thickness. The applied stress to the subgrade, with most of the fill being below the average water elevation is much less than the load applied by the ECD, and therefore the settlement is significantly less.

Hydraulic Fill

Settlement of the marsh creation area consists primarily of two separate processes: consolidation of dredged fill and consolidation of the foundation soils. Consolidation of the dredged fill was modeled using PSDDF (Primary consolidation, Secondary compression, and Desiccation of Dredged Fill), a program created for the United States Army Corps of Engineers (USACE) to simulate finite strain consolidation in dredged fill materials. Consolidation of the foundation soils was modeled iteratively using a one-dimensional consolidation program.

Inputs into the PSDDF program were developed as follows:

- Fill compressibility values and void ratios were obtained from two low-stress consolidation tests. On the higher moisture, lower density end, we used results from a test on a slurry prepared at 490.2 percent moisture (224 grams per liter [g/L]), and on the lower moisture, higher density end, we used results from a test on a slurry prepared at 344.2 percent moisture (262 g/L).
- A long-term target marsh elevation of El. 0.8 ft. was desired. Initial fill elevations that provided long-term elevations bracketing this target were selected, then we interpolated results between these two runs. The high fill start level was selected at El. +3.5 ft., and the low fill start level was selected at El. +1.5 ft.
- Based on discussions with the Natural Resources Conservation Service (NRCS) and considering previous experience at an adjacent marsh creation project, a period of 25 days was used to model the fill placement time. Fill was modeled as being placed in incremental lifts during the 25-day fill period to mimic the filling process and allow for some consolidation during fill placement as shown in Table I-1.

TABLE I-1. INCREMENTAL FILL LIFTS

Target Fill El.	Fill Layer Thickness added at Day # During Fill Period (ft. @ day)			
+3.5	1.4 ft. @ day 6	1.0 ft. @ day 12	1.0 ft. @ day 18	1.0 ft. @ day 24
+1.5	0.9 ft. @ day 6	0.5 ft. @ day 12	0.5 ft. @ day 18	0.5 ft. @ day 24

- A mudline elevation of El. -0.93 ft. and a mean water level of El. 0.74 ft. were used for initial conditions.
- Subsidence was deducted from the fill elevation at a rate of 4.3 millimeters (mm) per year starting at the end of construction. Accretion was added to the fill elevation at a rate of 2.5 mm per year starting at year 6 after construction.
- Sea level rise was used to raise the mean high and low water elevations at a rate of 0.026 feet per year.

The combined effects of the PSDDF model output for different fill densities and elevations, subgrade settlement from Settle3, subsidence, accretion and sea level rise were combined in a series of figures requested by NRCS included in this report.

NRCS also asked for a chart for each fill density using the fill elevation that achieved El. 0.8 ft. at year 20, also included an upper and lower bound representing 95 percent confidence intervals. The way we approached this was to grid the marsh creation area with at 100-foot square grid and obtain a mudline elevation at each grid intersection within the marsh creation area limits based on a survey provided to us by NRCS. We then determined the median and standard deviation for this data set (as presented in Appendix F). Using marsh mudline elevations representing the mean plus 2 standard deviations and minus 2 standard deviations, we re-ran the PSDDF analyses with the same target fill elevations (adjusting the fill increments accordingly) to determine the effect on the long-term fill elevation for these high and low mudline elevations that approximately represent a 95 percent confidence interval around the mean marsh elevation.

This appendix contains sample PSDDF output and settlement calculations. Output and results can be viewed in their native file format in a companion electronic file submission.

Filename: 344.2% moisture slurry

Initial Mudline El. (ft) -0.929 Subsidence (4.3mm/yr) -0.01410761 ft/yr
 Initial CMFE (ft) 3.52 Accretion (2.5mm/yr) 0.0082021 ft/yr, begins at year 6
 Initial Marsh Thickness (ft) 4.45

	(a)	(b)	(c)	(d)	(e)	(f)	(g)	(h)
		Settle3	Mudline		PSDDF		Final MFE +	Final MFE + Subsidence +
Time (days)	Time (years)	Settlement (in)	El. (ft)	MFE (ft)	Settlement	Final MFE (ft)	Subsidence (ft)	Accretion (ft)
0.00	0.00	0.00	-0.93	3.52		0.00	0.00	0.00
0.13	0.00	0.13	-0.94	3.51		3.51	3.51	3.51
0.33	0.00	0.19	-0.94	3.50		3.50	3.50	3.50
0.63	0.00	0.24	-0.95	3.50		3.50	3.50	3.50
1.08	0.00	0.30	-0.95	3.49		3.49	3.49	3.49
1.76	0.00	0.37	-0.96	3.49		3.49	3.49	3.49
2.77	0.01	0.45	-0.97	3.48		3.48	3.48	3.48
4.29	0.01	0.54	-0.97	3.48		3.48	3.47	3.47
6.57	0.02	0.63	-0.98	3.47		3.47	3.47	3.47
9.99	0.03	0.73	-0.99	3.46		3.46	3.46	3.46
15.00	0.04	0.83	-1.00	3.45	0.04	3.41	3.41	3.41
20.28	0.06	0.92	-1.01	3.44		3.44	3.44	3.44
30.00	0.08	1.04	-1.02	3.43	0.08	3.36	3.36	3.36
38.10	0.10	1.12	-1.02	3.43		3.43	3.42	3.42
50.26	0.14	1.22	-1.03	3.42		3.42	3.42	3.42
60.00	0.16	1.29	-1.04	3.41	0.15	3.26	3.26	3.26
79.49	0.22	1.40	-1.05	3.40		3.40	3.40	3.40
90.00	0.25	1.46	-1.05	3.40	0.23	3.17	3.17	3.17
120.00	0.33	1.60	-1.06	3.39	0.54	2.85	2.84	2.84
150.00	0.41	1.71	-1.07	3.38	0.91	2.46	2.46	2.46
180.00	0.49	1.80	-1.08	3.37	1.18	2.19	2.18	2.18
213.33	0.58	1.88	-1.09	3.36		3.36	3.36	3.36
270.00	0.74	1.99	-1.10	3.35	1.62	1.73	1.72	1.72
321.52	0.88	2.08	-1.10	3.35		3.35	3.33	3.33
365.00	1.00	2.15	-1.11	3.34	1.84	1.50	1.49	1.49
444.06	1.22	2.25	-1.12	3.33		3.33	3.32	3.32
562.66	1.54	2.38	-1.13	3.32		3.32	3.30	3.30
730.00	2.00	2.52	-1.14	3.31	2.00	1.31	1.28	1.28
915.94	2.51	2.64	-1.15	3.30		3.30	3.26	3.26
1095.00	3.00	2.77	-1.16	3.29	2.01	1.28	1.23	1.23
1393.44	3.82	2.95	-1.17	3.27		3.27	3.22	3.22
1841.10	5.04	3.11	-1.19	3.26		3.26	3.19	3.19
2190.00	6.00	3.19	-1.19	3.25	2.01	1.24	1.16	1.16
2887.79	7.91	3.26	-1.20	3.25		3.25	3.14	3.15
3650.00	10.00	3.30	-1.20	3.25	2.01	1.23	1.09	1.12
4738.87	12.98	3.31	-1.21	3.24		3.24	3.06	3.12
6372.17	17.46	3.32	-1.21	3.24		3.24	3.00	3.09
7300.00	20.00	3.32	-1.21	3.24	2.01	1.23	0.95	1.06

Fill EI = +3.5 ft

PSDDF Output adjusted to
remove 1st 25 days

days	settlement
0	0
15	0.038
30	0.077
60	0.152
90	0.228
120	0.54
150	0.914
180	1.183
270	1.623
365	1.84
730	2.002
1095	2.013
2190	2.013
3650	2.013
7300	2.013

 Consolidation and desiccation of soft layers---dredged fill

Problem Grand Chenier - MC Target 340 MF+3.5 25 days

*****Soil data for dredged fill*****

Material Type	Specific Gravity	Ca/Cc	Cr/Cc	Saturation Limit	Disiccation Limit	Max. Depth	Crust Saturation at DL
1	2.677	0.035	0.064	5.144	2.260	0.831	0.355

Material type : 1

I	Ratio	Stress	Perm-	k/1+e	PK	Beta	Dsde	Alpha
1	7.970	0.000E+00	0.139E-01	0.155E-02	0.118E-02	-0.345E+01	-0.534E-02	
2	7.390	0.200E+01	0.725E-02	0.864E-03	0.849E-03	-0.370E+01	-0.320E-02	
3	6.620	0.500E+01	0.307E-02	0.403E-03	0.472E-03	-0.593E+01	-0.239E-02	
4	6.040	0.100E+02	0.160E-02	0.227E-03	0.236E-03	-0.129E+02	-0.294E-02	
5	5.460	0.200E+02	0.835E-03	0.129E-03	0.148E-03	-0.220E+02	-0.284E-02	
6	5.130	0.300E+02	0.570E-03	0.930E-04	0.953E-04	-0.345E+02	-0.321E-02	
7	4.880	0.400E+02	0.435E-03	0.740E-04	0.604E-04	-0.602E+02	-0.446E-02	
8	4.300	0.800E+02	0.227E-03	0.428E-04	0.422E-04	-0.103E+03	-0.443E-02	
9	3.720	0.160E+03	0.118E-03	0.250E-04	0.241E-04	-0.207E+03	-0.517E-02	
10	3.140	0.320E+03	0.618E-04	0.149E-04	0.138E-04	-0.414E+03	-0.618E-02	
11	2.560	0.640E+03	0.322E-04	0.904E-05	0.101E-04	-0.552E+03	-0.499E-02	

Summary of lifts and print detail

Time days	Material Type	Fill Height	# Sub-layers	Void ratio	Start Day	Dessic. Month	Print detail
0.	1	0.1	5	7.97	115.	5	1
6.	1	1.4	40	7.97	115.	5	1

12.	1	1.0	40	7.97	115.	5	1
18.	1	1.0	40	7.97	115.	5	1
24.	1	1.0	40	7.97	115.	5	1
25.				115.	5	1	
40.				115.	5	1	
55.				115.	5	1	
85.				115.	5	1	
115.				115.	5	1	
145.				115.	5	1	
175.				115.	5	1	
205.				115.	5	1	
295.				115.	5	1	
390.				115.	5	1	
755.				115.	5	1	
1120.				115.	5	1	
2215.				115.	5	1	
3675.				115.	5	1	
7325.				115.	5	1	

Summary of monthly rainfall and evaporation potential

Month	Rainfall	Evaporation
1	0.470	0.140
2	0.270	0.180
3	0.280	0.290
4	0.390	0.380
5	0.370	0.490
6	0.490	0.510
7	0.580	0.510
8	0.590	0.480
9	0.500	0.370
10	0.310	0.310
11	0.360	0.180
12	0.330	0.140

*****Calculation data*****

tau	Lower layer Void ratio	Lower layer Permeability	drainage path Length
.249E-01	3.380	0.10000E-05	z = 1.14

Summary of desiccation parameters

Parameter	Value
Surface Drainage Efficiency	0.80
maximum evaporation efficiency	0.75
time to desic. after initial fill	115.00
month of initial desiccation	5
elevation of fixed water table	0.71
elevation of top of incompres. found.	-0.93

*****Initial Conditions in Dredged Fill*****

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
0.10	0.10	0.01	7.97	7.97	7.97	1
0.08	0.08	0.01	7.97	7.97	7.90	1
0.06	0.06	0.01	7.97	7.97	7.83	1
0.04	0.04	0.00	7.97	7.97	7.77	1
0.02	0.02	0.00	7.97	7.97	7.70	1
0.00	0.00	0.00	7.97	7.97	7.63	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
0.10	96.03	0.00	96.03	96.03	0.00	1
0.08	97.51	0.00	97.51	97.28	0.23	1
0.06	99.00	0.00	99.00	98.53	0.47	1
0.04	100.48	0.00	100.48	99.78	0.70	1
0.02	101.96	0.00	101.96	101.03	0.93	1
0.00	103.44	0.00	103.44	102.27	1.17	1

Time = 0. Degree of Consolidation = 0.0%

Total Settlement = 0.000

Settlement at End of Primary Consolidation = 0.002

Settlement caused by Primary Consolidation at time 0. = 0.000

Settlement caused by Secondary Compression at time 0. = 0.000

*****Current Conditions in Dredged Fill*****

***** Coordinates ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
0.10	0.10	0.01	7.97	7.97	7.97	1
0.08	0.08	0.01	7.97	7.90	7.90	1
0.06	0.06	0.01	7.97	7.84	7.83	1
0.04	0.04	0.00	7.97	7.77	7.77	1
0.02	0.02	0.00	7.97	7.71	7.70	1
0.00	0.00	0.00	7.97	7.64	7.63	1

***** Stresses ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
0.10	96.15	0.00	96.15	96.15	0.00	1
0.08	97.62	0.23	97.40	97.39	0.01	1
0.06	99.09	0.45	98.64	98.62	0.02	1
0.04	100.55	0.68	99.87	99.85	0.02	1
0.02	102.00	0.90	101.10	101.07	0.03	1
0.00	103.44	1.12	102.32	102.27	0.04	1

Time = 6. Degree of Consolidation = 97.0%

Total Settlement = 0.002

Settlement at End of Primary Consolidation = 0.002

Settlement caused by Primary Consolidation at time 6. = 0.002

Settlement caused by Secondary Compression at time 6. = 0.000

Surface Elevation = -0.83

*****Current Conditions in Dredged Fill*****

***** Coordinates *****

***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
1.50	1.48	0.17	7.97	7.97	7.97	1
1.46	1.45	0.16	7.97	7.97	7.85	1
1.43	1.41	0.16	7.97	7.97	7.73	1
1.39	1.38	0.16	7.97	7.97	7.61	1
1.36	1.34	0.15	7.97	7.97	7.50	1
1.32	1.31	0.15	7.97	7.97	7.38	1
1.29	1.27	0.14	7.97	7.97	7.27	1
1.25	1.24	0.14	7.97	7.97	7.17	1
1.22	1.20	0.14	7.97	7.97	7.06	1
1.18	1.17	0.13	7.97	7.97	6.96	1
1.15	1.13	0.13	7.97	7.97	6.86	1
1.11	1.10	0.12	7.97	7.97	6.75	1
1.08	1.06	0.12	7.97	7.97	6.65	1
1.05	1.03	0.12	7.97	7.97	6.58	1
1.01	0.99	0.11	7.97	7.97	6.54	1
0.98	0.96	0.11	7.97	7.97	6.49	1
0.94	0.92	0.10	7.97	7.97	6.44	1
0.91	0.89	0.10	7.97	7.97	6.39	1
0.87	0.85	0.10	7.97	7.97	6.35	1
0.84	0.82	0.09	7.97	7.97	6.30	1
0.80	0.78	0.09	7.97	7.96	6.25	1
0.77	0.75	0.09	7.97	7.96	6.21	1
0.73	0.71	0.08	7.97	7.96	6.16	1
0.70	0.68	0.08	7.97	7.96	6.11	1
0.66	0.64	0.07	7.97	7.95	6.06	1
0.62	0.61	0.07	7.97	7.95	6.03	1
0.59	0.57	0.07	7.97	7.94	6.00	1
0.55	0.54	0.06	7.97	7.93	5.98	1
0.52	0.50	0.06	7.97	7.92	5.96	1
0.48	0.47	0.05	7.97	7.90	5.93	1
0.45	0.43	0.05	7.97	7.89	5.91	1
0.41	0.40	0.05	7.97	7.87	5.89	1
0.38	0.36	0.04	7.97	7.85	5.86	1
0.34	0.33	0.04	7.97	7.82	5.84	1
0.31	0.30	0.03	7.97	7.79	5.81	1
0.28	0.26	0.03	7.97	7.75	5.79	1
0.24	0.23	0.03	7.97	7.71	5.77	1
0.21	0.19	0.02	7.97	7.66	5.74	1
0.17	0.16	0.02	7.97	7.61	5.72	1
0.14	0.13	0.02	7.97	7.54	5.70	1
0.10	0.09	0.01	7.97	7.47	5.67	1
0.10	0.09	0.01	7.97	7.47	5.67	1
0.08	0.07	0.01	7.97	7.43	5.66	1
0.06	0.06	0.01	7.97	7.38	5.65	1
0.04	0.04	0.00	7.97	7.33	5.63	1
0.02	0.02	0.00	7.97	7.28	5.62	1
0.00	0.00	0.00	7.97	7.23	5.61	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
1.48	9.77	0.00	9.77	9.77	0.00	1
1.45	12.36	0.00	12.36	11.96	0.41	1
1.41	14.96	0.00	14.96	14.14	0.82	1
1.38	17.55	0.00	17.55	16.32	1.22	1
1.34	20.14	0.00	20.14	18.51	1.63	1
1.31	22.73	0.00	22.73	20.69	2.04	1
1.27	25.33	0.00	25.33	22.88	2.45	1
1.24	27.92	0.00	27.92	25.06	2.86	1
1.20	30.51	0.00	30.51	27.24	3.27	1
1.17	33.10	0.00	33.10	29.43	3.67	1
1.13	35.70	0.00	35.69	31.61	4.08	1
1.10	38.29	0.00	38.29	33.80	4.49	1
1.06	40.88	0.00	40.88	35.98	4.90	1
1.03	43.47	0.00	43.47	38.16	5.31	1
0.99	46.06	0.00	46.06	40.35	5.71	1
0.96	48.66	0.00	48.65	42.53	6.12	1
0.92	51.25	0.00	51.24	44.72	6.53	1
0.89	53.84	0.01	53.83	46.90	6.93	1
0.85	56.43	0.01	56.42	49.08	7.34	1
0.82	59.02	0.01	59.01	51.27	7.74	1
0.78	61.61	0.02	61.59	53.45	8.15	1
0.75	64.21	0.03	64.18	55.63	8.55	1
0.71	66.80	0.04	66.76	57.81	8.95	1
0.68	69.38	0.05	69.34	59.99	9.34	1
0.64	71.97	0.07	71.91	62.17	9.73	1
0.61	74.56	0.09	74.47	64.35	10.12	1
0.57	77.15	0.11	77.03	66.53	10.51	1
0.54	79.73	0.14	79.59	68.70	10.88	1
0.50	82.31	0.18	82.13	70.88	11.25	1
0.47	84.89	0.23	84.66	73.05	11.61	1
0.43	87.46	0.28	87.18	75.21	11.97	1
0.40	90.03	0.35	89.68	77.37	12.31	1
0.36	92.60	0.43	92.17	79.53	12.64	1
0.33	95.16	0.52	94.63	81.68	12.95	1
0.30	97.71	0.63	97.08	83.82	13.25	1
0.26	100.25	0.76	99.49	85.96	13.53	1
0.23	102.78	0.90	101.88	88.08	13.80	1
0.19	105.31	1.07	104.24	90.20	14.04	1
0.16	107.82	1.26	106.56	92.30	14.26	1
0.13	110.31	1.47	108.84	94.39	14.45	1
0.09	112.79	1.72	111.07	96.46	14.61	1
0.09	112.79	1.72	111.07	96.46	14.61	1
0.07	114.20	1.87	112.34	97.64	14.70	1
0.06	115.61	2.03	113.58	98.81	14.77	1
0.04	117.00	2.22	114.78	99.97	14.81	1
0.02	118.39	2.42	115.97	101.13	14.84	1
0.00	119.77	2.64	117.14	102.27	14.86	1

Time = 12. Degree of Consolidation = 7.0%

Total Settlement = 0.018

Settlement at End of Primary Consolidation = 0.265

Settlement caused by Primary Consolidation at time 12. = 0.018

Settlement caused by Secondary Compression at time 12. = 0.000

Surface Elevation = 0.55

*****Current Conditions in Dredged Fill*****

***** Coordinates *****

***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
2.50	2.47	0.28	7.97	7.97	7.97	1
2.47	2.44	0.28	7.97	7.97	7.89	1
2.45	2.42	0.27	7.97	7.97	7.80	1
2.42	2.39	0.27	7.97	7.97	7.72	1
2.40	2.37	0.27	7.97	7.97	7.63	1
2.37	2.34	0.26	7.97	7.97	7.55	1
2.35	2.32	0.26	7.97	7.97	7.46	1
2.32	2.29	0.26	7.97	7.97	7.38	1
2.30	2.27	0.26	7.97	7.97	7.30	1
2.27	2.24	0.25	7.97	7.97	7.23	1
2.25	2.22	0.25	7.97	7.97	7.15	1
2.22	2.19	0.25	7.97	7.97	7.08	1
2.20	2.17	0.25	7.97	7.97	7.01	1
2.17	2.14	0.24	7.97	7.97	6.93	1
2.15	2.12	0.24	7.97	7.97	6.86	1
2.12	2.09	0.24	7.97	7.97	6.78	1
2.10	2.07	0.23	7.97	7.97	6.71	1
2.07	2.04	0.23	7.97	7.97	6.63	1
2.05	2.02	0.23	7.97	7.97	6.59	1
2.02	1.99	0.23	7.97	7.97	6.56	1
2.00	1.97	0.22	7.97	7.97	6.52	1
1.97	1.94	0.22	7.97	7.97	6.49	1
1.95	1.92	0.22	7.97	7.97	6.46	1
1.92	1.89	0.21	7.97	7.97	6.42	1
1.90	1.87	0.21	7.97	7.97	6.39	1
1.87	1.84	0.21	7.97	7.97	6.35	1
1.85	1.82	0.21	7.97	7.97	6.32	1
1.82	1.79	0.20	7.97	7.97	6.29	1
1.80	1.77	0.20	7.97	7.97	6.25	1
1.77	1.74	0.20	7.97	7.97	6.22	1
1.75	1.72	0.20	7.97	7.97	6.19	1
1.72	1.69	0.19	7.97	7.97	6.15	1
1.70	1.67	0.19	7.97	7.97	6.12	1
1.67	1.64	0.19	7.97	7.97	6.08	1

1.65	1.62	0.18	7.97	7.97	6.05	1
1.62	1.59	0.18	7.97	7.97	6.03	1
1.60	1.57	0.18	7.97	7.97	6.01	1
1.57	1.54	0.18	7.97	7.97	5.99	1
1.55	1.52	0.17	7.97	7.97	5.98	1
1.52	1.49	0.17	7.97	7.97	5.96	1
1.50	1.47	0.17	7.97	7.97	5.94	1
1.50	1.47	0.17	7.97	7.97	5.94	1
1.46	1.43	0.16	7.97	7.97	5.92	1
1.43	1.40	0.16	7.97	7.97	5.90	1
1.39	1.36	0.16	7.97	7.97	5.87	1
1.36	1.33	0.15	7.97	7.97	5.85	1
1.32	1.29	0.15	7.97	7.97	5.82	1
1.29	1.26	0.14	7.97	7.97	5.80	1
1.25	1.22	0.14	7.97	7.97	5.78	1
1.22	1.19	0.14	7.97	7.97	5.75	1
1.18	1.15	0.13	7.97	7.96	5.73	1
1.15	1.12	0.13	7.97	7.96	5.71	1
1.11	1.08	0.12	7.97	7.96	5.68	1
1.08	1.05	0.12	7.97	7.96	5.66	1
1.05	1.01	0.12	7.97	7.96	5.64	1
1.01	0.98	0.11	7.97	7.95	5.61	1
0.98	0.94	0.11	7.97	7.95	5.59	1
0.94	0.91	0.10	7.97	7.94	5.56	1
0.91	0.87	0.10	7.97	7.94	5.54	1
0.87	0.84	0.10	7.97	7.93	5.52	1
0.84	0.80	0.09	7.97	7.93	5.49	1
0.80	0.77	0.09	7.97	7.92	5.47	1
0.77	0.73	0.09	7.97	7.91	5.45	1
0.73	0.70	0.08	7.97	7.90	5.44	1
0.70	0.66	0.08	7.97	7.88	5.43	1
0.66	0.63	0.07	7.97	7.87	5.41	1
0.62	0.59	0.07	7.97	7.85	5.40	1
0.59	0.56	0.07	7.97	7.83	5.38	1
0.55	0.53	0.06	7.97	7.81	5.37	1
0.52	0.49	0.06	7.97	7.79	5.36	1
0.48	0.46	0.05	7.97	7.77	5.34	1
0.45	0.42	0.05	7.97	7.74	5.33	1
0.41	0.39	0.05	7.97	7.71	5.32	1
0.38	0.36	0.04	7.97	7.67	5.30	1
0.34	0.32	0.04	7.97	7.63	5.29	1
0.31	0.29	0.03	7.97	7.59	5.28	1
0.28	0.25	0.03	7.97	7.55	5.26	1
0.24	0.22	0.03	7.97	7.49	5.25	1
0.21	0.19	0.02	7.97	7.44	5.24	1
0.17	0.16	0.02	7.97	7.37	5.22	1
0.14	0.12	0.02	7.97	7.30	5.21	1
0.10	0.09	0.01	7.97	7.23	5.20	1
0.10	0.09	0.01	7.97	7.23	5.20	1
0.08	0.07	0.01	7.97	7.19	5.19	1
0.06	0.05	0.01	7.97	7.14	5.18	1
0.04	0.04	0.00	7.97	7.10	5.17	1
0.02	0.02	0.00	7.97	7.05	5.17	1
0.00	0.00	0.00	7.97	7.01	5.16	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
2.47	0.00	0.00	0.00	0.00	0.00	1
2.44	1.85	0.00	1.85	1.56	0.29	1
2.42	3.70	0.00	3.70	3.12	0.58	1
2.39	5.55	0.00	5.55	4.68	0.87	1
2.37	7.41	0.00	7.41	6.24	1.17	1
2.34	9.26	0.00	9.26	7.80	1.46	1
2.32	11.11	0.00	11.11	9.36	1.75	1
2.29	12.96	0.00	12.96	10.92	2.04	1
2.27	14.81	0.00	14.81	12.48	2.33	1
2.24	16.66	0.00	16.66	14.04	2.62	1
2.22	18.52	0.00	18.52	15.60	2.92	1
2.19	20.37	0.00	20.37	17.16	3.21	1
2.17	22.22	0.00	22.22	18.72	3.50	1
2.14	24.07	0.00	24.07	20.28	3.79	1
2.12	25.92	0.00	25.92	21.84	4.08	1
2.09	27.77	0.00	27.77	23.40	4.37	1
2.07	29.63	0.00	29.63	24.96	4.67	1
2.04	31.48	0.00	31.48	26.52	4.96	1
2.02	33.33	0.00	33.33	28.08	5.25	1
1.99	35.18	0.00	35.18	29.64	5.54	1
1.97	37.03	0.00	37.03	31.20	5.83	1
1.94	38.88	0.00	38.88	32.76	6.12	1
1.92	40.74	0.00	40.74	34.32	6.42	1
1.89	42.59	0.00	42.59	35.88	6.71	1
1.87	44.44	0.00	44.44	37.44	7.00	1
1.84	46.29	0.00	46.29	39.00	7.29	1
1.82	48.14	0.00	48.14	40.56	7.58	1
1.79	49.99	0.00	49.99	42.12	7.87	1
1.77	51.85	0.00	51.85	43.68	8.17	1
1.74	53.70	0.00	53.70	45.24	8.46	1
1.72	55.55	0.00	55.55	46.80	8.75	1
1.69	57.40	0.00	57.40	48.36	9.04	1
1.67	59.25	0.00	59.25	49.92	9.33	1
1.64	61.10	0.00	61.10	51.48	9.62	1
1.62	62.96	0.00	62.96	53.04	9.92	1
1.59	64.81	0.00	64.81	54.60	10.21	1
1.57	66.66	0.00	66.66	56.16	10.50	1
1.54	68.51	0.00	68.51	57.72	10.79	1
1.52	70.36	0.00	70.36	59.28	11.08	1
1.49	72.21	0.00	72.21	60.84	11.37	1
1.47	74.07	0.00	74.06	62.40	11.66	1
1.47	74.07	0.00	74.06	62.40	11.66	1
1.43	76.66	0.00	76.66	64.58	12.07	1
1.40	79.25	0.00	79.25	66.77	12.48	1
1.36	81.84	0.00	81.84	68.95	12.89	1
1.33	84.43	0.01	84.43	71.13	13.29	1
1.29	87.03	0.01	87.02	73.32	13.70	1
1.26	89.62	0.01	89.61	75.50	14.11	1
1.22	92.21	0.01	92.20	77.68	14.51	1

1.19	94.80	0.02	94.78	79.87	14.92	1
1.15	97.39	0.02	97.37	82.05	15.32	1
1.12	99.98	0.03	99.96	84.23	15.72	1
1.08	102.57	0.03	102.54	86.41	16.13	1
1.05	105.16	0.04	105.12	88.60	16.53	1
1.01	107.75	0.05	107.70	90.78	16.93	1
0.98	110.34	0.06	110.28	92.96	17.32	1
0.94	112.93	0.07	112.85	95.14	17.72	1
0.91	115.51	0.09	115.43	97.31	18.11	1
0.87	118.10	0.11	117.99	99.49	18.50	1
0.84	120.68	0.13	120.55	101.67	18.89	1
0.80	123.27	0.15	123.11	103.84	19.27	1
0.77	125.85	0.18	125.66	106.01	19.65	1
0.73	128.42	0.22	128.21	108.18	20.02	1
0.70	131.00	0.25	130.75	110.35	20.39	1
0.66	133.57	0.30	133.28	112.52	20.76	1
0.63	136.14	0.35	135.80	114.68	21.12	1
0.59	138.71	0.40	138.31	116.83	21.47	1
0.56	141.27	0.47	140.80	118.99	21.82	1
0.53	143.83	0.54	143.29	121.14	22.15	1
0.49	146.38	0.61	145.76	123.28	22.48	1
0.46	148.92	0.70	148.22	125.42	22.80	1
0.42	151.46	0.80	150.66	127.55	23.12	1
0.39	154.00	0.91	153.09	129.67	23.42	1
0.36	156.52	1.03	155.49	131.79	23.71	1
0.32	159.04	1.16	157.88	133.90	23.98	1
0.29	161.54	1.30	160.24	135.99	24.24	1
0.25	164.04	1.47	162.57	138.08	24.49	1
0.22	166.52	1.64	164.88	140.15	24.72	1
0.19	168.99	1.84	167.15	142.21	24.93	1
0.16	171.44	2.07	169.37	144.26	25.11	1
0.12	173.88	2.34	171.54	146.29	25.25	1
0.09	176.30	2.62	173.68	148.30	25.38	1
0.09	176.30	2.62	173.68	148.30	25.38	1
0.07	177.68	2.79	174.89	149.45	25.45	1
0.05	179.05	2.96	176.09	150.58	25.51	1
0.04	180.41	3.13	177.28	151.71	25.57	1
0.02	181.77	3.31	178.45	152.84	25.62	1
0.00	183.12	3.50	179.62	153.95	25.67	1

Time = 18. Degree of Consolidation = 6%

Total Settlement = 0.033

Settlement at End of Primary Consolidation = 0.557

Settlement caused by Primary Consolidation at time 18. = 0.033

Settlement caused by Secondary Compression at time 18. = 0.000

Surface Elevation = 1.54

*****Current Conditions in Dredged Fill*****

***** Coordinates *****

***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
3.50	3.45	0.39	7.97	7.97	7.97	1
3.47	3.43	0.39	7.97	7.97	7.89	1
3.45	3.40	0.38	7.97	7.97	7.80	1
3.42	3.38	0.38	7.97	7.97	7.72	1
3.40	3.35	0.38	7.97	7.97	7.63	1
3.37	3.33	0.38	7.97	7.97	7.55	1
3.35	3.30	0.37	7.97	7.97	7.46	1
3.32	3.28	0.37	7.97	7.97	7.38	1
3.30	3.25	0.37	7.97	7.97	7.30	1
3.27	3.23	0.37	7.97	7.97	7.23	1
3.25	3.20	0.36	7.97	7.97	7.15	1
3.22	3.18	0.36	7.97	7.97	7.08	1
3.20	3.15	0.36	7.97	7.97	7.01	1
3.17	3.13	0.35	7.97	7.97	6.93	1
3.15	3.10	0.35	7.97	7.97	6.86	1
3.12	3.08	0.35	7.97	7.97	6.78	1
3.10	3.05	0.35	7.97	7.97	6.71	1
3.07	3.03	0.34	7.97	7.97	6.63	1
3.05	3.00	0.34	7.97	7.97	6.59	1
3.02	2.98	0.34	7.97	7.97	6.56	1
3.00	2.95	0.33	7.97	7.97	6.52	1
2.97	2.93	0.33	7.97	7.97	6.49	1
2.95	2.90	0.33	7.97	7.97	6.46	1
2.92	2.88	0.33	7.97	7.97	6.42	1
2.90	2.85	0.32	7.97	7.97	6.39	1
2.87	2.83	0.32	7.97	7.97	6.35	1
2.85	2.80	0.32	7.97	7.97	6.32	1
2.82	2.78	0.31	7.97	7.97	6.29	1
2.80	2.75	0.31	7.97	7.97	6.25	1
2.77	2.73	0.31	7.97	7.97	6.22	1
2.75	2.70	0.31	7.97	7.97	6.19	1
2.72	2.68	0.30	7.97	7.97	6.15	1
2.70	2.65	0.30	7.97	7.97	6.12	1
2.67	2.63	0.30	7.97	7.97	6.08	1
2.65	2.60	0.30	7.97	7.97	6.05	1
2.62	2.58	0.29	7.97	7.97	6.03	1
2.60	2.55	0.29	7.97	7.97	6.01	1
2.57	2.53	0.29	7.97	7.97	5.99	1
2.55	2.50	0.28	7.97	7.97	5.98	1
2.52	2.48	0.28	7.97	7.97	5.96	1
2.50	2.45	0.28	7.97	7.97	5.94	1
2.50	2.45	0.28	7.97	7.97	5.94	1
2.47	2.43	0.28	7.97	7.97	5.93	1
2.45	2.40	0.27	7.97	7.97	5.91	1
2.42	2.38	0.27	7.97	7.97	5.89	1
2.40	2.35	0.27	7.97	7.97	5.88	1

2.37	2.33	0.26	7.97	7.97	5.86	1
2.35	2.30	0.26	7.97	7.97	5.84	1
2.32	2.28	0.26	7.97	7.97	5.82	1
2.30	2.25	0.26	7.97	7.97	5.81	1
2.27	2.23	0.25	7.97	7.97	5.79	1
2.25	2.20	0.25	7.97	7.97	5.77	1
2.22	2.18	0.25	7.97	7.97	5.76	1
2.20	2.15	0.25	7.97	7.97	5.74	1
2.17	2.13	0.24	7.97	7.97	5.72	1
2.15	2.10	0.24	7.97	7.97	5.71	1
2.12	2.08	0.24	7.97	7.97	5.69	1
2.10	2.05	0.23	7.97	7.97	5.67	1
2.07	2.03	0.23	7.97	7.97	5.66	1
2.05	2.00	0.23	7.97	7.97	5.64	1
2.02	1.98	0.23	7.97	7.97	5.62	1
2.00	1.95	0.22	7.97	7.97	5.61	1
1.97	1.93	0.22	7.97	7.97	5.59	1
1.95	1.90	0.22	7.97	7.97	5.57	1
1.92	1.88	0.21	7.97	7.97	5.55	1
1.90	1.85	0.21	7.97	7.97	5.54	1
1.87	1.83	0.21	7.97	7.97	5.52	1
1.85	1.80	0.21	7.97	7.97	5.50	1
1.82	1.78	0.20	7.97	7.97	5.49	1
1.80	1.75	0.20	7.97	7.97	5.47	1
1.77	1.73	0.20	7.97	7.97	5.46	1
1.75	1.70	0.20	7.97	7.97	5.45	1
1.72	1.68	0.19	7.97	7.97	5.44	1
1.70	1.65	0.19	7.97	7.97	5.43	1
1.67	1.63	0.19	7.97	7.97	5.42	1
1.65	1.60	0.18	7.97	7.97	5.41	1
1.62	1.58	0.18	7.97	7.97	5.40	1
1.60	1.55	0.18	7.97	7.97	5.39	1
1.57	1.53	0.18	7.97	7.97	5.38	1
1.55	1.50	0.17	7.97	7.97	5.37	1
1.52	1.48	0.17	7.97	7.96	5.36	1
1.50	1.45	0.17	7.97	7.96	5.35	1
1.50	1.45	0.17	7.97	7.96	5.35	1
1.46	1.42	0.16	7.97	7.96	5.34	1
1.43	1.38	0.16	7.97	7.96	5.32	1
1.39	1.35	0.16	7.97	7.96	5.31	1
1.36	1.31	0.15	7.97	7.96	5.30	1
1.32	1.28	0.15	7.97	7.95	5.28	1
1.29	1.24	0.14	7.97	7.95	5.27	1
1.25	1.21	0.14	7.97	7.95	5.26	1
1.22	1.17	0.14	7.97	7.95	5.24	1
1.18	1.14	0.13	7.97	7.94	5.23	1
1.15	1.10	0.13	7.97	7.94	5.22	1
1.11	1.07	0.12	7.97	7.93	5.20	1
1.08	1.03	0.12	7.97	7.92	5.19	1
1.05	1.00	0.12	7.97	7.92	5.17	1
1.01	0.96	0.11	7.97	7.91	5.16	1
0.98	0.93	0.11	7.97	7.90	5.15	1
0.94	0.89	0.10	7.97	7.89	5.13	1
0.91	0.86	0.10	7.97	7.88	5.12	1

0.87	0.83	0.10	7.97	7.87	5.11	1
0.84	0.79	0.09	7.97	7.86	5.10	1
0.80	0.76	0.09	7.97	7.84	5.09	1
0.77	0.72	0.09	7.97	7.83	5.08	1
0.73	0.69	0.08	7.97	7.81	5.07	1
0.70	0.65	0.08	7.97	7.79	5.06	1
0.66	0.62	0.07	7.97	7.77	5.05	1
0.62	0.58	0.07	7.97	7.75	5.04	1
0.59	0.55	0.07	7.97	7.72	5.03	1
0.55	0.52	0.06	7.97	7.69	5.02	1
0.52	0.48	0.06	7.97	7.66	5.01	1
0.48	0.45	0.05	7.97	7.63	5.00	1
0.45	0.41	0.05	7.97	7.60	4.99	1
0.41	0.38	0.05	7.97	7.56	4.98	1
0.38	0.35	0.04	7.97	7.52	4.97	1
0.34	0.32	0.04	7.97	7.48	4.96	1
0.31	0.28	0.03	7.97	7.43	4.95	1
0.28	0.25	0.03	7.97	7.38	4.94	1
0.24	0.22	0.03	7.97	7.32	4.93	1
0.21	0.18	0.02	7.97	7.26	4.92	1
0.17	0.15	0.02	7.97	7.20	4.91	1
0.14	0.12	0.02	7.97	7.13	4.90	1
0.10	0.09	0.01	7.97	7.06	4.89	1
0.10	0.09	0.01	7.97	7.06	4.89	1
0.08	0.07	0.01	7.97	7.02	4.88	1
0.06	0.05	0.01	7.97	6.98	4.88	1
0.04	0.04	0.00	7.97	6.94	4.87	1
0.02	0.02	0.00	7.97	6.90	4.87	1
0.00	0.00	0.00	7.97	6.85	4.87	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
3.45	0.00	0.00	0.00	0.00	0.00	1
3.43	1.85	0.00	1.85	1.56	0.29	1
3.40	3.70	0.00	3.70	3.12	0.58	1
3.38	5.55	0.00	5.55	4.68	0.87	1
3.35	7.41	0.00	7.41	6.24	1.17	1
3.33	9.26	0.00	9.26	7.80	1.46	1
3.30	11.11	0.00	11.11	9.36	1.75	1
3.28	12.96	0.00	12.96	10.92	2.04	1
3.25	14.81	0.00	14.81	12.48	2.33	1
3.23	16.66	0.00	16.66	14.04	2.62	1
3.20	18.52	0.00	18.52	15.60	2.92	1
3.18	20.37	0.00	20.37	17.16	3.21	1
3.15	22.22	0.00	22.22	18.72	3.50	1
3.13	24.07	0.00	24.07	20.28	3.79	1
3.10	25.92	0.00	25.92	21.84	4.08	1
3.08	27.77	0.00	27.77	23.40	4.37	1
3.05	29.63	0.00	29.63	24.96	4.67	1
3.03	31.48	0.00	31.48	26.52	4.96	1
3.00	33.33	0.00	33.33	28.08	5.25	1
2.98	35.18	0.00	35.18	29.64	5.54	1

2.95	37.03	0.00	37.03	31.20	5.83	1
2.93	38.88	0.00	38.88	32.76	6.12	1
2.90	40.74	0.00	40.74	34.32	6.42	1
2.88	42.59	0.00	42.59	35.88	6.71	1
2.85	44.44	0.00	44.44	37.44	7.00	1
2.83	46.29	0.00	46.29	39.00	7.29	1
2.80	48.14	0.00	48.14	40.56	7.58	1
2.78	49.99	0.00	49.99	42.12	7.87	1
2.75	51.85	0.00	51.85	43.68	8.17	1
2.73	53.70	0.00	53.70	45.24	8.46	1
2.70	55.55	0.00	55.55	46.80	8.75	1
2.68	57.40	0.00	57.40	48.36	9.04	1
2.65	59.25	0.00	59.25	49.92	9.33	1
2.63	61.10	0.00	61.10	51.48	9.62	1
2.60	62.96	0.00	62.96	53.04	9.92	1
2.58	64.81	0.00	64.81	54.60	10.21	1
2.55	66.66	0.00	66.66	56.16	10.50	1
2.53	68.51	0.00	68.51	57.72	10.79	1
2.50	70.36	0.00	70.36	59.28	11.08	1
2.48	72.21	0.00	72.21	60.84	11.37	1
2.45	74.07	0.00	74.07	62.40	11.67	1
2.45	74.07	0.00	74.07	62.40	11.67	1
2.43	75.92	0.00	75.92	63.96	11.96	1
2.40	77.77	0.00	77.77	65.52	12.25	1
2.38	79.62	0.00	79.62	67.08	12.54	1
2.35	81.47	0.00	81.47	68.64	12.83	1
2.33	83.32	0.00	83.32	70.20	13.12	1
2.30	85.18	0.00	85.18	71.76	13.42	1
2.28	87.03	0.00	87.03	73.32	13.71	1
2.25	88.88	0.00	88.88	74.88	14.00	1
2.23	90.73	0.00	90.73	76.44	14.29	1
2.20	92.58	0.00	92.58	78.00	14.58	1
2.18	94.43	0.00	94.43	79.56	14.87	1
2.15	96.29	0.00	96.29	81.12	15.17	1
2.13	98.14	0.00	98.14	82.68	15.46	1
2.10	99.99	0.00	99.99	84.24	15.75	1
2.08	101.84	0.00	101.84	85.80	16.04	1
2.05	103.69	0.00	103.69	87.36	16.33	1
2.03	105.54	0.00	105.54	88.92	16.62	1
2.00	107.40	0.00	107.39	90.48	16.92	1
1.98	109.25	0.00	109.25	92.04	17.21	1
1.95	111.10	0.00	111.10	93.60	17.50	1
1.93	112.95	0.00	112.95	95.16	17.79	1
1.90	114.80	0.00	114.80	96.72	18.08	1
1.88	116.65	0.00	116.65	98.28	18.37	1
1.85	118.51	0.00	118.50	99.84	18.66	1
1.83	120.36	0.00	120.35	101.40	18.96	1
1.80	122.21	0.00	122.21	102.96	19.25	1
1.78	124.06	0.00	124.06	104.52	19.54	1
1.75	125.91	0.00	125.91	106.08	19.83	1
1.73	127.76	0.00	127.76	107.64	20.12	1
1.70	129.61	0.01	129.61	109.20	20.41	1
1.68	131.47	0.01	131.46	110.76	20.70	1
1.65	133.32	0.01	133.31	112.32	20.99	1

1.63	135.17	0.01	135.16	113.88	21.28	1
1.60	137.02	0.01	137.01	115.44	21.57	1
1.58	138.87	0.01	138.86	117.00	21.86	1
1.55	140.72	0.01	140.71	118.56	22.15	1
1.53	142.57	0.01	142.56	120.12	22.44	1
1.50	144.42	0.02	144.41	121.67	22.73	1
1.48	146.27	0.02	146.25	123.23	23.02	1
1.45	148.12	0.02	148.10	124.79	23.31	1
1.45	148.12	0.02	148.10	124.79	23.31	1
1.42	150.72	0.03	150.69	126.97	23.71	1
1.38	153.31	0.03	153.27	129.16	24.12	1
1.35	155.90	0.04	155.86	131.34	24.52	1
1.31	158.48	0.04	158.44	133.52	24.92	1
1.28	161.07	0.05	161.02	135.70	25.32	1
1.24	163.66	0.06	163.60	137.88	25.72	1
1.21	166.25	0.07	166.18	140.06	26.12	1
1.17	168.84	0.09	168.75	142.24	26.51	1
1.14	171.42	0.10	171.32	144.42	26.91	1
1.10	174.01	0.12	173.89	146.59	27.30	1
1.07	176.59	0.13	176.46	148.77	27.69	1
1.03	179.17	0.16	179.02	150.94	28.08	1
1.00	181.75	0.18	181.57	153.11	28.46	1
0.96	184.33	0.21	184.12	155.28	28.84	1
0.93	186.91	0.24	186.67	157.45	29.22	1
0.89	189.48	0.27	189.21	159.62	29.60	1
0.86	192.05	0.31	191.75	161.78	29.97	1
0.83	194.62	0.35	194.28	163.94	30.33	1
0.79	197.19	0.39	196.80	166.10	30.70	1
0.76	199.75	0.44	199.31	168.25	31.06	1
0.72	202.31	0.50	201.81	170.41	31.41	1
0.69	204.87	0.56	204.31	172.55	31.76	1
0.65	207.42	0.62	206.79	174.69	32.10	1
0.62	209.96	0.70	209.27	176.83	32.44	1
0.58	212.50	0.77	211.73	178.96	32.77	1
0.55	215.04	0.86	214.18	181.09	33.09	1
0.52	217.57	0.95	216.61	183.21	33.40	1
0.48	220.09	1.05	219.04	185.32	33.71	1
0.45	222.60	1.16	221.44	187.43	34.01	1
0.41	225.11	1.28	223.83	189.53	34.30	1
0.38	227.61	1.41	226.20	191.62	34.58	1
0.35	230.09	1.55	228.55	193.70	34.85	1
0.32	232.57	1.70	230.87	195.77	35.11	1
0.28	235.04	1.87	233.17	197.82	35.35	1
0.25	237.49	2.05	235.44	199.87	35.57	1
0.22	239.93	2.27	237.66	201.90	35.76	1
0.18	242.36	2.51	239.85	203.92	35.93	1
0.15	244.77	2.75	242.02	205.92	36.10	1
0.12	247.17	3.01	244.16	207.91	36.25	1
0.09	249.55	3.27	246.28	209.88	36.39	1
0.09	249.55	3.27	246.28	209.88	36.39	1
0.07	250.90	3.43	247.47	211.00	36.47	1
0.05	252.25	3.59	248.66	212.12	36.55	1
0.04	253.59	3.75	249.84	213.22	36.62	1
0.02	254.92	3.92	251.01	214.33	36.68	1

0.00 256.25 4.09 252.17 215.42 36.74 1

Time = 24. Degree of Consolidation = 5.0%

Total Settlement = 0.048

Settlement at End of Primary Consolidation = 0.887

Settlement caused by Primary Consolidation at time 24. = 0.048

Settlement caused by Secondary Compression at time 24. = 0.000

Surface Elevation = 2.52

*****Current Conditions in Dredged Fill*****

***** Coordinates *****

***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
4.50	4.45	0.50	7.97	7.97	7.97	1
4.47	4.42	0.50	7.97	7.97	7.89	1
4.45	4.40	0.50	7.97	7.97	7.80	1
4.42	4.37	0.49	7.97	7.97	7.72	1
4.40	4.35	0.49	7.97	7.97	7.63	1
4.37	4.32	0.49	7.97	7.97	7.55	1
4.35	4.30	0.48	7.97	7.97	7.46	1
4.32	4.27	0.48	7.97	7.97	7.38	1
4.30	4.25	0.48	7.97	7.97	7.30	1
4.27	4.22	0.48	7.97	7.97	7.23	1
4.25	4.20	0.47	7.97	7.97	7.15	1
4.22	4.17	0.47	7.97	7.97	7.08	1
4.20	4.15	0.47	7.97	7.97	7.01	1
4.17	4.12	0.47	7.97	7.97	6.93	1
4.15	4.10	0.46	7.97	7.97	6.86	1
4.12	4.07	0.46	7.97	7.97	6.78	1
4.10	4.05	0.46	7.97	7.97	6.71	1
4.07	4.02	0.45	7.97	7.97	6.63	1
4.05	4.00	0.45	7.97	7.97	6.59	1
4.02	3.97	0.45	7.97	7.97	6.56	1
4.00	3.95	0.45	7.97	7.97	6.52	1
3.97	3.92	0.44	7.97	7.97	6.49	1
3.95	3.90	0.44	7.97	7.97	6.46	1
3.92	3.87	0.44	7.97	7.97	6.42	1
3.90	3.85	0.43	7.97	7.97	6.39	1
3.87	3.82	0.43	7.97	7.97	6.35	1
3.85	3.80	0.43	7.97	7.97	6.32	1
3.82	3.77	0.43	7.97	7.97	6.29	1
3.80	3.75	0.42	7.97	7.97	6.25	1
3.77	3.72	0.42	7.97	7.97	6.22	1

3.75	3.70	0.42	7.97	7.97	6.19	1
3.72	3.67	0.42	7.97	7.97	6.15	1
3.70	3.65	0.41	7.97	7.97	6.12	1
3.67	3.62	0.41	7.97	7.97	6.08	1
3.65	3.60	0.41	7.97	7.97	6.05	1
3.62	3.57	0.40	7.97	7.97	6.03	1
3.60	3.55	0.40	7.97	7.97	6.01	1
3.57	3.52	0.40	7.97	7.97	5.99	1
3.55	3.50	0.40	7.97	7.97	5.98	1
3.52	3.47	0.39	7.97	7.97	5.96	1
3.50	3.45	0.39	7.97	7.97	5.94	1
3.50	3.45	0.39	7.97	7.97	5.94	1
3.47	3.42	0.39	7.97	7.97	5.93	1
3.45	3.40	0.38	7.97	7.97	5.91	1
3.42	3.37	0.38	7.97	7.97	5.89	1
3.40	3.35	0.38	7.97	7.97	5.88	1
3.37	3.32	0.38	7.97	7.97	5.86	1
3.35	3.30	0.37	7.97	7.97	5.84	1
3.32	3.27	0.37	7.97	7.97	5.82	1
3.30	3.25	0.37	7.97	7.97	5.81	1
3.27	3.22	0.37	7.97	7.97	5.79	1
3.25	3.20	0.36	7.97	7.97	5.77	1
3.22	3.17	0.36	7.97	7.97	5.76	1
3.20	3.15	0.36	7.97	7.97	5.74	1
3.17	3.12	0.35	7.97	7.97	5.72	1
3.15	3.10	0.35	7.97	7.97	5.71	1
3.12	3.07	0.35	7.97	7.97	5.69	1
3.10	3.05	0.35	7.97	7.97	5.67	1
3.07	3.02	0.34	7.97	7.97	5.66	1
3.05	3.00	0.34	7.97	7.97	5.64	1
3.02	2.97	0.34	7.97	7.97	5.62	1
3.00	2.95	0.33	7.97	7.97	5.61	1
2.97	2.92	0.33	7.97	7.97	5.59	1
2.95	2.90	0.33	7.97	7.97	5.57	1
2.92	2.87	0.33	7.97	7.97	5.55	1
2.90	2.85	0.32	7.97	7.97	5.54	1
2.87	2.82	0.32	7.97	7.97	5.52	1
2.85	2.80	0.32	7.97	7.97	5.50	1
2.82	2.77	0.31	7.97	7.97	5.49	1
2.80	2.75	0.31	7.97	7.97	5.47	1
2.77	2.72	0.31	7.97	7.97	5.46	1
2.75	2.70	0.31	7.97	7.97	5.45	1
2.72	2.67	0.30	7.97	7.97	5.44	1
2.70	2.65	0.30	7.97	7.97	5.43	1
2.67	2.62	0.30	7.97	7.97	5.42	1
2.65	2.60	0.30	7.97	7.97	5.41	1
2.62	2.57	0.29	7.97	7.97	5.40	1
2.60	2.55	0.29	7.97	7.97	5.39	1
2.57	2.52	0.29	7.97	7.97	5.38	1
2.55	2.50	0.28	7.97	7.97	5.37	1
2.52	2.47	0.28	7.97	7.97	5.36	1
2.50	2.45	0.28	7.97	7.97	5.35	1
2.50	2.45	0.28	7.97	7.97	5.35	1
2.47	2.42	0.28	7.97	7.97	5.34	1

2.45	2.40	0.27	7.97	7.97	5.33	1
2.42	2.37	0.27	7.97	7.97	5.32	1
2.40	2.35	0.27	7.97	7.97	5.31	1
2.37	2.32	0.26	7.97	7.97	5.30	1
2.35	2.30	0.26	7.97	7.97	5.29	1
2.32	2.27	0.26	7.97	7.97	5.28	1
2.30	2.25	0.26	7.97	7.97	5.27	1
2.27	2.22	0.25	7.97	7.97	5.26	1
2.25	2.20	0.25	7.97	7.97	5.25	1
2.22	2.17	0.25	7.97	7.97	5.24	1
2.20	2.15	0.25	7.97	7.97	5.23	1
2.17	2.12	0.24	7.97	7.97	5.22	1
2.15	2.10	0.24	7.97	7.97	5.22	1
2.12	2.07	0.24	7.97	7.97	5.21	1
2.10	2.05	0.23	7.97	7.97	5.20	1
2.07	2.02	0.23	7.97	7.97	5.19	1
2.05	2.00	0.23	7.97	7.97	5.18	1
2.02	1.97	0.23	7.97	7.97	5.17	1
2.00	1.95	0.22	7.97	7.97	5.16	1
1.97	1.92	0.22	7.97	7.97	5.15	1
1.95	1.90	0.22	7.97	7.97	5.14	1
1.92	1.87	0.21	7.97	7.97	5.13	1
1.90	1.85	0.21	7.97	7.97	5.12	1
1.87	1.82	0.21	7.97	7.97	5.11	1
1.85	1.80	0.21	7.97	7.97	5.11	1
1.82	1.77	0.20	7.97	7.97	5.10	1
1.80	1.75	0.20	7.97	7.97	5.09	1
1.77	1.72	0.20	7.97	7.97	5.09	1
1.75	1.70	0.20	7.97	7.97	5.08	1
1.72	1.67	0.19	7.97	7.97	5.07	1
1.70	1.65	0.19	7.97	7.97	5.06	1
1.67	1.62	0.19	7.97	7.97	5.06	1
1.65	1.60	0.18	7.97	7.97	5.05	1
1.62	1.57	0.18	7.97	7.97	5.04	1
1.60	1.55	0.18	7.97	7.97	5.03	1
1.57	1.52	0.18	7.97	7.96	5.03	1
1.55	1.50	0.17	7.97	7.96	5.02	1
1.52	1.47	0.17	7.97	7.96	5.01	1
1.50	1.45	0.17	7.97	7.96	5.01	1
1.50	1.45	0.17	7.97	7.96	5.01	1
1.46	1.41	0.16	7.97	7.96	4.99	1
1.43	1.38	0.16	7.97	7.96	4.98	1
1.39	1.35	0.16	7.97	7.96	4.97	1
1.36	1.31	0.15	7.97	7.95	4.96	1
1.32	1.28	0.15	7.97	7.95	4.95	1
1.29	1.24	0.14	7.97	7.95	4.94	1
1.25	1.21	0.14	7.97	7.94	4.93	1
1.22	1.17	0.14	7.97	7.94	4.92	1
1.18	1.14	0.13	7.97	7.94	4.91	1
1.15	1.10	0.13	7.97	7.93	4.90	1
1.11	1.07	0.12	7.97	7.92	4.89	1
1.08	1.03	0.12	7.97	7.92	4.88	1
1.05	1.00	0.12	7.97	7.91	4.88	1
1.01	0.96	0.11	7.97	7.90	4.87	1

0.98	0.93	0.11	7.97	7.89	4.86	1
0.94	0.89	0.10	7.97	7.88	4.86	1
0.91	0.86	0.10	7.97	7.87	4.85	1
0.87	0.82	0.10	7.97	7.86	4.85	1
0.84	0.79	0.09	7.97	7.84	4.84	1
0.80	0.75	0.09	7.97	7.83	4.83	1
0.77	0.72	0.09	7.97	7.81	4.83	1
0.73	0.69	0.08	7.97	7.79	4.82	1
0.70	0.65	0.08	7.97	7.77	4.82	1
0.66	0.62	0.07	7.97	7.75	4.81	1
0.62	0.58	0.07	7.97	7.73	4.80	1
0.59	0.55	0.07	7.97	7.70	4.80	1
0.55	0.51	0.06	7.97	7.67	4.79	1
0.52	0.48	0.06	7.97	7.64	4.79	1
0.48	0.45	0.05	7.97	7.61	4.78	1
0.45	0.41	0.05	7.97	7.58	4.77	1
0.41	0.38	0.05	7.97	7.54	4.77	1
0.38	0.35	0.04	7.97	7.50	4.76	1
0.34	0.31	0.04	7.97	7.45	4.76	1
0.31	0.28	0.03	7.97	7.40	4.75	1
0.28	0.25	0.03	7.97	7.35	4.75	1
0.24	0.22	0.03	7.97	7.29	4.74	1
0.21	0.18	0.02	7.97	7.23	4.73	1
0.17	0.15	0.02	7.97	7.17	4.73	1
0.14	0.12	0.02	7.97	7.11	4.72	1
0.10	0.09	0.01	7.97	7.04	4.72	1
0.10	0.09	0.01	7.97	7.04	4.72	1
0.08	0.07	0.01	7.97	7.00	4.71	1
0.06	0.05	0.01	7.97	6.96	4.71	1
0.04	0.04	0.00	7.97	6.92	4.71	1
0.02	0.02	0.00	7.97	6.88	4.70	1
0.00	0.00	0.00	7.97	6.83	4.70	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
4.45	0.00	0.00	0.00	0.00	0.00	1
4.42	1.85	0.00	1.85	1.56	0.29	1
4.40	3.70	0.00	3.70	3.12	0.58	1
4.37	5.55	0.00	5.55	4.68	0.87	1
4.35	7.41	0.00	7.41	6.24	1.17	1
4.32	9.26	0.00	9.26	7.80	1.46	1
4.30	11.11	0.00	11.11	9.36	1.75	1
4.27	12.96	0.00	12.96	10.92	2.04	1
4.25	14.81	0.00	14.81	12.48	2.33	1
4.22	16.66	0.00	16.66	14.04	2.62	1
4.20	18.52	0.00	18.52	15.60	2.92	1
4.17	20.37	0.00	20.37	17.16	3.21	1
4.15	22.22	0.00	22.22	18.72	3.50	1
4.12	24.07	0.00	24.07	20.28	3.79	1
4.10	25.92	0.00	25.92	21.84	4.08	1
4.07	27.77	0.00	27.77	23.40	4.37	1
4.05	29.63	0.00	29.63	24.96	4.67	1

4.02	31.48	0.00	31.48	26.52	4.96	1
4.00	33.33	0.00	33.33	28.08	5.25	1
3.97	35.18	0.00	35.18	29.64	5.54	1
3.95	37.03	0.00	37.03	31.20	5.83	1
3.92	38.88	0.00	38.88	32.76	6.12	1
3.90	40.74	0.00	40.74	34.32	6.42	1
3.87	42.59	0.00	42.59	35.88	6.71	1
3.85	44.44	0.00	44.44	37.44	7.00	1
3.82	46.29	0.00	46.29	39.00	7.29	1
3.80	48.14	0.00	48.14	40.56	7.58	1
3.77	49.99	0.00	49.99	42.12	7.87	1
3.75	51.85	0.00	51.85	43.68	8.17	1
3.72	53.70	0.00	53.70	45.24	8.46	1
3.70	55.55	0.00	55.55	46.80	8.75	1
3.67	57.40	0.00	57.40	48.36	9.04	1
3.65	59.25	0.00	59.25	49.92	9.33	1
3.62	61.10	0.00	61.10	51.48	9.62	1
3.60	62.96	0.00	62.96	53.04	9.92	1
3.57	64.81	0.00	64.81	54.60	10.21	1
3.55	66.66	0.00	66.66	56.16	10.50	1
3.52	68.51	0.00	68.51	57.72	10.79	1
3.50	70.36	0.00	70.36	59.28	11.08	1
3.47	72.21	0.00	72.21	60.84	11.37	1
3.45	74.07	0.00	74.07	62.40	11.67	1
3.45	74.07	0.00	74.07	62.40	11.67	1
3.42	75.92	0.00	75.92	63.96	11.96	1
3.40	77.77	0.00	77.77	65.52	12.25	1
3.37	79.62	0.00	79.62	67.08	12.54	1
3.35	81.47	0.00	81.47	68.64	12.83	1
3.32	83.32	0.00	83.32	70.20	13.12	1
3.30	85.18	0.00	85.18	71.76	13.42	1
3.27	87.03	0.00	87.03	73.32	13.71	1
3.25	88.88	0.00	88.88	74.88	14.00	1
3.22	90.73	0.00	90.73	76.44	14.29	1
3.20	92.58	0.00	92.58	78.00	14.58	1
3.17	94.43	0.00	94.43	79.56	14.87	1
3.15	96.29	0.00	96.29	81.12	15.17	1
3.12	98.14	0.00	98.14	82.68	15.46	1
3.10	99.99	0.00	99.99	84.24	15.75	1
3.07	101.84	0.00	101.84	85.80	16.04	1
3.05	103.69	0.00	103.69	87.36	16.33	1
3.02	105.54	0.00	105.54	88.92	16.62	1
3.00	107.40	0.00	107.40	90.48	16.92	1
2.97	109.25	0.00	109.25	92.04	17.21	1
2.95	111.10	0.00	111.10	93.60	17.50	1
2.92	112.95	0.00	112.95	95.16	17.79	1
2.90	114.80	0.00	114.80	96.72	18.08	1
2.87	116.65	0.00	116.65	98.28	18.37	1
2.85	118.51	0.00	118.51	99.84	18.67	1
2.82	120.36	0.00	120.36	101.40	18.96	1
2.80	122.21	0.00	122.21	102.96	19.25	1
2.77	124.06	0.00	124.06	104.52	19.54	1
2.75	125.91	0.00	125.91	106.08	19.83	1
2.72	127.76	0.00	127.76	107.64	20.12	1

2.70	129.62	0.00	129.62	109.20	20.42	1
2.67	131.47	0.00	131.47	110.76	20.71	1
2.65	133.32	0.00	133.32	112.32	21.00	1
2.62	135.17	0.00	135.17	113.88	21.29	1
2.60	137.02	0.00	137.02	115.44	21.58	1
2.57	138.87	0.00	138.87	117.00	21.87	1
2.55	140.73	0.00	140.73	118.56	22.17	1
2.52	142.58	0.00	142.58	120.12	22.46	1
2.50	144.43	0.00	144.43	121.68	22.75	1
2.47	146.28	0.00	146.28	123.24	23.04	1
2.45	148.13	0.00	148.13	124.80	23.33	1
2.45	148.13	0.00	148.13	124.80	23.33	1
2.42	149.98	0.00	149.98	126.36	23.62	1
2.40	151.84	0.00	151.84	127.92	23.92	1
2.37	153.69	0.00	153.69	129.48	24.21	1
2.35	155.54	0.00	155.54	131.04	24.50	1
2.32	157.39	0.00	157.39	132.60	24.79	1
2.30	159.24	0.00	159.24	134.16	25.08	1
2.27	161.09	0.00	161.09	135.72	25.37	1
2.25	162.95	0.00	162.95	137.28	25.67	1
2.22	164.80	0.00	164.80	138.84	25.96	1
2.20	166.65	0.00	166.65	140.40	26.25	1
2.17	168.50	0.00	168.50	141.96	26.54	1
2.15	170.35	0.00	170.35	143.52	26.83	1
2.12	172.20	0.00	172.20	145.08	27.12	1
2.10	174.06	0.00	174.05	146.64	27.41	1
2.07	175.91	0.00	175.91	148.20	27.71	1
2.05	177.76	0.00	177.76	149.76	28.00	1
2.02	179.61	0.00	179.61	151.32	28.29	1
2.00	181.46	0.00	181.46	152.88	28.58	1
1.97	183.31	0.00	183.31	154.44	28.87	1
1.95	185.16	0.00	185.16	156.00	29.16	1
1.92	187.02	0.00	187.01	157.56	29.46	1
1.90	188.87	0.00	188.87	159.12	29.75	1
1.87	190.72	0.00	190.72	160.68	30.04	1
1.85	192.57	0.00	192.57	162.24	30.33	1
1.82	194.42	0.00	194.42	163.80	30.62	1
1.80	196.27	0.00	196.27	165.36	30.91	1
1.77	198.13	0.00	198.12	166.92	31.20	1
1.75	199.98	0.01	199.97	168.48	31.49	1
1.72	201.83	0.01	201.82	170.04	31.78	1
1.70	203.68	0.01	203.67	171.60	32.07	1
1.67	205.53	0.01	205.52	173.16	32.37	1
1.65	207.38	0.01	207.37	174.72	32.66	1
1.62	209.23	0.01	209.22	176.28	32.95	1
1.60	211.08	0.01	211.07	177.84	33.24	1
1.57	212.94	0.01	212.92	179.40	33.53	1
1.55	214.79	0.02	214.77	180.95	33.81	1
1.52	216.64	0.02	216.62	182.51	34.10	1
1.50	218.49	0.02	218.47	184.07	34.39	1
1.47	220.34	0.03	220.31	185.63	34.68	1
1.45	222.19	0.03	222.16	187.19	34.97	1
1.45	222.19	0.03	222.16	187.19	34.97	1
1.41	224.78	0.03	224.74	189.37	35.37	1

1.38	227.37	0.04	227.33	191.55	35.78	1
1.35	229.96	0.05	229.91	193.73	36.18	1
1.31	232.55	0.06	232.49	195.91	36.58	1
1.28	235.13	0.06	235.07	198.09	36.98	1
1.24	237.72	0.08	237.65	200.27	37.37	1
1.21	240.31	0.09	240.22	202.45	37.77	1
1.17	242.89	0.10	242.79	204.63	38.16	1
1.14	245.48	0.12	245.36	206.80	38.55	1
1.10	248.06	0.14	247.92	208.98	38.94	1
1.07	250.64	0.16	250.48	211.15	39.33	1
1.03	253.22	0.18	253.04	213.33	39.72	1
1.00	255.80	0.21	255.59	215.50	40.10	1
0.96	258.38	0.24	258.14	217.66	40.48	1
0.93	260.95	0.27	260.68	219.83	40.85	1
0.89	263.52	0.31	263.22	221.99	41.23	1
0.86	266.09	0.35	265.75	224.15	41.59	1
0.82	268.66	0.39	268.27	226.31	41.96	1
0.79	271.22	0.44	270.79	228.47	42.32	1
0.75	273.78	0.49	273.29	230.62	42.67	1
0.72	276.34	0.55	275.79	232.77	43.02	1
0.69	278.89	0.61	278.28	234.91	43.37	1
0.65	281.44	0.68	280.76	237.05	43.71	1
0.62	283.98	0.75	283.22	239.18	44.04	1
0.58	286.52	0.84	285.68	241.31	44.37	1
0.55	289.05	0.92	288.12	243.43	44.69	1
0.51	291.57	1.02	290.55	245.55	45.00	1
0.48	294.09	1.12	292.96	247.65	45.31	1
0.45	296.59	1.23	295.36	249.76	45.61	1
0.41	299.10	1.36	297.74	251.85	45.89	1
0.38	301.59	1.49	300.10	253.93	46.17	1
0.35	304.07	1.63	302.44	256.01	46.44	1
0.31	306.54	1.78	304.76	258.07	46.69	1
0.28	309.00	1.95	307.05	260.12	46.93	1
0.25	311.45	2.16	309.30	262.16	47.13	1
0.22	313.89	2.37	311.51	264.19	47.32	1
0.18	316.31	2.61	313.70	266.20	47.50	1
0.15	318.71	2.85	315.86	268.20	47.67	1
0.12	321.10	3.10	318.00	270.18	47.82	1
0.09	323.48	3.37	320.11	272.14	47.96	1
0.09	323.48	3.37	320.11	272.14	47.96	1
0.07	324.82	3.52	321.30	273.26	48.04	1
0.05	326.17	3.68	322.49	274.37	48.12	1
0.04	327.51	3.84	323.67	275.48	48.19	1
0.02	328.84	4.00	324.84	276.57	48.26	1
0.00	330.16	4.17	325.99	277.67	48.33	1

Time = 25. Degree of Consolidation = 4.0%

Total Settlement = 0.050

Settlement at End of Primary Consolidation = 1.243

Settlement caused by Primary Consolidation at time 25. = 0.050

Settlement caused by Secondary Compression at time 25. = 0.000

Surface Elevation = 3.52

*****Current Conditions in Dredged Fill*****

***** Coordinates *****

***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
4.50	4.41	0.50	7.97	7.97	7.97	1
4.47	4.39	0.50	7.97	7.97	7.89	1
4.45	4.36	0.50	7.97	7.97	7.80	1
4.42	4.34	0.49	7.97	7.97	7.72	1
4.40	4.31	0.49	7.97	7.97	7.63	1
4.37	4.29	0.49	7.97	7.97	7.55	1
4.35	4.26	0.48	7.97	7.97	7.46	1
4.32	4.24	0.48	7.97	7.97	7.38	1
4.30	4.21	0.48	7.97	7.97	7.30	1
4.27	4.19	0.48	7.97	7.97	7.23	1
4.25	4.16	0.47	7.97	7.97	7.15	1
4.22	4.14	0.47	7.97	7.97	7.08	1
4.20	4.11	0.47	7.97	7.97	7.01	1
4.17	4.09	0.47	7.97	7.97	6.93	1
4.15	4.06	0.46	7.97	7.97	6.86	1
4.12	4.04	0.46	7.97	7.97	6.78	1
4.10	4.01	0.46	7.97	7.97	6.71	1
4.07	3.99	0.45	7.97	7.97	6.63	1
4.05	3.96	0.45	7.97	7.97	6.59	1
4.02	3.94	0.45	7.97	7.97	6.56	1
4.00	3.91	0.45	7.97	7.97	6.52	1
3.97	3.89	0.44	7.97	7.97	6.49	1
3.95	3.86	0.44	7.97	7.97	6.46	1
3.92	3.84	0.44	7.97	7.97	6.42	1
3.90	3.81	0.43	7.97	7.97	6.39	1
3.87	3.79	0.43	7.97	7.97	6.35	1
3.85	3.76	0.43	7.97	7.97	6.32	1
3.82	3.74	0.43	7.97	7.97	6.29	1
3.80	3.71	0.42	7.97	7.97	6.25	1
3.77	3.69	0.42	7.97	7.97	6.22	1
3.75	3.66	0.42	7.97	7.97	6.19	1
3.72	3.64	0.42	7.97	7.97	6.15	1
3.70	3.61	0.41	7.97	7.97	6.12	1
3.67	3.59	0.41	7.97	7.97	6.08	1
3.65	3.56	0.41	7.97	7.97	6.05	1
3.62	3.54	0.40	7.97	7.97	6.03	1
3.60	3.51	0.40	7.97	7.97	6.01	1
3.57	3.49	0.40	7.97	7.97	5.99	1
3.55	3.46	0.40	7.97	7.97	5.98	1
3.52	3.44	0.39	7.97	7.97	5.96	1

3.50	3.41	0.39	7.97	7.97	5.94	1
3.50	3.41	0.39	7.97	7.97	5.94	1
3.47	3.39	0.39	7.97	7.97	5.93	1
3.45	3.36	0.38	7.97	7.97	5.91	1
3.42	3.34	0.38	7.97	7.97	5.89	1
3.40	3.31	0.38	7.97	7.97	5.88	1
3.37	3.29	0.38	7.97	7.97	5.86	1
3.35	3.26	0.37	7.97	7.97	5.84	1
3.32	3.24	0.37	7.97	7.97	5.82	1
3.30	3.21	0.37	7.97	7.97	5.81	1
3.27	3.19	0.37	7.97	7.97	5.79	1
3.25	3.16	0.36	7.97	7.97	5.77	1
3.22	3.14	0.36	7.97	7.97	5.76	1
3.20	3.11	0.36	7.97	7.97	5.74	1
3.17	3.09	0.35	7.97	7.97	5.72	1
3.15	3.06	0.35	7.97	7.97	5.71	1
3.12	3.04	0.35	7.97	7.97	5.69	1
3.10	3.01	0.35	7.97	7.97	5.67	1
3.07	2.99	0.34	7.97	7.97	5.66	1
3.05	2.96	0.34	7.97	7.97	5.64	1
3.02	2.94	0.34	7.97	7.97	5.62	1
3.00	2.91	0.33	7.97	7.97	5.61	1
2.97	2.89	0.33	7.97	7.97	5.59	1
2.95	2.86	0.33	7.97	7.97	5.57	1
2.92	2.84	0.33	7.97	7.97	5.55	1
2.90	2.81	0.32	7.97	7.97	5.54	1
2.87	2.79	0.32	7.97	7.97	5.52	1
2.85	2.76	0.32	7.97	7.97	5.50	1
2.82	2.74	0.31	7.97	7.97	5.49	1
2.80	2.71	0.31	7.97	7.97	5.47	1
2.77	2.69	0.31	7.97	7.97	5.46	1
2.75	2.66	0.31	7.97	7.97	5.45	1
2.72	2.64	0.30	7.97	7.97	5.44	1
2.70	2.61	0.30	7.97	7.97	5.43	1
2.67	2.59	0.30	7.97	7.97	5.42	1
2.65	2.56	0.30	7.97	7.97	5.41	1
2.62	2.54	0.29	7.97	7.97	5.40	1
2.60	2.51	0.29	7.97	7.97	5.39	1
2.57	2.49	0.29	7.97	7.97	5.38	1
2.55	2.46	0.28	7.97	7.97	5.37	1
2.52	2.44	0.28	7.97	7.97	5.36	1
2.50	2.41	0.28	7.97	7.97	5.35	1
2.50	2.41	0.28	7.97	7.97	5.35	1
2.47	2.39	0.28	7.97	7.97	5.34	1
2.45	2.36	0.27	7.97	7.97	5.33	1
2.42	2.34	0.27	7.97	7.97	5.32	1
2.40	2.31	0.27	7.97	7.97	5.31	1
2.37	2.29	0.26	7.97	7.97	5.30	1
2.35	2.26	0.26	7.97	7.97	5.29	1
2.32	2.24	0.26	7.97	7.97	5.28	1
2.30	2.21	0.26	7.97	7.97	5.27	1
2.27	2.19	0.25	7.97	7.96	5.26	1
2.25	2.16	0.25	7.97	7.96	5.25	1
2.22	2.14	0.25	7.97	7.96	5.24	1

2.20	2.11	0.25	7.97	7.96	5.23	1
2.17	2.09	0.24	7.97	7.96	5.22	1
2.15	2.06	0.24	7.97	7.96	5.22	1
2.12	2.04	0.24	7.97	7.96	5.21	1
2.10	2.01	0.23	7.97	7.96	5.20	1
2.07	1.99	0.23	7.97	7.96	5.19	1
2.05	1.96	0.23	7.97	7.96	5.18	1
2.02	1.94	0.23	7.97	7.96	5.17	1
2.00	1.91	0.22	7.97	7.96	5.16	1
1.97	1.89	0.22	7.97	7.95	5.15	1
1.95	1.86	0.22	7.97	7.95	5.14	1
1.92	1.84	0.21	7.97	7.95	5.13	1
1.90	1.81	0.21	7.97	7.95	5.12	1
1.87	1.79	0.21	7.97	7.95	5.11	1
1.85	1.76	0.21	7.97	7.95	5.11	1
1.82	1.74	0.20	7.97	7.94	5.10	1
1.80	1.71	0.20	7.97	7.94	5.09	1
1.77	1.69	0.20	7.97	7.94	5.09	1
1.75	1.66	0.20	7.97	7.94	5.08	1
1.72	1.64	0.19	7.97	7.93	5.07	1
1.70	1.61	0.19	7.97	7.93	5.06	1
1.67	1.59	0.19	7.97	7.93	5.06	1
1.65	1.56	0.18	7.97	7.92	5.05	1
1.62	1.54	0.18	7.97	7.92	5.04	1
1.60	1.51	0.18	7.97	7.92	5.03	1
1.57	1.49	0.18	7.97	7.91	5.03	1
1.55	1.46	0.17	7.97	7.91	5.02	1
1.52	1.44	0.17	7.97	7.90	5.01	1
1.50	1.41	0.17	7.97	7.90	5.01	1
1.50	1.41	0.17	7.97	7.90	5.01	1
1.46	1.38	0.16	7.97	7.89	4.99	1
1.43	1.35	0.16	7.97	7.88	4.98	1
1.39	1.31	0.16	7.97	7.88	4.97	1
1.36	1.28	0.15	7.97	7.87	4.96	1
1.32	1.24	0.15	7.97	7.86	4.95	1
1.29	1.21	0.14	7.97	7.85	4.94	1
1.25	1.17	0.14	7.97	7.84	4.93	1
1.22	1.14	0.14	7.97	7.83	4.92	1
1.18	1.10	0.13	7.97	7.81	4.91	1
1.15	1.07	0.13	7.97	7.80	4.90	1
1.11	1.03	0.12	7.97	7.79	4.89	1
1.08	1.00	0.12	7.97	7.77	4.88	1
1.05	0.97	0.12	7.97	7.76	4.88	1
1.01	0.93	0.11	7.97	7.74	4.87	1
0.98	0.90	0.11	7.97	7.72	4.86	1
0.94	0.86	0.10	7.97	7.70	4.86	1
0.91	0.83	0.10	7.97	7.68	4.85	1
0.87	0.80	0.10	7.97	7.66	4.85	1
0.84	0.76	0.09	7.97	7.64	4.84	1
0.80	0.73	0.09	7.97	7.61	4.83	1
0.77	0.70	0.09	7.97	7.59	4.83	1
0.73	0.66	0.08	7.97	7.56	4.82	1
0.70	0.63	0.08	7.97	7.53	4.82	1
0.66	0.60	0.07	7.97	7.50	4.81	1

0.62	0.56	0.07	7.97	7.47	4.80	1
0.59	0.53	0.07	7.97	7.43	4.80	1
0.55	0.50	0.06	7.97	7.40	4.79	1
0.52	0.46	0.06	7.97	7.36	4.79	1
0.48	0.43	0.05	7.97	7.32	4.78	1
0.45	0.40	0.05	7.97	7.27	4.77	1
0.41	0.37	0.05	7.97	7.23	4.77	1
0.38	0.33	0.04	7.97	7.18	4.76	1
0.34	0.30	0.04	7.97	7.14	4.76	1
0.31	0.27	0.03	7.97	7.09	4.75	1
0.28	0.24	0.03	7.97	7.03	4.75	1
0.24	0.21	0.03	7.97	6.98	4.74	1
0.21	0.18	0.02	7.97	6.93	4.73	1
0.17	0.15	0.02	7.97	6.87	4.73	1
0.14	0.12	0.02	7.97	6.81	4.72	1
0.10	0.09	0.01	7.97	6.75	4.72	1
0.10	0.09	0.01	7.97	6.75	4.72	1
0.08	0.07	0.01	7.97	6.72	4.71	1
0.06	0.05	0.01	7.97	6.68	4.71	1
0.04	0.03	0.00	7.97	6.65	4.71	1
0.02	0.02	0.00	7.97	6.61	4.70	1
0.00	0.00	0.00	7.97	6.57	4.70	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
4.41	0.00	0.00	0.00	0.00	0.00	1
4.39	1.85	0.00	1.85	1.56	0.29	1
4.36	3.70	0.00	3.70	3.12	0.58	1
4.34	5.55	0.00	5.55	4.68	0.87	1
4.31	7.41	0.00	7.41	6.24	1.17	1
4.29	9.26	0.00	9.26	7.80	1.46	1
4.26	11.11	0.00	11.11	9.36	1.75	1
4.24	12.96	0.00	12.96	10.92	2.04	1
4.21	14.81	0.00	14.81	12.48	2.33	1
4.19	16.66	0.00	16.66	14.04	2.62	1
4.16	18.52	0.00	18.52	15.60	2.92	1
4.14	20.37	0.00	20.37	17.16	3.21	1
4.11	22.22	0.00	22.22	18.72	3.50	1
4.09	24.07	0.00	24.07	20.28	3.79	1
4.06	25.92	0.00	25.92	21.84	4.08	1
4.04	27.77	0.00	27.77	23.40	4.37	1
4.01	29.63	0.00	29.63	24.96	4.67	1
3.99	31.48	0.00	31.48	26.52	4.96	1
3.96	33.33	0.00	33.33	28.08	5.25	1
3.94	35.18	0.00	35.18	29.64	5.54	1
3.91	37.03	0.00	37.03	31.20	5.83	1
3.89	38.88	0.00	38.88	32.76	6.12	1
3.86	40.74	0.00	40.74	34.32	6.42	1
3.84	42.59	0.00	42.59	35.88	6.71	1
3.81	44.44	0.00	44.44	37.44	7.00	1
3.79	46.29	0.00	46.29	39.00	7.29	1
3.76	48.14	0.00	48.14	40.56	7.58	1

3.74	49.99	0.00	49.99	42.12	7.87	1
3.71	51.85	0.00	51.85	43.68	8.17	1
3.69	53.70	0.00	53.70	45.24	8.46	1
3.66	55.55	0.00	55.55	46.80	8.75	1
3.64	57.40	0.00	57.40	48.36	9.04	1
3.61	59.25	0.00	59.25	49.92	9.33	1
3.59	61.10	0.00	61.10	51.48	9.62	1
3.56	62.96	0.00	62.96	53.04	9.92	1
3.54	64.81	0.00	64.81	54.60	10.21	1
3.51	66.66	0.00	66.66	56.16	10.50	1
3.49	68.51	0.00	68.51	57.72	10.79	1
3.46	70.36	0.00	70.36	59.28	11.08	1
3.44	72.21	0.00	72.21	60.84	11.37	1
3.41	74.07	0.00	74.07	62.40	11.67	1
3.41	74.07	0.00	74.07	62.40	11.67	1
3.39	75.92	0.00	75.92	63.96	11.96	1
3.36	77.77	0.00	77.77	65.52	12.25	1
3.34	79.62	0.00	79.62	67.08	12.54	1
3.31	81.47	0.00	81.47	68.64	12.83	1
3.29	83.32	0.00	83.32	70.20	13.12	1
3.26	85.18	0.00	85.18	71.76	13.42	1
3.24	87.03	0.00	87.03	73.32	13.71	1
3.21	88.88	0.00	88.88	74.88	14.00	1
3.19	90.73	0.00	90.73	76.44	14.29	1
3.16	92.58	0.00	92.58	78.00	14.58	1
3.14	94.43	0.00	94.43	79.56	14.87	1
3.11	96.29	0.00	96.29	81.12	15.17	1
3.09	98.14	0.00	98.14	82.68	15.46	1
3.06	99.99	0.00	99.99	84.24	15.75	1
3.04	101.84	0.00	101.84	85.80	16.04	1
3.01	103.69	0.00	103.69	87.36	16.33	1
2.99	105.54	0.00	105.54	88.92	16.62	1
2.96	107.40	0.00	107.40	90.48	16.92	1
2.94	109.25	0.00	109.25	92.04	17.21	1
2.91	111.10	0.00	111.10	93.60	17.50	1
2.89	112.95	0.00	112.95	95.16	17.79	1
2.86	114.80	0.00	114.80	96.72	18.08	1
2.84	116.65	0.00	116.65	98.28	18.37	1
2.81	118.51	0.00	118.50	99.84	18.66	1
2.79	120.36	0.00	120.36	101.40	18.96	1
2.76	122.21	0.00	122.21	102.96	19.25	1
2.74	124.06	0.00	124.06	104.52	19.54	1
2.71	125.91	0.00	125.91	106.08	19.83	1
2.69	127.76	0.00	127.76	107.64	20.12	1
2.66	129.61	0.00	129.61	109.20	20.41	1
2.64	131.47	0.00	131.46	110.76	20.70	1
2.61	133.32	0.00	133.32	112.32	21.00	1
2.59	135.17	0.00	135.17	113.88	21.29	1
2.56	137.02	0.00	137.02	115.44	21.58	1
2.54	138.87	0.00	138.87	117.00	21.87	1
2.51	140.72	0.00	140.72	118.56	22.16	1
2.49	142.58	0.01	142.57	120.12	22.45	1
2.46	144.43	0.01	144.42	121.68	22.74	1
2.44	146.28	0.01	146.27	123.24	23.03	1

2.41	148.13	0.01	148.12	124.80	23.33	1
2.41	148.13	0.01	148.12	124.80	23.33	1
2.39	149.98	0.01	149.97	126.36	23.62	1
2.36	151.83	0.01	151.82	127.92	23.91	1
2.34	153.68	0.01	153.67	129.48	24.20	1
2.31	155.53	0.01	155.52	131.04	24.49	1
2.29	157.39	0.01	157.37	132.59	24.78	1
2.26	159.24	0.01	159.22	134.15	25.07	1
2.24	161.09	0.01	161.07	135.71	25.36	1
2.21	162.94	0.02	162.92	137.27	25.65	1
2.19	164.79	0.02	164.77	138.83	25.94	1
2.16	166.64	0.02	166.62	140.39	26.23	1
2.14	168.49	0.02	168.47	141.95	26.52	1
2.11	170.34	0.02	170.32	143.51	26.81	1
2.09	172.19	0.03	172.16	145.07	27.10	1
2.06	174.04	0.03	174.01	146.63	27.39	1
2.04	175.89	0.03	175.86	148.18	27.67	1
2.01	177.74	0.04	177.71	149.74	27.96	1
1.99	179.59	0.04	179.55	151.30	28.25	1
1.96	181.44	0.04	181.40	152.86	28.54	1
1.94	183.29	0.05	183.24	154.42	28.83	1
1.91	185.14	0.05	185.09	155.97	29.11	1
1.89	186.99	0.06	186.93	157.53	29.40	1
1.86	188.84	0.06	188.78	159.09	29.69	1
1.84	190.69	0.07	190.62	160.64	29.97	1
1.81	192.53	0.07	192.46	162.20	30.26	1
1.79	194.38	0.08	194.30	163.76	30.54	1
1.76	196.23	0.09	196.14	165.31	30.83	1
1.74	198.08	0.09	197.98	166.87	31.11	1
1.71	199.92	0.10	199.82	168.42	31.40	1
1.69	201.77	0.11	201.66	169.98	31.68	1
1.66	203.61	0.12	203.50	171.53	31.96	1
1.64	205.46	0.13	205.33	173.09	32.25	1
1.61	207.31	0.14	207.17	174.64	32.53	1
1.59	209.15	0.15	209.00	176.19	32.81	1
1.56	210.99	0.16	210.83	177.75	33.09	1
1.54	212.84	0.17	212.66	179.30	33.37	1
1.51	214.68	0.19	214.49	180.85	33.65	1
1.49	216.52	0.20	216.32	182.40	33.92	1
1.46	218.36	0.21	218.15	183.95	34.20	1
1.44	220.20	0.23	219.97	185.50	34.48	1
1.41	222.04	0.25	221.80	187.04	34.75	1
1.41	222.04	0.25	221.80	187.04	34.75	1
1.38	224.62	0.27	224.35	189.21	35.14	1
1.35	227.19	0.29	226.89	191.37	35.52	1
1.31	229.76	0.32	229.44	193.54	35.90	1
1.28	232.33	0.35	231.98	195.70	36.28	1
1.24	234.89	0.38	234.51	197.85	36.66	1
1.21	237.46	0.42	237.04	200.01	37.03	1
1.17	240.02	0.46	239.56	202.16	37.40	1
1.14	242.58	0.50	242.08	204.31	37.77	1
1.10	245.13	0.54	244.60	206.46	38.13	1
1.07	247.69	0.58	247.10	208.61	38.50	1
1.03	250.24	0.63	249.60	210.75	38.86	1

1.00	252.78	0.68	252.10	212.88	39.21	1
0.97	255.32	0.74	254.59	215.02	39.57	1
0.93	257.86	0.80	257.07	217.15	39.92	1
0.90	260.40	0.86	259.54	219.27	40.26	1
0.86	262.93	0.92	262.00	221.39	40.61	1
0.83	265.45	0.99	264.46	223.51	40.95	1
0.80	267.97	1.07	266.90	225.62	41.28	1
0.76	270.48	1.15	269.34	227.73	41.61	1
0.73	272.99	1.23	271.76	229.83	41.93	1
0.70	275.49	1.32	274.18	231.92	42.26	1
0.66	277.99	1.41	276.58	234.01	42.57	1
0.63	280.48	1.51	278.97	236.09	42.88	1
0.60	282.96	1.62	281.35	238.16	43.18	1
0.56	285.44	1.73	283.71	240.23	43.48	1
0.53	287.90	1.85	286.05	242.29	43.77	1
0.50	290.36	1.98	288.38	244.34	44.05	1
0.46	292.81	2.13	290.68	246.38	44.30	1
0.43	295.25	2.29	292.96	248.41	44.55	1
0.40	297.67	2.45	295.22	250.43	44.79	1
0.37	300.09	2.63	297.46	252.44	45.03	1
0.33	302.50	2.81	299.69	254.43	45.26	1
0.30	304.89	2.99	301.90	256.42	45.48	1
0.27	307.28	3.19	304.09	258.39	45.70	1
0.24	309.65	3.38	306.26	260.36	45.90	1
0.21	312.00	3.59	308.41	262.31	46.11	1
0.18	314.35	3.80	310.55	264.24	46.30	1
0.15	316.68	4.02	312.66	266.17	46.49	1
0.12	319.00	4.25	314.75	268.08	46.67	1
0.09	321.30	4.48	316.82	269.97	46.85	1
0.09	321.30	4.48	316.82	269.97	46.85	1
0.07	322.61	4.62	317.99	271.05	46.95	1
0.05	323.92	4.76	319.16	272.12	47.04	1
0.03	325.22	4.90	320.32	273.19	47.14	1
0.02	326.51	5.08	321.43	274.25	47.18	1
0.00	327.80	5.39	322.41	275.30	47.10	1

Time = 40. Degree of Consolidation = 7.0%

Total Settlement = 0.088

Settlement at End of Primary Consolidation = 1.243

Settlement caused by Primary Consolidation at time 40. = 0.088

Settlement caused by Secondary Compression at time 40. = 0.000

Surface Elevation = 3.48

*****Current Conditions in Dredged Fill*****

***** Coordinates *****

***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
4.50	4.37	0.50	7.97	7.97	7.97	1
4.47	4.35	0.50	7.97	7.97	7.89	1
4.45	4.32	0.50	7.97	7.97	7.80	1
4.42	4.30	0.49	7.97	7.97	7.72	1
4.40	4.27	0.49	7.97	7.97	7.63	1
4.37	4.25	0.49	7.97	7.97	7.55	1
4.35	4.22	0.48	7.97	7.97	7.46	1
4.32	4.20	0.48	7.97	7.97	7.38	1
4.30	4.17	0.48	7.97	7.97	7.30	1
4.27	4.15	0.48	7.97	7.97	7.23	1
4.25	4.12	0.47	7.97	7.97	7.15	1
4.22	4.10	0.47	7.97	7.97	7.08	1
4.20	4.07	0.47	7.97	7.97	7.01	1
4.17	4.05	0.47	7.97	7.97	6.93	1
4.15	4.02	0.46	7.97	7.97	6.86	1
4.12	4.00	0.46	7.97	7.97	6.78	1
4.10	3.97	0.46	7.97	7.97	6.71	1
4.07	3.95	0.45	7.97	7.97	6.63	1
4.05	3.92	0.45	7.97	7.97	6.59	1
4.02	3.90	0.45	7.97	7.97	6.56	1
4.00	3.87	0.45	7.97	7.97	6.52	1
3.97	3.85	0.44	7.97	7.97	6.49	1
3.95	3.82	0.44	7.97	7.97	6.46	1
3.92	3.80	0.44	7.97	7.97	6.42	1
3.90	3.77	0.43	7.97	7.97	6.39	1
3.87	3.75	0.43	7.97	7.97	6.35	1
3.85	3.72	0.43	7.97	7.97	6.32	1
3.82	3.70	0.43	7.97	7.97	6.29	1
3.80	3.67	0.42	7.97	7.97	6.25	1
3.77	3.65	0.42	7.97	7.97	6.22	1
3.75	3.62	0.42	7.97	7.97	6.19	1
3.72	3.60	0.42	7.97	7.97	6.15	1
3.70	3.57	0.41	7.97	7.97	6.12	1
3.67	3.55	0.41	7.97	7.97	6.08	1
3.65	3.52	0.41	7.97	7.97	6.05	1
3.62	3.50	0.40	7.97	7.97	6.03	1
3.60	3.47	0.40	7.97	7.97	6.01	1
3.57	3.45	0.40	7.97	7.97	5.99	1
3.55	3.42	0.40	7.97	7.97	5.98	1
3.52	3.40	0.39	7.97	7.97	5.96	1
3.50	3.37	0.39	7.97	7.97	5.94	1
3.50	3.37	0.39	7.97	7.97	5.94	1
3.47	3.35	0.39	7.97	7.97	5.93	1
3.45	3.32	0.38	7.97	7.97	5.91	1
3.42	3.30	0.38	7.97	7.97	5.89	1
3.40	3.27	0.38	7.97	7.97	5.88	1
3.37	3.25	0.38	7.97	7.97	5.86	1
3.35	3.22	0.37	7.97	7.97	5.84	1
3.32	3.20	0.37	7.97	7.97	5.82	1
3.30	3.17	0.37	7.97	7.97	5.81	1

3.27	3.15	0.37	7.97	7.97	5.79	1
3.25	3.12	0.36	7.97	7.97	5.77	1
3.22	3.10	0.36	7.97	7.97	5.76	1
3.20	3.07	0.36	7.97	7.97	5.74	1
3.17	3.05	0.35	7.97	7.97	5.72	1
3.15	3.02	0.35	7.97	7.97	5.71	1
3.12	3.00	0.35	7.97	7.97	5.69	1
3.10	2.97	0.35	7.97	7.97	5.67	1
3.07	2.95	0.34	7.97	7.97	5.66	1
3.05	2.92	0.34	7.97	7.97	5.64	1
3.02	2.90	0.34	7.97	7.97	5.62	1
3.00	2.87	0.33	7.97	7.97	5.61	1
2.97	2.85	0.33	7.97	7.97	5.59	1
2.95	2.82	0.33	7.97	7.97	5.57	1
2.92	2.80	0.33	7.97	7.97	5.55	1
2.90	2.77	0.32	7.97	7.97	5.54	1
2.87	2.75	0.32	7.97	7.96	5.52	1
2.85	2.72	0.32	7.97	7.96	5.50	1
2.82	2.70	0.31	7.97	7.96	5.49	1
2.80	2.67	0.31	7.97	7.96	5.47	1
2.77	2.65	0.31	7.97	7.96	5.46	1
2.75	2.62	0.31	7.97	7.96	5.45	1
2.72	2.60	0.30	7.97	7.96	5.44	1
2.70	2.57	0.30	7.97	7.96	5.43	1
2.67	2.55	0.30	7.97	7.96	5.42	1
2.65	2.52	0.30	7.97	7.96	5.41	1
2.62	2.50	0.29	7.97	7.96	5.40	1
2.60	2.47	0.29	7.97	7.96	5.39	1
2.57	2.45	0.29	7.97	7.96	5.38	1
2.55	2.42	0.28	7.97	7.96	5.37	1
2.52	2.40	0.28	7.97	7.95	5.36	1
2.50	2.37	0.28	7.97	7.95	5.35	1
2.50	2.37	0.28	7.97	7.95	5.35	1
2.47	2.35	0.28	7.97	7.95	5.34	1
2.45	2.32	0.27	7.97	7.95	5.33	1
2.42	2.30	0.27	7.97	7.95	5.32	1
2.40	2.27	0.27	7.97	7.95	5.31	1
2.37	2.25	0.26	7.97	7.95	5.30	1
2.35	2.22	0.26	7.97	7.94	5.29	1
2.32	2.20	0.26	7.97	7.94	5.28	1
2.30	2.17	0.26	7.97	7.94	5.27	1
2.27	2.15	0.25	7.97	7.94	5.26	1
2.25	2.12	0.25	7.97	7.94	5.25	1
2.22	2.10	0.25	7.97	7.93	5.24	1
2.20	2.07	0.25	7.97	7.93	5.23	1
2.17	2.05	0.24	7.97	7.93	5.22	1
2.15	2.03	0.24	7.97	7.93	5.22	1
2.12	2.00	0.24	7.97	7.92	5.21	1
2.10	1.98	0.23	7.97	7.92	5.20	1
2.07	1.95	0.23	7.97	7.92	5.19	1
2.05	1.93	0.23	7.97	7.91	5.18	1
2.02	1.90	0.23	7.97	7.91	5.17	1
2.00	1.88	0.22	7.97	7.91	5.16	1
1.97	1.85	0.22	7.97	7.90	5.15	1

1.95	1.83	0.22	7.97	7.90	5.14	1
1.92	1.80	0.21	7.97	7.90	5.13	1
1.90	1.78	0.21	7.97	7.89	5.12	1
1.87	1.75	0.21	7.97	7.89	5.11	1
1.85	1.73	0.21	7.97	7.88	5.11	1
1.82	1.70	0.20	7.97	7.88	5.10	1
1.80	1.68	0.20	7.97	7.87	5.09	1
1.77	1.65	0.20	7.97	7.87	5.09	1
1.75	1.63	0.20	7.97	7.86	5.08	1
1.72	1.60	0.19	7.97	7.86	5.07	1
1.70	1.58	0.19	7.97	7.85	5.06	1
1.67	1.55	0.19	7.97	7.84	5.06	1
1.65	1.53	0.18	7.97	7.84	5.05	1
1.62	1.51	0.18	7.97	7.83	5.04	1
1.60	1.48	0.18	7.97	7.82	5.03	1
1.57	1.46	0.18	7.97	7.82	5.03	1
1.55	1.43	0.17	7.97	7.81	5.02	1
1.52	1.41	0.17	7.97	7.80	5.01	1
1.50	1.38	0.17	7.97	7.79	5.01	1
1.50	1.38	0.17	7.97	7.79	5.01	1
1.46	1.35	0.16	7.97	7.78	4.99	1
1.43	1.31	0.16	7.97	7.77	4.98	1
1.39	1.28	0.16	7.97	7.76	4.97	1
1.36	1.25	0.15	7.97	7.74	4.96	1
1.32	1.21	0.15	7.97	7.73	4.95	1
1.29	1.18	0.14	7.97	7.71	4.94	1
1.25	1.14	0.14	7.97	7.70	4.93	1
1.22	1.11	0.14	7.97	7.68	4.92	1
1.18	1.08	0.13	7.97	7.66	4.91	1
1.15	1.04	0.13	7.97	7.65	4.90	1
1.11	1.01	0.12	7.97	7.63	4.89	1
1.08	0.97	0.12	7.97	7.61	4.88	1
1.05	0.94	0.12	7.97	7.59	4.88	1
1.01	0.91	0.11	7.97	7.56	4.87	1
0.98	0.87	0.11	7.97	7.54	4.86	1
0.94	0.84	0.10	7.97	7.52	4.86	1
0.91	0.81	0.10	7.97	7.49	4.85	1
0.87	0.77	0.10	7.97	7.46	4.85	1
0.84	0.74	0.09	7.97	7.43	4.84	1
0.80	0.71	0.09	7.97	7.40	4.83	1
0.77	0.68	0.09	7.97	7.37	4.83	1
0.73	0.64	0.08	7.97	7.34	4.82	1
0.70	0.61	0.08	7.97	7.31	4.82	1
0.66	0.58	0.07	7.97	7.27	4.81	1
0.62	0.55	0.07	7.97	7.23	4.80	1
0.59	0.51	0.07	7.97	7.20	4.80	1
0.55	0.48	0.06	7.97	7.16	4.79	1
0.52	0.45	0.06	7.97	7.12	4.79	1
0.48	0.42	0.05	7.97	7.08	4.78	1
0.45	0.39	0.05	7.97	7.04	4.77	1
0.41	0.36	0.05	7.97	6.99	4.77	1
0.38	0.33	0.04	7.97	6.95	4.76	1
0.34	0.29	0.04	7.97	6.90	4.76	1
0.31	0.26	0.03	7.97	6.85	4.75	1

0.28	0.23	0.03	7.97	6.80	4.75	1
0.24	0.20	0.03	7.97	6.75	4.74	1
0.21	0.17	0.02	7.97	6.70	4.73	1
0.17	0.14	0.02	7.97	6.65	4.73	1
0.14	0.11	0.02	7.97	6.60	4.72	1
0.10	0.08	0.01	7.97	6.55	4.72	1
0.10	0.08	0.01	7.97	6.55	4.72	1
0.08	0.07	0.01	7.97	6.52	4.71	1
0.06	0.05	0.01	7.97	6.49	4.71	1
0.04	0.03	0.00	7.97	6.46	4.71	1
0.02	0.02	0.00	7.97	6.43	4.70	1
0.00	0.00	0.00	7.97	6.40	4.70	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
4.37	0.00	0.00	0.00	0.00	0.00	1
4.35	1.85	0.00	1.85	1.56	0.29	1
4.32	3.70	0.00	3.70	3.12	0.58	1
4.30	5.55	0.00	5.55	4.68	0.87	1
4.27	7.41	0.00	7.41	6.24	1.17	1
4.25	9.26	0.00	9.26	7.80	1.46	1
4.22	11.11	0.00	11.11	9.36	1.75	1
4.20	12.96	0.00	12.96	10.92	2.04	1
4.17	14.81	0.00	14.81	12.48	2.33	1
4.15	16.66	0.00	16.66	14.04	2.62	1
4.12	18.52	0.00	18.52	15.60	2.92	1
4.10	20.37	0.00	20.37	17.16	3.21	1
4.07	22.22	0.00	22.22	18.72	3.50	1
4.05	24.07	0.00	24.07	20.28	3.79	1
4.02	25.92	0.00	25.92	21.84	4.08	1
4.00	27.77	0.00	27.77	23.40	4.37	1
3.97	29.63	0.00	29.63	24.96	4.67	1
3.95	31.48	0.00	31.48	26.52	4.96	1
3.92	33.33	0.00	33.33	28.08	5.25	1
3.90	35.18	0.00	35.18	29.64	5.54	1
3.87	37.03	0.00	37.03	31.20	5.83	1
3.85	38.88	0.00	38.88	32.76	6.12	1
3.82	40.74	0.00	40.74	34.32	6.42	1
3.80	42.59	0.00	42.59	35.88	6.71	1
3.77	44.44	0.00	44.44	37.44	7.00	1
3.75	46.29	0.00	46.29	39.00	7.29	1
3.72	48.14	0.00	48.14	40.56	7.58	1
3.70	49.99	0.00	49.99	42.12	7.87	1
3.67	51.85	0.00	51.85	43.68	8.17	1
3.65	53.70	0.00	53.70	45.24	8.46	1
3.62	55.55	0.00	55.55	46.80	8.75	1
3.60	57.40	0.00	57.40	48.36	9.04	1
3.57	59.25	0.00	59.25	49.92	9.33	1
3.55	61.10	0.00	61.10	51.48	9.62	1
3.52	62.96	0.00	62.95	53.04	9.92	1
3.50	64.81	0.00	64.81	54.60	10.21	1
3.47	66.66	0.00	66.66	56.16	10.50	1

3.45	68.51	0.00	68.51	57.72	10.79	1
3.42	70.36	0.00	70.36	59.28	11.08	1
3.40	72.21	0.00	72.21	60.84	11.37	1
3.37	74.07	0.00	74.06	62.40	11.66	1
3.37	74.07	0.00	74.06	62.40	11.66	1
3.35	75.92	0.00	75.91	63.96	11.96	1
3.32	77.77	0.00	77.77	65.52	12.25	1
3.30	79.62	0.00	79.62	67.08	12.54	1
3.27	81.47	0.00	81.47	68.64	12.83	1
3.25	83.32	0.00	83.32	70.20	13.12	1
3.22	85.17	0.00	85.17	71.76	13.41	1
3.20	87.03	0.00	87.02	73.32	13.70	1
3.17	88.88	0.00	88.87	74.88	14.00	1
3.15	90.73	0.00	90.72	76.44	14.29	1
3.12	92.58	0.00	92.58	78.00	14.58	1
3.10	94.43	0.01	94.43	79.56	14.87	1
3.07	96.28	0.01	96.28	81.12	15.16	1
3.05	98.13	0.01	98.13	82.68	15.45	1
3.02	99.99	0.01	99.98	84.24	15.74	1
3.00	101.84	0.01	101.83	85.80	16.03	1
2.97	103.69	0.01	103.68	87.36	16.32	1
2.95	105.54	0.01	105.53	88.92	16.62	1
2.92	107.39	0.01	107.38	90.47	16.91	1
2.90	109.24	0.01	109.23	92.03	17.20	1
2.87	111.09	0.01	111.08	93.59	17.49	1
2.85	112.94	0.01	112.93	95.15	17.78	1
2.82	114.79	0.01	114.78	96.71	18.07	1
2.80	116.65	0.02	116.63	98.27	18.36	1
2.77	118.50	0.02	118.48	99.83	18.65	1
2.75	120.35	0.02	120.33	101.39	18.94	1
2.72	122.20	0.02	122.18	102.95	19.23	1
2.70	124.05	0.02	124.03	104.51	19.52	1
2.67	125.90	0.02	125.88	106.07	19.81	1
2.65	127.75	0.03	127.72	107.63	20.10	1
2.62	129.60	0.03	129.57	109.18	20.39	1
2.60	131.45	0.03	131.42	110.74	20.68	1
2.57	133.30	0.03	133.27	112.30	20.97	1
2.55	135.15	0.04	135.12	113.86	21.26	1
2.52	137.00	0.04	136.96	115.42	21.54	1
2.50	138.85	0.04	138.81	116.98	21.83	1
2.47	140.70	0.04	140.66	118.53	22.12	1
2.45	142.55	0.05	142.50	120.09	22.41	1
2.42	144.40	0.05	144.35	121.65	22.70	1
2.40	146.25	0.06	146.19	123.21	22.99	1
2.37	148.10	0.06	148.04	124.76	23.27	1
2.37	148.10	0.06	148.04	124.76	23.27	1
2.35	149.94	0.06	149.88	126.32	23.56	1
2.32	151.79	0.07	151.72	127.88	23.85	1
2.30	153.64	0.07	153.57	129.43	24.13	1
2.27	155.49	0.08	155.41	130.99	24.42	1
2.25	157.34	0.08	157.25	132.55	24.71	1
2.22	159.18	0.09	159.09	134.10	24.99	1
2.20	161.03	0.10	160.93	135.66	25.28	1
2.17	162.88	0.10	162.77	137.21	25.56	1

2.15	164.72	0.11	164.61	138.77	25.85	1
2.12	166.57	0.12	166.45	140.32	26.13	1
2.10	168.41	0.12	168.29	141.87	26.42	1
2.07	170.26	0.13	170.13	143.43	26.70	1
2.05	172.10	0.14	171.96	144.98	26.98	1
2.03	173.95	0.15	173.80	146.53	27.27	1
2.00	175.79	0.16	175.63	148.09	27.55	1
1.98	177.64	0.17	177.47	149.64	27.83	1
1.95	179.48	0.18	179.30	151.19	28.11	1
1.93	181.32	0.19	181.13	152.74	28.39	1
1.90	183.16	0.20	182.96	154.29	28.67	1
1.88	185.00	0.21	184.79	155.84	28.95	1
1.85	186.84	0.23	186.62	157.39	29.23	1
1.83	188.68	0.24	188.44	158.94	29.51	1
1.80	190.52	0.25	190.27	160.48	29.79	1
1.78	192.36	0.27	192.09	162.03	30.06	1
1.75	194.20	0.28	193.92	163.58	30.34	1
1.73	196.04	0.30	195.74	165.12	30.61	1
1.70	197.87	0.32	197.56	166.67	30.89	1
1.68	199.71	0.33	199.37	168.21	31.16	1
1.65	201.54	0.35	201.19	169.75	31.44	1
1.63	203.38	0.37	203.00	171.29	31.71	1
1.60	205.21	0.39	204.82	172.83	31.98	1
1.58	207.04	0.41	206.63	174.37	32.25	1
1.55	208.87	0.43	208.44	175.91	32.52	1
1.53	210.70	0.46	210.24	177.45	32.79	1
1.51	212.53	0.48	212.05	178.99	33.06	1
1.48	214.35	0.50	213.85	180.52	33.33	1
1.46	216.18	0.53	215.65	182.06	33.59	1
1.43	218.00	0.55	217.45	183.59	33.86	1
1.41	219.83	0.58	219.25	185.12	34.12	1
1.38	221.65	0.61	221.04	186.65	34.39	1
1.38	221.65	0.61	221.04	186.65	34.39	1
1.35	224.20	0.65	223.55	188.79	34.76	1
1.31	226.74	0.69	226.05	190.93	35.12	1
1.28	229.28	0.74	228.55	193.06	35.49	1
1.25	231.82	0.78	231.04	195.19	35.85	1
1.21	234.36	0.83	233.52	197.32	36.21	1
1.18	236.89	0.88	236.00	199.44	36.56	1
1.14	239.42	0.94	238.48	201.56	36.92	1
1.11	241.94	1.00	240.94	203.68	37.27	1
1.08	244.46	1.06	243.40	205.79	37.62	1
1.04	246.98	1.12	245.86	207.89	37.96	1
1.01	249.49	1.19	248.30	210.00	38.30	1
0.97	251.99	1.25	250.74	212.10	38.64	1
0.94	254.49	1.33	253.17	214.19	38.98	1
0.91	256.99	1.40	255.59	216.28	39.31	1
0.87	259.48	1.48	258.00	218.36	39.64	1
0.84	261.97	1.57	260.40	220.43	39.96	1
0.81	264.44	1.66	262.79	222.50	40.28	1
0.77	266.92	1.75	265.17	224.57	40.60	1
0.74	269.38	1.85	267.53	226.63	40.91	1
0.71	271.84	1.95	269.89	228.68	41.21	1
0.68	274.29	2.07	272.22	230.72	41.51	1

0.64	276.73	2.20	274.54	232.75	41.79	1
0.61	279.17	2.33	276.84	234.78	42.06	1
0.58	281.59	2.47	279.13	236.80	42.33	1
0.55	284.01	2.61	281.41	238.81	42.60	1
0.51	286.42	2.75	283.67	240.81	42.86	1
0.48	288.82	2.90	285.92	242.80	43.12	1
0.45	291.21	3.06	288.15	244.78	43.37	1
0.42	293.59	3.22	290.37	246.75	43.62	1
0.39	295.96	3.38	292.58	248.71	43.87	1
0.36	298.32	3.55	294.77	250.66	44.10	1
0.33	300.67	3.73	296.94	252.60	44.34	1
0.29	303.01	3.91	299.10	254.53	44.56	1
0.26	305.33	4.09	301.24	256.45	44.79	1
0.23	307.65	4.28	303.36	258.36	45.01	1
0.20	309.95	4.48	305.47	260.25	45.22	1
0.17	312.24	4.68	307.56	262.13	45.43	1
0.14	314.52	4.88	309.64	264.00	45.64	1
0.11	316.78	5.18	311.60	265.86	45.74	1
0.08	319.03	5.63	313.40	267.70	45.70	1
0.08	319.03	5.63	313.40	267.70	45.70	1
0.07	320.31	5.88	314.43	268.75	45.68	1
0.05	321.59	6.13	315.46	269.79	45.66	1
0.03	322.86	6.38	316.48	270.83	45.65	1
0.02	324.13	6.62	317.51	271.87	45.64	1
0.00	325.40	6.86	318.54	272.90	45.64	1

Time = 55. Degree of Consolidation = 10.0%

Total Settlement = 0.127

Settlement at End of Primary Consolidation = 1.243

Settlement caused by Primary Consolidation at time 55. = 0.127

Settlement caused by Secondary Compression at time 55. = 0.000

Surface Elevation = 3.44

*****Current Conditions in Dredged Fill*****

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
4.50	4.30	0.50	7.97	7.97	7.97	1
4.47	4.27	0.50	7.97	7.97	7.89	1
4.45	4.25	0.50	7.97	7.97	7.80	1
4.42	4.22	0.49	7.97	7.97	7.72	1
4.40	4.20	0.49	7.97	7.97	7.63	1
4.37	4.17	0.49	7.97	7.97	7.55	1

4.35	4.15	0.48	7.97	7.97	7.46	1
4.32	4.12	0.48	7.97	7.97	7.38	1
4.30	4.10	0.48	7.97	7.97	7.30	1
4.27	4.07	0.48	7.97	7.97	7.23	1
4.25	4.05	0.47	7.97	7.97	7.15	1
4.22	4.02	0.47	7.97	7.97	7.08	1
4.20	4.00	0.47	7.97	7.97	7.01	1
4.17	3.97	0.47	7.97	7.97	6.93	1
4.15	3.95	0.46	7.97	7.97	6.86	1
4.12	3.92	0.46	7.97	7.97	6.78	1
4.10	3.90	0.46	7.97	7.97	6.71	1
4.07	3.87	0.45	7.97	7.97	6.63	1
4.05	3.85	0.45	7.97	7.97	6.59	1
4.02	3.82	0.45	7.97	7.97	6.56	1
4.00	3.80	0.45	7.97	7.97	6.52	1
3.97	3.77	0.44	7.97	7.97	6.49	1
3.95	3.75	0.44	7.97	7.96	6.46	1
3.92	3.72	0.44	7.97	7.96	6.42	1
3.90	3.70	0.43	7.97	7.96	6.39	1
3.87	3.67	0.43	7.97	7.96	6.35	1
3.85	3.65	0.43	7.97	7.96	6.32	1
3.82	3.62	0.43	7.97	7.96	6.29	1
3.80	3.60	0.42	7.97	7.96	6.25	1
3.77	3.57	0.42	7.97	7.96	6.22	1
3.75	3.55	0.42	7.97	7.96	6.19	1
3.72	3.52	0.42	7.97	7.96	6.15	1
3.70	3.50	0.41	7.97	7.96	6.12	1
3.67	3.47	0.41	7.97	7.96	6.08	1
3.65	3.45	0.41	7.97	7.96	6.05	1
3.62	3.42	0.40	7.97	7.96	6.03	1
3.60	3.40	0.40	7.97	7.96	6.01	1
3.57	3.37	0.40	7.97	7.96	5.99	1
3.55	3.35	0.40	7.97	7.96	5.98	1
3.52	3.32	0.39	7.97	7.95	5.96	1
3.50	3.30	0.39	7.97	7.95	5.94	1
3.50	3.30	0.39	7.97	7.95	5.94	1
3.47	3.27	0.39	7.97	7.95	5.93	1
3.45	3.25	0.38	7.97	7.95	5.91	1
3.42	3.22	0.38	7.97	7.95	5.89	1
3.40	3.20	0.38	7.97	7.95	5.88	1
3.37	3.17	0.38	7.97	7.95	5.86	1
3.35	3.15	0.37	7.97	7.95	5.84	1
3.32	3.12	0.37	7.97	7.95	5.82	1
3.30	3.10	0.37	7.97	7.95	5.81	1
3.27	3.07	0.37	7.97	7.94	5.79	1
3.25	3.05	0.36	7.97	7.94	5.77	1
3.22	3.02	0.36	7.97	7.94	5.76	1
3.20	3.00	0.36	7.97	7.94	5.74	1
3.17	2.97	0.35	7.97	7.94	5.72	1
3.15	2.95	0.35	7.97	7.94	5.71	1
3.12	2.92	0.35	7.97	7.93	5.69	1
3.10	2.90	0.35	7.97	7.93	5.67	1
3.07	2.87	0.34	7.97	7.93	5.66	1
3.05	2.85	0.34	7.97	7.93	5.64	1

3.02	2.82	0.34	7.97	7.93	5.62	1
3.00	2.80	0.33	7.97	7.92	5.61	1
2.97	2.78	0.33	7.97	7.92	5.59	1
2.95	2.75	0.33	7.97	7.92	5.57	1
2.92	2.73	0.33	7.97	7.92	5.55	1
2.90	2.70	0.32	7.97	7.92	5.54	1
2.87	2.68	0.32	7.97	7.91	5.52	1
2.85	2.65	0.32	7.97	7.91	5.50	1
2.82	2.63	0.31	7.97	7.91	5.49	1
2.80	2.60	0.31	7.97	7.90	5.47	1
2.77	2.58	0.31	7.97	7.90	5.46	1
2.75	2.55	0.31	7.97	7.90	5.45	1
2.72	2.53	0.30	7.97	7.90	5.44	1
2.70	2.50	0.30	7.97	7.89	5.43	1
2.67	2.48	0.30	7.97	7.89	5.42	1
2.65	2.45	0.30	7.97	7.89	5.41	1
2.62	2.43	0.29	7.97	7.88	5.40	1
2.60	2.40	0.29	7.97	7.88	5.39	1
2.57	2.38	0.29	7.97	7.87	5.38	1
2.55	2.35	0.28	7.97	7.87	5.37	1
2.52	2.33	0.28	7.97	7.87	5.36	1
2.50	2.30	0.28	7.97	7.86	5.35	1
2.50	2.30	0.28	7.97	7.86	5.35	1
2.47	2.28	0.28	7.97	7.86	5.34	1
2.45	2.25	0.27	7.97	7.85	5.33	1
2.42	2.23	0.27	7.97	7.85	5.32	1
2.40	2.21	0.27	7.97	7.84	5.31	1
2.37	2.18	0.26	7.97	7.84	5.30	1
2.35	2.16	0.26	7.97	7.83	5.29	1
2.32	2.13	0.26	7.97	7.83	5.28	1
2.30	2.11	0.26	7.97	7.82	5.27	1
2.27	2.08	0.25	7.97	7.82	5.26	1
2.25	2.06	0.25	7.97	7.81	5.25	1
2.22	2.03	0.25	7.97	7.81	5.24	1
2.20	2.01	0.25	7.97	7.80	5.23	1
2.17	1.98	0.24	7.97	7.79	5.22	1
2.15	1.96	0.24	7.97	7.79	5.22	1
2.12	1.94	0.24	7.97	7.78	5.21	1
2.10	1.91	0.23	7.97	7.77	5.20	1
2.07	1.89	0.23	7.97	7.77	5.19	1
2.05	1.86	0.23	7.97	7.76	5.18	1
2.02	1.84	0.23	7.97	7.75	5.17	1
2.00	1.81	0.22	7.97	7.74	5.16	1
1.97	1.79	0.22	7.97	7.74	5.15	1
1.95	1.76	0.22	7.97	7.73	5.14	1
1.92	1.74	0.21	7.97	7.72	5.13	1
1.90	1.72	0.21	7.97	7.71	5.12	1
1.87	1.69	0.21	7.97	7.70	5.11	1
1.85	1.67	0.21	7.97	7.69	5.11	1
1.82	1.64	0.20	7.97	7.69	5.10	1
1.80	1.62	0.20	7.97	7.68	5.09	1
1.77	1.59	0.20	7.97	7.67	5.09	1
1.75	1.57	0.20	7.97	7.66	5.08	1
1.72	1.55	0.19	7.97	7.65	5.07	1

1.70	1.52	0.19	7.97	7.64	5.06	1
1.67	1.50	0.19	7.97	7.63	5.06	1
1.65	1.47	0.18	7.97	7.62	5.05	1
1.62	1.45	0.18	7.97	7.60	5.04	1
1.60	1.43	0.18	7.97	7.59	5.03	1
1.57	1.40	0.18	7.97	7.58	5.03	1
1.55	1.38	0.17	7.97	7.57	5.02	1
1.52	1.35	0.17	7.97	7.56	5.01	1
1.50	1.33	0.17	7.97	7.54	5.01	1
1.50	1.33	0.17	7.97	7.54	5.01	1
1.46	1.30	0.16	7.97	7.53	4.99	1
1.43	1.26	0.16	7.97	7.51	4.98	1
1.39	1.23	0.16	7.97	7.49	4.97	1
1.36	1.20	0.15	7.97	7.47	4.96	1
1.32	1.17	0.15	7.97	7.45	4.95	1
1.29	1.13	0.14	7.97	7.43	4.94	1
1.25	1.10	0.14	7.97	7.40	4.93	1
1.22	1.07	0.14	7.97	7.38	4.92	1
1.18	1.03	0.13	7.97	7.36	4.91	1
1.15	1.00	0.13	7.97	7.33	4.90	1
1.11	0.97	0.12	7.97	7.30	4.89	1
1.08	0.94	0.12	7.97	7.28	4.88	1
1.05	0.90	0.12	7.97	7.25	4.88	1
1.01	0.87	0.11	7.97	7.22	4.87	1
0.98	0.84	0.11	7.97	7.20	4.86	1
0.94	0.81	0.10	7.97	7.17	4.86	1
0.91	0.78	0.10	7.97	7.14	4.85	1
0.87	0.74	0.10	7.97	7.11	4.85	1
0.84	0.71	0.09	7.97	7.08	4.84	1
0.80	0.68	0.09	7.97	7.05	4.83	1
0.77	0.65	0.09	7.97	7.02	4.83	1
0.73	0.62	0.08	7.97	6.99	4.82	1
0.70	0.59	0.08	7.97	6.95	4.82	1
0.66	0.56	0.07	7.97	6.92	4.81	1
0.62	0.53	0.07	7.97	6.89	4.80	1
0.59	0.50	0.07	7.97	6.85	4.80	1
0.55	0.46	0.06	7.97	6.82	4.79	1
0.52	0.43	0.06	7.97	6.78	4.79	1
0.48	0.40	0.05	7.97	6.74	4.78	1
0.45	0.37	0.05	7.97	6.71	4.77	1
0.41	0.34	0.05	7.97	6.67	4.77	1
0.38	0.31	0.04	7.97	6.63	4.76	1
0.34	0.28	0.04	7.97	6.59	4.76	1
0.31	0.25	0.03	7.97	6.55	4.75	1
0.28	0.23	0.03	7.97	6.51	4.75	1
0.24	0.20	0.03	7.97	6.47	4.74	1
0.21	0.17	0.02	7.97	6.43	4.73	1
0.17	0.14	0.02	7.97	6.39	4.73	1
0.14	0.11	0.02	7.97	6.36	4.72	1
0.10	0.08	0.01	7.97	6.32	4.72	1
0.10	0.08	0.01	7.97	6.32	4.72	1
0.08	0.06	0.01	7.97	6.30	4.71	1
0.06	0.05	0.01	7.97	6.27	4.71	1
0.04	0.03	0.00	7.97	6.25	4.71	1

0.02	0.02	0.00	7.97	6.23	4.70	1
0.00	0.00	0.00	7.97	6.21	4.70	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
4.30	0.00	0.00	0.00	0.00	0.00	1
4.27	1.85	0.00	1.85	1.56	0.29	1
4.25	3.70	0.00	3.70	3.12	0.58	1
4.22	5.55	0.00	5.55	4.68	0.87	1
4.20	7.41	0.00	7.40	6.24	1.16	1
4.17	9.26	0.00	9.25	7.80	1.45	1
4.15	11.11	0.00	11.10	9.36	1.75	1
4.12	12.96	0.01	12.96	10.92	2.04	1
4.10	14.81	0.01	14.81	12.48	2.33	1
4.07	16.66	0.01	16.66	14.04	2.62	1
4.05	18.51	0.01	18.51	15.60	2.91	1
4.02	20.37	0.01	20.36	17.16	3.20	1
4.00	22.22	0.01	22.21	18.72	3.49	1
3.97	24.07	0.01	24.06	20.28	3.78	1
3.95	25.92	0.01	25.91	21.84	4.07	1
3.92	27.77	0.01	27.76	23.40	4.36	1
3.90	29.62	0.01	29.61	24.96	4.65	1
3.87	31.47	0.01	31.46	26.51	4.95	1
3.85	33.32	0.01	33.31	28.07	5.24	1
3.82	35.17	0.01	35.16	29.63	5.53	1
3.80	37.03	0.02	37.01	31.19	5.82	1
3.77	38.88	0.02	38.86	32.75	6.11	1
3.75	40.73	0.02	40.71	34.31	6.40	1
3.72	42.58	0.02	42.56	35.87	6.69	1
3.70	44.43	0.02	44.41	37.43	6.98	1
3.67	46.28	0.02	46.26	38.99	7.27	1
3.65	48.13	0.02	48.11	40.55	7.56	1
3.62	49.98	0.03	49.96	42.11	7.85	1
3.60	51.83	0.03	51.80	43.66	8.14	1
3.57	53.68	0.03	53.65	45.22	8.43	1
3.55	55.53	0.03	55.50	46.78	8.72	1
3.52	57.38	0.03	57.35	48.34	9.01	1
3.50	59.23	0.03	59.20	49.90	9.30	1
3.47	61.08	0.04	61.04	51.46	9.59	1
3.45	62.93	0.04	62.89	53.01	9.88	1
3.42	64.78	0.04	64.74	54.57	10.17	1
3.40	66.63	0.04	66.59	56.13	10.46	1
3.37	68.48	0.05	68.43	57.69	10.75	1
3.35	70.33	0.05	70.28	59.25	11.03	1
3.32	72.18	0.05	72.13	60.80	11.32	1
3.30	74.03	0.05	73.97	62.36	11.61	1
3.30	74.03	0.05	73.97	62.36	11.61	1
3.27	75.88	0.06	75.82	63.92	11.90	1
3.25	77.72	0.06	77.66	65.47	12.19	1
3.22	79.57	0.06	79.51	67.03	12.48	1
3.20	81.42	0.07	81.35	68.59	12.76	1
3.17	83.27	0.07	83.20	70.14	13.05	1

3.15	85.12	0.08	85.04	71.70	13.34	1
3.12	86.96	0.08	86.88	73.26	13.63	1
3.10	88.81	0.08	88.73	74.81	13.91	1
3.07	90.66	0.09	90.57	76.37	14.20	1
3.05	92.51	0.09	92.41	77.92	14.49	1
3.02	94.35	0.10	94.25	79.48	14.78	1
3.00	96.20	0.10	96.10	81.03	15.06	1
2.97	98.05	0.11	97.94	82.59	15.35	1
2.95	99.89	0.12	99.78	84.14	15.63	1
2.92	101.74	0.12	101.62	85.70	15.92	1
2.90	103.58	0.13	103.45	87.25	16.20	1
2.87	105.43	0.13	105.29	88.80	16.49	1
2.85	107.27	0.14	107.13	90.36	16.77	1
2.82	109.12	0.15	108.97	91.91	17.06	1
2.80	110.96	0.16	110.81	93.46	17.34	1
2.78	112.80	0.16	112.64	95.01	17.63	1
2.75	114.65	0.17	114.48	96.57	17.91	1
2.73	116.49	0.18	116.31	98.12	18.20	1
2.70	118.33	0.19	118.15	99.67	18.48	1
2.68	120.17	0.20	119.98	101.22	18.76	1
2.65	122.02	0.21	121.81	102.77	19.04	1
2.63	123.86	0.22	123.64	104.32	19.33	1
2.60	125.70	0.22	125.47	105.87	19.61	1
2.58	127.54	0.24	127.30	107.41	19.89	1
2.55	129.38	0.25	129.13	108.96	20.17	1
2.53	131.22	0.26	130.96	110.51	20.45	1
2.50	133.06	0.27	132.79	112.06	20.73	1
2.48	134.89	0.28	134.61	113.60	21.01	1
2.45	136.73	0.29	136.44	115.15	21.29	1
2.43	138.57	0.30	138.26	116.69	21.57	1
2.40	140.40	0.32	140.09	118.24	21.85	1
2.38	142.24	0.33	141.91	119.78	22.13	1
2.35	144.07	0.34	143.73	121.32	22.40	1
2.33	145.91	0.36	145.55	122.87	22.68	1
2.30	147.74	0.37	147.37	124.41	22.96	1
2.30	147.74	0.37	147.37	124.41	22.96	1
2.28	149.57	0.39	149.18	125.95	23.24	1
2.25	151.40	0.40	151.00	127.49	23.51	1
2.23	153.23	0.42	152.81	129.03	23.79	1
2.21	155.06	0.44	154.63	130.57	24.06	1
2.18	156.89	0.45	156.44	132.10	24.34	1
2.16	158.72	0.47	158.25	133.64	24.61	1
2.13	160.55	0.49	160.06	135.18	24.88	1
2.11	162.38	0.51	161.87	136.71	25.16	1
2.08	164.20	0.53	163.67	138.24	25.43	1
2.06	166.03	0.55	165.48	139.78	25.70	1
2.03	167.85	0.57	167.28	141.31	25.97	1
2.01	169.67	0.59	169.08	142.84	26.24	1
1.98	171.49	0.61	170.88	144.37	26.51	1
1.96	173.31	0.63	172.68	145.90	26.78	1
1.94	175.13	0.66	174.48	147.43	27.05	1
1.91	176.95	0.68	176.27	148.95	27.32	1
1.89	178.77	0.70	178.06	150.48	27.59	1
1.86	180.58	0.73	179.86	152.00	27.85	1

1.84	182.40	0.75	181.64	153.52	28.12	1
1.81	184.21	0.78	183.43	155.05	28.39	1
1.79	186.02	0.81	185.22	156.57	28.65	1
1.76	187.83	0.83	187.00	158.08	28.91	1
1.74	189.64	0.86	188.78	159.60	29.18	1
1.72	191.45	0.89	190.56	161.12	29.44	1
1.69	193.26	0.92	192.33	162.63	29.70	1
1.67	195.06	0.95	194.11	164.14	29.96	1
1.64	196.86	0.98	195.88	165.66	30.22	1
1.62	198.66	1.01	197.65	167.17	30.48	1
1.59	200.46	1.05	199.42	168.67	30.74	1
1.57	202.26	1.08	201.18	170.18	31.00	1
1.55	204.06	1.12	202.94	171.68	31.26	1
1.52	205.85	1.15	204.70	173.19	31.51	1
1.50	207.64	1.19	206.46	174.69	31.77	1
1.47	209.44	1.22	208.21	176.19	32.02	1
1.45	211.22	1.26	209.96	177.68	32.28	1
1.43	213.01	1.30	211.71	179.18	32.53	1
1.40	214.80	1.34	213.46	180.67	32.78	1
1.38	216.58	1.38	215.20	182.16	33.03	1
1.35	218.36	1.43	216.94	183.65	33.28	1
1.33	220.14	1.47	218.67	185.14	33.53	1
1.33	220.14	1.47	218.67	185.14	33.53	1
1.30	222.63	1.53	221.10	187.22	33.88	1
1.26	225.11	1.59	223.51	189.29	34.22	1
1.23	227.59	1.66	225.92	191.36	34.56	1
1.20	230.06	1.73	228.33	193.43	34.90	1
1.17	232.53	1.80	230.72	195.49	35.24	1
1.13	234.99	1.88	233.11	197.54	35.57	1
1.10	237.44	1.96	235.49	199.59	35.90	1
1.07	239.90	2.04	237.85	201.63	36.22	1
1.03	242.34	2.14	240.21	203.67	36.54	1
1.00	244.78	2.23	242.55	205.70	36.85	1
0.97	247.21	2.33	244.88	207.73	37.16	1
0.94	249.64	2.43	247.21	209.74	37.46	1
0.90	252.06	2.54	249.53	211.76	37.77	1
0.87	254.48	2.64	251.83	213.76	38.07	1
0.84	256.88	2.75	254.13	215.76	38.37	1
0.81	259.29	2.86	256.42	217.75	38.67	1
0.78	261.68	2.97	258.70	219.74	38.97	1
0.74	264.07	3.09	260.98	221.72	39.26	1
0.71	266.45	3.21	263.24	223.69	39.55	1
0.68	268.82	3.33	265.49	225.65	39.84	1
0.65	271.18	3.45	267.73	227.61	40.12	1
0.62	273.54	3.57	269.97	229.56	40.41	1
0.59	275.89	3.70	272.19	231.50	40.69	1
0.56	278.23	3.83	274.40	233.43	40.97	1
0.53	280.56	3.96	276.60	235.35	41.25	1
0.50	282.89	4.10	278.79	237.27	41.52	1
0.46	285.20	4.23	280.97	239.18	41.79	1
0.43	287.51	4.37	283.14	241.08	42.06	1
0.40	289.81	4.52	285.29	242.97	42.32	1
0.37	292.10	4.66	287.43	244.85	42.59	1
0.34	294.38	4.81	289.56	246.72	42.84	1

0.31	296.65	4.97	291.68	248.58	43.10	1
0.28	298.91	5.27	293.64	250.43	43.21	1
0.25	301.16	5.61	295.55	252.28	43.27	1
0.23	303.40	5.95	297.45	254.11	43.34	1
0.20	305.63	6.28	299.35	255.94	43.41	1
0.17	307.86	6.62	301.24	257.75	43.49	1
0.14	310.07	6.95	303.12	259.55	43.57	1
0.11	312.27	7.28	304.99	261.35	43.64	1
0.08	314.47	7.61	306.86	263.14	43.73	1
0.08	314.47	7.61	306.86	263.14	43.73	1
0.06	315.72	7.79	307.92	264.15	43.77	1
0.05	316.96	7.98	308.98	265.17	43.82	1
0.03	318.21	8.17	310.04	266.18	43.86	1
0.02	319.45	8.35	311.10	267.18	43.91	1
0.00	320.69	8.54	312.15	268.19	43.96	1

Time = 85. Degree of Consolidation = 16.0%

Total Settlement = 0.202

Settlement at End of Primary Consolidation = 1.243

Settlement caused by Primary Consolidation at time 85. = 0.202

Settlement caused by Secondary Compression at time 85. = 0.000

Surface Elevation = 3.37

*****Current Conditions in Dredged Fill*****

***** Coordinates *****

***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
4.50	4.22	0.50	7.97	7.97	7.97	1
4.47	4.20	0.50	7.97	7.97	7.89	1
4.45	4.17	0.50	7.97	7.97	7.80	1
4.42	4.15	0.49	7.97	7.96	7.72	1
4.40	4.12	0.49	7.97	7.96	7.63	1
4.37	4.10	0.49	7.97	7.96	7.55	1
4.35	4.07	0.48	7.97	7.96	7.46	1
4.32	4.05	0.48	7.97	7.96	7.38	1
4.30	4.02	0.48	7.97	7.96	7.30	1
4.27	4.00	0.48	7.97	7.95	7.23	1
4.25	3.97	0.47	7.97	7.95	7.15	1
4.22	3.95	0.47	7.97	7.95	7.08	1
4.20	3.92	0.47	7.97	7.95	7.01	1
4.17	3.90	0.47	7.97	7.95	6.93	1
4.15	3.87	0.46	7.97	7.95	6.86	1
4.12	3.85	0.46	7.97	7.95	6.78	1

4.10	3.82	0.46	7.97	7.94	6.71	1
4.07	3.80	0.45	7.97	7.94	6.63	1
4.05	3.77	0.45	7.97	7.94	6.59	1
4.02	3.75	0.45	7.97	7.94	6.56	1
4.00	3.72	0.45	7.97	7.94	6.52	1
3.97	3.70	0.44	7.97	7.94	6.49	1
3.95	3.67	0.44	7.97	7.94	6.46	1
3.92	3.65	0.44	7.97	7.93	6.42	1
3.90	3.62	0.43	7.97	7.93	6.39	1
3.87	3.60	0.43	7.97	7.93	6.35	1
3.85	3.57	0.43	7.97	7.93	6.32	1
3.82	3.55	0.43	7.97	7.93	6.29	1
3.80	3.52	0.42	7.97	7.93	6.25	1
3.77	3.50	0.42	7.97	7.92	6.22	1
3.75	3.47	0.42	7.97	7.92	6.19	1
3.72	3.45	0.42	7.97	7.92	6.15	1
3.70	3.42	0.41	7.97	7.92	6.12	1
3.67	3.40	0.41	7.97	7.92	6.08	1
3.65	3.37	0.41	7.97	7.91	6.05	1
3.62	3.35	0.40	7.97	7.91	6.03	1
3.60	3.33	0.40	7.97	7.91	6.01	1
3.57	3.30	0.40	7.97	7.91	5.99	1
3.55	3.28	0.40	7.97	7.90	5.98	1
3.52	3.25	0.39	7.97	7.90	5.96	1
3.50	3.23	0.39	7.97	7.90	5.94	1
3.50	3.23	0.39	7.97	7.90	5.94	1
3.47	3.20	0.39	7.97	7.90	5.93	1
3.45	3.18	0.38	7.97	7.89	5.91	1
3.42	3.15	0.38	7.97	7.89	5.89	1
3.40	3.13	0.38	7.97	7.89	5.88	1
3.37	3.10	0.38	7.97	7.88	5.86	1
3.35	3.08	0.37	7.97	7.88	5.84	1
3.32	3.05	0.37	7.97	7.88	5.82	1
3.30	3.03	0.37	7.97	7.88	5.81	1
3.27	3.00	0.37	7.97	7.87	5.79	1
3.25	2.98	0.36	7.97	7.87	5.77	1
3.22	2.95	0.36	7.97	7.87	5.76	1
3.20	2.93	0.36	7.97	7.86	5.74	1
3.17	2.90	0.35	7.97	7.86	5.72	1
3.15	2.88	0.35	7.97	7.85	5.71	1
3.12	2.85	0.35	7.97	7.85	5.69	1
3.10	2.83	0.35	7.97	7.85	5.67	1
3.07	2.81	0.34	7.97	7.84	5.66	1
3.05	2.78	0.34	7.97	7.84	5.64	1
3.02	2.76	0.34	7.97	7.83	5.62	1
3.00	2.73	0.33	7.97	7.83	5.61	1
2.97	2.71	0.33	7.97	7.83	5.59	1
2.95	2.68	0.33	7.97	7.82	5.57	1
2.92	2.66	0.33	7.97	7.82	5.55	1
2.90	2.63	0.32	7.97	7.81	5.54	1
2.87	2.61	0.32	7.97	7.81	5.52	1
2.85	2.58	0.32	7.97	7.80	5.50	1
2.82	2.56	0.31	7.97	7.80	5.49	1
2.80	2.54	0.31	7.97	7.79	5.47	1

2.77	2.51	0.31	7.97	7.79	5.46	1
2.75	2.49	0.31	7.97	7.78	5.45	1
2.72	2.46	0.30	7.97	7.77	5.44	1
2.70	2.44	0.30	7.97	7.77	5.43	1
2.67	2.41	0.30	7.97	7.76	5.42	1
2.65	2.39	0.30	7.97	7.76	5.41	1
2.62	2.36	0.29	7.97	7.75	5.40	1
2.60	2.34	0.29	7.97	7.74	5.39	1
2.57	2.32	0.29	7.97	7.74	5.38	1
2.55	2.29	0.28	7.97	7.73	5.37	1
2.52	2.27	0.28	7.97	7.72	5.36	1
2.50	2.24	0.28	7.97	7.72	5.35	1
2.50	2.24	0.28	7.97	7.72	5.35	1
2.47	2.22	0.28	7.97	7.71	5.34	1
2.45	2.19	0.27	7.97	7.70	5.33	1
2.42	2.17	0.27	7.97	7.70	5.32	1
2.40	2.15	0.27	7.97	7.69	5.31	1
2.37	2.12	0.26	7.97	7.68	5.30	1
2.35	2.10	0.26	7.97	7.67	5.29	1
2.32	2.07	0.26	7.97	7.67	5.28	1
2.30	2.05	0.26	7.97	7.66	5.27	1
2.27	2.02	0.25	7.97	7.65	5.26	1
2.25	2.00	0.25	7.97	7.64	5.25	1
2.22	1.98	0.25	7.97	7.63	5.24	1
2.20	1.95	0.25	7.97	7.62	5.23	1
2.17	1.93	0.24	7.97	7.61	5.22	1
2.15	1.90	0.24	7.97	7.61	5.22	1
2.12	1.88	0.24	7.97	7.60	5.21	1
2.10	1.86	0.23	7.97	7.59	5.20	1
2.07	1.83	0.23	7.97	7.58	5.19	1
2.05	1.81	0.23	7.97	7.57	5.18	1
2.02	1.78	0.23	7.97	7.56	5.17	1
2.00	1.76	0.22	7.97	7.55	5.16	1
1.97	1.74	0.22	7.97	7.54	5.15	1
1.95	1.71	0.22	7.97	7.53	5.14	1
1.92	1.69	0.21	7.97	7.52	5.13	1
1.90	1.67	0.21	7.97	7.50	5.12	1
1.87	1.64	0.21	7.97	7.49	5.11	1
1.85	1.62	0.21	7.97	7.48	5.11	1
1.82	1.59	0.20	7.97	7.47	5.10	1
1.80	1.57	0.20	7.97	7.46	5.09	1
1.77	1.55	0.20	7.97	7.44	5.09	1
1.75	1.52	0.20	7.97	7.43	5.08	1
1.72	1.50	0.19	7.97	7.42	5.07	1
1.70	1.48	0.19	7.97	7.41	5.06	1
1.67	1.45	0.19	7.97	7.39	5.06	1
1.65	1.43	0.18	7.97	7.38	5.05	1
1.62	1.41	0.18	7.97	7.36	5.04	1
1.60	1.38	0.18	7.97	7.35	5.03	1
1.57	1.36	0.18	7.97	7.34	5.03	1
1.55	1.34	0.17	7.97	7.32	5.02	1
1.52	1.31	0.17	7.97	7.31	5.01	1
1.50	1.29	0.17	7.97	7.29	5.01	1
1.50	1.29	0.17	7.97	7.29	5.01	1

1.46	1.26	0.16	7.97	7.27	4.99	1
1.43	1.23	0.16	7.97	7.25	4.98	1
1.39	1.19	0.16	7.97	7.23	4.97	1
1.36	1.16	0.15	7.97	7.20	4.96	1
1.32	1.13	0.15	7.97	7.18	4.95	1
1.29	1.10	0.14	7.97	7.16	4.94	1
1.25	1.07	0.14	7.97	7.14	4.93	1
1.22	1.03	0.14	7.97	7.11	4.92	1
1.18	1.00	0.13	7.97	7.09	4.91	1
1.15	0.97	0.13	7.97	7.06	4.90	1
1.11	0.94	0.12	7.97	7.04	4.89	1
1.08	0.91	0.12	7.97	7.01	4.88	1
1.05	0.88	0.12	7.97	6.99	4.88	1
1.01	0.85	0.11	7.97	6.96	4.87	1
0.98	0.82	0.11	7.97	6.93	4.86	1
0.94	0.78	0.10	7.97	6.91	4.86	1
0.91	0.75	0.10	7.97	6.88	4.85	1
0.87	0.72	0.10	7.97	6.85	4.85	1
0.84	0.69	0.09	7.97	6.82	4.84	1
0.80	0.66	0.09	7.97	6.79	4.83	1
0.77	0.63	0.09	7.97	6.76	4.83	1
0.73	0.60	0.08	7.97	6.73	4.82	1
0.70	0.57	0.08	7.97	6.70	4.82	1
0.66	0.54	0.07	7.97	6.67	4.81	1
0.62	0.51	0.07	7.97	6.64	4.80	1
0.59	0.48	0.07	7.97	6.60	4.80	1
0.55	0.45	0.06	7.97	6.57	4.79	1
0.52	0.42	0.06	7.97	6.54	4.79	1
0.48	0.39	0.05	7.97	6.51	4.78	1
0.45	0.36	0.05	7.97	6.47	4.77	1
0.41	0.34	0.05	7.97	6.44	4.77	1
0.38	0.31	0.04	7.97	6.41	4.76	1
0.34	0.28	0.04	7.97	6.38	4.76	1
0.31	0.25	0.03	7.97	6.34	4.75	1
0.28	0.22	0.03	7.97	6.31	4.75	1
0.24	0.19	0.03	7.97	6.28	4.74	1
0.21	0.16	0.02	7.97	6.25	4.73	1
0.17	0.14	0.02	7.97	6.21	4.73	1
0.14	0.11	0.02	7.97	6.18	4.72	1
0.10	0.08	0.01	7.97	6.15	4.72	1
0.10	0.08	0.01	7.97	6.15	4.72	1
0.08	0.06	0.01	7.97	6.13	4.71	1
0.06	0.05	0.01	7.97	6.11	4.71	1
0.04	0.03	0.00	7.97	6.10	4.71	1
0.02	0.02	0.00	7.97	6.08	4.70	1
0.00	0.00	0.00	7.97	6.06	4.70	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
4.22	0.00	0.00	0.00	0.00	0.00	1
4.20	1.85	0.01	1.84	1.56	0.28	1
4.17	3.70	0.01	3.69	3.12	0.57	1

4.15	5.55	0.02	5.53	4.68	0.86	1
4.12	7.40	0.03	7.38	6.24	1.14	1
4.10	9.25	0.03	9.22	7.80	1.43	1
4.07	11.10	0.04	11.07	9.35	1.71	1
4.05	12.95	0.04	12.91	10.91	2.00	1
4.02	14.80	0.05	14.76	12.47	2.29	1
4.00	16.65	0.05	16.60	14.03	2.57	1
3.97	18.50	0.06	18.44	15.58	2.86	1
3.95	20.35	0.06	20.29	17.14	3.15	1
3.92	22.20	0.07	22.13	18.70	3.43	1
3.90	24.05	0.07	23.97	20.25	3.72	1
3.87	25.89	0.08	25.82	21.81	4.01	1
3.85	27.74	0.08	27.66	23.37	4.29	1
3.82	29.59	0.09	29.50	24.92	4.58	1
3.80	31.44	0.09	31.35	26.48	4.87	1
3.77	33.28	0.10	33.19	28.03	5.15	1
3.75	35.13	0.10	35.03	29.59	5.44	1
3.72	36.98	0.11	36.87	31.14	5.73	1
3.70	38.82	0.11	38.71	32.70	6.01	1
3.67	40.67	0.12	40.55	34.25	6.30	1
3.65	42.51	0.12	42.39	35.81	6.59	1
3.62	44.36	0.13	44.23	37.36	6.87	1
3.60	46.20	0.13	46.07	38.91	7.16	1
3.57	48.05	0.14	47.91	40.47	7.44	1
3.55	49.89	0.15	49.75	42.02	7.73	1
3.52	51.74	0.15	51.58	43.57	8.01	1
3.50	53.58	0.16	53.42	45.12	8.30	1
3.47	55.42	0.17	55.26	46.68	8.58	1
3.45	57.27	0.17	57.09	48.23	8.87	1
3.42	59.11	0.18	58.93	49.78	9.15	1
3.40	60.95	0.19	60.77	51.33	9.44	1
3.37	62.80	0.19	62.60	52.88	9.72	1
3.35	64.64	0.20	64.43	54.43	10.01	1
3.33	66.48	0.21	66.27	55.98	10.29	1
3.30	68.32	0.22	68.10	57.53	10.57	1
3.28	70.16	0.23	69.93	59.08	10.86	1
3.25	72.00	0.24	71.76	60.62	11.14	1
3.23	73.84	0.24	73.59	62.17	11.42	1
3.23	73.84	0.24	73.59	62.17	11.42	1
3.20	75.68	0.25	75.42	63.72	11.70	1
3.18	77.52	0.26	77.25	65.27	11.99	1
3.15	79.35	0.27	79.08	66.81	12.27	1
3.13	81.19	0.28	80.91	68.36	12.55	1
3.10	83.03	0.29	82.74	69.90	12.83	1
3.08	84.87	0.30	84.56	71.45	13.11	1
3.05	86.70	0.31	86.39	72.99	13.39	1
3.03	88.54	0.33	88.21	74.54	13.67	1
3.00	90.37	0.34	90.04	76.08	13.95	1
2.98	92.21	0.35	91.86	77.62	14.23	1
2.95	94.04	0.36	93.68	79.17	14.51	1
2.93	95.87	0.37	95.50	80.71	14.79	1
2.90	97.71	0.39	97.32	82.25	15.07	1
2.88	99.54	0.40	99.14	83.79	15.35	1
2.85	101.37	0.41	100.96	85.33	15.63	1

2.83	103.20	0.43	102.77	86.87	15.91	1
2.81	105.03	0.44	104.59	88.41	16.18	1
2.78	106.86	0.45	106.40	89.94	16.46	1
2.76	108.69	0.47	108.22	91.48	16.74	1
2.73	110.51	0.48	110.03	93.02	17.02	1
2.71	112.34	0.50	111.84	94.55	17.29	1
2.68	114.17	0.52	113.65	96.09	17.57	1
2.66	115.99	0.53	115.46	97.62	17.84	1
2.63	117.82	0.55	117.27	99.15	18.12	1
2.61	119.64	0.56	119.08	100.68	18.39	1
2.58	121.46	0.58	120.88	102.21	18.67	1
2.56	123.29	0.60	122.69	103.74	18.94	1
2.54	125.11	0.62	124.49	105.27	19.21	1
2.51	126.93	0.64	126.29	106.80	19.49	1
2.49	128.75	0.66	128.09	108.33	19.76	1
2.46	130.56	0.68	129.89	109.86	20.03	1
2.44	132.38	0.70	131.69	111.38	20.30	1
2.41	134.20	0.72	133.48	112.91	20.58	1
2.39	136.01	0.74	135.28	114.43	20.85	1
2.36	137.83	0.76	137.07	115.95	21.12	1
2.34	139.64	0.78	138.86	117.47	21.39	1
2.32	141.45	0.80	140.65	118.99	21.66	1
2.29	143.26	0.82	142.44	120.51	21.93	1
2.27	145.07	0.85	144.22	122.03	22.19	1
2.24	146.88	0.87	146.01	123.55	22.46	1
2.24	146.88	0.87	146.01	123.55	22.46	1
2.22	148.69	0.89	147.79	125.06	22.73	1
2.19	150.49	0.92	149.57	126.58	23.00	1
2.17	152.30	0.94	151.35	128.09	23.26	1
2.15	154.10	0.97	153.13	129.60	23.53	1
2.12	155.90	1.00	154.91	131.11	23.79	1
2.10	157.70	1.02	156.68	132.62	24.06	1
2.07	159.50	1.05	158.45	134.13	24.32	1
2.05	161.30	1.08	160.22	135.64	24.59	1
2.02	163.10	1.11	161.99	137.14	24.85	1
2.00	164.89	1.13	163.76	138.64	25.11	1
1.98	166.69	1.16	165.52	140.15	25.38	1
1.95	168.48	1.19	167.28	141.65	25.64	1
1.93	170.27	1.22	169.04	143.15	25.90	1
1.90	172.06	1.26	170.80	144.64	26.16	1
1.88	173.85	1.29	172.56	146.14	26.42	1
1.86	175.63	1.32	174.31	147.63	26.68	1
1.83	177.42	1.35	176.06	149.13	26.94	1
1.81	179.20	1.39	177.81	150.62	27.19	1
1.78	180.98	1.42	179.56	152.11	27.45	1
1.76	182.76	1.46	181.30	153.59	27.71	1
1.74	184.54	1.49	183.04	155.08	27.96	1
1.71	186.31	1.53	184.78	156.56	28.22	1
1.69	188.08	1.57	186.52	158.04	28.47	1
1.67	189.86	1.61	188.25	159.52	28.73	1
1.64	191.63	1.65	189.98	161.00	28.98	1
1.62	193.39	1.69	191.71	162.48	29.23	1
1.59	195.16	1.73	193.43	163.95	29.48	1
1.57	196.92	1.77	195.15	165.42	29.73	1

1.55	198.68	1.81	196.87	166.89	29.98	1
1.52	200.44	1.85	198.59	168.36	30.23	1
1.50	202.20	1.90	200.30	169.83	30.47	1
1.48	203.95	1.95	202.01	171.29	30.72	1
1.45	205.71	1.99	203.71	172.75	30.96	1
1.43	207.46	2.05	205.41	174.21	31.20	1
1.41	209.20	2.10	207.10	175.66	31.44	1
1.38	210.95	2.16	208.79	177.12	31.68	1
1.36	212.69	2.21	210.48	178.57	31.91	1
1.34	214.43	2.27	212.16	180.02	32.15	1
1.31	216.17	2.33	213.84	181.46	32.38	1
1.29	217.90	2.38	215.52	182.91	32.61	1
1.29	217.90	2.38	215.52	182.91	32.61	1
1.26	220.33	2.47	217.86	184.92	32.94	1
1.23	222.75	2.55	220.20	186.93	33.26	1
1.19	225.16	2.64	222.53	188.94	33.59	1
1.16	227.57	2.72	224.85	190.94	33.91	1
1.13	229.97	2.81	227.16	192.93	34.23	1
1.10	232.37	2.90	229.47	194.92	34.55	1
1.07	234.76	2.99	231.77	196.91	34.86	1
1.03	237.15	3.09	234.06	198.89	35.18	1
1.00	239.53	3.18	236.35	200.86	35.49	1
0.97	241.90	3.28	238.63	202.82	35.81	1
0.94	244.27	3.37	240.90	204.78	36.12	1
0.91	246.64	3.47	243.16	206.74	36.43	1
0.88	248.99	3.57	245.42	208.68	36.73	1
0.85	251.34	3.68	247.66	210.63	37.04	1
0.82	253.68	3.78	249.90	212.56	37.34	1
0.78	256.02	3.89	252.13	214.49	37.64	1
0.75	258.35	3.99	254.36	216.41	37.95	1
0.72	260.67	4.10	256.57	218.33	38.24	1
0.69	262.99	4.22	258.77	220.23	38.54	1
0.66	265.30	4.33	260.97	222.13	38.83	1
0.63	267.60	4.45	263.15	224.03	39.13	1
0.60	269.89	4.56	265.33	225.91	39.42	1
0.57	272.18	4.69	267.50	227.79	39.70	1
0.54	274.46	4.81	269.65	229.66	39.99	1
0.51	276.73	4.94	271.80	231.53	40.27	1
0.48	279.00	5.14	273.86	233.38	40.47	1
0.45	281.25	5.42	275.83	235.23	40.60	1
0.42	283.50	5.71	277.79	237.07	40.72	1
0.39	285.74	5.99	279.75	238.90	40.85	1
0.36	287.97	6.27	281.70	240.72	40.98	1
0.34	290.19	6.55	283.64	242.54	41.10	1
0.31	292.41	6.83	285.58	244.35	41.23	1
0.28	294.62	7.11	287.51	246.15	41.36	1
0.25	296.82	7.39	289.43	247.94	41.49	1
0.22	299.01	7.67	291.34	249.72	41.62	1
0.19	301.20	7.94	293.25	251.50	41.75	1
0.16	303.37	8.22	295.15	253.27	41.88	1
0.14	305.54	8.50	297.04	255.03	42.02	1
0.11	307.70	8.77	298.93	256.78	42.15	1
0.08	309.85	9.05	300.80	258.52	42.28	1
0.08	309.85	9.05	300.80	258.52	42.28	1

0.06	311.08	9.21	301.87	259.52	42.36	1
0.05	312.31	9.37	302.94	260.51	42.43	1
0.03	313.53	9.52	304.00	261.50	42.51	1
0.02	314.75	9.68	305.06	262.48	42.58	1
0.00	315.96	9.84	306.12	263.47	42.66	1

Time = 115. Degree of Consolidation = 22.0%

Total Settlement = 0.278

Settlement at End of Primary Consolidation = 1.243

Settlement caused by Primary Consolidation at time 115. = 0.278

Settlement caused by Secondary Compression at time 115. = 0.000

Settlement Due to Desiccation = 0.000

Surface Elevation = 3.29

*****Current Conditions in Dredged Fill*****

***** Coordinates *****

***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
4.50	3.91	0.50	7.97	5.14	7.97	1
4.47	3.89	0.50	7.97	5.14	7.89	1
4.45	3.88	0.50	7.97	5.14	7.80	1
4.42	3.86	0.49	7.97	5.14	7.72	1
4.40	3.84	0.49	7.97	5.14	7.63	1
4.37	3.82	0.49	7.97	5.14	7.55	1
4.35	3.81	0.48	7.97	5.14	7.46	1
4.32	3.79	0.48	7.97	5.14	7.38	1
4.30	3.77	0.48	7.97	5.14	7.30	1
4.27	3.76	0.48	7.97	5.14	7.23	1
4.25	3.74	0.47	7.97	5.14	7.15	1
4.22	3.72	0.47	7.97	5.14	7.08	1
4.20	3.70	0.47	7.97	5.14	7.01	1
4.17	3.69	0.47	7.97	5.14	6.93	1
4.15	3.67	0.46	7.97	5.14	6.86	1
4.12	3.65	0.46	7.97	5.14	6.78	1
4.10	3.64	0.46	7.97	5.14	6.71	1
4.07	3.62	0.45	7.97	5.14	6.63	1
4.05	3.60	0.45	7.97	5.14	6.59	1
4.02	3.58	0.45	7.97	5.14	6.56	1
4.00	3.57	0.45	7.97	5.14	6.52	1
3.97	3.55	0.44	7.97	5.14	6.49	1
3.95	3.53	0.44	7.97	5.14	6.46	1
3.92	3.52	0.44	7.97	5.14	6.42	1

3.90	3.50	0.43	7.97	5.14	6.39	1
3.87	3.48	0.43	7.97	5.14	6.35	1
3.85	3.47	0.43	7.97	5.14	6.32	1
3.82	3.45	0.43	7.97	5.14	6.29	1
3.80	3.43	0.42	7.97	5.14	6.25	1
3.77	3.41	0.42	7.97	5.14	6.22	1
3.75	3.40	0.42	7.97	5.14	6.19	1
3.72	3.38	0.42	7.97	6.52	6.15	1
3.70	3.35	0.41	7.97	7.84	6.12	1
3.67	3.33	0.41	7.97	7.84	6.08	1
3.65	3.31	0.41	7.97	7.83	6.05	1
3.62	3.28	0.40	7.97	7.83	6.03	1
3.60	3.26	0.40	7.97	7.82	6.01	1
3.57	3.23	0.40	7.97	7.82	5.99	1
3.55	3.21	0.40	7.97	7.82	5.98	1
3.52	3.18	0.39	7.97	7.81	5.96	1
3.50	3.16	0.39	7.97	7.81	5.94	1
3.50	3.16	0.39	7.97	7.81	5.94	1
3.47	3.13	0.39	7.97	7.80	5.93	1
3.45	3.11	0.38	7.97	7.80	5.91	1
3.42	3.08	0.38	7.97	7.79	5.89	1
3.40	3.06	0.38	7.97	7.79	5.88	1
3.37	3.04	0.38	7.97	7.78	5.86	1
3.35	3.01	0.37	7.97	7.78	5.84	1
3.32	2.99	0.37	7.97	7.78	5.82	1
3.30	2.96	0.37	7.97	7.77	5.81	1
3.27	2.94	0.37	7.97	7.76	5.79	1
3.25	2.91	0.36	7.97	7.76	5.77	1
3.22	2.89	0.36	7.97	7.75	5.76	1
3.20	2.86	0.36	7.97	7.75	5.74	1
3.17	2.84	0.35	7.97	7.74	5.72	1
3.15	2.82	0.35	7.97	7.74	5.71	1
3.12	2.79	0.35	7.97	7.73	5.69	1
3.10	2.77	0.35	7.97	7.73	5.67	1
3.07	2.74	0.34	7.97	7.72	5.66	1
3.05	2.72	0.34	7.97	7.71	5.64	1
3.02	2.69	0.34	7.97	7.71	5.62	1
3.00	2.67	0.33	7.97	7.70	5.61	1
2.97	2.65	0.33	7.97	7.70	5.59	1
2.95	2.62	0.33	7.97	7.69	5.57	1
2.92	2.60	0.33	7.97	7.68	5.55	1
2.90	2.57	0.32	7.97	7.68	5.54	1
2.87	2.55	0.32	7.97	7.67	5.52	1
2.85	2.52	0.32	7.97	7.66	5.50	1
2.82	2.50	0.31	7.97	7.66	5.49	1
2.80	2.48	0.31	7.97	7.65	5.47	1
2.77	2.45	0.31	7.97	7.64	5.46	1
2.75	2.43	0.31	7.97	7.63	5.45	1
2.72	2.40	0.30	7.97	7.63	5.44	1
2.70	2.38	0.30	7.97	7.62	5.43	1
2.67	2.36	0.30	7.97	7.61	5.42	1
2.65	2.33	0.30	7.97	7.60	5.41	1
2.62	2.31	0.29	7.97	7.60	5.40	1
2.60	2.28	0.29	7.97	7.59	5.39	1

2.57	2.26	0.29	7.97	7.58	5.38	1
2.55	2.24	0.28	7.97	7.57	5.37	1
2.52	2.21	0.28	7.97	7.56	5.36	1
2.50	2.19	0.28	7.97	7.55	5.35	1
2.50	2.19	0.28	7.97	7.55	5.35	1
2.47	2.16	0.28	7.97	7.55	5.34	1
2.45	2.14	0.27	7.97	7.54	5.33	1
2.42	2.12	0.27	7.97	7.53	5.32	1
2.40	2.09	0.27	7.97	7.52	5.31	1
2.37	2.07	0.26	7.97	7.51	5.30	1
2.35	2.05	0.26	7.97	7.50	5.29	1
2.32	2.02	0.26	7.97	7.49	5.28	1
2.30	2.00	0.26	7.97	7.48	5.27	1
2.27	1.97	0.25	7.97	7.47	5.26	1
2.25	1.95	0.25	7.97	7.46	5.25	1
2.22	1.93	0.25	7.97	7.45	5.24	1
2.20	1.90	0.25	7.97	7.44	5.23	1
2.17	1.88	0.24	7.97	7.43	5.22	1
2.15	1.86	0.24	7.97	7.42	5.22	1
2.12	1.83	0.24	7.97	7.40	5.21	1
2.10	1.81	0.23	7.97	7.39	5.20	1
2.07	1.79	0.23	7.97	7.38	5.19	1
2.05	1.76	0.23	7.97	7.37	5.18	1
2.02	1.74	0.23	7.97	7.36	5.17	1
2.00	1.72	0.22	7.97	7.35	5.16	1
1.97	1.69	0.22	7.97	7.33	5.15	1
1.95	1.67	0.22	7.97	7.32	5.14	1
1.92	1.65	0.21	7.97	7.31	5.13	1
1.90	1.62	0.21	7.97	7.30	5.12	1
1.87	1.60	0.21	7.97	7.28	5.11	1
1.85	1.58	0.21	7.97	7.27	5.11	1
1.82	1.56	0.20	7.97	7.26	5.10	1
1.80	1.53	0.20	7.97	7.24	5.09	1
1.77	1.51	0.20	7.97	7.23	5.09	1
1.75	1.49	0.20	7.97	7.22	5.08	1
1.72	1.46	0.19	7.97	7.20	5.07	1
1.70	1.44	0.19	7.97	7.19	5.06	1
1.67	1.42	0.19	7.97	7.17	5.06	1
1.65	1.40	0.18	7.97	7.16	5.05	1
1.62	1.37	0.18	7.97	7.15	5.04	1
1.60	1.35	0.18	7.97	7.13	5.03	1
1.57	1.33	0.18	7.97	7.12	5.03	1
1.55	1.30	0.17	7.97	7.10	5.02	1
1.52	1.28	0.17	7.97	7.09	5.01	1
1.50	1.26	0.17	7.97	7.07	5.01	1
1.50	1.26	0.17	7.97	7.07	5.01	1
1.46	1.23	0.16	7.97	7.05	4.99	1
1.43	1.20	0.16	7.97	7.03	4.98	1
1.39	1.17	0.16	7.97	7.01	4.97	1
1.36	1.13	0.15	7.97	6.99	4.96	1
1.32	1.10	0.15	7.97	6.97	4.95	1
1.29	1.07	0.14	7.97	6.94	4.94	1
1.25	1.04	0.14	7.97	6.92	4.93	1
1.22	1.01	0.14	7.97	6.90	4.92	1

1.18	0.98	0.13	7.97	6.87	4.91	1
1.15	0.95	0.13	7.97	6.85	4.90	1
1.11	0.92	0.12	7.97	6.82	4.89	1
1.08	0.89	0.12	7.97	6.80	4.88	1
1.05	0.86	0.12	7.97	6.77	4.88	1
1.01	0.83	0.11	7.97	6.75	4.87	1
0.98	0.80	0.11	7.97	6.72	4.86	1
0.94	0.77	0.10	7.97	6.70	4.86	1
0.91	0.74	0.10	7.97	6.67	4.85	1
0.87	0.71	0.10	7.97	6.64	4.85	1
0.84	0.68	0.09	7.97	6.61	4.84	1
0.80	0.65	0.09	7.97	6.58	4.83	1
0.77	0.62	0.09	7.97	6.56	4.83	1
0.73	0.59	0.08	7.97	6.53	4.82	1
0.70	0.56	0.08	7.97	6.50	4.82	1
0.66	0.53	0.07	7.97	6.47	4.81	1
0.62	0.50	0.07	7.97	6.44	4.80	1
0.59	0.47	0.07	7.97	6.41	4.80	1
0.55	0.44	0.06	7.97	6.39	4.79	1
0.52	0.41	0.06	7.97	6.36	4.79	1
0.48	0.39	0.05	7.97	6.33	4.78	1
0.45	0.36	0.05	7.97	6.30	4.77	1
0.41	0.33	0.05	7.97	6.27	4.77	1
0.38	0.30	0.04	7.97	6.24	4.76	1
0.34	0.27	0.04	7.97	6.21	4.76	1
0.31	0.24	0.03	7.97	6.18	4.75	1
0.28	0.22	0.03	7.97	6.16	4.75	1
0.24	0.19	0.03	7.97	6.13	4.74	1
0.21	0.16	0.02	7.97	6.10	4.73	1
0.17	0.13	0.02	7.97	6.07	4.73	1
0.14	0.11	0.02	7.97	6.04	4.72	1
0.10	0.08	0.01	7.97	6.01	4.72	1
0.10	0.08	0.01	7.97	6.01	4.72	1
0.08	0.06	0.01	7.97	5.99	4.71	1
0.06	0.05	0.01	7.97	5.98	4.71	1
0.04	0.03	0.00	7.97	5.96	4.71	1
0.02	0.02	0.00	7.97	5.95	4.70	1
0.00	0.00	0.00	7.97	5.93	4.70	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
3.91	0.00	0.00	0.00	0.00	0.00	1
3.89	1.36	0.29	1.07	1.07	0.00	1
3.88	2.72	0.58	2.14	2.14	0.00	1
3.86	4.08	0.87	3.21	3.21	0.00	1
3.84	5.44	1.17	4.27	4.27	0.00	1
3.82	6.80	1.46	5.34	5.34	0.00	1
3.81	8.16	1.75	6.41	6.41	0.00	1
3.79	9.52	2.04	7.48	7.48	0.00	1
3.77	10.88	2.33	8.55	8.55	0.00	1
3.76	12.24	2.62	9.62	9.62	0.00	1
3.74	13.60	2.92	10.69	10.69	0.00	1

3.72	14.96	3.21	11.75	11.75	0.00	1
3.70	16.32	3.50	12.82	12.82	0.00	1
3.69	17.68	3.79	13.89	13.89	0.00	1
3.67	19.04	4.08	14.96	14.96	0.00	1
3.65	20.40	4.37	16.03	16.03	0.00	1
3.64	21.76	4.67	17.10	17.10	0.00	1
3.62	23.12	4.96	18.16	18.16	0.00	1
3.60	24.48	5.25	19.23	19.23	0.00	1
3.58	25.84	5.54	20.30	20.30	0.00	1
3.57	27.20	5.83	21.37	21.37	0.00	1
3.55	28.56	6.12	22.44	22.44	0.00	1
3.53	29.92	6.42	23.51	23.51	0.00	1
3.52	31.28	6.71	24.58	24.58	0.00	1
3.50	32.64	7.00	25.64	25.64	0.00	1
3.48	34.00	7.29	26.71	26.71	0.00	1
3.47	35.36	7.58	27.78	27.78	0.00	1
3.45	36.72	7.87	28.85	28.85	0.00	1
3.43	38.08	8.17	29.92	29.92	0.00	1
3.41	39.48	8.46	31.02	31.02	0.00	1
3.40	40.81	8.75	32.06	32.06	0.00	1
3.38	42.26	5.83	36.43	33.22	3.21	1
3.35	44.00	0.45	43.56	34.67	8.89	1
3.33	45.83	0.46	45.37	36.21	9.16	1
3.31	47.66	0.47	47.19	37.74	9.44	1
3.28	49.49	0.49	49.00	39.28	9.72	1
3.26	51.31	0.50	50.81	40.81	10.00	1
3.23	53.14	0.52	52.62	42.35	10.28	1
3.21	54.96	0.53	54.43	43.88	10.55	1
3.18	56.79	0.54	56.24	45.41	10.83	1
3.16	58.61	0.56	58.05	46.95	11.11	1
3.16	58.61	0.56	58.05	46.95	11.11	1
3.13	60.44	0.57	59.86	48.48	11.38	1
3.11	62.26	0.59	61.67	50.01	11.66	1
3.08	64.08	0.61	63.47	51.54	11.93	1
3.06	65.90	0.62	65.28	53.07	12.21	1
3.04	67.72	0.64	67.08	54.60	12.49	1
3.01	69.54	0.66	68.88	56.12	12.76	1
2.99	71.36	0.67	70.68	57.65	13.04	1
2.96	73.17	0.69	72.48	59.17	13.31	1
2.94	74.99	0.71	74.28	60.70	13.58	1
2.91	76.81	0.72	76.08	62.22	13.86	1
2.89	78.62	0.74	77.88	63.75	14.13	1
2.86	80.43	0.76	79.67	65.27	14.40	1
2.84	82.25	0.78	81.47	66.79	14.68	1
2.82	84.06	0.80	83.26	68.31	14.95	1
2.79	85.87	0.82	85.05	69.83	15.22	1
2.77	87.68	0.84	86.84	71.35	15.49	1
2.74	89.49	0.86	88.63	72.86	15.77	1
2.72	91.30	0.88	90.42	74.38	16.04	1
2.69	93.10	0.90	92.20	75.90	16.31	1
2.67	94.91	0.92	93.99	77.41	16.58	1
2.65	96.71	0.94	95.77	78.92	16.85	1
2.62	98.52	0.97	97.55	80.43	17.12	1
2.60	100.32	0.99	99.33	81.95	17.39	1

2.57	102.12	1.01	101.11	83.45	17.66	1
2.55	103.92	1.03	102.89	84.96	17.92	1
2.52	105.72	1.06	104.66	86.47	18.19	1
2.50	107.52	1.08	106.44	87.98	18.46	1
2.48	109.31	1.11	108.21	89.48	18.73	1
2.45	111.11	1.13	109.98	90.99	18.99	1
2.43	112.90	1.16	111.75	92.49	19.26	1
2.40	114.70	1.18	113.51	93.99	19.53	1
2.38	116.49	1.21	115.28	95.49	19.79	1
2.36	118.28	1.23	117.04	96.99	20.06	1
2.33	120.07	1.26	118.81	98.48	20.32	1
2.31	121.85	1.29	120.57	99.98	20.59	1
2.28	123.64	1.32	122.32	101.47	20.85	1
2.26	125.42	1.34	124.08	102.97	21.11	1
2.24	127.21	1.37	125.83	104.46	21.38	1
2.21	128.99	1.40	127.59	105.95	21.64	1
2.19	130.77	1.43	129.34	107.44	21.90	1
2.19	130.77	1.43	129.34	107.44	21.90	1
2.16	132.55	1.46	131.09	108.92	22.16	1
2.14	134.32	1.49	132.83	110.41	22.42	1
2.12	136.10	1.52	134.58	111.89	22.68	1
2.09	137.87	1.56	136.32	113.38	22.94	1
2.07	139.65	1.59	138.06	114.86	23.20	1
2.05	141.42	1.62	139.80	116.34	23.46	1
2.02	143.19	1.66	141.53	117.81	23.72	1
2.00	144.95	1.69	143.26	119.29	23.98	1
1.97	146.72	1.73	144.99	120.76	24.23	1
1.95	148.48	1.76	146.72	122.23	24.49	1
1.93	150.24	1.80	148.45	123.70	24.74	1
1.90	152.00	1.83	150.17	125.17	25.00	1
1.88	153.76	1.87	151.89	126.64	25.25	1
1.86	155.52	1.91	153.61	128.10	25.51	1
1.83	157.27	1.95	155.33	129.57	25.76	1
1.81	159.03	1.99	157.04	131.03	26.01	1
1.79	160.78	2.03	158.74	132.49	26.26	1
1.76	162.52	2.08	160.45	133.94	26.50	1
1.74	164.27	2.13	162.14	135.40	26.75	1
1.72	166.02	2.17	163.84	136.85	26.99	1
1.69	167.76	2.22	165.53	138.30	27.23	1
1.67	169.50	2.27	167.23	139.75	27.48	1
1.65	171.23	2.32	168.91	141.19	27.72	1
1.62	172.97	2.37	170.60	142.64	27.96	1
1.60	174.70	2.42	172.28	144.08	28.20	1
1.58	176.43	2.47	173.96	145.52	28.45	1
1.56	178.16	2.52	175.64	146.96	28.69	1
1.53	179.89	2.57	177.32	148.39	28.93	1
1.51	181.61	2.62	178.99	149.82	29.17	1
1.49	183.33	2.68	180.66	151.25	29.40	1
1.46	185.05	2.73	182.32	152.68	29.64	1
1.44	186.77	2.78	183.99	154.11	29.88	1
1.42	188.49	2.84	185.65	155.53	30.12	1
1.40	190.20	2.89	187.30	156.95	30.36	1
1.37	191.91	2.95	188.96	158.37	30.59	1
1.35	193.61	3.00	190.61	159.78	30.83	1

1.33	195.32	3.06	192.26	161.20	31.06	1
1.30	197.02	3.12	193.90	162.61	31.30	1
1.28	198.72	3.17	195.55	164.01	31.53	1
1.26	200.42	3.23	197.19	165.42	31.77	1
1.26	200.42	3.23	197.19	165.42	31.77	1
1.23	202.79	3.32	199.47	167.38	32.09	1
1.20	205.16	3.40	201.76	169.34	32.42	1
1.17	207.52	3.48	204.03	171.29	32.74	1
1.13	209.87	3.57	206.30	173.24	33.06	1
1.10	212.22	3.66	208.57	175.18	33.38	1
1.07	214.57	3.74	210.82	177.12	33.70	1
1.04	216.91	3.83	213.07	179.05	34.02	1
1.01	219.24	3.92	215.32	180.98	34.34	1
0.98	221.57	4.02	217.55	182.90	34.66	1
0.95	223.89	4.11	219.78	184.81	34.97	1
0.92	226.21	4.21	222.00	186.72	35.28	1
0.89	228.52	4.30	224.22	188.62	35.60	1
0.86	230.82	4.40	226.42	190.52	35.91	1
0.83	233.12	4.50	228.62	192.41	36.21	1
0.80	235.41	4.60	230.81	194.29	36.52	1
0.77	237.70	4.71	232.99	196.17	36.83	1
0.74	239.98	4.81	235.16	198.04	37.13	1
0.71	242.25	4.92	237.33	199.90	37.43	1
0.68	244.51	5.06	239.45	201.76	37.69	1
0.65	246.77	5.31	241.46	203.61	37.86	1
0.62	249.02	5.55	243.47	205.45	38.02	1
0.59	251.27	5.80	245.47	207.29	38.18	1
0.56	253.50	6.04	247.47	209.12	38.35	1
0.53	255.74	6.28	249.45	210.94	38.51	1
0.50	257.96	6.53	251.43	212.75	38.68	1
0.47	260.18	6.77	253.41	214.56	38.84	1
0.44	262.39	7.01	255.37	216.36	39.01	1
0.41	264.59	7.26	257.33	218.16	39.17	1
0.39	266.79	7.51	259.28	219.95	39.33	1
0.36	268.98	7.75	261.22	221.73	39.49	1
0.33	271.16	8.00	263.16	223.50	39.65	1
0.30	273.33	8.25	265.08	225.27	39.81	1
0.27	275.50	8.50	267.00	227.03	39.97	1
0.24	277.66	8.75	268.91	228.78	40.13	1
0.22	279.82	9.01	270.81	230.53	40.28	1
0.19	281.96	9.26	272.71	232.27	40.44	1
0.16	284.10	9.51	274.59	234.00	40.60	1
0.13	286.24	9.76	276.48	235.72	40.75	1
0.11	288.36	10.02	278.35	237.44	40.91	1
0.08	290.48	10.51	279.97	239.15	40.82	1
0.08	290.48	10.51	279.97	239.15	40.82	1
0.06	291.69	10.79	280.90	240.12	40.78	1
0.05	292.89	11.07	281.83	241.10	40.73	1
0.03	294.10	11.34	282.75	242.07	40.69	1
0.02	295.30	11.62	283.68	243.03	40.64	1
0.00	296.50	11.90	284.60	244.00	40.60	1

Time = 145. Degree of Consolidation = 28.0%

Total Settlement = 0.590

Settlement at End of Primary Consolidation = 1.243

Settlement caused by Primary Consolidation at time 145. = 0.352

Settlement caused by Secondary Compression at time 145. = 0.000

Settlement Due to Desiccation = 0.238

Surface Elevation = 2.98

*****Current Conditions in Dredged Fill*****

***** Coordinates *****

***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
4.50	3.54	0.50	7.97	2.26	2.26	1
4.47	3.53	0.50	7.97	2.26	2.26	1
4.45	3.52	0.50	7.97	2.26	2.26	1
4.42	3.51	0.49	7.97	2.26	2.26	1
4.40	3.50	0.49	7.97	2.26	2.26	1
4.37	3.49	0.49	7.97	2.26	2.26	1
4.35	3.48	0.48	7.97	2.26	2.26	1
4.32	3.47	0.48	7.97	2.26	2.26	1
4.30	3.46	0.48	7.97	2.26	2.26	1
4.27	3.45	0.48	7.97	2.26	2.26	1
4.25	3.45	0.47	7.97	2.26	2.26	1
4.22	3.44	0.47	7.97	2.26	2.26	1
4.20	3.43	0.47	7.97	2.26	2.26	1
4.17	3.42	0.47	7.97	2.26	2.26	1
4.15	3.41	0.46	7.97	2.26	2.26	1
4.12	3.40	0.46	7.97	2.26	2.26	1
4.10	3.39	0.46	7.97	2.26	2.26	1
4.07	3.38	0.45	7.97	2.26	2.26	1
4.05	3.37	0.45	7.97	2.26	2.26	1
4.02	3.36	0.45	7.97	2.26	2.26	1
4.00	3.35	0.45	7.97	2.26	2.26	1
3.97	3.34	0.44	7.97	4.35	5.87	1
3.95	3.33	0.44	7.97	5.14	5.85	1
3.92	3.31	0.44	7.97	5.14	5.84	1
3.90	3.29	0.43	7.97	5.14	5.82	1
3.87	3.27	0.43	7.97	5.14	5.80	1
3.85	3.26	0.43	7.97	5.14	5.79	1
3.82	3.24	0.43	7.97	5.14	5.77	1
3.80	3.22	0.42	7.97	5.14	5.75	1
3.77	3.21	0.42	7.97	5.14	5.74	1
3.75	3.19	0.42	7.97	5.14	5.72	1
3.72	3.17	0.42	7.97	5.14	5.70	1

3.70	3.15	0.41	7.97	5.14	5.69	1
3.67	3.14	0.41	7.97	5.14	5.67	1
3.65	3.12	0.41	7.97	5.14	5.65	1
3.62	3.10	0.40	7.97	5.14	5.63	1
3.60	3.09	0.40	7.97	5.14	5.62	1
3.57	3.07	0.40	7.97	5.14	5.60	1
3.55	3.05	0.40	7.97	5.14	5.58	1
3.52	3.03	0.39	7.97	5.14	5.57	1
3.50	3.02	0.39	7.97	5.14	5.55	1
3.50	3.02	0.39	7.97	5.14	5.55	1
3.47	3.00	0.39	7.97	5.14	5.53	1
3.45	2.98	0.38	7.97	5.14	5.52	1
3.42	2.97	0.38	7.97	5.14	5.50	1
3.40	2.95	0.38	7.97	5.80	5.48	1
3.37	2.93	0.38	7.97	5.92	5.47	1
3.35	2.91	0.37	7.97	6.04	5.45	1
3.32	2.89	0.37	7.97	6.16	5.44	1
3.30	2.87	0.37	7.97	6.28	5.43	1
3.27	2.85	0.37	7.97	6.39	5.42	1
3.25	2.83	0.36	7.97	6.51	5.41	1
3.22	2.81	0.36	7.97	6.62	5.41	1
3.20	2.79	0.36	7.97	6.72	5.40	1
3.17	2.76	0.35	7.97	6.82	5.39	1
3.15	2.74	0.35	7.97	6.90	5.38	1
3.12	2.72	0.35	7.97	6.97	5.37	1
3.10	2.70	0.35	7.97	7.03	5.36	1
3.07	2.68	0.34	7.97	7.08	5.35	1
3.05	2.65	0.34	7.97	7.13	5.34	1
3.02	2.63	0.34	7.97	7.17	5.33	1
3.00	2.61	0.33	7.97	7.21	5.32	1
2.97	2.59	0.33	7.97	7.24	5.31	1
2.95	2.56	0.33	7.97	7.27	5.30	1
2.92	2.54	0.33	7.97	7.29	5.29	1
2.90	2.52	0.32	7.97	7.31	5.28	1
2.87	2.49	0.32	7.97	7.33	5.27	1
2.85	2.47	0.32	7.97	7.34	5.26	1
2.82	2.45	0.31	7.97	7.35	5.25	1
2.80	2.42	0.31	7.97	7.36	5.24	1
2.77	2.40	0.31	7.97	7.37	5.23	1
2.75	2.38	0.31	7.97	7.38	5.22	1
2.72	2.35	0.30	7.97	7.38	5.21	1
2.70	2.33	0.30	7.97	7.38	5.20	1
2.67	2.31	0.30	7.97	7.38	5.19	1
2.65	2.28	0.30	7.97	7.38	5.18	1
2.62	2.26	0.29	7.97	7.38	5.17	1
2.60	2.24	0.29	7.97	7.38	5.16	1
2.57	2.21	0.29	7.97	7.37	5.16	1
2.55	2.19	0.28	7.97	7.37	5.15	1
2.52	2.17	0.28	7.97	7.36	5.14	1
2.50	2.14	0.28	7.97	7.36	5.13	1
2.50	2.14	0.28	7.97	7.36	5.13	1
2.47	2.12	0.28	7.97	7.35	5.12	1
2.45	2.10	0.27	7.97	7.34	5.11	1
2.42	2.07	0.27	7.97	7.33	5.11	1

2.40	2.05	0.27	7.97	7.33	5.10	1
2.37	2.03	0.26	7.97	7.32	5.09	1
2.35	2.00	0.26	7.97	7.31	5.08	1
2.32	1.98	0.26	7.97	7.30	5.08	1
2.30	1.96	0.26	7.97	7.29	5.07	1
2.27	1.93	0.25	7.97	7.28	5.06	1
2.25	1.91	0.25	7.97	7.27	5.05	1
2.22	1.89	0.25	7.97	7.26	5.05	1
2.20	1.87	0.25	7.97	7.25	5.04	1
2.17	1.84	0.24	7.97	7.24	5.03	1
2.15	1.82	0.24	7.97	7.23	5.03	1
2.12	1.80	0.24	7.97	7.22	5.02	1
2.10	1.77	0.23	7.97	7.21	5.01	1
2.07	1.75	0.23	7.97	7.19	5.00	1
2.05	1.73	0.23	7.97	7.18	5.00	1
2.02	1.70	0.23	7.97	7.17	4.99	1
2.00	1.68	0.22	7.97	7.16	4.98	1
1.97	1.66	0.22	7.97	7.15	4.97	1
1.95	1.64	0.22	7.97	7.13	4.97	1
1.92	1.61	0.21	7.97	7.12	4.96	1
1.90	1.59	0.21	7.97	7.11	4.95	1
1.87	1.57	0.21	7.97	7.10	4.94	1
1.85	1.55	0.21	7.97	7.08	4.94	1
1.82	1.52	0.20	7.97	7.07	4.93	1
1.80	1.50	0.20	7.97	7.06	4.92	1
1.77	1.48	0.20	7.97	7.04	4.92	1
1.75	1.46	0.20	7.97	7.03	4.91	1
1.72	1.43	0.19	7.97	7.02	4.90	1
1.70	1.41	0.19	7.97	7.00	4.89	1
1.67	1.39	0.19	7.97	6.99	4.89	1
1.65	1.37	0.18	7.97	6.98	4.88	1
1.62	1.35	0.18	7.97	6.96	4.88	1
1.60	1.32	0.18	7.97	6.95	4.87	1
1.57	1.30	0.18	7.97	6.93	4.87	1
1.55	1.28	0.17	7.97	6.92	4.86	1
1.52	1.26	0.17	7.97	6.90	4.86	1
1.50	1.23	0.17	7.97	6.89	4.85	1
1.50	1.23	0.17	7.97	6.89	4.85	1
1.46	1.20	0.16	7.97	6.87	4.85	1
1.43	1.17	0.16	7.97	6.85	4.84	1
1.39	1.14	0.16	7.97	6.83	4.84	1
1.36	1.11	0.15	7.97	6.80	4.83	1
1.32	1.08	0.15	7.97	6.78	4.82	1
1.29	1.05	0.14	7.97	6.76	4.82	1
1.25	1.02	0.14	7.97	6.74	4.81	1
1.22	0.99	0.14	7.97	6.71	4.81	1
1.18	0.96	0.13	7.97	6.69	4.80	1
1.15	0.93	0.13	7.97	6.67	4.79	1
1.11	0.90	0.12	7.97	6.64	4.79	1
1.08	0.87	0.12	7.97	6.62	4.78	1
1.05	0.84	0.12	7.97	6.59	4.78	1
1.01	0.81	0.11	7.97	6.57	4.77	1
0.98	0.78	0.11	7.97	6.54	4.77	1
0.94	0.75	0.10	7.97	6.52	4.76	1

0.91	0.72	0.10	7.97	6.49	4.75	1
0.87	0.69	0.10	7.97	6.47	4.75	1
0.84	0.67	0.09	7.97	6.44	4.74	1
0.80	0.64	0.09	7.97	6.42	4.74	1
0.77	0.61	0.09	7.97	6.39	4.73	1
0.73	0.58	0.08	7.97	6.37	4.72	1
0.70	0.55	0.08	7.97	6.35	4.72	1
0.66	0.52	0.07	7.97	6.32	4.71	1
0.62	0.49	0.07	7.97	6.30	4.71	1
0.59	0.46	0.07	7.97	6.27	4.70	1
0.55	0.44	0.06	7.97	6.25	4.69	1
0.52	0.41	0.06	7.97	6.22	4.69	1
0.48	0.38	0.05	7.97	6.20	4.68	1
0.45	0.35	0.05	7.97	6.17	4.68	1
0.41	0.32	0.05	7.97	6.15	4.67	1
0.38	0.30	0.04	7.97	6.12	4.66	1
0.34	0.27	0.04	7.97	6.10	4.66	1
0.31	0.24	0.03	7.97	6.07	4.65	1
0.28	0.21	0.03	7.97	6.05	4.65	1
0.24	0.19	0.03	7.97	6.03	4.64	1
0.21	0.16	0.02	7.97	6.00	4.64	1
0.17	0.13	0.02	7.97	5.98	4.63	1
0.14	0.10	0.02	7.97	5.95	4.62	1
0.10	0.08	0.01	7.97	5.93	4.62	1
0.10	0.08	0.01	7.97	5.93	4.62	1
0.08	0.06	0.01	7.97	5.91	4.61	1
0.06	0.05	0.01	7.97	5.90	4.61	1
0.04	0.03	0.00	7.97	5.88	4.61	1
0.02	0.02	0.00	7.97	5.87	4.60	1
0.00	0.00	0.00	7.97	5.85	4.60	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
3.54	0.00	0.00	0.00	0.00	0.00	1
3.53	0.61	0.61	0.00	0.00	0.00	1
3.52	1.21	1.21	0.00	0.00	0.00	1
3.51	1.82	1.82	0.00	0.00	0.00	1
3.50	2.42	2.42	0.00	0.00	0.00	1
3.49	3.03	3.03	0.00	0.00	0.00	1
3.48	3.63	3.63	0.00	0.00	0.00	1
3.47	4.24	4.24	0.00	0.00	0.00	1
3.46	4.84	4.84	0.00	0.00	0.00	1
3.45	5.45	5.45	0.00	0.00	0.00	1
3.45	6.05	6.05	0.00	0.00	0.00	1
3.44	6.66	6.66	0.00	0.00	0.00	1
3.43	7.26	7.26	0.00	0.00	0.00	1
3.42	7.87	7.87	0.00	0.00	0.00	1
3.41	8.47	8.47	0.00	0.00	0.00	1
3.40	9.08	9.08	0.00	0.00	0.00	1
3.39	9.68	9.68	0.00	0.00	0.00	1
3.38	10.29	10.29	0.00	0.00	0.00	1
3.37	10.89	10.89	0.00	0.00	0.00	1

3.36	11.50	11.50	0.00	0.00	0.00	1
3.35	12.10	12.10	0.00	0.00	0.00	1
3.34	12.91	12.91	0.00	0.00	0.00	1
3.33	14.21	13.20	1.02	1.02	0.00	1
3.31	15.58	13.49	2.09	2.09	0.00	1
3.29	16.94	13.78	3.15	3.15	0.00	1
3.27	18.30	14.07	4.22	4.22	0.00	1
3.26	19.66	14.36	5.29	5.29	0.00	1
3.24	21.02	14.66	6.36	6.36	0.00	1
3.22	22.38	14.95	7.43	7.43	0.00	1
3.21	23.74	15.24	8.50	8.50	0.00	1
3.19	25.10	15.53	9.57	9.57	0.00	1
3.17	26.46	15.82	10.63	10.63	0.00	1
3.15	27.82	16.11	11.70	11.70	0.00	1
3.14	29.18	16.41	12.77	12.77	0.00	1
3.12	30.54	16.70	13.84	13.84	0.00	1
3.10	31.90	16.99	14.91	14.91	0.00	1
3.09	33.26	17.28	15.98	15.98	0.00	1
3.07	34.62	17.57	17.04	17.04	0.00	1
3.05	35.98	17.86	18.11	18.11	0.00	1
3.03	37.34	18.16	19.18	19.18	0.00	1
3.02	38.70	18.45	20.25	20.25	0.00	1
3.02	38.70	18.45	20.25	20.25	0.00	1
3.00	40.05	18.74	21.31	21.31	0.00	1
2.98	41.42	19.03	22.39	22.39	0.00	1
2.97	42.75	19.32	23.43	23.43	0.00	1
2.95	44.18	14.19	29.99	24.56	5.42	1
2.93	45.66	12.06	33.60	25.76	7.85	1
2.91	47.17	10.00	37.17	26.97	10.20	1
2.89	48.69	8.98	39.71	28.20	11.51	1
2.87	50.24	7.96	42.28	29.46	12.82	1
2.85	51.81	6.95	44.85	30.73	14.12	1
2.83	53.39	5.96	47.43	32.03	15.40	1
2.81	55.00	5.00	50.01	33.35	16.66	1
2.79	56.63	4.59	52.03	34.68	17.35	1
2.76	58.27	4.24	54.03	36.03	18.00	1
2.74	59.93	3.93	56.00	37.40	18.60	1
2.72	61.60	3.65	57.95	38.78	19.17	1
2.70	63.28	3.41	59.87	40.17	19.70	1
2.68	64.98	3.20	61.78	41.57	20.21	1
2.65	66.68	3.01	63.67	42.98	20.69	1
2.63	68.39	2.85	65.54	44.40	21.14	1
2.61	70.10	2.70	67.40	45.82	21.58	1
2.59	71.83	2.58	69.25	47.25	21.99	1
2.56	73.55	2.47	71.08	48.69	22.39	1
2.54	75.28	2.38	72.90	50.13	22.77	1
2.52	77.02	2.30	74.72	51.57	23.14	1
2.49	78.76	2.24	76.52	53.02	23.50	1
2.47	80.50	2.18	78.32	54.47	23.85	1
2.45	82.24	2.14	80.10	55.92	24.18	1
2.42	83.99	2.10	81.89	57.38	24.51	1
2.40	85.74	2.08	83.66	58.83	24.83	1
2.38	87.48	2.06	85.43	60.29	25.14	1
2.35	89.23	2.04	87.19	61.74	25.45	1

2.33	90.98	2.04	88.94	63.20	25.74	1
2.31	92.73	2.03	90.70	64.66	26.04	1
2.28	94.48	2.04	92.44	66.12	26.33	1
2.26	96.23	2.05	94.18	67.57	26.61	1
2.24	97.98	2.06	95.92	69.03	26.89	1
2.21	99.73	2.07	97.65	70.49	27.17	1
2.19	101.47	2.09	99.38	71.94	27.44	1
2.17	103.22	2.11	101.11	73.40	27.71	1
2.14	104.96	2.14	102.83	74.85	27.98	1
2.14	104.96	2.14	102.83	74.85	27.98	1
2.12	106.71	2.16	104.55	76.30	28.25	1
2.10	108.45	2.19	106.26	77.75	28.51	1
2.07	110.19	2.22	107.98	79.20	28.77	1
2.05	111.93	2.25	109.69	80.65	29.03	1
2.03	113.67	2.28	111.39	82.10	29.29	1
2.00	115.41	2.31	113.10	83.55	29.55	1
1.98	117.15	2.35	114.80	84.99	29.81	1
1.96	118.88	2.39	116.49	86.43	30.06	1
1.93	120.61	2.42	118.19	87.87	30.31	1
1.91	122.34	2.46	119.88	89.31	30.57	1
1.89	124.07	2.50	121.57	90.75	30.82	1
1.87	125.80	2.55	123.26	92.19	31.07	1
1.84	127.53	2.59	124.94	93.62	31.32	1
1.82	129.25	2.63	126.62	95.05	31.57	1
1.80	130.97	2.67	128.30	96.48	31.81	1
1.77	132.69	2.72	129.97	97.91	32.06	1
1.75	134.41	2.76	131.64	99.34	32.31	1
1.73	136.12	2.81	133.31	100.76	32.55	1
1.70	137.84	2.86	134.98	102.18	32.80	1
1.68	139.55	2.90	136.65	103.60	33.04	1
1.66	141.26	2.95	138.31	105.02	33.29	1
1.64	142.97	3.00	139.97	106.44	33.53	1
1.61	144.67	3.05	141.62	107.85	33.77	1
1.59	146.37	3.10	143.28	109.26	34.02	1
1.57	148.07	3.15	144.93	110.67	34.26	1
1.55	149.77	3.20	146.58	112.08	34.50	1
1.52	151.47	3.25	148.22	113.48	34.74	1
1.50	153.16	3.30	149.87	114.88	34.98	1
1.48	154.86	3.35	151.51	116.28	35.22	1
1.46	156.54	3.40	153.14	117.68	35.46	1
1.43	158.23	3.45	154.78	119.08	35.70	1
1.41	159.92	3.51	156.41	120.47	35.94	1
1.39	161.60	3.56	158.04	121.86	36.18	1
1.37	163.28	3.61	159.66	123.25	36.42	1
1.35	164.96	3.67	161.29	124.63	36.65	1
1.32	166.63	3.72	162.91	126.02	36.89	1
1.30	168.30	3.78	164.52	127.40	37.13	1
1.28	169.97	3.84	166.14	128.78	37.36	1
1.26	171.64	3.89	167.75	130.15	37.60	1
1.23	173.31	3.95	169.36	131.53	37.83	1
1.23	173.31	3.95	169.36	131.53	37.83	1
1.20	175.63	4.03	171.60	133.45	38.16	1
1.17	177.96	4.11	173.84	135.36	38.48	1
1.14	180.27	4.20	176.08	137.27	38.81	1

1.11	182.58	4.28	178.30	139.17	39.13	1
1.08	184.89	4.37	180.52	141.07	39.46	1
1.05	187.19	4.45	182.74	142.96	39.78	1
1.02	189.48	4.54	184.94	144.85	40.10	1
0.99	191.77	4.63	187.14	146.73	40.42	1
0.96	194.06	4.72	189.34	148.60	40.73	1
0.93	196.34	4.81	191.52	150.47	41.05	1
0.90	198.61	4.91	193.70	152.34	41.36	1
0.87	200.87	5.01	195.86	154.20	41.67	1
0.84	203.13	5.23	197.91	156.05	41.86	1
0.81	205.39	5.44	199.95	157.89	42.05	1
0.78	207.64	5.66	201.98	159.73	42.25	1
0.75	209.88	5.87	204.01	161.57	42.44	1
0.72	212.12	6.09	206.03	163.39	42.64	1
0.69	214.35	6.30	208.05	165.22	42.83	1
0.67	216.57	6.51	210.06	167.03	43.02	1
0.64	218.79	6.73	212.06	168.84	43.22	1
0.61	221.00	6.94	214.06	170.64	43.41	1
0.58	223.20	7.15	216.05	172.44	43.61	1
0.55	225.40	7.37	218.04	174.23	43.80	1
0.52	227.60	7.58	220.02	176.02	44.00	1
0.49	229.79	7.79	221.99	177.80	44.19	1
0.46	231.97	8.01	223.96	179.57	44.39	1
0.44	234.14	8.22	225.93	181.34	44.59	1
0.41	236.31	8.43	227.88	183.10	44.78	1
0.38	238.48	8.64	229.84	184.86	44.98	1
0.35	240.63	8.85	231.78	186.61	45.18	1
0.32	242.79	9.06	233.72	188.35	45.37	1
0.30	244.93	9.28	235.66	190.09	45.57	1
0.27	247.07	9.49	237.58	191.82	45.77	1
0.24	249.21	9.70	239.51	193.54	45.96	1
0.21	251.33	9.91	241.42	195.26	46.16	1
0.19	253.46	10.24	243.21	196.98	46.24	1
0.16	255.57	10.67	244.90	198.68	46.22	1
0.13	257.68	11.10	246.58	200.39	46.20	1
0.10	259.79	11.53	248.25	202.08	46.17	1
0.08	261.88	11.97	249.91	203.77	46.14	1
0.08	261.88	11.97	249.91	203.77	46.14	1
0.06	263.08	12.22	250.86	204.73	46.13	1
0.05	264.27	12.47	251.80	205.69	46.11	1
0.03	265.46	12.72	252.74	206.65	46.09	1
0.02	266.65	12.97	253.68	207.61	46.07	1
0.00	267.84	13.23	254.62	208.56	46.05	1

Time = 175. Degree of Consolidation = 28.%

Total Settlement = 0.964

Settlement at End of Primary Consolidation = 1.618

Settlement caused by Primary Consolidation at time 175. = 0.459

Settlement caused by Secondary Compression at time 175. = 0.000

Settlement Due to Desiccation = 0.505

Surface Elevation = 2.61

*****Current Conditions in Dredged Fill*****

***** Coordinates *****

***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
4.50	3.27	0.50	7.97	2.26	2.26	1
4.47	3.26	0.50	7.97	2.26	2.26	1
4.45	3.25	0.50	7.97	2.26	2.26	1
4.42	3.24	0.49	7.97	2.26	2.26	1
4.40	3.23	0.49	7.97	2.26	2.26	1
4.37	3.22	0.49	7.97	2.26	2.26	1
4.35	3.21	0.48	7.97	2.26	2.26	1
4.32	3.20	0.48	7.97	2.26	2.26	1
4.30	3.19	0.48	7.97	2.26	2.26	1
4.27	3.19	0.48	7.97	2.26	2.26	1
4.25	3.18	0.47	7.97	2.26	2.26	1
4.22	3.17	0.47	7.97	2.26	2.26	1
4.20	3.16	0.47	7.97	2.26	2.26	1
4.17	3.15	0.47	7.97	2.26	2.26	1
4.15	3.14	0.46	7.97	2.26	2.26	1
4.12	3.13	0.46	7.97	2.26	2.26	1
4.10	3.12	0.46	7.97	2.26	2.26	1
4.07	3.11	0.45	7.97	2.26	2.26	1
4.05	3.10	0.45	7.97	2.26	2.26	1
4.02	3.09	0.45	7.97	2.26	2.26	1
4.00	3.09	0.45	7.97	2.26	2.26	1
3.97	3.08	0.44	7.97	2.26	2.26	1
3.95	3.07	0.44	7.97	2.26	2.26	1
3.92	3.06	0.44	7.97	2.26	2.26	1
3.90	3.05	0.43	7.97	2.26	2.26	1
3.87	3.04	0.43	7.97	2.26	2.26	1
3.85	3.03	0.43	7.97	2.26	2.26	1
3.82	3.02	0.43	7.97	2.26	2.26	1
3.80	3.01	0.42	7.97	2.26	2.26	1
3.77	3.00	0.42	7.97	2.26	2.26	1
3.75	2.99	0.42	7.97	2.26	2.26	1
3.72	2.99	0.42	7.97	2.26	2.26	1
3.70	2.98	0.41	7.97	2.26	2.26	1
3.67	2.97	0.41	7.97	2.26	2.26	1
3.65	2.96	0.41	7.97	2.26	2.26	1
3.62	2.95	0.40	7.97	2.26	2.26	1
3.60	2.94	0.40	7.97	2.26	2.26	1
3.57	2.93	0.40	7.97	2.26	2.26	1
3.55	2.92	0.40	7.97	2.26	2.26	1
3.52	2.91	0.39	7.97	2.26	2.26	1

3.50	2.90	0.39	7.97	2.26	2.26	1
3.50	2.90	0.39	7.97	2.26	2.26	1
3.47	2.89	0.39	7.97	2.26	2.26	1
3.45	2.89	0.38	7.97	2.26	2.26	1
3.42	2.88	0.38	7.97	2.26	2.26	1
3.40	2.87	0.38	7.97	2.26	2.26	1
3.37	2.85	0.38	7.97	4.80	5.25	1
3.35	2.84	0.37	7.97	5.61	5.24	1
3.32	2.82	0.37	7.97	5.72	5.23	1
3.30	2.80	0.37	7.97	5.82	5.22	1
3.27	2.78	0.37	7.97	5.92	5.21	1
3.25	2.76	0.36	7.97	6.02	5.20	1
3.22	2.74	0.36	7.97	6.11	5.19	1
3.20	2.72	0.36	7.97	6.20	5.18	1
3.17	2.70	0.35	7.97	6.29	5.17	1
3.15	2.68	0.35	7.97	6.38	5.16	1
3.12	2.66	0.35	7.97	6.47	5.15	1
3.10	2.64	0.35	7.97	6.55	5.14	1
3.07	2.62	0.34	7.97	6.63	5.14	1
3.05	2.60	0.34	7.97	6.70	5.13	1
3.02	2.57	0.34	7.97	6.76	5.12	1
3.00	2.55	0.33	7.97	6.82	5.11	1
2.97	2.53	0.33	7.97	6.87	5.10	1
2.95	2.51	0.33	7.97	6.91	5.10	1
2.92	2.49	0.33	7.97	6.95	5.09	1
2.90	2.46	0.32	7.97	6.98	5.08	1
2.87	2.44	0.32	7.97	7.01	5.08	1
2.85	2.42	0.32	7.97	7.04	5.07	1
2.82	2.40	0.31	7.97	7.06	5.06	1
2.80	2.38	0.31	7.97	7.08	5.05	1
2.77	2.35	0.31	7.97	7.10	5.05	1
2.75	2.33	0.31	7.97	7.11	5.04	1
2.72	2.31	0.30	7.97	7.12	5.03	1
2.70	2.28	0.30	7.97	7.13	5.02	1
2.67	2.26	0.30	7.97	7.14	5.02	1
2.65	2.24	0.30	7.97	7.14	5.01	1
2.62	2.22	0.29	7.97	7.15	5.00	1
2.60	2.19	0.29	7.97	7.15	5.00	1
2.57	2.17	0.29	7.97	7.15	4.99	1
2.55	2.15	0.28	7.97	7.15	4.98	1
2.52	2.13	0.28	7.97	7.15	4.97	1
2.50	2.10	0.28	7.97	7.15	4.97	1
2.50	2.10	0.28	7.97	7.15	4.96	1
2.47	2.08	0.28	7.97	7.14	4.95	1
2.45	2.06	0.27	7.97	7.14	4.94	1
2.42	2.04	0.27	7.97	7.14	4.94	1
2.40	2.01	0.27	7.97	7.13	4.93	1
2.37	1.99	0.26	7.97	7.13	4.93	1
2.35	1.97	0.26	7.97	7.12	4.92	1
2.32	1.94	0.26	7.97	7.11	4.92	1
2.30	1.92	0.26	7.97	7.11	4.91	1
2.27	1.90	0.25	7.97	7.10	4.90	1
2.25	1.88	0.25	7.97	7.09	4.89	1
2.22	1.85	0.25	7.97	7.08	4.89	1

2.20	1.83	0.25	7.97	7.07	4.88	1
2.17	1.81	0.24	7.97	7.06	4.88	1
2.15	1.79	0.24	7.97	7.05	4.87	1
2.12	1.76	0.24	7.97	7.04	4.87	1
2.10	1.74	0.23	7.97	7.03	4.86	1
2.07	1.72	0.23	7.97	7.02	4.86	1
2.05	1.70	0.23	7.97	7.01	4.85	1
2.02	1.68	0.23	7.97	7.00	4.85	1
2.00	1.65	0.22	7.97	6.99	4.85	1
1.97	1.63	0.22	7.97	6.98	4.84	1
1.95	1.61	0.22	7.97	6.97	4.84	1
1.92	1.59	0.21	7.97	6.95	4.83	1
1.90	1.56	0.21	7.97	6.94	4.83	1
1.87	1.54	0.21	7.97	6.93	4.82	1
1.85	1.52	0.21	7.97	6.92	4.82	1
1.82	1.50	0.20	7.97	6.91	4.82	1
1.80	1.48	0.20	7.97	6.89	4.81	1
1.77	1.45	0.20	7.97	6.88	4.81	1
1.75	1.43	0.20	7.97	6.87	4.80	1
1.72	1.41	0.19	7.97	6.85	4.80	1
1.70	1.39	0.19	7.97	6.84	4.79	1
1.67	1.37	0.19	7.97	6.83	4.79	1
1.65	1.34	0.18	7.97	6.81	4.79	1
1.62	1.32	0.18	7.97	6.80	4.78	1
1.60	1.30	0.18	7.97	6.79	4.78	1
1.57	1.28	0.18	7.97	6.77	4.77	1
1.55	1.26	0.17	7.97	6.76	4.77	1
1.52	1.24	0.17	7.97	6.74	4.77	1
1.50	1.21	0.17	7.97	6.73	4.76	1
1.50	1.21	0.17	7.97	6.73	4.76	1
1.46	1.18	0.16	7.97	6.71	4.75	1
1.43	1.15	0.16	7.97	6.69	4.75	1
1.39	1.12	0.16	7.97	6.67	4.74	1
1.36	1.09	0.15	7.97	6.65	4.74	1
1.32	1.06	0.15	7.97	6.63	4.74	1
1.29	1.03	0.14	7.97	6.60	4.73	1
1.25	1.01	0.14	7.97	6.58	4.73	1
1.22	0.98	0.14	7.97	6.56	4.72	1
1.18	0.95	0.13	7.97	6.54	4.72	1
1.15	0.92	0.13	7.97	6.51	4.71	1
1.11	0.89	0.12	7.97	6.49	4.70	1
1.08	0.86	0.12	7.97	6.47	4.70	1
1.05	0.83	0.12	7.97	6.45	4.69	1
1.01	0.80	0.11	7.97	6.43	4.69	1
0.98	0.77	0.11	7.97	6.40	4.68	1
0.94	0.74	0.10	7.97	6.38	4.67	1
0.91	0.71	0.10	7.97	6.36	4.67	1
0.87	0.69	0.10	7.97	6.34	4.66	1
0.84	0.66	0.09	7.97	6.32	4.66	1
0.80	0.63	0.09	7.97	6.30	4.65	1
0.77	0.60	0.09	7.97	6.27	4.65	1
0.73	0.57	0.08	7.97	6.25	4.64	1
0.70	0.54	0.08	7.97	6.23	4.63	1
0.66	0.51	0.07	7.97	6.21	4.63	1

0.62	0.49	0.07	7.97	6.19	4.62	1
0.59	0.46	0.07	7.97	6.16	4.62	1
0.55	0.43	0.06	7.97	6.14	4.61	1
0.52	0.40	0.06	7.97	6.12	4.60	1
0.48	0.38	0.05	7.97	6.10	4.60	1
0.45	0.35	0.05	7.97	6.08	4.59	1
0.41	0.32	0.05	7.97	6.05	4.59	1
0.38	0.29	0.04	7.97	6.03	4.58	1
0.34	0.27	0.04	7.97	6.01	4.57	1
0.31	0.24	0.03	7.97	5.99	4.57	1
0.28	0.21	0.03	7.97	5.96	4.56	1
0.24	0.18	0.03	7.97	5.94	4.56	1
0.21	0.16	0.02	7.97	5.92	4.55	1
0.17	0.13	0.02	7.97	5.89	4.54	1
0.14	0.10	0.02	7.97	5.87	4.54	1
0.10	0.08	0.01	7.97	5.85	4.53	1
0.10	0.08	0.01	7.97	5.85	4.53	1
0.08	0.06	0.01	7.97	5.83	4.52	1
0.06	0.05	0.01	7.97	5.82	4.51	1
0.04	0.03	0.00	7.97	5.81	4.51	1
0.02	0.02	0.00	7.97	5.79	4.50	1
0.00	0.00	0.00	7.97	5.78	4.50	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
3.27	0.00	0.00	0.00	0.00	0.00	1
3.26	0.61	0.61	0.00	0.00	0.00	1
3.25	1.21	1.21	0.00	0.00	0.00	1
3.24	1.82	1.82	0.00	0.00	0.00	1
3.23	2.42	2.42	0.00	0.00	0.00	1
3.22	3.03	3.03	0.00	0.00	0.00	1
3.21	3.63	3.63	0.00	0.00	0.00	1
3.20	4.24	4.24	0.00	0.00	0.00	1
3.19	4.84	4.84	0.00	0.00	0.00	1
3.19	5.45	5.45	0.00	0.00	0.00	1
3.18	6.05	6.05	0.00	0.00	0.00	1
3.17	6.66	6.66	0.00	0.00	0.00	1
3.16	7.26	7.26	0.00	0.00	0.00	1
3.15	7.87	7.87	0.00	0.00	0.00	1
3.14	8.47	8.47	0.00	0.00	0.00	1
3.13	9.08	9.08	0.00	0.00	0.00	1
3.12	9.68	9.68	0.00	0.00	0.00	1
3.11	10.29	10.29	0.00	0.00	0.00	1
3.10	10.89	10.89	0.00	0.00	0.00	1
3.09	11.50	11.50	0.00	0.00	0.00	1
3.09	12.10	12.10	0.00	0.00	0.00	1
3.08	12.71	12.71	0.00	0.00	0.00	1
3.07	13.31	13.31	0.00	0.00	0.00	1
3.06	13.92	13.92	0.00	0.00	0.00	1
3.05	14.52	14.52	0.00	0.00	0.00	1
3.04	15.13	15.13	0.00	0.00	0.00	1
3.03	15.73	15.73	0.00	0.00	0.00	1

3.02	16.34	16.34	0.00	0.00	0.00	1
3.01	16.94	16.94	0.00	0.00	0.00	1
3.00	17.55	17.55	0.00	0.00	0.00	1
2.99	18.15	18.15	0.00	0.00	0.00	1
2.99	18.76	18.76	0.00	0.00	0.00	1
2.98	19.36	19.36	0.00	0.00	0.00	1
2.97	19.97	19.97	0.00	0.00	0.00	1
2.96	20.57	20.57	0.00	0.00	0.00	1
2.95	21.18	21.18	0.00	0.00	0.00	1
2.94	21.78	21.78	0.00	0.00	0.00	1
2.93	22.39	22.39	0.00	0.00	0.00	1
2.92	22.99	22.99	0.00	0.00	0.00	1
2.91	23.60	23.60	0.00	0.00	0.00	1
2.90	24.20	24.20	0.00	0.00	0.00	1
2.90	24.81	24.81	0.00	0.00	0.00	1
2.89	25.41	25.41	0.00	0.00	0.00	1
2.89	26.02	26.02	0.00	0.00	0.00	1
2.88	26.62	26.62	0.00	0.00	0.00	1
2.87	27.23	27.23	0.00	0.00	0.00	1
2.85	45.66	19.29	33.60	25.76	15.79	1
2.84	47.17	17.40	37.17	26.97	17.98	1
2.82	48.69	15.57	39.71	28.20	20.11	1
2.80	50.24	13.78	42.28	29.46	22.18	1
2.78	51.81	12.06	44.85	30.73	24.19	1
2.76	53.39	10.41	47.43	32.03	26.14	1
2.74	55.00	9.40	50.01	33.35	27.44	1
2.72	56.63	8.60	52.03	34.68	28.53	1
2.70	58.27	7.82	54.03	36.03	29.61	1
2.68	59.93	7.05	56.00	37.40	30.66	1
2.66	61.60	6.31	57.95	38.78	31.70	1
2.64	63.28	5.59	59.87	40.17	32.70	1
2.62	64.98	4.96	61.78	41.57	33.62	1
2.60	66.68	4.69	63.67	42.98	34.19	1
2.57	68.39	4.44	65.54	44.40	34.73	1
2.55	70.10	4.22	67.40	45.82	35.24	1
2.53	71.83	4.03	69.25	47.25	35.72	1
2.51	73.55	3.86	71.08	48.69	36.19	1
2.49	75.28	3.71	72.90	50.13	36.63	1
2.46	77.02	3.58	74.72	51.57	37.05	1
2.44	78.76	3.47	76.52	53.02	37.46	1
2.42	80.50	3.37	78.32	54.47	37.85	1
2.40	82.24	3.28	80.10	55.92	38.22	1
2.38	83.99	3.21	81.89	57.38	38.59	1
2.35	85.74	3.14	83.66	58.83	38.94	1
2.33	87.48	3.09	85.43	60.29	39.29	1
2.31	89.23	3.05	87.19	61.74	39.62	1
2.28	90.98	3.01	88.94	63.20	39.95	1
2.26	92.73	2.98	90.70	64.66	40.27	1
2.24	94.48	2.96	92.44	66.12	40.58	1
2.22	96.23	2.95	94.18	67.57	40.89	1
2.19	97.98	2.94	95.92	69.03	41.19	1
2.17	99.73	2.94	97.65	70.49	41.48	1
2.15	101.47	2.94	99.38	71.94	41.78	1
2.13	103.22	2.94	101.11	73.40	42.06	1

2.10	104.96	2.95	102.83	74.85	42.34	1
2.10	104.96	2.14	102.83	74.85	42.34	1
2.08	106.71	2.96	104.55	76.30	42.63	1
2.06	108.45	2.97	106.26	77.75	42.91	1
2.04	110.19	2.99	107.98	79.20	43.18	1
2.01	111.93	3.01	109.69	80.65	43.45	1
1.99	113.67	3.03	111.39	82.10	43.72	1
1.97	115.41	3.05	113.10	83.55	43.99	1
1.94	117.15	3.08	114.80	84.99	44.26	1
1.92	118.88	3.11	116.49	86.43	44.52	1
1.90	120.61	3.14	118.19	87.87	44.78	1
1.88	122.34	3.17	119.88	89.31	45.04	1
1.85	124.07	3.20	121.57	90.75	45.30	1
1.83	125.80	3.24	123.26	92.19	45.56	1
1.81	127.53	3.28	124.94	93.62	45.81	1
1.79	129.25	3.31	126.62	95.05	46.06	1
1.76	130.97	3.35	128.30	96.48	46.32	1
1.74	132.69	3.39	129.97	97.91	46.57	1
1.72	134.41	3.43	131.64	99.34	46.82	1
1.70	136.12	3.47	133.31	100.76	47.07	1
1.68	137.84	3.52	134.98	102.18	47.32	1
1.65	139.55	3.56	136.65	103.60	47.57	1
1.63	141.26	3.60	138.31	105.02	47.81	1
1.61	142.97	3.65	139.97	106.44	48.06	1
1.59	144.67	3.70	141.62	107.85	48.31	1
1.56	146.37	3.74	143.28	109.26	48.55	1
1.54	148.07	3.79	144.93	110.67	48.80	1
1.52	149.77	3.84	146.58	112.08	49.04	1
1.50	151.47	3.89	148.22	113.48	49.28	1
1.48	153.16	3.93	149.87	114.88	49.53	1
1.45	154.86	3.98	151.51	116.28	49.77	1
1.43	156.54	4.03	153.14	117.68	50.01	1
1.41	158.23	4.09	154.78	119.08	50.25	1
1.39	159.92	4.14	156.41	120.47	50.49	1
1.37	161.60	4.19	158.04	121.86	50.73	1
1.34	163.28	4.24	159.66	123.25	50.97	1
1.32	164.96	4.29	161.29	124.63	51.21	1
1.30	166.63	4.35	162.91	126.02	51.45	1
1.28	168.30	4.40	164.52	127.40	51.68	1
1.26	169.97	4.46	166.14	128.78	51.92	1
1.24	171.64	4.51	167.75	130.15	52.16	1
1.21	173.31	4.57	169.36	131.53	52.39	1
1.21	173.31	3.95	169.36	131.53	52.39	1
1.18	175.63	4.65	171.60	133.45	52.72	1
1.15	177.96	4.73	173.84	135.36	53.05	1
1.12	180.27	4.81	176.08	137.27	53.37	1
1.09	182.58	4.90	178.30	139.17	53.70	1
1.06	184.89	4.98	180.52	141.07	54.02	1
1.03	187.19	5.15	182.74	142.96	54.26	1
1.01	189.48	5.34	184.94	144.85	54.48	1
0.98	191.77	5.53	187.14	146.73	54.70	1
0.95	194.06	5.72	189.34	148.60	54.92	1
0.92	196.34	5.91	191.52	150.47	55.14	1
0.89	198.61	6.10	193.70	152.34	55.36	1

0.86	200.87	6.29	195.86	154.20	55.57	1
0.83	203.13	6.48	197.91	156.05	55.79	1
0.80	205.39	6.67	199.95	157.89	56.01	1
0.77	207.64	6.85	201.98	159.73	56.23	1
0.74	209.88	7.04	204.01	161.57	56.45	1
0.71	212.12	7.23	206.03	163.39	56.67	1
0.69	214.35	7.42	208.05	165.22	56.89	1
0.66	216.57	7.61	210.06	167.03	57.11	1
0.63	218.79	7.80	212.06	168.84	57.33	1
0.60	221.00	7.99	214.06	170.64	57.55	1
0.57	223.20	8.18	216.05	172.44	57.77	1
0.54	225.40	8.37	218.04	174.23	57.98	1
0.51	227.60	8.56	220.02	176.02	58.20	1
0.49	229.79	8.75	221.99	177.80	58.42	1
0.46	231.97	8.94	223.96	179.57	58.64	1
0.43	234.14	9.13	225.93	181.34	58.86	1
0.40	236.31	9.32	227.88	183.10	59.08	1
0.38	238.48	9.51	229.84	184.86	59.30	1
0.35	240.63	9.70	231.78	186.61	59.52	1
0.32	242.79	9.89	233.72	188.35	59.73	1
0.29	244.93	10.15	235.66	190.09	59.87	1
0.27	247.07	10.54	237.58	191.82	59.90	1
0.24	249.21	10.93	239.51	193.54	59.92	1
0.21	251.33	11.32	241.42	195.26	59.93	1
0.18	170.15	11.71	158.43	166.66	-8.23	1
0.16	172.06	12.11	159.94	168.35	-8.40	1
0.13	173.96	12.51	161.45	170.03	-8.58	1
0.10	175.86	12.92	162.94	171.70	-8.77	1
0.08	177.75	13.32	164.42	173.37	-8.95	1
0.08	178.21	13.32	164.89	173.37	-8.49	1
0.06	179.49	13.56	165.93	174.33	-8.39	1
0.05	180.77	13.79	166.98	175.28	-8.30	1
0.03	182.04	14.03	168.02	176.22	-8.21	1
0.02	183.32	14.26	169.05	177.17	-8.12	1
0.00	184.59	14.50	170.09	178.11	0.00	1

Time = 205. Degree of Consolidation = 27.0%

Total Settlement = 1.233

Settlement at End of Primary Consolidation = 1.895

Settlement caused by Primary Consolidation at time 205. = 0.517

Settlement caused by Secondary Compression at time 205. = 0.000

Settlement Due to Desiccation = 0.715

Surface Elevation = 2.34

*****Current Conditions in Dredged Fill*****

***** Coordinates *****

***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
4.50	2.83	0.50	7.97	2.26	2.26	1
4.47	2.82	0.50	7.97	2.26	2.26	1
4.45	2.81	0.50	7.97	2.26	2.26	1
4.42	2.80	0.49	7.97	2.26	2.26	1
4.40	2.79	0.49	7.97	2.26	2.26	1
4.37	2.78	0.49	7.97	2.26	2.26	1
4.35	2.77	0.48	7.97	2.26	2.26	1
4.32	2.76	0.48	7.97	2.26	2.26	1
4.30	2.75	0.48	7.97	2.26	2.26	1
4.27	2.75	0.48	7.97	2.26	2.26	1
4.25	2.74	0.47	7.97	2.26	2.26	1
4.22	2.73	0.47	7.97	2.26	2.26	1
4.20	2.72	0.47	7.97	2.26	2.26	1
4.17	2.71	0.47	7.97	2.26	2.26	1
4.15	2.70	0.46	7.97	2.26	2.26	1
4.12	2.69	0.46	7.97	2.26	2.26	1
4.10	2.68	0.46	7.97	2.26	2.26	1
4.07	2.67	0.45	7.97	2.26	2.26	1
4.05	2.66	0.45	7.97	2.26	2.26	1
4.02	2.65	0.45	7.97	2.26	2.26	1
4.00	2.65	0.45	7.97	2.26	2.26	1
3.97	2.64	0.44	7.97	2.26	2.26	1
3.95	2.63	0.44	7.97	2.26	2.26	1
3.92	2.62	0.44	7.97	2.26	2.26	1
3.90	2.61	0.43	7.97	2.26	2.26	1
3.87	2.60	0.43	7.97	2.26	2.26	1
3.85	2.59	0.43	7.97	2.26	2.26	1
3.82	2.58	0.43	7.97	2.26	2.26	1
3.80	2.57	0.42	7.97	2.26	2.26	1
3.77	2.56	0.42	7.97	2.26	2.26	1
3.75	2.55	0.42	7.97	2.26	2.26	1
3.72	2.55	0.42	7.97	2.26	2.26	1
3.70	2.54	0.41	7.97	2.26	2.26	1
3.67	2.53	0.41	7.97	2.26	2.26	1
3.65	2.52	0.41	7.97	2.26	2.26	1
3.62	2.51	0.40	7.97	2.26	2.26	1
3.60	2.50	0.40	7.97	2.26	2.26	1
3.57	2.49	0.40	7.97	2.26	2.26	1
3.55	2.48	0.40	7.97	2.26	2.26	1
3.52	2.47	0.39	7.97	2.26	2.26	1
3.50	2.46	0.39	7.97	2.26	2.26	1
3.50	2.46	0.39	7.97	2.26	2.26	1
3.47	2.45	0.39	7.97	2.26	5.29	1
3.45	2.45	0.38	7.97	2.26	5.28	1
3.42	2.44	0.38	7.97	2.26	5.27	1
3.40	2.43	0.38	7.97	2.26	5.26	1
3.37	2.42	0.38	7.97	2.26	5.25	1
3.35	2.41	0.37	7.97	2.26	5.25	1

3.32	2.40	0.37	7.97	2.26	5.24	1
3.30	2.39	0.37	7.97	2.26	5.23	1
3.27	2.38	0.37	7.97	2.26	5.22	1
3.25	2.37	0.36	7.97	2.26	5.21	1
3.22	2.36	0.36	7.97	2.26	5.20	1
3.20	2.35	0.36	7.97	2.26	5.19	1
3.17	2.35	0.35	7.97	2.26	5.18	1
3.15	2.34	0.35	7.97	2.26	5.17	1
3.12	2.33	0.35	7.97	2.26	5.16	1
3.10	2.32	0.35	7.97	2.26	5.15	1
3.07	2.31	0.34	7.97	2.26	5.14	1
3.05	2.30	0.34	7.97	2.26	5.13	1
3.02	2.29	0.34	7.97	2.26	5.12	1
3.00	2.28	0.33	7.97	2.26	5.12	1
2.97	2.27	0.33	7.97	2.26	5.11	1
2.95	2.26	0.33	7.97	2.26	5.10	1
2.92	2.25	0.33	7.97	2.26	5.09	1
2.90	2.25	0.32	7.97	2.26	5.09	1
2.87	2.24	0.32	7.97	2.26	2.26	1
2.85	2.23	0.32	7.97	2.26	2.26	1
2.82	2.22	0.31	7.97	2.26	2.26	1
2.80	2.21	0.31	7.97	2.87	5.04	1
2.77	2.19	0.31	7.97	5.28	5.03	1
2.75	2.18	0.31	7.97	5.33	5.03	1
2.72	2.16	0.30	7.97	5.38	5.02	1
2.70	2.14	0.30	7.97	5.44	5.01	1
2.67	2.12	0.30	7.97	5.49	5.00	1
2.65	2.10	0.30	7.97	5.54	5.00	1
2.62	2.09	0.29	7.97	5.59	4.99	1
2.60	2.07	0.29	7.97	5.64	4.98	1
2.57	2.05	0.29	7.97	5.69	4.97	1
2.55	2.03	0.28	7.97	5.74	4.97	1
2.52	2.01	0.28	7.97	5.78	4.96	1
2.50	1.99	0.28	7.97	5.82	4.95	1
2.50	1.99	0.28	7.97	5.82	4.95	1
2.47	1.97	0.28	7.97	5.87	4.94	1
2.45	1.95	0.27	7.97	5.91	4.93	1
2.42	1.93	0.27	7.97	5.95	4.92	1
2.40	1.92	0.27	7.97	5.98	4.92	1
2.37	1.90	0.26	7.97	6.02	4.91	1
2.35	1.88	0.26	7.97	6.05	4.90	1
2.32	1.86	0.26	7.97	6.08	4.89	1
2.30	1.84	0.26	7.97	6.12	4.89	1
2.27	1.82	0.25	7.97	6.14	4.88	1
2.25	1.80	0.25	7.97	6.17	4.88	1
2.22	1.78	0.25	7.97	6.20	4.87	1
2.20	1.76	0.25	7.97	6.22	4.87	1
2.17	1.74	0.24	7.97	6.25	4.86	1
2.15	1.72	0.24	7.97	6.27	4.86	1
2.12	1.70	0.24	7.97	6.29	4.85	1
2.10	1.68	0.23	7.97	6.30	4.85	1
2.07	1.66	0.23	7.97	6.32	4.85	1
2.05	1.64	0.23	7.97	6.33	4.84	1
2.02	1.61	0.23	7.97	6.35	4.84	1

2.00	1.59	0.22	7.97	6.36	4.83	1
1.97	1.57	0.22	7.97	6.37	4.83	1
1.95	1.55	0.22	7.97	6.37	4.82	1
1.92	1.53	0.21	7.97	6.38	4.82	1
1.90	1.51	0.21	7.97	6.39	4.82	1
1.87	1.49	0.21	7.97	6.39	4.81	1
1.85	1.47	0.21	7.97	6.39	4.81	1
1.82	1.45	0.20	7.97	6.40	4.80	1
1.80	1.43	0.20	7.97	6.40	4.80	1
1.77	1.41	0.20	7.97	6.40	4.80	1
1.75	1.39	0.20	7.97	6.39	4.80	1
1.72	1.37	0.19	7.97	6.39	4.79	1
1.70	1.35	0.19	7.97	6.39	4.79	1
1.67	1.33	0.19	7.97	6.39	4.78	1
1.65	1.31	0.18	7.97	6.38	4.78	1
1.62	1.29	0.18	7.97	6.38	4.77	1
1.60	1.26	0.18	7.97	6.37	4.77	1
1.57	1.24	0.18	7.97	6.37	4.77	1
1.55	1.22	0.17	7.97	6.36	4.76	1
1.52	1.20	0.17	7.97	6.35	4.76	1
1.50	1.18	0.17	7.97	6.35	4.75	1
1.50	1.18	0.17	7.97	6.35	4.75	1
1.46	1.15	0.16	7.97	6.34	4.74	1
1.43	1.13	0.16	7.97	6.32	4.74	1
1.39	1.10	0.16	7.97	6.31	4.74	1
1.36	1.07	0.15	7.97	6.30	4.73	1
1.32	1.04	0.15	7.97	6.29	4.73	1
1.29	1.01	0.14	7.97	6.28	4.72	1
1.25	0.98	0.14	7.97	6.26	4.72	1
1.22	0.95	0.14	7.97	6.25	4.71	1
1.18	0.93	0.13	7.97	6.24	4.71	1
1.15	0.90	0.13	7.97	6.22	4.71	1
1.11	0.87	0.12	7.97	6.21	4.70	1
1.08	0.84	0.12	7.97	6.20	4.70	1
1.05	0.81	0.12	7.97	6.18	4.69	1
1.01	0.79	0.11	7.97	6.17	4.69	1
0.98	0.76	0.11	7.97	6.16	4.69	1
0.94	0.73	0.10	7.97	6.14	4.68	1
0.91	0.70	0.10	7.97	6.13	4.68	1
0.87	0.67	0.10	7.97	6.12	4.67	1
0.84	0.65	0.09	7.97	6.10	4.67	1
0.80	0.62	0.09	7.97	6.09	4.66	1
0.77	0.59	0.09	7.97	6.07	4.66	1
0.73	0.56	0.08	7.97	6.06	4.66	1
0.70	0.54	0.08	7.97	6.05	4.65	1
0.66	0.51	0.07	7.97	6.04	4.65	1
0.62	0.48	0.07	7.97	6.02	4.64	1
0.59	0.45	0.07	7.97	6.01	4.64	1
0.55	0.43	0.06	7.97	6.00	4.63	1
0.52	0.40	0.06	7.97	5.98	4.63	1
0.48	0.37	0.05	7.97	5.97	4.63	1
0.45	0.35	0.05	7.97	5.96	4.62	1
0.41	0.32	0.05	7.97	5.95	4.62	1
0.38	0.29	0.04	7.97	5.94	4.61	1

0.34	0.26	0.04	7.97	5.92	4.60	1
0.31	0.24	0.03	7.97	5.91	4.60	1
0.28	0.21	0.03	7.97	5.90	4.59	1
0.24	0.18	0.03	7.97	5.89	4.59	1
0.21	0.16	0.02	7.97	5.88	4.58	1
0.17	0.13	0.02	7.97	5.87	4.58	1
0.14	0.10	0.02	7.97	5.86	4.57	1
0.10	0.08	0.01	7.97	5.85	4.56	1
0.10	0.08	0.01	7.97	5.85	4.56	1
0.08	0.06	0.01	7.97	5.83	4.55	1
0.06	0.05	0.01	7.97	5.82	4.55	1
0.04	0.03	0.00	7.97	5.80	4.54	1
0.02	0.02	0.00	7.97	5.79	4.53	1
0.00	0.00	0.00	7.97	5.78	4.53	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
2.83	0.00	0.00	0.00	0.00	0.00	1
2.82	0.61	0.61	0.00	0.00	0.00	1
2.81	1.21	1.21	0.00	0.00	0.00	1
2.80	1.82	1.82	0.00	0.00	0.00	1
2.79	2.42	2.42	0.00	0.00	0.00	1
2.78	3.03	3.03	0.00	0.00	0.00	1
2.77	3.63	3.63	0.00	0.00	0.00	1
2.76	4.24	4.24	0.00	0.00	0.00	1
2.75	4.84	4.84	0.00	0.00	0.00	1
2.75	5.45	5.45	0.00	0.00	0.00	1
2.74	6.05	6.05	0.00	0.00	0.00	1
2.73	6.66	6.66	0.00	0.00	0.00	1
2.72	7.26	7.26	0.00	0.00	0.00	1
2.71	7.87	7.87	0.00	0.00	0.00	1
2.70	8.47	8.47	0.00	0.00	0.00	1
2.69	9.08	9.08	0.00	0.00	0.00	1
2.68	9.68	9.68	0.00	0.00	0.00	1
2.67	10.29	10.29	0.00	0.00	0.00	1
2.66	10.89	10.89	0.00	0.00	0.00	1
2.65	11.50	11.50	0.00	0.00	0.00	1
2.65	12.10	12.10	0.00	0.00	0.00	1
2.64	12.71	12.71	0.00	0.00	0.00	1
2.63	13.31	13.31	0.00	0.00	0.00	1
2.62	13.92	13.92	0.00	0.00	0.00	1
2.61	14.52	14.52	0.00	0.00	0.00	1
2.60	15.13	15.13	0.00	0.00	0.00	1
2.59	15.73	15.73	0.00	0.00	0.00	1
2.58	16.34	16.34	0.00	0.00	0.00	1
2.57	16.94	16.94	0.00	0.00	0.00	1
2.56	17.55	17.55	0.00	0.00	0.00	1
2.55	18.15	18.15	0.00	0.00	0.00	1
2.55	18.76	18.76	0.00	0.00	0.00	1
2.54	19.36	19.36	0.00	0.00	0.00	1
2.53	19.97	19.97	0.00	0.00	0.00	1
2.52	20.57	20.57	0.00	0.00	0.00	1

2.51	21.18	21.18	0.00	0.00	0.00	1
2.50	21.78	21.78	0.00	0.00	0.00	1
2.49	22.39	22.39	0.00	0.00	0.00	1
2.48	22.99	22.99	0.00	0.00	0.00	1
2.47	23.60	23.60	0.00	0.00	0.00	1
2.46	24.20	24.20	0.00	0.00	0.00	1
2.46	24.81	24.81	0.00	0.00	0.00	1
2.45	25.54	25.54	0.00	0.00	0.00	1
2.45	26.27	26.27	0.00	0.00	0.00	1
2.44	26.88	26.88	0.00	0.00	0.00	1
2.43	27.48	27.48	0.00	0.00	0.00	1
2.42	28.09	28.09	0.00	0.00	0.00	1
2.41	28.69	28.69	0.00	0.00	0.00	1
2.40	29.30	29.30	0.00	0.00	0.00	1
2.39	29.90	29.90	0.00	0.00	0.00	1
2.38	30.51	30.51	0.00	0.00	0.00	1
2.37	31.11	31.11	0.00	0.00	0.00	1
2.36	31.72	31.72	0.00	0.00	0.00	1
2.35	32.32	32.32	0.00	0.00	0.00	1
2.35	32.93	32.93	0.00	0.00	0.00	1
2.34	33.53	33.53	0.00	0.00	0.00	1
2.33	34.14	34.14	0.00	0.00	0.00	1
2.32	34.74	34.74	0.00	0.00	0.00	1
2.31	35.35	35.35	0.00	0.00	0.00	1
2.30	35.95	35.95	0.00	0.00	0.00	1
2.29	36.56	36.56	0.00	0.00	0.00	1
2.28	37.16	37.16	0.00	0.00	0.00	1
2.27	37.77	37.77	0.00	0.00	0.00	1
2.26	38.37	38.37	0.00	0.00	0.00	1
2.25	38.98	38.98	0.00	0.00	0.00	1
2.25	39.58	39.58	0.00	0.00	0.00	1
2.24	40.19	40.19	0.00	0.00	0.00	1
2.23	40.79	40.79	0.00	0.00	0.00	1
2.22	41.40	41.40	0.00	0.00	0.00	1
2.21	83.99	27.21	81.89	57.38	28.55	1
2.19	85.74	25.60	83.66	58.83	30.46	1
2.18	87.48	23.97	85.43	60.29	32.38	1
2.16	89.23	22.34	87.19	61.74	34.30	1
2.14	90.98	20.71	88.94	63.20	36.22	1
2.12	92.73	19.48	90.70	64.66	37.74	1
2.10	94.48	18.58	92.44	66.12	38.93	1
2.09	96.23	17.70	94.18	67.57	40.10	1
2.07	97.98	16.85	95.92	69.03	41.24	1
2.05	99.73	16.03	97.65	70.49	42.36	1
2.03	101.47	15.24	99.38	71.94	43.44	1
2.01	103.22	14.47	101.11	73.40	44.50	1
1.99	104.96	13.74	102.83	74.85	45.53	1
1.99	104.96	2.14	102.83	74.85	45.53	1
1.97	106.71	13.00	104.55	76.30	46.55	1
1.95	108.45	12.30	106.26	77.75	47.55	1
1.93	110.19	11.63	107.98	79.20	48.51	1
1.92	111.93	10.98	109.69	80.65	49.45	1
1.90	113.67	10.37	111.39	82.10	50.35	1
1.88	115.41	9.89	113.10	83.55	51.12	1

1.86	117.15	9.62	114.80	84.99	51.69	1
1.84	118.88	9.35	116.49	86.43	52.25	1
1.82	120.61	9.10	118.19	87.87	52.79	1
1.80	122.34	8.86	119.88	89.31	53.32	1
1.78	124.07	8.63	121.57	90.75	53.84	1
1.76	125.80	8.42	123.26	92.19	54.34	1
1.74	127.53	8.23	124.94	93.62	54.83	1
1.72	129.25	8.05	126.62	95.05	55.30	1
1.70	130.97	7.88	128.30	96.48	55.76	1
1.68	132.69	7.73	129.97	97.91	56.20	1
1.66	134.41	7.59	131.64	99.34	56.63	1
1.64	136.12	7.47	133.31	100.76	57.04	1
1.61	137.84	7.36	134.98	102.18	57.44	1
1.59	139.55	7.26	136.65	103.60	57.83	1
1.57	141.26	7.18	138.31	105.02	58.21	1
1.55	142.97	7.11	139.97	106.44	58.57	1
1.53	144.67	7.06	141.62	107.85	58.92	1
1.51	146.37	7.01	143.28	109.26	59.25	1
1.49	148.07	6.97	144.93	110.67	59.58	1
1.47	149.77	6.95	146.58	112.08	59.90	1
1.45	151.47	6.93	148.22	113.48	60.20	1
1.43	153.16	6.93	149.87	114.88	60.50	1
1.41	154.86	6.93	151.51	116.28	60.79	1
1.39	156.54	6.94	153.14	117.68	61.07	1
1.37	158.23	6.96	154.78	119.08	61.35	1
1.35	159.92	6.98	156.41	120.47	61.61	1
1.33	161.60	7.01	158.04	121.86	61.87	1
1.31	163.28	7.05	159.66	123.25	62.13	1
1.29	164.96	7.09	161.29	124.63	62.38	1
1.26	166.63	7.14	162.91	126.02	62.63	1
1.24	168.30	7.19	164.52	127.40	62.87	1
1.22	169.97	7.24	166.14	128.78	63.10	1
1.20	171.64	7.30	167.75	130.15	63.34	1
1.18	173.31	7.36	169.36	131.53	63.57	1
1.18	173.31	3.95	169.36	131.53	63.57	1
1.15	175.63	7.45	171.60	133.45	63.89	1
1.13	177.96	7.55	173.84	135.36	64.20	1
1.10	180.27	7.64	176.08	137.27	64.51	1
1.07	182.58	7.75	178.30	139.17	64.82	1
1.04	184.89	7.85	180.52	141.07	65.12	1
1.01	187.19	7.96	182.74	142.96	65.42	1
0.98	189.48	8.07	184.94	144.85	65.72	1
0.95	191.77	8.18	187.14	146.73	66.01	1
0.93	194.06	8.30	189.34	148.60	66.31	1
0.90	196.34	8.41	191.52	150.47	66.60	1
0.87	198.61	8.53	193.70	152.34	66.89	1
0.84	200.87	8.65	195.86	154.20	67.18	1
0.81	203.13	8.76	197.91	156.05	67.47	1
0.79	205.39	8.88	199.95	157.89	67.76	1
0.76	207.64	9.00	201.98	159.73	68.05	1
0.73	209.88	9.12	204.01	161.57	68.35	1
0.70	212.12	9.23	206.03	163.39	68.64	1
0.67	214.35	9.35	208.05	165.22	68.93	1
0.65	216.57	9.47	210.06	167.03	69.22	1

0.62	218.79	9.58	212.06	168.84	69.51	1
0.59	221.00	9.70	214.06	170.64	69.80	1
0.56	223.20	9.81	216.05	172.44	70.10	1
0.54	225.40	9.93	218.04	174.23	70.39	1
0.51	227.60	10.08	220.02	176.02	70.65	1
0.48	229.79	10.30	221.99	177.80	70.84	1
0.45	231.97	10.52	223.96	179.57	71.02	1
0.43	234.14	10.74	225.93	181.34	71.21	1
0.40	236.31	10.96	227.88	183.10	71.40	1
0.37	238.48	11.18	229.84	184.86	71.59	1
0.35	240.63	11.39	231.78	186.61	71.79	1
0.32	242.79	11.60	233.72	188.35	71.99	1
0.29	244.93	11.81	235.66	190.09	72.19	1
0.26	247.07	12.01	237.58	191.82	72.39	1
0.24	249.21	12.21	239.51	193.54	72.60	1
0.21	135.72	12.41	123.31	124.73	-1.42	1
0.18	137.62	12.60	125.02	126.41	-1.39	1
0.16	139.52	12.79	126.73	128.09	-1.35	1
0.13	141.41	12.97	128.44	129.76	-1.32	1
0.10	143.31	13.15	130.16	131.43	-1.27	1
0.08	145.20	13.32	131.87	133.10	-1.23	1
0.08	145.66	13.32	132.34	133.10	-0.76	1
0.06	146.94	13.58	133.36	134.05	-0.69	1
0.05	148.22	13.83	134.39	135.00	-0.61	1
0.03	149.49	14.07	135.42	135.95	-0.53	1
0.02	150.76	14.31	136.45	136.89	-0.44	1
0.00	152.03	14.55	137.48	137.84	0.00	1

Time = 295. Degree of Consolidation = 33.0%

Total Settlement = 1.673

Settlement at End of Primary Consolidation = 1.887

Settlement caused by Primary Consolidation at time 295. = 0.628

Settlement caused by Secondary Compression at time 295. = 0.000

Settlement Due to Desiccation = 1.045

Surface Elevation = 1.90

*****Current Conditions in Dredged Fill*****

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
4.50	2.61	0.50	7.97	2.26	2.26	1
4.47	2.60	0.50	7.97	2.26	2.26	1

4.45	2.59	0.50	7.97	2.26	2.26	1
4.42	2.58	0.49	7.97	2.26	2.26	1
4.40	2.57	0.49	7.97	2.26	2.26	1
4.37	2.56	0.49	7.97	2.26	2.26	1
4.35	2.56	0.48	7.97	2.26	2.26	1
4.32	2.55	0.48	7.97	2.26	2.26	1
4.30	2.54	0.48	7.97	2.26	2.26	1
4.27	2.53	0.48	7.97	2.26	2.26	1
4.25	2.52	0.47	7.97	2.26	2.26	1
4.22	2.51	0.47	7.97	2.26	2.26	1
4.20	2.50	0.47	7.97	2.26	2.26	1
4.17	2.49	0.47	7.97	2.26	2.26	1
4.15	2.48	0.46	7.97	2.26	2.26	1
4.12	2.47	0.46	7.97	2.26	2.26	1
4.10	2.46	0.46	7.97	2.26	2.26	1
4.07	2.46	0.45	7.97	2.26	2.26	1
4.05	2.45	0.45	7.97	2.26	2.26	1
4.02	2.44	0.45	7.97	2.26	2.26	1
4.00	2.43	0.45	7.97	2.26	2.26	1
3.97	2.42	0.44	7.97	2.26	2.26	1
3.95	2.41	0.44	7.97	2.26	2.26	1
3.92	2.40	0.44	7.97	2.26	2.26	1
3.90	2.39	0.43	7.97	2.26	2.26	1
3.87	2.38	0.43	7.97	2.26	2.26	1
3.85	2.37	0.43	7.97	2.26	2.26	1
3.82	2.36	0.43	7.97	2.26	2.26	1
3.80	2.36	0.42	7.97	2.26	2.26	1
3.77	2.35	0.42	7.97	2.26	2.26	1
3.75	2.34	0.42	7.97	2.26	2.26	1
3.72	2.33	0.42	7.97	2.26	2.26	1
3.70	2.32	0.41	7.97	2.26	2.26	1
3.67	2.31	0.41	7.97	2.26	2.26	1
3.65	2.30	0.41	7.97	2.26	2.26	1
3.62	2.29	0.40	7.97	2.26	2.26	1
3.60	2.28	0.40	7.97	2.26	2.26	1
3.57	2.27	0.40	7.97	2.26	2.26	1
3.55	2.27	0.40	7.97	2.26	2.26	1
3.52	2.26	0.39	7.97	2.26	2.26	1
3.50	2.24	0.39	7.97	5.32	2.26	1
3.50	2.24	0.39	7.97	5.31	2.26	1
3.47	2.23	0.39	7.97	2.26	5.30	1
3.45	2.22	0.38	7.97	2.26	5.29	1
3.42	2.21	0.38	7.97	2.26	5.28	1
3.40	2.20	0.38	7.97	2.26	5.27	1
3.37	2.20	0.38	7.97	2.26	5.26	1
3.35	2.19	0.37	7.97	2.26	5.25	1
3.32	2.18	0.37	7.97	2.26	5.24	1
3.30	2.17	0.37	7.97	2.26	5.23	1
3.27	2.16	0.37	7.97	2.26	5.22	1
3.25	2.15	0.36	7.97	2.26	5.21	1
3.22	2.14	0.36	7.97	2.26	5.20	1
3.20	2.13	0.36	7.97	2.26	5.19	1
3.17	2.12	0.35	7.97	2.26	5.18	1
3.15	2.11	0.35	7.97	2.26	5.17	1

3.12	2.10	0.35	7.97	2.26	5.16	1
3.10	2.10	0.35	7.97	2.26	5.15	1
3.07	2.09	0.34	7.97	2.26	5.14	1
3.05	2.08	0.34	7.97	2.26	5.13	1
3.02	2.07	0.34	7.97	2.26	5.13	1
3.00	2.06	0.33	7.97	2.26	5.12	1
2.97	2.05	0.33	7.97	2.26	5.11	1
2.95	2.04	0.33	7.97	2.26	5.10	1
2.92	2.03	0.33	7.97	2.26	5.10	1
2.90	2.02	0.32	7.97	2.26	5.09	1
2.87	2.01	0.32	7.97	2.26	5.08	1
2.85	2.00	0.32	7.97	2.26	5.07	1
2.82	2.00	0.31	7.97	2.26	5.07	1
2.80	1.99	0.31	7.97	2.26	5.06	1
2.77	1.98	0.31	7.97	2.26	5.05	1
2.75	1.97	0.31	7.97	2.26	5.04	1
2.72	1.96	0.30	7.97	2.26	5.04	1
2.70	1.95	0.30	7.97	2.26	5.03	1
2.67	1.94	0.30	7.97	2.26	5.02	1
2.65	1.93	0.30	7.97	2.26	5.02	1
2.62	1.92	0.29	7.97	2.26	5.01	1
2.60	1.91	0.29	7.97	2.26	5.00	1
2.57	1.91	0.29	7.97	2.26	4.99	1
2.55	1.90	0.28	7.97	2.26	4.99	1
2.52	1.89	0.28	7.97	2.26	4.98	1
2.50	1.88	0.28	7.97	4.97	2.26	1
2.50	1.88	0.28	7.97	4.97	2.26	1
2.47	1.86	0.28	7.97	2.90	4.93	1
2.45	1.85	0.27	7.97	4.96	4.92	1
2.42	1.83	0.27	7.97	4.99	4.92	1
2.40	1.82	0.27	7.97	5.02	4.91	1
2.37	1.80	0.26	7.97	5.05	4.90	1
2.35	1.78	0.26	7.97	5.08	4.89	1
2.32	1.77	0.26	7.97	5.12	4.89	1
2.30	1.75	0.26	7.97	5.15	4.88	1
2.27	1.73	0.25	7.97	5.19	4.88	1
2.25	1.71	0.25	7.97	5.22	4.87	1
2.22	1.70	0.25	7.97	5.26	4.87	1
2.20	1.68	0.25	7.97	5.29	4.86	1
2.17	1.66	0.24	7.97	5.33	4.86	1
2.15	1.64	0.24	7.97	5.36	4.85	1
2.12	1.63	0.24	7.97	5.40	4.85	1
2.10	1.61	0.23	7.97	5.43	4.85	1
2.07	1.59	0.23	7.97	5.46	4.84	1
2.05	1.57	0.23	7.97	5.49	4.84	1
2.02	1.55	0.23	7.97	5.52	4.83	1
2.00	1.54	0.22	7.97	5.55	4.83	1
1.97	1.52	0.22	7.97	5.58	4.82	1
1.95	1.50	0.22	7.97	5.61	4.82	1
1.92	1.48	0.21	7.97	5.63	4.82	1
1.90	1.46	0.21	7.97	5.66	4.81	1
1.87	1.44	0.21	7.97	5.68	4.81	1
1.85	1.42	0.21	7.97	5.70	4.80	1
1.82	1.41	0.20	7.97	5.73	4.80	1

1.80	1.39	0.20	7.97	5.75	4.79	1
1.77	1.37	0.20	7.97	5.77	4.79	1
1.75	1.35	0.20	7.97	5.78	4.79	1
1.72	1.33	0.19	7.97	5.80	4.78	1
1.70	1.31	0.19	7.97	5.82	4.78	1
1.67	1.29	0.19	7.97	5.83	4.77	1
1.65	1.27	0.18	7.97	5.85	4.77	1
1.62	1.25	0.18	7.97	5.86	4.77	1
1.60	1.24	0.18	7.97	5.87	4.76	1
1.57	1.22	0.18	7.97	5.88	4.76	1
1.55	1.20	0.17	7.97	5.90	4.75	1
1.52	1.18	0.17	7.97	5.91	4.75	1
1.50	1.16	0.17	7.97	5.91	4.74	1
1.50	1.16	0.17	7.97	5.91	4.74	1
1.46	1.13	0.16	7.97	5.93	4.74	1
1.43	1.10	0.16	7.97	5.94	4.74	1
1.39	1.08	0.16	7.97	5.95	4.73	1
1.36	1.05	0.15	7.97	5.96	4.73	1
1.32	1.02	0.15	7.97	5.96	4.72	1
1.29	1.00	0.14	7.97	5.97	4.72	1
1.25	0.97	0.14	7.97	5.97	4.71	1
1.22	0.94	0.14	7.97	5.98	4.71	1
1.18	0.91	0.13	7.97	5.98	4.71	1
1.15	0.89	0.13	7.97	5.98	4.70	1
1.11	0.86	0.12	7.97	5.98	4.70	1
1.08	0.83	0.12	7.97	5.98	4.69	1
1.05	0.81	0.12	7.97	5.98	4.69	1
1.01	0.78	0.11	7.97	5.98	4.69	1
0.98	0.75	0.11	7.97	5.98	4.68	1
0.94	0.72	0.10	7.97	5.98	4.68	1
0.91	0.70	0.10	7.97	5.97	4.67	1
0.87	0.67	0.10	7.97	5.97	4.67	1
0.84	0.64	0.09	7.97	5.97	4.66	1
0.80	0.61	0.09	7.97	5.96	4.66	1
0.77	0.59	0.09	7.97	5.96	4.66	1
0.73	0.56	0.08	7.97	5.95	4.65	1
0.70	0.53	0.08	7.97	5.95	4.65	1
0.66	0.51	0.07	7.97	5.94	4.64	1
0.62	0.48	0.07	7.97	5.94	4.64	1
0.59	0.45	0.07	7.97	5.93	4.63	1
0.55	0.43	0.06	7.97	5.92	4.63	1
0.52	0.40	0.06	7.97	5.92	4.63	1
0.48	0.37	0.05	7.97	5.91	4.62	1
0.45	0.34	0.05	7.97	5.91	4.62	1
0.41	0.32	0.05	7.97	5.90	4.61	1
0.38	0.29	0.04	7.97	5.89	4.61	1
0.34	0.26	0.04	7.97	5.89	4.60	1
0.31	0.24	0.03	7.97	5.88	4.60	1
0.28	0.21	0.03	7.97	5.88	4.60	1
0.24	0.18	0.03	7.97	5.87	4.59	1
0.21	0.16	0.02	7.97	5.86	4.59	1
0.17	0.13	0.02	7.97	5.86	4.58	1
0.14	0.10	0.02	7.97	5.85	4.58	1
0.10	0.08	0.01	7.97	5.85	4.58	1

0.10	0.08	0.01	7.97	5.85	4.57	1
0.08	0.06	0.01	7.97	5.83	4.57	1
0.06	0.05	0.01	7.97	5.82	4.56	1
0.04	0.03	0.00	7.97	5.80	4.56	1
0.02	0.02	0.00	7.97	5.79	4.55	1
0.00	0.00	0.00	7.97	5.78	4.55	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
2.61	0.00	0.00	0.00	0.00	0.00	1
2.60	0.61	0.61	0.00	0.00	0.00	1
2.59	1.21	1.21	0.00	0.00	0.00	1
2.58	1.82	1.82	0.00	0.00	0.00	1
2.57	2.42	2.42	0.00	0.00	0.00	1
2.56	3.03	3.03	0.00	0.00	0.00	1
2.56	3.63	3.63	0.00	0.00	0.00	1
2.55	4.24	4.24	0.00	0.00	0.00	1
2.54	4.84	4.84	0.00	0.00	0.00	1
2.53	5.45	5.45	0.00	0.00	0.00	1
2.52	6.05	6.05	0.00	0.00	0.00	1
2.51	6.66	6.66	0.00	0.00	0.00	1
2.50	7.26	7.26	0.00	0.00	0.00	1
2.49	7.87	7.87	0.00	0.00	0.00	1
2.48	8.47	8.47	0.00	0.00	0.00	1
2.47	9.08	9.08	0.00	0.00	0.00	1
2.46	9.68	9.68	0.00	0.00	0.00	1
2.46	10.29	10.29	0.00	0.00	0.00	1
2.45	10.89	10.89	0.00	0.00	0.00	1
2.44	11.50	11.50	0.00	0.00	0.00	1
2.43	12.10	12.10	0.00	0.00	0.00	1
2.42	12.71	12.71	0.00	0.00	0.00	1
2.41	13.31	13.31	0.00	0.00	0.00	1
2.40	13.92	13.92	0.00	0.00	0.00	1
2.39	14.52	14.52	0.00	0.00	0.00	1
2.38	15.13	15.13	0.00	0.00	0.00	1
2.37	15.73	15.73	0.00	0.00	0.00	1
2.36	16.34	16.34	0.00	0.00	0.00	1
2.36	16.94	16.94	0.00	0.00	0.00	1
2.35	17.55	17.55	0.00	0.00	0.00	1
2.34	18.15	18.15	0.00	0.00	0.00	1
2.33	18.76	18.76	0.00	0.00	0.00	1
2.32	19.36	19.36	0.00	0.00	0.00	1
2.31	19.97	19.97	0.00	0.00	0.00	1
2.30	20.57	20.57	0.00	0.00	0.00	1
2.29	21.18	21.18	0.00	0.00	0.00	1
2.28	21.78	21.78	0.00	0.00	0.00	1
2.27	22.39	22.39	0.00	0.00	0.00	1
2.27	22.99	22.99	0.00	0.00	0.00	1
2.26	23.60	23.60	0.00	0.00	0.00	1
2.24	24.20	24.20	0.00	0.00	0.00	1
2.24	24.81	24.81	0.00	0.00	0.00	1
2.23	25.54	25.54	0.00	0.00	0.00	1

2.22	26.27	26.27	0.00	0.00	0.00	1
2.21	26.88	26.88	0.00	0.00	0.00	1
2.20	27.48	27.48	0.00	0.00	0.00	1
2.20	28.09	28.09	0.00	0.00	0.00	1
2.19	28.69	28.69	0.00	0.00	0.00	1
2.18	29.30	29.30	0.00	0.00	0.00	1
2.17	29.90	29.90	0.00	0.00	0.00	1
2.16	30.51	30.51	0.00	0.00	0.00	1
2.15	31.11	31.11	0.00	0.00	0.00	1
2.14	31.72	31.72	0.00	0.00	0.00	1
2.13	32.32	32.32	0.00	0.00	0.00	1
2.12	32.93	32.93	0.00	0.00	0.00	1
2.11	33.53	33.53	0.00	0.00	0.00	1
2.10	34.14	34.14	0.00	0.00	0.00	1
2.10	34.74	34.74	0.00	0.00	0.00	1
2.09	35.35	35.35	0.00	0.00	0.00	1
2.08	35.95	35.95	0.00	0.00	0.00	1
2.07	36.56	36.56	0.00	0.00	0.00	1
2.06	37.16	37.16	0.00	0.00	0.00	1
2.05	37.77	37.77	0.00	0.00	0.00	1
2.04	38.37	38.37	0.00	0.00	0.00	1
2.03	38.98	38.98	0.00	0.00	0.00	1
2.02	39.58	39.58	0.00	0.00	0.00	1
2.01	40.19	40.19	0.00	0.00	0.00	1
2.00	40.79	40.79	0.00	0.00	0.00	1
2.00	41.40	41.40	0.00	0.00	0.00	1
1.99	42.01	42.01	0.00	0.00	0.00	1
1.98	42.61	42.61	0.00	0.00	0.00	1
1.97	43.22	43.22	0.00	0.00	0.00	1
1.96	43.82	43.82	0.00	0.00	0.00	1
1.95	44.43	44.43	0.00	0.00	0.00	1
1.94	45.03	45.03	0.00	0.00	0.00	1
1.93	45.64	45.64	0.00	0.00	0.00	1
1.92	46.24	46.24	0.00	0.00	0.00	1
1.91	46.85	46.85	0.00	0.00	0.00	1
1.91	47.45	47.45	0.00	0.00	0.00	1
1.90	48.06	48.06	0.00	0.00	0.00	1
1.89	48.66	48.66	0.00	0.00	0.00	1
1.88	49.27	22.60	0.00	0.00	26.67	1
1.88	49.87	49.87	0.00	0.00	26.67	1
1.86	106.71	14.69	104.55	76.30	53.34	1
1.85	108.45	36.83	106.26	77.75	31.49	1
1.83	110.19	35.64	107.98	79.20	32.98	1
1.82	111.93	34.41	109.69	80.65	34.50	1
1.80	113.67	33.13	111.39	82.10	36.07	1
1.78	115.41	31.81	113.10	83.55	37.68	1
1.77	117.15	30.44	114.80	84.99	39.34	1
1.75	118.88	29.27	116.49	86.43	40.80	1
1.73	120.61	28.20	118.19	87.87	42.16	1
1.71	122.34	27.14	119.88	89.31	43.52	1
1.70	124.07	26.08	121.57	90.75	44.86	1
1.68	125.80	25.03	123.26	92.19	46.20	1
1.66	127.53	23.99	124.94	93.62	47.53	1
1.64	129.25	22.97	126.62	95.05	48.85	1

1.63	130.97	21.95	128.30	96.48	50.16	1
1.61	132.69	20.96	129.97	97.91	51.45	1
1.59	134.41	19.99	131.64	99.34	52.71	1
1.57	136.12	19.44	133.31	100.76	53.54	1
1.55	137.84	18.92	134.98	102.18	54.36	1
1.54	139.55	18.41	136.65	103.60	55.16	1
1.52	141.26	17.93	138.31	105.02	55.93	1
1.50	142.97	17.46	139.97	106.44	56.69	1
1.48	144.67	17.02	141.62	107.85	57.43	1
1.46	146.37	16.59	143.28	109.26	58.15	1
1.44	148.07	16.18	144.93	110.67	58.85	1
1.42	149.77	15.79	146.58	112.08	59.53	1
1.41	151.47	15.42	148.22	113.48	60.20	1
1.39	153.16	15.06	149.87	114.88	60.84	1
1.37	154.86	14.73	151.51	116.28	61.47	1
1.35	156.54	14.41	153.14	117.68	62.07	1
1.33	158.23	14.12	154.78	119.08	62.66	1
1.31	159.92	13.83	156.41	120.47	63.24	1
1.29	161.60	13.57	158.04	121.86	63.79	1
1.27	163.28	13.32	159.66	123.25	64.33	1
1.25	164.96	13.09	161.29	124.63	64.86	1
1.24	166.63	12.87	162.91	126.02	65.36	1
1.22	168.30	12.67	164.52	127.40	65.86	1
1.20	169.97	12.49	166.14	128.78	66.33	1
1.18	171.64	12.32	167.75	130.15	66.80	1
1.16	173.31	12.16	169.36	131.53	67.24	1
1.16	173.31	3.95	169.36	131.53	67.24	1
1.13	175.63	11.94	171.60	133.45	67.87	1
1.10	177.96	11.75	173.84	135.36	68.47	1
1.08	180.27	11.58	176.08	137.27	69.05	1
1.05	182.58	11.44	178.30	139.17	69.60	1
1.02	184.89	11.32	180.52	141.07	70.13	1
1.00	187.19	11.22	182.74	142.96	70.64	1
0.97	189.48	11.13	184.94	144.85	71.13	1
0.94	191.77	11.07	187.14	146.73	71.60	1
0.91	194.06	11.03	189.34	148.60	72.05	1
0.89	196.34	11.00	191.52	150.47	72.49	1
0.86	198.61	10.98	193.70	152.34	72.91	1
0.83	200.87	10.98	195.86	154.20	73.32	1
0.81	203.13	10.99	197.91	156.05	73.72	1
0.78	205.39	11.02	199.95	157.89	74.11	1
0.75	207.64	11.05	201.98	159.73	74.48	1
0.72	209.88	11.09	204.01	161.57	74.84	1
0.70	212.12	11.15	206.03	163.39	75.20	1
0.67	214.35	11.21	208.05	165.22	75.55	1
0.64	216.57	11.28	210.06	167.03	75.89	1
0.61	218.79	11.35	212.06	168.84	76.22	1
0.59	221.00	11.43	214.06	170.64	76.55	1
0.56	223.20	11.52	216.05	172.44	76.87	1
0.53	225.40	11.61	218.04	174.23	77.19	1
0.51	227.60	11.70	220.02	176.02	77.50	1
0.48	229.79	11.80	221.99	177.80	77.81	1
0.45	231.97	11.90	223.96	179.57	78.12	1
0.43	234.14	12.00	225.93	181.34	78.43	1

0.40	236.31	12.10	227.88	183.10	78.73	1
0.37	238.48	12.21	229.84	184.86	79.04	1
0.34	240.63	12.31	231.78	186.61	79.34	1
0.32	242.79	12.42	233.72	188.35	79.64	1
0.29	244.93	12.52	235.66	190.09	79.95	1
0.26	247.07	12.63	237.58	191.82	80.25	1
0.24	117.01	12.73	104.27	101.56	2.72	1
0.21	118.90	12.84	106.07	103.23	2.84	1
0.18	120.80	12.94	107.86	104.90	2.96	1
0.16	122.69	13.04	109.65	106.58	3.08	1
0.13	124.58	13.14	111.45	108.25	3.20	1
0.10	126.48	13.23	113.24	109.92	3.33	1
0.08	128.37	13.32	115.04	111.58	3.46	1
0.08	128.83	13.32	115.51	111.58	3.92	1
0.06	130.11	13.58	116.53	112.53	4.00	1
0.05	131.39	13.83	117.56	113.48	4.07	1
0.03	132.66	14.07	118.59	114.43	4.16	1
0.02	133.93	14.31	119.62	115.38	4.24	1
0.00	135.20	14.55	120.65	116.32	4.33	1

Time = 390. Degree of Consolidation = 35.0%

Total Settlement = 1.890

Settlement at End of Primary Consolidation = 1.866

Settlement caused by Primary Consolidation at time 390. = 0.660

Settlement caused by Secondary Compression at time 390. = 0.000

Settlement Due to Desiccation = 1.230

Surface Elevation = 1.68

*****Current Conditions in Dredged Fill*****

***** Coordinates *****

***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
4.50	2.45	0.50	7.97	2.26	2.26	1
4.47	2.44	0.50	7.97	2.26	2.26	1
4.45	2.43	0.50	7.97	2.26	2.26	1
4.42	2.42	0.49	7.97	2.26	2.26	1
4.40	2.41	0.49	7.97	2.26	2.26	1
4.37	2.40	0.49	7.97	2.26	2.26	1
4.35	2.39	0.48	7.97	2.26	2.26	1
4.32	2.38	0.48	7.97	2.26	2.26	1
4.30	2.38	0.48	7.97	2.26	2.26	1
4.27	2.37	0.48	7.97	2.26	2.26	1

4.25	2.36	0.47	7.97	2.26	2.26	1
4.22	2.35	0.47	7.97	2.26	2.26	1
4.20	2.34	0.47	7.97	2.26	2.26	1
4.17	2.33	0.47	7.97	2.26	2.26	1
4.15	2.32	0.46	7.97	2.26	2.26	1
4.12	2.31	0.46	7.97	2.26	2.26	1
4.10	2.30	0.46	7.97	2.26	2.26	1
4.07	2.29	0.45	7.97	2.26	2.26	1
4.05	2.28	0.45	7.97	2.26	2.26	1
4.02	2.28	0.45	7.97	2.26	2.26	1
4.00	2.27	0.45	7.97	2.26	2.26	1
3.97	2.26	0.44	7.97	2.26	2.26	1
3.95	2.25	0.44	7.97	2.26	2.26	1
3.92	2.24	0.44	7.97	2.26	2.26	1
3.90	2.23	0.43	7.97	2.26	2.26	1
3.87	2.22	0.43	7.97	2.26	2.26	1
3.85	2.21	0.43	7.97	2.26	2.26	1
3.82	2.20	0.43	7.97	2.26	2.26	1
3.80	2.19	0.42	7.97	2.26	2.26	1
3.77	2.18	0.42	7.97	2.26	2.26	1
3.75	2.18	0.42	7.97	2.26	2.26	1
3.72	2.17	0.42	7.97	2.26	2.26	1
3.70	2.16	0.41	7.97	2.26	2.26	1
3.67	2.15	0.41	7.97	2.26	2.26	1
3.65	2.14	0.41	7.97	2.26	2.26	1
3.62	2.13	0.40	7.97	2.26	2.26	1
3.60	2.12	0.40	7.97	2.26	2.26	1
3.57	2.11	0.40	7.97	2.26	2.26	1
3.55	2.10	0.40	7.97	2.26	2.26	1
3.52	2.09	0.39	7.97	2.26	2.26	1
3.50	2.08	0.39	7.97	5.31	2.26	1
3.50	2.08	0.39	7.97	5.31	2.26	1
3.47	2.07	0.39	7.97	2.26	5.30	1
3.45	2.06	0.38	7.97	2.26	5.29	1
3.42	2.05	0.38	7.97	2.26	5.28	1
3.40	2.04	0.38	7.97	2.26	5.27	1
3.37	2.03	0.38	7.97	2.26	5.26	1
3.35	2.02	0.37	7.97	2.26	5.25	1
3.32	2.02	0.37	7.97	2.26	5.24	1
3.30	2.01	0.37	7.97	2.26	5.24	1
3.27	2.00	0.37	7.97	2.26	5.23	1
3.25	1.99	0.36	7.97	2.26	5.22	1
3.22	1.98	0.36	7.97	2.26	5.21	1
3.20	1.97	0.36	7.97	2.26	5.20	1
3.17	1.96	0.35	7.97	2.26	5.19	1
3.15	1.95	0.35	7.97	2.26	5.18	1
3.12	1.94	0.35	7.97	2.26	5.17	1
3.10	1.93	0.35	7.97	2.26	5.16	1
3.07	1.92	0.34	7.97	2.26	5.15	1
3.05	1.92	0.34	7.97	2.26	5.14	1
3.02	1.91	0.34	7.97	2.26	5.13	1
3.00	1.90	0.33	7.97	2.26	5.12	1
2.97	1.89	0.33	7.97	2.26	5.11	1
2.95	1.88	0.33	7.97	2.26	5.11	1

2.92	1.87	0.33	7.97	2.26	5.10	1
2.90	1.86	0.32	7.97	2.26	5.09	1
2.87	1.85	0.32	7.97	2.26	5.09	1
2.85	1.84	0.32	7.97	2.26	5.08	1
2.82	1.83	0.31	7.97	2.26	5.07	1
2.80	1.82	0.31	7.97	2.26	5.06	1
2.77	1.82	0.31	7.97	2.26	5.06	1
2.75	1.81	0.31	7.97	2.26	5.05	1
2.72	1.80	0.30	7.97	2.26	5.04	1
2.70	1.79	0.30	7.97	2.26	5.03	1
2.67	1.78	0.30	7.97	2.26	5.03	1
2.65	1.77	0.30	7.97	2.26	5.02	1
2.62	1.76	0.29	7.97	2.26	5.01	1
2.60	1.75	0.29	7.97	2.26	5.01	1
2.57	1.74	0.29	7.97	2.26	5.00	1
2.55	1.73	0.28	7.97	2.26	4.99	1
2.52	1.73	0.28	7.97	2.26	4.98	1
2.50	1.71	0.28	7.97	4.75	2.26	1
2.50	1.71	0.28	7.97	4.75	2.26	1
2.47	1.70	0.28	7.97	2.26	4.97	1
2.45	1.69	0.27	7.97	2.26	4.96	1
2.42	1.68	0.27	7.97	2.26	4.95	1
2.40	1.67	0.27	7.97	2.26	4.95	1
2.37	1.67	0.26	7.97	2.26	4.94	1
2.35	1.66	0.26	7.97	2.26	4.93	1
2.32	1.65	0.26	7.97	2.26	4.93	1
2.30	1.64	0.26	7.97	2.26	4.92	1
2.27	1.63	0.25	7.97	2.26	2.26	1
2.25	1.62	0.25	7.97	4.86	4.86	1
2.22	1.60	0.25	7.97	4.87	4.86	1
2.20	1.59	0.25	7.97	4.89	4.85	1
2.17	1.57	0.24	7.97	4.90	4.85	1
2.15	1.55	0.24	7.97	4.91	4.84	1
2.12	1.54	0.24	7.97	4.93	4.84	1
2.10	1.52	0.23	7.97	4.94	4.84	1
2.07	1.50	0.23	7.97	4.95	4.83	1
2.05	1.49	0.23	7.97	4.97	4.83	1
2.02	1.47	0.23	7.97	4.98	4.82	1
2.00	1.45	0.22	7.97	5.00	4.82	1
1.97	1.44	0.22	7.97	5.01	4.81	1
1.95	1.42	0.22	7.97	5.02	4.81	1
1.92	1.40	0.21	7.97	5.04	4.81	1
1.90	1.39	0.21	7.97	5.05	4.80	1
1.87	1.37	0.21	7.97	5.07	4.80	1
1.85	1.35	0.21	7.97	5.08	4.79	1
1.82	1.33	0.20	7.97	5.10	4.79	1
1.80	1.32	0.20	7.97	5.12	4.78	1
1.77	1.30	0.20	7.97	5.13	4.78	1
1.75	1.28	0.20	7.97	5.15	4.78	1
1.72	1.27	0.19	7.97	5.16	4.77	1
1.70	1.25	0.19	7.97	5.18	4.77	1
1.67	1.23	0.19	7.97	5.20	4.76	1
1.65	1.21	0.18	7.97	5.21	4.76	1
1.62	1.20	0.18	7.97	5.23	4.76	1

1.60	1.18	0.18	7.97	5.24	4.75	1
1.57	1.16	0.18	7.97	5.26	4.75	1
1.55	1.14	0.17	7.97	5.27	4.74	1
1.52	1.13	0.17	7.97	5.29	4.74	1
1.50	1.11	0.17	7.97	5.30	4.73	1
1.50	1.11	0.17	7.97	5.30	4.73	1
1.46	1.09	0.16	7.97	5.32	4.73	1
1.43	1.06	0.16	7.97	5.34	4.72	1
1.39	1.04	0.16	7.97	5.36	4.72	1
1.36	1.01	0.15	7.97	5.38	4.71	1
1.32	0.99	0.15	7.97	5.40	4.71	1
1.29	0.96	0.14	7.97	5.42	4.70	1
1.25	0.94	0.14	7.97	5.44	4.70	1
1.22	0.91	0.14	7.97	5.46	4.70	1
1.18	0.89	0.13	7.97	5.48	4.69	1
1.15	0.86	0.13	7.97	5.50	4.69	1
1.11	0.83	0.12	7.97	5.52	4.69	1
1.08	0.81	0.12	7.97	5.53	4.68	1
1.05	0.78	0.12	7.97	5.55	4.68	1
1.01	0.76	0.11	7.97	5.56	4.68	1
0.98	0.73	0.11	7.97	5.58	4.67	1
0.94	0.71	0.10	7.97	5.60	4.67	1
0.91	0.68	0.10	7.97	5.61	4.66	1
0.87	0.66	0.10	7.97	5.62	4.66	1
0.84	0.63	0.09	7.97	5.64	4.65	1
0.80	0.60	0.09	7.97	5.65	4.65	1
0.77	0.58	0.09	7.97	5.66	4.65	1
0.73	0.55	0.08	7.97	5.68	4.64	1
0.70	0.53	0.08	7.97	5.69	4.64	1
0.66	0.50	0.07	7.97	5.70	4.63	1
0.62	0.47	0.07	7.97	5.71	4.63	1
0.59	0.45	0.07	7.97	5.72	4.62	1
0.55	0.42	0.06	7.97	5.73	4.62	1
0.52	0.39	0.06	7.97	5.74	4.62	1
0.48	0.37	0.05	7.97	5.75	4.61	1
0.45	0.34	0.05	7.97	5.76	4.61	1
0.41	0.32	0.05	7.97	5.77	4.60	1
0.38	0.29	0.04	7.97	5.78	4.60	1
0.34	0.26	0.04	7.97	5.79	4.59	1
0.31	0.24	0.03	7.97	5.80	4.59	1
0.28	0.21	0.03	7.97	5.81	4.59	1
0.24	0.18	0.03	7.97	5.82	4.58	1
0.21	0.16	0.02	7.97	5.82	4.58	1
0.17	0.13	0.02	7.97	5.83	4.57	1
0.14	0.10	0.02	7.97	5.84	4.57	1
0.10	0.08	0.01	7.97	5.85	4.57	1
0.10	0.08	0.01	7.97	5.85	4.56	1
0.08	0.06	0.01	7.97	5.83	4.56	1
0.06	0.05	0.01	7.97	5.82	4.55	1
0.04	0.03	0.00	7.97	5.80	4.55	1
0.02	0.02	0.00	7.97	5.79	4.54	1
0.00	0.00	0.00	7.97	5.78	4.54	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
2.45	0.00	0.00	0.00	0.00	0.00	1
2.44	0.61	0.61	0.00	0.00	0.00	1
2.43	1.21	1.21	0.00	0.00	0.00	1
2.42	1.82	1.82	0.00	0.00	0.00	1
2.41	2.42	2.42	0.00	0.00	0.00	1
2.40	3.03	3.03	0.00	0.00	0.00	1
2.39	3.63	3.63	0.00	0.00	0.00	1
2.38	4.24	4.24	0.00	0.00	0.00	1
2.38	4.84	4.84	0.00	0.00	0.00	1
2.37	5.45	5.45	0.00	0.00	0.00	1
2.36	6.05	6.05	0.00	0.00	0.00	1
2.35	6.66	6.66	0.00	0.00	0.00	1
2.34	7.26	7.26	0.00	0.00	0.00	1
2.33	7.87	7.87	0.00	0.00	0.00	1
2.32	8.47	8.47	0.00	0.00	0.00	1
2.31	9.08	9.08	0.00	0.00	0.00	1
2.30	9.68	9.68	0.00	0.00	0.00	1
2.29	10.29	10.29	0.00	0.00	0.00	1
2.28	10.89	10.89	0.00	0.00	0.00	1
2.28	11.50	11.50	0.00	0.00	0.00	1
2.27	12.10	12.10	0.00	0.00	0.00	1
2.26	12.71	12.71	0.00	0.00	0.00	1
2.25	13.31	13.31	0.00	0.00	0.00	1
2.24	13.92	13.92	0.00	0.00	0.00	1
2.23	14.52	14.52	0.00	0.00	0.00	1
2.22	15.13	15.13	0.00	0.00	0.00	1
2.21	15.73	15.73	0.00	0.00	0.00	1
2.20	16.34	16.34	0.00	0.00	0.00	1
2.19	16.94	16.94	0.00	0.00	0.00	1
2.18	17.55	17.55	0.00	0.00	0.00	1
2.18	18.15	18.15	0.00	0.00	0.00	1
2.17	18.76	18.76	0.00	0.00	0.00	1
2.16	19.36	19.36	0.00	0.00	0.00	1
2.15	19.97	19.97	0.00	0.00	0.00	1
2.14	20.57	20.57	0.00	0.00	0.00	1
2.13	21.18	21.18	0.00	0.00	0.00	1
2.12	21.78	21.78	0.00	0.00	0.00	1
2.11	22.39	22.39	0.00	0.00	0.00	1
2.10	22.99	22.99	0.00	0.00	0.00	1
2.09	23.60	23.60	0.00	0.00	0.00	1
2.08	24.20	24.20	0.00	0.00	0.00	1
2.08	24.81	24.81	0.00	0.00	0.00	1
2.07	25.54	25.54	0.00	0.00	0.00	1
2.06	26.27	26.27	0.00	0.00	0.00	1
2.05	26.88	26.88	0.00	0.00	0.00	1
2.04	27.48	27.48	0.00	0.00	0.00	1
2.03	28.09	28.09	0.00	0.00	0.00	1
2.02	28.69	28.69	0.00	0.00	0.00	1
2.02	29.30	29.30	0.00	0.00	0.00	1
2.01	29.90	29.90	0.00	0.00	0.00	1
2.00	30.51	30.51	0.00	0.00	0.00	1

1.99	31.11	31.11	0.00	0.00	0.00	1
1.98	31.72	31.72	0.00	0.00	0.00	1
1.97	32.32	32.32	0.00	0.00	0.00	1
1.96	32.93	32.93	0.00	0.00	0.00	1
1.95	33.53	33.53	0.00	0.00	0.00	1
1.94	34.14	34.14	0.00	0.00	0.00	1
1.93	34.74	34.74	0.00	0.00	0.00	1
1.92	35.35	35.35	0.00	0.00	0.00	1
1.92	35.95	35.95	0.00	0.00	0.00	1
1.91	36.56	36.56	0.00	0.00	0.00	1
1.90	37.16	37.16	0.00	0.00	0.00	1
1.89	37.77	37.77	0.00	0.00	0.00	1
1.88	38.37	38.37	0.00	0.00	0.00	1
1.87	38.98	38.98	0.00	0.00	0.00	1
1.86	39.58	39.58	0.00	0.00	0.00	1
1.85	40.19	40.19	0.00	0.00	0.00	1
1.84	40.79	40.79	0.00	0.00	0.00	1
1.83	41.40	41.40	0.00	0.00	0.00	1
1.82	42.01	42.01	0.00	0.00	0.00	1
1.82	42.61	42.61	0.00	0.00	0.00	1
1.81	43.22	43.22	0.00	0.00	0.00	1
1.80	43.82	43.82	0.00	0.00	0.00	1
1.79	44.43	44.43	0.00	0.00	0.00	1
1.78	45.03	45.03	0.00	0.00	0.00	1
1.77	45.64	45.64	0.00	0.00	0.00	1
1.76	46.24	46.24	0.00	0.00	0.00	1
1.75	46.85	46.85	0.00	0.00	0.00	1
1.74	47.45	47.45	0.00	0.00	0.00	1
1.73	48.06	48.06	0.00	0.00	0.00	1
1.73	48.66	48.66	0.00	0.00	0.00	1
1.71	49.27	49.27	0.00	0.00	0.00	1
1.71	49.87	49.87	0.00	0.00	0.00	1
1.70	50.60	50.60	0.00	0.00	0.00	1
1.69	51.34	51.34	0.00	0.00	0.00	1
1.68	51.94	51.94	0.00	0.00	0.00	1
1.67	52.55	52.55	0.00	0.00	0.00	1
1.67	53.15	53.15	0.00	0.00	0.00	1
1.66	53.76	53.76	0.00	0.00	0.00	1
1.65	54.36	54.36	0.00	0.00	0.00	1
1.64	54.97	54.97	0.00	0.00	0.00	1
1.63	55.57	55.57	0.00	0.00	0.00	1
1.62	122.34	30.98	119.88	89.31	45.62	1
1.60	124.07	40.41	121.57	90.75	36.48	1
1.59	125.80	39.72	123.26	92.19	37.46	1
1.57	127.53	39.19	124.94	93.62	38.28	1
1.55	129.25	38.66	126.62	95.05	39.10	1
1.54	130.97	38.13	128.30	96.48	39.93	1
1.52	132.69	37.58	129.97	97.91	40.76	1
1.50	134.41	37.04	131.64	99.34	41.60	1
1.49	136.12	36.48	133.31	100.76	42.44	1
1.47	137.84	35.92	134.98	102.18	43.30	1
1.45	139.55	35.36	136.65	103.60	44.15	1
1.44	141.26	34.78	138.31	105.02	45.02	1
1.42	142.97	34.20	139.97	106.44	45.89	1

1.40	144.67	33.61	141.62	107.85	46.77	1
1.39	146.37	33.02	143.28	109.26	47.66	1
1.37	148.07	32.41	144.93	110.67	48.55	1
1.35	149.77	31.80	146.58	112.08	49.46	1
1.33	151.47	31.18	148.22	113.48	50.37	1
1.32	153.16	30.56	149.87	114.88	51.29	1
1.30	154.86	29.94	151.51	116.28	52.20	1
1.28	156.54	29.45	153.14	117.68	52.97	1
1.27	158.23	28.97	154.78	119.08	53.75	1
1.25	159.92	28.49	156.41	120.47	54.52	1
1.23	161.60	28.02	158.04	121.86	55.29	1
1.21	163.28	27.54	159.66	123.25	56.05	1
1.20	164.96	27.07	161.29	124.63	56.81	1
1.18	166.63	26.60	162.91	126.02	57.57	1
1.16	168.30	26.14	164.52	127.40	58.33	1
1.14	169.97	25.68	166.14	128.78	59.08	1
1.13	171.64	25.22	167.75	130.15	59.83	1
1.11	173.31	24.77	169.36	131.53	60.57	1
1.11	173.31	3.95	169.36	131.53	60.57	1
1.09	175.63	24.14	171.60	133.45	61.62	1
1.06	177.96	23.51	173.84	135.36	62.65	1
1.04	180.27	22.89	176.08	137.27	63.67	1
1.01	182.58	22.29	178.30	139.17	64.69	1
0.99	184.89	21.69	180.52	141.07	65.70	1
0.96	187.19	21.10	182.74	142.96	66.70	1
0.94	189.48	20.52	184.94	144.85	67.68	1
0.91	191.77	19.97	187.14	146.73	68.64	1
0.89	194.06	19.65	189.34	148.60	69.36	1
0.86	196.34	19.35	191.52	150.47	70.08	1
0.83	198.61	19.05	193.70	152.34	70.79	1
0.81	200.87	18.76	195.86	154.20	71.49	1
0.78	203.13	18.47	197.91	156.05	72.18	1
0.76	205.39	18.20	199.95	157.89	72.86	1
0.73	207.64	17.93	201.98	159.73	73.54	1
0.71	209.88	17.67	204.01	161.57	74.21	1
0.68	212.12	17.42	206.03	163.39	74.87	1
0.66	214.35	17.18	208.05	165.22	75.52	1
0.63	216.57	16.94	210.06	167.03	76.16	1
0.60	218.79	16.71	212.06	168.84	76.80	1
0.58	221.00	16.48	214.06	170.64	77.43	1
0.55	223.20	16.27	216.05	172.44	78.06	1
0.53	225.40	16.06	218.04	174.23	78.68	1
0.50	227.60	15.85	220.02	176.02	79.29	1
0.47	229.79	15.66	221.99	177.80	79.89	1
0.45	231.97	15.47	223.96	179.57	80.49	1
0.42	234.14	15.28	225.93	181.34	81.09	1
0.39	236.31	15.10	227.88	183.10	81.68	1
0.37	238.48	14.93	229.84	184.86	82.26	1
0.34	240.63	14.76	231.78	186.61	82.84	1
0.32	242.79	14.59	233.72	188.35	83.41	1
0.29	244.93	14.43	235.66	190.09	83.97	1
0.26	103.60	14.28	89.32	84.59	4.73	1
0.24	105.48	14.13	91.34	86.24	5.10	1
0.21	107.35	13.99	93.37	87.90	5.47	1

0.18	109.23	13.85	95.39	89.56	5.83	1
0.16	111.12	13.71	97.41	91.22	6.19	1
0.13	113.00	13.58	99.42	92.88	6.54	1
0.10	114.89	13.45	101.44	94.55	6.89	1
0.08	116.78	13.32	103.45	96.21	7.24	1
0.08	117.24	13.32	103.92	96.21	7.70	1
0.06	118.52	13.58	104.94	97.17	7.78	1
0.05	119.80	13.83	105.97	98.12	7.86	1
0.03	121.07	14.07	107.00	99.06	7.94	1
0.02	122.34	14.31	108.03	100.01	8.02	1
0.00	123.61	14.55	109.06	100.95	8.11	1

Time = 755. Degree of Consolidation = 35.0%

Total Settlement = 2.052

Settlement at End of Primary Consolidation = 1.877

Settlement caused by Primary Consolidation at time 755. = 0.665

Settlement caused by Secondary Compression at time 755. = 0.000

Settlement Due to Desiccation = 1.387

Surface Elevation = 1.52

*****Current Conditions in Dredged Fill*****

***** Coordinates *****

***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
4.50	2.44	0.50	7.97	2.26	2.26	1
4.47	2.43	0.50	7.97	2.26	2.26	1
4.45	2.42	0.50	7.97	2.26	2.26	1
4.42	2.41	0.49	7.97	2.26	2.26	1
4.40	2.40	0.49	7.97	2.26	2.26	1
4.37	2.39	0.49	7.97	2.26	2.26	1
4.35	2.38	0.48	7.97	2.26	2.26	1
4.32	2.37	0.48	7.97	2.26	2.26	1
4.30	2.36	0.48	7.97	2.26	2.26	1
4.27	2.36	0.48	7.97	2.26	2.26	1
4.25	2.35	0.47	7.97	2.26	2.26	1
4.22	2.34	0.47	7.97	2.26	2.26	1
4.20	2.33	0.47	7.97	2.26	2.26	1
4.17	2.32	0.47	7.97	2.26	2.26	1
4.15	2.31	0.46	7.97	2.26	2.26	1
4.12	2.30	0.46	7.97	2.26	2.26	1
4.10	2.29	0.46	7.97	2.26	2.26	1
4.07	2.28	0.45	7.97	2.26	2.26	1

4.05	2.27	0.45	7.97	2.26	2.26	1
4.02	2.26	0.45	7.97	2.26	2.26	1
4.00	2.26	0.45	7.97	2.26	2.26	1
3.97	2.25	0.44	7.97	2.26	2.26	1
3.95	2.24	0.44	7.97	2.26	2.26	1
3.92	2.23	0.44	7.97	2.26	2.26	1
3.90	2.22	0.43	7.97	2.26	2.26	1
3.87	2.21	0.43	7.97	2.26	2.26	1
3.85	2.20	0.43	7.97	2.26	2.26	1
3.82	2.19	0.43	7.97	2.26	2.26	1
3.80	2.18	0.42	7.97	2.26	2.26	1
3.77	2.17	0.42	7.97	2.26	2.26	1
3.75	2.16	0.42	7.97	2.26	2.26	1
3.72	2.16	0.42	7.97	2.26	2.26	1
3.70	2.15	0.41	7.97	2.26	2.26	1
3.67	2.14	0.41	7.97	2.26	2.26	1
3.65	2.13	0.41	7.97	2.26	2.26	1
3.62	2.12	0.40	7.97	2.26	2.26	1
3.60	2.11	0.40	7.97	2.26	2.26	1
3.57	2.10	0.40	7.97	2.26	2.26	1
3.55	2.09	0.40	7.97	2.26	2.26	1
3.52	2.08	0.39	7.97	2.26	2.26	1
3.50	2.07	0.39	7.97	5.31	2.26	1
3.50	2.07	0.39	7.97	5.31	2.26	1
3.47	2.06	0.39	7.97	2.26	5.30	1
3.45	2.05	0.38	7.97	2.26	5.29	1
3.42	2.04	0.38	7.97	2.26	5.28	1
3.40	2.03	0.38	7.97	2.26	5.27	1
3.37	2.02	0.38	7.97	2.26	5.26	1
3.35	2.01	0.37	7.97	2.26	5.25	1
3.32	2.00	0.37	7.97	2.26	5.24	1
3.30	2.00	0.37	7.97	2.26	5.23	1
3.27	1.99	0.37	7.97	2.26	5.22	1
3.25	1.98	0.36	7.97	2.26	5.22	1
3.22	1.97	0.36	7.97	2.26	5.21	1
3.20	1.96	0.36	7.97	2.26	5.20	1
3.17	1.95	0.35	7.97	2.26	5.19	1
3.15	1.94	0.35	7.97	2.26	5.18	1
3.12	1.93	0.35	7.97	2.26	5.17	1
3.10	1.92	0.35	7.97	2.26	5.16	1
3.07	1.91	0.34	7.97	2.26	5.15	1
3.05	1.90	0.34	7.97	2.26	5.14	1
3.02	1.90	0.34	7.97	2.26	5.13	1
3.00	1.89	0.33	7.97	2.26	5.12	1
2.97	1.88	0.33	7.97	2.26	5.11	1
2.95	1.87	0.33	7.97	2.26	5.11	1
2.92	1.86	0.33	7.97	2.26	5.10	1
2.90	1.85	0.32	7.97	2.26	5.09	1
2.87	1.84	0.32	7.97	2.26	5.09	1
2.85	1.83	0.32	7.97	2.26	5.08	1
2.82	1.82	0.31	7.97	2.26	5.07	1
2.80	1.81	0.31	7.97	2.26	5.06	1
2.77	1.80	0.31	7.97	2.26	5.06	1
2.75	1.80	0.31	7.97	2.26	5.05	1

2.72	1.79	0.30	7.97	2.26	5.04	1
2.70	1.78	0.30	7.97	2.26	5.03	1
2.67	1.77	0.30	7.97	2.26	5.03	1
2.65	1.76	0.30	7.97	2.26	5.02	1
2.62	1.75	0.29	7.97	2.26	5.01	1
2.60	1.74	0.29	7.97	2.26	5.00	1
2.57	1.73	0.29	7.97	2.26	5.00	1
2.55	1.72	0.28	7.97	2.26	4.99	1
2.52	1.71	0.28	7.97	2.26	4.98	1
2.50	1.70	0.28	7.97	4.75	2.26	1
2.50	1.70	0.28	7.97	4.75	2.26	1
2.47	1.69	0.28	7.97	2.26	4.97	1
2.45	1.68	0.27	7.97	2.26	4.96	1
2.42	1.67	0.27	7.97	2.26	4.95	1
2.40	1.66	0.27	7.97	2.26	4.95	1
2.37	1.65	0.26	7.97	2.26	4.94	1
2.35	1.65	0.26	7.97	2.26	4.93	1
2.32	1.64	0.26	7.97	2.26	4.92	1
2.30	1.63	0.26	7.97	2.26	4.92	1
2.27	1.62	0.25	7.97	2.26	4.91	1
2.25	1.61	0.25	7.97	2.26	2.26	1
2.22	1.59	0.25	7.97	4.86	4.86	1
2.20	1.58	0.25	7.97	4.87	4.85	1
2.17	1.56	0.24	7.97	4.88	4.85	1
2.15	1.55	0.24	7.97	4.89	4.84	1
2.12	1.53	0.24	7.97	4.91	4.84	1
2.10	1.51	0.23	7.97	4.92	4.84	1
2.07	1.50	0.23	7.97	4.93	4.83	1
2.05	1.48	0.23	7.97	4.94	4.83	1
2.02	1.46	0.23	7.97	4.96	4.82	1
2.00	1.45	0.22	7.97	4.97	4.82	1
1.97	1.43	0.22	7.97	4.98	4.81	1
1.95	1.41	0.22	7.97	5.00	4.81	1
1.92	1.40	0.21	7.97	5.01	4.81	1
1.90	1.38	0.21	7.97	5.02	4.80	1
1.87	1.36	0.21	7.97	5.04	4.80	1
1.85	1.35	0.21	7.97	5.05	4.79	1
1.82	1.33	0.20	7.97	5.07	4.79	1
1.80	1.31	0.20	7.97	5.08	4.78	1
1.77	1.30	0.20	7.97	5.10	4.78	1
1.75	1.28	0.20	7.97	5.11	4.78	1
1.72	1.26	0.19	7.97	5.13	4.77	1
1.70	1.24	0.19	7.97	5.14	4.77	1
1.67	1.23	0.19	7.97	5.16	4.76	1
1.65	1.21	0.18	7.97	5.17	4.76	1
1.62	1.19	0.18	7.97	5.19	4.76	1
1.60	1.18	0.18	7.97	5.20	4.75	1
1.57	1.16	0.18	7.97	5.22	4.75	1
1.55	1.14	0.17	7.97	5.23	4.74	1
1.52	1.12	0.17	7.97	5.25	4.74	1
1.50	1.11	0.17	7.97	5.26	4.73	1
1.50	1.11	0.17	7.97	5.26	4.73	1
1.46	1.08	0.16	7.97	5.28	4.73	1
1.43	1.06	0.16	7.97	5.30	4.72	1

1.39	1.03	0.16	7.97	5.32	4.72	1
1.36	1.01	0.15	7.97	5.34	4.71	1
1.32	0.98	0.15	7.97	5.36	4.71	1
1.29	0.96	0.14	7.97	5.38	4.70	1
1.25	0.93	0.14	7.97	5.40	4.70	1
1.22	0.91	0.14	7.97	5.42	4.70	1
1.18	0.88	0.13	7.97	5.44	4.69	1
1.15	0.86	0.13	7.97	5.46	4.69	1
1.11	0.83	0.12	7.97	5.48	4.69	1
1.08	0.81	0.12	7.97	5.49	4.68	1
1.05	0.78	0.12	7.97	5.51	4.68	1
1.01	0.76	0.11	7.97	5.53	4.67	1
0.98	0.73	0.11	7.97	5.55	4.67	1
0.94	0.71	0.10	7.97	5.56	4.67	1
0.91	0.68	0.10	7.97	5.58	4.66	1
0.87	0.65	0.10	7.97	5.59	4.66	1
0.84	0.63	0.09	7.97	5.61	4.65	1
0.80	0.60	0.09	7.97	5.62	4.65	1
0.77	0.58	0.09	7.97	5.64	4.65	1
0.73	0.55	0.08	7.97	5.65	4.64	1
0.70	0.52	0.08	7.97	5.66	4.64	1
0.66	0.50	0.07	7.97	5.68	4.63	1
0.62	0.47	0.07	7.97	5.69	4.63	1
0.59	0.45	0.07	7.97	5.70	4.62	1
0.55	0.42	0.06	7.97	5.72	4.62	1
0.52	0.39	0.06	7.97	5.73	4.62	1
0.48	0.37	0.05	7.97	5.74	4.61	1
0.45	0.34	0.05	7.97	5.75	4.61	1
0.41	0.31	0.05	7.97	5.76	4.60	1
0.38	0.29	0.04	7.97	5.77	4.60	1
0.34	0.26	0.04	7.97	5.78	4.59	1
0.31	0.24	0.03	7.97	5.79	4.59	1
0.28	0.21	0.03	7.97	5.80	4.59	1
0.24	0.18	0.03	7.97	5.81	4.58	1
0.21	0.16	0.02	7.97	5.82	4.58	1
0.17	0.13	0.02	7.97	5.83	4.57	1
0.14	0.10	0.02	7.97	5.84	4.57	1
0.10	0.08	0.01	7.97	5.85	4.56	1
0.10	0.08	0.01	7.97	5.85	4.56	1
0.08	0.06	0.01	7.97	5.83	4.56	1
0.06	0.05	0.01	7.97	5.82	4.55	1
0.04	0.03	0.00	7.97	5.80	4.55	1
0.02	0.02	0.00	7.97	5.79	4.54	1
0.00	0.00	0.00	7.97	5.78	4.54	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
2.44	0.00	0.00	0.00	0.00	0.00	1
2.43	0.61	0.61	0.00	0.00	0.00	1
2.42	1.21	1.21	0.00	0.00	0.00	1
2.41	1.82	1.82	0.00	0.00	0.00	1
2.40	2.42	2.42	0.00	0.00	0.00	1

2.39	3.03	3.03	0.00	0.00	0.00	1
2.38	3.63	3.63	0.00	0.00	0.00	1
2.37	4.24	4.24	0.00	0.00	0.00	1
2.36	4.84	4.84	0.00	0.00	0.00	1
2.36	5.45	5.45	0.00	0.00	0.00	1
2.35	6.05	6.05	0.00	0.00	0.00	1
2.34	6.66	6.66	0.00	0.00	0.00	1
2.33	7.26	7.26	0.00	0.00	0.00	1
2.32	7.87	7.87	0.00	0.00	0.00	1
2.31	8.47	8.47	0.00	0.00	0.00	1
2.30	9.08	9.08	0.00	0.00	0.00	1
2.29	9.68	9.68	0.00	0.00	0.00	1
2.28	10.29	10.29	0.00	0.00	0.00	1
2.27	10.89	10.89	0.00	0.00	0.00	1
2.26	11.50	11.50	0.00	0.00	0.00	1
2.26	12.10	12.10	0.00	0.00	0.00	1
2.25	12.71	12.71	0.00	0.00	0.00	1
2.24	13.31	13.31	0.00	0.00	0.00	1
2.23	13.92	13.92	0.00	0.00	0.00	1
2.22	14.52	14.52	0.00	0.00	0.00	1
2.21	15.13	15.13	0.00	0.00	0.00	1
2.20	15.73	15.73	0.00	0.00	0.00	1
2.19	16.34	16.34	0.00	0.00	0.00	1
2.18	16.94	16.94	0.00	0.00	0.00	1
2.17	17.55	17.55	0.00	0.00	0.00	1
2.16	18.15	18.15	0.00	0.00	0.00	1
2.16	18.76	18.76	0.00	0.00	0.00	1
2.15	19.36	19.36	0.00	0.00	0.00	1
2.14	19.97	19.97	0.00	0.00	0.00	1
2.13	20.57	20.57	0.00	0.00	0.00	1
2.12	21.18	21.18	0.00	0.00	0.00	1
2.11	21.78	21.78	0.00	0.00	0.00	1
2.10	22.39	22.39	0.00	0.00	0.00	1
2.09	22.99	22.99	0.00	0.00	0.00	1
2.08	23.60	23.60	0.00	0.00	0.00	1
2.07	24.20	24.20	0.00	0.00	0.00	1
2.07	24.81	24.81	0.00	0.00	0.00	1
2.06	25.54	25.54	0.00	0.00	0.00	1
2.05	26.27	26.27	0.00	0.00	0.00	1
2.04	26.88	26.88	0.00	0.00	0.00	1
2.03	27.48	27.48	0.00	0.00	0.00	1
2.02	28.09	28.09	0.00	0.00	0.00	1
2.01	28.69	28.69	0.00	0.00	0.00	1
2.00	29.30	29.30	0.00	0.00	0.00	1
2.00	29.90	29.90	0.00	0.00	0.00	1
1.99	30.51	30.51	0.00	0.00	0.00	1
1.98	31.11	31.11	0.00	0.00	0.00	1
1.97	31.72	31.72	0.00	0.00	0.00	1
1.96	32.32	32.32	0.00	0.00	0.00	1
1.95	32.93	32.93	0.00	0.00	0.00	1
1.94	33.53	33.53	0.00	0.00	0.00	1
1.93	34.14	34.14	0.00	0.00	0.00	1
1.92	34.74	34.74	0.00	0.00	0.00	1
1.91	35.35	35.35	0.00	0.00	0.00	1

1.90	35.95	35.95	0.00	0.00	0.00	1
1.90	36.56	36.56	0.00	0.00	0.00	1
1.89	37.16	37.16	0.00	0.00	0.00	1
1.88	37.77	37.77	0.00	0.00	0.00	1
1.87	38.37	38.37	0.00	0.00	0.00	1
1.86	38.98	38.98	0.00	0.00	0.00	1
1.85	39.58	39.58	0.00	0.00	0.00	1
1.84	40.19	40.19	0.00	0.00	0.00	1
1.83	40.79	40.79	0.00	0.00	0.00	1
1.82	41.40	41.40	0.00	0.00	0.00	1
1.81	42.01	42.01	0.00	0.00	0.00	1
1.80	42.61	42.61	0.00	0.00	0.00	1
1.80	43.22	43.22	0.00	0.00	0.00	1
1.79	43.82	43.82	0.00	0.00	0.00	1
1.78	44.43	44.43	0.00	0.00	0.00	1
1.77	45.03	45.03	0.00	0.00	0.00	1
1.76	45.64	45.64	0.00	0.00	0.00	1
1.75	46.24	46.24	0.00	0.00	0.00	1
1.74	46.85	46.85	0.00	0.00	0.00	1
1.73	47.45	47.45	0.00	0.00	0.00	1
1.72	48.06	48.06	0.00	0.00	0.00	1
1.71	48.66	48.66	0.00	0.00	0.00	1
1.70	49.27	49.27	0.00	0.00	0.00	1
1.70	49.87	49.87	0.00	0.00	0.00	1
1.69	50.60	50.60	0.00	0.00	0.00	1
1.68	51.34	51.34	0.00	0.00	0.00	1
1.67	51.94	51.94	0.00	0.00	0.00	1
1.66	52.55	52.55	0.00	0.00	0.00	1
1.65	53.15	53.15	0.00	0.00	0.00	1
1.65	53.76	53.76	0.00	0.00	0.00	1
1.64	54.36	54.36	0.00	0.00	0.00	1
1.63	54.97	54.97	0.00	0.00	0.00	1
1.62	55.57	55.57	0.00	0.00	0.00	1
1.61	56.18	56.18	0.00	0.00	0.00	1
1.59	124.07	40.41	121.57	90.75	37.07	1
1.58	125.80	40.75	123.26	92.19	37.02	1
1.56	127.53	39.94	124.94	93.62	38.12	1
1.55	129.25	39.45	126.62	95.05	38.90	1
1.53	130.97	38.95	128.30	96.48	39.69	1
1.51	132.69	38.44	129.97	97.91	40.49	1
1.50	134.41	37.94	131.64	99.34	41.29	1
1.48	136.12	37.42	133.31	100.76	42.10	1
1.46	137.84	36.90	134.98	102.18	42.91	1
1.45	139.55	36.37	136.65	103.60	43.73	1
1.43	141.26	35.84	138.31	105.02	44.55	1
1.41	142.97	35.30	139.97	106.44	45.38	1
1.40	144.67	34.76	141.62	107.85	46.22	1
1.38	146.37	34.21	143.28	109.26	47.06	1
1.36	148.07	33.65	144.93	110.67	47.91	1
1.35	149.77	33.08	146.58	112.08	48.77	1
1.33	151.47	32.51	148.22	113.48	49.63	1
1.31	153.16	31.93	149.87	114.88	50.51	1
1.30	154.86	31.34	151.51	116.28	51.39	1
1.28	156.54	30.75	153.14	117.68	52.27	1

1.26	158.23	30.14	154.78	119.08	53.17	1
1.24	159.92	29.64	156.41	120.47	53.96	1
1.23	161.60	29.18	158.04	121.86	54.71	1
1.21	163.28	28.72	159.66	123.25	55.46	1
1.19	164.96	28.27	161.29	124.63	56.21	1
1.18	166.63	27.81	162.91	126.02	56.96	1
1.16	168.30	27.36	164.52	127.40	57.70	1
1.14	169.97	26.91	166.14	128.78	58.45	1
1.12	171.64	26.46	167.75	130.15	59.19	1
1.11	173.31	26.01	169.36	131.53	59.92	1
1.11	173.31	3.95	169.36	131.53	59.92	1
1.08	175.63	25.39	171.60	133.45	60.96	1
1.06	177.96	24.77	173.84	135.36	61.98	1
1.03	180.27	24.16	176.08	137.27	63.00	1
1.01	182.58	23.55	178.30	139.17	64.02	1
0.98	184.89	22.95	180.52	141.07	65.03	1
0.96	187.19	22.36	182.74	142.96	66.03	1
0.93	189.48	21.77	184.94	144.85	67.03	1
0.91	191.77	21.19	187.14	146.73	68.01	1
0.88	194.06	20.62	189.34	148.60	68.99	1
0.86	196.34	20.05	191.52	150.47	69.97	1
0.83	198.61	19.71	193.70	152.34	70.71	1
0.81	200.87	19.41	195.86	154.20	71.43	1
0.78	203.13	19.10	197.91	156.05	72.14	1
0.76	205.39	18.81	199.95	157.89	72.84	1
0.73	207.64	18.52	201.98	159.73	73.54	1
0.71	209.88	18.24	204.01	161.57	74.23	1
0.68	212.12	17.97	206.03	163.39	74.91	1
0.65	214.35	17.70	208.05	165.22	75.58	1
0.63	216.57	17.44	210.06	167.03	76.25	1
0.60	218.79	17.19	212.06	168.84	76.91	1
0.58	221.00	16.94	214.06	170.64	77.57	1
0.55	223.20	16.70	216.05	172.44	78.22	1
0.52	225.40	16.47	218.04	174.23	78.86	1
0.50	227.60	16.24	220.02	176.02	79.50	1
0.47	229.79	16.02	221.99	177.80	80.13	1
0.45	231.97	15.80	223.96	179.57	80.75	1
0.42	234.14	15.59	225.93	181.34	81.37	1
0.39	236.31	15.38	227.88	183.10	81.99	1
0.37	238.48	15.18	229.84	184.86	82.59	1
0.34	240.63	14.99	231.78	186.61	83.20	1
0.31	242.79	14.80	233.72	188.35	83.79	1
0.29	101.07	14.62	86.46	81.52	4.93	1
0.26	102.95	14.44	88.51	83.17	5.34	1
0.24	104.82	14.27	90.55	84.82	5.73	1
0.21	106.70	14.10	92.60	86.48	6.12	1
0.18	108.58	13.93	94.64	88.14	6.51	1
0.16	110.46	13.77	96.68	89.80	6.89	1
0.13	112.34	13.62	98.72	91.46	7.26	1
0.10	114.23	13.47	100.76	93.12	7.64	1
0.08	116.12	13.32	102.79	94.79	8.00	1
0.08	116.58	13.32	103.26	94.79	8.47	1
0.06	117.86	13.58	104.28	95.74	8.54	1
0.05	119.14	13.83	105.31	96.69	8.62	1

0.03	120.41	14.07	106.34	97.64	8.70	1
0.02	121.68	14.31	107.37	98.58	8.79	1
0.00	122.95	14.55	108.40	99.53	8.88	1

Time = 1120. Degree of Consolidation = 34.0%

Total Settlement = 2.063

Settlement at End of Primary Consolidation = 1.872

Settlement caused by Primary Consolidation at time 1120. = 0.638

Settlement caused by Secondary Compression at time 1120. = 0.000

Settlement Due to Desiccation = 1.425

Surface Elevation = 1.51

*****Current Conditions in Dredged Fill*****

***** Coordinates *****

***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
4.50	2.44	0.50	7.97	2.26	2.26	1
4.47	2.43	0.50	7.97	2.26	2.26	1
4.45	2.42	0.50	7.97	2.26	2.26	1
4.42	2.41	0.49	7.97	2.26	2.26	1
4.40	2.40	0.49	7.97	2.26	2.26	1
4.37	2.39	0.49	7.97	2.26	2.26	1
4.35	2.38	0.48	7.97	2.26	2.26	1
4.32	2.37	0.48	7.97	2.26	2.26	1
4.30	2.36	0.48	7.97	2.26	2.26	1
4.27	2.35	0.48	7.97	2.26	2.26	1
4.25	2.35	0.47	7.97	2.26	2.26	1
4.22	2.34	0.47	7.97	2.26	2.26	1
4.20	2.33	0.47	7.97	2.26	2.26	1
4.17	2.32	0.47	7.97	2.26	2.26	1
4.15	2.31	0.46	7.97	2.26	2.26	1
4.12	2.30	0.46	7.97	2.26	2.26	1
4.10	2.29	0.46	7.97	2.26	2.26	1
4.07	2.28	0.45	7.97	2.26	2.26	1
4.05	2.27	0.45	7.97	2.26	2.26	1
4.02	2.26	0.45	7.97	2.26	2.26	1
4.00	2.25	0.45	7.97	2.26	2.26	1
3.97	2.25	0.44	7.97	2.26	2.26	1
3.95	2.24	0.44	7.97	2.26	2.26	1
3.92	2.23	0.44	7.97	2.26	2.26	1
3.90	2.22	0.43	7.97	2.26	2.26	1
3.87	2.21	0.43	7.97	2.26	2.26	1

3.85	2.20	0.43	7.97	2.26	2.26	1
3.82	2.19	0.43	7.97	2.26	2.26	1
3.80	2.18	0.42	7.97	2.26	2.26	1
3.77	2.17	0.42	7.97	2.26	2.26	1
3.75	2.16	0.42	7.97	2.26	2.26	1
3.72	2.15	0.42	7.97	2.26	2.26	1
3.70	2.15	0.41	7.97	2.26	2.26	1
3.67	2.14	0.41	7.97	2.26	2.26	1
3.65	2.13	0.41	7.97	2.26	2.26	1
3.62	2.12	0.40	7.97	2.26	2.26	1
3.60	2.11	0.40	7.97	2.26	2.26	1
3.57	2.10	0.40	7.97	2.26	2.26	1
3.55	2.09	0.40	7.97	2.26	2.26	1
3.52	2.08	0.39	7.97	2.26	2.26	1
3.50	2.07	0.39	7.97	5.31	2.26	1
3.50	2.07	0.39	7.97	5.31	2.26	1
3.47	2.06	0.39	7.97	2.26	5.30	1
3.45	2.05	0.38	7.97	2.26	5.29	1
3.42	2.04	0.38	7.97	2.26	5.28	1
3.40	2.03	0.38	7.97	2.26	5.27	1
3.37	2.02	0.38	7.97	2.26	5.26	1
3.35	2.01	0.37	7.97	2.26	5.25	1
3.32	2.00	0.37	7.97	2.26	5.24	1
3.30	1.99	0.37	7.97	2.26	5.23	1
3.27	1.99	0.37	7.97	2.26	5.22	1
3.25	1.98	0.36	7.97	2.26	5.22	1
3.22	1.97	0.36	7.97	2.26	5.21	1
3.20	1.96	0.36	7.97	2.26	5.20	1
3.17	1.95	0.35	7.97	2.26	5.19	1
3.15	1.94	0.35	7.97	2.26	5.18	1
3.12	1.93	0.35	7.97	2.26	5.17	1
3.10	1.92	0.35	7.97	2.26	5.16	1
3.07	1.91	0.34	7.97	2.26	5.15	1
3.05	1.90	0.34	7.97	2.26	5.14	1
3.02	1.89	0.34	7.97	2.26	5.13	1
3.00	1.89	0.33	7.97	2.26	5.12	1
2.97	1.88	0.33	7.97	2.26	5.11	1
2.95	1.87	0.33	7.97	2.26	5.11	1
2.92	1.86	0.33	7.97	2.26	5.10	1
2.90	1.85	0.32	7.97	2.26	5.09	1
2.87	1.84	0.32	7.97	2.26	5.09	1
2.85	1.83	0.32	7.97	2.26	5.08	1
2.82	1.82	0.31	7.97	2.26	5.07	1
2.80	1.81	0.31	7.97	2.26	5.06	1
2.77	1.80	0.31	7.97	2.26	5.06	1
2.75	1.79	0.31	7.97	2.26	5.05	1
2.72	1.79	0.30	7.97	2.26	5.04	1
2.70	1.78	0.30	7.97	2.26	5.03	1
2.67	1.77	0.30	7.97	2.26	5.03	1
2.65	1.76	0.30	7.97	2.26	5.02	1
2.62	1.75	0.29	7.97	2.26	5.01	1
2.60	1.74	0.29	7.97	2.26	5.00	1
2.57	1.73	0.29	7.97	2.26	5.00	1
2.55	1.72	0.28	7.97	2.26	4.99	1

2.52	1.71	0.28	7.97	2.26	4.98	1
2.50	1.70	0.28	7.97	4.75	2.26	1
2.50	1.70	0.28	7.97	4.75	2.26	1
2.47	1.69	0.28	7.97	2.26	4.97	1
2.45	1.68	0.27	7.97	2.26	4.96	1
2.42	1.67	0.27	7.97	2.26	4.95	1
2.40	1.66	0.27	7.97	2.26	4.95	1
2.37	1.65	0.26	7.97	2.26	4.94	1
2.35	1.64	0.26	7.97	2.26	4.93	1
2.32	1.64	0.26	7.97	2.26	4.92	1
2.30	1.63	0.26	7.97	2.26	4.92	1
2.27	1.62	0.25	7.97	2.26	4.91	1
2.25	1.61	0.25	7.97	2.26	2.26	1
2.22	1.59	0.25	7.97	4.86	4.86	1
2.20	1.58	0.25	7.97	4.87	4.85	1
2.17	1.56	0.24	7.97	4.88	4.85	1
2.15	1.55	0.24	7.97	4.89	4.84	1
2.12	1.53	0.24	7.97	4.91	4.84	1
2.10	1.51	0.23	7.97	4.92	4.84	1
2.07	1.50	0.23	7.97	4.93	4.83	1
2.05	1.48	0.23	7.97	4.94	4.83	1
2.02	1.46	0.23	7.97	4.96	4.82	1
2.00	1.45	0.22	7.97	4.97	4.82	1
1.97	1.43	0.22	7.97	4.98	4.81	1
1.95	1.41	0.22	7.97	5.00	4.81	1
1.92	1.40	0.21	7.97	5.01	4.81	1
1.90	1.38	0.21	7.97	5.02	4.80	1
1.87	1.36	0.21	7.97	5.04	4.80	1
1.85	1.35	0.21	7.97	5.05	4.79	1
1.82	1.33	0.20	7.97	5.07	4.79	1
1.80	1.31	0.20	7.97	5.08	4.78	1
1.77	1.30	0.20	7.97	5.10	4.78	1
1.75	1.28	0.20	7.97	5.11	4.78	1
1.72	1.26	0.19	7.97	5.12	4.77	1
1.70	1.24	0.19	7.97	5.14	4.77	1
1.67	1.23	0.19	7.97	5.16	4.76	1
1.65	1.21	0.18	7.97	5.17	4.76	1
1.62	1.19	0.18	7.97	5.19	4.76	1
1.60	1.18	0.18	7.97	5.20	4.75	1
1.57	1.16	0.18	7.97	5.22	4.75	1
1.55	1.14	0.17	7.97	5.23	4.74	1
1.52	1.12	0.17	7.97	5.24	4.74	1
1.50	1.11	0.17	7.97	5.26	4.73	1
1.50	1.11	0.17	7.97	5.26	4.73	1
1.46	1.08	0.16	7.97	5.28	4.73	1
1.43	1.06	0.16	7.97	5.30	4.72	1
1.39	1.03	0.16	7.97	5.32	4.72	1
1.36	1.01	0.15	7.97	5.34	4.71	1
1.32	0.98	0.15	7.97	5.36	4.71	1
1.29	0.96	0.14	7.97	5.38	4.70	1
1.25	0.93	0.14	7.97	5.40	4.70	1
1.22	0.91	0.14	7.97	5.42	4.70	1
1.18	0.88	0.13	7.97	5.44	4.69	1
1.15	0.86	0.13	7.97	5.46	4.69	1

1.11	0.83	0.12	7.97	5.47	4.69	1
1.08	0.81	0.12	7.97	5.49	4.68	1
1.05	0.78	0.12	7.97	5.51	4.68	1
1.01	0.76	0.11	7.97	5.53	4.67	1
0.98	0.73	0.11	7.97	5.54	4.67	1
0.94	0.71	0.10	7.97	5.56	4.67	1
0.91	0.68	0.10	7.97	5.58	4.66	1
0.87	0.65	0.10	7.97	5.59	4.66	1
0.84	0.63	0.09	7.97	5.61	4.65	1
0.80	0.60	0.09	7.97	5.62	4.65	1
0.77	0.58	0.09	7.97	5.64	4.65	1
0.73	0.55	0.08	7.97	5.65	4.64	1
0.70	0.52	0.08	7.97	5.66	4.64	1
0.66	0.50	0.07	7.97	5.68	4.63	1
0.62	0.47	0.07	7.97	5.69	4.63	1
0.59	0.45	0.07	7.97	5.70	4.62	1
0.55	0.42	0.06	7.97	5.71	4.62	1
0.52	0.39	0.06	7.97	5.73	4.62	1
0.48	0.37	0.05	7.97	5.74	4.61	1
0.45	0.34	0.05	7.97	5.75	4.61	1
0.41	0.31	0.05	7.97	5.76	4.60	1
0.38	0.29	0.04	7.97	5.77	4.60	1
0.34	0.26	0.04	7.97	5.78	4.59	1
0.31	0.24	0.03	7.97	5.79	4.59	1
0.28	0.21	0.03	7.97	5.80	4.59	1
0.24	0.18	0.03	7.97	5.81	4.58	1
0.21	0.16	0.02	7.97	5.82	4.58	1
0.17	0.13	0.02	7.97	5.83	4.57	1
0.14	0.10	0.02	7.97	5.84	4.57	1
0.10	0.08	0.01	7.97	5.85	4.56	1
0.10	0.08	0.01	7.97	5.85	4.56	1
0.08	0.06	0.01	7.97	5.83	4.56	1
0.06	0.05	0.01	7.97	5.82	4.55	1
0.04	0.03	0.00	7.97	5.80	4.55	1
0.02	0.02	0.00	7.97	5.79	4.54	1
0.00	0.00	0.00	7.97	5.78	4.54	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
2.44	0.00	0.00	0.00	0.00	0.00	1
2.43	0.61	0.61	0.00	0.00	0.00	1
2.42	1.21	1.21	0.00	0.00	0.00	1
2.41	1.82	1.82	0.00	0.00	0.00	1
2.40	2.42	2.42	0.00	0.00	0.00	1
2.39	3.03	3.03	0.00	0.00	0.00	1
2.38	3.63	3.63	0.00	0.00	0.00	1
2.37	4.24	4.24	0.00	0.00	0.00	1
2.36	4.84	4.84	0.00	0.00	0.00	1
2.35	5.45	5.45	0.00	0.00	0.00	1
2.35	6.05	6.05	0.00	0.00	0.00	1
2.34	6.66	6.66	0.00	0.00	0.00	1
2.33	7.26	7.26	0.00	0.00	0.00	1

2.32	7.87	7.87	0.00	0.00	0.00	1
2.31	8.47	8.47	0.00	0.00	0.00	1
2.30	9.08	9.08	0.00	0.00	0.00	1
2.29	9.68	9.68	0.00	0.00	0.00	1
2.28	10.29	10.29	0.00	0.00	0.00	1
2.27	10.89	10.89	0.00	0.00	0.00	1
2.26	11.50	11.50	0.00	0.00	0.00	1
2.25	12.10	12.10	0.00	0.00	0.00	1
2.25	12.71	12.71	0.00	0.00	0.00	1
2.24	13.31	13.31	0.00	0.00	0.00	1
2.23	13.92	13.92	0.00	0.00	0.00	1
2.22	14.52	14.52	0.00	0.00	0.00	1
2.21	15.13	15.13	0.00	0.00	0.00	1
2.20	15.73	15.73	0.00	0.00	0.00	1
2.19	16.34	16.34	0.00	0.00	0.00	1
2.18	16.94	16.94	0.00	0.00	0.00	1
2.17	17.55	17.55	0.00	0.00	0.00	1
2.16	18.15	18.15	0.00	0.00	0.00	1
2.15	18.76	18.76	0.00	0.00	0.00	1
2.15	19.36	19.36	0.00	0.00	0.00	1
2.14	19.97	19.97	0.00	0.00	0.00	1
2.13	20.57	20.57	0.00	0.00	0.00	1
2.12	21.18	21.18	0.00	0.00	0.00	1
2.11	21.78	21.78	0.00	0.00	0.00	1
2.10	22.39	22.39	0.00	0.00	0.00	1
2.09	22.99	22.99	0.00	0.00	0.00	1
2.08	23.60	23.60	0.00	0.00	0.00	1
2.07	24.20	24.20	0.00	0.00	0.00	1
2.07	24.81	24.81	0.00	0.00	0.00	1
2.06	25.54	25.54	0.00	0.00	0.00	1
2.05	26.27	26.27	0.00	0.00	0.00	1
2.04	26.88	26.88	0.00	0.00	0.00	1
2.03	27.48	27.48	0.00	0.00	0.00	1
2.02	28.09	28.09	0.00	0.00	0.00	1
2.01	28.69	28.69	0.00	0.00	0.00	1
2.00	29.30	29.30	0.00	0.00	0.00	1
1.99	29.90	29.90	0.00	0.00	0.00	1
1.99	30.51	30.51	0.00	0.00	0.00	1
1.98	31.11	31.11	0.00	0.00	0.00	1
1.97	31.72	31.72	0.00	0.00	0.00	1
1.96	32.32	32.32	0.00	0.00	0.00	1
1.95	32.93	32.93	0.00	0.00	0.00	1
1.94	33.53	33.53	0.00	0.00	0.00	1
1.93	34.14	34.14	0.00	0.00	0.00	1
1.92	34.74	34.74	0.00	0.00	0.00	1
1.91	35.35	35.35	0.00	0.00	0.00	1
1.90	35.95	35.95	0.00	0.00	0.00	1
1.89	36.56	36.56	0.00	0.00	0.00	1
1.89	37.16	37.16	0.00	0.00	0.00	1
1.88	37.77	37.77	0.00	0.00	0.00	1
1.87	38.37	38.37	0.00	0.00	0.00	1
1.86	38.98	38.98	0.00	0.00	0.00	1
1.85	39.58	39.58	0.00	0.00	0.00	1
1.84	40.19	40.19	0.00	0.00	0.00	1

1.83	40.79	40.79	0.00	0.00	0.00	1
1.82	41.40	41.40	0.00	0.00	0.00	1
1.81	42.01	42.01	0.00	0.00	0.00	1
1.80	42.61	42.61	0.00	0.00	0.00	1
1.79	43.22	43.22	0.00	0.00	0.00	1
1.79	43.82	43.82	0.00	0.00	0.00	1
1.78	44.43	44.43	0.00	0.00	0.00	1
1.77	45.03	45.03	0.00	0.00	0.00	1
1.76	45.64	45.64	0.00	0.00	0.00	1
1.75	46.24	46.24	0.00	0.00	0.00	1
1.74	46.85	46.85	0.00	0.00	0.00	1
1.73	47.45	47.45	0.00	0.00	0.00	1
1.72	48.06	48.06	0.00	0.00	0.00	1
1.71	48.66	48.66	0.00	0.00	0.00	1
1.70	49.27	49.27	0.00	0.00	0.00	1
1.70	49.87	49.87	0.00	0.00	0.00	1
1.69	50.60	50.60	0.00	0.00	0.00	1
1.68	51.34	51.34	0.00	0.00	0.00	1
1.67	51.94	51.94	0.00	0.00	0.00	1
1.66	52.55	52.55	0.00	0.00	0.00	1
1.65	53.15	53.15	0.00	0.00	0.00	1
1.64	53.76	53.76	0.00	0.00	0.00	1
1.64	54.36	54.36	0.00	0.00	0.00	1
1.63	54.97	54.97	0.00	0.00	0.00	1
1.62	55.57	55.57	0.00	0.00	0.00	1
1.61	56.18	56.18	0.00	0.00	0.00	1
1.59	124.07	40.41	121.57	90.75	37.07	1
1.58	125.80	40.76	123.26	92.19	37.01	1
1.56	127.53	39.95	124.94	93.62	38.11	1
1.55	129.25	39.46	126.62	95.05	38.90	1
1.53	130.97	38.96	128.30	96.48	39.68	1
1.51	132.69	38.46	129.97	97.91	40.48	1
1.50	134.41	37.95	131.64	99.34	41.28	1
1.48	136.12	37.44	133.31	100.76	42.08	1
1.46	137.84	36.92	134.98	102.18	42.89	1
1.45	139.55	36.40	136.65	103.60	43.71	1
1.43	141.26	35.87	138.31	105.02	44.53	1
1.41	142.97	35.33	139.97	106.44	45.35	1
1.40	144.67	34.79	141.62	107.85	46.19	1
1.38	146.37	34.24	143.28	109.26	47.03	1
1.36	148.07	33.69	144.93	110.67	47.87	1
1.35	149.77	33.12	146.58	112.08	48.73	1
1.33	151.47	32.56	148.22	113.48	49.59	1
1.31	153.16	31.98	149.87	114.88	50.46	1
1.30	154.86	31.39	151.51	116.28	51.33	1
1.28	156.54	30.80	153.14	117.68	52.22	1
1.26	158.23	30.20	154.78	119.08	53.11	1
1.24	159.92	29.69	156.41	120.47	53.91	1
1.23	161.60	29.23	158.04	121.86	54.66	1
1.21	163.28	28.78	159.66	123.25	55.41	1
1.19	164.96	28.32	161.29	124.63	56.16	1
1.18	166.63	27.87	162.91	126.02	56.90	1
1.16	168.30	27.41	164.52	127.40	57.65	1
1.14	169.97	26.96	166.14	128.78	58.39	1

1.12	171.64	26.52	167.75	130.15	59.13	1
1.11	173.31	26.07	169.36	131.53	59.86	1
1.11	173.31	3.95	169.36	131.53	59.86	1
1.08	175.63	25.45	171.60	133.45	60.89	1
1.06	177.96	24.83	173.84	135.36	61.92	1
1.03	180.27	24.22	176.08	137.27	62.94	1
1.01	182.58	23.62	178.30	139.17	63.95	1
0.98	184.89	23.02	180.52	141.07	64.96	1
0.96	187.19	22.42	182.74	142.96	65.96	1
0.93	189.48	21.84	184.94	144.85	66.96	1
0.91	191.77	21.26	187.14	146.73	67.94	1
0.88	194.06	20.69	189.34	148.60	68.92	1
0.86	196.34	20.12	191.52	150.47	69.90	1
0.83	198.61	19.75	193.70	152.34	70.67	1
0.81	200.87	19.44	195.86	154.20	71.39	1
0.78	203.13	19.14	197.91	156.05	72.10	1
0.76	205.39	18.85	199.95	157.89	72.80	1
0.73	207.64	18.56	201.98	159.73	73.50	1
0.71	209.88	18.28	204.01	161.57	74.19	1
0.68	212.12	18.00	206.03	163.39	74.87	1
0.65	214.35	17.73	208.05	165.22	75.55	1
0.63	216.57	17.47	210.06	167.03	76.22	1
0.60	218.79	17.22	212.06	168.84	76.88	1
0.58	221.00	16.97	214.06	170.64	77.54	1
0.55	223.20	16.73	216.05	172.44	78.19	1
0.52	225.40	16.49	218.04	174.23	78.83	1
0.50	227.60	16.26	220.02	176.02	79.47	1
0.47	229.79	16.04	221.99	177.80	80.11	1
0.45	231.97	15.82	223.96	179.57	80.73	1
0.42	234.14	15.61	225.93	181.34	81.35	1
0.39	236.31	15.40	227.88	183.10	81.97	1
0.37	238.48	15.20	229.84	184.86	82.58	1
0.34	240.63	15.00	231.78	186.61	83.18	1
0.31	99.65	14.81	84.84	79.86	4.98	1
0.29	101.52	14.63	86.89	81.50	5.39	1
0.26	103.39	14.45	88.94	83.15	5.79	1
0.24	105.27	14.27	90.99	84.81	6.19	1
0.21	107.14	14.10	93.04	86.46	6.58	1
0.18	109.02	13.94	95.08	88.12	6.97	1
0.16	110.90	13.78	97.13	89.78	7.35	1
0.13	112.79	13.62	99.17	91.44	7.73	1
0.10	114.67	13.47	101.20	93.10	8.10	1
0.08	116.56	13.32	103.24	94.77	8.47	1
0.08	117.03	13.32	103.70	94.77	8.93	1
0.06	118.31	13.58	104.73	95.72	9.01	1
0.05	119.58	13.83	105.76	96.67	9.09	1
0.03	120.86	14.07	106.79	97.62	9.17	1
0.02	122.13	14.31	107.82	98.56	9.25	1
0.00	123.40	14.55	108.85	99.51	9.34	1

Time = 2215. Degree of Consolidation = 34.0%

Total Settlement = 2.063

Settlement at End of Primary Consolidation = 1.872

Settlement caused by Primary Consolidation at time 2215. = 0.638

Settlement caused by Secondary Compression at time 2215. = 0.000

Settlement Due to Desiccation = 1.425

Surface Elevation = 1.51

*****Current Conditions in Dredged Fill*****

***** Coordinates *****

***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
4.50	2.44	0.50	7.97	2.26	2.26	1
4.47	2.43	0.50	7.97	2.26	2.26	1
4.45	2.42	0.50	7.97	2.26	2.26	1
4.42	2.41	0.49	7.97	2.26	2.26	1
4.40	2.40	0.49	7.97	2.26	2.26	1
4.37	2.39	0.49	7.97	2.26	2.26	1
4.35	2.38	0.48	7.97	2.26	2.26	1
4.32	2.37	0.48	7.97	2.26	2.26	1
4.30	2.36	0.48	7.97	2.26	2.26	1
4.27	2.35	0.48	7.97	2.26	2.26	1
4.25	2.35	0.47	7.97	2.26	2.26	1
4.22	2.34	0.47	7.97	2.26	2.26	1
4.20	2.33	0.47	7.97	2.26	2.26	1
4.17	2.32	0.47	7.97	2.26	2.26	1
4.15	2.31	0.46	7.97	2.26	2.26	1
4.12	2.30	0.46	7.97	2.26	2.26	1
4.10	2.29	0.46	7.97	2.26	2.26	1
4.07	2.28	0.45	7.97	2.26	2.26	1
4.05	2.27	0.45	7.97	2.26	2.26	1
4.02	2.26	0.45	7.97	2.26	2.26	1
4.00	2.25	0.45	7.97	2.26	2.26	1
3.97	2.25	0.44	7.97	2.26	2.26	1
3.95	2.24	0.44	7.97	2.26	2.26	1
3.92	2.23	0.44	7.97	2.26	2.26	1
3.90	2.22	0.43	7.97	2.26	2.26	1
3.87	2.21	0.43	7.97	2.26	2.26	1
3.85	2.20	0.43	7.97	2.26	2.26	1
3.82	2.19	0.43	7.97	2.26	2.26	1
3.80	2.18	0.42	7.97	2.26	2.26	1
3.77	2.17	0.42	7.97	2.26	2.26	1
3.75	2.16	0.42	7.97	2.26	2.26	1
3.72	2.15	0.42	7.97	2.26	2.26	1
3.70	2.15	0.41	7.97	2.26	2.26	1
3.67	2.14	0.41	7.97	2.26	2.26	1

3.65	2.13	0.41	7.97	2.26	2.26	1
3.62	2.12	0.40	7.97	2.26	2.26	1
3.60	2.11	0.40	7.97	2.26	2.26	1
3.57	2.10	0.40	7.97	2.26	2.26	1
3.55	2.09	0.40	7.97	2.26	2.26	1
3.52	2.08	0.39	7.97	2.26	2.26	1
3.50	2.07	0.39	7.97	5.31	2.26	1
3.50	2.07	0.39	7.97	5.31	2.26	1
3.47	2.06	0.39	7.97	2.26	5.30	1
3.45	2.05	0.38	7.97	2.26	5.29	1
3.42	2.04	0.38	7.97	2.26	5.28	1
3.40	2.03	0.38	7.97	2.26	5.27	1
3.37	2.02	0.38	7.97	2.26	5.26	1
3.35	2.01	0.37	7.97	2.26	5.25	1
3.32	2.00	0.37	7.97	2.26	5.24	1
3.30	1.99	0.37	7.97	2.26	5.23	1
3.27	1.99	0.37	7.97	2.26	5.22	1
3.25	1.98	0.36	7.97	2.26	5.22	1
3.22	1.97	0.36	7.97	2.26	5.21	1
3.20	1.96	0.36	7.97	2.26	5.20	1
3.17	1.95	0.35	7.97	2.26	5.19	1
3.15	1.94	0.35	7.97	2.26	5.18	1
3.12	1.93	0.35	7.97	2.26	5.17	1
3.10	1.92	0.35	7.97	2.26	5.16	1
3.07	1.91	0.34	7.97	2.26	5.15	1
3.05	1.90	0.34	7.97	2.26	5.14	1
3.02	1.89	0.34	7.97	2.26	5.13	1
3.00	1.89	0.33	7.97	2.26	5.12	1
2.97	1.88	0.33	7.97	2.26	5.11	1
2.95	1.87	0.33	7.97	2.26	5.11	1
2.92	1.86	0.33	7.97	2.26	5.10	1
2.90	1.85	0.32	7.97	2.26	5.09	1
2.87	1.84	0.32	7.97	2.26	5.09	1
2.85	1.83	0.32	7.97	2.26	5.08	1
2.82	1.82	0.31	7.97	2.26	5.07	1
2.80	1.81	0.31	7.97	2.26	5.06	1
2.77	1.80	0.31	7.97	2.26	5.06	1
2.75	1.79	0.31	7.97	2.26	5.05	1
2.72	1.79	0.30	7.97	2.26	5.04	1
2.70	1.78	0.30	7.97	2.26	5.03	1
2.67	1.77	0.30	7.97	2.26	5.03	1
2.65	1.76	0.30	7.97	2.26	5.02	1
2.62	1.75	0.29	7.97	2.26	5.01	1
2.60	1.74	0.29	7.97	2.26	5.00	1
2.57	1.73	0.29	7.97	2.26	5.00	1
2.55	1.72	0.28	7.97	2.26	4.99	1
2.52	1.71	0.28	7.97	2.26	4.98	1
2.50	1.70	0.28	7.97	4.75	2.26	1
2.50	1.70	0.28	7.97	4.75	2.26	1
2.47	1.69	0.28	7.97	2.26	4.97	1
2.45	1.68	0.27	7.97	2.26	4.96	1
2.42	1.67	0.27	7.97	2.26	4.95	1
2.40	1.66	0.27	7.97	2.26	4.95	1
2.37	1.65	0.26	7.97	2.26	4.94	1

2.35	1.64	0.26	7.97	2.26	4.93	1
2.32	1.64	0.26	7.97	2.26	4.92	1
2.30	1.63	0.26	7.97	2.26	4.92	1
2.27	1.62	0.25	7.97	2.26	4.91	1
2.25	1.61	0.25	7.97	2.26	2.26	1
2.22	1.59	0.25	7.97	4.86	4.86	1
2.20	1.58	0.25	7.97	4.87	4.85	1
2.17	1.56	0.24	7.97	4.88	4.85	1
2.15	1.55	0.24	7.97	4.89	4.84	1
2.12	1.53	0.24	7.97	4.91	4.84	1
2.10	1.51	0.23	7.97	4.92	4.84	1
2.07	1.50	0.23	7.97	4.93	4.83	1
2.05	1.48	0.23	7.97	4.94	4.83	1
2.02	1.46	0.23	7.97	4.96	4.82	1
2.00	1.45	0.22	7.97	4.97	4.82	1
1.97	1.43	0.22	7.97	4.98	4.81	1
1.95	1.41	0.22	7.97	5.00	4.81	1
1.92	1.40	0.21	7.97	5.01	4.81	1
1.90	1.38	0.21	7.97	5.02	4.80	1
1.87	1.36	0.21	7.97	5.04	4.80	1
1.85	1.35	0.21	7.97	5.05	4.79	1
1.82	1.33	0.20	7.97	5.07	4.79	1
1.80	1.31	0.20	7.97	5.08	4.78	1
1.77	1.30	0.20	7.97	5.10	4.78	1
1.75	1.28	0.20	7.97	5.11	4.78	1
1.72	1.26	0.19	7.97	5.12	4.77	1
1.70	1.24	0.19	7.97	5.14	4.77	1
1.67	1.23	0.19	7.97	5.16	4.76	1
1.65	1.21	0.18	7.97	5.17	4.76	1
1.62	1.19	0.18	7.97	5.19	4.76	1
1.60	1.18	0.18	7.97	5.20	4.75	1
1.57	1.16	0.18	7.97	5.22	4.75	1
1.55	1.14	0.17	7.97	5.23	4.74	1
1.52	1.12	0.17	7.97	5.24	4.74	1
1.50	1.11	0.17	7.97	5.26	4.73	1
1.50	1.11	0.17	7.97	5.26	4.73	1
1.46	1.08	0.16	7.97	5.28	4.73	1
1.43	1.06	0.16	7.97	5.30	4.72	1
1.39	1.03	0.16	7.97	5.32	4.72	1
1.36	1.01	0.15	7.97	5.34	4.71	1
1.32	0.98	0.15	7.97	5.36	4.71	1
1.29	0.96	0.14	7.97	5.38	4.70	1
1.25	0.93	0.14	7.97	5.40	4.70	1
1.22	0.91	0.14	7.97	5.42	4.70	1
1.18	0.88	0.13	7.97	5.44	4.69	1
1.15	0.86	0.13	7.97	5.46	4.69	1
1.11	0.83	0.12	7.97	5.47	4.69	1
1.08	0.81	0.12	7.97	5.49	4.68	1
1.05	0.78	0.12	7.97	5.51	4.68	1
1.01	0.76	0.11	7.97	5.53	4.67	1
0.98	0.73	0.11	7.97	5.54	4.67	1
0.94	0.71	0.10	7.97	5.56	4.67	1
0.91	0.68	0.10	7.97	5.58	4.66	1
0.87	0.65	0.10	7.97	5.59	4.66	1

0.84	0.63	0.09	7.97	5.61	4.65	1
0.80	0.60	0.09	7.97	5.62	4.65	1
0.77	0.58	0.09	7.97	5.64	4.65	1
0.73	0.55	0.08	7.97	5.65	4.64	1
0.70	0.52	0.08	7.97	5.66	4.64	1
0.66	0.50	0.07	7.97	5.68	4.63	1
0.62	0.47	0.07	7.97	5.69	4.63	1
0.59	0.45	0.07	7.97	5.70	4.62	1
0.55	0.42	0.06	7.97	5.71	4.62	1
0.52	0.39	0.06	7.97	5.73	4.62	1
0.48	0.37	0.05	7.97	5.74	4.61	1
0.45	0.34	0.05	7.97	5.75	4.61	1
0.41	0.31	0.05	7.97	5.76	4.60	1
0.38	0.29	0.04	7.97	5.77	4.60	1
0.34	0.26	0.04	7.97	5.78	4.59	1
0.31	0.24	0.03	7.97	5.79	4.59	1
0.28	0.21	0.03	7.97	5.80	4.59	1
0.24	0.18	0.03	7.97	5.81	4.58	1
0.21	0.16	0.02	7.97	5.82	4.58	1
0.17	0.13	0.02	7.97	5.83	4.57	1
0.14	0.10	0.02	7.97	5.84	4.57	1
0.10	0.08	0.01	7.97	5.85	4.56	1
0.10	0.08	0.01	7.97	5.85	4.56	1
0.08	0.06	0.01	7.97	5.83	4.56	1
0.06	0.05	0.01	7.97	5.82	4.55	1
0.04	0.03	0.00	7.97	5.80	4.55	1
0.02	0.02	0.00	7.97	5.79	4.54	1
0.00	0.00	0.00	7.97	5.78	4.54	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
2.44	0.00	0.00	0.00	0.00	0.00	1
2.43	0.61	0.61	0.00	0.00	0.00	1
2.42	1.21	1.21	0.00	0.00	0.00	1
2.41	1.82	1.82	0.00	0.00	0.00	1
2.40	2.42	2.42	0.00	0.00	0.00	1
2.39	3.03	3.03	0.00	0.00	0.00	1
2.38	3.63	3.63	0.00	0.00	0.00	1
2.37	4.24	4.24	0.00	0.00	0.00	1
2.36	4.84	4.84	0.00	0.00	0.00	1
2.35	5.45	5.45	0.00	0.00	0.00	1
2.35	6.05	6.05	0.00	0.00	0.00	1
2.34	6.66	6.66	0.00	0.00	0.00	1
2.33	7.26	7.26	0.00	0.00	0.00	1
2.32	7.87	7.87	0.00	0.00	0.00	1
2.31	8.47	8.47	0.00	0.00	0.00	1
2.30	9.08	9.08	0.00	0.00	0.00	1
2.29	9.68	9.68	0.00	0.00	0.00	1
2.28	10.29	10.29	0.00	0.00	0.00	1
2.27	10.89	10.89	0.00	0.00	0.00	1
2.26	11.50	11.50	0.00	0.00	0.00	1
2.25	12.10	12.10	0.00	0.00	0.00	1

2.25	12.71	12.71	0.00	0.00	0.00	1
2.24	13.31	13.31	0.00	0.00	0.00	1
2.23	13.92	13.92	0.00	0.00	0.00	1
2.22	14.52	14.52	0.00	0.00	0.00	1
2.21	15.13	15.13	0.00	0.00	0.00	1
2.20	15.73	15.73	0.00	0.00	0.00	1
2.19	16.34	16.34	0.00	0.00	0.00	1
2.18	16.94	16.94	0.00	0.00	0.00	1
2.17	17.55	17.55	0.00	0.00	0.00	1
2.16	18.15	18.15	0.00	0.00	0.00	1
2.15	18.76	18.76	0.00	0.00	0.00	1
2.15	19.36	19.36	0.00	0.00	0.00	1
2.14	19.97	19.97	0.00	0.00	0.00	1
2.13	20.57	20.57	0.00	0.00	0.00	1
2.12	21.18	21.18	0.00	0.00	0.00	1
2.11	21.78	21.78	0.00	0.00	0.00	1
2.10	22.39	22.39	0.00	0.00	0.00	1
2.09	22.99	22.99	0.00	0.00	0.00	1
2.08	23.60	23.60	0.00	0.00	0.00	1
2.07	24.20	24.20	0.00	0.00	0.00	1
2.07	24.81	24.81	0.00	0.00	0.00	1
2.06	25.54	25.54	0.00	0.00	0.00	1
2.05	26.27	26.27	0.00	0.00	0.00	1
2.04	26.88	26.88	0.00	0.00	0.00	1
2.03	27.48	27.48	0.00	0.00	0.00	1
2.02	28.09	28.09	0.00	0.00	0.00	1
2.01	28.69	28.69	0.00	0.00	0.00	1
2.00	29.30	29.30	0.00	0.00	0.00	1
1.99	29.90	29.90	0.00	0.00	0.00	1
1.99	30.51	30.51	0.00	0.00	0.00	1
1.98	31.11	31.11	0.00	0.00	0.00	1
1.97	31.72	31.72	0.00	0.00	0.00	1
1.96	32.32	32.32	0.00	0.00	0.00	1
1.95	32.93	32.93	0.00	0.00	0.00	1
1.94	33.53	33.53	0.00	0.00	0.00	1
1.93	34.14	34.14	0.00	0.00	0.00	1
1.92	34.74	34.74	0.00	0.00	0.00	1
1.91	35.35	35.35	0.00	0.00	0.00	1
1.90	35.95	35.95	0.00	0.00	0.00	1
1.89	36.56	36.56	0.00	0.00	0.00	1
1.89	37.16	37.16	0.00	0.00	0.00	1
1.88	37.77	37.77	0.00	0.00	0.00	1
1.87	38.37	38.37	0.00	0.00	0.00	1
1.86	38.98	38.98	0.00	0.00	0.00	1
1.85	39.58	39.58	0.00	0.00	0.00	1
1.84	40.19	40.19	0.00	0.00	0.00	1
1.83	40.79	40.79	0.00	0.00	0.00	1
1.82	41.40	41.40	0.00	0.00	0.00	1
1.81	42.01	42.01	0.00	0.00	0.00	1
1.80	42.61	42.61	0.00	0.00	0.00	1
1.79	43.22	43.22	0.00	0.00	0.00	1
1.79	43.82	43.82	0.00	0.00	0.00	1
1.78	44.43	44.43	0.00	0.00	0.00	1
1.77	45.03	45.03	0.00	0.00	0.00	1

1.76	45.64	45.64	0.00	0.00	0.00	1
1.75	46.24	46.24	0.00	0.00	0.00	1
1.74	46.85	46.85	0.00	0.00	0.00	1
1.73	47.45	47.45	0.00	0.00	0.00	1
1.72	48.06	48.06	0.00	0.00	0.00	1
1.71	48.66	48.66	0.00	0.00	0.00	1
1.70	49.27	49.27	0.00	0.00	0.00	1
1.70	49.87	49.87	0.00	0.00	0.00	1
1.69	50.60	50.60	0.00	0.00	0.00	1
1.68	51.34	51.34	0.00	0.00	0.00	1
1.67	51.94	51.94	0.00	0.00	0.00	1
1.66	52.55	52.55	0.00	0.00	0.00	1
1.65	53.15	53.15	0.00	0.00	0.00	1
1.64	53.76	53.76	0.00	0.00	0.00	1
1.64	54.36	54.36	0.00	0.00	0.00	1
1.63	54.97	54.97	0.00	0.00	0.00	1
1.62	55.57	55.57	0.00	0.00	0.00	1
1.61	56.18	56.18	0.00	0.00	0.00	1
1.59	124.07	40.41	121.57	90.75	37.07	1
1.58	125.80	40.76	123.26	92.19	37.01	1
1.56	127.53	39.95	124.94	93.62	38.11	1
1.55	129.25	39.46	126.62	95.05	38.90	1
1.53	130.97	38.96	128.30	96.48	39.68	1
1.51	132.69	38.46	129.97	97.91	40.48	1
1.50	134.41	37.95	131.64	99.34	41.28	1
1.48	136.12	37.44	133.31	100.76	42.08	1
1.46	137.84	36.92	134.98	102.18	42.89	1
1.45	139.55	36.40	136.65	103.60	43.71	1
1.43	141.26	35.87	138.31	105.02	44.53	1
1.41	142.97	35.33	139.97	106.44	45.35	1
1.40	144.67	34.79	141.62	107.85	46.19	1
1.38	146.37	34.24	143.28	109.26	47.03	1
1.36	148.07	33.69	144.93	110.67	47.87	1
1.35	149.77	33.12	146.58	112.08	48.73	1
1.33	151.47	32.56	148.22	113.48	49.59	1
1.31	153.16	31.98	149.87	114.88	50.46	1
1.30	154.86	31.39	151.51	116.28	51.33	1
1.28	156.54	30.80	153.14	117.68	52.22	1
1.26	158.23	30.20	154.78	119.08	53.11	1
1.24	159.92	29.69	156.41	120.47	53.91	1
1.23	161.60	29.23	158.04	121.86	54.66	1
1.21	163.28	28.78	159.66	123.25	55.41	1
1.19	164.96	28.32	161.29	124.63	56.16	1
1.18	166.63	27.87	162.91	126.02	56.90	1
1.16	168.30	27.41	164.52	127.40	57.65	1
1.14	169.97	26.96	166.14	128.78	58.39	1
1.12	171.64	26.52	167.75	130.15	59.13	1
1.11	173.31	26.07	169.36	131.53	59.86	1
1.11	173.31	3.95	169.36	131.53	59.86	1
1.08	175.63	25.45	171.60	133.45	60.89	1
1.06	177.96	24.83	173.84	135.36	61.92	1
1.03	180.27	24.22	176.08	137.27	62.94	1
1.01	182.58	23.62	178.30	139.17	63.95	1
0.98	184.89	23.02	180.52	141.07	64.96	1

0.96	187.19	22.42	182.74	142.96	65.96	1
0.93	189.48	21.84	184.94	144.85	66.96	1
0.91	191.77	21.26	187.14	146.73	67.94	1
0.88	194.06	20.69	189.34	148.60	68.92	1
0.86	196.34	20.12	191.52	150.47	69.90	1
0.83	198.61	19.75	193.70	152.34	70.67	1
0.81	200.87	19.44	195.86	154.20	71.39	1
0.78	203.13	19.14	197.91	156.05	72.10	1
0.76	205.39	18.85	199.95	157.89	72.80	1
0.73	207.64	18.56	201.98	159.73	73.50	1
0.71	209.88	18.28	204.01	161.57	74.19	1
0.68	212.12	18.00	206.03	163.39	74.87	1
0.65	214.35	17.73	208.05	165.22	75.55	1
0.63	216.57	17.47	210.06	167.03	76.22	1
0.60	218.79	17.22	212.06	168.84	76.88	1
0.58	221.00	16.97	214.06	170.64	77.54	1
0.55	223.20	16.73	216.05	172.44	78.19	1
0.52	225.40	16.49	218.04	174.23	78.83	1
0.50	227.60	16.26	220.02	176.02	79.47	1
0.47	229.79	16.04	221.99	177.80	80.11	1
0.45	231.97	15.82	223.96	179.57	80.73	1
0.42	234.14	15.61	225.93	181.34	81.35	1
0.39	236.31	15.40	227.88	183.10	81.97	1
0.37	238.48	15.20	229.84	184.86	82.58	1
0.34	98.25	15.00	83.25	78.21	5.03	1
0.31	100.12	14.81	85.30	79.86	5.45	1
0.29	101.99	14.63	87.36	81.50	5.85	1
0.26	103.86	14.45	89.41	83.15	6.26	1
0.24	105.73	14.27	91.46	84.81	6.65	1
0.21	107.61	14.10	93.50	86.46	7.04	1
0.18	109.49	13.94	95.55	88.12	7.43	1
0.16	111.37	13.78	97.59	89.78	7.81	1
0.13	113.25	13.62	99.63	91.44	8.19	1
0.10	115.14	13.47	101.67	93.10	8.57	1
0.08	117.03	13.32	103.70	94.77	8.93	1
0.08	117.49	13.32	104.17	94.77	9.40	1
0.06	118.77	13.58	105.19	95.72	9.47	1
0.05	120.05	13.83	106.22	96.67	9.55	1
0.03	121.32	14.07	107.25	97.62	9.63	1
0.02	122.59	14.31	108.28	98.56	9.72	1
0.00	123.86	14.55	109.31	99.51	9.81	1

Time = 3675. Degree of Consolidation = 34.0%

Total Settlement = 2.063

Settlement at End of Primary Consolidation = 1.872

Settlement caused by Primary Consolidation at time 3675. = 0.638

Settlement caused by Secondary Compression at time 3675. = 0.000

Settlement Due to Desiccation = 1.425

Surface Elevation = 1.51

*****Current Conditions in Dredged Fill*****

***** Coordinates *****

***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
4.50	2.44	0.50	7.97	2.26	2.26	1
4.47	2.43	0.50	7.97	2.26	2.26	1
4.45	2.42	0.50	7.97	2.26	2.26	1
4.42	2.41	0.49	7.97	2.26	2.26	1
4.40	2.40	0.49	7.97	2.26	2.26	1
4.37	2.39	0.49	7.97	2.26	2.26	1
4.35	2.38	0.48	7.97	2.26	2.26	1
4.32	2.37	0.48	7.97	2.26	2.26	1
4.30	2.36	0.48	7.97	2.26	2.26	1
4.27	2.35	0.48	7.97	2.26	2.26	1
4.25	2.35	0.47	7.97	2.26	2.26	1
4.22	2.34	0.47	7.97	2.26	2.26	1
4.20	2.33	0.47	7.97	2.26	2.26	1
4.17	2.32	0.47	7.97	2.26	2.26	1
4.15	2.31	0.46	7.97	2.26	2.26	1
4.12	2.30	0.46	7.97	2.26	2.26	1
4.10	2.29	0.46	7.97	2.26	2.26	1
4.07	2.28	0.45	7.97	2.26	2.26	1
4.05	2.27	0.45	7.97	2.26	2.26	1
4.02	2.26	0.45	7.97	2.26	2.26	1
4.00	2.25	0.45	7.97	2.26	2.26	1
3.97	2.25	0.44	7.97	2.26	2.26	1
3.95	2.24	0.44	7.97	2.26	2.26	1
3.92	2.23	0.44	7.97	2.26	2.26	1
3.90	2.22	0.43	7.97	2.26	2.26	1
3.87	2.21	0.43	7.97	2.26	2.26	1
3.85	2.20	0.43	7.97	2.26	2.26	1
3.82	2.19	0.43	7.97	2.26	2.26	1
3.80	2.18	0.42	7.97	2.26	2.26	1
3.77	2.17	0.42	7.97	2.26	2.26	1
3.75	2.16	0.42	7.97	2.26	2.26	1
3.72	2.15	0.42	7.97	2.26	2.26	1
3.70	2.15	0.41	7.97	2.26	2.26	1
3.67	2.14	0.41	7.97	2.26	2.26	1
3.65	2.13	0.41	7.97	2.26	2.26	1
3.62	2.12	0.40	7.97	2.26	2.26	1
3.60	2.11	0.40	7.97	2.26	2.26	1
3.57	2.10	0.40	7.97	2.26	2.26	1
3.55	2.09	0.40	7.97	2.26	2.26	1
3.52	2.08	0.39	7.97	2.26	2.26	1
3.50	2.07	0.39	7.97	5.31	2.26	1
3.50	2.07	0.39	7.97	5.31	2.26	1

3.47	2.06	0.39	7.97	2.26	5.30	1
3.45	2.05	0.38	7.97	2.26	5.29	1
3.42	2.04	0.38	7.97	2.26	5.28	1
3.40	2.03	0.38	7.97	2.26	5.27	1
3.37	2.02	0.38	7.97	2.26	5.26	1
3.35	2.01	0.37	7.97	2.26	5.25	1
3.32	2.00	0.37	7.97	2.26	5.24	1
3.30	1.99	0.37	7.97	2.26	5.23	1
3.27	1.99	0.37	7.97	2.26	5.22	1
3.25	1.98	0.36	7.97	2.26	5.22	1
3.22	1.97	0.36	7.97	2.26	5.21	1
3.20	1.96	0.36	7.97	2.26	5.20	1
3.17	1.95	0.35	7.97	2.26	5.19	1
3.15	1.94	0.35	7.97	2.26	5.18	1
3.12	1.93	0.35	7.97	2.26	5.17	1
3.10	1.92	0.35	7.97	2.26	5.16	1
3.07	1.91	0.34	7.97	2.26	5.15	1
3.05	1.90	0.34	7.97	2.26	5.14	1
3.02	1.89	0.34	7.97	2.26	5.13	1
3.00	1.89	0.33	7.97	2.26	5.12	1
2.97	1.88	0.33	7.97	2.26	5.11	1
2.95	1.87	0.33	7.97	2.26	5.11	1
2.92	1.86	0.33	7.97	2.26	5.10	1
2.90	1.85	0.32	7.97	2.26	5.09	1
2.87	1.84	0.32	7.97	2.26	5.09	1
2.85	1.83	0.32	7.97	2.26	5.08	1
2.82	1.82	0.31	7.97	2.26	5.07	1
2.80	1.81	0.31	7.97	2.26	5.06	1
2.77	1.80	0.31	7.97	2.26	5.06	1
2.75	1.79	0.31	7.97	2.26	5.05	1
2.72	1.79	0.30	7.97	2.26	5.04	1
2.70	1.78	0.30	7.97	2.26	5.03	1
2.67	1.77	0.30	7.97	2.26	5.03	1
2.65	1.76	0.30	7.97	2.26	5.02	1
2.62	1.75	0.29	7.97	2.26	5.01	1
2.60	1.74	0.29	7.97	2.26	5.00	1
2.57	1.73	0.29	7.97	2.26	5.00	1
2.55	1.72	0.28	7.97	2.26	4.99	1
2.52	1.71	0.28	7.97	2.26	4.98	1
2.50	1.70	0.28	7.97	4.75	2.26	1
2.50	1.70	0.28	7.97	4.75	2.26	1
2.47	1.69	0.28	7.97	2.26	4.97	1
2.45	1.68	0.27	7.97	2.26	4.96	1
2.42	1.67	0.27	7.97	2.26	4.95	1
2.40	1.66	0.27	7.97	2.26	4.95	1
2.37	1.65	0.26	7.97	2.26	4.94	1
2.35	1.64	0.26	7.97	2.26	4.93	1
2.32	1.64	0.26	7.97	2.26	4.92	1
2.30	1.63	0.26	7.97	2.26	4.92	1
2.27	1.62	0.25	7.97	2.26	4.91	1
2.25	1.61	0.25	7.97	2.26	2.26	1
2.22	1.59	0.25	7.97	4.86	4.86	1
2.20	1.58	0.25	7.97	4.87	4.85	1
2.17	1.56	0.24	7.97	4.88	4.85	1

2.15	1.55	0.24	7.97	4.89	4.84	1
2.12	1.53	0.24	7.97	4.91	4.84	1
2.10	1.51	0.23	7.97	4.92	4.84	1
2.07	1.50	0.23	7.97	4.93	4.83	1
2.05	1.48	0.23	7.97	4.94	4.83	1
2.02	1.46	0.23	7.97	4.96	4.82	1
2.00	1.45	0.22	7.97	4.97	4.82	1
1.97	1.43	0.22	7.97	4.98	4.81	1
1.95	1.41	0.22	7.97	5.00	4.81	1
1.92	1.40	0.21	7.97	5.01	4.81	1
1.90	1.38	0.21	7.97	5.02	4.80	1
1.87	1.36	0.21	7.97	5.04	4.80	1
1.85	1.35	0.21	7.97	5.05	4.79	1
1.82	1.33	0.20	7.97	5.07	4.79	1
1.80	1.31	0.20	7.97	5.08	4.78	1
1.77	1.30	0.20	7.97	5.10	4.78	1
1.75	1.28	0.20	7.97	5.11	4.78	1
1.72	1.26	0.19	7.97	5.12	4.77	1
1.70	1.24	0.19	7.97	5.14	4.77	1
1.67	1.23	0.19	7.97	5.16	4.76	1
1.65	1.21	0.18	7.97	5.17	4.76	1
1.62	1.19	0.18	7.97	5.19	4.76	1
1.60	1.18	0.18	7.97	5.20	4.75	1
1.57	1.16	0.18	7.97	5.22	4.75	1
1.55	1.14	0.17	7.97	5.23	4.74	1
1.52	1.12	0.17	7.97	5.24	4.74	1
1.50	1.11	0.17	7.97	5.26	4.73	1
1.50	1.11	0.17	7.97	5.26	4.73	1
1.46	1.08	0.16	7.97	5.28	4.73	1
1.43	1.06	0.16	7.97	5.30	4.72	1
1.39	1.03	0.16	7.97	5.32	4.72	1
1.36	1.01	0.15	7.97	5.34	4.71	1
1.32	0.98	0.15	7.97	5.36	4.71	1
1.29	0.96	0.14	7.97	5.38	4.70	1
1.25	0.93	0.14	7.97	5.40	4.70	1
1.22	0.91	0.14	7.97	5.42	4.70	1
1.18	0.88	0.13	7.97	5.44	4.69	1
1.15	0.86	0.13	7.97	5.46	4.69	1
1.11	0.83	0.12	7.97	5.47	4.69	1
1.08	0.81	0.12	7.97	5.49	4.68	1
1.05	0.78	0.12	7.97	5.51	4.68	1
1.01	0.76	0.11	7.97	5.53	4.67	1
0.98	0.73	0.11	7.97	5.54	4.67	1
0.94	0.71	0.10	7.97	5.56	4.67	1
0.91	0.68	0.10	7.97	5.58	4.66	1
0.87	0.65	0.10	7.97	5.59	4.66	1
0.84	0.63	0.09	7.97	5.61	4.65	1
0.80	0.60	0.09	7.97	5.62	4.65	1
0.77	0.58	0.09	7.97	5.64	4.65	1
0.73	0.55	0.08	7.97	5.65	4.64	1
0.70	0.52	0.08	7.97	5.66	4.64	1
0.66	0.50	0.07	7.97	5.68	4.63	1
0.62	0.47	0.07	7.97	5.69	4.63	1
0.59	0.45	0.07	7.97	5.70	4.62	1

0.55	0.42	0.06	7.97	5.71	4.62	1
0.52	0.39	0.06	7.97	5.73	4.62	1
0.48	0.37	0.05	7.97	5.74	4.61	1
0.45	0.34	0.05	7.97	5.75	4.61	1
0.41	0.31	0.05	7.97	5.76	4.60	1
0.38	0.29	0.04	7.97	5.77	4.60	1
0.34	0.26	0.04	7.97	5.78	4.59	1
0.31	0.24	0.03	7.97	5.79	4.59	1
0.28	0.21	0.03	7.97	5.80	4.59	1
0.24	0.18	0.03	7.97	5.81	4.58	1
0.21	0.16	0.02	7.97	5.82	4.58	1
0.17	0.13	0.02	7.97	5.83	4.57	1
0.14	0.10	0.02	7.97	5.84	4.57	1
0.10	0.08	0.01	7.97	5.85	4.56	1
0.10	0.08	0.01	7.97	5.85	4.56	1
0.08	0.06	0.01	7.97	5.83	4.56	1
0.06	0.05	0.01	7.97	5.82	4.55	1
0.04	0.03	0.00	7.97	5.80	4.55	1
0.02	0.02	0.00	7.97	5.79	4.54	1
0.00	0.00	0.00	7.97	5.78	4.54	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
2.44	0.00	0.00	0.00	0.00	0.00	1
2.43	0.61	0.61	0.00	0.00	0.00	1
2.42	1.21	1.21	0.00	0.00	0.00	1
2.41	1.82	1.82	0.00	0.00	0.00	1
2.40	2.42	2.42	0.00	0.00	0.00	1
2.39	3.03	3.03	0.00	0.00	0.00	1
2.38	3.63	3.63	0.00	0.00	0.00	1
2.37	4.24	4.24	0.00	0.00	0.00	1
2.36	4.84	4.84	0.00	0.00	0.00	1
2.35	5.45	5.45	0.00	0.00	0.00	1
2.35	6.05	6.05	0.00	0.00	0.00	1
2.34	6.66	6.66	0.00	0.00	0.00	1
2.33	7.26	7.26	0.00	0.00	0.00	1
2.32	7.87	7.87	0.00	0.00	0.00	1
2.31	8.47	8.47	0.00	0.00	0.00	1
2.30	9.08	9.08	0.00	0.00	0.00	1
2.29	9.68	9.68	0.00	0.00	0.00	1
2.28	10.29	10.29	0.00	0.00	0.00	1
2.27	10.89	10.89	0.00	0.00	0.00	1
2.26	11.50	11.50	0.00	0.00	0.00	1
2.25	12.10	12.10	0.00	0.00	0.00	1
2.25	12.71	12.71	0.00	0.00	0.00	1
2.24	13.31	13.31	0.00	0.00	0.00	1
2.23	13.92	13.92	0.00	0.00	0.00	1
2.22	14.52	14.52	0.00	0.00	0.00	1
2.21	15.13	15.13	0.00	0.00	0.00	1
2.20	15.73	15.73	0.00	0.00	0.00	1
2.19	16.34	16.34	0.00	0.00	0.00	1
2.18	16.94	16.94	0.00	0.00	0.00	1

2.17	17.55	17.55	0.00	0.00	0.00	1
2.16	18.15	18.15	0.00	0.00	0.00	1
2.15	18.76	18.76	0.00	0.00	0.00	1
2.15	19.36	19.36	0.00	0.00	0.00	1
2.14	19.97	19.97	0.00	0.00	0.00	1
2.13	20.57	20.57	0.00	0.00	0.00	1
2.12	21.18	21.18	0.00	0.00	0.00	1
2.11	21.78	21.78	0.00	0.00	0.00	1
2.10	22.39	22.39	0.00	0.00	0.00	1
2.09	22.99	22.99	0.00	0.00	0.00	1
2.08	23.60	23.60	0.00	0.00	0.00	1
2.07	24.20	24.20	0.00	0.00	0.00	1
2.07	24.81	24.81	0.00	0.00	0.00	1
2.06	25.54	25.54	0.00	0.00	0.00	1
2.05	26.27	26.27	0.00	0.00	0.00	1
2.04	26.88	26.88	0.00	0.00	0.00	1
2.03	27.48	27.48	0.00	0.00	0.00	1
2.02	28.09	28.09	0.00	0.00	0.00	1
2.01	28.69	28.69	0.00	0.00	0.00	1
2.00	29.30	29.30	0.00	0.00	0.00	1
1.99	29.90	29.90	0.00	0.00	0.00	1
1.99	30.51	30.51	0.00	0.00	0.00	1
1.98	31.11	31.11	0.00	0.00	0.00	1
1.97	31.72	31.72	0.00	0.00	0.00	1
1.96	32.32	32.32	0.00	0.00	0.00	1
1.95	32.93	32.93	0.00	0.00	0.00	1
1.94	33.53	33.53	0.00	0.00	0.00	1
1.93	34.14	34.14	0.00	0.00	0.00	1
1.92	34.74	34.74	0.00	0.00	0.00	1
1.91	35.35	35.35	0.00	0.00	0.00	1
1.90	35.95	35.95	0.00	0.00	0.00	1
1.89	36.56	36.56	0.00	0.00	0.00	1
1.89	37.16	37.16	0.00	0.00	0.00	1
1.88	37.77	37.77	0.00	0.00	0.00	1
1.87	38.37	38.37	0.00	0.00	0.00	1
1.86	38.98	38.98	0.00	0.00	0.00	1
1.85	39.58	39.58	0.00	0.00	0.00	1
1.84	40.19	40.19	0.00	0.00	0.00	1
1.83	40.79	40.79	0.00	0.00	0.00	1
1.82	41.40	41.40	0.00	0.00	0.00	1
1.81	42.01	42.01	0.00	0.00	0.00	1
1.80	42.61	42.61	0.00	0.00	0.00	1
1.79	43.22	43.22	0.00	0.00	0.00	1
1.79	43.82	43.82	0.00	0.00	0.00	1
1.78	44.43	44.43	0.00	0.00	0.00	1
1.77	45.03	45.03	0.00	0.00	0.00	1
1.76	45.64	45.64	0.00	0.00	0.00	1
1.75	46.24	46.24	0.00	0.00	0.00	1
1.74	46.85	46.85	0.00	0.00	0.00	1
1.73	47.45	47.45	0.00	0.00	0.00	1
1.72	48.06	48.06	0.00	0.00	0.00	1
1.71	48.66	48.66	0.00	0.00	0.00	1
1.70	49.27	49.27	0.00	0.00	0.00	1
1.70	49.87	49.87	0.00	0.00	0.00	1

1.69	50.60	50.60	0.00	0.00	0.00	1
1.68	51.34	51.34	0.00	0.00	0.00	1
1.67	51.94	51.94	0.00	0.00	0.00	1
1.66	52.55	52.55	0.00	0.00	0.00	1
1.65	53.15	53.15	0.00	0.00	0.00	1
1.64	53.76	53.76	0.00	0.00	0.00	1
1.64	54.36	54.36	0.00	0.00	0.00	1
1.63	54.97	54.97	0.00	0.00	0.00	1
1.62	55.57	55.57	0.00	0.00	0.00	1
1.61	56.18	56.18	0.00	0.00	0.00	1
1.59	124.07	40.41	121.57	90.75	37.07	1
1.58	125.80	40.76	123.26	92.19	37.01	1
1.56	127.53	39.95	124.94	93.62	38.11	1
1.55	129.25	39.46	126.62	95.05	38.90	1
1.53	130.97	38.96	128.30	96.48	39.68	1
1.51	132.69	38.46	129.97	97.91	40.48	1
1.50	134.41	37.95	131.64	99.34	41.28	1
1.48	136.12	37.44	133.31	100.76	42.08	1
1.46	137.84	36.92	134.98	102.18	42.89	1
1.45	139.55	36.40	136.65	103.60	43.71	1
1.43	141.26	35.87	138.31	105.02	44.53	1
1.41	142.97	35.33	139.97	106.44	45.35	1
1.40	144.67	34.79	141.62	107.85	46.19	1
1.38	146.37	34.24	143.28	109.26	47.03	1
1.36	148.07	33.69	144.93	110.67	47.87	1
1.35	149.77	33.12	146.58	112.08	48.73	1
1.33	151.47	32.56	148.22	113.48	49.59	1
1.31	153.16	31.98	149.87	114.88	50.46	1
1.30	154.86	31.39	151.51	116.28	51.33	1
1.28	156.54	30.80	153.14	117.68	52.22	1
1.26	158.23	30.20	154.78	119.08	53.11	1
1.24	159.92	29.69	156.41	120.47	53.91	1
1.23	161.60	29.23	158.04	121.86	54.66	1
1.21	163.28	28.78	159.66	123.25	55.41	1
1.19	164.96	28.32	161.29	124.63	56.16	1
1.18	166.63	27.87	162.91	126.02	56.90	1
1.16	168.30	27.41	164.52	127.40	57.65	1
1.14	169.97	26.96	166.14	128.78	58.39	1
1.12	171.64	26.52	167.75	130.15	59.13	1
1.11	173.31	26.07	169.36	131.53	59.86	1
1.11	173.31	3.95	169.36	131.53	59.86	1
1.08	175.63	25.45	171.60	133.45	60.89	1
1.06	177.96	24.83	173.84	135.36	61.92	1
1.03	180.27	24.22	176.08	137.27	62.94	1
1.01	182.58	23.62	178.30	139.17	63.95	1
0.98	184.89	23.02	180.52	141.07	64.96	1
0.96	187.19	22.42	182.74	142.96	65.96	1
0.93	189.48	21.84	184.94	144.85	66.96	1
0.91	191.77	21.26	187.14	146.73	67.94	1
0.88	194.06	20.69	189.34	148.60	68.92	1
0.86	196.34	20.12	191.52	150.47	69.90	1
0.83	198.61	19.75	193.70	152.34	70.67	1
0.81	200.87	19.44	195.86	154.20	71.39	1
0.78	203.13	19.14	197.91	156.05	72.10	1

0.76	205.39	18.85	199.95	157.89	72.80	1
0.73	207.64	18.56	201.98	159.73	73.50	1
0.71	209.88	18.28	204.01	161.57	74.19	1
0.68	212.12	18.00	206.03	163.39	74.87	1
0.65	214.35	17.73	208.05	165.22	75.55	1
0.63	216.57	17.47	210.06	167.03	76.22	1
0.60	218.79	17.22	212.06	168.84	76.88	1
0.58	221.00	16.97	214.06	170.64	77.54	1
0.55	223.20	16.73	216.05	172.44	78.19	1
0.52	225.40	16.49	218.04	174.23	78.83	1
0.50	227.60	16.26	220.02	176.02	79.47	1
0.47	229.79	16.04	221.99	177.80	80.11	1
0.45	231.97	15.82	223.96	179.57	80.73	1
0.42	234.14	15.61	225.93	181.34	81.35	1
0.39	236.31	15.40	227.88	183.10	81.97	1
0.37	96.85	15.20	81.65	76.57	5.08	1
0.34	98.71	15.00	83.71	78.21	5.50	1
0.31	100.58	14.81	85.77	79.86	5.91	1
0.29	102.45	14.63	87.82	81.50	6.32	1
0.26	104.32	14.45	89.87	83.15	6.72	1
0.24	106.20	14.27	91.92	84.81	7.12	1
0.21	108.08	14.10	93.97	86.46	7.51	1
0.18	109.95	13.94	96.02	88.12	7.90	1
0.16	111.84	13.78	98.06	89.78	8.28	1
0.13	113.72	13.62	100.10	91.44	8.66	1
0.10	115.61	13.47	102.13	93.10	9.03	1
0.08	117.49	13.32	104.17	94.77	9.40	1
0.08	117.96	13.32	104.64	94.77	9.87	1
0.06	119.24	13.58	105.66	95.72	9.94	1
0.05	120.51	13.83	106.69	96.67	10.02	1
0.03	121.79	14.07	107.72	97.62	10.10	1
0.02	123.06	14.31	108.75	98.56	10.18	1
0.00	124.33	14.55	109.78	99.51	10.27	1

Time = 7325. Degree of Consolidation = 34.0%

Total Settlement = 2.063

Settlement at End of Primary Consolidation = 1.872

Settlement caused by Primary Consolidation at time 7325. = 0.638

Settlement caused by Secondary Compression at time 7325. = 0.000

Settlement Due to Desiccation = 1.425

Surface Elevation = 1.51



Grand Chenier Marsh Creation
GeoEngineers, Inc.

Report Creation Date: 2023/02/24, 15:20:12

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Settle3 Analysis Information

Grand Chenier Marsh Creation

Project Settings

Document Name	Grand Chenier_MC340_MF+3.5
Project Title	Grand Chenier Marsh Creation
Analysis	ML -0.929 , MF +3.5
Author	DNF
Company	GeoEngineers, Inc.
Date Created	1/27/2023
Last saved with Settle3 version	5.017
Stress Computation Method	Boussinesq
Stress Units	Imperial, stress as ksf
Settlement Units	inches
Time-dependent Consolidation Analysis	
Time Units	days
Permeability Units	inches/year

Advanced Settings

Start of secondary consolidation (% of primary)	95
Min. stress for secondary consolidation (% of initial)	1
Reset time when load changes for secondary consolidation	No
Minimum settlement ratio for subgrade modulus	0.9
Use average poisson's ratio to calculate layered stresses	
Ignore negative effective stresses in settlement calculations	
Add field points to load edges	

Soil Profile

Layer Option	Horizontal Soil Layers
Vertical Axis	Depth below ground surface

Stage Settings

Stage #	Name	Time [days]
1	Stage 1	0
2	Stage 2	15
3	Stage 3	30
4	Stage 4	60
5	Stage 5	90
6	Stage 6	120
7	Stage 7	150
8	Stage 8	180
9	Stage 9	270
10	Stage 10	365
11	Stage 11	730
12	Stage 12	1095
13	Stage 13	2190
14	Stage 14	3650
15	Stage 15	7300

Results

Time taken to compute: 0 seconds

Stage: Stage 1 = 0 d

Data Type	Minimum	Maximum
Total Settlement [in]	0	0
Total Consolidation Settlement [in]	0	0
Virgin Consolidation Settlement [in]	0	0
Recompression Consolidation Settlement [in]	0	0
Immediate Settlement [in]	0	0
Secondary Settlement [in]	0	0
Loading Stress ZZ [ksf]	0.0826902	0.103576
Loading Stress XX [ksf]	0.0103871	0.0701154
Loading Stress YY [ksf]	0.0103871	0.0701154
Effective Stress ZZ [ksf]	0	1.64871
Effective Stress XX [ksf]	0.0701154	1.6591
Effective Stress YY [ksf]	0.0701154	1.6591
Total Stress ZZ [ksf]	0.103576	4.16944
Total Stress XX [ksf]	0.173692	4.17982
Total Stress YY [ksf]	0.173692	4.17982
Modulus of Subgrade Reaction (Total) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Immediate) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Consolidation) [ksf/ft]	0	0
Total Strain	0	0
Pore Water Pressure [ksf]	0.103576	2.52072
Excess Pore Water Pressure [ksf]	0.0826902	0.103576
Degree of Consolidation [%]	0	0
Pre-consolidation Stress [ksf]	0.272	1.64785
Over-consolidation Ratio	1	204.951
Void Ratio	0	3.38
Permeability [in/y]	0	53.1409
Coefficient of Consolidation [in ² /y]	0	1051
Hydroconsolidation Settlement [in]	0	0
Average Degree of Consolidation [%]	0	0
Undrained Shear Strength	0	0

Stage: Stage 2 = 15 d

Data Type	Minimum	Maximum
Total Settlement [in]	0	0.83338
Total Consolidation Settlement [in]	0	0.83338
Virgin Consolidation Settlement [in]	0	0.290151
Recompression Consolidation Settlement [in]	0	0.543229
Immediate Settlement [in]	0	0
Secondary Settlement [in]	0	0
Loading Stress ZZ [ksf]	0.0826902	0.103576
Loading Stress XX [ksf]	0.0103871	0.0701154
Loading Stress YY [ksf]	0.0103871	0.0701154
Effective Stress ZZ [ksf]	0.0692978	1.7314
Effective Stress XX [ksf]	0.136236	1.74179
Effective Stress YY [ksf]	0.136236	1.74179
Total Stress ZZ [ksf]	0.103576	4.16944
Total Stress XX [ksf]	0.173692	4.17982
Total Stress YY [ksf]	0.173692	4.17982
Modulus of Subgrade Reaction (Total) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Immediate) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Consolidation) [ksf/ft]	0	0
Total Strain	0	0.0563058
Pore Water Pressure [ksf]	0	2.43803
Excess Pore Water Pressure [ksf]	0	0.103064
Degree of Consolidation [%]	0	98.9949
Pre-consolidation Stress [ksf]	0.272	1.73056
Over-consolidation Ratio	1	3.52436
Void Ratio	0	3.37998
Permeability [in/y]	0	53.1409
Coefficient of Consolidation [in ² /y]	0	1051
Hydroconsolidation Settlement [in]	0	0
Average Degree of Consolidation [%]	0	0
Undrained Shear Strength	0	0.00437087

Stage: Stage 3 = 30 d

Data Type	Minimum	Maximum
Total Settlement [in]	0	1.04173
Total Consolidation Settlement [in]	0	1.04173
Virgin Consolidation Settlement [in]	0	0.384051
Recompression Consolidation Settlement [in]	0	0.657677
Immediate Settlement [in]	0	0
Secondary Settlement [in]	0	0
Loading Stress ZZ [ksf]	0.0826902	0.103576
Loading Stress XX [ksf]	0.0103871	0.0701154
Loading Stress YY [ksf]	0.0103871	0.0701154
Effective Stress ZZ [ksf]	0.0899063	1.7314
Effective Stress XX [ksf]	0.156038	1.74179
Effective Stress YY [ksf]	0.156038	1.74179
Total Stress ZZ [ksf]	0.103576	4.16944
Total Stress XX [ksf]	0.173692	4.17982
Total Stress YY [ksf]	0.173692	4.17982
Modulus of Subgrade Reaction (Total) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Immediate) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Consolidation) [ksf/ft]	0	0
Total Strain	0	0.0563162
Pore Water Pressure [ksf]	0	2.43803
Excess Pore Water Pressure [ksf]	0	0.1028
Degree of Consolidation [%]	0	99.2787
Pre-consolidation Stress [ksf]	0.272	1.73056
Over-consolidation Ratio	1	2.87014
Void Ratio	0	3.37987
Permeability [in/y]	0	53.1409
Coefficient of Consolidation [in ² /y]	0	1051
Hydroconsolidation Settlement [in]	0	0
Average Degree of Consolidation [%]	0	0
Undrained Shear Strength	0	0.00437087

Stage: Stage 4 = 60 d

Data Type	Minimum	Maximum
Total Settlement [in]	0	1.29273
Total Consolidation Settlement [in]	0	1.29273
Virgin Consolidation Settlement [in]	0	0.496385
Recompression Consolidation Settlement [in]	0	0.796343
Immediate Settlement [in]	0	0
Secondary Settlement [in]	0	0
Loading Stress ZZ [ksf]	0.0826902	0.103576
Loading Stress XX [ksf]	0.0103871	0.0701154
Loading Stress YY [ksf]	0.0103871	0.0701154
Effective Stress ZZ [ksf]	0.103576	1.7314
Effective Stress XX [ksf]	0.173692	1.74179
Effective Stress YY [ksf]	0.173692	1.74179
Total Stress ZZ [ksf]	0.103576	4.16944
Total Stress XX [ksf]	0.173692	4.17982
Total Stress YY [ksf]	0.173692	4.17982
Modulus of Subgrade Reaction (Total) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Immediate) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Consolidation) [ksf/ft]	0	0
Total Strain	0	0.0563217
Pore Water Pressure [ksf]	0	2.43803
Excess Pore Water Pressure [ksf]	0	0.102049
Degree of Consolidation [%]	0	99.467
Pre-consolidation Stress [ksf]	0.272	1.73056
Over-consolidation Ratio	1	2.59443
Void Ratio	0	3.37935
Permeability [in/y]	0	53.1409
Coefficient of Consolidation [in ² /y]	0	1051
Hydroconsolidation Settlement [in]	0	0
Average Degree of Consolidation [%]	0	0
Undrained Shear Strength	0	0.00437087

Stage: Stage 5 = 90 d

Data Type	Minimum	Maximum
Total Settlement [in]	0	1.45808
Total Consolidation Settlement [in]	0	1.45808
Virgin Consolidation Settlement [in]	0	0.578431
Recompression Consolidation Settlement [in]	0	0.879652
Immediate Settlement [in]	0	0
Secondary Settlement [in]	0	0
Loading Stress ZZ [ksf]	0.0826902	0.103576
Loading Stress XX [ksf]	0.0103871	0.0701154
Loading Stress YY [ksf]	0.0103871	0.0701154
Effective Stress ZZ [ksf]	0.103576	1.7314
Effective Stress XX [ksf]	0.173692	1.74179
Effective Stress YY [ksf]	0.173692	1.74179
Total Stress ZZ [ksf]	0.103576	4.16944
Total Stress XX [ksf]	0.173692	4.17982
Total Stress YY [ksf]	0.173692	4.17982
Modulus of Subgrade Reaction (Total) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Immediate) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Consolidation) [ksf/ft]	0	0
Total Strain	0	0.0563247
Pore Water Pressure [ksf]	0	2.43803
Excess Pore Water Pressure [ksf]	0	0.100312
Degree of Consolidation [%]	0	99.5594
Pre-consolidation Stress [ksf]	0.272	1.73056
Over-consolidation Ratio	1	2.59383
Void Ratio	0	3.37872
Permeability [in/y]	0	53.1409
Coefficient of Consolidation [in ² /y]	0	1051
Hydroconsolidation Settlement [in]	0	0
Average Degree of Consolidation [%]	0	0
Undrained Shear Strength	0	0.00437087

Stage: Stage 6 = 120 d

Data Type	Minimum	Maximum
Total Settlement [in]	0	1.59912
Total Consolidation Settlement [in]	0	1.59912
Virgin Consolidation Settlement [in]	0	0.666613
Recompression Consolidation Settlement [in]	0	0.932507
Immediate Settlement [in]	0	0
Secondary Settlement [in]	0	0
Loading Stress ZZ [ksf]	0.0826902	0.103576
Loading Stress XX [ksf]	0.0103871	0.0701154
Loading Stress YY [ksf]	0.0103871	0.0701154
Effective Stress ZZ [ksf]	0.103576	1.7314
Effective Stress XX [ksf]	0.173692	1.74179
Effective Stress YY [ksf]	0.173692	1.74179
Total Stress ZZ [ksf]	0.103576	4.16944
Total Stress XX [ksf]	0.173692	4.17982
Total Stress YY [ksf]	0.173692	4.17982
Modulus of Subgrade Reaction (Total) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Immediate) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Consolidation) [ksf/ft]	0	0
Total Strain	0	0.0563265
Pore Water Pressure [ksf]	0	2.43803
Excess Pore Water Pressure [ksf]	0	0.0976774
Degree of Consolidation [%]	0	99.6174
Pre-consolidation Stress [ksf]	0.272	1.73056
Over-consolidation Ratio	1	2.59346
Void Ratio	0	3.37845
Permeability [in/y]	0	53.1409
Coefficient of Consolidation [in ² /y]	0	1051
Hydroconsolidation Settlement [in]	0	0
Average Degree of Consolidation [%]	0	0
Undrained Shear Strength	0	0.00437087

Stage: Stage 7 = 150 d

Data Type	Minimum	Maximum
Total Settlement [in]	0	1.70798
Total Consolidation Settlement [in]	0	1.70798
Virgin Consolidation Settlement [in]	0	0.737879
Recompression Consolidation Settlement [in]	0	0.970099
Immediate Settlement [in]	0	0
Secondary Settlement [in]	0	0
Loading Stress ZZ [ksf]	0.0826902	0.103576
Loading Stress XX [ksf]	0.0103871	0.0701154
Loading Stress YY [ksf]	0.0103871	0.0701154
Effective Stress ZZ [ksf]	0.103576	1.7314
Effective Stress XX [ksf]	0.173692	1.74179
Effective Stress YY [ksf]	0.173692	1.74179
Total Stress ZZ [ksf]	0.103576	4.16944
Total Stress XX [ksf]	0.173692	4.17982
Total Stress YY [ksf]	0.173692	4.17982
Modulus of Subgrade Reaction (Total) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Immediate) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Consolidation) [ksf/ft]	0	0
Total Strain	0	0.0563276
Pore Water Pressure [ksf]	0	2.43803
Excess Pore Water Pressure [ksf]	0	0.0943901
Degree of Consolidation [%]	0	99.6571
Pre-consolidation Stress [ksf]	0.272	1.73056
Over-consolidation Ratio	1	2.59324
Void Ratio	0	3.37822
Permeability [in/y]	0	53.1409
Coefficient of Consolidation [in ² /y]	0	1051
Hydroconsolidation Settlement [in]	0	0
Average Degree of Consolidation [%]	0	0
Undrained Shear Strength	0	0.00437087

Stage: Stage 8 = 180 d

Data Type	Minimum	Maximum
Total Settlement [in]	0	1.79636
Total Consolidation Settlement [in]	0	1.79636
Virgin Consolidation Settlement [in]	0	0.797925
Recompression Consolidation Settlement [in]	0	0.998437
Immediate Settlement [in]	0	0
Secondary Settlement [in]	0	0
Loading Stress ZZ [ksf]	0.0826902	0.103576
Loading Stress XX [ksf]	0.0103871	0.0701154
Loading Stress YY [ksf]	0.0103871	0.0701154
Effective Stress ZZ [ksf]	0.103576	1.7314
Effective Stress XX [ksf]	0.173692	1.74179
Effective Stress YY [ksf]	0.173692	1.74179
Total Stress ZZ [ksf]	0.103576	4.16944
Total Stress XX [ksf]	0.173692	4.17982
Total Stress YY [ksf]	0.173692	4.17982
Modulus of Subgrade Reaction (Total) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Immediate) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Consolidation) [ksf/ft]	0	0
Total Strain	0	0.0563283
Pore Water Pressure [ksf]	0	2.43803
Excess Pore Water Pressure [ksf]	0	0.0920787
Degree of Consolidation [%]	0	99.6861
Pre-consolidation Stress [ksf]	0.272	1.73056
Over-consolidation Ratio	1	2.5931
Void Ratio	0	3.37801
Permeability [in/y]	0	53.1409
Coefficient of Consolidation [in ² /y]	0	1051
Hydroconsolidation Settlement [in]	0	0
Average Degree of Consolidation [%]	0	0
Undrained Shear Strength	0	0.00437087

Stage: Stage 9 = 270 d

Data Type	Minimum	Maximum
Total Settlement [in]	0	1.99392
Total Consolidation Settlement [in]	0	1.99392
Virgin Consolidation Settlement [in]	0	0.938569
Recompression Consolidation Settlement [in]	0	1.05535
Immediate Settlement [in]	0	0
Secondary Settlement [in]	0	0
Loading Stress ZZ [ksf]	0.0826902	0.103576
Loading Stress XX [ksf]	0.0103871	0.0701154
Loading Stress YY [ksf]	0.0103871	0.0701154
Effective Stress ZZ [ksf]	0.103576	1.7314
Effective Stress XX [ksf]	0.173692	1.74179
Effective Stress YY [ksf]	0.173692	1.74179
Total Stress ZZ [ksf]	0.103576	4.16944
Total Stress XX [ksf]	0.173692	4.17982
Total Stress YY [ksf]	0.173692	4.17982
Modulus of Subgrade Reaction (Total) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Immediate) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Consolidation) [ksf/ft]	0	0
Total Strain	0	0.0563292
Pore Water Pressure [ksf]	0	2.43803
Excess Pore Water Pressure [ksf]	0	0.0856971
Degree of Consolidation [%]	0	99.742
Pre-consolidation Stress [ksf]	0.272	1.73056
Over-consolidation Ratio	1	2.59292
Void Ratio	0	3.37743
Permeability [in/y]	0	53.1409
Coefficient of Consolidation [in ² /y]	0	1051
Hydroconsolidation Settlement [in]	0	0
Average Degree of Consolidation [%]	0	0
Undrained Shear Strength	0	0.00437087

Stage: Stage 10 = 365 d

Data Type	Minimum	Maximum
Total Settlement [in]	0	2.14633
Total Consolidation Settlement [in]	0	2.14633
Virgin Consolidation Settlement [in]	0	1.05124
Recompression Consolidation Settlement [in]	0	1.09508
Immediate Settlement [in]	0	0
Secondary Settlement [in]	0	0
Loading Stress ZZ [ksf]	0.0826902	0.103576
Loading Stress XX [ksf]	0.0103871	0.0701154
Loading Stress YY [ksf]	0.0103871	0.0701154
Effective Stress ZZ [ksf]	0.103576	1.7314
Effective Stress XX [ksf]	0.173692	1.74179
Effective Stress YY [ksf]	0.173692	1.74179
Total Stress ZZ [ksf]	0.103576	4.16944
Total Stress XX [ksf]	0.173692	4.17982
Total Stress YY [ksf]	0.173692	4.17982
Modulus of Subgrade Reaction (Total) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Immediate) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Consolidation) [ksf/ft]	0	0
Total Strain	0	0.0563294
Pore Water Pressure [ksf]	0	2.43803
Excess Pore Water Pressure [ksf]	0	0.0785961
Degree of Consolidation [%]	0	99.7785
Pre-consolidation Stress [ksf]	0.272	1.73056
Over-consolidation Ratio	1	2.59288
Void Ratio	0	3.37682
Permeability [in/y]	0	53.1409
Coefficient of Consolidation [in ² /y]	0	1051
Hydroconsolidation Settlement [in]	0	0
Average Degree of Consolidation [%]	0	0
Undrained Shear Strength	0	0.00437087

Stage: Stage 11 = 730 d

Data Type	Minimum	Maximum
Total Settlement [in]	0	2.52059
Total Consolidation Settlement [in]	0	2.52059
Virgin Consolidation Settlement [in]	0	1.33416
Recompression Consolidation Settlement [in]	0	1.18643
Immediate Settlement [in]	0	0
Secondary Settlement [in]	0	0
Loading Stress ZZ [ksf]	0.0826902	0.103576
Loading Stress XX [ksf]	0.0103871	0.0701154
Loading Stress YY [ksf]	0.0103871	0.0701154
Effective Stress ZZ [ksf]	0.103576	1.7314
Effective Stress XX [ksf]	0.173692	1.74179
Effective Stress YY [ksf]	0.173692	1.74179
Total Stress ZZ [ksf]	0.103576	4.16944
Total Stress XX [ksf]	0.173692	4.17982
Total Stress YY [ksf]	0.173692	4.17982
Modulus of Subgrade Reaction (Total) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Immediate) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Consolidation) [ksf/ft]	0	0
Total Strain	0	0.0563295
Pore Water Pressure [ksf]	0	2.43803
Excess Pore Water Pressure [ksf]	0	0.0538496
Degree of Consolidation [%]	0	99.8578
Pre-consolidation Stress [ksf]	0.272	1.73056
Over-consolidation Ratio	1	2.59287
Void Ratio	0	3.3748
Permeability [in/y]	0	53.1409
Coefficient of Consolidation [in ² /y]	0	1051
Hydroconsolidation Settlement [in]	0	0
Average Degree of Consolidation [%]	0	0
Undrained Shear Strength	0	0.00437087

Stage: Stage 12 = 1095 d

Data Type	Minimum	Maximum
Total Settlement [in]	0	2.76753
Total Consolidation Settlement [in]	0	2.76753
Virgin Consolidation Settlement [in]	0	1.53804
Recompression Consolidation Settlement [in]	0	1.22949
Immediate Settlement [in]	0	0
Secondary Settlement [in]	0	0
Loading Stress ZZ [ksf]	0.0826902	0.103576
Loading Stress XX [ksf]	0.0103871	0.0701154
Loading Stress YY [ksf]	0.0103871	0.0701154
Effective Stress ZZ [ksf]	0.103576	1.7314
Effective Stress XX [ksf]	0.173692	1.74179
Effective Stress YY [ksf]	0.173692	1.74179
Total Stress ZZ [ksf]	0.103576	4.16944
Total Stress XX [ksf]	0.173692	4.17982
Total Stress YY [ksf]	0.173692	4.17982
Modulus of Subgrade Reaction (Total) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Immediate) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Consolidation) [ksf/ft]	0	0
Total Strain	0	0.0563295
Pore Water Pressure [ksf]	0	2.43803
Excess Pore Water Pressure [ksf]	0	0.0363085
Degree of Consolidation [%]	0	99.9046
Pre-consolidation Stress [ksf]	0.272	1.73056
Over-consolidation Ratio	1	2.59287
Void Ratio	0	3.37342
Permeability [in/y]	0	53.1409
Coefficient of Consolidation [in ² /y]	0	1051
Hydroconsolidation Settlement [in]	0	0
Average Degree of Consolidation [%]	0	0
Undrained Shear Strength	0	0.00437087

Stage: Stage 13 = 2190 d

Data Type	Minimum	Maximum
Total Settlement [in]	0	3.18783
Total Consolidation Settlement [in]	0	3.18783
Virgin Consolidation Settlement [in]	0	1.92965
Recompression Consolidation Settlement [in]	0	1.25818
Immediate Settlement [in]	0	0
Secondary Settlement [in]	0	0
Loading Stress ZZ [ksf]	0.0826902	0.103576
Loading Stress XX [ksf]	0.0103871	0.0701154
Loading Stress YY [ksf]	0.0103871	0.0701154
Effective Stress ZZ [ksf]	0.103576	1.7314
Effective Stress XX [ksf]	0.173692	1.74179
Effective Stress YY [ksf]	0.173692	1.74179
Total Stress ZZ [ksf]	0.103576	4.16944
Total Stress XX [ksf]	0.173692	4.17982
Total Stress YY [ksf]	0.173692	4.17982
Modulus of Subgrade Reaction (Total) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Immediate) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Consolidation) [ksf/ft]	0	0
Total Strain	0	0.0563295
Pore Water Pressure [ksf]	0	2.43803
Excess Pore Water Pressure [ksf]	0	0.0110821
Degree of Consolidation [%]	0	99.9709
Pre-consolidation Stress [ksf]	0.272	1.73056
Over-consolidation Ratio	1	2.59287
Void Ratio	0	3.37049
Permeability [in/y]	0	53.1409
Coefficient of Consolidation [in ² /y]	0	1051
Hydroconsolidation Settlement [in]	0	0
Average Degree of Consolidation [%]	0	0
Undrained Shear Strength	0	0.00465092

Stage: Stage 14 = 3650 d

Data Type	Minimum	Maximum
Total Settlement [in]	0	3.29823
Total Consolidation Settlement [in]	0	3.29823
Virgin Consolidation Settlement [in]	0	2.03393
Recompression Consolidation Settlement [in]	0	1.26429
Immediate Settlement [in]	0	0
Secondary Settlement [in]	0	0
Loading Stress ZZ [ksf]	0.0826902	0.103576
Loading Stress XX [ksf]	0.0103871	0.0701154
Loading Stress YY [ksf]	0.0103871	0.0701154
Effective Stress ZZ [ksf]	0.103576	1.7314
Effective Stress XX [ksf]	0.173692	1.74179
Effective Stress YY [ksf]	0.173692	1.74179
Total Stress ZZ [ksf]	0.103576	4.16944
Total Stress XX [ksf]	0.173692	4.17982
Total Stress YY [ksf]	0.173692	4.17982
Modulus of Subgrade Reaction (Total) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Immediate) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Consolidation) [ksf/ft]	0	0
Total Strain	0	0.0563295
Pore Water Pressure [ksf]	0	2.43803
Excess Pore Water Pressure [ksf]	-5.21541e-26	0.00227648
Degree of Consolidation [%]	0	99.994
Pre-consolidation Stress [ksf]	0.272	1.73056
Over-consolidation Ratio	1	2.59287
Void Ratio	0	3.37002
Permeability [in/y]	0	53.1409
Coefficient of Consolidation [in ² /y]	0	1051
Hydroconsolidation Settlement [in]	0	0
Average Degree of Consolidation [%]	0	0
Undrained Shear Strength	0	0.00474924

Stage: Stage 15 = 7300 d

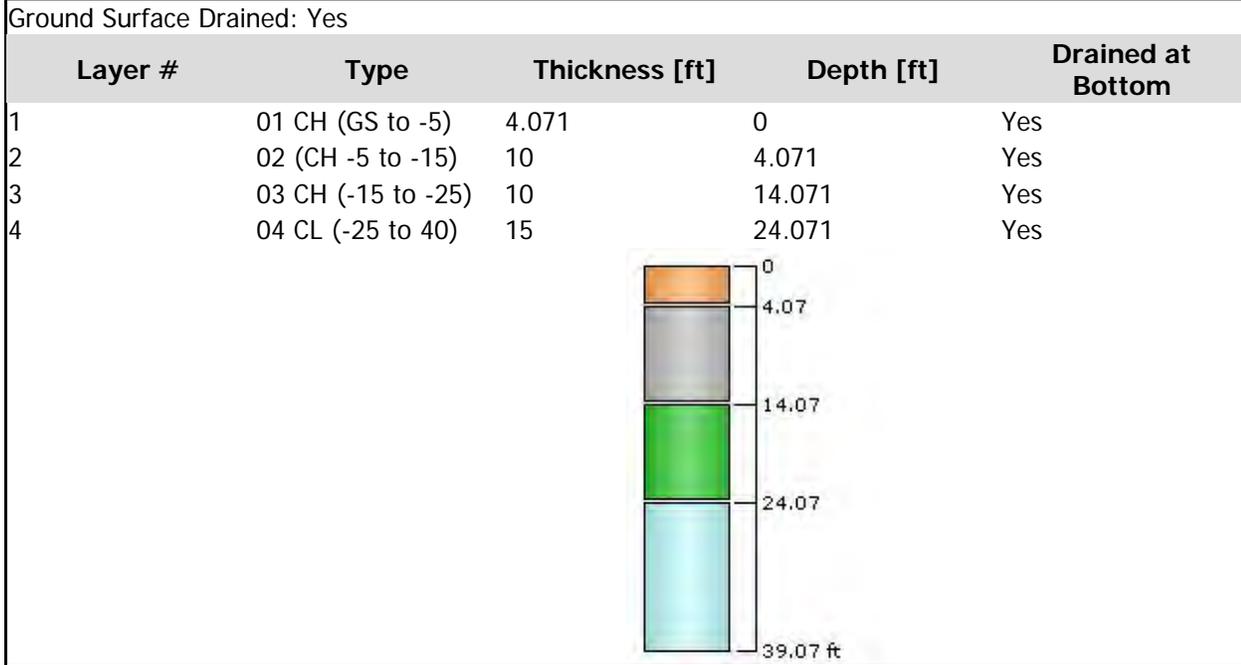
Data Type	Minimum	Maximum
Total Settlement [in]	0	3.32143
Total Consolidation Settlement [in]	0	3.32143
Virgin Consolidation Settlement [in]	0	2.05608
Recompression Consolidation Settlement [in]	0	1.26535
Immediate Settlement [in]	0	0
Secondary Settlement [in]	0	0
Loading Stress ZZ [ksf]	0.0826902	0.103576
Loading Stress XX [ksf]	0.0103871	0.0701154
Loading Stress YY [ksf]	0.0103871	0.0701154
Effective Stress ZZ [ksf]	0.103576	1.7314
Effective Stress XX [ksf]	0.173692	1.74179
Effective Stress YY [ksf]	0.173692	1.74179
Total Stress ZZ [ksf]	0.103576	4.16944
Total Stress XX [ksf]	0.173692	4.17982
Total Stress YY [ksf]	0.173692	4.17982
Modulus of Subgrade Reaction (Total) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Immediate) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Consolidation) [ksf/ft]	0	0
Total Strain	0	0.0563295
Pore Water Pressure [ksf]	0	2.43803
Excess Pore Water Pressure [ksf]	-8.85575e-26	4.34334e-05
Degree of Consolidation [%]	0	99.9999
Pre-consolidation Stress [ksf]	0.272	1.73056
Over-consolidation Ratio	1	2.59287
Void Ratio	0	3.3699
Permeability [in/y]	0	53.1409
Coefficient of Consolidation [in ² /y]	0	1051
Hydroconsolidation Settlement [in]	0	0
Average Degree of Consolidation [%]	0	0
Undrained Shear Strength	0	0.004757

Embankments

1. Embankment: "Marsh Fill +3.5"

Label	Marsh Fill +3.5						
Center Line	(-50, 50) to (50, 50)						
Near End Angle	90 degrees						
Far End Angle	90 degrees						
Number of Layers	2						
Base Width	100						
Layer	Stage	Left Bench Width (ft)	Left Angle (deg)	Height (ft)	Unit Weight (kips/ft3)	Right Angle (deg)	Right Bench Width (ft)
1	Stage 1 = 0 d	0	90	1.639	0.022	90	0
2	Stage 1 = 0 d	0	90	0.8	0.0844	90	0

Soil Layers



Soil Properties

Property	01 CH (GS to - 5)	02 (CH -5 to - 15)	03 CH (-15 to - 25)	04 CL (-25 to 40)
Color				
Unit Weight [kips/ft3]	0.095	0.095	0.095	0.12
Saturated Unit Weight [kips/ft3]	0.095	0.095	0.095	0.12
K0	1	1	1	1
Primary Consolidation	Enabled	Enabled	Enabled	Disabled
Material Type	Non-Linear	Non-Linear	Non-Linear	
Cc	1.19	1.19	1.19	-
Cr	0.13	0.13	0.13	-
e0	3.38	3.38	3.38	-
Pc [ksf]	0.272	0.408	0.654	-
Cv [in2/y]	1051	1051	1051	-
Cvr [in2/y]	1051	1051	1051	-
B-bar	1	1	1	-
Undrained Su A [kips/ft2]	0	0	0	0
Undrained Su S	0.2	0.2	0.2	0.2
Undrained Su m	0.8	0.8	0.8	0.8
Piezo Line ID	1	1	1	1

Groundwater

Groundwater method
Water Unit Weight

Piezometric Lines
0.0624 kips/ft³

Piezometric Line Entities

ID	Depth (ft)
1	0 ft

Query

Query Points

Point #	Query Point Name	(X,Y) Location	Number of Divisions
1	Query Point 1	0, 50	Auto: 65

Filename: 344.2% moisture slurry

Initial Mudline El. (ft) -0.929 Subsidence (4.3mm/yr) -0.01410761 ft/yr
 Initial CMFE (ft) 1.52 Accretion (2.5mm/yr) 0.0082021 ft/yr, begins at year 6
 Initial Marsh Thickness (ft) 2.45

	(a)	(b)	(c)	(d)	(e)	(f)	(g)	(h)
		Settle3	Mudline		PSDDF		Final MFE +	Final MFE + Subsidence +
Time (days)	Time (years)	Settlement (in)	El. (ft)	MFE (ft)	Settlement	Final MFE (ft)	Subsidence (ft)	Accretion (ft)
0.00	0.00	0.00	-0.93	1.52		0.00	0.00	0.00
0.13	0.00	0.07	-0.94	1.51		1.51	1.51	1.51
0.33	0.00	0.10	-0.94	1.51		1.51	1.51	1.51
0.63	0.00	0.12	-0.94	1.51		1.51	1.51	1.51
1.08	0.00	0.15	-0.94	1.51		1.51	1.51	1.51
1.76	0.00	0.18	-0.94	1.50		1.50	1.50	1.50
2.77	0.01	0.21	-0.95	1.50		1.50	1.50	1.50
4.29	0.01	0.25	-0.95	1.50		1.50	1.50	1.50
6.57	0.02	0.29	-0.95	1.50		1.50	1.50	1.50
9.99	0.03	0.33	-0.96	1.49		1.49	1.49	1.49
15.00	0.04	0.37	-0.96	1.49	0.04	1.45	1.45	1.45
20.28	0.06	0.40	-0.96	1.49		1.49	1.49	1.49
30.00	0.08	0.45	-0.97	1.48	0.08	1.41	1.41	1.41
38.10	0.10	0.48	-0.97	1.48		1.48	1.48	1.48
50.26	0.14	0.52	-0.97	1.48		1.48	1.47	1.47
60.00	0.16	0.55	-0.98	1.47	0.14	1.33	1.33	1.33
79.49	0.22	0.60	-0.98	1.47		1.47	1.47	1.47
90.00	0.25	0.62	-0.98	1.47	0.20	1.27	1.27	1.27
120.00	0.33	0.67	-0.98	1.46	0.44	1.02	1.02	1.02
150.00	0.41	0.71	-0.99	1.46	0.62	0.84	0.83	0.83
180.00	0.49	0.74	-0.99	1.46	0.84	0.62	0.62	0.62
213.33	0.58	0.77	-0.99	1.46		1.46	1.45	1.45
270.00	0.74	0.82	-1.00	1.45	0.89	0.56	0.55	0.55
321.52	0.88	0.86	-1.00	1.45		1.45	1.44	1.44
365.00	1.00	0.89	-1.00	1.45	0.90	0.55	0.53	0.53
444.06	1.22	0.93	-1.01	1.44		1.44	1.43	1.43
562.66	1.54	0.98	-1.01	1.44		1.44	1.42	1.42
730.00	2.00	1.03	-1.01	1.43	0.91	0.53	0.50	0.50
915.94	2.51	1.06	-1.02	1.43		1.43	1.40	1.40
1095.00	3.00	1.08	-1.02	1.43	0.91	0.52	0.48	0.48
1393.44	3.82	1.10	-1.02	1.43		1.43	1.37	1.37
1841.10	5.04	1.12	-1.02	1.43		1.43	1.36	1.36
2190.00	6.00	1.12	-1.02	1.43	0.91	0.52	0.43	0.43
2887.79	7.91	1.12	-1.02	1.43		1.43	1.31	1.33
3650.00	10.00	1.13	-1.02	1.43	0.91	0.52	0.38	0.41
4738.87	12.98	1.13	-1.02	1.43		1.43	1.24	1.30
6372.17	17.46	1.13	-1.02	1.43		1.43	1.18	1.27
7300.00	20.00	1.13	-1.02	1.43	0.91	0.52	0.23	0.35

Fill EI = +1.5 ft

PSDDF Output asjusted to
remove 1st 25 days

0	0
15	0.038
30	0.075
60	0.142
90	0.199
120	0.44
150	0.624
180	0.836
270	0.889
365	0.9
730	0.908
1095	0.91
2190	0.91
3650	0.91
7300	0.91

 Consolidation and desiccation of soft layers---dredged fill

Problem Grand Chenier - MC Target 340 MF+1.5 25 days

*****Soil data for dredged fill*****

Material Type	Specific Gravity	Ca/Cc	Cr/Cc	Saturation Limit	Disiccation Limit	Max. Crust Depth	Saturation at DL
1	2.677	0.035	0.064	5.144	2.260	0.831	0.355

Material type : 1

I	Ratio	Stress	Perm-	k/1+e	PK	Beta	Dsde	Alpha
1	7.970	0.000E+00	0.139E-01	0.155E-02	0.118E-02	-0.345E+01	-0.534E-02	
2	7.390	0.200E+01	0.725E-02	0.864E-03	0.849E-03	-0.370E+01	-0.320E-02	
3	6.620	0.500E+01	0.307E-02	0.403E-03	0.472E-03	-0.593E+01	-0.239E-02	
4	6.040	0.100E+02	0.160E-02	0.227E-03	0.236E-03	-0.129E+02	-0.294E-02	
5	5.460	0.200E+02	0.835E-03	0.129E-03	0.148E-03	-0.220E+02	-0.284E-02	
6	5.130	0.300E+02	0.570E-03	0.930E-04	0.953E-04	-0.345E+02	-0.321E-02	
7	4.880	0.400E+02	0.435E-03	0.740E-04	0.604E-04	-0.602E+02	-0.446E-02	
8	4.300	0.800E+02	0.227E-03	0.428E-04	0.422E-04	-0.103E+03	-0.443E-02	
9	3.720	0.160E+03	0.118E-03	0.250E-04	0.241E-04	-0.207E+03	-0.517E-02	
10	3.140	0.320E+03	0.618E-04	0.149E-04	0.138E-04	-0.414E+03	-0.618E-02	
11	2.560	0.640E+03	0.322E-04	0.904E-05	0.101E-04	-0.552E+03	-0.499E-02	

Summary of lifts and print detail

Time days	Material Type	Fill Height	# Sub-layers	Void ratio	Start Day	Dessic. Month	Print detail
0.	1	0.1	5	7.97	115.	5	1
6.	1	0.9	40	7.97	115.	5	1

12.	1	0.5	40	7.97	115.	5	1
18.	1	0.5	40	7.97	115.	5	1
24.	1	0.5	40	7.97	115.	5	1
25.				115.	5	1	
40.				115.	5	1	
55.				115.	5	1	
85.				115.	5	1	
115.				115.	5	1	
145.				115.	5	1	
175.				115.	5	1	
205.				115.	5	1	
295.				115.	5	1	
390.				115.	5	1	
755.				115.	5	1	
1120.				115.	5	1	
2215.				115.	5	1	
3675.				115.	5	1	
7325.				115.	5	1	

Summary of monthly rainfall and evaporation potential

Month	Rainfall	Evaporation
1	0.470	0.140
2	0.270	0.180
3	0.280	0.290
4	0.390	0.380
5	0.370	0.490
6	0.490	0.510
7	0.580	0.510
8	0.590	0.480
9	0.500	0.370
10	0.310	0.310
11	0.360	0.180
12	0.330	0.140

*****Calculation data*****

tau	Lower layer Void ratio	Lower layer Permeability	drainage path Length
.971E-02	3.380	0.10000E-05	z = 1.14

Summary of desiccation parameters

Parameter	Value
Surface Drainage Efficiency	0.80
maximum evaporation efficiency	0.75
time to desic. after initial fill	115.00
month of initial desiccation	5
elevation of fixed water table	0.71
elevation of top of incompres. found.	-0.93

*****Initial Conditions in Dredged Fill*****

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
0.10	0.10	0.01	7.97	7.97	7.97	1
0.08	0.08	0.01	7.97	7.97	7.90	1
0.06	0.06	0.01	7.97	7.97	7.83	1
0.04	0.04	0.00	7.97	7.97	7.77	1
0.02	0.02	0.00	7.97	7.97	7.70	1
0.00	0.00	0.00	7.97	7.97	7.63	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
0.10	96.03	0.00	96.03	96.03	0.00	1
0.08	97.51	0.00	97.51	97.28	0.23	1
0.06	99.00	0.00	99.00	98.53	0.47	1
0.04	100.48	0.00	100.48	99.78	0.70	1
0.02	101.96	0.00	101.96	101.03	0.93	1
0.00	103.44	0.00	103.44	102.27	1.17	1

Time = 0. Degree of Consolidation = 0.0%

Total Settlement = 0.000

Settlement at End of Primary Consolidation = 0.002

Settlement caused by Primary Consolidation at time 0. = 0.000

Settlement caused by Secondary Compression at time 0. = 0.000

*****Current Conditions in Dredged Fill*****

***** Coordinates ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
0.10	0.10	0.01	7.97	7.97	7.97	1
0.08	0.08	0.01	7.97	7.90	7.90	1
0.06	0.06	0.01	7.97	7.84	7.83	1
0.04	0.04	0.00	7.97	7.77	7.77	1
0.02	0.02	0.00	7.97	7.71	7.70	1
0.00	0.00	0.00	7.97	7.64	7.63	1

***** Stresses ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
0.10	96.15	0.00	96.15	96.15	0.00	1
0.08	97.62	0.23	97.40	97.39	0.01	1
0.06	99.09	0.45	98.64	98.62	0.02	1
0.04	100.55	0.68	99.87	99.85	0.02	1
0.02	102.00	0.90	101.10	101.07	0.03	1
0.00	103.44	1.12	102.32	102.27	0.04	1

Time = 6. Degree of Consolidation = 97.0%

Total Settlement = 0.002

Settlement at End of Primary Consolidation = 0.002

Settlement caused by Primary Consolidation at time 6. = 0.002

Settlement caused by Secondary Compression at time 6. = 0.000

Surface Elevation = -0.83

*****Current Conditions in Dredged Fill*****

***** Coordinates *****

***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
1.00	0.98	0.11	7.97	7.97	7.97	1
0.98	0.96	0.11	7.97	7.97	7.89	1
0.95	0.94	0.11	7.97	7.97	7.82	1
0.93	0.92	0.10	7.97	7.97	7.74	1
0.91	0.89	0.10	7.97	7.97	7.67	1
0.89	0.87	0.10	7.97	7.97	7.59	1
0.86	0.85	0.10	7.97	7.97	7.51	1
0.84	0.83	0.09	7.97	7.97	7.44	1
0.82	0.80	0.09	7.97	7.97	7.36	1
0.80	0.78	0.09	7.97	7.96	7.30	1
0.77	0.76	0.09	7.97	7.96	7.23	1
0.75	0.74	0.08	7.97	7.96	7.16	1
0.73	0.71	0.08	7.97	7.96	7.09	1
0.71	0.69	0.08	7.97	7.96	7.03	1
0.68	0.67	0.08	7.97	7.95	6.96	1
0.66	0.65	0.07	7.97	7.95	6.89	1
0.64	0.62	0.07	7.97	7.95	6.83	1
0.62	0.60	0.07	7.97	7.94	6.76	1
0.59	0.58	0.07	7.97	7.94	6.69	1
0.57	0.56	0.06	7.97	7.93	6.62	1
0.55	0.53	0.06	7.97	7.93	6.59	1
0.53	0.51	0.06	7.97	7.92	6.56	1
0.51	0.49	0.06	7.97	7.91	6.53	1
0.48	0.47	0.05	7.97	7.90	6.50	1
0.46	0.44	0.05	7.97	7.89	6.47	1
0.44	0.42	0.05	7.97	7.88	6.44	1
0.42	0.40	0.05	7.97	7.87	6.41	1
0.39	0.38	0.04	7.97	7.86	6.38	1
0.37	0.35	0.04	7.97	7.84	6.35	1
0.35	0.33	0.04	7.97	7.82	6.32	1
0.33	0.31	0.04	7.97	7.80	6.29	1
0.30	0.29	0.03	7.97	7.78	6.26	1
0.28	0.27	0.03	7.97	7.76	6.23	1
0.26	0.24	0.03	7.97	7.73	6.20	1
0.23	0.22	0.03	7.97	7.71	6.16	1
0.21	0.20	0.02	7.97	7.68	6.13	1
0.19	0.18	0.02	7.97	7.64	6.10	1
0.17	0.16	0.02	7.97	7.61	6.07	1
0.14	0.14	0.02	7.97	7.57	6.04	1
0.12	0.11	0.01	7.97	7.52	6.03	1
0.10	0.09	0.01	7.97	7.48	6.01	1
0.10	0.09	0.01	7.97	7.48	6.01	1
0.08	0.07	0.01	7.97	7.43	6.00	1
0.06	0.06	0.01	7.97	7.39	5.98	1
0.04	0.04	0.00	7.97	7.34	5.97	1
0.02	0.02	0.00	7.97	7.29	5.96	1
0.00	0.00	0.00	7.97	7.23	5.94	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
0.98	40.96	0.00	40.96	40.96	0.00	1
0.96	42.63	0.00	42.63	42.36	0.26	1
0.94	44.29	0.00	44.29	43.77	0.52	1
0.92	45.96	0.00	45.96	45.17	0.78	1
0.89	47.63	0.01	47.62	46.58	1.04	1
0.87	49.29	0.01	49.28	47.98	1.30	1
0.85	50.96	0.01	50.95	49.38	1.56	1
0.83	52.62	0.01	52.61	50.79	1.82	1
0.80	54.29	0.02	54.27	52.19	2.08	1
0.78	55.96	0.02	55.94	53.59	2.34	1
0.76	57.62	0.02	57.60	55.00	2.60	1
0.74	59.29	0.03	59.26	56.40	2.86	1
0.71	60.95	0.04	60.92	57.80	3.11	1
0.69	62.62	0.04	62.57	59.20	3.37	1
0.67	64.28	0.05	64.23	60.61	3.62	1
0.65	65.94	0.06	65.88	62.01	3.87	1
0.62	67.61	0.08	67.53	63.41	4.12	1
0.60	69.27	0.09	69.18	64.81	4.37	1
0.58	70.93	0.11	70.83	66.21	4.62	1
0.56	72.59	0.12	72.47	67.61	4.86	1
0.53	74.25	0.15	74.11	69.00	5.10	1
0.51	75.91	0.17	75.74	70.40	5.34	1
0.49	77.57	0.20	77.37	71.80	5.58	1
0.47	79.23	0.23	79.00	73.19	5.81	1
0.44	80.88	0.26	80.62	74.58	6.04	1
0.42	82.54	0.30	82.23	75.97	6.26	1
0.40	84.19	0.35	83.84	77.36	6.48	1
0.38	85.84	0.40	85.44	78.75	6.69	1
0.35	87.49	0.45	87.04	80.14	6.90	1
0.33	89.13	0.51	88.62	81.52	7.10	1
0.31	90.77	0.58	90.20	82.90	7.30	1
0.29	92.41	0.65	91.76	84.27	7.49	1
0.27	94.05	0.73	93.32	85.65	7.67	1
0.24	95.68	0.82	94.86	87.02	7.85	1
0.22	97.30	0.91	96.39	88.38	8.01	1
0.20	98.93	1.02	97.91	89.74	8.17	1
0.18	100.55	1.13	99.41	91.10	8.32	1
0.16	102.16	1.26	100.90	92.45	8.46	1
0.14	103.76	1.39	102.37	93.79	8.58	1
0.11	105.36	1.54	103.82	95.13	8.70	1
0.09	106.96	1.70	105.26	96.46	8.80	1
0.09	106.96	1.70	105.26	96.46	8.80	1
0.07	108.37	1.85	106.52	97.63	8.89	1
0.06	109.77	2.01	107.76	98.80	8.96	1
0.04	111.17	2.20	108.97	99.97	9.00	1
0.02	112.56	2.40	110.15	101.12	9.03	1
0.00	113.94	2.62	111.32	102.27	9.05	1

Time = 12. Degree of Consolidation = 12.0%

Total Settlement = 0.017

Settlement at End of Primary Consolidation = 0.143

Settlement caused by Primary Consolidation at time 12. = 0.017

Settlement caused by Secondary Compression at time 12. = 0.000

Surface Elevation = 0.05

*****Current Conditions in Dredged Fill*****

***** Coordinates *****

***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
1.50	1.47	0.17	7.97	7.97	7.97	1
1.49	1.46	0.17	7.97	7.97	7.93	1
1.47	1.44	0.16	7.97	7.97	7.89	1
1.46	1.43	0.16	7.97	7.97	7.84	1
1.45	1.42	0.16	7.97	7.97	7.80	1
1.44	1.41	0.16	7.97	7.97	7.76	1
1.42	1.39	0.16	7.97	7.97	7.72	1
1.41	1.38	0.16	7.97	7.97	7.67	1
1.40	1.37	0.16	7.97	7.97	7.63	1
1.39	1.36	0.15	7.97	7.97	7.59	1
1.37	1.34	0.15	7.97	7.97	7.55	1
1.36	1.33	0.15	7.97	7.97	7.50	1
1.35	1.32	0.15	7.97	7.97	7.46	1
1.34	1.31	0.15	7.97	7.97	7.42	1
1.32	1.29	0.15	7.97	7.97	7.38	1
1.31	1.28	0.15	7.97	7.97	7.34	1
1.30	1.27	0.14	7.97	7.97	7.30	1
1.29	1.26	0.14	7.97	7.97	7.27	1
1.27	1.24	0.14	7.97	7.97	7.23	1
1.26	1.23	0.14	7.97	7.97	7.19	1
1.25	1.22	0.14	7.97	7.97	7.15	1
1.24	1.21	0.14	7.97	7.97	7.12	1
1.22	1.19	0.14	7.97	7.97	7.08	1
1.21	1.18	0.14	7.97	7.97	7.04	1
1.20	1.17	0.13	7.97	7.96	7.01	1
1.19	1.16	0.13	7.97	7.96	6.97	1
1.17	1.14	0.13	7.97	7.96	6.93	1
1.16	1.13	0.13	7.97	7.96	6.89	1
1.15	1.12	0.13	7.97	7.96	6.86	1
1.14	1.11	0.13	7.97	7.96	6.82	1
1.12	1.09	0.13	7.97	7.96	6.78	1
1.11	1.08	0.12	7.97	7.96	6.74	1
1.10	1.07	0.12	7.97	7.96	6.71	1
1.09	1.06	0.12	7.97	7.96	6.67	1

1.07	1.04	0.12	7.97	7.96	6.63	1
1.06	1.03	0.12	7.97	7.96	6.61	1
1.05	1.02	0.12	7.97	7.96	6.59	1
1.04	1.01	0.12	7.97	7.96	6.57	1
1.02	0.99	0.11	7.97	7.95	6.56	1
1.01	0.98	0.11	7.97	7.95	6.54	1
1.00	0.97	0.11	7.97	7.95	6.52	1
1.00	0.97	0.11	7.97	7.95	6.52	1
0.98	0.95	0.11	7.97	7.95	6.49	1
0.95	0.92	0.11	7.97	7.95	6.46	1
0.93	0.90	0.10	7.97	7.94	6.43	1
0.91	0.88	0.10	7.97	7.94	6.40	1
0.89	0.86	0.10	7.97	7.94	6.37	1
0.86	0.83	0.10	7.97	7.93	6.34	1
0.84	0.81	0.09	7.97	7.93	6.31	1
0.82	0.79	0.09	7.97	7.92	6.28	1
0.80	0.77	0.09	7.97	7.92	6.25	1
0.77	0.74	0.09	7.97	7.91	6.22	1
0.75	0.72	0.08	7.97	7.90	6.19	1
0.73	0.70	0.08	7.97	7.90	6.16	1
0.71	0.68	0.08	7.97	7.89	6.13	1
0.68	0.65	0.08	7.97	7.88	6.10	1
0.66	0.63	0.07	7.97	7.87	6.07	1
0.64	0.61	0.07	7.97	7.86	6.04	1
0.62	0.59	0.07	7.97	7.85	6.02	1
0.59	0.57	0.07	7.97	7.84	6.01	1
0.57	0.54	0.06	7.97	7.83	5.99	1
0.55	0.52	0.06	7.97	7.81	5.98	1
0.53	0.50	0.06	7.97	7.80	5.96	1
0.51	0.48	0.06	7.97	7.78	5.95	1
0.48	0.46	0.05	7.97	7.77	5.93	1
0.46	0.43	0.05	7.97	7.75	5.92	1
0.44	0.41	0.05	7.97	7.73	5.90	1
0.42	0.39	0.05	7.97	7.71	5.89	1
0.39	0.37	0.04	7.97	7.69	5.87	1
0.37	0.35	0.04	7.97	7.67	5.86	1
0.35	0.32	0.04	7.97	7.64	5.84	1
0.33	0.30	0.04	7.97	7.61	5.82	1
0.30	0.28	0.03	7.97	7.59	5.81	1
0.28	0.26	0.03	7.97	7.56	5.79	1
0.26	0.24	0.03	7.97	7.53	5.78	1
0.23	0.22	0.03	7.97	7.49	5.76	1
0.21	0.20	0.02	7.97	7.45	5.75	1
0.19	0.17	0.02	7.97	7.42	5.73	1
0.17	0.15	0.02	7.97	7.37	5.72	1
0.14	0.13	0.02	7.97	7.33	5.70	1
0.12	0.11	0.01	7.97	7.28	5.69	1
0.10	0.09	0.01	7.97	7.24	5.67	1
0.10	0.09	0.01	7.97	7.24	5.67	1
0.08	0.07	0.01	7.97	7.19	5.66	1
0.06	0.05	0.01	7.97	7.15	5.65	1
0.04	0.04	0.00	7.97	7.11	5.63	1
0.02	0.02	0.00	7.97	7.06	5.62	1
0.00	0.00	0.00	7.97	7.01	5.61	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
1.47	10.70	0.00	10.70	10.70	0.00	1
1.46	11.62	0.00	11.62	11.48	0.15	1
1.44	12.55	0.00	12.55	12.26	0.29	1
1.43	13.48	0.00	13.48	13.04	0.44	1
1.42	14.40	0.00	14.40	13.82	0.58	1
1.41	15.33	0.00	15.33	14.60	0.73	1
1.39	16.25	0.00	16.25	15.38	0.87	1
1.38	17.18	0.00	17.18	16.16	1.02	1
1.37	18.11	0.00	18.10	16.94	1.16	1
1.36	19.03	0.00	19.03	17.72	1.31	1
1.34	19.96	0.00	19.95	18.50	1.45	1
1.33	20.88	0.01	20.88	19.28	1.60	1
1.32	21.81	0.01	21.80	20.06	1.74	1
1.31	22.73	0.01	22.73	20.84	1.89	1
1.29	23.66	0.01	23.65	21.62	2.03	1
1.28	24.59	0.01	24.58	22.40	2.18	1
1.27	25.51	0.01	25.50	23.18	2.32	1
1.26	26.44	0.01	26.43	23.96	2.47	1
1.24	27.36	0.01	27.35	24.74	2.61	1
1.23	28.29	0.01	28.28	25.52	2.76	1
1.22	29.21	0.01	29.20	26.30	2.90	1
1.21	30.14	0.01	30.12	27.08	3.05	1
1.19	31.06	0.02	31.05	27.86	3.19	1
1.18	31.99	0.02	31.97	28.64	3.34	1
1.17	32.91	0.02	32.90	29.42	3.48	1
1.16	33.84	0.02	33.82	30.19	3.63	1
1.14	34.77	0.02	34.74	30.97	3.77	1
1.13	35.69	0.02	35.67	31.75	3.91	1
1.12	36.62	0.03	36.59	32.53	4.06	1
1.11	37.54	0.03	37.51	33.31	4.20	1
1.09	38.47	0.03	38.44	34.09	4.35	1
1.08	39.39	0.03	39.36	34.87	4.49	1
1.07	40.32	0.03	40.28	35.65	4.63	1
1.06	41.24	0.04	41.20	36.43	4.77	1
1.04	42.17	0.04	42.13	37.21	4.92	1
1.03	43.09	0.04	43.05	37.99	5.06	1
1.02	44.02	0.05	43.97	38.77	5.20	1
1.01	44.94	0.05	44.89	39.54	5.34	1
0.99	45.86	0.05	45.81	40.32	5.49	1
0.98	46.79	0.06	46.73	41.10	5.63	1
0.97	47.71	0.06	47.65	41.88	5.77	1
0.97	47.71	0.06	47.65	41.88	5.77	1
0.95	49.38	0.07	49.30	43.28	6.02	1
0.92	51.04	0.08	50.96	44.68	6.28	1
0.90	52.70	0.09	52.61	46.08	6.53	1
0.88	54.36	0.10	54.26	47.48	6.78	1
0.86	56.03	0.12	55.91	48.88	7.03	1
0.83	57.69	0.13	57.56	50.28	7.28	1
0.81	59.35	0.15	59.20	51.68	7.52	1

0.79	61.01	0.16	60.84	53.07	7.77	1
0.77	62.67	0.18	62.48	54.47	8.01	1
0.74	64.32	0.20	64.12	55.86	8.25	1
0.72	65.98	0.23	65.75	57.26	8.49	1
0.70	67.64	0.25	67.38	58.65	8.73	1
0.68	69.29	0.28	69.01	60.04	8.97	1
0.65	70.94	0.31	70.64	61.44	9.20	1
0.63	72.59	0.34	72.26	62.82	9.43	1
0.61	74.25	0.37	73.87	64.21	9.66	1
0.59	75.89	0.41	75.48	65.60	9.88	1
0.57	77.54	0.45	77.09	66.98	10.11	1
0.54	79.19	0.49	78.69	68.37	10.33	1
0.52	80.83	0.54	80.29	69.75	10.54	1
0.50	82.47	0.59	81.88	71.12	10.76	1
0.48	84.11	0.64	83.46	72.50	10.96	1
0.46	85.74	0.70	85.04	73.87	11.17	1
0.43	87.38	0.76	86.62	75.24	11.37	1
0.41	89.01	0.83	88.18	76.61	11.57	1
0.39	90.64	0.90	89.74	77.98	11.76	1
0.37	92.26	0.97	91.29	79.34	11.95	1
0.35	93.88	1.05	92.83	80.70	12.13	1
0.32	95.50	1.14	94.36	82.05	12.31	1
0.30	97.11	1.23	95.88	83.40	12.48	1
0.28	98.72	1.32	97.40	84.75	12.65	1
0.26	100.32	1.42	98.90	86.09	12.81	1
0.24	101.92	1.53	100.39	87.43	12.96	1
0.22	103.52	1.65	101.86	88.76	13.11	1
0.20	105.10	1.78	103.33	90.08	13.24	1
0.17	106.69	1.91	104.78	91.41	13.37	1
0.15	108.26	2.06	106.20	92.72	13.48	1
0.13	109.83	2.23	107.60	94.03	13.57	1
0.11	111.40	2.41	108.99	95.33	13.66	1
0.09	112.95	2.60	110.36	96.62	13.74	1
0.09	112.95	2.60	110.36	96.62	13.74	1
0.07	114.33	2.76	111.57	97.76	13.81	1
0.05	115.70	2.93	112.77	98.90	13.87	1
0.04	117.06	3.11	113.96	100.03	13.93	1
0.02	118.42	3.29	115.13	101.16	13.98	1
0.00	119.77	3.47	116.30	102.27	14.02	1

Time = 18. Degree of Consolidation = 12.0%

Total Settlement = 0.032

Settlement at End of Primary Consolidation = 0.265

Settlement caused by Primary Consolidation at time 18. = 0.032

Settlement caused by Secondary Compression at time 18. = 0.000

Surface Elevation = 0.54

*****Current Conditions in Dredged Fill*****

***** Coordinates *****

***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
2.00	1.95	0.22	7.97	7.97	7.97	1
1.99	1.94	0.22	7.97	7.97	7.93	1
1.97	1.93	0.22	7.97	7.97	7.89	1
1.96	1.92	0.22	7.97	7.97	7.84	1
1.95	1.90	0.22	7.97	7.97	7.80	1
1.94	1.89	0.22	7.97	7.97	7.76	1
1.92	1.88	0.21	7.97	7.97	7.72	1
1.91	1.87	0.21	7.97	7.97	7.67	1
1.90	1.85	0.21	7.97	7.97	7.63	1
1.89	1.84	0.21	7.97	7.97	7.59	1
1.87	1.83	0.21	7.97	7.97	7.55	1
1.86	1.82	0.21	7.97	7.97	7.50	1
1.85	1.80	0.21	7.97	7.97	7.46	1
1.84	1.79	0.20	7.97	7.97	7.42	1
1.82	1.78	0.20	7.97	7.97	7.38	1
1.81	1.77	0.20	7.97	7.97	7.34	1
1.80	1.75	0.20	7.97	7.97	7.30	1
1.79	1.74	0.20	7.97	7.97	7.27	1
1.77	1.73	0.20	7.97	7.97	7.23	1
1.76	1.72	0.20	7.97	7.97	7.19	1
1.75	1.70	0.20	7.97	7.97	7.15	1
1.74	1.69	0.19	7.97	7.97	7.12	1
1.72	1.68	0.19	7.97	7.97	7.08	1
1.71	1.67	0.19	7.97	7.97	7.04	1
1.70	1.65	0.19	7.97	7.97	7.01	1
1.69	1.64	0.19	7.97	7.97	6.97	1
1.67	1.63	0.19	7.97	7.97	6.93	1
1.66	1.62	0.19	7.97	7.97	6.89	1
1.65	1.60	0.18	7.97	7.97	6.86	1
1.64	1.59	0.18	7.97	7.97	6.82	1
1.62	1.58	0.18	7.97	7.97	6.78	1
1.61	1.57	0.18	7.97	7.97	6.74	1
1.60	1.55	0.18	7.97	7.97	6.71	1
1.59	1.54	0.18	7.97	7.97	6.67	1
1.57	1.53	0.18	7.97	7.97	6.63	1
1.56	1.52	0.17	7.97	7.97	6.61	1
1.55	1.50	0.17	7.97	7.97	6.59	1
1.54	1.49	0.17	7.97	7.97	6.57	1
1.52	1.48	0.17	7.97	7.96	6.56	1
1.51	1.47	0.17	7.97	7.96	6.54	1
1.50	1.45	0.17	7.97	7.96	6.52	1
1.50	1.45	0.17	7.97	7.96	6.52	1
1.49	1.44	0.17	7.97	7.96	6.51	1
1.47	1.43	0.16	7.97	7.96	6.49	1
1.46	1.42	0.16	7.97	7.96	6.47	1
1.45	1.40	0.16	7.97	7.96	6.46	1

1.44	1.39	0.16	7.97	7.96	6.44	1
1.42	1.38	0.16	7.97	7.96	6.42	1
1.41	1.37	0.16	7.97	7.96	6.40	1
1.40	1.35	0.16	7.97	7.96	6.39	1
1.39	1.34	0.15	7.97	7.96	6.37	1
1.37	1.33	0.15	7.97	7.96	6.35	1
1.36	1.32	0.15	7.97	7.96	6.34	1
1.35	1.30	0.15	7.97	7.96	6.32	1
1.34	1.29	0.15	7.97	7.96	6.30	1
1.32	1.28	0.15	7.97	7.95	6.29	1
1.31	1.27	0.15	7.97	7.95	6.27	1
1.30	1.25	0.14	7.97	7.95	6.25	1
1.29	1.24	0.14	7.97	7.95	6.24	1
1.27	1.23	0.14	7.97	7.95	6.22	1
1.26	1.22	0.14	7.97	7.95	6.20	1
1.25	1.20	0.14	7.97	7.95	6.19	1
1.24	1.19	0.14	7.97	7.95	6.17	1
1.22	1.18	0.14	7.97	7.95	6.15	1
1.21	1.17	0.14	7.97	7.94	6.13	1
1.20	1.15	0.13	7.97	7.94	6.12	1
1.19	1.14	0.13	7.97	7.94	6.10	1
1.17	1.13	0.13	7.97	7.94	6.08	1
1.16	1.12	0.13	7.97	7.94	6.07	1
1.15	1.10	0.13	7.97	7.94	6.05	1
1.14	1.09	0.13	7.97	7.93	6.04	1
1.12	1.08	0.13	7.97	7.93	6.03	1
1.11	1.07	0.12	7.97	7.93	6.02	1
1.10	1.05	0.12	7.97	7.93	6.01	1
1.09	1.04	0.12	7.97	7.93	6.00	1
1.07	1.03	0.12	7.97	7.92	5.99	1
1.06	1.02	0.12	7.97	7.92	5.99	1
1.05	1.00	0.12	7.97	7.92	5.98	1
1.04	0.99	0.12	7.97	7.92	5.97	1
1.02	0.98	0.11	7.97	7.91	5.96	1
1.01	0.97	0.11	7.97	7.91	5.95	1
1.00	0.95	0.11	7.97	7.91	5.94	1
1.00	0.95	0.11	7.97	7.91	5.94	1
0.98	0.93	0.11	7.97	7.90	5.93	1
0.95	0.91	0.11	7.97	7.90	5.91	1
0.93	0.89	0.10	7.97	7.89	5.90	1
0.91	0.86	0.10	7.97	7.88	5.88	1
0.89	0.84	0.10	7.97	7.88	5.87	1
0.86	0.82	0.10	7.97	7.87	5.85	1
0.84	0.80	0.09	7.97	7.86	5.84	1
0.82	0.78	0.09	7.97	7.85	5.82	1
0.80	0.75	0.09	7.97	7.84	5.81	1
0.77	0.73	0.09	7.97	7.83	5.79	1
0.75	0.71	0.08	7.97	7.82	5.78	1
0.73	0.69	0.08	7.97	7.81	5.76	1
0.71	0.67	0.08	7.97	7.80	5.75	1
0.68	0.64	0.08	7.97	7.78	5.73	1
0.66	0.62	0.07	7.97	7.77	5.72	1
0.64	0.60	0.07	7.97	7.76	5.70	1
0.62	0.58	0.07	7.97	7.74	5.68	1

0.59	0.56	0.07	7.97	7.73	5.67	1
0.57	0.53	0.06	7.97	7.71	5.65	1
0.55	0.51	0.06	7.97	7.69	5.64	1
0.53	0.49	0.06	7.97	7.67	5.62	1
0.51	0.47	0.06	7.97	7.65	5.61	1
0.48	0.45	0.05	7.97	7.63	5.59	1
0.46	0.42	0.05	7.97	7.61	5.58	1
0.44	0.40	0.05	7.97	7.59	5.56	1
0.42	0.38	0.05	7.97	7.57	5.55	1
0.39	0.36	0.04	7.97	7.54	5.53	1
0.37	0.34	0.04	7.97	7.51	5.52	1
0.35	0.32	0.04	7.97	7.48	5.50	1
0.33	0.30	0.04	7.97	7.45	5.49	1
0.30	0.28	0.03	7.97	7.42	5.47	1
0.28	0.25	0.03	7.97	7.39	5.46	1
0.26	0.23	0.03	7.97	7.35	5.45	1
0.23	0.21	0.03	7.97	7.32	5.44	1
0.21	0.19	0.02	7.97	7.28	5.43	1
0.19	0.17	0.02	7.97	7.24	5.42	1
0.17	0.15	0.02	7.97	7.20	5.41	1
0.14	0.13	0.02	7.97	7.16	5.41	1
0.12	0.11	0.01	7.97	7.11	5.40	1
0.10	0.09	0.01	7.97	7.07	5.39	1
0.10	0.09	0.01	7.97	7.07	5.39	1
0.08	0.07	0.01	7.97	7.03	5.38	1
0.06	0.05	0.01	7.97	6.99	5.37	1
0.04	0.04	0.00	7.97	6.95	5.37	1
0.02	0.02	0.00	7.97	6.90	5.36	1
0.00	0.00	0.00	7.97	6.86	5.35	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
1.95	0.00	0.00	0.00	0.00	0.00	1
1.94	0.93	0.00	0.93	0.78	0.15	1
1.93	1.85	0.00	1.85	1.56	0.29	1
1.92	2.78	0.00	2.78	2.34	0.44	1
1.90	3.70	0.00	3.70	3.12	0.58	1
1.89	4.63	0.00	4.63	3.90	0.73	1
1.88	5.55	0.00	5.55	4.68	0.87	1
1.87	6.48	0.00	6.48	5.46	1.02	1
1.85	7.41	0.00	7.41	6.24	1.17	1
1.84	8.33	0.00	8.33	7.02	1.31	1
1.83	9.26	0.00	9.26	7.80	1.46	1
1.82	10.18	0.00	10.18	8.58	1.60	1
1.80	11.11	0.00	11.11	9.36	1.75	1
1.79	12.04	0.00	12.03	10.14	1.89	1
1.78	12.96	0.00	12.96	10.92	2.04	1
1.77	13.89	0.00	13.88	11.70	2.18	1
1.75	14.81	0.00	14.81	12.48	2.33	1
1.74	15.74	0.00	15.74	13.26	2.48	1
1.73	16.66	0.00	16.66	14.04	2.62	1
1.72	17.59	0.00	17.59	14.82	2.77	1

1.70	18.52	0.00	18.51	15.60	2.91	1
1.69	19.44	0.00	19.44	16.38	3.06	1
1.68	20.37	0.01	20.36	17.16	3.20	1
1.67	21.29	0.01	21.29	17.94	3.35	1
1.65	22.22	0.01	22.21	18.72	3.49	1
1.64	23.14	0.01	23.14	19.50	3.64	1
1.63	24.07	0.01	24.06	20.28	3.78	1
1.62	25.00	0.01	24.99	21.06	3.93	1
1.60	25.92	0.01	25.91	21.84	4.07	1
1.59	26.85	0.01	26.84	22.62	4.22	1
1.58	27.77	0.01	27.76	23.40	4.36	1
1.57	28.70	0.01	28.69	24.18	4.51	1
1.55	29.62	0.01	29.61	24.96	4.65	1
1.54	30.55	0.01	30.54	25.74	4.80	1
1.53	31.47	0.01	31.46	26.52	4.94	1
1.52	32.40	0.01	32.39	27.30	5.09	1
1.50	33.33	0.02	33.31	28.08	5.23	1
1.49	34.25	0.02	34.23	28.85	5.38	1
1.48	35.18	0.02	35.16	29.63	5.52	1
1.47	36.10	0.02	36.08	30.41	5.67	1
1.45	37.03	0.02	37.01	31.19	5.81	1
1.45	37.03	0.02	37.01	31.19	5.81	1
1.44	37.95	0.02	37.93	31.97	5.96	1
1.43	38.88	0.02	38.85	32.75	6.10	1
1.42	39.80	0.03	39.78	33.53	6.24	1
1.40	40.73	0.03	40.70	34.31	6.39	1
1.39	41.65	0.03	41.62	35.09	6.53	1
1.38	42.58	0.03	42.55	35.87	6.68	1
1.37	43.50	0.03	43.47	36.65	6.82	1
1.35	44.43	0.04	44.39	37.43	6.96	1
1.34	45.35	0.04	45.31	38.21	7.11	1
1.33	46.28	0.04	46.24	38.99	7.25	1
1.32	47.20	0.04	47.16	39.76	7.39	1
1.30	48.13	0.05	48.08	40.54	7.54	1
1.29	49.05	0.05	49.00	41.32	7.68	1
1.28	49.98	0.05	49.92	42.10	7.82	1
1.27	50.90	0.06	50.85	42.88	7.97	1
1.25	51.82	0.06	51.77	43.66	8.11	1
1.24	52.75	0.06	52.69	44.44	8.25	1
1.23	53.67	0.07	53.61	45.22	8.39	1
1.22	54.60	0.07	54.53	45.99	8.53	1
1.20	55.52	0.07	55.45	46.77	8.68	1
1.19	56.45	0.08	56.37	47.55	8.82	1
1.18	57.37	0.08	57.29	48.33	8.96	1
1.17	58.29	0.09	58.20	49.11	9.10	1
1.15	59.22	0.09	59.12	49.88	9.24	1
1.14	60.14	0.10	60.04	50.66	9.38	1
1.13	61.06	0.10	60.96	51.44	9.52	1
1.12	61.99	0.11	61.88	52.22	9.66	1
1.10	62.91	0.12	62.79	52.99	9.80	1
1.09	63.83	0.12	63.71	53.77	9.94	1
1.08	64.75	0.13	64.62	54.55	10.08	1
1.07	65.68	0.14	65.54	55.32	10.22	1
1.05	66.60	0.14	66.46	56.10	10.36	1

1.04	67.52	0.15	67.37	56.88	10.49	1
1.03	68.44	0.16	68.28	57.65	10.63	1
1.02	69.37	0.17	69.20	58.43	10.77	1
1.00	70.29	0.18	70.11	59.20	10.91	1
0.99	71.21	0.19	71.02	59.98	11.04	1
0.98	72.13	0.20	71.93	60.75	11.18	1
0.97	73.05	0.21	72.84	61.53	11.32	1
0.95	73.97	0.22	73.75	62.30	11.45	1
0.95	73.97	0.22	73.75	62.30	11.45	1
0.93	75.63	0.23	75.39	63.70	11.69	1
0.91	77.28	0.25	77.03	65.09	11.94	1
0.89	78.94	0.28	78.66	66.48	12.18	1
0.86	80.59	0.30	80.29	67.87	12.42	1
0.84	82.24	0.33	81.92	69.26	12.65	1
0.82	83.89	0.35	83.54	70.65	12.89	1
0.80	85.54	0.38	85.16	72.04	13.12	1
0.78	87.19	0.41	86.78	73.43	13.35	1
0.75	88.84	0.44	88.39	74.81	13.58	1
0.73	90.48	0.48	90.01	76.19	13.81	1
0.71	92.13	0.51	91.61	77.57	14.04	1
0.69	93.77	0.55	93.22	78.95	14.26	1
0.67	95.41	0.59	94.82	80.33	14.48	1
0.64	97.05	0.64	96.41	81.71	14.70	1
0.62	98.69	0.68	98.00	83.08	14.92	1
0.60	100.32	0.73	99.59	84.45	15.13	1
0.58	101.95	0.79	101.17	85.82	15.34	1
0.56	103.58	0.84	102.74	87.19	15.55	1
0.53	105.21	0.90	104.31	88.56	15.76	1
0.51	106.83	0.96	105.88	89.92	15.96	1
0.49	108.45	1.02	107.43	91.28	16.16	1
0.47	110.07	1.09	108.98	92.63	16.35	1
0.45	111.69	1.16	110.53	93.99	16.54	1
0.42	113.30	1.23	112.07	95.34	16.73	1
0.40	114.91	1.31	113.60	96.68	16.91	1
0.38	116.51	1.40	115.12	98.02	17.09	1
0.36	118.12	1.48	116.63	99.36	17.27	1
0.34	119.71	1.58	118.14	100.70	17.44	1
0.32	121.31	1.67	119.63	102.03	17.60	1
0.30	122.89	1.78	121.12	103.35	17.76	1
0.28	124.48	1.89	122.59	104.67	17.91	1
0.25	126.06	2.01	124.05	105.99	18.06	1
0.23	127.63	2.14	125.48	107.30	18.18	1
0.21	129.19	2.29	126.91	108.60	18.30	1
0.19	130.76	2.44	128.32	109.90	18.42	1
0.17	132.31	2.59	129.72	111.20	18.53	1
0.15	133.86	2.75	131.11	112.48	18.63	1
0.13	135.40	2.91	132.49	113.76	18.73	1
0.11	136.94	3.08	133.86	115.04	18.82	1
0.09	138.47	3.25	135.21	116.30	18.91	1
0.09	138.47	3.25	135.21	116.30	18.91	1
0.07	139.82	3.41	136.41	117.42	18.99	1
0.05	141.17	3.57	137.60	118.54	19.07	1
0.04	142.51	3.73	138.78	119.64	19.14	1
0.02	143.85	3.90	139.95	120.75	19.20	1

0.00 145.18 4.07 141.11 121.84 19.26 1

Time = 24. Degree of Consolidation = 12.0%

Total Settlement = 0.047

Settlement at End of Primary Consolidation = 0.405

Settlement caused by Primary Consolidation at time 24. = 0.047

Settlement caused by Secondary Compression at time 24. = 0.000

Surface Elevation = 1.02

*****Current Conditions in Dredged Fill*****

***** Coordinates *****

***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
2.50	2.45	0.28	7.97	7.97	7.97	1
2.49	2.44	0.28	7.97	7.97	7.93	1
2.48	2.43	0.28	7.97	7.97	7.89	1
2.46	2.41	0.27	7.97	7.97	7.84	1
2.45	2.40	0.27	7.97	7.97	7.80	1
2.44	2.39	0.27	7.97	7.97	7.76	1
2.43	2.38	0.27	7.97	7.97	7.72	1
2.41	2.36	0.27	7.97	7.97	7.67	1
2.40	2.35	0.27	7.97	7.97	7.63	1
2.39	2.34	0.27	7.97	7.97	7.59	1
2.38	2.33	0.26	7.97	7.97	7.55	1
2.36	2.31	0.26	7.97	7.97	7.50	1
2.35	2.30	0.26	7.97	7.97	7.46	1
2.34	2.29	0.26	7.97	7.97	7.42	1
2.33	2.28	0.26	7.97	7.97	7.38	1
2.31	2.26	0.26	7.97	7.97	7.34	1
2.30	2.25	0.26	7.97	7.97	7.30	1
2.29	2.24	0.26	7.97	7.97	7.27	1
2.27	2.23	0.25	7.97	7.97	7.23	1
2.26	2.21	0.25	7.97	7.97	7.19	1
2.25	2.20	0.25	7.97	7.97	7.15	1
2.24	2.19	0.25	7.97	7.97	7.12	1
2.22	2.18	0.25	7.97	7.97	7.08	1
2.21	2.16	0.25	7.97	7.97	7.04	1
2.20	2.15	0.25	7.97	7.97	7.01	1
2.19	2.14	0.24	7.97	7.97	6.97	1
2.17	2.13	0.24	7.97	7.97	6.93	1
2.16	2.11	0.24	7.97	7.97	6.89	1
2.15	2.10	0.24	7.97	7.97	6.86	1
2.14	2.09	0.24	7.97	7.97	6.82	1

2.12	2.08	0.24	7.97	7.97	6.78	1
2.11	2.06	0.24	7.97	7.97	6.74	1
2.10	2.05	0.23	7.97	7.97	6.71	1
2.09	2.04	0.23	7.97	7.97	6.67	1
2.07	2.03	0.23	7.97	7.97	6.63	1
2.06	2.01	0.23	7.97	7.97	6.61	1
2.05	2.00	0.23	7.97	7.97	6.59	1
2.04	1.99	0.23	7.97	7.97	6.57	1
2.02	1.98	0.23	7.97	7.97	6.56	1
2.01	1.96	0.22	7.97	7.97	6.54	1
2.00	1.95	0.22	7.97	7.97	6.52	1
2.00	1.95	0.22	7.97	7.97	6.52	1
1.99	1.94	0.22	7.97	7.97	6.51	1
1.97	1.93	0.22	7.97	7.97	6.49	1
1.96	1.91	0.22	7.97	7.97	6.47	1
1.95	1.90	0.22	7.97	7.97	6.46	1
1.94	1.89	0.22	7.97	7.97	6.44	1
1.92	1.88	0.21	7.97	7.97	6.42	1
1.91	1.86	0.21	7.97	7.97	6.40	1
1.90	1.85	0.21	7.97	7.97	6.39	1
1.89	1.84	0.21	7.97	7.97	6.37	1
1.87	1.83	0.21	7.97	7.97	6.35	1
1.86	1.81	0.21	7.97	7.97	6.34	1
1.85	1.80	0.21	7.97	7.97	6.32	1
1.84	1.79	0.20	7.97	7.97	6.30	1
1.82	1.78	0.20	7.97	7.97	6.29	1
1.81	1.76	0.20	7.97	7.97	6.27	1
1.80	1.75	0.20	7.97	7.97	6.25	1
1.79	1.74	0.20	7.97	7.97	6.24	1
1.77	1.73	0.20	7.97	7.97	6.22	1
1.76	1.71	0.20	7.97	7.97	6.20	1
1.75	1.70	0.20	7.97	7.97	6.19	1
1.74	1.69	0.19	7.97	7.97	6.17	1
1.72	1.68	0.19	7.97	7.97	6.15	1
1.71	1.66	0.19	7.97	7.97	6.13	1
1.70	1.65	0.19	7.97	7.97	6.12	1
1.69	1.64	0.19	7.97	7.97	6.10	1
1.67	1.63	0.19	7.97	7.97	6.08	1
1.66	1.61	0.19	7.97	7.97	6.07	1
1.65	1.60	0.18	7.97	7.97	6.05	1
1.64	1.59	0.18	7.97	7.97	6.04	1
1.62	1.58	0.18	7.97	7.97	6.03	1
1.61	1.56	0.18	7.97	7.97	6.02	1
1.60	1.55	0.18	7.97	7.97	6.01	1
1.59	1.54	0.18	7.97	7.97	6.00	1
1.57	1.53	0.18	7.97	7.96	5.99	1
1.56	1.51	0.17	7.97	7.96	5.99	1
1.55	1.50	0.17	7.97	7.96	5.98	1
1.54	1.49	0.17	7.97	7.96	5.97	1
1.52	1.48	0.17	7.97	7.96	5.96	1
1.51	1.46	0.17	7.97	7.96	5.95	1
1.50	1.45	0.17	7.97	7.96	5.94	1
1.50	1.45	0.17	7.97	7.96	5.94	1
1.49	1.44	0.17	7.97	7.96	5.93	1

1.47	1.43	0.16	7.97	7.96	5.93	1
1.46	1.41	0.16	7.97	7.96	5.92	1
1.45	1.40	0.16	7.97	7.96	5.91	1
1.44	1.39	0.16	7.97	7.96	5.90	1
1.42	1.38	0.16	7.97	7.96	5.89	1
1.41	1.36	0.16	7.97	7.96	5.88	1
1.40	1.35	0.16	7.97	7.96	5.88	1
1.39	1.34	0.15	7.97	7.96	5.87	1
1.37	1.33	0.15	7.97	7.96	5.86	1
1.36	1.31	0.15	7.97	7.95	5.85	1
1.35	1.30	0.15	7.97	7.95	5.84	1
1.34	1.29	0.15	7.97	7.95	5.83	1
1.32	1.28	0.15	7.97	7.95	5.82	1
1.31	1.26	0.15	7.97	7.95	5.82	1
1.30	1.25	0.14	7.97	7.95	5.81	1
1.29	1.24	0.14	7.97	7.95	5.80	1
1.27	1.23	0.14	7.97	7.95	5.79	1
1.26	1.21	0.14	7.97	7.95	5.78	1
1.25	1.20	0.14	7.97	7.94	5.77	1
1.24	1.19	0.14	7.97	7.94	5.77	1
1.22	1.18	0.14	7.97	7.94	5.76	1
1.21	1.16	0.14	7.97	7.94	5.75	1
1.20	1.15	0.13	7.97	7.94	5.74	1
1.19	1.14	0.13	7.97	7.94	5.73	1
1.17	1.13	0.13	7.97	7.93	5.72	1
1.16	1.11	0.13	7.97	7.93	5.72	1
1.15	1.10	0.13	7.97	7.93	5.71	1
1.14	1.09	0.13	7.97	7.93	5.70	1
1.12	1.08	0.13	7.97	7.93	5.69	1
1.11	1.06	0.12	7.97	7.92	5.68	1
1.10	1.05	0.12	7.97	7.92	5.67	1
1.09	1.04	0.12	7.97	7.92	5.66	1
1.07	1.03	0.12	7.97	7.92	5.66	1
1.06	1.01	0.12	7.97	7.91	5.65	1
1.05	1.00	0.12	7.97	7.91	5.64	1
1.04	0.99	0.12	7.97	7.91	5.63	1
1.02	0.98	0.11	7.97	7.90	5.62	1
1.01	0.96	0.11	7.97	7.90	5.61	1
1.00	0.95	0.11	7.97	7.90	5.61	1
1.00	0.95	0.11	7.97	7.90	5.61	1
0.98	0.93	0.11	7.97	7.89	5.59	1
0.95	0.91	0.11	7.97	7.89	5.57	1
0.93	0.89	0.10	7.97	7.88	5.56	1
0.91	0.86	0.10	7.97	7.87	5.54	1
0.89	0.84	0.10	7.97	7.86	5.53	1
0.86	0.82	0.10	7.97	7.86	5.51	1
0.84	0.80	0.09	7.97	7.85	5.50	1
0.82	0.77	0.09	7.97	7.84	5.48	1
0.80	0.75	0.09	7.97	7.83	5.47	1
0.77	0.73	0.09	7.97	7.82	5.46	1
0.75	0.71	0.08	7.97	7.81	5.45	1
0.73	0.69	0.08	7.97	7.79	5.44	1
0.71	0.66	0.08	7.97	7.78	5.43	1
0.68	0.64	0.08	7.97	7.77	5.42	1

0.66	0.62	0.07	7.97	7.75	5.41	1
0.64	0.60	0.07	7.97	7.74	5.40	1
0.62	0.58	0.07	7.97	7.72	5.40	1
0.59	0.55	0.07	7.97	7.71	5.39	1
0.57	0.53	0.06	7.97	7.69	5.38	1
0.55	0.51	0.06	7.97	7.67	5.37	1
0.53	0.49	0.06	7.97	7.65	5.36	1
0.51	0.47	0.06	7.97	7.63	5.35	1
0.48	0.45	0.05	7.97	7.61	5.34	1
0.46	0.42	0.05	7.97	7.59	5.33	1
0.44	0.40	0.05	7.97	7.57	5.33	1
0.42	0.38	0.05	7.97	7.54	5.32	1
0.39	0.36	0.04	7.97	7.52	5.31	1
0.37	0.34	0.04	7.97	7.49	5.30	1
0.35	0.32	0.04	7.97	7.46	5.29	1
0.33	0.30	0.04	7.97	7.43	5.28	1
0.30	0.27	0.03	7.97	7.40	5.27	1
0.28	0.25	0.03	7.97	7.36	5.27	1
0.26	0.23	0.03	7.97	7.33	5.26	1
0.23	0.21	0.03	7.97	7.29	5.25	1
0.21	0.19	0.02	7.97	7.25	5.24	1
0.19	0.17	0.02	7.97	7.21	5.23	1
0.17	0.15	0.02	7.97	7.17	5.22	1
0.14	0.13	0.02	7.97	7.13	5.21	1
0.12	0.11	0.01	7.97	7.09	5.20	1
0.10	0.09	0.01	7.97	7.04	5.20	1
0.10	0.09	0.01	7.97	7.04	5.20	1
0.08	0.07	0.01	7.97	7.00	5.19	1
0.06	0.05	0.01	7.97	6.96	5.18	1
0.04	0.04	0.00	7.97	6.92	5.17	1
0.02	0.02	0.00	7.97	6.88	5.17	1
0.00	0.00	0.00	7.97	6.84	5.16	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
2.45	0.00	0.00	0.00	0.00	0.00	1
2.44	0.93	0.00	0.93	0.78	0.15	1
2.43	1.85	0.00	1.85	1.56	0.29	1
2.41	2.78	0.00	2.78	2.34	0.44	1
2.40	3.70	0.00	3.70	3.12	0.58	1
2.39	4.63	0.00	4.63	3.90	0.73	1
2.38	5.55	0.00	5.55	4.68	0.87	1
2.36	6.48	0.00	6.48	5.46	1.02	1
2.35	7.41	0.00	7.41	6.24	1.17	1
2.34	8.33	0.00	8.33	7.02	1.31	1
2.33	9.26	0.00	9.26	7.80	1.46	1
2.31	10.18	0.00	10.18	8.58	1.60	1
2.30	11.11	0.00	11.11	9.36	1.75	1
2.29	12.04	0.00	12.04	10.14	1.90	1
2.28	12.96	0.00	12.96	10.92	2.04	1
2.26	13.89	0.00	13.89	11.70	2.19	1
2.25	14.81	0.00	14.81	12.48	2.33	1

2.24	15.74	0.00	15.74	13.26	2.48	1
2.23	16.66	0.00	16.66	14.04	2.62	1
2.21	17.59	0.00	17.59	14.82	2.77	1
2.20	18.52	0.00	18.52	15.60	2.92	1
2.19	19.44	0.00	19.44	16.38	3.06	1
2.18	20.37	0.00	20.37	17.16	3.21	1
2.16	21.29	0.00	21.29	17.94	3.35	1
2.15	22.22	0.00	22.22	18.72	3.50	1
2.14	23.15	0.00	23.15	19.50	3.65	1
2.13	24.07	0.00	24.07	20.28	3.79	1
2.11	25.00	0.00	25.00	21.06	3.94	1
2.10	25.92	0.00	25.92	21.84	4.08	1
2.09	26.85	0.00	26.85	22.62	4.23	1
2.08	27.77	0.00	27.77	23.40	4.37	1
2.06	28.70	0.00	28.70	24.18	4.52	1
2.05	29.63	0.00	29.63	24.96	4.67	1
2.04	30.55	0.00	30.55	25.74	4.81	1
2.03	31.48	0.00	31.48	26.52	4.96	1
2.01	32.40	0.00	32.40	27.30	5.10	1
2.00	33.33	0.00	33.33	28.08	5.25	1
1.99	34.26	0.00	34.25	28.86	5.40	1
1.98	35.18	0.00	35.18	29.64	5.54	1
1.96	36.11	0.00	36.11	30.42	5.69	1
1.95	37.03	0.00	37.03	31.20	5.83	1
1.95	37.03	0.00	37.03	31.20	5.83	1
1.94	37.96	0.00	37.96	31.98	5.98	1
1.93	38.88	0.00	38.88	32.76	6.12	1
1.91	39.81	0.00	39.81	33.54	6.27	1
1.90	40.74	0.00	40.73	34.32	6.41	1
1.89	41.66	0.00	41.66	35.10	6.56	1
1.88	42.59	0.00	42.59	35.88	6.71	1
1.86	43.51	0.00	43.51	36.66	6.85	1
1.85	44.44	0.00	44.44	37.44	7.00	1
1.84	45.37	0.00	45.36	38.22	7.14	1
1.83	46.29	0.00	46.29	39.00	7.29	1
1.81	47.22	0.00	47.21	39.78	7.43	1
1.80	48.14	0.00	48.14	40.56	7.58	1
1.79	49.07	0.00	49.06	41.34	7.73	1
1.78	49.99	0.00	49.99	42.12	7.87	1
1.76	50.92	0.00	50.92	42.90	8.02	1
1.75	51.85	0.00	51.84	43.68	8.16	1
1.74	52.77	0.01	52.77	44.46	8.31	1
1.73	53.70	0.01	53.69	45.24	8.45	1
1.71	54.62	0.01	54.62	46.02	8.60	1
1.70	55.55	0.01	55.54	46.80	8.74	1
1.69	56.47	0.01	56.47	47.58	8.89	1
1.68	57.40	0.01	57.39	48.36	9.03	1
1.66	58.32	0.01	58.32	49.14	9.18	1
1.65	59.25	0.01	59.24	49.92	9.32	1
1.64	60.18	0.01	60.17	50.70	9.47	1
1.63	61.10	0.01	61.09	51.48	9.61	1
1.61	62.03	0.01	62.02	52.26	9.76	1
1.60	62.95	0.01	62.94	53.04	9.90	1
1.59	63.88	0.01	63.87	53.82	10.05	1

1.58	64.80	0.01	64.79	54.60	10.19	1
1.56	65.73	0.01	65.71	55.38	10.34	1
1.55	66.65	0.02	66.64	56.16	10.48	1
1.54	67.58	0.02	67.56	56.93	10.63	1
1.53	68.51	0.02	68.49	57.71	10.77	1
1.51	69.43	0.02	69.41	58.49	10.92	1
1.50	70.36	0.02	70.34	59.27	11.06	1
1.49	71.28	0.02	71.26	60.05	11.21	1
1.48	72.21	0.02	72.18	60.83	11.35	1
1.46	73.13	0.03	73.11	61.61	11.49	1
1.45	74.06	0.03	74.03	62.39	11.64	1
1.45	74.06	0.03	74.03	62.39	11.64	1
1.44	74.98	0.03	74.95	63.17	11.78	1
1.43	75.91	0.03	75.88	63.95	11.93	1
1.41	76.83	0.03	76.80	64.73	12.07	1
1.40	77.76	0.04	77.72	65.51	12.21	1
1.39	78.68	0.04	78.64	66.29	12.36	1
1.38	79.61	0.04	79.57	67.07	12.50	1
1.36	80.53	0.04	80.49	67.84	12.64	1
1.35	81.46	0.05	81.41	68.62	12.79	1
1.34	82.38	0.05	82.33	69.40	12.93	1
1.33	83.31	0.05	83.25	70.18	13.07	1
1.31	84.23	0.05	84.18	70.96	13.22	1
1.30	85.15	0.06	85.10	71.74	13.36	1
1.29	86.08	0.06	86.02	72.52	13.50	1
1.28	87.00	0.06	86.94	73.30	13.64	1
1.26	87.93	0.07	87.86	74.07	13.79	1
1.25	88.85	0.07	88.78	74.85	13.93	1
1.24	89.78	0.08	89.70	75.63	14.07	1
1.23	90.70	0.08	90.62	76.41	14.21	1
1.21	91.62	0.09	91.54	77.19	14.35	1
1.20	92.55	0.09	92.46	77.96	14.49	1
1.19	93.47	0.10	93.37	78.74	14.63	1
1.18	94.39	0.10	94.29	79.52	14.77	1
1.16	95.32	0.11	95.21	80.30	14.91	1
1.15	96.24	0.11	96.13	81.07	15.05	1
1.14	97.16	0.12	97.04	81.85	15.19	1
1.13	98.09	0.12	97.96	82.63	15.33	1
1.11	99.01	0.13	98.88	83.40	15.47	1
1.10	99.93	0.14	99.79	84.18	15.61	1
1.09	100.85	0.15	100.71	84.96	15.75	1
1.08	101.77	0.15	101.62	85.73	15.89	1
1.06	102.70	0.16	102.54	86.51	16.03	1
1.05	103.62	0.17	103.45	87.29	16.16	1
1.04	104.54	0.18	104.36	88.06	16.30	1
1.03	105.46	0.19	105.28	88.84	16.44	1
1.01	106.38	0.20	106.19	89.61	16.57	1
1.00	107.30	0.20	107.10	90.39	16.71	1
0.99	108.22	0.21	108.01	91.16	16.85	1
0.98	109.14	0.22	108.92	91.94	16.98	1
0.96	110.06	0.24	109.83	92.71	17.12	1
0.95	110.98	0.25	110.74	93.48	17.25	1
0.95	110.98	0.25	110.74	93.48	17.25	1
0.93	112.64	0.27	112.37	94.88	17.49	1

0.91	114.29	0.29	114.00	96.27	17.73	1
0.89	115.94	0.31	115.63	97.66	17.97	1
0.86	117.60	0.34	117.26	99.05	18.21	1
0.84	119.25	0.37	118.88	100.44	18.45	1
0.82	120.90	0.39	120.50	101.82	18.68	1
0.80	122.54	0.42	122.12	103.21	18.91	1
0.77	124.19	0.46	123.73	104.59	19.14	1
0.75	125.84	0.49	125.34	105.97	19.37	1
0.73	127.48	0.53	126.95	107.36	19.60	1
0.71	129.12	0.57	128.55	108.73	19.82	1
0.69	130.76	0.61	130.15	110.11	20.04	1
0.66	132.40	0.65	131.75	111.49	20.26	1
0.64	134.03	0.70	133.34	112.86	20.48	1
0.62	135.67	0.74	134.92	114.23	20.69	1
0.60	137.30	0.79	136.51	115.60	20.90	1
0.58	138.93	0.85	138.08	116.97	21.11	1
0.55	140.56	0.90	139.65	118.33	21.32	1
0.53	142.18	0.96	141.22	119.69	21.52	1
0.51	143.80	1.03	142.78	121.05	21.72	1
0.49	145.42	1.09	144.33	122.41	21.92	1
0.47	147.04	1.16	145.88	123.76	22.11	1
0.45	148.65	1.23	147.41	125.11	22.30	1
0.42	150.26	1.31	148.95	126.46	22.49	1
0.40	151.86	1.39	150.47	127.80	22.67	1
0.38	153.46	1.48	151.99	129.14	22.85	1
0.36	155.06	1.56	153.50	130.47	23.02	1
0.34	156.65	1.66	154.99	131.81	23.19	1
0.32	158.24	1.76	156.48	133.13	23.35	1
0.30	159.83	1.87	157.96	134.45	23.51	1
0.27	161.41	1.98	159.43	135.77	23.66	1
0.25	162.98	2.11	160.87	137.08	23.79	1
0.23	164.55	2.25	162.30	138.39	23.91	1
0.21	166.11	2.39	163.72	139.69	24.03	1
0.19	167.67	2.54	165.13	140.98	24.15	1
0.17	169.22	2.69	166.53	142.27	24.26	1
0.15	170.76	2.85	167.92	143.55	24.36	1
0.13	172.30	3.01	169.29	144.83	24.46	1
0.11	173.84	3.18	170.66	146.10	24.56	1
0.09	175.36	3.35	172.01	147.36	24.65	1
0.09	175.36	3.35	172.01	147.36	24.65	1
0.07	176.71	3.50	173.21	148.48	24.73	1
0.05	178.05	3.66	174.40	149.59	24.81	1
0.04	179.39	3.82	175.57	150.69	24.88	1
0.02	180.73	3.98	176.74	151.79	24.95	1
0.00	182.05	4.15	177.90	152.89	25.01	1

Time = 25. Degree of Consolidation = 9%

Total Settlement = 0.050

Settlement at End of Primary Consolidation = 0.557

Settlement caused by Primary Consolidation at time 25. = 0.050

Settlement caused by Secondary Compression at time 25. = 0.000

Surface Elevation = 1.52

*****Current Conditions in Dredged Fill*****

***** Coordinates *****

***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
2.50	2.41	0.28	7.97	7.97	7.97	1
2.49	2.40	0.28	7.97	7.97	7.93	1
2.48	2.39	0.28	7.97	7.97	7.89	1
2.46	2.37	0.27	7.97	7.97	7.84	1
2.45	2.36	0.27	7.97	7.97	7.80	1
2.44	2.35	0.27	7.97	7.97	7.76	1
2.43	2.34	0.27	7.97	7.97	7.72	1
2.41	2.32	0.27	7.97	7.97	7.67	1
2.40	2.31	0.27	7.97	7.97	7.63	1
2.39	2.30	0.27	7.97	7.97	7.59	1
2.38	2.29	0.26	7.97	7.97	7.55	1
2.36	2.27	0.26	7.97	7.97	7.50	1
2.35	2.26	0.26	7.97	7.97	7.46	1
2.34	2.25	0.26	7.97	7.97	7.42	1
2.33	2.24	0.26	7.97	7.97	7.38	1
2.31	2.22	0.26	7.97	7.97	7.34	1
2.30	2.21	0.26	7.97	7.97	7.30	1
2.29	2.20	0.26	7.97	7.97	7.27	1
2.27	2.19	0.25	7.97	7.97	7.23	1
2.26	2.17	0.25	7.97	7.97	7.19	1
2.25	2.16	0.25	7.97	7.96	7.15	1
2.24	2.15	0.25	7.97	7.96	7.12	1
2.22	2.14	0.25	7.97	7.96	7.08	1
2.21	2.12	0.25	7.97	7.96	7.04	1
2.20	2.11	0.25	7.97	7.96	7.01	1
2.19	2.10	0.24	7.97	7.96	6.97	1
2.17	2.09	0.24	7.97	7.96	6.93	1
2.16	2.08	0.24	7.97	7.96	6.89	1
2.15	2.06	0.24	7.97	7.96	6.86	1
2.14	2.05	0.24	7.97	7.96	6.82	1
2.12	2.04	0.24	7.97	7.96	6.78	1
2.11	2.03	0.24	7.97	7.96	6.74	1
2.10	2.01	0.23	7.97	7.96	6.71	1
2.09	2.00	0.23	7.97	7.96	6.67	1
2.07	1.99	0.23	7.97	7.96	6.63	1
2.06	1.98	0.23	7.97	7.96	6.61	1
2.05	1.96	0.23	7.97	7.96	6.59	1
2.04	1.95	0.23	7.97	7.96	6.57	1
2.02	1.94	0.23	7.97	7.96	6.56	1
2.01	1.93	0.22	7.97	7.96	6.54	1

2.00	1.91	0.22	7.97	7.96	6.52	1
2.00	1.91	0.22	7.97	7.96	6.52	1
1.99	1.90	0.22	7.97	7.95	6.51	1
1.97	1.89	0.22	7.97	7.95	6.49	1
1.96	1.88	0.22	7.97	7.95	6.47	1
1.95	1.86	0.22	7.97	7.95	6.46	1
1.94	1.85	0.22	7.97	7.95	6.44	1
1.92	1.84	0.21	7.97	7.95	6.42	1
1.91	1.83	0.21	7.97	7.95	6.40	1
1.90	1.81	0.21	7.97	7.95	6.39	1
1.89	1.80	0.21	7.97	7.95	6.37	1
1.87	1.79	0.21	7.97	7.95	6.35	1
1.86	1.78	0.21	7.97	7.95	6.34	1
1.85	1.76	0.21	7.97	7.95	6.32	1
1.84	1.75	0.20	7.97	7.94	6.30	1
1.82	1.74	0.20	7.97	7.94	6.29	1
1.81	1.73	0.20	7.97	7.94	6.27	1
1.80	1.71	0.20	7.97	7.94	6.25	1
1.79	1.70	0.20	7.97	7.94	6.24	1
1.77	1.69	0.20	7.97	7.94	6.22	1
1.76	1.68	0.20	7.97	7.94	6.20	1
1.75	1.66	0.20	7.97	7.94	6.19	1
1.74	1.65	0.19	7.97	7.94	6.17	1
1.72	1.64	0.19	7.97	7.93	6.15	1
1.71	1.63	0.19	7.97	7.93	6.13	1
1.70	1.61	0.19	7.97	7.93	6.12	1
1.69	1.60	0.19	7.97	7.93	6.10	1
1.67	1.59	0.19	7.97	7.93	6.08	1
1.66	1.58	0.19	7.97	7.93	6.07	1
1.65	1.56	0.18	7.97	7.92	6.05	1
1.64	1.55	0.18	7.97	7.92	6.04	1
1.62	1.54	0.18	7.97	7.92	6.03	1
1.61	1.53	0.18	7.97	7.92	6.02	1
1.60	1.51	0.18	7.97	7.92	6.01	1
1.59	1.50	0.18	7.97	7.92	6.00	1
1.57	1.49	0.18	7.97	7.91	5.99	1
1.56	1.48	0.17	7.97	7.91	5.99	1
1.55	1.46	0.17	7.97	7.91	5.98	1
1.54	1.45	0.17	7.97	7.91	5.97	1
1.52	1.44	0.17	7.97	7.90	5.96	1
1.51	1.43	0.17	7.97	7.90	5.95	1
1.50	1.41	0.17	7.97	7.90	5.94	1
1.50	1.41	0.17	7.97	7.90	5.94	1
1.49	1.40	0.17	7.97	7.90	5.93	1
1.47	1.39	0.16	7.97	7.89	5.93	1
1.46	1.38	0.16	7.97	7.89	5.92	1
1.45	1.37	0.16	7.97	7.89	5.91	1
1.44	1.35	0.16	7.97	7.89	5.90	1
1.42	1.34	0.16	7.97	7.88	5.89	1
1.41	1.33	0.16	7.97	7.88	5.88	1
1.40	1.32	0.16	7.97	7.88	5.88	1
1.39	1.30	0.15	7.97	7.88	5.87	1
1.37	1.29	0.15	7.97	7.87	5.86	1
1.36	1.28	0.15	7.97	7.87	5.85	1

1.35	1.27	0.15	7.97	7.87	5.84	1
1.34	1.25	0.15	7.97	7.86	5.83	1
1.32	1.24	0.15	7.97	7.86	5.82	1
1.31	1.23	0.15	7.97	7.86	5.82	1
1.30	1.22	0.14	7.97	7.85	5.81	1
1.29	1.20	0.14	7.97	7.85	5.80	1
1.27	1.19	0.14	7.97	7.84	5.79	1
1.26	1.18	0.14	7.97	7.84	5.78	1
1.25	1.17	0.14	7.97	7.84	5.77	1
1.24	1.16	0.14	7.97	7.83	5.77	1
1.22	1.14	0.14	7.97	7.83	5.76	1
1.21	1.13	0.14	7.97	7.82	5.75	1
1.20	1.12	0.13	7.97	7.82	5.74	1
1.19	1.11	0.13	7.97	7.82	5.73	1
1.17	1.09	0.13	7.97	7.81	5.72	1
1.16	1.08	0.13	7.97	7.81	5.72	1
1.15	1.07	0.13	7.97	7.80	5.71	1
1.14	1.06	0.13	7.97	7.80	5.70	1
1.12	1.04	0.13	7.97	7.79	5.69	1
1.11	1.03	0.12	7.97	7.79	5.68	1
1.10	1.02	0.12	7.97	7.78	5.67	1
1.09	1.01	0.12	7.97	7.78	5.66	1
1.07	1.00	0.12	7.97	7.77	5.66	1
1.06	0.98	0.12	7.97	7.76	5.65	1
1.05	0.97	0.12	7.97	7.76	5.64	1
1.04	0.96	0.12	7.97	7.75	5.63	1
1.02	0.95	0.11	7.97	7.75	5.62	1
1.01	0.93	0.11	7.97	7.74	5.61	1
1.00	0.92	0.11	7.97	7.73	5.61	1
1.00	0.92	0.11	7.97	7.73	5.61	1
0.98	0.90	0.11	7.97	7.72	5.59	1
0.95	0.88	0.11	7.97	7.71	5.57	1
0.93	0.86	0.10	7.97	7.70	5.56	1
0.91	0.84	0.10	7.97	7.69	5.54	1
0.89	0.81	0.10	7.97	7.67	5.53	1
0.86	0.79	0.10	7.97	7.66	5.51	1
0.84	0.77	0.09	7.97	7.64	5.50	1
0.82	0.75	0.09	7.97	7.63	5.48	1
0.80	0.73	0.09	7.97	7.61	5.47	1
0.77	0.71	0.09	7.97	7.60	5.46	1
0.75	0.68	0.08	7.97	7.58	5.45	1
0.73	0.66	0.08	7.97	7.56	5.44	1
0.71	0.64	0.08	7.97	7.54	5.43	1
0.68	0.62	0.08	7.97	7.53	5.42	1
0.66	0.60	0.07	7.97	7.51	5.41	1
0.64	0.58	0.07	7.97	7.49	5.40	1
0.62	0.56	0.07	7.97	7.46	5.40	1
0.59	0.53	0.07	7.97	7.44	5.39	1
0.57	0.51	0.06	7.97	7.42	5.38	1
0.55	0.49	0.06	7.97	7.39	5.37	1
0.53	0.47	0.06	7.97	7.37	5.36	1
0.51	0.45	0.06	7.97	7.34	5.35	1
0.48	0.43	0.05	7.97	7.32	5.34	1
0.46	0.41	0.05	7.97	7.29	5.33	1

0.44	0.39	0.05	7.97	7.26	5.33	1
0.42	0.37	0.05	7.97	7.23	5.32	1
0.39	0.35	0.04	7.97	7.20	5.31	1
0.37	0.33	0.04	7.97	7.17	5.30	1
0.35	0.31	0.04	7.97	7.14	5.29	1
0.33	0.28	0.04	7.97	7.11	5.28	1
0.30	0.26	0.03	7.97	7.08	5.27	1
0.28	0.24	0.03	7.97	7.05	5.27	1
0.26	0.22	0.03	7.97	7.01	5.26	1
0.23	0.20	0.03	7.97	6.98	5.25	1
0.21	0.18	0.02	7.97	6.94	5.24	1
0.19	0.16	0.02	7.97	6.91	5.23	1
0.17	0.14	0.02	7.97	6.87	5.22	1
0.14	0.12	0.02	7.97	6.83	5.21	1
0.12	0.10	0.01	7.97	6.80	5.20	1
0.10	0.09	0.01	7.97	6.76	5.20	1
0.10	0.09	0.01	7.97	6.76	5.20	1
0.08	0.07	0.01	7.97	6.72	5.19	1
0.06	0.05	0.01	7.97	6.69	5.18	1
0.04	0.03	0.00	7.97	6.65	5.17	1
0.02	0.02	0.00	7.97	6.61	5.17	1
0.00	0.00	0.00	7.97	6.58	5.16	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
2.41	0.00	0.00	0.00	0.00	0.00	1
2.40	0.93	0.00	0.92	0.78	0.14	1
2.39	1.85	0.00	1.85	1.56	0.29	1
2.37	2.78	0.00	2.77	2.34	0.43	1
2.36	3.70	0.00	3.70	3.12	0.58	1
2.35	4.63	0.00	4.62	3.90	0.72	1
2.34	5.55	0.01	5.55	4.68	0.87	1
2.32	6.48	0.01	6.47	5.46	1.01	1
2.31	7.41	0.01	7.40	6.24	1.16	1
2.30	8.33	0.01	8.32	7.02	1.30	1
2.29	9.26	0.01	9.25	7.80	1.45	1
2.27	10.18	0.01	10.17	8.58	1.59	1
2.26	11.11	0.01	11.10	9.36	1.74	1
2.25	12.03	0.01	12.02	10.14	1.88	1
2.24	12.96	0.01	12.95	10.92	2.03	1
2.22	13.88	0.01	13.87	11.70	2.17	1
2.21	14.81	0.01	14.80	12.48	2.32	1
2.20	15.74	0.02	15.72	13.26	2.46	1
2.19	16.66	0.02	16.65	14.04	2.61	1
2.17	17.59	0.02	17.57	14.82	2.75	1
2.16	18.51	0.02	18.49	15.60	2.90	1
2.15	19.44	0.02	19.42	16.38	3.04	1
2.14	20.36	0.02	20.34	17.15	3.19	1
2.12	21.29	0.02	21.27	17.93	3.33	1
2.11	22.21	0.02	22.19	18.71	3.48	1
2.10	23.14	0.02	23.11	19.49	3.62	1
2.09	24.06	0.03	24.04	20.27	3.77	1

2.08	24.99	0.03	24.96	21.05	3.91	1
2.06	25.91	0.03	25.89	21.83	4.05	1
2.05	26.84	0.03	26.81	22.61	4.20	1
2.04	27.76	0.03	27.73	23.39	4.34	1
2.03	28.69	0.03	28.66	24.17	4.49	1
2.01	29.61	0.03	29.58	24.95	4.63	1
2.00	30.54	0.04	30.50	25.73	4.78	1
1.99	31.46	0.04	31.43	26.51	4.92	1
1.98	32.39	0.04	32.35	27.28	5.06	1
1.96	33.31	0.04	33.27	28.06	5.21	1
1.95	34.24	0.04	34.19	28.84	5.35	1
1.94	35.16	0.05	35.12	29.62	5.50	1
1.93	36.09	0.05	36.04	30.40	5.64	1
1.91	37.01	0.05	36.96	31.18	5.78	1
1.91	37.01	0.05	36.96	31.18	5.78	1
1.90	37.94	0.05	37.88	31.96	5.93	1
1.89	38.86	0.05	38.81	32.74	6.07	1
1.88	39.79	0.06	39.73	33.52	6.21	1
1.86	40.71	0.06	40.65	34.29	6.36	1
1.85	41.63	0.06	41.57	35.07	6.50	1
1.84	42.56	0.07	42.49	35.85	6.64	1
1.83	43.48	0.07	43.41	36.63	6.79	1
1.81	44.41	0.07	44.34	37.41	6.93	1
1.80	45.33	0.07	45.26	38.19	7.07	1
1.79	46.25	0.08	46.18	38.96	7.21	1
1.78	47.18	0.08	47.10	39.74	7.36	1
1.76	48.10	0.08	48.02	40.52	7.50	1
1.75	49.03	0.09	48.94	41.30	7.64	1
1.74	49.95	0.09	49.86	42.07	7.78	1
1.73	50.87	0.09	50.78	42.85	7.93	1
1.71	51.80	0.10	51.70	43.63	8.07	1
1.70	52.72	0.10	52.62	44.41	8.21	1
1.69	53.64	0.11	53.54	45.18	8.35	1
1.68	54.57	0.11	54.45	45.96	8.49	1
1.66	55.49	0.12	55.37	46.74	8.63	1
1.65	56.41	0.12	56.29	47.52	8.77	1
1.64	57.33	0.13	57.21	48.29	8.92	1
1.63	58.26	0.13	58.13	49.07	9.06	1
1.61	59.18	0.14	59.04	49.85	9.20	1
1.60	60.10	0.14	59.96	50.62	9.34	1
1.59	61.02	0.15	60.88	51.40	9.48	1
1.58	61.95	0.15	61.79	52.18	9.62	1
1.56	62.87	0.16	62.71	52.95	9.76	1
1.55	63.79	0.16	63.63	53.73	9.90	1
1.54	64.71	0.17	64.54	54.50	10.04	1
1.53	65.63	0.18	65.46	55.28	10.18	1
1.51	66.55	0.18	66.37	56.05	10.32	1
1.50	67.48	0.19	67.29	56.83	10.46	1
1.49	68.40	0.20	68.20	57.61	10.60	1
1.48	69.32	0.20	69.11	58.38	10.73	1
1.46	70.24	0.21	70.03	59.16	10.87	1
1.45	71.16	0.22	70.94	59.93	11.01	1
1.44	72.08	0.23	71.85	60.70	11.15	1
1.43	73.00	0.23	72.77	61.48	11.29	1

1.41	73.92	0.24	73.68	62.25	11.42	1
1.41	73.92	0.24	73.68	62.25	11.42	1
1.40	74.84	0.25	74.59	63.03	11.56	1
1.39	75.76	0.26	75.50	63.80	11.70	1
1.38	76.68	0.27	76.41	64.57	11.84	1
1.37	77.60	0.28	77.32	65.35	11.97	1
1.35	78.51	0.29	78.23	66.12	12.11	1
1.34	79.43	0.30	79.14	66.89	12.25	1
1.33	80.35	0.31	80.05	67.66	12.38	1
1.32	81.27	0.32	80.95	68.44	12.52	1
1.30	82.19	0.33	81.86	69.21	12.65	1
1.29	83.10	0.34	82.77	69.98	12.79	1
1.28	84.02	0.35	83.67	70.75	12.92	1
1.27	84.94	0.36	84.58	71.52	13.06	1
1.25	85.85	0.37	85.48	72.29	13.19	1
1.24	86.77	0.38	86.39	73.06	13.32	1
1.23	87.69	0.39	87.29	73.83	13.46	1
1.22	88.60	0.41	88.20	74.60	13.59	1
1.20	89.52	0.42	89.10	75.37	13.73	1
1.19	90.43	0.43	90.00	76.14	13.86	1
1.18	91.35	0.45	90.90	76.91	13.99	1
1.17	92.26	0.46	91.80	77.68	14.12	1
1.16	93.18	0.47	92.70	78.45	14.25	1
1.14	94.09	0.49	93.60	79.22	14.39	1
1.13	95.00	0.50	94.50	79.98	14.52	1
1.12	95.92	0.52	95.40	80.75	14.65	1
1.11	96.83	0.53	96.30	81.52	14.78	1
1.09	97.74	0.55	97.19	82.28	14.91	1
1.08	98.65	0.57	98.09	83.05	15.04	1
1.07	99.56	0.58	98.98	83.82	15.17	1
1.06	100.48	0.60	99.88	84.58	15.30	1
1.04	101.39	0.62	100.77	85.34	15.42	1
1.03	102.30	0.63	101.66	86.11	15.55	1
1.02	103.21	0.65	102.55	86.87	15.68	1
1.01	104.11	0.67	103.44	87.64	15.81	1
1.00	105.02	0.69	104.33	88.40	15.93	1
0.98	105.93	0.71	105.22	89.16	16.06	1
0.97	106.84	0.73	106.11	89.92	16.19	1
0.96	107.75	0.75	107.00	90.68	16.31	1
0.95	108.65	0.77	107.88	91.45	16.44	1
0.93	109.56	0.79	108.77	92.21	16.56	1
0.92	110.46	0.81	109.65	92.97	16.69	1
0.92	110.46	0.81	109.65	92.97	16.69	1
0.90	112.09	0.85	111.24	94.33	16.91	1
0.88	113.72	0.89	112.83	95.70	17.13	1
0.86	115.35	0.94	114.41	97.06	17.35	1
0.84	116.97	0.98	115.99	98.42	17.57	1
0.81	118.59	1.03	117.56	99.78	17.78	1
0.79	120.21	1.07	119.13	101.13	18.00	1
0.77	121.82	1.12	120.70	102.49	18.21	1
0.75	123.44	1.18	122.26	103.84	18.42	1
0.73	125.05	1.23	123.82	105.19	18.63	1
0.71	126.66	1.29	125.37	106.54	18.84	1
0.68	128.27	1.34	126.92	107.88	19.04	1

0.66	129.87	1.40	128.47	109.22	19.24	1
0.64	131.47	1.47	130.01	110.56	19.44	1
0.62	133.07	1.53	131.54	111.90	19.64	1
0.60	134.67	1.60	133.07	113.23	19.84	1
0.58	136.26	1.67	134.59	114.56	20.03	1
0.56	137.85	1.74	136.10	115.89	20.22	1
0.53	139.43	1.82	137.61	117.21	20.40	1
0.51	141.01	1.90	139.11	118.53	20.58	1
0.49	142.59	1.99	140.61	119.84	20.76	1
0.47	144.17	2.08	142.09	121.16	20.93	1
0.45	145.74	2.18	143.55	122.46	21.09	1
0.43	147.30	2.29	145.02	123.77	21.25	1
0.41	148.87	2.39	146.47	125.07	21.41	1
0.39	150.42	2.50	147.92	126.36	21.56	1
0.37	151.98	2.61	149.36	127.65	21.71	1
0.35	153.53	2.73	150.80	128.94	21.86	1
0.33	155.07	2.85	152.22	130.22	22.00	1
0.31	156.61	2.97	153.64	131.50	22.15	1
0.28	158.14	3.09	155.06	132.77	22.29	1
0.26	159.67	3.21	156.46	134.04	22.42	1
0.24	161.20	3.34	157.86	135.30	22.56	1
0.22	162.72	3.47	159.25	136.56	22.69	1
0.20	164.23	3.61	160.63	137.81	22.82	1
0.18	165.74	3.74	162.00	139.05	22.94	1
0.16	167.24	3.88	163.36	140.29	23.07	1
0.14	168.74	4.02	164.72	141.53	23.19	1
0.12	170.23	4.17	166.06	142.76	23.30	1
0.10	171.72	4.32	167.40	143.98	23.42	1
0.09	173.20	4.47	168.73	145.20	23.53	1
0.09	173.20	4.47	168.73	145.20	23.53	1
0.07	174.51	4.60	169.90	146.27	23.63	1
0.05	175.81	4.74	171.07	147.35	23.72	1
0.03	177.11	4.88	172.23	148.41	23.82	1
0.02	178.41	5.05	173.36	149.48	23.88	1
0.00	179.70	5.37	174.33	150.53	23.80	1

Time = 40. Degree of Consolidation = 16.0%

Total Settlement = 0.088

Settlement at End of Primary Consolidation = 0.557

Settlement caused by Primary Consolidation at time 40. = 0.088

Settlement caused by Secondary Compression at time 40. = 0.000

Surface Elevation = 1.48

*****Current Conditions in Dredged Fill*****

***** Coordinates *****

***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
2.50	2.37	0.28	7.97	7.97	7.97	1
2.49	2.36	0.28	7.97	7.97	7.93	1
2.48	2.35	0.28	7.97	7.97	7.89	1
2.46	2.34	0.27	7.97	7.97	7.84	1
2.45	2.32	0.27	7.97	7.96	7.80	1
2.44	2.31	0.27	7.97	7.96	7.76	1
2.43	2.30	0.27	7.97	7.96	7.72	1
2.41	2.29	0.27	7.97	7.96	7.67	1
2.40	2.28	0.27	7.97	7.96	7.63	1
2.39	2.26	0.27	7.97	7.96	7.59	1
2.38	2.25	0.26	7.97	7.95	7.55	1
2.36	2.24	0.26	7.97	7.95	7.50	1
2.35	2.23	0.26	7.97	7.95	7.46	1
2.34	2.21	0.26	7.97	7.95	7.42	1
2.33	2.20	0.26	7.97	7.95	7.38	1
2.31	2.19	0.26	7.97	7.95	7.34	1
2.30	2.18	0.26	7.97	7.95	7.30	1
2.29	2.16	0.26	7.97	7.95	7.27	1
2.27	2.15	0.25	7.97	7.94	7.23	1
2.26	2.14	0.25	7.97	7.94	7.19	1
2.25	2.13	0.25	7.97	7.94	7.15	1
2.24	2.11	0.25	7.97	7.94	7.12	1
2.22	2.10	0.25	7.97	7.94	7.08	1
2.21	2.09	0.25	7.97	7.94	7.04	1
2.20	2.08	0.25	7.97	7.94	7.01	1
2.19	2.06	0.24	7.97	7.93	6.97	1
2.17	2.05	0.24	7.97	7.93	6.93	1
2.16	2.04	0.24	7.97	7.93	6.89	1
2.15	2.03	0.24	7.97	7.93	6.86	1
2.14	2.01	0.24	7.97	7.93	6.82	1
2.12	2.00	0.24	7.97	7.93	6.78	1
2.11	1.99	0.24	7.97	7.92	6.74	1
2.10	1.98	0.23	7.97	7.92	6.71	1
2.09	1.96	0.23	7.97	7.92	6.67	1
2.07	1.95	0.23	7.97	7.92	6.63	1
2.06	1.94	0.23	7.97	7.92	6.61	1
2.05	1.93	0.23	7.97	7.92	6.59	1
2.04	1.91	0.23	7.97	7.91	6.57	1
2.02	1.90	0.23	7.97	7.91	6.56	1
2.01	1.89	0.22	7.97	7.91	6.54	1
2.00	1.88	0.22	7.97	7.91	6.52	1
2.00	1.88	0.22	7.97	7.91	6.52	1
1.99	1.86	0.22	7.97	7.91	6.51	1
1.97	1.85	0.22	7.97	7.91	6.49	1
1.96	1.84	0.22	7.97	7.90	6.47	1
1.95	1.83	0.22	7.97	7.90	6.46	1
1.94	1.81	0.22	7.97	7.90	6.44	1
1.92	1.80	0.21	7.97	7.90	6.42	1
1.91	1.79	0.21	7.97	7.90	6.40	1
1.90	1.78	0.21	7.97	7.89	6.39	1

1.89	1.76	0.21	7.97	7.89	6.37	1
1.87	1.75	0.21	7.97	7.89	6.35	1
1.86	1.74	0.21	7.97	7.89	6.34	1
1.85	1.73	0.21	7.97	7.88	6.32	1
1.84	1.72	0.20	7.97	7.88	6.30	1
1.82	1.70	0.20	7.97	7.88	6.29	1
1.81	1.69	0.20	7.97	7.88	6.27	1
1.80	1.68	0.20	7.97	7.87	6.25	1
1.79	1.67	0.20	7.97	7.87	6.24	1
1.77	1.65	0.20	7.97	7.87	6.22	1
1.76	1.64	0.20	7.97	7.87	6.20	1
1.75	1.63	0.20	7.97	7.86	6.19	1
1.74	1.62	0.19	7.97	7.86	6.17	1
1.72	1.60	0.19	7.97	7.86	6.15	1
1.71	1.59	0.19	7.97	7.85	6.13	1
1.70	1.58	0.19	7.97	7.85	6.12	1
1.69	1.57	0.19	7.97	7.85	6.10	1
1.67	1.55	0.19	7.97	7.85	6.08	1
1.66	1.54	0.19	7.97	7.84	6.07	1
1.65	1.53	0.18	7.97	7.84	6.05	1
1.64	1.52	0.18	7.97	7.84	6.04	1
1.62	1.51	0.18	7.97	7.83	6.03	1
1.61	1.49	0.18	7.97	7.83	6.02	1
1.60	1.48	0.18	7.97	7.83	6.01	1
1.59	1.47	0.18	7.97	7.82	6.00	1
1.57	1.46	0.18	7.97	7.82	5.99	1
1.56	1.44	0.17	7.97	7.81	5.99	1
1.55	1.43	0.17	7.97	7.81	5.98	1
1.54	1.42	0.17	7.97	7.81	5.97	1
1.52	1.41	0.17	7.97	7.80	5.96	1
1.51	1.40	0.17	7.97	7.80	5.95	1
1.50	1.38	0.17	7.97	7.79	5.94	1
1.50	1.38	0.17	7.97	7.79	5.94	1
1.49	1.37	0.17	7.97	7.79	5.93	1
1.47	1.36	0.16	7.97	7.79	5.93	1
1.46	1.35	0.16	7.97	7.78	5.92	1
1.45	1.33	0.16	7.97	7.78	5.91	1
1.44	1.32	0.16	7.97	7.77	5.90	1
1.42	1.31	0.16	7.97	7.77	5.89	1
1.41	1.30	0.16	7.97	7.76	5.88	1
1.40	1.28	0.16	7.97	7.76	5.88	1
1.39	1.27	0.15	7.97	7.75	5.87	1
1.37	1.26	0.15	7.97	7.75	5.86	1
1.36	1.25	0.15	7.97	7.74	5.85	1
1.35	1.24	0.15	7.97	7.74	5.84	1
1.34	1.22	0.15	7.97	7.73	5.83	1
1.32	1.21	0.15	7.97	7.73	5.82	1
1.31	1.20	0.15	7.97	7.72	5.82	1
1.30	1.19	0.14	7.97	7.72	5.81	1
1.29	1.18	0.14	7.97	7.71	5.80	1
1.27	1.16	0.14	7.97	7.71	5.79	1
1.26	1.15	0.14	7.97	7.70	5.78	1
1.25	1.14	0.14	7.97	7.70	5.77	1
1.24	1.13	0.14	7.97	7.69	5.77	1

1.22	1.11	0.14	7.97	7.68	5.76	1
1.21	1.10	0.14	7.97	7.68	5.75	1
1.20	1.09	0.13	7.97	7.67	5.74	1
1.19	1.08	0.13	7.97	7.67	5.73	1
1.17	1.07	0.13	7.97	7.66	5.72	1
1.16	1.05	0.13	7.97	7.65	5.72	1
1.15	1.04	0.13	7.97	7.65	5.71	1
1.14	1.03	0.13	7.97	7.64	5.70	1
1.12	1.02	0.13	7.97	7.63	5.69	1
1.11	1.01	0.12	7.97	7.63	5.68	1
1.10	0.99	0.12	7.97	7.62	5.67	1
1.09	0.98	0.12	7.97	7.61	5.66	1
1.07	0.97	0.12	7.97	7.60	5.66	1
1.06	0.96	0.12	7.97	7.60	5.65	1
1.05	0.95	0.12	7.97	7.59	5.64	1
1.04	0.93	0.12	7.97	7.58	5.63	1
1.02	0.92	0.11	7.97	7.57	5.62	1
1.01	0.91	0.11	7.97	7.57	5.61	1
1.00	0.90	0.11	7.97	7.56	5.61	1
1.00	0.90	0.11	7.97	7.56	5.61	1
0.98	0.88	0.11	7.97	7.54	5.59	1
0.95	0.86	0.11	7.97	7.53	5.57	1
0.93	0.83	0.10	7.97	7.51	5.56	1
0.91	0.81	0.10	7.97	7.49	5.54	1
0.89	0.79	0.10	7.97	7.48	5.53	1
0.86	0.77	0.10	7.97	7.46	5.51	1
0.84	0.75	0.09	7.97	7.44	5.50	1
0.82	0.73	0.09	7.97	7.42	5.48	1
0.80	0.71	0.09	7.97	7.40	5.47	1
0.77	0.69	0.09	7.97	7.38	5.46	1
0.75	0.66	0.08	7.97	7.36	5.45	1
0.73	0.64	0.08	7.97	7.34	5.44	1
0.71	0.62	0.08	7.97	7.32	5.43	1
0.68	0.60	0.08	7.97	7.30	5.42	1
0.66	0.58	0.07	7.97	7.28	5.41	1
0.64	0.56	0.07	7.97	7.25	5.40	1
0.62	0.54	0.07	7.97	7.23	5.40	1
0.59	0.52	0.07	7.97	7.21	5.39	1
0.57	0.50	0.06	7.97	7.18	5.38	1
0.55	0.48	0.06	7.97	7.16	5.37	1
0.53	0.46	0.06	7.97	7.13	5.36	1
0.51	0.44	0.06	7.97	7.10	5.35	1
0.48	0.42	0.05	7.97	7.08	5.34	1
0.46	0.40	0.05	7.97	7.05	5.33	1
0.44	0.38	0.05	7.97	7.02	5.33	1
0.42	0.36	0.05	7.97	7.00	5.32	1
0.39	0.34	0.04	7.97	6.97	5.31	1
0.37	0.32	0.04	7.97	6.94	5.30	1
0.35	0.30	0.04	7.97	6.91	5.29	1
0.33	0.28	0.04	7.97	6.88	5.28	1
0.30	0.26	0.03	7.97	6.85	5.27	1
0.28	0.24	0.03	7.97	6.82	5.27	1
0.26	0.22	0.03	7.97	6.79	5.26	1
0.23	0.20	0.03	7.97	6.75	5.25	1

0.21	0.18	0.02	7.97	6.72	5.24	1
0.19	0.16	0.02	7.97	6.69	5.23	1
0.17	0.14	0.02	7.97	6.66	5.22	1
0.14	0.12	0.02	7.97	6.62	5.21	1
0.12	0.10	0.01	7.97	6.59	5.20	1
0.10	0.08	0.01	7.97	6.55	5.20	1
0.10	0.08	0.01	7.97	6.55	5.20	1
0.08	0.07	0.01	7.97	6.53	5.19	1
0.06	0.05	0.01	7.97	6.50	5.18	1
0.04	0.03	0.00	7.97	6.47	5.17	1
0.02	0.02	0.00	7.97	6.44	5.17	1
0.00	0.00	0.00	7.97	6.41	5.16	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
2.37	0.00	0.00	0.00	0.00	0.00	1
2.36	0.93	0.01	0.92	0.78	0.14	1
2.35	1.85	0.01	1.84	1.56	0.28	1
2.34	2.78	0.02	2.76	2.34	0.42	1
2.32	3.70	0.02	3.68	3.12	0.56	1
2.31	4.63	0.03	4.60	3.90	0.70	1
2.30	5.55	0.03	5.52	4.68	0.84	1
2.29	6.48	0.04	6.44	5.46	0.98	1
2.28	7.40	0.04	7.36	6.24	1.12	1
2.26	8.33	0.05	8.28	7.01	1.26	1
2.25	9.25	0.05	9.20	7.79	1.41	1
2.24	10.18	0.06	10.12	8.57	1.55	1
2.23	11.10	0.06	11.04	9.35	1.69	1
2.21	12.02	0.07	11.96	10.13	1.83	1
2.20	12.95	0.07	12.88	10.91	1.97	1
2.19	13.87	0.08	13.80	11.68	2.11	1
2.18	14.80	0.08	14.71	12.46	2.25	1
2.16	15.72	0.09	15.63	13.24	2.39	1
2.15	16.64	0.09	16.55	14.02	2.53	1
2.14	17.57	0.10	17.47	14.80	2.68	1
2.13	18.49	0.10	18.39	15.57	2.82	1
2.11	19.41	0.10	19.31	16.35	2.96	1
2.10	20.34	0.11	20.23	17.13	3.10	1
2.09	21.26	0.11	21.14	17.91	3.24	1
2.08	22.18	0.12	22.06	18.68	3.38	1
2.06	23.11	0.12	22.98	19.46	3.52	1
2.05	24.03	0.13	23.90	20.24	3.66	1
2.04	24.95	0.13	24.82	21.01	3.80	1
2.03	25.87	0.14	25.73	21.79	3.94	1
2.01	26.79	0.14	26.65	22.57	4.08	1
2.00	27.72	0.15	27.57	23.34	4.22	1
1.99	28.64	0.16	28.48	24.12	4.37	1
1.98	29.56	0.16	29.40	24.89	4.51	1
1.96	30.48	0.17	30.32	25.67	4.65	1
1.95	31.40	0.17	31.23	26.45	4.79	1
1.94	32.33	0.18	32.15	27.22	4.93	1
1.93	33.25	0.18	33.06	28.00	5.07	1

1.91	34.17	0.19	33.98	28.77	5.21	1
1.90	35.09	0.20	34.89	29.55	5.35	1
1.89	36.01	0.20	35.81	30.32	5.48	1
1.88	36.93	0.21	36.72	31.10	5.62	1
1.88	36.93	0.21	36.72	31.10	5.62	1
1.86	37.85	0.22	37.64	31.87	5.76	1
1.85	38.77	0.22	38.55	32.65	5.90	1
1.84	39.69	0.23	39.46	33.42	6.04	1
1.83	40.61	0.24	40.38	34.19	6.18	1
1.81	41.53	0.24	41.29	34.97	6.32	1
1.80	42.45	0.25	42.20	35.74	6.46	1
1.79	43.37	0.26	43.11	36.52	6.60	1
1.78	44.29	0.26	44.02	37.29	6.74	1
1.76	45.21	0.27	44.94	38.06	6.87	1
1.75	46.13	0.28	45.85	38.84	7.01	1
1.74	47.05	0.29	46.76	39.61	7.15	1
1.73	47.96	0.30	47.67	40.38	7.29	1
1.72	48.88	0.30	48.58	41.15	7.42	1
1.70	49.80	0.31	49.49	41.93	7.56	1
1.69	50.72	0.32	50.40	42.70	7.70	1
1.68	51.64	0.33	51.31	43.47	7.84	1
1.67	52.55	0.34	52.21	44.24	7.97	1
1.65	53.47	0.35	53.12	45.01	8.11	1
1.64	54.39	0.36	54.03	45.78	8.25	1
1.63	55.30	0.37	54.94	46.55	8.38	1
1.62	56.22	0.38	55.84	47.33	8.52	1
1.60	57.14	0.39	56.75	48.10	8.65	1
1.59	58.05	0.40	57.66	48.87	8.79	1
1.58	58.97	0.41	58.56	49.64	8.93	1
1.57	59.88	0.42	59.47	50.41	9.06	1
1.55	60.80	0.43	60.37	51.17	9.20	1
1.54	61.71	0.44	61.27	51.94	9.33	1
1.53	62.63	0.45	62.18	52.71	9.47	1
1.52	63.54	0.46	63.08	53.48	9.60	1
1.51	64.46	0.47	63.98	54.25	9.73	1
1.49	65.37	0.49	64.88	55.02	9.87	1
1.48	66.28	0.50	65.79	55.78	10.00	1
1.47	67.20	0.51	66.69	56.55	10.13	1
1.46	68.11	0.52	67.59	57.32	10.27	1
1.44	69.02	0.54	68.49	58.09	10.40	1
1.43	69.93	0.55	69.39	58.85	10.53	1
1.42	70.85	0.56	70.28	59.62	10.67	1
1.41	71.76	0.58	71.18	60.38	10.80	1
1.40	72.67	0.59	72.08	61.15	10.93	1
1.38	73.58	0.60	72.98	61.91	11.06	1
1.38	73.58	0.60	72.98	61.91	11.06	1
1.37	74.49	0.62	73.87	62.68	11.19	1
1.36	75.40	0.63	74.77	63.44	11.33	1
1.35	76.31	0.65	75.66	64.21	11.46	1
1.33	77.22	0.66	76.56	64.97	11.59	1
1.32	78.13	0.68	77.45	65.73	11.72	1
1.31	79.04	0.69	78.34	66.50	11.85	1
1.30	79.94	0.71	79.24	67.26	11.98	1
1.28	80.85	0.73	80.13	68.02	12.11	1

1.27	81.76	0.74	81.02	68.78	12.24	1
1.26	82.67	0.76	81.91	69.54	12.37	1
1.25	83.57	0.78	82.80	70.30	12.49	1
1.24	84.48	0.79	83.69	71.06	12.62	1
1.22	85.38	0.81	84.57	71.82	12.75	1
1.21	86.29	0.83	85.46	72.58	12.88	1
1.20	87.19	0.85	86.35	73.34	13.01	1
1.19	88.10	0.87	87.23	74.10	13.13	1
1.18	89.00	0.89	88.12	74.86	13.26	1
1.16	89.91	0.90	89.00	75.62	13.39	1
1.15	90.81	0.92	89.88	76.37	13.51	1
1.14	91.71	0.94	90.77	77.13	13.64	1
1.13	92.61	0.96	91.65	77.88	13.76	1
1.11	93.51	0.99	92.53	78.64	13.89	1
1.10	94.41	1.01	93.41	79.39	14.01	1
1.09	95.31	1.03	94.29	80.15	14.14	1
1.08	96.21	1.05	95.17	80.90	14.26	1
1.07	97.11	1.07	96.04	81.66	14.39	1
1.05	98.01	1.09	96.92	82.41	14.51	1
1.04	98.91	1.12	97.79	83.16	14.63	1
1.03	99.81	1.14	98.67	83.91	14.76	1
1.02	100.70	1.16	99.54	84.66	14.88	1
1.01	101.60	1.19	100.41	85.41	15.00	1
0.99	102.50	1.21	101.28	86.16	15.12	1
0.98	103.39	1.24	102.15	86.91	15.24	1
0.97	104.29	1.26	103.02	87.66	15.36	1
0.96	105.18	1.29	103.89	88.41	15.48	1
0.95	106.07	1.31	104.76	89.16	15.60	1
0.93	106.96	1.34	105.62	89.90	15.72	1
0.92	107.86	1.37	106.49	90.65	15.84	1
0.91	108.75	1.40	107.35	91.39	15.96	1
0.90	109.64	1.42	108.21	92.14	16.08	1
0.90	109.64	1.42	108.21	92.14	16.08	1
0.88	111.24	1.47	109.76	93.48	16.29	1
0.86	112.84	1.53	111.31	94.81	16.50	1
0.83	114.43	1.58	112.85	96.15	16.70	1
0.81	116.03	1.64	114.39	97.48	16.91	1
0.79	117.62	1.70	115.92	98.80	17.11	1
0.77	119.20	1.76	117.45	100.13	17.32	1
0.75	120.79	1.82	118.97	101.45	17.52	1
0.73	122.37	1.89	120.49	102.77	17.71	1
0.71	123.95	1.95	122.00	104.09	17.91	1
0.69	125.53	2.02	123.50	105.40	18.10	1
0.66	127.10	2.11	125.00	106.71	18.28	1
0.64	128.67	2.19	126.48	108.02	18.46	1
0.62	130.24	2.27	127.96	109.33	18.64	1
0.60	131.80	2.36	129.44	110.63	18.82	1
0.58	133.36	2.45	130.91	111.92	18.99	1
0.56	134.92	2.54	132.38	113.22	19.16	1
0.54	136.47	2.63	133.84	114.51	19.33	1
0.52	138.02	2.72	135.30	115.79	19.50	1
0.50	139.56	2.82	136.75	117.08	19.67	1
0.48	141.10	2.91	138.19	118.35	19.84	1
0.46	142.64	3.01	139.63	119.63	20.00	1

0.44	144.17	3.11	141.06	120.90	20.16	1
0.42	145.70	3.22	142.49	122.17	20.32	1
0.40	147.23	3.32	143.91	123.43	20.48	1
0.38	148.75	3.43	145.32	124.69	20.63	1
0.36	150.26	3.54	146.73	125.94	20.79	1
0.34	151.77	3.65	148.13	127.19	20.94	1
0.32	153.28	3.76	149.52	128.43	21.09	1
0.30	154.78	3.87	150.91	129.67	21.24	1
0.28	156.28	3.99	152.29	130.91	21.38	1
0.26	157.78	4.11	153.67	132.14	21.53	1
0.24	159.26	4.23	155.03	133.37	21.67	1
0.22	160.75	4.35	156.39	134.59	21.81	1
0.20	162.23	4.48	157.75	135.80	21.95	1
0.18	163.70	4.60	159.10	137.01	22.08	1
0.16	165.17	4.73	160.44	138.22	22.22	1
0.14	166.63	4.86	161.77	139.42	22.35	1
0.12	168.09	4.99	163.10	140.62	22.48	1
0.10	169.54	5.27	164.27	141.81	22.46	1
0.08	170.99	5.56	165.43	142.99	22.44	1
0.08	170.99	5.56	165.43	142.99	22.44	1
0.07	172.27	5.82	166.46	144.04	22.42	1
0.05	173.55	6.07	167.49	145.09	22.40	1
0.03	174.83	6.31	168.51	146.13	22.39	1
0.02	176.10	6.56	169.54	147.16	22.37	1
0.00	177.36	6.80	170.57	148.20	22.37	1

Time = 55. Degree of Consolidation = 22.0%

Total Settlement = 0.125

Settlement at End of Primary Consolidation = 0.557

Settlement caused by Primary Consolidation at time 55. = 0.125

Settlement caused by Secondary Compression at time 55. = 0.000

Surface Elevation = 1.45

*****Current Conditions in Dredged Fill*****

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
2.50	2.31	0.28	7.97	7.97	7.97	1
2.49	2.30	0.28	7.97	7.96	7.93	1
2.48	2.28	0.28	7.97	7.96	7.89	1
2.46	2.27	0.27	7.97	7.95	7.84	1
2.45	2.26	0.27	7.97	7.94	7.80	1
2.44	2.25	0.27	7.97	7.94	7.76	1

2.43	2.23	0.27	7.97	7.93	7.72	1
2.41	2.22	0.27	7.97	7.92	7.67	1
2.40	2.21	0.27	7.97	7.92	7.63	1
2.39	2.20	0.27	7.97	7.91	7.59	1
2.38	2.18	0.26	7.97	7.90	7.55	1
2.36	2.17	0.26	7.97	7.90	7.50	1
2.35	2.16	0.26	7.97	7.89	7.46	1
2.34	2.15	0.26	7.97	7.89	7.42	1
2.33	2.13	0.26	7.97	7.88	7.38	1
2.31	2.12	0.26	7.97	7.88	7.34	1
2.30	2.11	0.26	7.97	7.87	7.30	1
2.29	2.10	0.26	7.97	7.87	7.27	1
2.27	2.08	0.25	7.97	7.86	7.23	1
2.26	2.07	0.25	7.97	7.86	7.19	1
2.25	2.06	0.25	7.97	7.85	7.15	1
2.24	2.05	0.25	7.97	7.85	7.12	1
2.22	2.03	0.25	7.97	7.84	7.08	1
2.21	2.02	0.25	7.97	7.84	7.04	1
2.20	2.01	0.25	7.97	7.83	7.01	1
2.19	2.00	0.24	7.97	7.83	6.97	1
2.17	1.99	0.24	7.97	7.82	6.93	1
2.16	1.97	0.24	7.97	7.82	6.89	1
2.15	1.96	0.24	7.97	7.81	6.86	1
2.14	1.95	0.24	7.97	7.81	6.82	1
2.12	1.94	0.24	7.97	7.80	6.78	1
2.11	1.92	0.24	7.97	7.80	6.74	1
2.10	1.91	0.23	7.97	7.79	6.71	1
2.09	1.90	0.23	7.97	7.79	6.67	1
2.07	1.89	0.23	7.97	7.79	6.63	1
2.06	1.88	0.23	7.97	7.78	6.61	1
2.05	1.86	0.23	7.97	7.78	6.59	1
2.04	1.85	0.23	7.97	7.77	6.57	1
2.02	1.84	0.23	7.97	7.77	6.56	1
2.01	1.83	0.22	7.97	7.76	6.54	1
2.00	1.81	0.22	7.97	7.76	6.52	1
2.00	1.81	0.22	7.97	7.76	6.52	1
1.99	1.80	0.22	7.97	7.75	6.51	1
1.97	1.79	0.22	7.97	7.75	6.49	1
1.96	1.78	0.22	7.97	7.74	6.47	1
1.95	1.77	0.22	7.97	7.74	6.46	1
1.94	1.75	0.22	7.97	7.74	6.44	1
1.92	1.74	0.21	7.97	7.73	6.42	1
1.91	1.73	0.21	7.97	7.73	6.40	1
1.90	1.72	0.21	7.97	7.72	6.39	1
1.89	1.70	0.21	7.97	7.72	6.37	1
1.87	1.69	0.21	7.97	7.71	6.35	1
1.86	1.68	0.21	7.97	7.71	6.34	1
1.85	1.67	0.21	7.97	7.70	6.32	1
1.84	1.66	0.20	7.97	7.70	6.30	1
1.82	1.64	0.20	7.97	7.69	6.29	1
1.81	1.63	0.20	7.97	7.69	6.27	1
1.80	1.62	0.20	7.97	7.68	6.25	1
1.79	1.61	0.20	7.97	7.68	6.24	1
1.77	1.60	0.20	7.97	7.67	6.22	1

1.76	1.58	0.20	7.97	7.67	6.20	1
1.75	1.57	0.20	7.97	7.66	6.19	1
1.74	1.56	0.19	7.97	7.66	6.17	1
1.72	1.55	0.19	7.97	7.65	6.15	1
1.71	1.53	0.19	7.97	7.65	6.13	1
1.70	1.52	0.19	7.97	7.64	6.12	1
1.69	1.51	0.19	7.97	7.64	6.10	1
1.67	1.50	0.19	7.97	7.63	6.08	1
1.66	1.49	0.19	7.97	7.62	6.07	1
1.65	1.47	0.18	7.97	7.62	6.05	1
1.64	1.46	0.18	7.97	7.61	6.04	1
1.62	1.45	0.18	7.97	7.61	6.03	1
1.61	1.44	0.18	7.97	7.60	6.02	1
1.60	1.43	0.18	7.97	7.60	6.01	1
1.59	1.41	0.18	7.97	7.59	6.00	1
1.57	1.40	0.18	7.97	7.58	5.99	1
1.56	1.39	0.17	7.97	7.58	5.99	1
1.55	1.38	0.17	7.97	7.57	5.98	1
1.54	1.37	0.17	7.97	7.57	5.97	1
1.52	1.36	0.17	7.97	7.56	5.96	1
1.51	1.34	0.17	7.97	7.55	5.95	1
1.50	1.33	0.17	7.97	7.55	5.94	1
1.50	1.33	0.17	7.97	7.55	5.94	1
1.49	1.32	0.17	7.97	7.54	5.93	1
1.47	1.31	0.16	7.97	7.53	5.93	1
1.46	1.30	0.16	7.97	7.53	5.92	1
1.45	1.28	0.16	7.97	7.52	5.91	1
1.44	1.27	0.16	7.97	7.51	5.90	1
1.42	1.26	0.16	7.97	7.51	5.89	1
1.41	1.25	0.16	7.97	7.50	5.88	1
1.40	1.24	0.16	7.97	7.49	5.88	1
1.39	1.22	0.15	7.97	7.49	5.87	1
1.37	1.21	0.15	7.97	7.48	5.86	1
1.36	1.20	0.15	7.97	7.47	5.85	1
1.35	1.19	0.15	7.97	7.46	5.84	1
1.34	1.18	0.15	7.97	7.46	5.83	1
1.32	1.17	0.15	7.97	7.45	5.82	1
1.31	1.15	0.15	7.97	7.44	5.82	1
1.30	1.14	0.14	7.97	7.43	5.81	1
1.29	1.13	0.14	7.97	7.43	5.80	1
1.27	1.12	0.14	7.97	7.42	5.79	1
1.26	1.11	0.14	7.97	7.41	5.78	1
1.25	1.10	0.14	7.97	7.40	5.77	1
1.24	1.08	0.14	7.97	7.39	5.77	1
1.22	1.07	0.14	7.97	7.38	5.76	1
1.21	1.06	0.14	7.97	7.38	5.75	1
1.20	1.05	0.13	7.97	7.37	5.74	1
1.19	1.04	0.13	7.97	7.36	5.73	1
1.17	1.02	0.13	7.97	7.35	5.72	1
1.16	1.01	0.13	7.97	7.34	5.72	1
1.15	1.00	0.13	7.97	7.33	5.71	1
1.14	0.99	0.13	7.97	7.32	5.70	1
1.12	0.98	0.13	7.97	7.31	5.69	1
1.11	0.97	0.12	7.97	7.30	5.68	1

1.10	0.96	0.12	7.97	7.30	5.67	1
1.09	0.94	0.12	7.97	7.29	5.66	1
1.07	0.93	0.12	7.97	7.28	5.66	1
1.06	0.92	0.12	7.97	7.27	5.65	1
1.05	0.91	0.12	7.97	7.26	5.64	1
1.04	0.90	0.12	7.97	7.25	5.63	1
1.02	0.89	0.11	7.97	7.24	5.62	1
1.01	0.87	0.11	7.97	7.23	5.61	1
1.00	0.86	0.11	7.97	7.22	5.61	1
1.00	0.86	0.11	7.97	7.22	5.61	1
0.98	0.84	0.11	7.97	7.20	5.59	1
0.95	0.82	0.11	7.97	7.18	5.57	1
0.93	0.80	0.10	7.97	7.16	5.56	1
0.91	0.78	0.10	7.97	7.15	5.54	1
0.89	0.76	0.10	7.97	7.13	5.53	1
0.86	0.74	0.10	7.97	7.11	5.51	1
0.84	0.72	0.09	7.97	7.09	5.50	1
0.82	0.70	0.09	7.97	7.07	5.48	1
0.80	0.68	0.09	7.97	7.05	5.47	1
0.77	0.66	0.09	7.97	7.03	5.46	1
0.75	0.64	0.08	7.97	7.01	5.45	1
0.73	0.62	0.08	7.97	6.99	5.44	1
0.71	0.60	0.08	7.97	6.97	5.43	1
0.68	0.58	0.08	7.97	6.95	5.42	1
0.66	0.56	0.07	7.97	6.93	5.41	1
0.64	0.54	0.07	7.97	6.90	5.40	1
0.62	0.52	0.07	7.97	6.88	5.40	1
0.59	0.50	0.07	7.97	6.86	5.39	1
0.57	0.48	0.06	7.97	6.84	5.38	1
0.55	0.46	0.06	7.97	6.81	5.37	1
0.53	0.44	0.06	7.97	6.79	5.36	1
0.51	0.42	0.06	7.97	6.77	5.35	1
0.48	0.40	0.05	7.97	6.74	5.34	1
0.46	0.38	0.05	7.97	6.72	5.33	1
0.44	0.36	0.05	7.97	6.70	5.33	1
0.42	0.34	0.05	7.97	6.67	5.32	1
0.39	0.32	0.04	7.97	6.65	5.31	1
0.37	0.31	0.04	7.97	6.62	5.30	1
0.35	0.29	0.04	7.97	6.60	5.29	1
0.33	0.27	0.04	7.97	6.57	5.28	1
0.30	0.25	0.03	7.97	6.54	5.27	1
0.28	0.23	0.03	7.97	6.52	5.27	1
0.26	0.21	0.03	7.97	6.49	5.26	1
0.23	0.19	0.03	7.97	6.47	5.25	1
0.21	0.17	0.02	7.97	6.44	5.24	1
0.19	0.15	0.02	7.97	6.42	5.23	1
0.17	0.14	0.02	7.97	6.39	5.22	1
0.14	0.12	0.02	7.97	6.37	5.21	1
0.12	0.10	0.01	7.97	6.34	5.20	1
0.10	0.08	0.01	7.97	6.32	5.20	1
0.10	0.08	0.01	7.97	6.32	5.20	1
0.08	0.06	0.01	7.97	6.30	5.19	1
0.06	0.05	0.01	7.97	6.28	5.18	1
0.04	0.03	0.00	7.97	6.25	5.17	1

0.02	0.02	0.00	7.97	6.23	5.17	1
0.00	0.00	0.00	7.97	6.21	5.16	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
2.31	0.00	0.00	0.00	0.00	0.00	1
2.30	0.93	0.03	0.90	0.78	0.12	1
2.28	1.85	0.05	1.80	1.56	0.24	1
2.27	2.77	0.07	2.70	2.34	0.36	1
2.26	3.70	0.10	3.60	3.12	0.49	1
2.25	4.62	0.12	4.50	3.89	0.61	1
2.23	5.54	0.14	5.40	4.67	0.73	1
2.22	6.47	0.16	6.30	5.45	0.86	1
2.21	7.39	0.19	7.20	6.22	0.98	1
2.20	8.31	0.21	8.10	7.00	1.11	1
2.18	9.23	0.23	9.00	7.77	1.23	1
2.17	10.15	0.25	9.90	8.54	1.36	1
2.16	11.07	0.27	10.80	9.32	1.48	1
2.15	11.99	0.29	11.70	10.09	1.61	1
2.13	12.91	0.30	12.60	10.86	1.74	1
2.12	13.82	0.32	13.50	11.64	1.86	1
2.11	14.74	0.34	14.40	12.41	1.99	1
2.10	15.66	0.36	15.30	13.18	2.12	1
2.08	16.57	0.38	16.20	13.95	2.25	1
2.07	17.49	0.39	17.10	14.72	2.38	1
2.06	18.41	0.41	17.99	15.49	2.51	1
2.05	19.32	0.43	18.89	16.26	2.63	1
2.03	20.24	0.44	19.79	17.03	2.76	1
2.02	21.15	0.46	20.69	17.80	2.89	1
2.01	22.06	0.48	21.59	18.56	3.02	1
2.00	22.98	0.49	22.48	19.33	3.15	1
1.99	23.89	0.51	23.38	20.10	3.28	1
1.97	24.80	0.53	24.28	20.87	3.41	1
1.96	25.72	0.54	25.17	21.63	3.54	1
1.95	26.63	0.56	26.07	22.40	3.67	1
1.94	27.54	0.57	26.97	23.16	3.80	1
1.92	28.45	0.59	27.86	23.93	3.93	1
1.91	29.36	0.60	28.76	24.70	4.06	1
1.90	30.27	0.62	29.65	25.46	4.19	1
1.89	31.18	0.64	30.55	26.22	4.32	1
1.88	32.09	0.65	31.44	26.99	4.45	1
1.86	33.00	0.67	32.33	27.75	4.58	1
1.85	33.91	0.68	33.23	28.51	4.71	1
1.84	34.82	0.70	34.12	29.28	4.84	1
1.83	35.73	0.71	35.01	30.04	4.97	1
1.81	36.63	0.73	35.90	30.80	5.10	1
1.81	36.63	0.73	35.90	30.80	5.10	1
1.80	37.54	0.74	36.80	31.56	5.23	1
1.79	38.45	0.76	37.69	32.32	5.36	1
1.78	39.35	0.78	38.58	33.08	5.49	1
1.77	40.26	0.79	39.47	33.84	5.62	1
1.75	41.17	0.81	40.36	34.60	5.75	1

1.74	42.07	0.82	41.25	35.36	5.88	1
1.73	42.98	0.84	42.14	36.12	6.01	1
1.72	43.88	0.86	43.02	36.88	6.14	1
1.70	44.78	0.87	43.91	37.64	6.27	1
1.69	45.69	0.89	44.80	38.40	6.40	1
1.68	46.59	0.91	45.69	39.15	6.53	1
1.67	47.49	0.92	46.57	39.91	6.66	1
1.66	48.40	0.94	47.46	40.67	6.79	1
1.64	49.30	0.96	48.34	41.42	6.92	1
1.63	50.20	0.97	49.23	42.18	7.05	1
1.62	51.10	0.99	50.11	42.93	7.18	1
1.61	52.00	1.01	50.99	43.69	7.30	1
1.60	52.90	1.03	51.88	44.44	7.43	1
1.58	53.80	1.04	52.76	45.20	7.56	1
1.57	54.70	1.06	53.64	45.95	7.69	1
1.56	55.60	1.08	54.52	46.70	7.82	1
1.55	56.50	1.10	55.40	47.46	7.94	1
1.53	57.40	1.11	56.28	48.21	8.07	1
1.52	58.29	1.13	57.16	48.96	8.20	1
1.51	59.19	1.15	58.04	49.71	8.33	1
1.50	60.09	1.17	58.92	50.46	8.45	1
1.49	60.98	1.19	59.79	51.21	8.58	1
1.47	61.88	1.21	60.67	51.96	8.71	1
1.46	62.77	1.23	61.55	52.71	8.83	1
1.45	63.67	1.25	62.42	53.46	8.96	1
1.44	64.56	1.27	63.29	54.21	9.09	1
1.43	65.46	1.29	64.17	54.96	9.21	1
1.41	66.35	1.31	65.04	55.70	9.34	1
1.40	67.24	1.33	65.91	56.45	9.46	1
1.39	68.13	1.35	66.78	57.20	9.59	1
1.38	69.03	1.37	67.65	57.94	9.71	1
1.37	69.92	1.39	68.52	58.69	9.84	1
1.36	70.81	1.41	69.39	59.43	9.96	1
1.34	71.70	1.43	70.26	60.18	10.09	1
1.33	72.59	1.46	71.13	60.92	10.21	1
1.33	72.59	1.46	71.13	60.92	10.21	1
1.32	73.47	1.48	72.00	61.66	10.33	1
1.31	74.36	1.50	72.86	62.41	10.46	1
1.30	75.25	1.52	73.73	63.15	10.58	1
1.28	76.14	1.55	74.59	63.89	10.70	1
1.27	77.02	1.57	75.45	64.63	10.82	1
1.26	77.91	1.59	76.32	65.37	10.95	1
1.25	78.80	1.62	77.18	66.11	11.07	1
1.24	79.68	1.64	78.04	66.85	11.19	1
1.22	80.56	1.67	78.90	67.59	11.31	1
1.21	81.45	1.69	79.76	68.32	11.43	1
1.20	82.33	1.72	80.61	69.06	11.55	1
1.19	83.21	1.74	81.47	69.80	11.67	1
1.18	84.09	1.77	82.33	70.53	11.79	1
1.17	84.98	1.80	83.18	71.27	11.91	1
1.15	85.86	1.82	84.03	72.00	12.03	1
1.14	86.73	1.85	84.89	72.74	12.15	1
1.13	87.61	1.88	85.74	73.47	12.27	1
1.12	88.49	1.90	86.59	74.20	12.39	1

1.11	89.37	1.93	87.44	74.93	12.50	1
1.10	90.25	1.96	88.29	75.66	12.62	1
1.08	91.12	1.99	89.13	76.39	12.74	1
1.07	92.00	2.02	89.98	77.12	12.85	1
1.06	92.87	2.06	90.82	77.85	12.96	1
1.05	93.75	2.09	91.66	78.58	13.08	1
1.04	94.62	2.12	92.50	79.31	13.19	1
1.02	95.49	2.16	93.33	80.03	13.30	1
1.01	96.36	2.19	94.17	80.76	13.41	1
1.00	97.23	2.23	95.01	81.48	13.52	1
0.99	98.10	2.26	95.84	82.21	13.63	1
0.98	98.97	2.30	96.67	82.93	13.74	1
0.97	99.84	2.33	97.51	83.65	13.85	1
0.96	100.71	2.37	98.34	84.38	13.96	1
0.94	101.58	2.41	99.17	85.10	14.07	1
0.93	102.44	2.44	100.00	85.82	14.18	1
0.92	103.31	2.48	100.83	86.54	14.29	1
0.91	104.17	2.52	101.65	87.25	14.40	1
0.90	105.03	2.55	102.48	87.97	14.51	1
0.89	105.90	2.59	103.31	88.69	14.62	1
0.87	106.76	2.63	104.13	89.40	14.72	1
0.86	107.62	2.67	104.95	90.12	14.83	1
0.86	107.62	2.67	104.95	90.12	14.83	1
0.84	109.17	2.74	106.43	91.41	15.03	1
0.82	110.71	2.81	107.90	92.69	15.22	1
0.80	112.25	2.88	109.37	93.97	15.41	1
0.78	113.79	2.95	110.84	95.24	15.60	1
0.76	115.33	3.02	112.30	96.52	15.79	1
0.74	116.86	3.10	113.76	97.79	15.98	1
0.72	118.39	3.17	115.22	99.05	16.16	1
0.70	119.92	3.25	116.67	100.32	16.35	1
0.68	121.44	3.33	118.12	101.58	16.54	1
0.66	122.96	3.40	119.56	102.84	16.72	1
0.64	124.48	3.48	121.00	104.09	16.90	1
0.62	126.00	3.56	122.43	105.35	17.09	1
0.60	127.51	3.64	123.86	106.60	17.27	1
0.58	129.01	3.73	125.29	107.84	17.45	1
0.56	130.52	3.81	126.71	109.08	17.63	1
0.54	132.02	3.89	128.13	110.32	17.81	1
0.52	133.52	3.98	129.54	111.56	17.98	1
0.50	135.01	4.06	130.95	112.79	18.16	1
0.48	136.50	4.15	132.35	114.02	18.33	1
0.46	137.99	4.24	133.75	115.24	18.51	1
0.44	139.48	4.33	135.15	116.46	18.68	1
0.42	140.96	4.42	136.53	117.68	18.85	1
0.40	142.43	4.51	137.92	118.90	19.02	1
0.38	143.91	4.61	139.30	120.11	19.19	1
0.36	145.37	4.70	140.67	121.31	19.36	1
0.34	146.84	4.80	142.04	122.52	19.52	1
0.32	148.30	4.90	143.40	123.71	19.69	1
0.31	149.76	5.00	144.76	124.91	19.85	1
0.29	151.21	5.22	146.00	126.10	19.90	1
0.27	152.66	5.44	147.22	127.29	19.94	1
0.25	154.11	5.66	148.45	128.47	19.98	1

0.23	155.55	5.87	149.67	129.65	20.02	1
0.21	156.98	6.09	150.89	130.82	20.07	1
0.19	158.42	6.31	152.11	131.99	20.12	1
0.17	159.85	6.52	153.32	133.16	20.16	1
0.15	161.27	6.74	154.53	134.32	20.21	1
0.14	162.69	6.95	155.74	135.48	20.26	1
0.12	164.11	7.16	156.95	136.64	20.31	1
0.10	165.53	7.38	158.15	137.79	20.36	1
0.08	166.94	7.59	159.35	138.94	20.41	1
0.08	166.94	7.59	159.35	138.94	20.41	1
0.06	168.19	7.78	160.41	139.96	20.46	1
0.05	169.43	7.96	161.47	140.97	20.50	1
0.03	170.68	8.15	162.53	141.98	20.55	1
0.02	171.92	8.34	163.58	142.99	20.60	1
0.00	173.16	8.52	164.64	143.99	20.64	1

Time = 85. Degree of Consolidation = 35.0%

Total Settlement = 0.192

Settlement at End of Primary Consolidation = 0.557

Settlement caused by Primary Consolidation at time 85. = 0.192

Settlement caused by Secondary Compression at time 85. = 0.000

Surface Elevation = 1.38

*****Current Conditions in Dredged Fill*****

***** Coordinates *****

***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
2.50	2.25	0.28	7.97	7.97	7.97	1
2.49	2.24	0.28	7.97	7.96	7.93	1
2.48	2.23	0.28	7.97	7.94	7.89	1
2.46	2.21	0.27	7.97	7.93	7.84	1
2.45	2.20	0.27	7.97	7.92	7.80	1
2.44	2.19	0.27	7.97	7.91	7.76	1
2.43	2.18	0.27	7.97	7.89	7.72	1
2.41	2.16	0.27	7.97	7.88	7.67	1
2.40	2.15	0.27	7.97	7.87	7.63	1
2.39	2.14	0.27	7.97	7.86	7.59	1
2.38	2.13	0.26	7.97	7.85	7.55	1
2.36	2.11	0.26	7.97	7.84	7.50	1
2.35	2.10	0.26	7.97	7.83	7.46	1
2.34	2.09	0.26	7.97	7.82	7.42	1
2.33	2.08	0.26	7.97	7.81	7.38	1
2.31	2.07	0.26	7.97	7.80	7.34	1

2.30	2.05	0.26	7.97	7.79	7.30	1
2.29	2.04	0.26	7.97	7.78	7.27	1
2.27	2.03	0.25	7.97	7.77	7.23	1
2.26	2.02	0.25	7.97	7.76	7.19	1
2.25	2.00	0.25	7.97	7.75	7.15	1
2.24	1.99	0.25	7.97	7.74	7.12	1
2.22	1.98	0.25	7.97	7.73	7.08	1
2.21	1.97	0.25	7.97	7.72	7.04	1
2.20	1.96	0.25	7.97	7.71	7.01	1
2.19	1.94	0.24	7.97	7.71	6.97	1
2.17	1.93	0.24	7.97	7.70	6.93	1
2.16	1.92	0.24	7.97	7.69	6.89	1
2.15	1.91	0.24	7.97	7.68	6.86	1
2.14	1.89	0.24	7.97	7.67	6.82	1
2.12	1.88	0.24	7.97	7.67	6.78	1
2.11	1.87	0.24	7.97	7.66	6.74	1
2.10	1.86	0.23	7.97	7.65	6.71	1
2.09	1.85	0.23	7.97	7.64	6.67	1
2.07	1.83	0.23	7.97	7.64	6.63	1
2.06	1.82	0.23	7.97	7.63	6.61	1
2.05	1.81	0.23	7.97	7.62	6.59	1
2.04	1.80	0.23	7.97	7.61	6.57	1
2.02	1.79	0.23	7.97	7.61	6.56	1
2.01	1.77	0.22	7.97	7.60	6.54	1
2.00	1.76	0.22	7.97	7.59	6.52	1
2.00	1.76	0.22	7.97	7.59	6.52	1
1.99	1.75	0.22	7.97	7.58	6.51	1
1.97	1.74	0.22	7.97	7.58	6.49	1
1.96	1.73	0.22	7.97	7.57	6.47	1
1.95	1.71	0.22	7.97	7.56	6.46	1
1.94	1.70	0.22	7.97	7.56	6.44	1
1.92	1.69	0.21	7.97	7.55	6.42	1
1.91	1.68	0.21	7.97	7.54	6.40	1
1.90	1.67	0.21	7.97	7.54	6.39	1
1.89	1.66	0.21	7.97	7.53	6.37	1
1.87	1.64	0.21	7.97	7.52	6.35	1
1.86	1.63	0.21	7.97	7.51	6.34	1
1.85	1.62	0.21	7.97	7.51	6.32	1
1.84	1.61	0.20	7.97	7.50	6.30	1
1.82	1.60	0.20	7.97	7.49	6.29	1
1.81	1.58	0.20	7.97	7.49	6.27	1
1.80	1.57	0.20	7.97	7.48	6.25	1
1.79	1.56	0.20	7.97	7.47	6.24	1
1.77	1.55	0.20	7.97	7.46	6.22	1
1.76	1.54	0.20	7.97	7.46	6.20	1
1.75	1.52	0.20	7.97	7.45	6.19	1
1.74	1.51	0.19	7.97	7.44	6.17	1
1.72	1.50	0.19	7.97	7.44	6.15	1
1.71	1.49	0.19	7.97	7.43	6.13	1
1.70	1.48	0.19	7.97	7.42	6.12	1
1.69	1.47	0.19	7.97	7.41	6.10	1
1.67	1.45	0.19	7.97	7.41	6.08	1
1.66	1.44	0.19	7.97	7.40	6.07	1
1.65	1.43	0.18	7.97	7.39	6.05	1

1.64	1.42	0.18	7.97	7.38	6.04	1
1.62	1.41	0.18	7.97	7.38	6.03	1
1.61	1.40	0.18	7.97	7.37	6.02	1
1.60	1.38	0.18	7.97	7.36	6.01	1
1.59	1.37	0.18	7.97	7.35	6.00	1
1.57	1.36	0.18	7.97	7.35	5.99	1
1.56	1.35	0.17	7.97	7.34	5.99	1
1.55	1.34	0.17	7.97	7.33	5.98	1
1.54	1.33	0.17	7.97	7.32	5.97	1
1.52	1.31	0.17	7.97	7.32	5.96	1
1.51	1.30	0.17	7.97	7.31	5.95	1
1.50	1.29	0.17	7.97	7.30	5.94	1
1.50	1.29	0.17	7.97	7.30	5.94	1
1.49	1.28	0.17	7.97	7.29	5.93	1
1.47	1.27	0.16	7.97	7.28	5.93	1
1.46	1.26	0.16	7.97	7.28	5.92	1
1.45	1.25	0.16	7.97	7.27	5.91	1
1.44	1.23	0.16	7.97	7.26	5.90	1
1.42	1.22	0.16	7.97	7.25	5.89	1
1.41	1.21	0.16	7.97	7.24	5.88	1
1.40	1.20	0.16	7.97	7.24	5.88	1
1.39	1.19	0.15	7.97	7.23	5.87	1
1.37	1.18	0.15	7.97	7.22	5.86	1
1.36	1.16	0.15	7.97	7.21	5.85	1
1.35	1.15	0.15	7.97	7.20	5.84	1
1.34	1.14	0.15	7.97	7.19	5.83	1
1.32	1.13	0.15	7.97	7.19	5.82	1
1.31	1.12	0.15	7.97	7.18	5.82	1
1.30	1.11	0.14	7.97	7.17	5.81	1
1.29	1.10	0.14	7.97	7.16	5.80	1
1.27	1.09	0.14	7.97	7.15	5.79	1
1.26	1.07	0.14	7.97	7.14	5.78	1
1.25	1.06	0.14	7.97	7.14	5.77	1
1.24	1.05	0.14	7.97	7.13	5.77	1
1.22	1.04	0.14	7.97	7.12	5.76	1
1.21	1.03	0.14	7.97	7.11	5.75	1
1.20	1.02	0.13	7.97	7.10	5.74	1
1.19	1.01	0.13	7.97	7.09	5.73	1
1.17	0.99	0.13	7.97	7.08	5.72	1
1.16	0.98	0.13	7.97	7.07	5.72	1
1.15	0.97	0.13	7.97	7.07	5.71	1
1.14	0.96	0.13	7.97	7.06	5.70	1
1.12	0.95	0.13	7.97	7.05	5.69	1
1.11	0.94	0.12	7.97	7.04	5.68	1
1.10	0.93	0.12	7.97	7.03	5.67	1
1.09	0.92	0.12	7.97	7.02	5.66	1
1.07	0.90	0.12	7.97	7.01	5.66	1
1.06	0.89	0.12	7.97	7.00	5.65	1
1.05	0.88	0.12	7.97	6.99	5.64	1
1.04	0.87	0.12	7.97	6.98	5.63	1
1.02	0.86	0.11	7.97	6.97	5.62	1
1.01	0.85	0.11	7.97	6.96	5.61	1
1.00	0.84	0.11	7.97	6.95	5.61	1
1.00	0.84	0.11	7.97	6.95	5.61	1

0.98	0.82	0.11	7.97	6.94	5.59	1
0.95	0.80	0.11	7.97	6.92	5.57	1
0.93	0.78	0.10	7.97	6.90	5.56	1
0.91	0.76	0.10	7.97	6.88	5.54	1
0.89	0.74	0.10	7.97	6.87	5.53	1
0.86	0.72	0.10	7.97	6.85	5.51	1
0.84	0.70	0.09	7.97	6.83	5.50	1
0.82	0.68	0.09	7.97	6.81	5.48	1
0.80	0.66	0.09	7.97	6.79	5.47	1
0.77	0.64	0.09	7.97	6.77	5.46	1
0.75	0.62	0.08	7.97	6.75	5.45	1
0.73	0.60	0.08	7.97	6.73	5.44	1
0.71	0.58	0.08	7.97	6.71	5.43	1
0.68	0.56	0.08	7.97	6.69	5.42	1
0.66	0.54	0.07	7.97	6.67	5.41	1
0.64	0.52	0.07	7.97	6.65	5.40	1
0.62	0.51	0.07	7.97	6.63	5.40	1
0.59	0.49	0.07	7.97	6.61	5.39	1
0.57	0.47	0.06	7.97	6.59	5.38	1
0.55	0.45	0.06	7.97	6.57	5.37	1
0.53	0.43	0.06	7.97	6.55	5.36	1
0.51	0.41	0.06	7.97	6.53	5.35	1
0.48	0.39	0.05	7.97	6.50	5.34	1
0.46	0.37	0.05	7.97	6.48	5.33	1
0.44	0.35	0.05	7.97	6.46	5.33	1
0.42	0.34	0.05	7.97	6.44	5.32	1
0.39	0.32	0.04	7.97	6.42	5.31	1
0.37	0.30	0.04	7.97	6.40	5.30	1
0.35	0.28	0.04	7.97	6.38	5.29	1
0.33	0.26	0.04	7.97	6.36	5.28	1
0.30	0.24	0.03	7.97	6.34	5.27	1
0.28	0.22	0.03	7.97	6.32	5.27	1
0.26	0.21	0.03	7.97	6.30	5.26	1
0.23	0.19	0.03	7.97	6.28	5.25	1
0.21	0.17	0.02	7.97	6.25	5.24	1
0.19	0.15	0.02	7.97	6.23	5.23	1
0.17	0.13	0.02	7.97	6.21	5.22	1
0.14	0.12	0.02	7.97	6.19	5.21	1
0.12	0.10	0.01	7.97	6.17	5.20	1
0.10	0.08	0.01	7.97	6.15	5.20	1
0.10	0.08	0.01	7.97	6.15	5.20	1
0.08	0.06	0.01	7.97	6.13	5.19	1
0.06	0.05	0.01	7.97	6.11	5.18	1
0.04	0.03	0.00	7.97	6.10	5.17	1
0.02	0.02	0.00	7.97	6.08	5.17	1
0.00	0.00	0.00	7.97	6.06	5.16	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
2.25	0.00	0.00	0.00	0.00	0.00	1
2.24	0.93	0.05	0.88	0.78	0.10	1
2.23	1.85	0.09	1.76	1.56	0.20	1

2.21	2.77	0.14	2.64	2.33	0.30	1
2.20	3.69	0.18	3.52	3.11	0.40	1
2.19	4.61	0.22	4.39	3.89	0.51	1
2.18	5.53	0.26	5.27	4.66	0.61	1
2.16	6.45	0.30	6.15	5.43	0.72	1
2.15	7.37	0.34	7.03	6.20	0.82	1
2.14	8.29	0.38	7.91	6.98	0.93	1
2.13	9.20	0.42	8.78	7.75	1.04	1
2.11	10.12	0.46	9.66	8.51	1.15	1
2.10	11.03	0.49	10.54	9.28	1.26	1
2.09	11.95	0.53	11.42	10.05	1.37	1
2.08	12.86	0.56	12.29	10.82	1.48	1
2.07	13.77	0.60	13.17	11.58	1.59	1
2.05	14.68	0.63	14.05	12.35	1.70	1
2.04	15.59	0.66	14.92	13.11	1.82	1
2.03	16.50	0.70	15.80	13.87	1.93	1
2.02	17.40	0.73	16.68	14.63	2.04	1
2.00	18.31	0.76	17.55	15.40	2.16	1
1.99	19.22	0.79	18.43	16.16	2.27	1
1.98	20.12	0.82	19.30	16.92	2.39	1
1.97	21.03	0.85	20.18	17.67	2.50	1
1.96	21.93	0.88	21.05	18.43	2.62	1
1.94	22.84	0.91	21.93	19.19	2.74	1
1.93	23.74	0.94	22.80	19.95	2.85	1
1.92	24.64	0.96	23.68	20.70	2.97	1
1.91	25.54	0.99	24.55	21.46	3.09	1
1.89	26.44	1.02	25.42	22.21	3.21	1
1.88	27.34	1.05	26.29	22.97	3.33	1
1.87	28.24	1.07	27.17	23.72	3.45	1
1.86	29.14	1.10	28.04	24.47	3.57	1
1.85	30.04	1.13	28.91	25.22	3.69	1
1.83	30.93	1.15	29.78	25.98	3.81	1
1.82	31.83	1.18	30.65	26.73	3.93	1
1.81	32.73	1.20	31.52	27.48	4.05	1
1.80	33.62	1.23	32.39	28.23	4.17	1
1.79	34.52	1.25	33.26	28.97	4.29	1
1.77	35.41	1.28	34.13	29.72	4.41	1
1.76	36.30	1.30	35.00	30.47	4.53	1
1.76	36.30	1.30	35.00	30.47	4.53	1
1.75	37.20	1.33	35.87	31.22	4.65	1
1.74	38.09	1.35	36.73	31.96	4.77	1
1.73	38.98	1.38	37.60	32.71	4.89	1
1.71	39.87	1.40	38.47	33.45	5.01	1
1.70	40.76	1.43	39.33	34.20	5.14	1
1.69	41.65	1.45	40.20	34.94	5.26	1
1.68	42.54	1.48	41.06	35.68	5.38	1
1.67	43.43	1.50	41.93	36.43	5.50	1
1.66	44.31	1.52	42.79	37.17	5.62	1
1.64	45.20	1.55	43.65	37.91	5.74	1
1.63	46.09	1.57	44.52	38.65	5.86	1
1.62	46.97	1.60	45.38	39.39	5.99	1
1.61	47.86	1.62	46.24	40.13	6.11	1
1.60	48.74	1.64	47.10	40.87	6.23	1
1.58	49.63	1.67	47.96	41.61	6.35	1

1.57	50.51	1.69	48.82	42.34	6.47	1
1.56	51.39	1.72	49.68	43.08	6.59	1
1.55	52.28	1.74	50.53	43.82	6.72	1
1.54	53.16	1.77	51.39	44.55	6.84	1
1.52	54.04	1.79	52.25	45.29	6.96	1
1.51	54.92	1.82	53.10	46.02	7.08	1
1.50	55.80	1.84	53.96	46.76	7.20	1
1.49	56.68	1.87	54.81	47.49	7.32	1
1.48	57.56	1.89	55.66	48.22	7.44	1
1.47	58.43	1.92	56.52	48.96	7.56	1
1.45	59.31	1.94	57.37	49.69	7.68	1
1.44	60.19	1.97	58.22	50.42	7.80	1
1.43	61.06	1.99	59.07	51.15	7.92	1
1.42	61.94	2.02	59.92	51.88	8.04	1
1.41	62.81	2.05	60.76	52.61	8.15	1
1.40	63.69	2.08	61.60	53.33	8.27	1
1.38	64.56	2.11	62.45	54.06	8.39	1
1.37	65.43	2.14	63.29	54.79	8.50	1
1.36	66.30	2.17	64.13	55.51	8.62	1
1.35	67.18	2.20	64.97	56.24	8.74	1
1.34	68.05	2.23	65.81	56.96	8.85	1
1.33	68.92	2.26	66.65	57.69	8.97	1
1.31	69.79	2.29	67.49	58.41	9.08	1
1.30	70.65	2.32	68.33	59.13	9.20	1
1.29	71.52	2.35	69.17	59.86	9.31	1
1.29	71.52	2.35	69.17	59.86	9.31	1
1.28	72.39	2.38	70.01	60.58	9.43	1
1.27	73.26	2.41	70.84	61.30	9.54	1
1.26	74.12	2.44	71.68	62.02	9.66	1
1.25	74.99	2.48	72.51	62.74	9.77	1
1.23	75.85	2.51	73.34	63.46	9.89	1
1.22	76.71	2.54	74.18	64.17	10.00	1
1.21	77.58	2.57	75.01	64.89	10.12	1
1.20	78.44	2.60	75.84	65.61	10.23	1
1.19	79.30	2.63	76.67	66.32	10.35	1
1.18	80.16	2.66	77.50	67.04	10.46	1
1.16	81.02	2.70	78.33	67.75	10.57	1
1.15	81.88	2.73	79.15	68.47	10.69	1
1.14	82.74	2.76	79.98	69.18	10.80	1
1.13	83.60	2.79	80.81	69.89	10.91	1
1.12	84.46	2.83	81.63	70.60	11.03	1
1.11	85.31	2.86	82.45	71.31	11.14	1
1.10	86.17	2.89	83.28	72.02	11.25	1
1.09	87.02	2.92	84.10	72.73	11.37	1
1.07	87.88	2.96	84.92	73.44	11.48	1
1.06	88.73	2.99	85.74	74.15	11.59	1
1.05	89.59	3.02	86.56	74.86	11.70	1
1.04	90.44	3.06	87.38	75.56	11.82	1
1.03	91.29	3.09	88.20	76.27	11.93	1
1.02	92.14	3.13	89.01	76.97	12.04	1
1.01	92.99	3.16	89.83	77.68	12.15	1
0.99	93.84	3.19	90.64	78.38	12.26	1
0.98	94.69	3.23	91.46	79.08	12.37	1
0.97	95.53	3.26	92.27	79.78	12.49	1

0.96	96.38	3.30	93.08	80.49	12.60	1
0.95	97.23	3.33	93.89	81.19	12.71	1
0.94	98.07	3.37	94.70	81.89	12.82	1
0.93	98.92	3.40	95.51	82.58	12.93	1
0.92	99.76	3.44	96.32	83.28	13.04	1
0.90	100.60	3.48	97.13	83.98	13.15	1
0.89	101.45	3.51	97.93	84.68	13.26	1
0.88	102.29	3.55	98.74	85.37	13.37	1
0.87	103.13	3.59	99.54	86.07	13.48	1
0.86	103.97	3.62	100.34	86.76	13.59	1
0.85	104.81	3.66	101.15	87.45	13.69	1
0.84	105.64	3.70	101.95	88.14	13.80	1
0.84	105.64	3.70	101.95	88.14	13.80	1
0.82	107.15	3.76	103.39	89.39	14.00	1
0.80	108.65	3.83	104.82	90.63	14.19	1
0.78	110.15	3.90	106.25	91.87	14.39	1
0.76	111.65	3.97	107.68	93.10	14.58	1
0.74	113.15	4.04	109.11	94.34	14.77	1
0.72	114.64	4.11	110.53	95.56	14.96	1
0.70	116.13	4.18	111.94	96.79	15.15	1
0.68	117.61	4.26	113.36	98.02	15.34	1
0.66	119.10	4.33	114.77	99.24	15.53	1
0.64	120.58	4.40	116.17	100.46	15.72	1
0.62	122.06	4.48	117.58	101.67	15.91	1
0.60	123.53	4.56	118.97	102.88	16.09	1
0.58	125.00	4.63	120.37	104.09	16.28	1
0.56	126.47	4.71	121.76	105.30	16.46	1
0.54	127.94	4.79	123.14	106.50	16.64	1
0.52	129.40	4.87	124.53	107.70	16.83	1
0.51	130.86	4.95	125.90	108.90	17.01	1
0.49	132.31	5.08	127.23	110.09	17.14	1
0.47	133.76	5.27	128.50	111.28	17.22	1
0.45	135.21	5.45	129.76	112.46	17.30	1
0.43	136.66	5.63	131.03	113.65	17.38	1
0.41	138.10	5.81	132.29	114.83	17.46	1
0.39	139.54	6.00	133.54	116.00	17.54	1
0.37	140.97	6.18	134.80	117.18	17.62	1
0.35	142.41	6.36	136.05	118.35	17.70	1
0.34	143.84	6.54	137.30	119.51	17.78	1
0.32	145.26	6.72	138.54	120.67	17.87	1
0.30	146.68	6.90	139.78	121.83	17.95	1
0.28	148.10	7.08	141.02	122.99	18.03	1
0.26	149.52	7.26	142.26	124.14	18.12	1
0.24	150.93	7.44	143.49	125.29	18.20	1
0.22	152.34	7.62	144.72	126.44	18.28	1
0.21	153.75	7.80	145.95	127.58	18.37	1
0.19	155.15	7.97	147.18	128.73	18.45	1
0.17	156.55	8.15	148.40	129.86	18.53	1
0.15	157.94	8.33	149.61	131.00	18.62	1
0.13	159.34	8.51	150.83	132.13	18.70	1
0.12	160.73	8.69	152.04	133.25	18.79	1
0.10	162.11	8.86	153.25	134.38	18.87	1
0.08	163.50	9.04	154.46	135.50	18.96	1
0.08	163.50	9.04	154.46	135.50	18.96	1

0.06	164.72	9.20	155.52	136.49	19.03	1
0.05	165.95	9.36	156.59	137.48	19.11	1
0.03	167.17	9.52	157.65	138.47	19.18	1
0.02	168.39	9.67	158.72	139.46	19.26	1
0.00	169.61	9.83	159.77	140.44	19.33	1

Time = 115. Degree of Consolidation = 45.0%

Total Settlement = 0.249

Settlement at End of Primary Consolidation = 0.557

Settlement caused by Primary Consolidation at time 115. = 0.249

Settlement caused by Secondary Compression at time 115. = 0.000

Settlement Due to Desiccation = 0.000

Surface Elevation = 1.32

*****Current Conditions in Dredged Fill*****

***** Coordinates *****

***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
2.50	2.01	0.28	7.97	2.26	2.26	1
2.49	2.01	0.28	7.97	2.26	2.26	1
2.48	2.00	0.28	7.97	2.26	2.26	1
2.46	2.00	0.27	7.97	2.26	2.26	1
2.45	1.99	0.27	7.97	2.26	2.26	1
2.44	1.99	0.27	7.97	2.26	2.26	1
2.43	1.98	0.27	7.97	2.26	2.26	1
2.41	1.98	0.27	7.97	2.26	2.26	1
2.40	1.97	0.27	7.97	2.26	2.26	1
2.39	1.97	0.27	7.97	2.26	2.26	1
2.38	1.96	0.26	7.97	2.26	2.26	1
2.36	1.96	0.26	7.97	2.26	2.26	1
2.35	1.95	0.26	7.97	4.56	6.94	1
2.34	1.95	0.26	7.97	5.14	6.91	1
2.33	1.94	0.26	7.97	5.14	6.87	1
2.31	1.93	0.26	7.97	5.14	6.83	1
2.30	1.92	0.26	7.97	5.14	6.79	1
2.29	1.91	0.26	7.97	5.14	6.76	1
2.27	1.90	0.25	7.97	5.14	6.72	1
2.26	1.89	0.25	7.97	5.14	6.68	1
2.25	1.89	0.25	7.97	5.14	6.64	1
2.24	1.88	0.25	7.97	5.14	6.61	1
2.22	1.87	0.25	7.97	5.14	6.60	1
2.21	1.86	0.25	7.97	5.14	6.58	1

2.20	1.85	0.25	7.97	5.14	6.56	1
2.19	1.84	0.24	7.97	5.14	6.55	1
2.17	1.83	0.24	7.97	5.14	6.53	1
2.16	1.83	0.24	7.97	5.14	6.51	1
2.15	1.82	0.24	7.97	5.14	6.50	1
2.14	1.81	0.24	7.97	5.14	6.48	1
2.12	1.80	0.24	7.97	5.14	6.46	1
2.11	1.79	0.24	7.97	5.14	6.44	1
2.10	1.78	0.23	7.97	5.14	6.43	1
2.09	1.77	0.23	7.97	5.14	6.41	1
2.07	1.77	0.23	7.97	5.14	6.39	1
2.06	1.76	0.23	7.97	5.14	6.38	1
2.05	1.75	0.23	7.97	5.14	6.36	1
2.04	1.74	0.23	7.97	5.14	6.34	1
2.02	1.73	0.23	7.97	5.14	6.33	1
2.01	1.72	0.22	7.97	5.14	6.31	1
2.00	1.71	0.22	7.97	5.14	6.29	1
2.00	1.71	0.22	7.97	5.14	6.29	1
1.99	1.71	0.22	7.97	5.14	6.28	1
1.97	1.70	0.22	7.97	7.41	6.26	1
1.96	1.68	0.22	7.97	7.40	6.24	1
1.95	1.67	0.22	7.97	7.39	6.22	1
1.94	1.66	0.22	7.97	7.38	6.21	1
1.92	1.65	0.21	7.97	7.37	6.19	1
1.91	1.64	0.21	7.97	7.37	6.17	1
1.90	1.63	0.21	7.97	7.36	6.16	1
1.89	1.61	0.21	7.97	7.35	6.14	1
1.87	1.60	0.21	7.97	7.34	6.12	1
1.86	1.59	0.21	7.97	7.33	6.11	1
1.85	1.58	0.21	7.97	7.32	6.09	1
1.84	1.57	0.20	7.97	7.31	6.07	1
1.82	1.56	0.20	7.97	7.30	6.06	1
1.81	1.55	0.20	7.97	7.29	6.04	1
1.80	1.53	0.20	7.97	7.28	6.03	1
1.79	1.52	0.20	7.97	7.28	6.02	1
1.77	1.51	0.20	7.97	7.27	6.01	1
1.76	1.50	0.20	7.97	7.26	6.01	1
1.75	1.49	0.20	7.97	7.25	6.00	1
1.74	1.48	0.19	7.97	7.24	5.99	1
1.72	1.46	0.19	7.97	7.23	5.98	1
1.71	1.45	0.19	7.97	7.23	5.97	1
1.70	1.44	0.19	7.97	7.22	5.96	1
1.69	1.43	0.19	7.97	7.21	5.95	1
1.67	1.42	0.19	7.97	7.20	5.95	1
1.66	1.41	0.19	7.97	7.19	5.94	1
1.65	1.40	0.18	7.97	7.18	5.93	1
1.64	1.38	0.18	7.97	7.18	5.92	1
1.62	1.37	0.18	7.97	7.17	5.91	1
1.61	1.36	0.18	7.97	7.16	5.90	1
1.60	1.35	0.18	7.97	7.15	5.90	1
1.59	1.34	0.18	7.97	7.14	5.89	1
1.57	1.33	0.18	7.97	7.14	5.88	1
1.56	1.32	0.17	7.97	7.13	5.87	1
1.55	1.31	0.17	7.97	7.12	5.86	1

1.54	1.29	0.17	7.97	7.11	5.85	1
1.52	1.28	0.17	7.97	7.10	5.84	1
1.51	1.27	0.17	7.97	7.10	5.84	1
1.50	1.26	0.17	7.97	7.09	5.83	1
1.50	1.26	0.17	7.97	7.09	5.83	1
1.49	1.25	0.17	7.97	7.08	5.82	1
1.47	1.24	0.16	7.97	7.07	5.81	1
1.46	1.23	0.16	7.97	7.06	5.80	1
1.45	1.21	0.16	7.97	7.06	5.79	1
1.44	1.20	0.16	7.97	7.05	5.79	1
1.42	1.19	0.16	7.97	7.04	5.78	1
1.41	1.18	0.16	7.97	7.03	5.77	1
1.40	1.17	0.16	7.97	7.02	5.76	1
1.39	1.16	0.15	7.97	7.01	5.75	1
1.37	1.15	0.15	7.97	7.01	5.74	1
1.36	1.14	0.15	7.97	7.00	5.73	1
1.35	1.13	0.15	7.97	6.99	5.73	1
1.34	1.11	0.15	7.97	6.98	5.72	1
1.32	1.10	0.15	7.97	6.97	5.71	1
1.31	1.09	0.15	7.97	6.96	5.70	1
1.30	1.08	0.14	7.97	6.96	5.69	1
1.29	1.07	0.14	7.97	6.95	5.68	1
1.27	1.06	0.14	7.97	6.94	5.68	1
1.26	1.05	0.14	7.97	6.93	5.67	1
1.25	1.04	0.14	7.97	6.92	5.66	1
1.24	1.03	0.14	7.97	6.91	5.65	1
1.22	1.01	0.14	7.97	6.90	5.64	1
1.21	1.00	0.14	7.97	6.90	5.63	1
1.20	0.99	0.13	7.97	6.89	5.62	1
1.19	0.98	0.13	7.97	6.88	5.62	1
1.17	0.97	0.13	7.97	6.87	5.61	1
1.16	0.96	0.13	7.97	6.86	5.60	1
1.15	0.95	0.13	7.97	6.85	5.59	1
1.14	0.94	0.13	7.97	6.84	5.58	1
1.12	0.93	0.13	7.97	6.84	5.57	1
1.11	0.92	0.12	7.97	6.83	5.57	1
1.10	0.91	0.12	7.97	6.82	5.56	1
1.09	0.89	0.12	7.97	6.81	5.55	1
1.07	0.88	0.12	7.97	6.80	5.54	1
1.06	0.87	0.12	7.97	6.79	5.53	1
1.05	0.86	0.12	7.97	6.78	5.52	1
1.04	0.85	0.12	7.97	6.77	5.51	1
1.02	0.84	0.11	7.97	6.76	5.51	1
1.01	0.83	0.11	7.97	6.75	5.50	1
1.00	0.82	0.11	7.97	6.74	5.49	1
1.00	0.82	0.11	7.97	6.74	5.49	1
0.98	0.80	0.11	7.97	6.73	5.47	1
0.95	0.78	0.11	7.97	6.71	5.46	1
0.93	0.76	0.10	7.97	6.69	5.45	1
0.91	0.74	0.10	7.97	6.67	5.44	1
0.89	0.72	0.10	7.97	6.66	5.43	1
0.86	0.70	0.10	7.97	6.64	5.42	1
0.84	0.68	0.09	7.97	6.62	5.42	1
0.82	0.66	0.09	7.97	6.60	5.41	1

0.80	0.65	0.09	7.97	6.58	5.40	1
0.77	0.63	0.09	7.97	6.57	5.39	1
0.75	0.61	0.08	7.97	6.55	5.38	1
0.73	0.59	0.08	7.97	6.53	5.37	1
0.71	0.57	0.08	7.97	6.51	5.36	1
0.68	0.55	0.08	7.97	6.49	5.36	1
0.66	0.53	0.07	7.97	6.47	5.35	1
0.64	0.51	0.07	7.97	6.46	5.34	1
0.62	0.49	0.07	7.97	6.44	5.33	1
0.59	0.48	0.07	7.97	6.42	5.32	1
0.57	0.46	0.06	7.97	6.40	5.31	1
0.55	0.44	0.06	7.97	6.38	5.30	1
0.53	0.42	0.06	7.97	6.37	5.29	1
0.51	0.40	0.06	7.97	6.35	5.29	1
0.48	0.38	0.05	7.97	6.33	5.28	1
0.46	0.37	0.05	7.97	6.31	5.27	1
0.44	0.35	0.05	7.97	6.29	5.26	1
0.42	0.33	0.05	7.97	6.27	5.25	1
0.39	0.31	0.04	7.97	6.26	5.24	1
0.37	0.29	0.04	7.97	6.24	5.23	1
0.35	0.27	0.04	7.97	6.22	5.23	1
0.33	0.26	0.04	7.97	6.20	5.22	1
0.30	0.24	0.03	7.97	6.18	5.21	1
0.28	0.22	0.03	7.97	6.16	5.20	1
0.26	0.20	0.03	7.97	6.14	5.19	1
0.23	0.18	0.03	7.97	6.13	5.18	1
0.21	0.17	0.02	7.97	6.11	5.17	1
0.19	0.15	0.02	7.97	6.09	5.16	1
0.17	0.13	0.02	7.97	6.07	5.16	1
0.14	0.11	0.02	7.97	6.05	5.15	1
0.12	0.10	0.01	7.97	6.03	5.14	1
0.10	0.08	0.01	7.97	6.02	5.13	1
0.10	0.08	0.01	7.97	6.02	5.13	1
0.08	0.06	0.01	7.97	6.00	5.12	1
0.06	0.05	0.01	7.97	5.98	5.12	1
0.04	0.03	0.00	7.97	5.97	5.11	1
0.02	0.02	0.00	7.97	5.95	5.11	1
0.00	0.00	0.00	7.97	5.94	5.10	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
2.01	0.00	0.00	0.00	0.00	0.00	1
2.01	0.30	0.30	0.00	0.00	0.00	1
2.00	0.61	0.61	0.00	0.00	0.00	1
2.00	0.91	0.91	0.00	0.00	0.00	1
1.99	1.21	1.21	0.00	0.00	0.00	1
1.99	1.51	1.51	0.00	0.00	0.00	1
1.98	1.82	1.82	0.00	0.00	0.00	1
1.98	2.12	2.12	0.00	0.00	0.00	1
1.97	2.42	2.42	0.00	0.00	0.00	1
1.97	2.72	2.72	0.00	0.00	0.00	1
1.96	3.03	3.03	0.00	0.00	0.00	1

1.96	3.33	3.33	0.00	0.00	0.00	1
1.95	3.74	3.74	0.00	0.00	0.00	1
1.95	4.41	3.89	0.52	0.52	0.00	1
1.94	5.09	4.03	1.05	1.05	0.00	1
1.93	5.77	4.18	1.59	1.59	0.00	1
1.92	6.45	4.33	2.12	2.12	0.00	1
1.91	7.13	4.47	2.65	2.65	0.00	1
1.90	7.81	4.62	3.19	3.19	0.00	1
1.89	8.49	4.76	3.72	3.72	0.00	1
1.89	9.17	4.91	4.26	4.26	0.00	1
1.88	9.85	5.05	4.79	4.79	0.00	1
1.87	10.53	5.20	5.33	5.33	0.00	1
1.86	11.21	5.35	5.86	5.86	0.00	1
1.85	11.89	5.49	6.39	6.39	0.00	1
1.84	12.57	5.64	6.93	6.93	0.00	1
1.83	13.25	5.78	7.46	7.46	0.00	1
1.83	13.93	5.93	8.00	8.00	0.00	1
1.82	14.61	6.08	8.53	8.53	0.00	1
1.81	15.29	6.22	9.07	9.07	0.00	1
1.80	15.97	6.37	9.60	9.60	0.00	1
1.79	16.65	6.51	10.13	10.13	0.00	1
1.78	17.33	6.66	10.67	10.67	0.00	1
1.77	18.01	6.80	11.20	11.20	0.00	1
1.77	18.69	6.95	11.74	11.74	0.00	1
1.76	19.37	7.10	12.27	12.27	0.00	1
1.75	20.05	7.24	12.81	12.81	0.00	1
1.74	20.73	7.39	13.34	13.34	0.00	1
1.73	21.41	7.53	13.87	13.87	0.00	1
1.72	22.09	7.68	14.41	14.41	0.00	1
1.71	22.77	7.83	14.94	14.94	0.00	1
1.71	22.77	7.83	14.94	14.94	0.00	1
1.71	23.39	7.97	15.42	15.42	0.00	1
1.70	24.19	1.92	22.28	16.08	6.20	1
1.68	25.07	1.95	23.12	16.81	6.31	1
1.67	25.95	1.99	23.96	17.54	6.42	1
1.66	26.82	2.02	24.80	18.27	6.53	1
1.65	27.70	2.06	25.64	19.00	6.64	1
1.64	28.57	2.10	26.47	19.72	6.75	1
1.63	29.44	2.13	27.31	20.45	6.86	1
1.61	30.32	2.17	28.15	21.18	6.97	1
1.60	31.19	2.20	28.98	21.90	7.08	1
1.59	32.06	2.24	29.82	22.63	7.19	1
1.58	32.93	2.27	30.65	23.35	7.30	1
1.57	33.80	2.31	31.49	24.07	7.41	1
1.56	34.66	2.34	32.32	24.80	7.52	1
1.55	35.53	2.38	33.15	25.52	7.64	1
1.53	36.40	2.41	33.99	26.24	7.75	1
1.52	37.26	2.44	34.82	26.96	7.86	1
1.51	38.13	2.48	35.65	27.68	7.97	1
1.50	38.99	2.51	36.48	28.40	8.09	1
1.49	39.86	2.54	37.31	29.11	8.20	1
1.48	40.72	2.58	38.14	29.83	8.31	1
1.46	41.58	2.61	38.97	30.55	8.43	1
1.45	42.44	2.64	39.80	31.26	8.54	1

1.44	43.30	2.67	40.63	31.98	8.65	1
1.43	44.16	2.70	41.46	32.69	8.77	1
1.42	45.02	2.74	42.29	33.41	8.88	1
1.41	45.88	2.77	43.11	34.12	8.99	1
1.40	46.74	2.80	43.94	34.83	9.11	1
1.38	47.60	2.83	44.76	35.54	9.22	1
1.37	48.45	2.86	45.59	36.25	9.34	1
1.36	49.31	2.90	46.41	36.96	9.45	1
1.35	50.16	2.93	47.24	37.67	9.57	1
1.34	51.02	2.96	48.06	38.38	9.68	1
1.33	51.87	2.99	48.88	39.09	9.79	1
1.32	52.72	3.02	49.70	39.80	9.91	1
1.31	53.58	3.05	50.52	40.50	10.02	1
1.29	54.43	3.08	51.34	41.21	10.14	1
1.28	55.28	3.12	52.16	41.91	10.25	1
1.27	56.13	3.15	52.98	42.62	10.37	1
1.26	56.98	3.18	53.80	43.32	10.48	1
1.26	56.98	3.18	53.80	43.32	10.48	1
1.25	57.83	3.21	54.62	44.02	10.59	1
1.24	58.68	3.24	55.43	44.73	10.71	1
1.23	59.52	3.27	56.25	45.43	10.82	1
1.21	60.37	3.30	57.07	46.13	10.94	1
1.20	61.22	3.34	57.88	46.83	11.05	1
1.19	62.06	3.37	58.69	47.53	11.16	1
1.18	62.91	3.40	59.51	48.23	11.28	1
1.17	63.75	3.43	60.32	48.92	11.39	1
1.16	64.59	3.46	61.13	49.62	11.51	1
1.15	65.43	3.50	61.94	50.32	11.62	1
1.14	66.28	3.53	62.75	51.01	11.73	1
1.13	67.12	3.56	63.56	51.71	11.85	1
1.11	67.96	3.59	64.36	52.40	11.96	1
1.10	68.80	3.63	65.17	53.10	12.07	1
1.09	69.64	3.66	65.98	53.79	12.19	1
1.08	70.47	3.69	66.78	54.48	12.30	1
1.07	71.31	3.72	67.59	55.17	12.41	1
1.06	72.15	3.76	68.39	55.86	12.53	1
1.05	72.98	3.79	69.19	56.55	12.64	1
1.04	73.82	3.82	70.00	57.24	12.75	1
1.03	74.65	3.86	70.80	57.93	12.86	1
1.01	75.49	3.89	71.60	58.62	12.98	1
1.00	76.32	3.92	72.40	59.31	13.09	1
0.99	77.15	3.96	73.19	59.99	13.20	1
0.98	77.98	3.99	73.99	60.68	13.31	1
0.97	78.81	4.02	74.79	61.36	13.43	1
0.96	79.64	4.06	75.58	62.05	13.54	1
0.95	80.47	4.09	76.38	62.73	13.65	1
0.94	81.30	4.13	77.17	63.41	13.76	1
0.93	82.13	4.16	77.97	64.09	13.87	1
0.92	82.95	4.20	78.76	64.78	13.98	1
0.91	83.78	4.23	79.55	65.46	14.09	1
0.89	84.61	4.27	80.34	66.14	14.20	1
0.88	85.43	4.30	81.13	66.81	14.31	1
0.87	86.25	4.34	81.92	67.49	14.42	1
0.86	87.08	4.37	82.70	68.17	14.54	1

0.85	87.90	4.41	83.49	68.84	14.65	1
0.84	88.72	4.44	84.28	69.52	14.75	1
0.83	89.54	4.48	85.06	70.19	14.86	1
0.82	90.36	4.52	85.84	70.87	14.97	1
0.82	90.36	4.52	85.84	70.87	14.97	1
0.80	91.83	4.58	87.25	72.08	15.17	1
0.78	93.30	4.65	88.65	73.29	15.37	1
0.76	94.77	4.72	90.05	74.49	15.56	1
0.74	96.24	4.79	91.45	75.70	15.76	1
0.72	97.70	4.86	92.84	76.90	15.95	1
0.70	99.16	4.93	94.23	78.09	16.14	1
0.68	100.62	5.00	95.62	79.29	16.33	1
0.66	102.07	5.15	96.92	80.48	16.44	1
0.65	103.52	5.31	98.21	81.67	16.55	1
0.63	104.97	5.47	99.50	82.85	16.65	1
0.61	106.41	5.62	100.79	84.04	16.76	1
0.59	107.86	5.78	102.08	85.22	16.86	1
0.57	109.30	5.94	103.36	86.39	16.97	1
0.55	110.73	6.09	104.64	87.57	17.07	1
0.53	112.17	6.25	105.92	88.74	17.18	1
0.51	113.60	6.41	107.19	89.91	17.28	1
0.49	115.03	6.56	108.46	91.07	17.39	1
0.48	116.45	6.72	109.73	92.23	17.49	1
0.46	117.87	6.88	111.00	93.39	17.60	1
0.44	119.29	7.04	112.26	94.55	17.71	1
0.42	120.71	7.19	113.52	95.71	17.81	1
0.40	122.12	7.35	114.77	96.86	17.92	1
0.38	123.54	7.51	116.03	98.01	18.02	1
0.37	124.94	7.67	117.28	99.15	18.12	1
0.35	126.35	7.82	118.52	100.30	18.23	1
0.33	127.75	7.98	119.77	101.44	18.33	1
0.31	129.15	8.14	121.01	102.57	18.44	1
0.29	130.55	8.30	122.25	103.71	18.54	1
0.27	131.94	8.46	123.48	104.84	18.64	1
0.26	133.33	8.62	124.71	105.97	18.75	1
0.24	134.72	8.78	125.94	107.09	18.85	1
0.22	136.11	8.94	127.16	108.21	18.95	1
0.20	137.49	9.10	128.39	109.33	19.05	1
0.18	138.87	9.26	129.61	110.45	19.16	1
0.17	140.24	9.42	130.82	111.56	19.26	1
0.15	141.62	9.58	132.04	112.68	19.36	1
0.13	142.99	9.74	133.25	113.78	19.47	1
0.11	144.35	9.89	134.46	114.89	19.57	1
0.10	145.72	10.10	135.62	115.99	19.63	1
0.08	147.08	10.41	136.67	117.09	19.58	1
0.08	147.08	10.41	136.67	117.09	19.58	1
0.06	148.29	10.69	137.60	118.07	19.54	1
0.05	149.50	10.97	138.53	119.04	19.49	1
0.03	150.70	11.24	139.46	120.01	19.45	1
0.02	151.90	11.52	140.38	120.98	19.40	1
0.00	153.10	11.80	141.30	121.94	19.36	1

Time = 145. Degree of Consolidation = 43.0%

Total Settlement = 0.490

Settlement at End of Primary Consolidation = 0.685

Settlement caused by Primary Consolidation at time 145. = 0.294

Settlement caused by Secondary Compression at time 145. = 0.000

Settlement Due to Desiccation = 0.196

Surface Elevation = 1.08

*****Current Conditions in Dredged Fill*****

***** Coordinates *****

***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
2.50	1.83	0.28	7.97	2.26	2.26	1
2.49	1.82	0.28	7.97	2.26	2.26	1
2.48	1.82	0.28	7.97	2.26	2.26	1
2.46	1.81	0.27	7.97	2.26	2.26	1
2.45	1.81	0.27	7.97	2.26	2.26	1
2.44	1.80	0.27	7.97	2.26	2.26	1
2.43	1.80	0.27	7.97	2.26	2.26	1
2.41	1.79	0.27	7.97	2.26	2.26	1
2.40	1.79	0.27	7.97	2.26	2.26	1
2.39	1.79	0.27	7.97	2.26	2.26	1
2.38	1.78	0.26	7.97	2.26	2.26	1
2.36	1.78	0.26	7.97	2.26	2.26	1
2.35	1.77	0.26	7.97	2.26	2.26	1
2.34	1.77	0.26	7.97	2.26	2.26	1
2.33	1.76	0.26	7.97	2.26	2.26	1
2.31	1.76	0.26	7.97	2.26	2.26	1
2.30	1.75	0.26	7.97	2.26	2.26	1
2.29	1.75	0.26	7.97	2.26	2.26	1
2.27	1.74	0.25	7.97	2.26	2.26	1
2.26	1.74	0.25	7.97	2.26	2.26	1
2.25	1.74	0.25	7.97	2.26	2.26	1
2.24	1.73	0.25	7.97	2.26	2.26	1
2.22	1.73	0.25	7.97	2.26	2.26	1
2.21	1.72	0.25	7.97	2.26	2.26	1
2.20	1.72	0.25	7.97	2.26	2.26	1
2.19	1.71	0.24	7.97	2.26	2.26	1
2.17	1.71	0.24	7.97	2.26	2.26	1
2.16	1.70	0.24	7.97	2.26	2.26	1
2.15	1.70	0.24	7.97	2.26	2.26	1
2.14	1.69	0.24	7.97	2.26	2.26	1
2.12	1.69	0.24	7.97	2.26	2.26	1
2.11	1.69	0.24	7.97	2.26	2.26	1

2.10	1.68	0.23	7.97	2.26	2.26	1
2.09	1.68	0.23	7.97	2.26	2.26	1
2.07	1.67	0.23	7.97	2.26	2.26	1
2.06	1.67	0.23	7.97	2.26	2.26	1
2.05	1.66	0.23	7.97	2.26	2.26	1
2.04	1.66	0.23	7.97	2.26	2.26	1
2.02	1.65	0.23	7.97	2.26	2.26	1
2.01	1.65	0.22	7.97	2.26	2.26	1
2.00	1.64	0.22	7.97	2.41	5.92	1
2.00	1.64	0.22	7.97	5.14	5.92	1
1.99	1.64	0.22	7.97	5.14	5.91	1
1.97	1.63	0.22	7.97	6.04	5.90	1
1.96	1.62	0.22	7.97	6.07	5.89	1
1.95	1.61	0.22	7.97	6.10	5.88	1
1.94	1.60	0.22	7.97	6.13	5.88	1
1.92	1.59	0.21	7.97	6.16	5.87	1
1.91	1.58	0.21	7.97	6.18	5.86	1
1.90	1.57	0.21	7.97	6.21	5.85	1
1.89	1.56	0.21	7.97	6.24	5.84	1
1.87	1.55	0.21	7.97	6.26	5.83	1
1.86	1.54	0.21	7.97	6.29	5.82	1
1.85	1.53	0.21	7.97	6.32	5.82	1
1.84	1.52	0.20	7.97	6.34	5.81	1
1.82	1.51	0.20	7.97	6.36	5.80	1
1.81	1.50	0.20	7.97	6.39	5.79	1
1.80	1.49	0.20	7.97	6.41	5.78	1
1.79	1.48	0.20	7.97	6.43	5.77	1
1.77	1.46	0.20	7.97	6.46	5.77	1
1.76	1.45	0.20	7.97	6.48	5.76	1
1.75	1.44	0.20	7.97	6.50	5.75	1
1.74	1.43	0.19	7.97	6.52	5.74	1
1.72	1.42	0.19	7.97	6.53	5.73	1
1.71	1.41	0.19	7.97	6.55	5.72	1
1.70	1.40	0.19	7.97	6.57	5.71	1
1.69	1.39	0.19	7.97	6.58	5.71	1
1.67	1.38	0.19	7.97	6.60	5.70	1
1.66	1.37	0.19	7.97	6.61	5.69	1
1.65	1.36	0.18	7.97	6.63	5.68	1
1.64	1.35	0.18	7.97	6.64	5.67	1
1.62	1.34	0.18	7.97	6.65	5.66	1
1.61	1.33	0.18	7.97	6.66	5.66	1
1.60	1.32	0.18	7.97	6.67	5.65	1
1.59	1.31	0.18	7.97	6.68	5.64	1
1.57	1.30	0.18	7.97	6.69	5.63	1
1.56	1.28	0.17	7.97	6.69	5.62	1
1.55	1.27	0.17	7.97	6.70	5.61	1
1.54	1.26	0.17	7.97	6.70	5.60	1
1.52	1.25	0.17	7.97	6.71	5.60	1
1.51	1.24	0.17	7.97	6.71	5.59	1
1.50	1.23	0.17	7.97	6.72	5.58	1
1.50	1.23	0.17	7.97	6.72	5.58	1
1.49	1.22	0.17	7.97	6.72	5.57	1
1.47	1.21	0.16	7.97	6.72	5.56	1
1.46	1.20	0.16	7.97	6.72	5.55	1

1.45	1.19	0.16	7.97	6.73	5.55	1
1.44	1.18	0.16	7.97	6.73	5.54	1
1.42	1.17	0.16	7.97	6.73	5.53	1
1.41	1.16	0.16	7.97	6.73	5.52	1
1.40	1.15	0.16	7.97	6.73	5.51	1
1.39	1.13	0.15	7.97	6.72	5.50	1
1.37	1.12	0.15	7.97	6.72	5.49	1
1.36	1.11	0.15	7.97	6.72	5.49	1
1.35	1.10	0.15	7.97	6.72	5.48	1
1.34	1.09	0.15	7.97	6.72	5.47	1
1.32	1.08	0.15	7.97	6.71	5.46	1
1.31	1.07	0.15	7.97	6.71	5.46	1
1.30	1.06	0.14	7.97	6.71	5.45	1
1.29	1.05	0.14	7.97	6.70	5.45	1
1.27	1.04	0.14	7.97	6.70	5.44	1
1.26	1.03	0.14	7.97	6.69	5.44	1
1.25	1.02	0.14	7.97	6.69	5.43	1
1.24	1.01	0.14	7.97	6.68	5.43	1
1.22	0.99	0.14	7.97	6.68	5.42	1
1.21	0.98	0.14	7.97	6.67	5.42	1
1.20	0.97	0.13	7.97	6.67	5.41	1
1.19	0.96	0.13	7.97	6.66	5.41	1
1.17	0.95	0.13	7.97	6.66	5.40	1
1.16	0.94	0.13	7.97	6.65	5.40	1
1.15	0.93	0.13	7.97	6.64	5.39	1
1.14	0.92	0.13	7.97	6.64	5.39	1
1.12	0.91	0.13	7.97	6.63	5.38	1
1.11	0.90	0.12	7.97	6.62	5.38	1
1.10	0.89	0.12	7.97	6.61	5.37	1
1.09	0.88	0.12	7.97	6.61	5.37	1
1.07	0.87	0.12	7.97	6.60	5.36	1
1.06	0.86	0.12	7.97	6.59	5.36	1
1.05	0.85	0.12	7.97	6.58	5.35	1
1.04	0.84	0.12	7.97	6.58	5.35	1
1.02	0.82	0.11	7.97	6.57	5.35	1
1.01	0.81	0.11	7.97	6.56	5.34	1
1.00	0.80	0.11	7.97	6.55	5.34	1
1.00	0.80	0.11	7.97	6.55	5.34	1
0.98	0.78	0.11	7.97	6.54	5.33	1
0.95	0.77	0.11	7.97	6.52	5.32	1
0.93	0.75	0.10	7.97	6.51	5.31	1
0.91	0.73	0.10	7.97	6.49	5.30	1
0.89	0.71	0.10	7.97	6.48	5.29	1
0.86	0.69	0.10	7.97	6.46	5.28	1
0.84	0.67	0.09	7.97	6.45	5.27	1
0.82	0.65	0.09	7.97	6.43	5.27	1
0.80	0.63	0.09	7.97	6.42	5.26	1
0.77	0.62	0.09	7.97	6.40	5.25	1
0.75	0.60	0.08	7.97	6.39	5.24	1
0.73	0.58	0.08	7.97	6.37	5.23	1
0.71	0.56	0.08	7.97	6.35	5.22	1
0.68	0.54	0.08	7.97	6.34	5.21	1
0.66	0.52	0.07	7.97	6.32	5.21	1
0.64	0.51	0.07	7.97	6.31	5.20	1

0.62	0.49	0.07	7.97	6.29	5.19	1
0.59	0.47	0.07	7.97	6.28	5.18	1
0.57	0.45	0.06	7.97	6.26	5.17	1
0.55	0.43	0.06	7.97	6.25	5.16	1
0.53	0.41	0.06	7.97	6.23	5.15	1
0.51	0.40	0.06	7.97	6.21	5.14	1
0.48	0.38	0.05	7.97	6.20	5.14	1
0.46	0.36	0.05	7.97	6.18	5.13	1
0.44	0.34	0.05	7.97	6.17	5.12	1
0.42	0.32	0.05	7.97	6.15	5.12	1
0.39	0.31	0.04	7.97	6.14	5.11	1
0.37	0.29	0.04	7.97	6.12	5.10	1
0.35	0.27	0.04	7.97	6.10	5.10	1
0.33	0.25	0.04	7.97	6.09	5.09	1
0.30	0.23	0.03	7.97	6.07	5.08	1
0.28	0.22	0.03	7.97	6.06	5.08	1
0.26	0.20	0.03	7.97	6.04	5.07	1
0.23	0.18	0.03	7.97	6.02	5.06	1
0.21	0.16	0.02	7.97	6.01	5.06	1
0.19	0.15	0.02	7.97	5.99	5.05	1
0.17	0.13	0.02	7.97	5.98	5.04	1
0.14	0.11	0.02	7.97	5.96	5.04	1
0.12	0.09	0.01	7.97	5.94	5.03	1
0.10	0.08	0.01	7.97	5.93	5.02	1
0.10	0.08	0.01	7.97	5.93	5.02	1
0.08	0.06	0.01	7.97	5.91	5.02	1
0.06	0.05	0.01	7.97	5.90	5.01	1
0.04	0.03	0.00	7.97	5.88	5.01	1
0.02	0.02	0.00	7.97	5.87	5.00	1
0.00	0.00	0.00	7.97	5.86	4.99	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
1.83	0.00	0.00	0.00	0.00	0.00	1
1.82	0.30	0.30	0.00	0.00	0.00	1
1.82	0.61	0.61	0.00	0.00	0.00	1
1.81	0.91	0.91	0.00	0.00	0.00	1
1.81	1.21	1.21	0.00	0.00	0.00	1
1.80	1.51	1.51	0.00	0.00	0.00	1
1.80	1.82	1.82	0.00	0.00	0.00	1
1.79	2.12	2.12	0.00	0.00	0.00	1
1.79	2.42	2.42	0.00	0.00	0.00	1
1.79	2.72	2.72	0.00	0.00	0.00	1
1.78	3.03	3.03	0.00	0.00	0.00	1
1.78	3.33	3.33	0.00	0.00	0.00	1
1.77	3.63	3.63	0.00	0.00	0.00	1
1.77	3.93	3.93	0.00	0.00	0.00	1
1.76	4.24	4.24	0.00	0.00	0.00	1
1.76	4.54	4.54	0.00	0.00	0.00	1
1.75	4.84	4.84	0.00	0.00	0.00	1
1.75	5.14	5.14	0.00	0.00	0.00	1
1.74	5.45	5.45	0.00	0.00	0.00	1

1.74	5.75	5.75	0.00	0.00	0.00	1
1.74	6.05	6.05	0.00	0.00	0.00	1
1.73	6.35	6.35	0.00	0.00	0.00	1
1.73	6.66	6.66	0.00	0.00	0.00	1
1.72	6.96	6.96	0.00	0.00	0.00	1
1.72	7.26	7.26	0.00	0.00	0.00	1
1.71	7.56	7.56	0.00	0.00	0.00	1
1.71	7.87	7.87	0.00	0.00	0.00	1
1.70	8.17	8.17	0.00	0.00	0.00	1
1.70	8.47	8.47	0.00	0.00	0.00	1
1.69	8.77	8.77	0.00	0.00	0.00	1
1.69	9.08	9.08	0.00	0.00	0.00	1
1.69	9.38	9.38	0.00	0.00	0.00	1
1.68	9.68	9.68	0.00	0.00	0.00	1
1.68	9.98	9.98	0.00	0.00	0.00	1
1.67	10.29	10.29	0.00	0.00	0.00	1
1.67	10.59	10.59	0.00	0.00	0.00	1
1.66	10.89	10.89	0.00	0.00	0.00	1
1.66	11.19	11.19	0.00	0.00	0.00	1
1.65	11.50	11.50	0.00	0.00	0.00	1
1.65	11.80	11.80	0.00	0.00	0.00	1
1.64	12.11	12.11	0.00	0.00	0.00	1
1.64	12.11	12.11	0.00	0.00	0.00	1
1.64	12.77	12.25	0.51	0.51	0.00	1
1.63	13.49	9.98	3.52	1.09	2.42	1
1.62	14.25	9.73	4.52	1.71	2.81	1
1.61	15.02	9.49	5.53	2.32	3.20	1
1.60	15.78	9.25	6.53	2.94	3.59	1
1.59	16.55	9.01	7.54	3.56	3.98	1
1.58	17.32	8.77	8.55	4.19	4.36	1
1.57	18.09	8.53	9.55	4.81	4.74	1
1.56	18.86	8.30	10.56	5.44	5.12	1
1.55	19.64	8.07	11.56	6.07	5.49	1
1.54	20.42	7.85	12.57	6.70	5.86	1
1.53	21.20	7.63	13.57	7.34	6.23	1
1.52	21.98	7.41	14.57	7.98	6.59	1
1.51	22.76	7.20	15.56	8.62	6.95	1
1.50	23.55	7.00	16.55	9.26	7.30	1
1.49	24.34	6.80	17.54	9.90	7.64	1
1.48	25.13	6.60	18.53	10.55	7.98	1
1.46	25.93	6.42	19.51	11.19	8.31	1
1.45	26.72	6.24	20.48	11.84	8.64	1
1.44	27.52	6.06	21.45	12.49	8.96	1
1.43	28.32	5.90	22.42	13.15	9.27	1
1.42	29.12	5.74	23.38	13.80	9.58	1
1.41	29.92	5.59	24.33	14.46	9.88	1
1.40	30.72	5.44	25.28	15.11	10.17	1
1.39	31.53	5.30	26.22	15.77	10.45	1
1.38	32.33	5.18	27.16	16.43	10.72	1
1.37	33.14	5.05	28.08	17.09	10.99	1
1.36	33.95	4.97	28.97	17.76	11.22	1
1.35	34.76	4.93	29.83	18.42	11.41	1
1.34	35.57	4.88	30.69	19.09	11.60	1
1.33	36.38	4.84	31.54	19.75	11.79	1

1.32	37.19	4.81	32.39	20.42	11.97	1
1.31	38.01	4.77	33.23	21.09	12.15	1
1.30	38.82	4.74	34.07	21.75	12.32	1
1.28	39.63	4.72	34.92	22.42	12.49	1
1.27	40.45	4.69	35.75	23.09	12.66	1
1.26	41.26	4.67	36.59	23.76	12.83	1
1.25	42.08	4.66	37.42	24.43	12.99	1
1.24	42.90	4.64	38.26	25.10	13.15	1
1.23	43.71	4.63	39.09	25.77	13.31	1
1.23	43.71	4.63	39.09	25.77	13.31	1
1.22	44.53	4.61	39.92	26.44	13.47	1
1.21	45.35	4.60	40.74	27.11	13.63	1
1.20	46.16	4.60	41.57	27.79	13.78	1
1.19	46.98	4.59	42.39	28.46	13.93	1
1.18	47.80	4.59	43.21	29.13	14.08	1
1.17	48.62	4.59	44.03	29.80	14.23	1
1.16	49.43	4.59	44.85	30.47	14.38	1
1.15	50.25	4.59	45.67	31.15	14.52	1
1.13	51.07	4.59	46.48	31.82	14.66	1
1.12	51.89	4.60	47.29	32.49	14.80	1
1.11	52.70	4.60	48.10	33.16	14.94	1
1.10	53.52	4.61	48.91	33.83	15.08	1
1.09	54.34	4.62	49.72	34.50	15.21	1
1.08	55.16	4.63	50.52	35.17	15.35	1
1.07	55.97	4.65	51.33	35.84	15.48	1
1.06	56.79	4.66	52.13	36.51	15.61	1
1.05	57.60	4.68	52.93	37.18	15.74	1
1.04	58.42	4.69	53.73	37.85	15.87	1
1.03	59.23	4.71	54.53	38.52	16.00	1
1.02	60.05	4.73	55.32	39.19	16.13	1
1.01	60.86	4.75	56.12	39.86	16.26	1
0.99	61.68	4.77	56.91	40.53	16.38	1
0.98	62.49	4.79	57.70	41.20	16.51	1
0.97	63.30	4.81	58.49	41.86	16.63	1
0.96	64.12	4.84	59.28	42.53	16.75	1
0.95	64.93	4.86	60.07	43.20	16.87	1
0.94	65.74	4.88	60.86	43.86	16.99	1
0.93	66.55	4.91	61.64	44.53	17.11	1
0.92	67.36	4.94	62.42	45.19	17.23	1
0.91	68.17	4.96	63.21	45.85	17.35	1
0.90	68.98	4.99	63.99	46.52	17.47	1
0.89	69.79	5.04	64.74	47.18	17.56	1
0.88	70.59	5.11	65.49	47.84	17.64	1
0.87	71.40	5.17	66.23	48.50	17.73	1
0.86	72.21	5.24	66.97	49.16	17.81	1
0.85	73.01	5.31	67.71	49.82	17.89	1
0.84	73.82	5.37	68.45	50.48	17.96	1
0.82	74.62	5.44	69.18	51.14	18.04	1
0.81	75.43	5.51	69.92	51.80	18.12	1
0.80	76.23	5.58	70.65	52.46	18.19	1
0.80	76.23	5.58	70.65	52.46	18.19	1
0.78	77.67	5.70	71.97	53.64	18.33	1
0.77	79.11	5.83	73.28	54.82	18.47	1
0.75	80.55	5.96	74.59	55.99	18.60	1

0.73	81.99	6.09	75.90	57.17	18.73	1
0.71	83.42	6.22	77.20	58.34	18.87	1
0.69	84.86	6.35	78.50	59.51	19.00	1
0.67	86.29	6.48	79.80	60.67	19.13	1
0.65	87.71	6.62	81.10	61.84	19.26	1
0.63	89.14	6.75	82.39	63.00	19.39	1
0.62	90.56	6.88	83.68	64.16	19.52	1
0.60	91.98	7.02	84.96	65.32	19.64	1
0.58	93.40	7.15	86.25	66.47	19.77	1
0.56	94.81	7.29	87.53	67.63	19.90	1
0.54	96.22	7.42	88.80	68.78	20.03	1
0.52	97.63	7.55	90.08	69.92	20.16	1
0.51	99.04	7.69	91.35	71.07	20.28	1
0.49	100.45	7.82	92.62	72.21	20.41	1
0.47	101.85	7.96	93.89	73.35	20.54	1
0.45	103.25	8.10	95.15	74.49	20.67	1
0.43	104.65	8.23	96.42	75.62	20.79	1
0.41	106.04	8.37	97.68	76.76	20.92	1
0.40	107.44	8.50	98.93	77.89	21.05	1
0.38	108.83	8.64	100.19	79.02	21.17	1
0.36	110.21	8.77	101.44	80.14	21.30	1
0.34	111.60	8.91	102.69	81.26	21.43	1
0.32	112.98	9.04	103.94	82.38	21.55	1
0.31	114.36	9.18	105.18	83.50	21.68	1
0.29	115.74	9.32	106.43	84.62	21.81	1
0.27	117.12	9.45	107.67	85.73	21.93	1
0.25	118.49	9.59	108.90	86.84	22.06	1
0.23	119.86	9.72	110.14	87.95	22.19	1
0.22	121.23	9.86	111.37	89.06	22.31	1
0.20	122.59	9.99	112.60	90.16	22.44	1
0.18	123.96	10.26	113.70	91.26	22.44	1
0.16	125.32	10.53	114.78	92.36	22.43	1
0.15	126.68	10.81	115.87	93.45	22.41	1
0.13	128.03	11.09	116.94	94.55	22.40	1
0.11	129.39	11.37	118.02	95.64	22.38	1
0.09	130.74	11.65	119.09	96.73	22.36	1
0.08	132.08	11.93	120.16	97.81	22.35	1
0.08	132.08	11.93	120.16	97.81	22.35	1
0.06	133.28	12.18	121.10	98.77	22.33	1
0.05	134.47	12.43	122.05	99.74	22.31	1
0.03	135.67	12.68	122.99	100.69	22.29	1
0.02	136.86	12.93	123.92	101.65	22.27	1
0.00	138.05	13.19	124.86	102.61	22.25	1

Time = 175. Degree of Consolidation = 40.0%

Total Settlement = 0.674

Settlement at End of Primary Consolidation = 0.895

Settlement caused by Primary Consolidation at time 175. = 0.362

Settlement caused by Secondary Compression at time 175. = 0.000

Settlement Due to Desiccation = 0.311

Surface Elevation = 0.90

*****Current Conditions in Dredged Fill*****

***** Coordinates *****

***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
2.50	1.61	0.28	7.97	2.26	2.26	1
2.49	1.61	0.28	7.97	2.26	2.26	1
2.48	1.60	0.28	7.97	2.26	2.26	1
2.46	1.60	0.27	7.97	2.26	2.26	1
2.45	1.60	0.27	7.97	2.26	2.26	1
2.44	1.59	0.27	7.97	2.26	2.26	1
2.43	1.59	0.27	7.97	2.26	2.26	1
2.41	1.58	0.27	7.97	2.26	2.26	1
2.40	1.58	0.27	7.97	2.26	2.26	1
2.39	1.57	0.27	7.97	2.26	2.26	1
2.38	1.57	0.26	7.97	2.26	2.26	1
2.36	1.56	0.26	7.97	2.26	2.26	1
2.35	1.56	0.26	7.97	2.26	2.26	1
2.34	1.55	0.26	7.97	2.26	2.26	1
2.33	1.55	0.26	7.97	2.26	2.26	1
2.31	1.55	0.26	7.97	2.26	2.26	1
2.30	1.54	0.26	7.97	2.26	2.26	1
2.29	1.54	0.26	7.97	2.26	2.26	1
2.27	1.53	0.25	7.97	2.26	2.26	1
2.26	1.53	0.25	7.97	2.26	2.26	1
2.25	1.52	0.25	7.97	2.26	2.26	1
2.24	1.52	0.25	7.97	2.26	2.26	1
2.22	1.51	0.25	7.97	2.26	2.26	1
2.21	1.51	0.25	7.97	2.26	2.26	1
2.20	1.50	0.25	7.97	2.26	2.26	1
2.19	1.50	0.24	7.97	2.26	2.26	1
2.17	1.50	0.24	7.97	2.26	2.26	1
2.16	1.49	0.24	7.97	2.26	2.26	1
2.15	1.49	0.24	7.97	2.26	2.26	1
2.14	1.48	0.24	7.97	2.26	2.26	1
2.12	1.48	0.24	7.97	2.26	2.26	1
2.11	1.47	0.24	7.97	2.26	2.26	1
2.10	1.47	0.23	7.97	2.26	2.26	1
2.09	1.46	0.23	7.97	2.26	2.26	1
2.07	1.46	0.23	7.97	2.26	2.26	1
2.06	1.45	0.23	7.97	2.26	2.26	1
2.05	1.45	0.23	7.97	2.26	2.26	1
2.04	1.45	0.23	7.97	2.26	2.26	1
2.02	1.44	0.23	7.97	2.26	2.26	1
2.01	1.44	0.22	7.97	2.26	2.26	1

2.00	1.43	0.22	7.97	2.26	2.26	1
2.00	1.43	0.22	7.97	2.26	2.26	1
1.99	1.43	0.22	7.97	2.26	2.26	1
1.97	1.42	0.22	7.97	2.26	2.26	1
1.96	1.42	0.22	7.97	2.26	2.26	1
1.95	1.41	0.22	7.97	2.26	2.26	1
1.94	1.41	0.22	7.97	2.26	2.26	1
1.92	1.40	0.21	7.97	2.26	2.26	1
1.91	1.40	0.21	7.97	2.26	2.26	1
1.90	1.40	0.21	7.97	2.26	2.26	1
1.89	1.39	0.21	7.97	2.26	2.26	1
1.87	1.39	0.21	7.97	2.26	2.26	1
1.86	1.38	0.21	7.97	2.26	2.26	1
1.85	1.38	0.21	7.97	2.26	2.26	1
1.84	1.37	0.20	7.97	2.26	2.26	1
1.82	1.37	0.20	7.97	2.26	2.26	1
1.81	1.36	0.20	7.97	2.26	2.26	1
1.80	1.36	0.20	7.97	2.26	2.26	1
1.79	1.35	0.20	7.97	2.26	2.26	1
1.77	1.35	0.20	7.97	2.26	2.26	1
1.76	1.35	0.20	7.97	2.26	2.26	1
1.75	1.34	0.20	7.97	2.26	2.26	1
1.74	1.34	0.19	7.97	2.26	2.26	1
1.72	1.33	0.19	7.97	2.26	2.26	1
1.71	1.33	0.19	7.97	2.26	2.26	1
1.70	1.32	0.19	7.97	2.26	2.26	1
1.69	1.32	0.19	7.97	2.26	2.26	1
1.67	1.31	0.19	7.97	2.26	2.26	1
1.66	1.31	0.19	7.97	2.26	2.26	1
1.65	1.30	0.18	7.97	2.26	2.26	1
1.64	1.30	0.18	7.97	2.26	2.26	1
1.62	1.29	0.18	7.97	5.62	5.62	1
1.61	1.28	0.18	7.97	5.93	5.61	1
1.60	1.27	0.18	7.97	5.95	5.60	1
1.59	1.27	0.18	7.97	5.97	5.59	1
1.57	1.26	0.18	7.97	5.99	5.59	1
1.56	1.25	0.17	7.97	6.01	5.58	1
1.55	1.24	0.17	7.97	6.02	5.57	1
1.54	1.23	0.17	7.97	6.04	5.56	1
1.52	1.22	0.17	7.97	6.06	5.55	1
1.51	1.21	0.17	7.97	6.08	5.54	1
1.50	1.20	0.17	7.97	6.09	5.53	1
1.50	1.20	0.17	7.97	6.09	5.53	1
1.49	1.19	0.17	7.97	6.11	5.52	1
1.47	1.18	0.16	7.97	6.13	5.51	1
1.46	1.17	0.16	7.97	6.14	5.50	1
1.45	1.16	0.16	7.97	6.16	5.49	1
1.44	1.15	0.16	7.97	6.17	5.48	1
1.42	1.14	0.16	7.97	6.18	5.48	1
1.41	1.13	0.16	7.97	6.20	5.47	1
1.40	1.12	0.16	7.97	6.21	5.46	1
1.39	1.11	0.15	7.97	6.22	5.45	1
1.37	1.10	0.15	7.97	6.23	5.45	1
1.36	1.09	0.15	7.97	6.25	5.44	1

1.35	1.08	0.15	7.97	6.26	5.44	1
1.34	1.07	0.15	7.97	6.27	5.44	1
1.32	1.06	0.15	7.97	6.28	5.43	1
1.31	1.05	0.15	7.97	6.28	5.43	1
1.30	1.04	0.14	7.97	6.29	5.42	1
1.29	1.03	0.14	7.97	6.30	5.42	1
1.27	1.02	0.14	7.97	6.31	5.41	1
1.26	1.01	0.14	7.97	6.31	5.41	1
1.25	1.00	0.14	7.97	6.32	5.40	1
1.24	0.98	0.14	7.97	6.33	5.40	1
1.22	0.97	0.14	7.97	6.33	5.39	1
1.21	0.96	0.14	7.97	6.34	5.39	1
1.20	0.95	0.13	7.97	6.34	5.38	1
1.19	0.94	0.13	7.97	6.34	5.38	1
1.17	0.93	0.13	7.97	6.35	5.37	1
1.16	0.92	0.13	7.97	6.35	5.37	1
1.15	0.91	0.13	7.97	6.35	5.36	1
1.14	0.90	0.13	7.97	6.35	5.36	1
1.12	0.89	0.13	7.97	6.35	5.36	1
1.11	0.88	0.12	7.97	6.35	5.35	1
1.10	0.87	0.12	7.97	6.35	5.35	1
1.09	0.86	0.12	7.97	6.35	5.34	1
1.07	0.85	0.12	7.97	6.35	5.34	1
1.06	0.84	0.12	7.97	6.35	5.33	1
1.05	0.83	0.12	7.97	6.35	5.33	1
1.04	0.82	0.12	7.97	6.35	5.32	1
1.02	0.81	0.11	7.97	6.34	5.32	1
1.01	0.80	0.11	7.97	6.34	5.31	1
1.00	0.79	0.11	7.97	6.34	5.31	1
1.00	0.79	0.11	7.97	6.34	5.31	1
0.98	0.77	0.11	7.97	6.33	5.30	1
0.95	0.75	0.11	7.97	6.33	5.30	1
0.93	0.74	0.10	7.97	6.32	5.29	1
0.91	0.72	0.10	7.97	6.31	5.29	1
0.89	0.70	0.10	7.97	6.31	5.28	1
0.86	0.68	0.10	7.97	6.30	5.28	1
0.84	0.66	0.09	7.97	6.29	5.27	1
0.82	0.64	0.09	7.97	6.28	5.27	1
0.80	0.63	0.09	7.97	6.27	5.26	1
0.77	0.61	0.09	7.97	6.26	5.26	1
0.75	0.59	0.08	7.97	6.24	5.25	1
0.73	0.57	0.08	7.97	6.23	5.25	1
0.71	0.55	0.08	7.97	6.22	5.24	1
0.68	0.53	0.08	7.97	6.21	5.24	1
0.66	0.52	0.07	7.97	6.20	5.23	1
0.64	0.50	0.07	7.97	6.18	5.23	1
0.62	0.48	0.07	7.97	6.17	5.22	1
0.59	0.46	0.07	7.97	6.16	5.22	1
0.57	0.44	0.06	7.97	6.15	5.21	1
0.55	0.43	0.06	7.97	6.13	5.21	1
0.53	0.41	0.06	7.97	6.12	5.20	1
0.51	0.39	0.06	7.97	6.11	5.20	1
0.48	0.37	0.05	7.97	6.09	5.19	1
0.46	0.36	0.05	7.97	6.08	5.19	1

0.44	0.34	0.05	7.97	6.07	5.18	1
0.42	0.32	0.05	7.97	6.05	5.18	1
0.39	0.30	0.04	7.97	6.04	5.18	1
0.37	0.28	0.04	7.97	6.02	5.17	1
0.35	0.27	0.04	7.97	6.01	5.17	1
0.33	0.25	0.04	7.97	6.00	5.17	1
0.30	0.23	0.03	7.97	5.98	5.16	1
0.28	0.21	0.03	7.97	5.97	5.15	1
0.26	0.20	0.03	7.97	5.95	5.14	1
0.23	0.18	0.03	7.97	5.94	5.13	1
0.21	0.16	0.02	7.97	5.92	5.12	1
0.19	0.14	0.02	7.97	5.91	5.12	1
0.17	0.13	0.02	7.97	5.89	5.11	1
0.14	0.11	0.02	7.97	5.88	5.10	1
0.12	0.09	0.01	7.97	5.86	5.10	1
0.10	0.08	0.01	7.97	5.85	5.09	1
0.10	0.08	0.01	7.97	5.85	5.08	1
0.08	0.06	0.01	7.97	5.83	5.08	1
0.06	0.05	0.01	7.97	5.82	5.07	1
0.04	0.03	0.00	7.97	5.81	5.07	1
0.02	0.02	0.00	7.97	5.79	5.06	1
0.00	0.00	0.00	7.97	5.78	5.05	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
1.61	0.00	0.00	0.00	0.00	0.00	1
1.61	0.30	0.30	0.00	0.00	0.00	1
1.60	0.61	0.61	0.00	0.00	0.00	1
1.60	0.91	0.91	0.00	0.00	0.00	1
1.60	1.21	1.21	0.00	0.00	0.00	1
1.59	1.51	1.51	0.00	0.00	0.00	1
1.59	1.82	1.82	0.00	0.00	0.00	1
1.58	2.12	2.12	0.00	0.00	0.00	1
1.58	2.42	2.42	0.00	0.00	0.00	1
1.57	2.72	2.72	0.00	0.00	0.00	1
1.57	3.03	3.03	0.00	0.00	0.00	1
1.56	3.33	3.33	0.00	0.00	0.00	1
1.56	3.63	3.63	0.00	0.00	0.00	1
1.55	3.93	3.93	0.00	0.00	0.00	1
1.55	4.24	4.24	0.00	0.00	0.00	1
1.55	4.54	4.54	0.00	0.00	0.00	1
1.54	4.84	4.84	0.00	0.00	0.00	1
1.54	5.14	5.14	0.00	0.00	0.00	1
1.53	5.45	5.45	0.00	0.00	0.00	1
1.53	5.75	5.75	0.00	0.00	0.00	1
1.52	6.05	6.05	0.00	0.00	0.00	1
1.52	6.35	6.35	0.00	0.00	0.00	1
1.51	6.66	6.66	0.00	0.00	0.00	1
1.51	6.96	6.96	0.00	0.00	0.00	1
1.50	7.26	7.26	0.00	0.00	0.00	1
1.50	7.56	7.56	0.00	0.00	0.00	1
1.50	7.87	7.87	0.00	0.00	0.00	1

1.49	8.17	8.17	0.00	0.00	0.00	1
1.49	8.47	8.47	0.00	0.00	0.00	1
1.48	8.77	8.77	0.00	0.00	0.00	1
1.48	9.08	9.08	0.00	0.00	0.00	1
1.47	9.38	9.38	0.00	0.00	0.00	1
1.47	9.68	9.68	0.00	0.00	0.00	1
1.46	9.98	9.98	0.00	0.00	0.00	1
1.46	10.29	10.29	0.00	0.00	0.00	1
1.45	10.59	10.59	0.00	0.00	0.00	1
1.45	10.89	10.89	0.00	0.00	0.00	1
1.45	11.19	11.19	0.00	0.00	0.00	1
1.44	11.50	11.50	0.00	0.00	0.00	1
1.44	11.80	11.80	0.00	0.00	0.00	1
1.43	12.10	12.10	0.00	0.00	0.00	1
1.43	12.40	12.40	0.00	0.00	0.00	1
1.43	12.77	12.77	0.00	0.00	0.00	1
1.42	13.14	13.14	0.00	0.00	0.00	1
1.42	13.44	13.44	0.00	0.00	0.00	1
1.41	13.74	13.74	0.00	0.00	0.00	1
1.41	14.04	14.04	0.00	0.00	0.00	1
1.40	14.35	14.35	0.00	0.00	0.00	1
1.40	14.65	14.65	0.00	0.00	0.00	1
1.40	14.95	14.95	0.00	0.00	0.00	1
1.39	15.25	15.25	0.00	0.00	0.00	1
1.39	15.56	15.56	0.00	0.00	0.00	1
1.38	15.86	15.86	0.00	0.00	0.00	1
1.38	16.16	16.16	0.00	0.00	0.00	1
1.37	16.46	16.46	0.00	0.00	0.00	1
1.37	16.77	16.77	0.00	0.00	0.00	1
1.36	17.07	17.07	0.00	0.00	0.00	1
1.36	17.37	17.37	0.00	0.00	0.00	1
1.35	17.67	17.67	0.00	0.00	0.00	1
1.35	17.98	17.98	0.00	0.00	0.00	1
1.35	18.28	18.28	0.00	0.00	0.00	1
1.34	18.58	18.58	0.00	0.00	0.00	1
1.34	18.88	18.88	0.00	0.00	0.00	1
1.33	19.19	19.19	0.00	0.00	0.00	1
1.33	19.49	19.49	0.00	0.00	0.00	1
1.32	19.79	19.79	0.00	0.00	0.00	1
1.32	20.09	20.09	0.00	0.00	0.00	1
1.31	20.40	20.40	0.00	0.00	0.00	1
1.31	20.70	20.70	0.00	0.00	0.00	1
1.30	21.00	21.00	0.00	0.00	0.00	1
1.30	21.31	21.31	0.00	0.00	0.00	1
1.29	35.57	12.28	30.69	19.09	13.87	1
1.28	36.38	11.93	31.54	19.75	14.37	1
1.27	37.19	11.58	32.39	20.42	14.86	1
1.27	38.01	11.24	33.23	21.09	15.34	1
1.26	38.82	10.91	34.07	21.75	15.82	1
1.25	39.63	10.59	34.92	22.42	16.29	1
1.24	40.45	10.27	35.75	23.09	16.75	1
1.23	41.26	9.98	36.59	23.76	17.18	1
1.22	42.08	9.83	37.42	24.43	17.48	1
1.21	42.90	9.69	38.26	25.10	17.77	1

1.20	43.71	9.55	39.09	25.77	18.06	1
1.20	43.71	4.63	39.09	25.77	18.06	1
1.19	44.53	9.40	39.92	26.44	18.35	1
1.18	45.35	9.27	40.74	27.11	18.63	1
1.17	46.16	9.13	41.57	27.79	18.91	1
1.16	46.98	9.00	42.39	28.46	19.19	1
1.15	47.80	8.88	43.21	29.13	19.46	1
1.14	48.62	8.76	44.03	29.80	19.72	1
1.13	49.43	8.64	44.85	30.47	19.99	1
1.12	50.25	8.53	45.67	31.15	20.24	1
1.11	51.07	8.42	46.48	31.82	20.49	1
1.10	51.89	8.32	47.29	32.49	20.74	1
1.09	52.70	8.23	48.10	33.16	20.98	1
1.08	53.52	8.13	48.91	33.83	21.22	1
1.07	54.34	8.05	49.72	34.50	21.45	1
1.06	55.16	7.97	50.52	35.17	21.68	1
1.05	55.97	7.89	51.33	35.84	21.90	1
1.04	56.79	7.82	52.13	36.51	22.12	1
1.03	57.60	7.75	52.93	37.18	22.33	1
1.02	58.42	7.69	53.73	37.85	22.54	1
1.01	59.23	7.63	54.53	38.52	22.74	1
1.00	60.05	7.58	55.32	39.19	22.94	1
0.98	60.86	7.53	56.12	39.86	23.13	1
0.97	61.68	7.49	56.91	40.53	23.32	1
0.96	62.49	7.45	57.70	41.20	23.51	1
0.95	63.30	7.42	58.49	41.86	23.68	1
0.94	64.12	7.39	59.28	42.53	23.86	1
0.93	64.93	7.37	60.07	43.20	24.03	1
0.92	65.74	7.35	60.86	43.86	24.19	1
0.91	66.55	7.33	61.64	44.53	24.36	1
0.90	67.36	7.32	62.42	45.19	24.51	1
0.89	68.17	7.31	63.21	45.85	24.67	1
0.88	68.98	7.31	63.99	46.52	24.82	1
0.87	69.79	7.31	64.74	47.18	24.96	1
0.86	70.59	7.31	65.49	47.84	25.11	1
0.85	71.40	7.32	66.23	48.50	25.25	1
0.84	72.21	7.33	66.97	49.16	25.38	1
0.83	73.01	7.34	67.71	49.82	25.51	1
0.82	73.82	7.36	68.45	50.48	25.64	1
0.81	74.62	7.38	69.18	51.14	25.77	1
0.80	75.43	7.40	69.92	51.80	25.90	1
0.79	76.23	7.42	70.65	52.46	26.02	1
0.79	76.23	5.58	70.65	52.46	26.02	1
0.77	77.67	7.47	71.97	53.64	26.24	1
0.75	79.11	7.52	73.28	54.82	26.45	1
0.74	80.55	7.58	74.59	55.99	26.65	1
0.72	81.99	7.64	75.90	57.17	26.85	1
0.70	83.42	7.71	77.20	58.34	27.04	1
0.68	84.86	7.79	78.50	59.51	27.22	1
0.66	86.29	7.87	79.80	60.67	27.41	1
0.64	87.71	7.96	81.10	61.84	27.58	1
0.63	89.14	8.05	82.39	63.00	27.75	1
0.61	90.56	8.14	83.68	64.16	27.92	1
0.59	91.98	8.24	84.96	65.32	28.09	1

0.57	93.40	8.33	86.25	66.47	28.25	1
0.55	94.81	8.44	87.53	67.63	28.41	1
0.53	96.22	8.54	88.80	68.78	28.57	1
0.52	97.63	8.65	90.08	69.92	28.73	1
0.50	99.04	8.75	91.35	71.07	28.88	1
0.48	100.45	8.86	92.62	72.21	29.04	1
0.46	101.85	8.97	93.89	73.35	29.19	1
0.44	103.25	9.09	95.15	74.49	29.34	1
0.43	104.65	9.20	96.42	75.62	29.49	1
0.41	106.04	9.31	97.68	76.76	29.64	1
0.39	107.44	9.43	98.93	77.89	29.78	1
0.37	108.83	9.55	100.19	79.02	29.93	1
0.36	110.21	9.66	101.44	80.14	30.07	1
0.34	111.60	9.78	102.69	81.26	30.22	1
0.32	112.98	9.90	103.94	82.38	30.36	1
0.30	114.36	10.04	105.18	83.50	30.49	1
0.28	115.74	10.28	106.43	84.62	30.51	1
0.27	117.12	10.52	107.67	85.73	30.53	1
0.25	118.49	10.77	108.90	86.84	30.55	1
0.23	119.86	11.01	110.14	87.95	30.56	1
0.21	121.23	11.26	111.37	89.06	30.58	1
0.20	122.59	11.51	112.60	90.16	30.59	1
0.18	123.96	11.76	113.70	91.26	30.60	1
0.16	125.32	12.02	114.78	92.36	30.61	1
0.14	77.86	12.27	65.59	73.29	-7.70	1
0.13	79.02	12.53	66.49	74.37	-7.88	1
0.11	80.17	12.79	67.38	75.44	-8.06	1
0.09	81.32	13.05	68.27	76.52	-8.25	1
0.08	82.47	13.31	69.16	77.59	-8.43	1
0.08	82.70	13.31	69.39	77.59	-8.20	1
0.06	83.75	13.54	70.21	78.54	-8.34	1
0.05	84.79	13.78	71.02	79.49	-8.48	1
0.03	85.83	14.01	71.82	80.44	-8.62	1
0.02	86.87	14.25	72.63	81.39	-8.76	1
0.00	87.91	14.48	73.43	82.33	0.00	1

Time = 205. Degree of Consolidation = 38.0%

Total Settlement = 0.886

Settlement at End of Primary Consolidation = 1.041

Settlement caused by Primary Consolidation at time 205. = 0.394

Settlement caused by Secondary Compression at time 205. = 0.000

Settlement Due to Desiccation = 0.492

Surface Elevation = 0.68

*****Current Conditions in Dredged Fill*****

***** Coordinates *****

***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
2.50	1.56	0.28	7.97	2.26	2.26	1
2.49	1.56	0.28	7.97	2.26	2.26	1
2.48	1.55	0.28	7.97	2.26	2.26	1
2.46	1.55	0.27	7.97	2.26	2.26	1
2.45	1.54	0.27	7.97	2.26	2.26	1
2.44	1.54	0.27	7.97	2.26	2.26	1
2.43	1.53	0.27	7.97	2.26	2.26	1
2.41	1.53	0.27	7.97	2.26	2.26	1
2.40	1.52	0.27	7.97	2.26	2.26	1
2.39	1.52	0.27	7.97	2.26	2.26	1
2.38	1.52	0.26	7.97	2.26	2.26	1
2.36	1.51	0.26	7.97	2.26	2.26	1
2.35	1.51	0.26	7.97	2.26	2.26	1
2.34	1.50	0.26	7.97	2.26	2.26	1
2.33	1.50	0.26	7.97	2.26	2.26	1
2.31	1.49	0.26	7.97	2.26	2.26	1
2.30	1.49	0.26	7.97	2.26	2.26	1
2.29	1.48	0.26	7.97	2.26	2.26	1
2.27	1.48	0.25	7.97	2.26	2.26	1
2.26	1.47	0.25	7.97	2.26	2.26	1
2.25	1.47	0.25	7.97	2.26	2.26	1
2.24	1.47	0.25	7.97	2.26	2.26	1
2.22	1.46	0.25	7.97	2.26	2.26	1
2.21	1.46	0.25	7.97	2.26	2.26	1
2.20	1.45	0.25	7.97	2.26	2.26	1
2.19	1.45	0.24	7.97	2.26	2.26	1
2.17	1.44	0.24	7.97	2.26	2.26	1
2.16	1.44	0.24	7.97	2.26	2.26	1
2.15	1.43	0.24	7.97	2.26	2.26	1
2.14	1.43	0.24	7.97	2.26	2.26	1
2.12	1.42	0.24	7.97	2.26	2.26	1
2.11	1.42	0.24	7.97	2.26	2.26	1
2.10	1.42	0.23	7.97	2.26	2.26	1
2.09	1.41	0.23	7.97	2.26	2.26	1
2.07	1.41	0.23	7.97	2.26	2.26	1
2.06	1.40	0.23	7.97	2.26	2.26	1
2.05	1.40	0.23	7.97	2.26	2.26	1
2.04	1.39	0.23	7.97	2.26	2.26	1
2.02	1.39	0.23	7.97	2.26	2.26	1
2.01	1.38	0.22	7.97	2.26	2.26	1
2.00	1.38	0.22	7.97	5.92	2.26	1
2.00	1.38	0.22	7.97	5.92	2.26	1
1.99	1.37	0.22	7.97	2.26	2.26	1
1.97	1.37	0.22	7.97	2.26	2.26	1
1.96	1.36	0.22	7.97	2.26	2.26	1
1.95	1.36	0.22	7.97	2.26	2.26	1
1.94	1.35	0.22	7.97	2.26	2.26	1
1.92	1.35	0.21	7.97	2.26	2.26	1

1.91	1.34	0.21	7.97	2.26	2.26	1
1.90	1.34	0.21	7.97	2.26	2.26	1
1.89	1.34	0.21	7.97	2.26	2.26	1
1.87	1.33	0.21	7.97	2.26	2.26	1
1.86	1.33	0.21	7.97	2.26	2.26	1
1.85	1.32	0.21	7.97	2.26	2.26	1
1.84	1.32	0.20	7.97	2.26	2.26	1
1.82	1.31	0.20	7.97	2.26	2.26	1
1.81	1.31	0.20	7.97	2.26	2.26	1
1.80	1.30	0.20	7.97	2.26	2.26	1
1.79	1.30	0.20	7.97	2.26	2.26	1
1.77	1.29	0.20	7.97	2.26	2.26	1
1.76	1.29	0.20	7.97	2.26	2.26	1
1.75	1.29	0.20	7.97	2.26	2.26	1
1.74	1.28	0.19	7.97	2.26	2.26	1
1.72	1.28	0.19	7.97	2.26	2.26	1
1.71	1.27	0.19	7.97	2.26	2.26	1
1.70	1.27	0.19	7.97	2.26	2.26	1
1.69	1.26	0.19	7.97	2.26	2.26	1
1.67	1.26	0.19	7.97	2.26	2.26	1
1.66	1.25	0.19	7.97	2.26	2.26	1
1.65	1.25	0.18	7.97	2.26	2.26	1
1.64	1.25	0.18	7.97	2.26	2.26	1
1.62	1.24	0.18	7.97	5.62	5.62	1
1.61	1.23	0.18	7.97	5.63	5.61	1
1.60	1.22	0.18	7.97	5.63	5.60	1
1.59	1.21	0.18	7.97	5.64	5.59	1
1.57	1.20	0.18	7.97	5.65	5.59	1
1.56	1.19	0.17	7.97	5.66	5.58	1
1.55	1.18	0.17	7.97	5.66	5.57	1
1.54	1.17	0.17	7.97	5.67	5.56	1
1.52	1.16	0.17	7.97	5.68	5.55	1
1.51	1.15	0.17	7.97	5.68	5.54	1
1.50	1.15	0.17	7.97	5.69	5.53	1
1.50	1.15	0.17	7.97	5.69	5.53	1
1.49	1.14	0.17	7.97	5.70	5.52	1
1.47	1.13	0.16	7.97	5.70	5.51	1
1.46	1.12	0.16	7.97	5.71	5.50	1
1.45	1.11	0.16	7.97	5.72	5.49	1
1.44	1.10	0.16	7.97	5.72	5.48	1
1.42	1.09	0.16	7.97	5.73	5.48	1
1.41	1.08	0.16	7.97	5.74	5.47	1
1.40	1.07	0.16	7.97	5.74	5.46	1
1.39	1.06	0.15	7.97	5.75	5.45	1
1.37	1.05	0.15	7.97	5.75	5.45	1
1.36	1.04	0.15	7.97	5.76	5.44	1
1.35	1.03	0.15	7.97	5.77	5.44	1
1.34	1.02	0.15	7.97	5.77	5.44	1
1.32	1.01	0.15	7.97	5.78	5.43	1
1.31	1.00	0.15	7.97	5.78	5.43	1
1.30	1.00	0.14	7.97	5.79	5.42	1
1.29	0.99	0.14	7.97	5.79	5.42	1
1.27	0.98	0.14	7.97	5.80	5.41	1
1.26	0.97	0.14	7.97	5.80	5.41	1

1.25	0.96	0.14	7.97	5.81	5.40	1
1.24	0.95	0.14	7.97	5.81	5.40	1
1.22	0.94	0.14	7.97	5.81	5.39	1
1.21	0.93	0.14	7.97	5.82	5.39	1
1.20	0.92	0.13	7.97	5.82	5.38	1
1.19	0.91	0.13	7.97	5.83	5.38	1
1.17	0.90	0.13	7.97	5.83	5.37	1
1.16	0.89	0.13	7.97	5.83	5.37	1
1.15	0.88	0.13	7.97	5.84	5.36	1
1.14	0.87	0.13	7.97	5.84	5.36	1
1.12	0.86	0.13	7.97	5.85	5.36	1
1.11	0.85	0.12	7.97	5.85	5.35	1
1.10	0.84	0.12	7.97	5.85	5.35	1
1.09	0.83	0.12	7.97	5.85	5.34	1
1.07	0.82	0.12	7.97	5.86	5.34	1
1.06	0.81	0.12	7.97	5.86	5.33	1
1.05	0.80	0.12	7.97	5.86	5.33	1
1.04	0.80	0.12	7.97	5.87	5.32	1
1.02	0.79	0.11	7.97	5.87	5.32	1
1.01	0.78	0.11	7.97	5.87	5.31	1
1.00	0.77	0.11	7.97	5.87	5.31	1
1.00	0.77	0.11	7.97	5.87	5.31	1
0.98	0.75	0.11	7.97	5.88	5.30	1
0.95	0.73	0.11	7.97	5.88	5.30	1
0.93	0.71	0.10	7.97	5.88	5.29	1
0.91	0.70	0.10	7.97	5.89	5.29	1
0.89	0.68	0.10	7.97	5.89	5.28	1
0.86	0.66	0.10	7.97	5.89	5.28	1
0.84	0.65	0.09	7.97	5.89	5.27	1
0.82	0.63	0.09	7.97	5.89	5.27	1
0.80	0.61	0.09	7.97	5.90	5.26	1
0.77	0.59	0.09	7.97	5.90	5.26	1
0.75	0.58	0.08	7.97	5.90	5.25	1
0.73	0.56	0.08	7.97	5.90	5.25	1
0.71	0.54	0.08	7.97	5.90	5.24	1
0.68	0.52	0.08	7.97	5.90	5.24	1
0.66	0.51	0.07	7.97	5.90	5.23	1
0.64	0.49	0.07	7.97	5.90	5.23	1
0.62	0.47	0.07	7.97	5.90	5.22	1
0.59	0.46	0.07	7.97	5.90	5.22	1
0.57	0.44	0.06	7.97	5.90	5.21	1
0.55	0.42	0.06	7.97	5.89	5.21	1
0.53	0.40	0.06	7.97	5.89	5.20	1
0.51	0.39	0.06	7.97	5.89	5.20	1
0.48	0.37	0.05	7.97	5.89	5.19	1
0.46	0.35	0.05	7.97	5.89	5.19	1
0.44	0.33	0.05	7.97	5.89	5.18	1
0.42	0.32	0.05	7.97	5.88	5.18	1
0.39	0.30	0.04	7.97	5.88	5.18	1
0.37	0.28	0.04	7.97	5.88	5.17	1
0.35	0.27	0.04	7.97	5.88	5.17	1
0.33	0.25	0.04	7.97	5.87	5.17	1
0.30	0.23	0.03	7.97	5.87	5.16	1
0.28	0.21	0.03	7.97	5.87	5.15	1

0.26	0.20	0.03	7.97	5.87	5.14	1
0.23	0.18	0.03	7.97	5.86	5.13	1
0.21	0.16	0.02	7.97	5.86	5.12	1
0.19	0.14	0.02	7.97	5.86	5.12	1
0.17	0.13	0.02	7.97	5.86	5.11	1
0.14	0.11	0.02	7.97	5.85	5.10	1
0.12	0.09	0.01	7.97	5.85	5.10	1
0.10	0.08	0.01	7.97	5.85	5.09	1
0.10	0.08	0.01	7.97	5.85	5.08	1
0.08	0.06	0.01	7.97	5.83	5.08	1
0.06	0.05	0.01	7.97	5.82	5.07	1
0.04	0.03	0.00	7.97	5.80	5.07	1
0.02	0.02	0.00	7.97	5.79	5.06	1
0.00	0.00	0.00	7.97	5.78	5.05	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
1.56	0.00	0.00	0.00	0.00	0.00	1
1.56	0.30	0.30	0.00	0.00	0.00	1
1.55	0.61	0.61	0.00	0.00	0.00	1
1.55	0.91	0.91	0.00	0.00	0.00	1
1.54	1.21	1.21	0.00	0.00	0.00	1
1.54	1.51	1.51	0.00	0.00	0.00	1
1.53	1.82	1.82	0.00	0.00	0.00	1
1.53	2.12	2.12	0.00	0.00	0.00	1
1.52	2.42	2.42	0.00	0.00	0.00	1
1.52	2.72	2.72	0.00	0.00	0.00	1
1.52	3.03	3.03	0.00	0.00	0.00	1
1.51	3.33	3.33	0.00	0.00	0.00	1
1.51	3.63	3.63	0.00	0.00	0.00	1
1.50	3.93	3.93	0.00	0.00	0.00	1
1.50	4.24	4.24	0.00	0.00	0.00	1
1.49	4.54	4.54	0.00	0.00	0.00	1
1.49	4.84	4.84	0.00	0.00	0.00	1
1.48	5.14	5.14	0.00	0.00	0.00	1
1.48	5.45	5.45	0.00	0.00	0.00	1
1.47	5.75	5.75	0.00	0.00	0.00	1
1.47	6.05	6.05	0.00	0.00	0.00	1
1.47	6.35	6.35	0.00	0.00	0.00	1
1.46	6.66	6.66	0.00	0.00	0.00	1
1.46	6.96	6.96	0.00	0.00	0.00	1
1.45	7.26	7.26	0.00	0.00	0.00	1
1.45	7.56	7.56	0.00	0.00	0.00	1
1.44	7.87	7.87	0.00	0.00	0.00	1
1.44	8.17	8.17	0.00	0.00	0.00	1
1.43	8.47	8.47	0.00	0.00	0.00	1
1.43	8.77	8.77	0.00	0.00	0.00	1
1.42	9.08	9.08	0.00	0.00	0.00	1
1.42	9.38	9.38	0.00	0.00	0.00	1
1.42	9.68	9.68	0.00	0.00	0.00	1
1.41	9.98	9.98	0.00	0.00	0.00	1
1.41	10.29	10.29	0.00	0.00	0.00	1

1.40	10.59	10.59	0.00	0.00	0.00	1
1.40	10.89	10.89	0.00	0.00	0.00	1
1.39	11.19	11.19	0.00	0.00	0.00	1
1.39	11.50	11.50	0.00	0.00	0.00	1
1.38	11.80	11.80	0.00	0.00	0.00	1
1.38	12.10	12.10	0.00	0.00	0.00	1
1.38	12.40	12.40	0.00	0.00	0.00	1
1.37	12.77	12.77	0.00	0.00	0.00	1
1.37	13.14	13.14	0.00	0.00	0.00	1
1.36	13.44	13.44	0.00	0.00	0.00	1
1.36	13.74	13.74	0.00	0.00	0.00	1
1.35	14.04	14.04	0.00	0.00	0.00	1
1.35	14.35	14.35	0.00	0.00	0.00	1
1.34	14.65	14.65	0.00	0.00	0.00	1
1.34	14.95	14.95	0.00	0.00	0.00	1
1.34	15.25	15.25	0.00	0.00	0.00	1
1.33	15.56	15.56	0.00	0.00	0.00	1
1.33	15.86	15.86	0.00	0.00	0.00	1
1.32	16.16	16.16	0.00	0.00	0.00	1
1.32	16.46	16.46	0.00	0.00	0.00	1
1.31	16.77	16.77	0.00	0.00	0.00	1
1.31	17.07	17.07	0.00	0.00	0.00	1
1.30	17.37	17.37	0.00	0.00	0.00	1
1.30	17.67	17.67	0.00	0.00	0.00	1
1.29	17.98	17.98	0.00	0.00	0.00	1
1.29	18.28	18.28	0.00	0.00	0.00	1
1.29	18.58	18.58	0.00	0.00	0.00	1
1.28	18.88	18.88	0.00	0.00	0.00	1
1.28	19.19	19.19	0.00	0.00	0.00	1
1.27	19.49	19.49	0.00	0.00	0.00	1
1.27	19.79	19.79	0.00	0.00	0.00	1
1.26	20.09	20.09	0.00	0.00	0.00	1
1.26	20.40	20.40	0.00	0.00	0.00	1
1.25	20.70	20.70	0.00	0.00	0.00	1
1.25	21.00	21.00	0.00	0.00	0.00	1
1.25	21.31	21.31	0.00	0.00	0.00	1
1.24	35.57	12.28	30.69	19.09	13.87	1
1.23	36.38	17.12	31.54	19.75	9.17	1
1.22	37.19	16.99	32.39	20.42	9.44	1
1.21	38.01	16.87	33.23	21.09	9.72	1
1.20	38.82	16.74	34.07	21.75	9.99	1
1.19	39.63	16.62	34.92	22.42	10.26	1
1.18	40.45	16.50	35.75	23.09	10.53	1
1.17	41.26	16.37	36.59	23.76	10.79	1
1.16	42.08	16.25	37.42	24.43	11.06	1
1.15	42.90	16.14	38.26	25.10	11.32	1
1.15	43.71	16.02	39.09	25.77	11.59	1
1.15	43.71	4.63	39.09	25.77	11.59	1
1.14	44.53	15.90	39.92	26.44	11.85	1
1.13	45.35	15.79	40.74	27.11	12.11	1
1.12	46.16	15.67	41.57	27.79	12.37	1
1.11	46.98	15.56	42.39	28.46	12.63	1
1.10	47.80	15.45	43.21	29.13	12.88	1
1.09	48.62	15.35	44.03	29.80	13.13	1

1.08	49.43	15.24	44.85	30.47	13.39	1
1.07	50.25	15.14	45.67	31.15	13.64	1
1.06	51.07	15.03	46.48	31.82	13.88	1
1.05	51.89	14.93	47.29	32.49	14.13	1
1.04	52.70	14.84	48.10	33.16	14.37	1
1.03	53.52	14.74	48.91	33.83	14.62	1
1.02	54.34	14.65	49.72	34.50	14.86	1
1.01	55.16	14.55	50.52	35.17	15.09	1
1.00	55.97	14.46	51.33	35.84	15.33	1
1.00	56.79	14.38	52.13	36.51	15.56	1
0.99	57.60	14.29	52.93	37.18	15.80	1
0.98	58.42	14.21	53.73	37.85	16.03	1
0.97	59.23	14.12	54.53	38.52	16.25	1
0.96	60.05	14.04	55.32	39.19	16.48	1
0.95	60.86	13.97	56.12	39.86	16.70	1
0.94	61.68	13.89	56.91	40.53	16.92	1
0.93	62.49	13.82	57.70	41.20	17.14	1
0.92	63.30	13.75	58.49	41.86	17.36	1
0.91	64.12	13.68	59.28	42.53	17.58	1
0.90	64.93	13.61	60.07	43.20	17.79	1
0.89	65.74	13.54	60.86	43.86	18.00	1
0.88	66.55	13.48	61.64	44.53	18.21	1
0.87	67.36	13.42	62.42	45.19	18.42	1
0.86	68.17	13.36	63.21	45.85	18.62	1
0.85	68.98	13.30	63.99	46.52	18.82	1
0.84	69.79	13.25	64.74	47.18	19.02	1
0.83	70.59	13.20	65.49	47.84	19.22	1
0.82	71.40	13.15	66.23	48.50	19.42	1
0.81	72.21	13.10	66.97	49.16	19.61	1
0.80	73.01	13.05	67.71	49.82	19.81	1
0.80	73.82	13.01	68.45	50.48	20.00	1
0.79	74.62	12.96	69.18	51.14	20.18	1
0.78	75.43	12.92	69.92	51.80	20.37	1
0.77	76.23	12.88	70.65	52.46	20.55	1
0.77	76.23	5.58	70.65	52.46	20.55	1
0.75	77.67	12.82	71.97	53.64	20.89	1
0.73	79.11	12.75	73.28	54.82	21.21	1
0.71	80.55	12.70	74.59	55.99	21.53	1
0.70	81.99	12.65	75.90	57.17	21.84	1
0.68	83.42	12.60	77.20	58.34	22.15	1
0.66	84.86	12.56	78.50	59.51	22.45	1
0.65	86.29	12.53	79.80	60.67	22.75	1
0.63	87.71	12.50	81.10	61.84	23.04	1
0.61	89.14	12.48	82.39	63.00	23.32	1
0.59	90.56	12.46	83.68	64.16	23.60	1
0.58	91.98	12.45	84.96	65.32	23.88	1
0.56	93.40	12.44	86.25	66.47	24.15	1
0.54	94.81	12.44	87.53	67.63	24.42	1
0.52	96.22	12.44	88.80	68.78	24.68	1
0.51	97.63	12.44	90.08	69.92	24.94	1
0.49	99.04	12.45	91.35	71.07	25.19	1
0.47	100.45	12.46	92.62	72.21	25.44	1
0.46	101.85	12.48	93.89	73.35	25.69	1
0.44	103.25	12.50	95.15	74.49	25.93	1

0.42	104.65	12.52	96.42	75.62	26.17	1
0.40	106.04	12.55	97.68	76.76	26.41	1
0.39	107.44	12.57	98.93	77.89	26.64	1
0.37	108.83	12.60	100.19	79.02	26.87	1
0.35	110.21	12.64	101.44	80.14	27.10	1
0.33	111.60	12.67	102.69	81.26	27.33	1
0.32	112.98	12.71	103.94	82.38	27.56	1
0.30	114.36	12.75	105.18	83.50	27.78	1
0.28	115.74	12.79	106.43	84.62	28.00	1
0.27	117.12	12.83	107.67	85.73	28.22	1
0.25	118.49	12.87	108.90	86.84	28.44	1
0.23	119.86	12.91	110.14	87.95	28.66	1
0.21	121.23	12.96	111.37	89.06	28.88	1
0.20	122.59	13.00	112.60	90.16	29.10	1
0.18	123.96	13.04	113.70	91.26	29.32	1
0.16	76.75	13.09	63.66	72.02	-8.36	1
0.14	77.90	13.13	64.76	73.09	-8.33	1
0.13	79.05	13.18	65.87	74.16	-8.30	1
0.11	80.20	13.22	66.97	75.24	-8.26	1
0.09	81.35	13.27	68.08	76.31	-8.23	1
0.08	82.49	13.31	69.18	77.38	-8.20	1
0.08	82.73	13.31	69.42	77.38	-7.96	1
0.06	83.77	13.56	70.21	78.33	-8.12	1
0.05	84.82	13.81	71.00	79.28	-8.28	1
0.03	85.86	14.06	71.80	80.23	-8.43	1
0.02	86.90	14.30	72.60	81.18	-8.58	1
0.00	87.93	14.54	73.40	82.12	0.00	1

Time = 295. Degree of Consolidation = 43.0%

Total Settlement = 0.939

Settlement at End of Primary Consolidation = 1.041

Settlement caused by Primary Consolidation at time 295. = 0.447

Settlement caused by Secondary Compression at time 295. = 0.000

Settlement Due to Desiccation = 0.492

Surface Elevation = 0.63

*****Current Conditions in Dredged Fill*****

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
2.50	1.55	0.28	7.97	2.26	2.26	1
2.49	1.55	0.28	7.97	2.26	2.26	1

2.48	1.54	0.28	7.97	2.26	2.26	1
2.46	1.54	0.27	7.97	2.26	2.26	1
2.45	1.53	0.27	7.97	2.26	2.26	1
2.44	1.53	0.27	7.97	2.26	2.26	1
2.43	1.52	0.27	7.97	2.26	2.26	1
2.41	1.52	0.27	7.97	2.26	2.26	1
2.40	1.51	0.27	7.97	2.26	2.26	1
2.39	1.51	0.27	7.97	2.26	2.26	1
2.38	1.50	0.26	7.97	2.26	2.26	1
2.36	1.50	0.26	7.97	2.26	2.26	1
2.35	1.50	0.26	7.97	2.26	2.26	1
2.34	1.49	0.26	7.97	2.26	2.26	1
2.33	1.49	0.26	7.97	2.26	2.26	1
2.31	1.48	0.26	7.97	2.26	2.26	1
2.30	1.48	0.26	7.97	2.26	2.26	1
2.29	1.47	0.26	7.97	2.26	2.26	1
2.27	1.47	0.25	7.97	2.26	2.26	1
2.26	1.46	0.25	7.97	2.26	2.26	1
2.25	1.46	0.25	7.97	2.26	2.26	1
2.24	1.45	0.25	7.97	2.26	2.26	1
2.22	1.45	0.25	7.97	2.26	2.26	1
2.21	1.45	0.25	7.97	2.26	2.26	1
2.20	1.44	0.25	7.97	2.26	2.26	1
2.19	1.44	0.24	7.97	2.26	2.26	1
2.17	1.43	0.24	7.97	2.26	2.26	1
2.16	1.43	0.24	7.97	2.26	2.26	1
2.15	1.42	0.24	7.97	2.26	2.26	1
2.14	1.42	0.24	7.97	2.26	2.26	1
2.12	1.41	0.24	7.97	2.26	2.26	1
2.11	1.41	0.24	7.97	2.26	2.26	1
2.10	1.40	0.23	7.97	2.26	2.26	1
2.09	1.40	0.23	7.97	2.26	2.26	1
2.07	1.40	0.23	7.97	2.26	2.26	1
2.06	1.39	0.23	7.97	2.26	2.26	1
2.05	1.39	0.23	7.97	2.26	2.26	1
2.04	1.38	0.23	7.97	2.26	2.26	1
2.02	1.38	0.23	7.97	2.26	2.26	1
2.01	1.37	0.22	7.97	2.26	2.26	1
2.00	1.37	0.22	7.97	5.92	2.26	1
2.00	1.37	0.22	7.97	5.92	2.26	1
1.99	1.36	0.22	7.97	2.26	2.26	1
1.97	1.36	0.22	7.97	2.26	2.26	1
1.96	1.35	0.22	7.97	2.26	2.26	1
1.95	1.35	0.22	7.97	2.26	2.26	1
1.94	1.34	0.22	7.97	2.26	2.26	1
1.92	1.34	0.21	7.97	2.26	2.26	1
1.91	1.33	0.21	7.97	2.26	2.26	1
1.90	1.33	0.21	7.97	2.26	2.26	1
1.89	1.32	0.21	7.97	2.26	2.26	1
1.87	1.32	0.21	7.97	2.26	2.26	1
1.86	1.32	0.21	7.97	2.26	2.26	1
1.85	1.31	0.21	7.97	2.26	2.26	1
1.84	1.31	0.20	7.97	2.26	2.26	1
1.82	1.30	0.20	7.97	2.26	2.26	1

1.81	1.30	0.20	7.97	2.26	2.26	1
1.80	1.29	0.20	7.97	2.26	2.26	1
1.79	1.29	0.20	7.97	2.26	2.26	1
1.77	1.28	0.20	7.97	2.26	2.26	1
1.76	1.28	0.20	7.97	2.26	2.26	1
1.75	1.27	0.20	7.97	2.26	2.26	1
1.74	1.27	0.19	7.97	2.26	2.26	1
1.72	1.27	0.19	7.97	2.26	2.26	1
1.71	1.26	0.19	7.97	2.26	2.26	1
1.70	1.26	0.19	7.97	2.26	2.26	1
1.69	1.25	0.19	7.97	2.26	2.26	1
1.67	1.25	0.19	7.97	2.26	2.26	1
1.66	1.24	0.19	7.97	2.26	2.26	1
1.65	1.24	0.18	7.97	2.26	2.26	1
1.64	1.23	0.18	7.97	2.26	2.26	1
1.62	1.23	0.18	7.97	5.62	5.62	1
1.61	1.22	0.18	7.97	5.62	5.61	1
1.60	1.21	0.18	7.97	5.63	5.60	1
1.59	1.20	0.18	7.97	5.63	5.59	1
1.57	1.19	0.18	7.97	5.64	5.59	1
1.56	1.18	0.17	7.97	5.64	5.58	1
1.55	1.17	0.17	7.97	5.64	5.57	1
1.54	1.16	0.17	7.97	5.65	5.56	1
1.52	1.15	0.17	7.97	5.65	5.55	1
1.51	1.14	0.17	7.97	5.65	5.54	1
1.50	1.13	0.17	7.97	5.66	5.53	1
1.50	1.13	0.17	7.97	5.66	5.53	1
1.49	1.13	0.17	7.97	5.66	5.52	1
1.47	1.12	0.16	7.97	5.66	5.51	1
1.46	1.11	0.16	7.97	5.67	5.50	1
1.45	1.10	0.16	7.97	5.67	5.49	1
1.44	1.09	0.16	7.97	5.68	5.48	1
1.42	1.08	0.16	7.97	5.68	5.48	1
1.41	1.07	0.16	7.97	5.68	5.47	1
1.40	1.06	0.16	7.97	5.69	5.46	1
1.39	1.05	0.15	7.97	5.69	5.45	1
1.37	1.04	0.15	7.97	5.69	5.45	1
1.36	1.03	0.15	7.97	5.70	5.44	1
1.35	1.02	0.15	7.97	5.70	5.44	1
1.34	1.01	0.15	7.97	5.70	5.44	1
1.32	1.00	0.15	7.97	5.71	5.43	1
1.31	0.99	0.15	7.97	5.71	5.43	1
1.30	0.99	0.14	7.97	5.71	5.42	1
1.29	0.98	0.14	7.97	5.71	5.42	1
1.27	0.97	0.14	7.97	5.72	5.41	1
1.26	0.96	0.14	7.97	5.72	5.41	1
1.25	0.95	0.14	7.97	5.72	5.40	1
1.24	0.94	0.14	7.97	5.73	5.40	1
1.22	0.93	0.14	7.97	5.73	5.39	1
1.21	0.92	0.14	7.97	5.73	5.39	1
1.20	0.91	0.13	7.97	5.73	5.38	1
1.19	0.90	0.13	7.97	5.74	5.38	1
1.17	0.89	0.13	7.97	5.74	5.37	1
1.16	0.88	0.13	7.97	5.74	5.37	1

1.15	0.87	0.13	7.97	5.74	5.36	1
1.14	0.86	0.13	7.97	5.75	5.36	1
1.12	0.85	0.13	7.97	5.75	5.36	1
1.11	0.84	0.12	7.97	5.75	5.35	1
1.10	0.84	0.12	7.97	5.75	5.35	1
1.09	0.83	0.12	7.97	5.76	5.34	1
1.07	0.82	0.12	7.97	5.76	5.34	1
1.06	0.81	0.12	7.97	5.76	5.33	1
1.05	0.80	0.12	7.97	5.76	5.33	1
1.04	0.79	0.12	7.97	5.77	5.32	1
1.02	0.78	0.11	7.97	5.77	5.32	1
1.01	0.77	0.11	7.97	5.77	5.31	1
1.00	0.76	0.11	7.97	5.77	5.31	1
1.00	0.76	0.11	7.97	5.77	5.31	1
0.98	0.74	0.11	7.97	5.78	5.30	1
0.95	0.73	0.11	7.97	5.78	5.30	1
0.93	0.71	0.10	7.97	5.78	5.29	1
0.91	0.69	0.10	7.97	5.79	5.29	1
0.89	0.67	0.10	7.97	5.79	5.28	1
0.86	0.66	0.10	7.97	5.79	5.28	1
0.84	0.64	0.09	7.97	5.79	5.27	1
0.82	0.62	0.09	7.97	5.80	5.27	1
0.80	0.61	0.09	7.97	5.80	5.26	1
0.77	0.59	0.09	7.97	5.80	5.26	1
0.75	0.57	0.08	7.97	5.81	5.25	1
0.73	0.56	0.08	7.97	5.81	5.25	1
0.71	0.54	0.08	7.97	5.81	5.24	1
0.68	0.52	0.08	7.97	5.81	5.24	1
0.66	0.50	0.07	7.97	5.81	5.23	1
0.64	0.49	0.07	7.97	5.82	5.23	1
0.62	0.47	0.07	7.97	5.82	5.22	1
0.59	0.45	0.07	7.97	5.82	5.22	1
0.57	0.44	0.06	7.97	5.82	5.21	1
0.55	0.42	0.06	7.97	5.82	5.21	1
0.53	0.40	0.06	7.97	5.83	5.20	1
0.51	0.38	0.06	7.97	5.83	5.20	1
0.48	0.37	0.05	7.97	5.83	5.19	1
0.46	0.35	0.05	7.97	5.83	5.19	1
0.44	0.33	0.05	7.97	5.83	5.18	1
0.42	0.32	0.05	7.97	5.83	5.18	1
0.39	0.30	0.04	7.97	5.83	5.18	1
0.37	0.28	0.04	7.97	5.83	5.17	1
0.35	0.26	0.04	7.97	5.84	5.17	1
0.33	0.25	0.04	7.97	5.84	5.17	1
0.30	0.23	0.03	7.97	5.84	5.16	1
0.28	0.21	0.03	7.97	5.84	5.15	1
0.26	0.20	0.03	7.97	5.84	5.14	1
0.23	0.18	0.03	7.97	5.84	5.13	1
0.21	0.16	0.02	7.97	5.84	5.12	1
0.19	0.14	0.02	7.97	5.84	5.12	1
0.17	0.13	0.02	7.97	5.84	5.11	1
0.14	0.11	0.02	7.97	5.84	5.10	1
0.12	0.09	0.01	7.97	5.84	5.10	1
0.10	0.08	0.01	7.97	5.84	5.09	1

0.10	0.08	0.01	7.97	5.84	5.08	1
0.08	0.06	0.01	7.97	5.83	5.08	1
0.06	0.05	0.01	7.97	5.82	5.07	1
0.04	0.03	0.00	7.97	5.80	5.07	1
0.02	0.02	0.00	7.97	5.79	5.06	1
0.00	0.00	0.00	7.97	5.77	5.05	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
1.55	0.00	0.00	0.00	0.00	0.00	1
1.55	0.30	0.30	0.00	0.00	0.00	1
1.54	0.61	0.61	0.00	0.00	0.00	1
1.54	0.91	0.91	0.00	0.00	0.00	1
1.53	1.21	1.21	0.00	0.00	0.00	1
1.53	1.51	1.51	0.00	0.00	0.00	1
1.52	1.82	1.82	0.00	0.00	0.00	1
1.52	2.12	2.12	0.00	0.00	0.00	1
1.51	2.42	2.42	0.00	0.00	0.00	1
1.51	2.72	2.72	0.00	0.00	0.00	1
1.50	3.03	3.03	0.00	0.00	0.00	1
1.50	3.33	3.33	0.00	0.00	0.00	1
1.50	3.63	3.63	0.00	0.00	0.00	1
1.49	3.93	3.93	0.00	0.00	0.00	1
1.49	4.24	4.24	0.00	0.00	0.00	1
1.48	4.54	4.54	0.00	0.00	0.00	1
1.48	4.84	4.84	0.00	0.00	0.00	1
1.47	5.14	5.14	0.00	0.00	0.00	1
1.47	5.45	5.45	0.00	0.00	0.00	1
1.46	5.75	5.75	0.00	0.00	0.00	1
1.46	6.05	6.05	0.00	0.00	0.00	1
1.45	6.35	6.35	0.00	0.00	0.00	1
1.45	6.66	6.66	0.00	0.00	0.00	1
1.45	6.96	6.96	0.00	0.00	0.00	1
1.44	7.26	7.26	0.00	0.00	0.00	1
1.44	7.56	7.56	0.00	0.00	0.00	1
1.43	7.87	7.87	0.00	0.00	0.00	1
1.43	8.17	8.17	0.00	0.00	0.00	1
1.42	8.47	8.47	0.00	0.00	0.00	1
1.42	8.77	8.77	0.00	0.00	0.00	1
1.41	9.08	9.08	0.00	0.00	0.00	1
1.41	9.38	9.38	0.00	0.00	0.00	1
1.40	9.68	9.68	0.00	0.00	0.00	1
1.40	9.98	9.98	0.00	0.00	0.00	1
1.40	10.29	10.29	0.00	0.00	0.00	1
1.39	10.59	10.59	0.00	0.00	0.00	1
1.39	10.89	10.89	0.00	0.00	0.00	1
1.38	11.19	11.19	0.00	0.00	0.00	1
1.38	11.50	11.50	0.00	0.00	0.00	1
1.37	11.80	11.80	0.00	0.00	0.00	1
1.37	12.10	12.10	0.00	0.00	0.00	1
1.37	12.40	12.40	0.00	0.00	0.00	1
1.36	12.77	12.77	0.00	0.00	0.00	1

1.36	13.14	13.14	0.00	0.00	0.00	1
1.35	13.44	13.44	0.00	0.00	0.00	1
1.35	13.74	13.74	0.00	0.00	0.00	1
1.34	14.04	14.04	0.00	0.00	0.00	1
1.34	14.35	14.35	0.00	0.00	0.00	1
1.33	14.65	14.65	0.00	0.00	0.00	1
1.33	14.95	14.95	0.00	0.00	0.00	1
1.32	15.25	15.25	0.00	0.00	0.00	1
1.32	15.56	15.56	0.00	0.00	0.00	1
1.32	15.86	15.86	0.00	0.00	0.00	1
1.31	16.16	16.16	0.00	0.00	0.00	1
1.31	16.46	16.46	0.00	0.00	0.00	1
1.30	16.77	16.77	0.00	0.00	0.00	1
1.30	17.07	17.07	0.00	0.00	0.00	1
1.29	17.37	17.37	0.00	0.00	0.00	1
1.29	17.67	17.67	0.00	0.00	0.00	1
1.28	17.98	17.98	0.00	0.00	0.00	1
1.28	18.28	18.28	0.00	0.00	0.00	1
1.27	18.58	18.58	0.00	0.00	0.00	1
1.27	18.88	18.88	0.00	0.00	0.00	1
1.27	19.19	19.19	0.00	0.00	0.00	1
1.26	19.49	19.49	0.00	0.00	0.00	1
1.26	19.79	19.79	0.00	0.00	0.00	1
1.25	20.09	20.09	0.00	0.00	0.00	1
1.25	20.40	20.40	0.00	0.00	0.00	1
1.24	20.70	20.70	0.00	0.00	0.00	1
1.24	21.00	21.00	0.00	0.00	0.00	1
1.23	21.31	21.31	0.00	0.00	0.00	1
1.23	35.57	12.28	30.69	19.09	13.87	1
1.22	36.38	17.18	31.54	19.75	9.11	1
1.21	37.19	17.11	32.39	20.42	9.32	1
1.20	38.01	17.05	33.23	21.09	9.54	1
1.19	38.82	16.98	34.07	21.75	9.75	1
1.18	39.63	16.91	34.92	22.42	9.96	1
1.17	40.45	16.85	35.75	23.09	10.17	1
1.16	41.26	16.78	36.59	23.76	10.38	1
1.15	42.08	16.72	37.42	24.43	10.60	1
1.14	42.90	16.66	38.26	25.10	10.80	1
1.13	43.71	16.59	39.09	25.77	11.01	1
1.13	43.71	4.63	39.09	25.77	11.01	1
1.13	44.53	16.53	39.92	26.44	11.22	1
1.12	45.35	16.47	40.74	27.11	11.43	1
1.11	46.16	16.41	41.57	27.79	11.64	1
1.10	46.98	16.34	42.39	28.46	11.84	1
1.09	47.80	16.28	43.21	29.13	12.05	1
1.08	48.62	16.22	44.03	29.80	12.26	1
1.07	49.43	16.17	44.85	30.47	12.46	1
1.06	50.25	16.11	45.67	31.15	12.66	1
1.05	51.07	16.05	46.48	31.82	12.87	1
1.04	51.89	15.99	47.29	32.49	13.07	1
1.03	52.70	15.94	48.10	33.16	13.27	1
1.02	53.52	15.88	48.91	33.83	13.47	1
1.01	54.34	15.83	49.72	34.50	13.67	1
1.00	55.16	15.77	50.52	35.17	13.87	1

0.99	55.97	15.72	51.33	35.84	14.07	1
0.99	56.79	15.67	52.13	36.51	14.27	1
0.98	57.60	15.62	52.93	37.18	14.47	1
0.97	58.42	15.57	53.73	37.85	14.66	1
0.96	59.23	15.52	54.53	38.52	14.86	1
0.95	60.05	15.47	55.32	39.19	15.05	1
0.94	60.86	15.42	56.12	39.86	15.25	1
0.93	61.68	15.37	56.91	40.53	15.44	1
0.92	62.49	15.32	57.70	41.20	15.64	1
0.91	63.30	15.28	58.49	41.86	15.83	1
0.90	64.12	15.23	59.28	42.53	16.02	1
0.89	64.93	15.19	60.07	43.20	16.21	1
0.88	65.74	15.14	60.86	43.86	16.40	1
0.87	66.55	15.10	61.64	44.53	16.59	1
0.86	67.36	15.06	62.42	45.19	16.78	1
0.85	68.17	15.01	63.21	45.85	16.97	1
0.84	68.98	14.97	63.99	46.52	17.15	1
0.84	69.79	14.93	64.74	47.18	17.34	1
0.83	70.59	14.89	65.49	47.84	17.53	1
0.82	71.40	14.85	66.23	48.50	17.71	1
0.81	72.21	14.81	66.97	49.16	17.90	1
0.80	73.01	14.78	67.71	49.82	18.08	1
0.79	73.82	14.74	68.45	50.48	18.26	1
0.78	74.62	14.70	69.18	51.14	18.45	1
0.77	75.43	14.67	69.92	51.80	18.63	1
0.76	76.23	14.63	70.65	52.46	18.81	1
0.76	76.23	5.58	70.65	52.46	18.81	1
0.74	77.67	14.57	71.97	53.64	19.13	1
0.73	79.11	14.51	73.28	54.82	19.46	1
0.71	80.55	14.45	74.59	55.99	19.78	1
0.69	81.99	14.39	75.90	57.17	20.10	1
0.67	83.42	14.33	77.20	58.34	20.42	1
0.66	84.86	14.28	78.50	59.51	20.73	1
0.64	86.29	14.23	79.80	60.67	21.05	1
0.62	87.71	14.18	81.10	61.84	21.36	1
0.61	89.14	14.13	82.39	63.00	21.67	1
0.59	90.56	14.09	83.68	64.16	21.97	1
0.57	91.98	14.05	84.96	65.32	22.28	1
0.56	93.40	14.00	86.25	66.47	22.58	1
0.54	94.81	13.96	87.53	67.63	22.89	1
0.52	96.22	13.93	88.80	68.78	23.19	1
0.50	97.63	13.89	90.08	69.92	23.49	1
0.49	99.04	13.85	91.35	71.07	23.78	1
0.47	100.45	13.82	92.62	72.21	24.08	1
0.45	101.85	13.79	93.89	73.35	24.37	1
0.44	103.25	13.76	95.15	74.49	24.67	1
0.42	104.65	13.73	96.42	75.62	24.96	1
0.40	106.04	13.70	97.68	76.76	25.25	1
0.38	107.44	13.67	98.93	77.89	25.54	1
0.37	108.83	13.65	100.19	79.02	25.83	1
0.35	110.21	13.63	101.44	80.14	26.11	1
0.33	111.60	13.60	102.69	81.26	26.40	1
0.32	112.98	13.58	103.94	82.38	26.68	1
0.30	114.36	13.56	105.18	83.50	26.97	1

0.28	115.74	13.54	106.43	84.62	27.25	1
0.26	117.12	13.52	107.67	85.73	27.53	1
0.25	118.49	13.51	108.90	86.84	27.81	1
0.23	119.86	13.49	110.14	87.95	28.09	1
0.21	121.23	13.47	111.37	89.06	28.36	1
0.20	122.59	13.46	112.60	90.16	28.64	1
0.18	75.85	13.44	62.40	70.96	-8.56	1
0.16	76.99	13.43	63.56	72.03	-8.47	1
0.14	78.14	13.42	64.72	73.10	-8.38	1
0.13	79.29	13.41	65.88	74.17	-8.29	1
0.11	80.43	13.40	67.04	75.24	-8.21	1
0.09	81.58	13.39	68.19	76.31	-8.12	1
0.08	82.73	13.38	69.35	77.38	-8.03	1
0.08	82.96	13.38	69.58	77.38	-7.80	1
0.06	84.01	13.63	70.38	78.34	-7.96	1
0.05	85.05	13.88	71.17	79.28	-8.11	1
0.03	86.09	14.12	71.97	80.23	-8.26	1
0.02	87.13	14.36	72.77	81.18	-8.41	1
0.00	88.17	14.60	73.57	82.12	0.00	1

Time = 390. Degree of Consolidation = 44.%

Total Settlement = 0.950

Settlement at End of Primary Consolidation = 1.041

Settlement caused by Primary Consolidation at time 390. = 0.458

Settlement caused by Secondary Compression at time 390. = 0.000

Settlement Due to Desiccation = 0.492

Surface Elevation = 0.62

*****Current Conditions in Dredged Fill*****

***** Coordinates *****

***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
2.50	1.54	0.28	7.97	2.26	2.26	1
2.49	1.54	0.28	7.97	2.26	2.26	1
2.48	1.53	0.28	7.97	2.26	2.26	1
2.46	1.53	0.27	7.97	2.26	2.26	1
2.45	1.52	0.27	7.97	2.26	2.26	1
2.44	1.52	0.27	7.97	2.26	2.26	1
2.43	1.51	0.27	7.97	2.26	2.26	1
2.41	1.51	0.27	7.97	2.26	2.26	1
2.40	1.51	0.27	7.97	2.26	2.26	1
2.39	1.50	0.27	7.97	2.26	2.26	1

2.38	1.50	0.26	7.97	2.26	2.26	1
2.36	1.49	0.26	7.97	2.26	2.26	1
2.35	1.49	0.26	7.97	2.26	2.26	1
2.34	1.48	0.26	7.97	2.26	2.26	1
2.33	1.48	0.26	7.97	2.26	2.26	1
2.31	1.47	0.26	7.97	2.26	2.26	1
2.30	1.47	0.26	7.97	2.26	2.26	1
2.29	1.46	0.26	7.97	2.26	2.26	1
2.27	1.46	0.25	7.97	2.26	2.26	1
2.26	1.46	0.25	7.97	2.26	2.26	1
2.25	1.45	0.25	7.97	2.26	2.26	1
2.24	1.45	0.25	7.97	2.26	2.26	1
2.22	1.44	0.25	7.97	2.26	2.26	1
2.21	1.44	0.25	7.97	2.26	2.26	1
2.20	1.43	0.25	7.97	2.26	2.26	1
2.19	1.43	0.24	7.97	2.26	2.26	1
2.17	1.42	0.24	7.97	2.26	2.26	1
2.16	1.42	0.24	7.97	2.26	2.26	1
2.15	1.41	0.24	7.97	2.26	2.26	1
2.14	1.41	0.24	7.97	2.26	2.26	1
2.12	1.41	0.24	7.97	2.26	2.26	1
2.11	1.40	0.24	7.97	2.26	2.26	1
2.10	1.40	0.23	7.97	2.26	2.26	1
2.09	1.39	0.23	7.97	2.26	2.26	1
2.07	1.39	0.23	7.97	2.26	2.26	1
2.06	1.38	0.23	7.97	2.26	2.26	1
2.05	1.38	0.23	7.97	2.26	2.26	1
2.04	1.37	0.23	7.97	2.26	2.26	1
2.02	1.37	0.23	7.97	2.26	2.26	1
2.01	1.36	0.22	7.97	2.26	2.26	1
2.00	1.36	0.22	7.97	5.92	2.26	1
2.00	1.36	0.22	7.97	5.92	2.26	1
1.99	1.35	0.22	7.97	2.26	2.26	1
1.97	1.35	0.22	7.97	2.26	2.26	1
1.96	1.34	0.22	7.97	2.26	2.26	1
1.95	1.34	0.22	7.97	2.26	2.26	1
1.94	1.33	0.22	7.97	2.26	2.26	1
1.92	1.33	0.21	7.97	2.26	2.26	1
1.91	1.32	0.21	7.97	2.26	2.26	1
1.90	1.32	0.21	7.97	2.26	2.26	1
1.89	1.32	0.21	7.97	2.26	2.26	1
1.87	1.31	0.21	7.97	2.26	2.26	1
1.86	1.31	0.21	7.97	2.26	2.26	1
1.85	1.30	0.21	7.97	2.26	2.26	1
1.84	1.30	0.20	7.97	2.26	2.26	1
1.82	1.29	0.20	7.97	2.26	2.26	1
1.81	1.29	0.20	7.97	2.26	2.26	1
1.80	1.28	0.20	7.97	2.26	2.26	1
1.79	1.28	0.20	7.97	2.26	2.26	1
1.77	1.27	0.20	7.97	2.26	2.26	1
1.76	1.27	0.20	7.97	2.26	2.26	1
1.75	1.27	0.20	7.97	2.26	2.26	1
1.74	1.26	0.19	7.97	2.26	2.26	1
1.72	1.26	0.19	7.97	2.26	2.26	1

1.71	1.25	0.19	7.97	2.26	2.26	1
1.70	1.25	0.19	7.97	2.26	2.26	1
1.69	1.24	0.19	7.97	2.26	2.26	1
1.67	1.24	0.19	7.97	2.26	2.26	1
1.66	1.23	0.19	7.97	2.26	2.26	1
1.65	1.23	0.18	7.97	2.26	2.26	1
1.64	1.23	0.18	7.97	2.26	2.26	1
1.62	1.22	0.18	7.97	5.62	5.62	1
1.61	1.21	0.18	7.97	5.62	5.61	1
1.60	1.20	0.18	7.97	5.62	5.60	1
1.59	1.19	0.18	7.97	5.63	5.59	1
1.57	1.18	0.18	7.97	5.63	5.59	1
1.56	1.17	0.17	7.97	5.63	5.58	1
1.55	1.16	0.17	7.97	5.63	5.57	1
1.54	1.15	0.17	7.97	5.64	5.56	1
1.52	1.14	0.17	7.97	5.64	5.55	1
1.51	1.14	0.17	7.97	5.64	5.54	1
1.50	1.13	0.17	7.97	5.64	5.53	1
1.50	1.13	0.17	7.97	5.64	5.53	1
1.49	1.12	0.17	7.97	5.65	5.52	1
1.47	1.11	0.16	7.97	5.65	5.51	1
1.46	1.10	0.16	7.97	5.65	5.50	1
1.45	1.09	0.16	7.97	5.65	5.49	1
1.44	1.08	0.16	7.97	5.65	5.48	1
1.42	1.07	0.16	7.97	5.66	5.48	1
1.41	1.06	0.16	7.97	5.66	5.47	1
1.40	1.05	0.16	7.97	5.66	5.46	1
1.39	1.04	0.15	7.97	5.66	5.45	1
1.37	1.03	0.15	7.97	5.66	5.45	1
1.36	1.02	0.15	7.97	5.67	5.44	1
1.35	1.01	0.15	7.97	5.67	5.44	1
1.34	1.01	0.15	7.97	5.67	5.44	1
1.32	1.00	0.15	7.97	5.67	5.43	1
1.31	0.99	0.15	7.97	5.67	5.43	1
1.30	0.98	0.14	7.97	5.68	5.42	1
1.29	0.97	0.14	7.97	5.68	5.42	1
1.27	0.96	0.14	7.97	5.68	5.41	1
1.26	0.95	0.14	7.97	5.68	5.41	1
1.25	0.94	0.14	7.97	5.68	5.40	1
1.24	0.93	0.14	7.97	5.69	5.40	1
1.22	0.92	0.14	7.97	5.69	5.39	1
1.21	0.91	0.14	7.97	5.69	5.39	1
1.20	0.90	0.13	7.97	5.69	5.38	1
1.19	0.89	0.13	7.97	5.69	5.38	1
1.17	0.88	0.13	7.97	5.70	5.37	1
1.16	0.88	0.13	7.97	5.70	5.37	1
1.15	0.87	0.13	7.97	5.70	5.36	1
1.14	0.86	0.13	7.97	5.70	5.36	1
1.12	0.85	0.13	7.97	5.70	5.36	1
1.11	0.84	0.12	7.97	5.70	5.35	1
1.10	0.83	0.12	7.97	5.71	5.35	1
1.09	0.82	0.12	7.97	5.71	5.34	1
1.07	0.81	0.12	7.97	5.71	5.34	1
1.06	0.80	0.12	7.97	5.71	5.33	1

1.05	0.79	0.12	7.97	5.71	5.33	1
1.04	0.78	0.12	7.97	5.71	5.32	1
1.02	0.77	0.11	7.97	5.72	5.32	1
1.01	0.76	0.11	7.97	5.72	5.31	1
1.00	0.75	0.11	7.97	5.72	5.31	1
1.00	0.75	0.11	7.97	5.72	5.31	1
0.98	0.74	0.11	7.97	5.72	5.30	1
0.95	0.72	0.11	7.97	5.72	5.30	1
0.93	0.70	0.10	7.97	5.73	5.29	1
0.91	0.69	0.10	7.97	5.73	5.29	1
0.89	0.67	0.10	7.97	5.73	5.28	1
0.86	0.65	0.10	7.97	5.73	5.28	1
0.84	0.64	0.09	7.97	5.74	5.27	1
0.82	0.62	0.09	7.97	5.74	5.27	1
0.80	0.60	0.09	7.97	5.74	5.26	1
0.77	0.58	0.09	7.97	5.74	5.26	1
0.75	0.57	0.08	7.97	5.75	5.25	1
0.73	0.55	0.08	7.97	5.75	5.25	1
0.71	0.53	0.08	7.97	5.75	5.24	1
0.68	0.52	0.08	7.97	5.75	5.24	1
0.66	0.50	0.07	7.97	5.75	5.23	1
0.64	0.48	0.07	7.97	5.76	5.23	1
0.62	0.47	0.07	7.97	5.76	5.22	1
0.59	0.45	0.07	7.97	5.76	5.22	1
0.57	0.43	0.06	7.97	5.76	5.21	1
0.55	0.42	0.06	7.97	5.76	5.21	1
0.53	0.40	0.06	7.97	5.77	5.20	1
0.51	0.38	0.06	7.97	5.77	5.20	1
0.48	0.36	0.05	7.97	5.77	5.19	1
0.46	0.35	0.05	7.97	5.77	5.19	1
0.44	0.33	0.05	7.97	5.77	5.18	1
0.42	0.31	0.05	7.97	5.77	5.18	1
0.39	0.30	0.04	7.97	5.78	5.18	1
0.37	0.28	0.04	7.97	5.78	5.17	1
0.35	0.26	0.04	7.97	5.78	5.17	1
0.33	0.25	0.04	7.97	5.78	5.17	1
0.30	0.23	0.03	7.97	5.78	5.16	1
0.28	0.21	0.03	7.97	5.78	5.15	1
0.26	0.19	0.03	7.97	5.78	5.14	1
0.23	0.18	0.03	7.97	5.79	5.13	1
0.21	0.16	0.02	7.97	5.79	5.12	1
0.19	0.14	0.02	7.97	5.79	5.12	1
0.17	0.13	0.02	7.97	5.79	5.11	1
0.14	0.11	0.02	7.97	5.79	5.10	1
0.12	0.09	0.01	7.97	5.79	5.10	1
0.10	0.08	0.01	7.97	5.79	5.09	1
0.10	0.08	0.01	7.97	5.79	5.08	1
0.08	0.06	0.01	7.97	5.78	5.08	1
0.06	0.05	0.01	7.97	5.77	5.07	1
0.04	0.03	0.00	7.97	5.75	5.07	1
0.02	0.02	0.00	7.97	5.74	5.06	1
0.00	0.00	0.00	7.97	5.73	5.05	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
1.54	0.00	0.00	0.00	0.00	0.00	1
1.54	0.30	0.30	0.00	0.00	0.00	1
1.53	0.61	0.61	0.00	0.00	0.00	1
1.53	0.91	0.91	0.00	0.00	0.00	1
1.52	1.21	1.21	0.00	0.00	0.00	1
1.52	1.51	1.51	0.00	0.00	0.00	1
1.51	1.82	1.82	0.00	0.00	0.00	1
1.51	2.12	2.12	0.00	0.00	0.00	1
1.51	2.42	2.42	0.00	0.00	0.00	1
1.50	2.72	2.72	0.00	0.00	0.00	1
1.50	3.03	3.03	0.00	0.00	0.00	1
1.49	3.33	3.33	0.00	0.00	0.00	1
1.49	3.63	3.63	0.00	0.00	0.00	1
1.48	3.93	3.93	0.00	0.00	0.00	1
1.48	4.24	4.24	0.00	0.00	0.00	1
1.47	4.54	4.54	0.00	0.00	0.00	1
1.47	4.84	4.84	0.00	0.00	0.00	1
1.46	5.14	5.14	0.00	0.00	0.00	1
1.46	5.45	5.45	0.00	0.00	0.00	1
1.46	5.75	5.75	0.00	0.00	0.00	1
1.45	6.05	6.05	0.00	0.00	0.00	1
1.45	6.35	6.35	0.00	0.00	0.00	1
1.44	6.66	6.66	0.00	0.00	0.00	1
1.44	6.96	6.96	0.00	0.00	0.00	1
1.43	7.26	7.26	0.00	0.00	0.00	1
1.43	7.56	7.56	0.00	0.00	0.00	1
1.42	7.87	7.87	0.00	0.00	0.00	1
1.42	8.17	8.17	0.00	0.00	0.00	1
1.41	8.47	8.47	0.00	0.00	0.00	1
1.41	8.77	8.77	0.00	0.00	0.00	1
1.41	9.08	9.08	0.00	0.00	0.00	1
1.40	9.38	9.38	0.00	0.00	0.00	1
1.40	9.68	9.68	0.00	0.00	0.00	1
1.39	9.98	9.98	0.00	0.00	0.00	1
1.39	10.29	10.29	0.00	0.00	0.00	1
1.38	10.59	10.59	0.00	0.00	0.00	1
1.38	10.89	10.89	0.00	0.00	0.00	1
1.37	11.19	11.19	0.00	0.00	0.00	1
1.37	11.50	11.50	0.00	0.00	0.00	1
1.36	11.80	11.80	0.00	0.00	0.00	1
1.36	12.10	12.10	0.00	0.00	0.00	1
1.36	12.40	12.40	0.00	0.00	0.00	1
1.35	12.77	12.77	0.00	0.00	0.00	1
1.35	13.14	13.14	0.00	0.00	0.00	1
1.34	13.44	13.44	0.00	0.00	0.00	1
1.34	13.74	13.74	0.00	0.00	0.00	1
1.33	14.04	14.04	0.00	0.00	0.00	1
1.33	14.35	14.35	0.00	0.00	0.00	1
1.32	14.65	14.65	0.00	0.00	0.00	1
1.32	14.95	14.95	0.00	0.00	0.00	1
1.32	15.25	15.25	0.00	0.00	0.00	1

1.31	15.56	15.56	0.00	0.00	0.00	1
1.31	15.86	15.86	0.00	0.00	0.00	1
1.30	16.16	16.16	0.00	0.00	0.00	1
1.30	16.46	16.46	0.00	0.00	0.00	1
1.29	16.77	16.77	0.00	0.00	0.00	1
1.29	17.07	17.07	0.00	0.00	0.00	1
1.28	17.37	17.37	0.00	0.00	0.00	1
1.28	17.67	17.67	0.00	0.00	0.00	1
1.27	17.98	17.98	0.00	0.00	0.00	1
1.27	18.28	18.28	0.00	0.00	0.00	1
1.27	18.58	18.58	0.00	0.00	0.00	1
1.26	18.88	18.88	0.00	0.00	0.00	1
1.26	19.19	19.19	0.00	0.00	0.00	1
1.25	19.49	19.49	0.00	0.00	0.00	1
1.25	19.79	19.79	0.00	0.00	0.00	1
1.24	20.09	20.09	0.00	0.00	0.00	1
1.24	20.40	20.40	0.00	0.00	0.00	1
1.23	20.70	20.70	0.00	0.00	0.00	1
1.23	21.00	21.00	0.00	0.00	0.00	1
1.23	21.31	21.31	0.00	0.00	0.00	1
1.22	35.57	12.28	30.69	19.09	13.87	1
1.21	36.38	17.21	31.54	19.75	9.08	1
1.20	37.19	17.17	32.39	20.42	9.27	1
1.19	38.01	17.13	33.23	21.09	9.46	1
1.18	38.82	17.08	34.07	21.75	9.65	1
1.17	39.63	17.04	34.92	22.42	9.83	1
1.16	40.45	17.00	35.75	23.09	10.02	1
1.15	41.26	16.96	36.59	23.76	10.20	1
1.14	42.08	16.92	37.42	24.43	10.39	1
1.14	42.90	16.88	38.26	25.10	10.58	1
1.13	43.71	16.85	39.09	25.77	10.76	1
1.13	43.71	4.63	39.09	25.77	10.76	1
1.12	44.53	16.81	39.92	26.44	10.95	1
1.11	45.35	16.77	40.74	27.11	11.13	1
1.10	46.16	16.73	41.57	27.79	11.31	1
1.09	46.98	16.69	42.39	28.46	11.50	1
1.08	47.80	16.65	43.21	29.13	11.68	1
1.07	48.62	16.62	44.03	29.80	11.86	1
1.06	49.43	16.58	44.85	30.47	12.05	1
1.05	50.25	16.54	45.67	31.15	12.23	1
1.04	51.07	16.51	46.48	31.82	12.41	1
1.03	51.89	16.47	47.29	32.49	12.59	1
1.02	52.70	16.44	48.10	33.16	12.77	1
1.01	53.52	16.40	48.91	33.83	12.96	1
1.01	54.34	16.36	49.72	34.50	13.14	1
1.00	55.16	16.33	50.52	35.17	13.32	1
0.99	55.97	16.30	51.33	35.84	13.50	1
0.98	56.79	16.26	52.13	36.51	13.68	1
0.97	57.60	16.23	52.93	37.18	13.86	1
0.96	58.42	16.20	53.73	37.85	14.03	1
0.95	59.23	16.16	54.53	38.52	14.21	1
0.94	60.05	16.13	55.32	39.19	14.39	1
0.93	60.86	16.10	56.12	39.86	14.57	1
0.92	61.68	16.07	56.91	40.53	14.75	1

0.91	62.49	16.03	57.70	41.20	14.92	1
0.90	63.30	16.00	58.49	41.86	15.10	1
0.89	64.12	15.97	59.28	42.53	15.28	1
0.88	64.93	15.94	60.07	43.20	15.46	1
0.88	65.74	15.91	60.86	43.86	15.63	1
0.87	66.55	15.88	61.64	44.53	15.81	1
0.86	67.36	15.85	62.42	45.19	15.98	1
0.85	68.17	15.82	63.21	45.85	16.16	1
0.84	68.98	15.79	63.99	46.52	16.33	1
0.83	69.79	15.77	64.74	47.18	16.51	1
0.82	70.59	15.74	65.49	47.84	16.68	1
0.81	71.40	15.71	66.23	48.50	16.86	1
0.80	72.21	15.68	66.97	49.16	17.03	1
0.79	73.01	15.65	67.71	49.82	17.20	1
0.78	73.82	15.63	68.45	50.48	17.38	1
0.77	74.62	15.60	69.18	51.14	17.55	1
0.76	75.43	15.57	69.92	51.80	17.72	1
0.75	76.23	15.55	70.65	52.46	17.89	1
0.75	76.23	5.58	70.65	52.46	17.89	1
0.74	77.67	15.50	71.97	53.64	18.20	1
0.72	79.11	15.45	73.28	54.82	18.51	1
0.70	80.55	15.41	74.59	55.99	18.82	1
0.69	81.99	15.36	75.90	57.17	19.13	1
0.67	83.42	15.32	77.20	58.34	19.43	1
0.65	84.86	15.27	78.50	59.51	19.74	1
0.64	86.29	15.23	79.80	60.67	20.04	1
0.62	87.71	15.19	81.10	61.84	20.35	1
0.60	89.14	15.15	82.39	63.00	20.65	1
0.58	90.56	15.11	83.68	64.16	20.95	1
0.57	91.98	15.07	84.96	65.32	21.25	1
0.55	93.40	15.03	86.25	66.47	21.55	1
0.53	94.81	15.00	87.53	67.63	21.85	1
0.52	96.22	14.96	88.80	68.78	22.15	1
0.50	97.63	14.92	90.08	69.92	22.45	1
0.48	99.04	14.89	91.35	71.07	22.75	1
0.47	100.45	14.86	92.62	72.21	23.05	1
0.45	101.85	14.82	93.89	73.35	23.34	1
0.43	103.25	14.79	95.15	74.49	23.64	1
0.42	104.65	14.76	96.42	75.62	23.93	1
0.40	106.04	14.73	97.68	76.76	24.23	1
0.38	107.44	14.69	98.93	77.89	24.52	1
0.36	108.83	14.66	100.19	79.02	24.81	1
0.35	110.21	14.64	101.44	80.14	25.10	1
0.33	111.60	14.61	102.69	81.26	25.39	1
0.31	112.98	14.58	103.94	82.38	25.68	1
0.30	114.36	14.55	105.18	83.50	25.97	1
0.28	115.74	14.52	106.43	84.62	26.26	1
0.26	117.12	14.50	107.67	85.73	26.55	1
0.25	118.49	14.47	108.90	86.84	26.84	1
0.23	119.86	14.45	110.14	87.95	27.13	1
0.21	121.23	14.42	111.37	89.06	27.42	1
0.19	75.02	14.40	60.62	69.98	-9.36	1
0.18	76.16	14.38	61.79	71.04	-9.26	1
0.16	77.30	14.35	62.95	72.10	-9.16	1

0.14	78.44	14.33	64.11	73.17	-9.06	1
0.13	79.58	14.31	65.27	74.23	-8.96	1
0.11	80.72	14.29	66.43	75.29	-8.86	1
0.09	81.86	14.27	67.59	76.36	-8.77	1
0.08	83.00	14.25	68.75	77.42	-8.67	1
0.08	83.23	14.25	68.98	77.42	-8.44	1
0.06	84.27	14.49	69.78	78.36	-8.58	1
0.05	85.30	14.72	70.58	79.31	-8.73	1
0.03	86.34	14.96	71.38	80.25	-8.87	1
0.02	87.37	15.19	72.18	81.18	-9.00	1
0.00	88.40	15.42	72.98	82.12	0.00	1

Time = 755. Degree of Consolidation = 45.0%

Total Settlement = 0.958

Settlement at End of Primary Consolidation = 1.041

Settlement caused by Primary Consolidation at time 755. = 0.466

Settlement caused by Secondary Compression at time 755. = 0.000

Settlement Due to Desiccation = 0.492

Surface Elevation = 0.61

*****Current Conditions in Dredged Fill*****

***** Coordinates *****

***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
2.50	1.54	0.28	7.97	2.26	2.26	1
2.49	1.54	0.28	7.97	2.26	2.26	1
2.48	1.53	0.28	7.97	2.26	2.26	1
2.46	1.53	0.27	7.97	2.26	2.26	1
2.45	1.52	0.27	7.97	2.26	2.26	1
2.44	1.52	0.27	7.97	2.26	2.26	1
2.43	1.51	0.27	7.97	2.26	2.26	1
2.41	1.51	0.27	7.97	2.26	2.26	1
2.40	1.50	0.27	7.97	2.26	2.26	1
2.39	1.50	0.27	7.97	2.26	2.26	1
2.38	1.49	0.26	7.97	2.26	2.26	1
2.36	1.49	0.26	7.97	2.26	2.26	1
2.35	1.49	0.26	7.97	2.26	2.26	1
2.34	1.48	0.26	7.97	2.26	2.26	1
2.33	1.48	0.26	7.97	2.26	2.26	1
2.31	1.47	0.26	7.97	2.26	2.26	1
2.30	1.47	0.26	7.97	2.26	2.26	1
2.29	1.46	0.26	7.97	2.26	2.26	1

2.27	1.46	0.25	7.97	2.26	2.26	1
2.26	1.45	0.25	7.97	2.26	2.26	1
2.25	1.45	0.25	7.97	2.26	2.26	1
2.24	1.44	0.25	7.97	2.26	2.26	1
2.22	1.44	0.25	7.97	2.26	2.26	1
2.21	1.44	0.25	7.97	2.26	2.26	1
2.20	1.43	0.25	7.97	2.26	2.26	1
2.19	1.43	0.24	7.97	2.26	2.26	1
2.17	1.42	0.24	7.97	2.26	2.26	1
2.16	1.42	0.24	7.97	2.26	2.26	1
2.15	1.41	0.24	7.97	2.26	2.26	1
2.14	1.41	0.24	7.97	2.26	2.26	1
2.12	1.40	0.24	7.97	2.26	2.26	1
2.11	1.40	0.24	7.97	2.26	2.26	1
2.10	1.39	0.23	7.97	2.26	2.26	1
2.09	1.39	0.23	7.97	2.26	2.26	1
2.07	1.39	0.23	7.97	2.26	2.26	1
2.06	1.38	0.23	7.97	2.26	2.26	1
2.05	1.38	0.23	7.97	2.26	2.26	1
2.04	1.37	0.23	7.97	2.26	2.26	1
2.02	1.37	0.23	7.97	2.26	2.26	1
2.01	1.36	0.22	7.97	2.26	2.26	1
2.00	1.36	0.22	7.97	5.92	2.26	1
2.00	1.36	0.22	7.97	5.92	2.26	1
1.99	1.35	0.22	7.97	2.26	2.26	1
1.97	1.35	0.22	7.97	2.26	2.26	1
1.96	1.34	0.22	7.97	2.26	2.26	1
1.95	1.34	0.22	7.97	2.26	2.26	1
1.94	1.33	0.22	7.97	2.26	2.26	1
1.92	1.33	0.21	7.97	2.26	2.26	1
1.91	1.32	0.21	7.97	2.26	2.26	1
1.90	1.32	0.21	7.97	2.26	2.26	1
1.89	1.31	0.21	7.97	2.26	2.26	1
1.87	1.31	0.21	7.97	2.26	2.26	1
1.86	1.31	0.21	7.97	2.26	2.26	1
1.85	1.30	0.21	7.97	2.26	2.26	1
1.84	1.30	0.20	7.97	2.26	2.26	1
1.82	1.29	0.20	7.97	2.26	2.26	1
1.81	1.29	0.20	7.97	2.26	2.26	1
1.80	1.28	0.20	7.97	2.26	2.26	1
1.79	1.28	0.20	7.97	2.26	2.26	1
1.77	1.27	0.20	7.97	2.26	2.26	1
1.76	1.27	0.20	7.97	2.26	2.26	1
1.75	1.26	0.20	7.97	2.26	2.26	1
1.74	1.26	0.19	7.97	2.26	2.26	1
1.72	1.26	0.19	7.97	2.26	2.26	1
1.71	1.25	0.19	7.97	2.26	2.26	1
1.70	1.25	0.19	7.97	2.26	2.26	1
1.69	1.24	0.19	7.97	2.26	2.26	1
1.67	1.24	0.19	7.97	2.26	2.26	1
1.66	1.23	0.19	7.97	2.26	2.26	1
1.65	1.23	0.18	7.97	2.26	2.26	1
1.64	1.22	0.18	7.97	2.26	2.26	1
1.62	1.22	0.18	7.97	5.62	5.62	1

1.61	1.21	0.18	7.97	5.62	5.61	1
1.60	1.20	0.18	7.97	5.62	5.60	1
1.59	1.19	0.18	7.97	5.63	5.59	1
1.57	1.18	0.18	7.97	5.63	5.59	1
1.56	1.17	0.17	7.97	5.63	5.58	1
1.55	1.16	0.17	7.97	5.63	5.57	1
1.54	1.15	0.17	7.97	5.63	5.56	1
1.52	1.14	0.17	7.97	5.64	5.55	1
1.51	1.13	0.17	7.97	5.64	5.54	1
1.50	1.12	0.17	7.97	5.64	5.53	1
1.50	1.12	0.17	7.97	5.64	5.53	1
1.49	1.12	0.17	7.97	5.64	5.52	1
1.47	1.11	0.16	7.97	5.65	5.51	1
1.46	1.10	0.16	7.97	5.65	5.50	1
1.45	1.09	0.16	7.97	5.65	5.49	1
1.44	1.08	0.16	7.97	5.65	5.48	1
1.42	1.07	0.16	7.97	5.65	5.48	1
1.41	1.06	0.16	7.97	5.66	5.47	1
1.40	1.05	0.16	7.97	5.66	5.46	1
1.39	1.04	0.15	7.97	5.66	5.45	1
1.37	1.03	0.15	7.97	5.66	5.45	1
1.36	1.02	0.15	7.97	5.66	5.44	1
1.35	1.01	0.15	7.97	5.66	5.44	1
1.34	1.00	0.15	7.97	5.67	5.44	1
1.32	1.00	0.15	7.97	5.67	5.43	1
1.31	0.99	0.15	7.97	5.67	5.43	1
1.30	0.98	0.14	7.97	5.67	5.42	1
1.29	0.97	0.14	7.97	5.67	5.42	1
1.27	0.96	0.14	7.97	5.68	5.41	1
1.26	0.95	0.14	7.97	5.68	5.41	1
1.25	0.94	0.14	7.97	5.68	5.40	1
1.24	0.93	0.14	7.97	5.68	5.40	1
1.22	0.92	0.14	7.97	5.68	5.39	1
1.21	0.91	0.14	7.97	5.68	5.39	1
1.20	0.90	0.13	7.97	5.69	5.38	1
1.19	0.89	0.13	7.97	5.69	5.38	1
1.17	0.88	0.13	7.97	5.69	5.37	1
1.16	0.87	0.13	7.97	5.69	5.37	1
1.15	0.86	0.13	7.97	5.69	5.36	1
1.14	0.86	0.13	7.97	5.69	5.36	1
1.12	0.85	0.13	7.97	5.70	5.36	1
1.11	0.84	0.12	7.97	5.70	5.35	1
1.10	0.83	0.12	7.97	5.70	5.35	1
1.09	0.82	0.12	7.97	5.70	5.34	1
1.07	0.81	0.12	7.97	5.70	5.34	1
1.06	0.80	0.12	7.97	5.70	5.33	1
1.05	0.79	0.12	7.97	5.70	5.33	1
1.04	0.78	0.12	7.97	5.71	5.32	1
1.02	0.77	0.11	7.97	5.71	5.32	1
1.01	0.76	0.11	7.97	5.71	5.31	1
1.00	0.75	0.11	7.97	5.71	5.31	1
1.00	0.75	0.11	7.97	5.71	5.31	1
0.98	0.74	0.11	7.97	5.71	5.30	1
0.95	0.72	0.11	7.97	5.72	5.30	1

0.93	0.70	0.10	7.97	5.72	5.29	1
0.91	0.69	0.10	7.97	5.72	5.29	1
0.89	0.67	0.10	7.97	5.72	5.28	1
0.86	0.65	0.10	7.97	5.73	5.28	1
0.84	0.63	0.09	7.97	5.73	5.27	1
0.82	0.62	0.09	7.97	5.73	5.27	1
0.80	0.60	0.09	7.97	5.73	5.26	1
0.77	0.58	0.09	7.97	5.73	5.26	1
0.75	0.57	0.08	7.97	5.74	5.25	1
0.73	0.55	0.08	7.97	5.74	5.25	1
0.71	0.53	0.08	7.97	5.74	5.24	1
0.68	0.52	0.08	7.97	5.74	5.24	1
0.66	0.50	0.07	7.97	5.74	5.23	1
0.64	0.48	0.07	7.97	5.75	5.23	1
0.62	0.47	0.07	7.97	5.75	5.22	1
0.59	0.45	0.07	7.97	5.75	5.22	1
0.57	0.43	0.06	7.97	5.75	5.21	1
0.55	0.41	0.06	7.97	5.75	5.21	1
0.53	0.40	0.06	7.97	5.76	5.20	1
0.51	0.38	0.06	7.97	5.76	5.20	1
0.48	0.36	0.05	7.97	5.76	5.19	1
0.46	0.35	0.05	7.97	5.76	5.19	1
0.44	0.33	0.05	7.97	5.76	5.18	1
0.42	0.31	0.05	7.97	5.76	5.18	1
0.39	0.30	0.04	7.97	5.77	5.18	1
0.37	0.28	0.04	7.97	5.77	5.17	1
0.35	0.26	0.04	7.97	5.77	5.17	1
0.33	0.25	0.04	7.97	5.77	5.17	1
0.30	0.23	0.03	7.97	5.77	5.16	1
0.28	0.21	0.03	7.97	5.77	5.15	1
0.26	0.19	0.03	7.97	5.78	5.14	1
0.23	0.18	0.03	7.97	5.78	5.13	1
0.21	0.16	0.02	7.97	5.78	5.12	1
0.19	0.14	0.02	7.97	5.78	5.12	1
0.17	0.13	0.02	7.97	5.78	5.11	1
0.14	0.11	0.02	7.97	5.78	5.10	1
0.12	0.09	0.01	7.97	5.78	5.10	1
0.10	0.08	0.01	7.97	5.78	5.09	1
0.10	0.08	0.01	7.97	5.78	5.08	1
0.08	0.06	0.01	7.97	5.77	5.08	1
0.06	0.05	0.01	7.97	5.76	5.07	1
0.04	0.03	0.00	7.97	5.74	5.07	1
0.02	0.01	0.00	7.97	5.73	5.06	1
0.00	0.00	0.00	7.97	5.72	5.05	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess Material	
1.54	0.00	0.00	0.00	0.00	0.00	1
1.54	0.30	0.30	0.00	0.00	0.00	1
1.53	0.61	0.61	0.00	0.00	0.00	1
1.53	0.91	0.91	0.00	0.00	0.00	1
1.52	1.21	1.21	0.00	0.00	0.00	1

1.52	1.51	1.51	0.00	0.00	0.00	1
1.51	1.82	1.82	0.00	0.00	0.00	1
1.51	2.12	2.12	0.00	0.00	0.00	1
1.50	2.42	2.42	0.00	0.00	0.00	1
1.50	2.72	2.72	0.00	0.00	0.00	1
1.49	3.03	3.03	0.00	0.00	0.00	1
1.49	3.33	3.33	0.00	0.00	0.00	1
1.49	3.63	3.63	0.00	0.00	0.00	1
1.48	3.93	3.93	0.00	0.00	0.00	1
1.48	4.24	4.24	0.00	0.00	0.00	1
1.47	4.54	4.54	0.00	0.00	0.00	1
1.47	4.84	4.84	0.00	0.00	0.00	1
1.46	5.14	5.14	0.00	0.00	0.00	1
1.46	5.45	5.45	0.00	0.00	0.00	1
1.45	5.75	5.75	0.00	0.00	0.00	1
1.45	6.05	6.05	0.00	0.00	0.00	1
1.44	6.35	6.35	0.00	0.00	0.00	1
1.44	6.66	6.66	0.00	0.00	0.00	1
1.44	6.96	6.96	0.00	0.00	0.00	1
1.43	7.26	7.26	0.00	0.00	0.00	1
1.43	7.56	7.56	0.00	0.00	0.00	1
1.42	7.87	7.87	0.00	0.00	0.00	1
1.42	8.17	8.17	0.00	0.00	0.00	1
1.41	8.47	8.47	0.00	0.00	0.00	1
1.41	8.77	8.77	0.00	0.00	0.00	1
1.40	9.08	9.08	0.00	0.00	0.00	1
1.40	9.38	9.38	0.00	0.00	0.00	1
1.39	9.68	9.68	0.00	0.00	0.00	1
1.39	9.98	9.98	0.00	0.00	0.00	1
1.39	10.29	10.29	0.00	0.00	0.00	1
1.38	10.59	10.59	0.00	0.00	0.00	1
1.38	10.89	10.89	0.00	0.00	0.00	1
1.37	11.19	11.19	0.00	0.00	0.00	1
1.37	11.50	11.50	0.00	0.00	0.00	1
1.36	11.80	11.80	0.00	0.00	0.00	1
1.36	12.10	12.10	0.00	0.00	0.00	1
1.36	12.40	12.40	0.00	0.00	0.00	1
1.35	12.77	12.77	0.00	0.00	0.00	1
1.35	13.14	13.14	0.00	0.00	0.00	1
1.34	13.44	13.44	0.00	0.00	0.00	1
1.34	13.74	13.74	0.00	0.00	0.00	1
1.33	14.04	14.04	0.00	0.00	0.00	1
1.33	14.35	14.35	0.00	0.00	0.00	1
1.32	14.65	14.65	0.00	0.00	0.00	1
1.32	14.95	14.95	0.00	0.00	0.00	1
1.31	15.25	15.25	0.00	0.00	0.00	1
1.31	15.56	15.56	0.00	0.00	0.00	1
1.31	15.86	15.86	0.00	0.00	0.00	1
1.30	16.16	16.16	0.00	0.00	0.00	1
1.30	16.46	16.46	0.00	0.00	0.00	1
1.29	16.77	16.77	0.00	0.00	0.00	1
1.29	17.07	17.07	0.00	0.00	0.00	1
1.28	17.37	17.37	0.00	0.00	0.00	1
1.28	17.67	17.67	0.00	0.00	0.00	1

1.27	17.98	17.98	0.00	0.00	0.00	1
1.27	18.28	18.28	0.00	0.00	0.00	1
1.26	18.58	18.58	0.00	0.00	0.00	1
1.26	18.88	18.88	0.00	0.00	0.00	1
1.26	19.19	19.19	0.00	0.00	0.00	1
1.25	19.49	19.49	0.00	0.00	0.00	1
1.25	19.79	19.79	0.00	0.00	0.00	1
1.24	20.09	20.09	0.00	0.00	0.00	1
1.24	20.40	20.40	0.00	0.00	0.00	1
1.23	20.70	20.70	0.00	0.00	0.00	1
1.23	21.00	21.00	0.00	0.00	0.00	1
1.22	21.31	21.31	0.00	0.00	0.00	1
1.22	35.57	12.28	30.69	19.09	13.87	1
1.21	36.38	17.21	31.54	19.75	9.08	1
1.20	37.19	17.17	32.39	20.42	9.26	1
1.19	38.01	17.14	33.23	21.09	9.45	1
1.18	38.82	17.10	34.07	21.75	9.63	1
1.17	39.63	17.06	34.92	22.42	9.81	1
1.16	40.45	17.02	35.75	23.09	10.00	1
1.15	41.26	16.99	36.59	23.76	10.18	1
1.14	42.08	16.95	37.42	24.43	10.36	1
1.13	42.90	16.92	38.26	25.10	10.54	1
1.12	43.71	16.88	39.09	25.77	10.73	1
1.12	43.71	4.63	39.09	25.77	10.73	1
1.12	44.53	16.84	39.92	26.44	10.91	1
1.11	45.35	16.81	40.74	27.11	11.09	1
1.10	46.16	16.77	41.57	27.79	11.27	1
1.09	46.98	16.74	42.39	28.46	11.45	1
1.08	47.80	16.70	43.21	29.13	11.63	1
1.07	48.62	16.67	44.03	29.80	11.81	1
1.06	49.43	16.64	44.85	30.47	11.99	1
1.05	50.25	16.60	45.67	31.15	12.17	1
1.04	51.07	16.57	46.48	31.82	12.35	1
1.03	51.89	16.54	47.29	32.49	12.53	1
1.02	52.70	16.50	48.10	33.16	12.71	1
1.01	53.52	16.47	48.91	33.83	12.88	1
1.00	54.34	16.44	49.72	34.50	13.06	1
1.00	55.16	16.41	50.52	35.17	13.24	1
0.99	55.97	16.38	51.33	35.84	13.42	1
0.98	56.79	16.35	52.13	36.51	13.59	1
0.97	57.60	16.31	52.93	37.18	13.77	1
0.96	58.42	16.28	53.73	37.85	13.95	1
0.95	59.23	16.25	54.53	38.52	14.12	1
0.94	60.05	16.22	55.32	39.19	14.30	1
0.93	60.86	16.19	56.12	39.86	14.47	1
0.92	61.68	16.16	56.91	40.53	14.65	1
0.91	62.49	16.14	57.70	41.20	14.82	1
0.90	63.30	16.11	58.49	41.86	15.00	1
0.89	64.12	16.08	59.28	42.53	15.17	1
0.88	64.93	16.05	60.07	43.20	15.35	1
0.87	65.74	16.02	60.86	43.86	15.52	1
0.86	66.55	15.99	61.64	44.53	15.69	1
0.86	67.36	15.97	62.42	45.19	15.87	1
0.85	68.17	15.94	63.21	45.85	16.04	1

0.84	68.98	15.91	63.99	46.52	16.21	1
0.83	69.79	15.89	64.74	47.18	16.39	1
0.82	70.59	15.86	65.49	47.84	16.56	1
0.81	71.40	15.83	66.23	48.50	16.73	1
0.80	72.21	15.81	66.97	49.16	16.90	1
0.79	73.01	15.78	67.71	49.82	17.07	1
0.78	73.82	15.76	68.45	50.48	17.25	1
0.77	74.62	15.73	69.18	51.14	17.42	1
0.76	75.43	15.71	69.92	51.80	17.59	1
0.75	76.23	15.68	70.65	52.46	17.76	1
0.75	76.23	5.58	70.65	52.46	17.76	1
0.74	77.67	15.64	71.97	53.64	18.07	1
0.72	79.11	15.59	73.28	54.82	18.37	1
0.70	80.55	15.55	74.59	55.99	18.68	1
0.69	81.99	15.51	75.90	57.17	18.98	1
0.67	83.42	15.46	77.20	58.34	19.29	1
0.65	84.86	15.42	78.50	59.51	19.59	1
0.63	86.29	15.38	79.80	60.67	19.89	1
0.62	87.71	15.34	81.10	61.84	20.19	1
0.60	89.14	15.31	82.39	63.00	20.50	1
0.58	90.56	15.27	83.68	64.16	20.80	1
0.57	91.98	15.23	84.96	65.32	21.10	1
0.55	93.40	15.19	86.25	66.47	21.39	1
0.53	94.81	15.16	87.53	67.63	21.69	1
0.52	96.22	15.12	88.80	68.78	21.99	1
0.50	97.63	15.09	90.08	69.92	22.29	1
0.48	99.04	15.05	91.35	71.07	22.59	1
0.47	100.45	15.02	92.62	72.21	22.88	1
0.45	101.85	14.99	93.89	73.35	23.18	1
0.43	103.25	14.95	95.15	74.49	23.47	1
0.41	104.65	14.92	96.42	75.62	23.77	1
0.40	106.04	14.89	97.68	76.76	24.06	1
0.38	107.44	14.86	98.93	77.89	24.35	1
0.36	108.83	14.83	100.19	79.02	24.64	1
0.35	110.21	14.80	101.44	80.14	24.94	1
0.33	111.60	14.77	102.69	81.26	25.23	1
0.31	112.98	14.74	103.94	82.38	25.52	1
0.30	114.36	14.72	105.18	83.50	25.81	1
0.28	115.74	14.69	106.43	84.62	26.10	1
0.26	117.12	14.66	107.67	85.73	26.39	1
0.25	118.49	14.64	108.90	86.84	26.68	1
0.23	119.86	14.61	110.14	87.95	26.97	1
0.21	74.14	14.58	59.55	68.94	-9.38	1
0.19	75.27	14.56	60.71	70.00	-9.28	1
0.18	76.41	14.53	61.87	71.06	-9.18	1
0.16	77.55	14.51	63.03	72.12	-9.08	1
0.14	78.68	14.49	64.20	73.18	-8.98	1
0.13	79.82	14.46	65.36	74.24	-8.88	1
0.11	80.96	14.44	66.52	75.30	-8.78	1
0.09	82.10	14.42	67.68	76.36	-8.69	1
0.08	83.23	14.40	68.84	77.42	-8.59	1
0.08	83.47	14.40	69.07	77.42	-8.35	1
0.06	84.50	14.64	69.87	78.37	-8.50	1
0.05	85.54	14.87	70.67	79.31	-8.64	1

0.03	86.57	15.10	71.47	80.25	-8.78	1
0.01	87.60	15.33	72.27	81.19	-8.92	1
0.00	88.63	15.56	73.07	82.12	0.00	1

Time = 1120. Degree of Consolidation = 45.0%

Total Settlement = 0.960

Settlement at End of Primary Consolidation = 1.041

Settlement caused by Primary Consolidation at time 1120. = 0.467

Settlement caused by Secondary Compression at time 1120. = 0.000

Settlement Due to Desiccation = 0.492

Surface Elevation = 0.61

*****Current Conditions in Dredged Fill*****

***** Coordinates *****

***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
2.50	1.54	0.28	7.97	2.26	2.26	1
2.49	1.54	0.28	7.97	2.26	2.26	1
2.48	1.53	0.28	7.97	2.26	2.26	1
2.46	1.53	0.27	7.97	2.26	2.26	1
2.45	1.52	0.27	7.97	2.26	2.26	1
2.44	1.52	0.27	7.97	2.26	2.26	1
2.43	1.51	0.27	7.97	2.26	2.26	1
2.41	1.51	0.27	7.97	2.26	2.26	1
2.40	1.50	0.27	7.97	2.26	2.26	1
2.39	1.50	0.27	7.97	2.26	2.26	1
2.38	1.49	0.26	7.97	2.26	2.26	1
2.36	1.49	0.26	7.97	2.26	2.26	1
2.35	1.49	0.26	7.97	2.26	2.26	1
2.34	1.48	0.26	7.97	2.26	2.26	1
2.33	1.48	0.26	7.97	2.26	2.26	1
2.31	1.47	0.26	7.97	2.26	2.26	1
2.30	1.47	0.26	7.97	2.26	2.26	1
2.29	1.46	0.26	7.97	2.26	2.26	1
2.27	1.46	0.25	7.97	2.26	2.26	1
2.26	1.45	0.25	7.97	2.26	2.26	1
2.25	1.45	0.25	7.97	2.26	2.26	1
2.24	1.44	0.25	7.97	2.26	2.26	1
2.22	1.44	0.25	7.97	2.26	2.26	1
2.21	1.44	0.25	7.97	2.26	2.26	1
2.20	1.43	0.25	7.97	2.26	2.26	1
2.19	1.43	0.24	7.97	2.26	2.26	1

2.17	1.42	0.24	7.97	2.26	2.26	1
2.16	1.42	0.24	7.97	2.26	2.26	1
2.15	1.41	0.24	7.97	2.26	2.26	1
2.14	1.41	0.24	7.97	2.26	2.26	1
2.12	1.40	0.24	7.97	2.26	2.26	1
2.11	1.40	0.24	7.97	2.26	2.26	1
2.10	1.39	0.23	7.97	2.26	2.26	1
2.09	1.39	0.23	7.97	2.26	2.26	1
2.07	1.39	0.23	7.97	2.26	2.26	1
2.06	1.38	0.23	7.97	2.26	2.26	1
2.05	1.38	0.23	7.97	2.26	2.26	1
2.04	1.37	0.23	7.97	2.26	2.26	1
2.02	1.37	0.23	7.97	2.26	2.26	1
2.01	1.36	0.22	7.97	2.26	2.26	1
2.00	1.36	0.22	7.97	5.92	2.26	1
2.00	1.36	0.22	7.97	5.92	2.26	1
1.99	1.35	0.22	7.97	2.26	2.26	1
1.97	1.35	0.22	7.97	2.26	2.26	1
1.96	1.34	0.22	7.97	2.26	2.26	1
1.95	1.34	0.22	7.97	2.26	2.26	1
1.94	1.33	0.22	7.97	2.26	2.26	1
1.92	1.33	0.21	7.97	2.26	2.26	1
1.91	1.32	0.21	7.97	2.26	2.26	1
1.90	1.32	0.21	7.97	2.26	2.26	1
1.89	1.31	0.21	7.97	2.26	2.26	1
1.87	1.31	0.21	7.97	2.26	2.26	1
1.86	1.30	0.21	7.97	2.26	2.26	1
1.85	1.30	0.21	7.97	2.26	2.26	1
1.84	1.30	0.20	7.97	2.26	2.26	1
1.82	1.29	0.20	7.97	2.26	2.26	1
1.81	1.29	0.20	7.97	2.26	2.26	1
1.80	1.28	0.20	7.97	2.26	2.26	1
1.79	1.28	0.20	7.97	2.26	2.26	1
1.77	1.27	0.20	7.97	2.26	2.26	1
1.76	1.27	0.20	7.97	2.26	2.26	1
1.75	1.26	0.20	7.97	2.26	2.26	1
1.74	1.26	0.19	7.97	2.26	2.26	1
1.72	1.26	0.19	7.97	2.26	2.26	1
1.71	1.25	0.19	7.97	2.26	2.26	1
1.70	1.25	0.19	7.97	2.26	2.26	1
1.69	1.24	0.19	7.97	2.26	2.26	1
1.67	1.24	0.19	7.97	2.26	2.26	1
1.66	1.23	0.19	7.97	2.26	2.26	1
1.65	1.23	0.18	7.97	2.26	2.26	1
1.64	1.22	0.18	7.97	2.26	2.26	1
1.62	1.22	0.18	7.97	5.62	5.62	1
1.61	1.21	0.18	7.97	5.62	5.61	1
1.60	1.20	0.18	7.97	5.62	5.60	1
1.59	1.19	0.18	7.97	5.63	5.59	1
1.57	1.18	0.18	7.97	5.63	5.59	1
1.56	1.17	0.17	7.97	5.63	5.58	1
1.55	1.16	0.17	7.97	5.63	5.57	1
1.54	1.15	0.17	7.97	5.63	5.56	1
1.52	1.14	0.17	7.97	5.64	5.55	1

1.51	1.13	0.17	7.97	5.64	5.54	1
1.50	1.12	0.17	7.97	5.64	5.53	1
1.50	1.12	0.17	7.97	5.64	5.53	1
1.49	1.12	0.17	7.97	5.64	5.52	1
1.47	1.11	0.16	7.97	5.64	5.51	1
1.46	1.10	0.16	7.97	5.65	5.50	1
1.45	1.09	0.16	7.97	5.65	5.49	1
1.44	1.08	0.16	7.97	5.65	5.48	1
1.42	1.07	0.16	7.97	5.65	5.48	1
1.41	1.06	0.16	7.97	5.65	5.47	1
1.40	1.05	0.16	7.97	5.66	5.46	1
1.39	1.04	0.15	7.97	5.66	5.45	1
1.37	1.03	0.15	7.97	5.66	5.45	1
1.36	1.02	0.15	7.97	5.66	5.44	1
1.35	1.01	0.15	7.97	5.66	5.44	1
1.34	1.00	0.15	7.97	5.67	5.44	1
1.32	0.99	0.15	7.97	5.67	5.43	1
1.31	0.99	0.15	7.97	5.67	5.43	1
1.30	0.98	0.14	7.97	5.67	5.42	1
1.29	0.97	0.14	7.97	5.67	5.42	1
1.27	0.96	0.14	7.97	5.67	5.41	1
1.26	0.95	0.14	7.97	5.68	5.41	1
1.25	0.94	0.14	7.97	5.68	5.40	1
1.24	0.93	0.14	7.97	5.68	5.40	1
1.22	0.92	0.14	7.97	5.68	5.39	1
1.21	0.91	0.14	7.97	5.68	5.39	1
1.20	0.90	0.13	7.97	5.68	5.38	1
1.19	0.89	0.13	7.97	5.69	5.38	1
1.17	0.88	0.13	7.97	5.69	5.37	1
1.16	0.87	0.13	7.97	5.69	5.37	1
1.15	0.86	0.13	7.97	5.69	5.36	1
1.14	0.86	0.13	7.97	5.69	5.36	1
1.12	0.85	0.13	7.97	5.69	5.36	1
1.11	0.84	0.12	7.97	5.70	5.35	1
1.10	0.83	0.12	7.97	5.70	5.35	1
1.09	0.82	0.12	7.97	5.70	5.34	1
1.07	0.81	0.12	7.97	5.70	5.34	1
1.06	0.80	0.12	7.97	5.70	5.33	1
1.05	0.79	0.12	7.97	5.70	5.33	1
1.04	0.78	0.12	7.97	5.70	5.32	1
1.02	0.77	0.11	7.97	5.71	5.32	1
1.01	0.76	0.11	7.97	5.71	5.31	1
1.00	0.75	0.11	7.97	5.71	5.31	1
1.00	0.75	0.11	7.97	5.71	5.31	1
0.98	0.74	0.11	7.97	5.71	5.30	1
0.95	0.72	0.11	7.97	5.71	5.30	1
0.93	0.70	0.10	7.97	5.72	5.29	1
0.91	0.69	0.10	7.97	5.72	5.29	1
0.89	0.67	0.10	7.97	5.72	5.28	1
0.86	0.65	0.10	7.97	5.72	5.28	1
0.84	0.63	0.09	7.97	5.73	5.27	1
0.82	0.62	0.09	7.97	5.73	5.27	1
0.80	0.60	0.09	7.97	5.73	5.26	1
0.77	0.58	0.09	7.97	5.73	5.26	1

0.75	0.57	0.08	7.97	5.73	5.25	1
0.73	0.55	0.08	7.97	5.74	5.25	1
0.71	0.53	0.08	7.97	5.74	5.24	1
0.68	0.52	0.08	7.97	5.74	5.24	1
0.66	0.50	0.07	7.97	5.74	5.23	1
0.64	0.48	0.07	7.97	5.75	5.23	1
0.62	0.47	0.07	7.97	5.75	5.22	1
0.59	0.45	0.07	7.97	5.75	5.22	1
0.57	0.43	0.06	7.97	5.75	5.21	1
0.55	0.41	0.06	7.97	5.75	5.21	1
0.53	0.40	0.06	7.97	5.75	5.20	1
0.51	0.38	0.06	7.97	5.76	5.20	1
0.48	0.36	0.05	7.97	5.76	5.19	1
0.46	0.35	0.05	7.97	5.76	5.19	1
0.44	0.33	0.05	7.97	5.76	5.18	1
0.42	0.31	0.05	7.97	5.76	5.18	1
0.39	0.30	0.04	7.97	5.76	5.18	1
0.37	0.28	0.04	7.97	5.77	5.17	1
0.35	0.26	0.04	7.97	5.77	5.17	1
0.33	0.25	0.04	7.97	5.77	5.17	1
0.30	0.23	0.03	7.97	5.77	5.16	1
0.28	0.21	0.03	7.97	5.77	5.15	1
0.26	0.19	0.03	7.97	5.77	5.14	1
0.23	0.18	0.03	7.97	5.78	5.13	1
0.21	0.16	0.02	7.97	5.78	5.12	1
0.19	0.14	0.02	7.97	5.78	5.12	1
0.17	0.13	0.02	7.97	5.78	5.11	1
0.14	0.11	0.02	7.97	5.78	5.10	1
0.12	0.09	0.01	7.97	5.78	5.10	1
0.10	0.08	0.01	7.97	5.78	5.09	1
0.10	0.08	0.01	7.97	5.78	5.08	1
0.08	0.06	0.01	7.97	5.77	5.08	1
0.06	0.05	0.01	7.97	5.76	5.07	1
0.04	0.03	0.00	7.97	5.74	5.07	1
0.02	0.01	0.00	7.97	5.73	5.06	1
0.00	0.00	0.00	7.97	5.72	5.05	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
1.54	0.00	0.00	0.00	0.00	0.00	1
1.54	0.30	0.30	0.00	0.00	0.00	1
1.53	0.61	0.61	0.00	0.00	0.00	1
1.53	0.91	0.91	0.00	0.00	0.00	1
1.52	1.21	1.21	0.00	0.00	0.00	1
1.52	1.51	1.51	0.00	0.00	0.00	1
1.51	1.82	1.82	0.00	0.00	0.00	1
1.51	2.12	2.12	0.00	0.00	0.00	1
1.50	2.42	2.42	0.00	0.00	0.00	1
1.50	2.72	2.72	0.00	0.00	0.00	1
1.49	3.03	3.03	0.00	0.00	0.00	1
1.49	3.33	3.33	0.00	0.00	0.00	1
1.49	3.63	3.63	0.00	0.00	0.00	1

1.48	3.93	3.93	0.00	0.00	0.00	1
1.48	4.24	4.24	0.00	0.00	0.00	1
1.47	4.54	4.54	0.00	0.00	0.00	1
1.47	4.84	4.84	0.00	0.00	0.00	1
1.46	5.14	5.14	0.00	0.00	0.00	1
1.46	5.45	5.45	0.00	0.00	0.00	1
1.45	5.75	5.75	0.00	0.00	0.00	1
1.45	6.05	6.05	0.00	0.00	0.00	1
1.44	6.35	6.35	0.00	0.00	0.00	1
1.44	6.66	6.66	0.00	0.00	0.00	1
1.44	6.96	6.96	0.00	0.00	0.00	1
1.43	7.26	7.26	0.00	0.00	0.00	1
1.43	7.56	7.56	0.00	0.00	0.00	1
1.42	7.87	7.87	0.00	0.00	0.00	1
1.42	8.17	8.17	0.00	0.00	0.00	1
1.41	8.47	8.47	0.00	0.00	0.00	1
1.41	8.77	8.77	0.00	0.00	0.00	1
1.40	9.08	9.08	0.00	0.00	0.00	1
1.40	9.38	9.38	0.00	0.00	0.00	1
1.39	9.68	9.68	0.00	0.00	0.00	1
1.39	9.98	9.98	0.00	0.00	0.00	1
1.39	10.29	10.29	0.00	0.00	0.00	1
1.38	10.59	10.59	0.00	0.00	0.00	1
1.38	10.89	10.89	0.00	0.00	0.00	1
1.37	11.19	11.19	0.00	0.00	0.00	1
1.37	11.50	11.50	0.00	0.00	0.00	1
1.36	11.80	11.80	0.00	0.00	0.00	1
1.36	12.10	12.10	0.00	0.00	0.00	1
1.36	12.40	12.40	0.00	0.00	0.00	1
1.35	12.77	12.77	0.00	0.00	0.00	1
1.35	13.14	13.14	0.00	0.00	0.00	1
1.34	13.44	13.44	0.00	0.00	0.00	1
1.34	13.74	13.74	0.00	0.00	0.00	1
1.33	14.04	14.04	0.00	0.00	0.00	1
1.33	14.35	14.35	0.00	0.00	0.00	1
1.32	14.65	14.65	0.00	0.00	0.00	1
1.32	14.95	14.95	0.00	0.00	0.00	1
1.31	15.25	15.25	0.00	0.00	0.00	1
1.31	15.56	15.56	0.00	0.00	0.00	1
1.30	15.86	15.86	0.00	0.00	0.00	1
1.30	16.16	16.16	0.00	0.00	0.00	1
1.30	16.46	16.46	0.00	0.00	0.00	1
1.29	16.77	16.77	0.00	0.00	0.00	1
1.29	17.07	17.07	0.00	0.00	0.00	1
1.28	17.37	17.37	0.00	0.00	0.00	1
1.28	17.67	17.67	0.00	0.00	0.00	1
1.27	17.98	17.98	0.00	0.00	0.00	1
1.27	18.28	18.28	0.00	0.00	0.00	1
1.26	18.58	18.58	0.00	0.00	0.00	1
1.26	18.88	18.88	0.00	0.00	0.00	1
1.26	19.19	19.19	0.00	0.00	0.00	1
1.25	19.49	19.49	0.00	0.00	0.00	1
1.25	19.79	19.79	0.00	0.00	0.00	1
1.24	20.09	20.09	0.00	0.00	0.00	1

1.24	20.40	20.40	0.00	0.00	0.00	1
1.23	20.70	20.70	0.00	0.00	0.00	1
1.23	21.00	21.00	0.00	0.00	0.00	1
1.22	21.31	21.31	0.00	0.00	0.00	1
1.22	35.57	12.28	30.69	19.09	13.87	1
1.21	36.38	17.21	31.54	19.75	9.08	1
1.20	37.19	17.18	32.39	20.42	9.26	1
1.19	38.01	17.14	33.23	21.09	9.45	1
1.18	38.82	17.10	34.07	21.75	9.63	1
1.17	39.63	17.07	34.92	22.42	9.81	1
1.16	40.45	17.03	35.75	23.09	9.99	1
1.15	41.26	16.99	36.59	23.76	10.18	1
1.14	42.08	16.96	37.42	24.43	10.36	1
1.13	42.90	16.92	38.26	25.10	10.54	1
1.12	43.71	16.89	39.09	25.77	10.72	1
1.12	43.71	4.63	39.09	25.77	10.72	1
1.12	44.53	16.85	39.92	26.44	10.90	1
1.11	45.35	16.82	40.74	27.11	11.08	1
1.10	46.16	16.78	41.57	27.79	11.26	1
1.09	46.98	16.75	42.39	28.46	11.44	1
1.08	47.80	16.71	43.21	29.13	11.62	1
1.07	48.62	16.68	44.03	29.80	11.80	1
1.06	49.43	16.65	44.85	30.47	11.98	1
1.05	50.25	16.61	45.67	31.15	12.16	1
1.04	51.07	16.58	46.48	31.82	12.34	1
1.03	51.89	16.55	47.29	32.49	12.51	1
1.02	52.70	16.52	48.10	33.16	12.69	1
1.01	53.52	16.49	48.91	33.83	12.87	1
1.00	54.34	16.45	49.72	34.50	13.05	1
0.99	55.16	16.42	50.52	35.17	13.22	1
0.99	55.97	16.39	51.33	35.84	13.40	1
0.98	56.79	16.36	52.13	36.51	13.58	1
0.97	57.60	16.33	52.93	37.18	13.75	1
0.96	58.42	16.30	53.73	37.85	13.93	1
0.95	59.23	16.27	54.53	38.52	14.10	1
0.94	60.05	16.24	55.32	39.19	14.28	1
0.93	60.86	16.21	56.12	39.86	14.46	1
0.92	61.68	16.18	56.91	40.53	14.63	1
0.91	62.49	16.16	57.70	41.20	14.80	1
0.90	63.30	16.13	58.49	41.86	14.98	1
0.89	64.12	16.10	59.28	42.53	15.15	1
0.88	64.93	16.07	60.07	43.20	15.33	1
0.87	65.74	16.04	60.86	43.86	15.50	1
0.86	66.55	16.02	61.64	44.53	15.67	1
0.86	67.36	15.99	62.42	45.19	15.85	1
0.85	68.17	15.96	63.21	45.85	16.02	1
0.84	68.98	15.94	63.99	46.52	16.19	1
0.83	69.79	15.91	64.74	47.18	16.36	1
0.82	70.59	15.88	65.49	47.84	16.54	1
0.81	71.40	15.86	66.23	48.50	16.71	1
0.80	72.21	15.83	66.97	49.16	16.88	1
0.79	73.01	15.81	67.71	49.82	17.05	1
0.78	73.82	15.78	68.45	50.48	17.22	1
0.77	74.62	15.76	69.18	51.14	17.39	1

0.76	75.43	15.73	69.92	51.80	17.56	1
0.75	76.23	15.71	70.65	52.46	17.73	1
0.75	76.23	5.58	70.65	52.46	17.73	1
0.74	77.67	15.66	71.97	53.64	18.04	1
0.72	79.11	15.62	73.28	54.82	18.34	1
0.70	80.55	15.58	74.59	55.99	18.65	1
0.69	81.99	15.54	75.90	57.17	18.95	1
0.67	83.42	15.49	77.20	58.34	19.26	1
0.65	84.86	15.45	78.50	59.51	19.56	1
0.63	86.29	15.41	79.80	60.67	19.86	1
0.62	87.71	15.37	81.10	61.84	20.16	1
0.60	89.14	15.34	82.39	63.00	20.46	1
0.58	90.56	15.30	83.68	64.16	20.76	1
0.57	91.98	15.26	84.96	65.32	21.06	1
0.55	93.40	15.23	86.25	66.47	21.36	1
0.53	94.81	15.19	87.53	67.63	21.66	1
0.52	96.22	15.15	88.80	68.78	21.96	1
0.50	97.63	15.12	90.08	69.92	22.26	1
0.48	99.04	15.09	91.35	71.07	22.55	1
0.47	100.45	15.05	92.62	72.21	22.85	1
0.45	101.85	15.02	93.89	73.35	23.14	1
0.43	103.25	14.99	95.15	74.49	23.44	1
0.41	104.65	14.96	96.42	75.62	23.73	1
0.40	106.04	14.92	97.68	76.76	24.03	1
0.38	107.44	14.89	98.93	77.89	24.32	1
0.36	108.83	14.86	100.19	79.02	24.61	1
0.35	110.21	14.83	101.44	80.14	24.90	1
0.33	111.60	14.81	102.69	81.26	25.20	1
0.31	112.98	14.78	103.94	82.38	25.49	1
0.30	114.36	14.75	105.18	83.50	25.78	1
0.28	115.74	14.72	106.43	84.62	26.07	1
0.26	117.12	14.69	107.67	85.73	26.36	1
0.25	118.49	14.67	108.90	86.84	26.65	1
0.23	73.24	14.64	58.59	67.88	-9.29	1
0.21	74.37	14.62	59.76	68.94	-9.18	1
0.19	75.51	14.59	60.92	70.00	-9.08	1
0.18	76.64	14.57	62.08	71.06	-8.98	1
0.16	77.78	14.54	63.24	72.12	-8.88	1
0.14	78.92	14.52	64.40	73.18	-8.78	1
0.13	80.06	14.49	65.56	74.24	-8.68	1
0.11	81.19	14.47	66.72	75.30	-8.58	1
0.09	82.33	14.45	67.88	76.36	-8.48	1
0.08	83.47	14.43	69.04	77.43	-8.38	1
0.08	83.70	14.43	69.27	77.43	-8.15	1
0.06	84.74	14.67	70.07	78.37	-8.30	1
0.05	85.77	14.90	70.87	79.31	-8.44	1
0.03	86.80	15.13	71.67	80.25	-8.58	1
0.01	87.84	15.36	72.47	81.19	-8.71	1
0.00	88.86	15.59	73.28	82.12	0.00	1

Time = 2215. Degree of Consolidation = 45.0%

Total Settlement = 0.960

Settlement at End of Primary Consolidation = 1.041

Settlement caused by Primary Consolidation at time 2215. = 0.468

Settlement caused by Secondary Compression at time 2215. = 0.000

Settlement Due to Desiccation = 0.492

Surface Elevation = 0.61

*****Current Conditions in Dredged Fill*****

***** Coordinates *****

***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
2.50	1.54	0.28	7.97	2.26	2.26	1
2.49	1.54	0.28	7.97	2.26	2.26	1
2.48	1.53	0.28	7.97	2.26	2.26	1
2.46	1.53	0.27	7.97	2.26	2.26	1
2.45	1.52	0.27	7.97	2.26	2.26	1
2.44	1.52	0.27	7.97	2.26	2.26	1
2.43	1.51	0.27	7.97	2.26	2.26	1
2.41	1.51	0.27	7.97	2.26	2.26	1
2.40	1.50	0.27	7.97	2.26	2.26	1
2.39	1.50	0.27	7.97	2.26	2.26	1
2.38	1.49	0.26	7.97	2.26	2.26	1
2.36	1.49	0.26	7.97	2.26	2.26	1
2.35	1.49	0.26	7.97	2.26	2.26	1
2.34	1.48	0.26	7.97	2.26	2.26	1
2.33	1.48	0.26	7.97	2.26	2.26	1
2.31	1.47	0.26	7.97	2.26	2.26	1
2.30	1.47	0.26	7.97	2.26	2.26	1
2.29	1.46	0.26	7.97	2.26	2.26	1
2.27	1.46	0.25	7.97	2.26	2.26	1
2.26	1.45	0.25	7.97	2.26	2.26	1
2.25	1.45	0.25	7.97	2.26	2.26	1
2.24	1.44	0.25	7.97	2.26	2.26	1
2.22	1.44	0.25	7.97	2.26	2.26	1
2.21	1.44	0.25	7.97	2.26	2.26	1
2.20	1.43	0.25	7.97	2.26	2.26	1
2.19	1.43	0.24	7.97	2.26	2.26	1
2.17	1.42	0.24	7.97	2.26	2.26	1
2.16	1.42	0.24	7.97	2.26	2.26	1
2.15	1.41	0.24	7.97	2.26	2.26	1
2.14	1.41	0.24	7.97	2.26	2.26	1
2.12	1.40	0.24	7.97	2.26	2.26	1
2.11	1.40	0.24	7.97	2.26	2.26	1
2.10	1.39	0.23	7.97	2.26	2.26	1
2.09	1.39	0.23	7.97	2.26	2.26	1

2.07	1.39	0.23	7.97	2.26	2.26	1
2.06	1.38	0.23	7.97	2.26	2.26	1
2.05	1.38	0.23	7.97	2.26	2.26	1
2.04	1.37	0.23	7.97	2.26	2.26	1
2.02	1.37	0.23	7.97	2.26	2.26	1
2.01	1.36	0.22	7.97	2.26	2.26	1
2.00	1.36	0.22	7.97	5.92	2.26	1
2.00	1.36	0.22	7.97	5.92	2.26	1
1.99	1.35	0.22	7.97	2.26	2.26	1
1.97	1.35	0.22	7.97	2.26	2.26	1
1.96	1.34	0.22	7.97	2.26	2.26	1
1.95	1.34	0.22	7.97	2.26	2.26	1
1.94	1.33	0.22	7.97	2.26	2.26	1
1.92	1.33	0.21	7.97	2.26	2.26	1
1.91	1.32	0.21	7.97	2.26	2.26	1
1.90	1.32	0.21	7.97	2.26	2.26	1
1.89	1.31	0.21	7.97	2.26	2.26	1
1.87	1.31	0.21	7.97	2.26	2.26	1
1.86	1.30	0.21	7.97	2.26	2.26	1
1.85	1.30	0.21	7.97	2.26	2.26	1
1.84	1.30	0.20	7.97	2.26	2.26	1
1.82	1.29	0.20	7.97	2.26	2.26	1
1.81	1.29	0.20	7.97	2.26	2.26	1
1.80	1.28	0.20	7.97	2.26	2.26	1
1.79	1.28	0.20	7.97	2.26	2.26	1
1.77	1.27	0.20	7.97	2.26	2.26	1
1.76	1.27	0.20	7.97	2.26	2.26	1
1.75	1.26	0.20	7.97	2.26	2.26	1
1.74	1.26	0.19	7.97	2.26	2.26	1
1.72	1.26	0.19	7.97	2.26	2.26	1
1.71	1.25	0.19	7.97	2.26	2.26	1
1.70	1.25	0.19	7.97	2.26	2.26	1
1.69	1.24	0.19	7.97	2.26	2.26	1
1.67	1.24	0.19	7.97	2.26	2.26	1
1.66	1.23	0.19	7.97	2.26	2.26	1
1.65	1.23	0.18	7.97	2.26	2.26	1
1.64	1.22	0.18	7.97	2.26	2.26	1
1.62	1.22	0.18	7.97	5.62	5.62	1
1.61	1.21	0.18	7.97	5.62	5.61	1
1.60	1.20	0.18	7.97	5.62	5.60	1
1.59	1.19	0.18	7.97	5.63	5.59	1
1.57	1.18	0.18	7.97	5.63	5.59	1
1.56	1.17	0.17	7.97	5.63	5.58	1
1.55	1.16	0.17	7.97	5.63	5.57	1
1.54	1.15	0.17	7.97	5.63	5.56	1
1.52	1.14	0.17	7.97	5.64	5.55	1
1.51	1.13	0.17	7.97	5.64	5.54	1
1.50	1.12	0.17	7.97	5.64	5.53	1
1.50	1.12	0.17	7.97	5.64	5.53	1
1.49	1.12	0.17	7.97	5.64	5.52	1
1.47	1.11	0.16	7.97	5.64	5.51	1
1.46	1.10	0.16	7.97	5.65	5.50	1
1.45	1.09	0.16	7.97	5.65	5.49	1
1.44	1.08	0.16	7.97	5.65	5.48	1

1.42	1.07	0.16	7.97	5.65	5.48	1
1.41	1.06	0.16	7.97	5.65	5.47	1
1.40	1.05	0.16	7.97	5.66	5.46	1
1.39	1.04	0.15	7.97	5.66	5.45	1
1.37	1.03	0.15	7.97	5.66	5.45	1
1.36	1.02	0.15	7.97	5.66	5.44	1
1.35	1.01	0.15	7.97	5.66	5.44	1
1.34	1.00	0.15	7.97	5.67	5.44	1
1.32	0.99	0.15	7.97	5.67	5.43	1
1.31	0.99	0.15	7.97	5.67	5.43	1
1.30	0.98	0.14	7.97	5.67	5.42	1
1.29	0.97	0.14	7.97	5.67	5.42	1
1.27	0.96	0.14	7.97	5.67	5.41	1
1.26	0.95	0.14	7.97	5.68	5.41	1
1.25	0.94	0.14	7.97	5.68	5.40	1
1.24	0.93	0.14	7.97	5.68	5.40	1
1.22	0.92	0.14	7.97	5.68	5.39	1
1.21	0.91	0.14	7.97	5.68	5.39	1
1.20	0.90	0.13	7.97	5.68	5.38	1
1.19	0.89	0.13	7.97	5.69	5.38	1
1.17	0.88	0.13	7.97	5.69	5.37	1
1.16	0.87	0.13	7.97	5.69	5.37	1
1.15	0.86	0.13	7.97	5.69	5.36	1
1.14	0.86	0.13	7.97	5.69	5.36	1
1.12	0.85	0.13	7.97	5.69	5.36	1
1.11	0.84	0.12	7.97	5.70	5.35	1
1.10	0.83	0.12	7.97	5.70	5.35	1
1.09	0.82	0.12	7.97	5.70	5.34	1
1.07	0.81	0.12	7.97	5.70	5.34	1
1.06	0.80	0.12	7.97	5.70	5.33	1
1.05	0.79	0.12	7.97	5.70	5.33	1
1.04	0.78	0.12	7.97	5.70	5.32	1
1.02	0.77	0.11	7.97	5.71	5.32	1
1.01	0.76	0.11	7.97	5.71	5.31	1
1.00	0.75	0.11	7.97	5.71	5.31	1
1.00	0.75	0.11	7.97	5.71	5.31	1
0.98	0.74	0.11	7.97	5.71	5.30	1
0.95	0.72	0.11	7.97	5.71	5.30	1
0.93	0.70	0.10	7.97	5.72	5.29	1
0.91	0.69	0.10	7.97	5.72	5.29	1
0.89	0.67	0.10	7.97	5.72	5.28	1
0.86	0.65	0.10	7.97	5.72	5.28	1
0.84	0.63	0.09	7.97	5.73	5.27	1
0.82	0.62	0.09	7.97	5.73	5.27	1
0.80	0.60	0.09	7.97	5.73	5.26	1
0.77	0.58	0.09	7.97	5.73	5.26	1
0.75	0.57	0.08	7.97	5.73	5.25	1
0.73	0.55	0.08	7.97	5.74	5.25	1
0.71	0.53	0.08	7.97	5.74	5.24	1
0.68	0.52	0.08	7.97	5.74	5.24	1
0.66	0.50	0.07	7.97	5.74	5.23	1
0.64	0.48	0.07	7.97	5.75	5.23	1
0.62	0.47	0.07	7.97	5.75	5.22	1
0.59	0.45	0.07	7.97	5.75	5.22	1

0.57	0.43	0.06	7.97	5.75	5.21	1
0.55	0.41	0.06	7.97	5.75	5.21	1
0.53	0.40	0.06	7.97	5.75	5.20	1
0.51	0.38	0.06	7.97	5.76	5.20	1
0.48	0.36	0.05	7.97	5.76	5.19	1
0.46	0.35	0.05	7.97	5.76	5.19	1
0.44	0.33	0.05	7.97	5.76	5.18	1
0.42	0.31	0.05	7.97	5.76	5.18	1
0.39	0.30	0.04	7.97	5.76	5.18	1
0.37	0.28	0.04	7.97	5.77	5.17	1
0.35	0.26	0.04	7.97	5.77	5.17	1
0.33	0.25	0.04	7.97	5.77	5.17	1
0.30	0.23	0.03	7.97	5.77	5.16	1
0.28	0.21	0.03	7.97	5.77	5.15	1
0.26	0.19	0.03	7.97	5.77	5.14	1
0.23	0.18	0.03	7.97	5.78	5.13	1
0.21	0.16	0.02	7.97	5.78	5.12	1
0.19	0.14	0.02	7.97	5.78	5.12	1
0.17	0.13	0.02	7.97	5.78	5.11	1
0.14	0.11	0.02	7.97	5.78	5.10	1
0.12	0.09	0.01	7.97	5.78	5.10	1
0.10	0.08	0.01	7.97	5.78	5.09	1
0.10	0.08	0.01	7.97	5.78	5.08	1
0.08	0.06	0.01	7.97	5.77	5.08	1
0.06	0.05	0.01	7.97	5.76	5.07	1
0.04	0.03	0.00	7.97	5.74	5.07	1
0.02	0.01	0.00	7.97	5.73	5.06	1
0.00	0.00	0.00	7.97	5.72	5.05	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
1.54	0.00	0.00	0.00	0.00	0.00	1
1.54	0.30	0.30	0.00	0.00	0.00	1
1.53	0.61	0.61	0.00	0.00	0.00	1
1.53	0.91	0.91	0.00	0.00	0.00	1
1.52	1.21	1.21	0.00	0.00	0.00	1
1.52	1.51	1.51	0.00	0.00	0.00	1
1.51	1.82	1.82	0.00	0.00	0.00	1
1.51	2.12	2.12	0.00	0.00	0.00	1
1.50	2.42	2.42	0.00	0.00	0.00	1
1.50	2.72	2.72	0.00	0.00	0.00	1
1.49	3.03	3.03	0.00	0.00	0.00	1
1.49	3.33	3.33	0.00	0.00	0.00	1
1.49	3.63	3.63	0.00	0.00	0.00	1
1.48	3.93	3.93	0.00	0.00	0.00	1
1.48	4.24	4.24	0.00	0.00	0.00	1
1.47	4.54	4.54	0.00	0.00	0.00	1
1.47	4.84	4.84	0.00	0.00	0.00	1
1.46	5.14	5.14	0.00	0.00	0.00	1
1.46	5.45	5.45	0.00	0.00	0.00	1
1.45	5.75	5.75	0.00	0.00	0.00	1
1.45	6.05	6.05	0.00	0.00	0.00	1

1.44	6.35	6.35	0.00	0.00	0.00	1
1.44	6.66	6.66	0.00	0.00	0.00	1
1.44	6.96	6.96	0.00	0.00	0.00	1
1.43	7.26	7.26	0.00	0.00	0.00	1
1.43	7.56	7.56	0.00	0.00	0.00	1
1.42	7.87	7.87	0.00	0.00	0.00	1
1.42	8.17	8.17	0.00	0.00	0.00	1
1.41	8.47	8.47	0.00	0.00	0.00	1
1.41	8.77	8.77	0.00	0.00	0.00	1
1.40	9.08	9.08	0.00	0.00	0.00	1
1.40	9.38	9.38	0.00	0.00	0.00	1
1.39	9.68	9.68	0.00	0.00	0.00	1
1.39	9.98	9.98	0.00	0.00	0.00	1
1.39	10.29	10.29	0.00	0.00	0.00	1
1.38	10.59	10.59	0.00	0.00	0.00	1
1.38	10.89	10.89	0.00	0.00	0.00	1
1.37	11.19	11.19	0.00	0.00	0.00	1
1.37	11.50	11.50	0.00	0.00	0.00	1
1.36	11.80	11.80	0.00	0.00	0.00	1
1.36	12.10	12.10	0.00	0.00	0.00	1
1.36	12.40	12.40	0.00	0.00	0.00	1
1.35	12.77	12.77	0.00	0.00	0.00	1
1.35	13.14	13.14	0.00	0.00	0.00	1
1.34	13.44	13.44	0.00	0.00	0.00	1
1.34	13.74	13.74	0.00	0.00	0.00	1
1.33	14.04	14.04	0.00	0.00	0.00	1
1.33	14.35	14.35	0.00	0.00	0.00	1
1.32	14.65	14.65	0.00	0.00	0.00	1
1.32	14.95	14.95	0.00	0.00	0.00	1
1.31	15.25	15.25	0.00	0.00	0.00	1
1.31	15.56	15.56	0.00	0.00	0.00	1
1.30	15.86	15.86	0.00	0.00	0.00	1
1.30	16.16	16.16	0.00	0.00	0.00	1
1.30	16.46	16.46	0.00	0.00	0.00	1
1.29	16.77	16.77	0.00	0.00	0.00	1
1.29	17.07	17.07	0.00	0.00	0.00	1
1.28	17.37	17.37	0.00	0.00	0.00	1
1.28	17.67	17.67	0.00	0.00	0.00	1
1.27	17.98	17.98	0.00	0.00	0.00	1
1.27	18.28	18.28	0.00	0.00	0.00	1
1.26	18.58	18.58	0.00	0.00	0.00	1
1.26	18.88	18.88	0.00	0.00	0.00	1
1.26	19.19	19.19	0.00	0.00	0.00	1
1.25	19.49	19.49	0.00	0.00	0.00	1
1.25	19.79	19.79	0.00	0.00	0.00	1
1.24	20.09	20.09	0.00	0.00	0.00	1
1.24	20.40	20.40	0.00	0.00	0.00	1
1.23	20.70	20.70	0.00	0.00	0.00	1
1.23	21.00	21.00	0.00	0.00	0.00	1
1.22	21.31	21.31	0.00	0.00	0.00	1
1.22	35.57	12.28	30.69	19.09	13.87	1
1.21	36.38	17.21	31.54	19.75	9.08	1
1.20	37.19	17.18	32.39	20.42	9.26	1
1.19	38.01	17.14	33.23	21.09	9.45	1

1.18	38.82	17.10	34.07	21.75	9.63	1
1.17	39.63	17.07	34.92	22.42	9.81	1
1.16	40.45	17.03	35.75	23.09	9.99	1
1.15	41.26	16.99	36.59	23.76	10.18	1
1.14	42.08	16.96	37.42	24.43	10.36	1
1.13	42.90	16.92	38.26	25.10	10.54	1
1.12	43.71	16.89	39.09	25.77	10.72	1
1.12	43.71	4.63	39.09	25.77	10.72	1
1.12	44.53	16.85	39.92	26.44	10.90	1
1.11	45.35	16.82	40.74	27.11	11.08	1
1.10	46.16	16.78	41.57	27.79	11.26	1
1.09	46.98	16.75	42.39	28.46	11.44	1
1.08	47.80	16.71	43.21	29.13	11.62	1
1.07	48.62	16.68	44.03	29.80	11.80	1
1.06	49.43	16.65	44.85	30.47	11.98	1
1.05	50.25	16.61	45.67	31.15	12.16	1
1.04	51.07	16.58	46.48	31.82	12.34	1
1.03	51.89	16.55	47.29	32.49	12.51	1
1.02	52.70	16.52	48.10	33.16	12.69	1
1.01	53.52	16.49	48.91	33.83	12.87	1
1.00	54.34	16.45	49.72	34.50	13.05	1
0.99	55.16	16.42	50.52	35.17	13.22	1
0.99	55.97	16.39	51.33	35.84	13.40	1
0.98	56.79	16.36	52.13	36.51	13.58	1
0.97	57.60	16.33	52.93	37.18	13.75	1
0.96	58.42	16.30	53.73	37.85	13.93	1
0.95	59.23	16.27	54.53	38.52	14.10	1
0.94	60.05	16.24	55.32	39.19	14.28	1
0.93	60.86	16.21	56.12	39.86	14.45	1
0.92	61.68	16.18	56.91	40.53	14.63	1
0.91	62.49	16.16	57.70	41.20	14.80	1
0.90	63.30	16.13	58.49	41.86	14.98	1
0.89	64.12	16.10	59.28	42.53	15.15	1
0.88	64.93	16.07	60.07	43.20	15.33	1
0.87	65.74	16.04	60.86	43.86	15.50	1
0.86	66.55	16.02	61.64	44.53	15.67	1
0.86	67.36	15.99	62.42	45.19	15.85	1
0.85	68.17	15.96	63.21	45.85	16.02	1
0.84	68.98	15.94	63.99	46.52	16.19	1
0.83	69.79	15.91	64.74	47.18	16.36	1
0.82	70.59	15.88	65.49	47.84	16.54	1
0.81	71.40	15.86	66.23	48.50	16.71	1
0.80	72.21	15.83	66.97	49.16	16.88	1
0.79	73.01	15.81	67.71	49.82	17.05	1
0.78	73.82	15.78	68.45	50.48	17.22	1
0.77	74.62	15.76	69.18	51.14	17.39	1
0.76	75.43	15.73	69.92	51.80	17.56	1
0.75	76.23	15.71	70.65	52.46	17.73	1
0.75	76.23	5.58	70.65	52.46	17.73	1
0.74	77.67	15.66	71.97	53.64	18.04	1
0.72	79.11	15.62	73.28	54.82	18.34	1
0.70	80.55	15.58	74.59	55.99	18.65	1
0.69	81.99	15.54	75.90	57.17	18.95	1
0.67	83.42	15.49	77.20	58.34	19.26	1

0.65	84.86	15.45	78.50	59.51	19.56	1
0.63	86.29	15.41	79.80	60.67	19.86	1
0.62	87.71	15.37	81.10	61.84	20.16	1
0.60	89.14	15.34	82.39	63.00	20.46	1
0.58	90.56	15.30	83.68	64.16	20.76	1
0.57	91.98	15.26	84.96	65.32	21.06	1
0.55	93.40	15.23	86.25	66.47	21.36	1
0.53	94.81	15.19	87.53	67.63	21.66	1
0.52	96.22	15.15	88.80	68.78	21.96	1
0.50	97.63	15.12	90.08	69.92	22.26	1
0.48	99.04	15.09	91.35	71.07	22.55	1
0.47	100.45	15.05	92.62	72.21	22.85	1
0.45	101.85	15.02	93.89	73.35	23.14	1
0.43	103.25	14.99	95.15	74.49	23.44	1
0.41	104.65	14.96	96.42	75.62	23.73	1
0.40	106.04	14.92	97.68	76.76	24.03	1
0.38	107.44	14.89	98.93	77.89	24.32	1
0.36	108.83	14.86	100.19	79.02	24.61	1
0.35	110.21	14.83	101.44	80.14	24.90	1
0.33	111.60	14.81	102.69	81.26	25.20	1
0.31	112.98	14.78	103.94	82.38	25.49	1
0.30	114.36	14.75	105.18	83.50	25.78	1
0.28	115.74	14.72	106.43	84.62	26.07	1
0.26	117.12	14.69	107.67	85.73	26.36	1
0.25	72.33	14.67	57.66	66.82	-9.15	1
0.23	73.47	14.64	58.83	67.88	-9.05	1
0.21	74.60	14.62	59.99	68.94	-8.95	1
0.19	75.74	14.59	61.15	70.00	-8.85	1
0.18	76.88	14.57	62.31	71.06	-8.75	1
0.16	78.01	14.54	63.47	72.12	-8.65	1
0.14	79.15	14.52	64.63	73.18	-8.55	1
0.13	80.29	14.49	65.79	74.24	-8.45	1
0.11	81.43	14.47	66.95	75.30	-8.35	1
0.09	82.56	14.45	68.11	76.36	-8.25	1
0.08	83.70	14.43	69.27	77.43	-8.15	1
0.08	83.93	14.43	69.51	77.43	-7.92	1
0.06	84.97	14.67	70.30	78.37	-8.06	1
0.05	86.00	14.90	71.10	79.31	-8.21	1
0.03	87.04	15.13	71.90	80.25	-8.34	1
0.01	88.07	15.36	72.71	81.19	-8.48	1
0.00	89.10	15.59	73.51	82.12	0.00	1

Time = 3675. Degree of Consolidation = 45.0%

Total Settlement = 0.960

Settlement at End of Primary Consolidation = 1.041

Settlement caused by Primary Consolidation at time 3675. = 0.468

Settlement caused by Secondary Compression at time 3675. = 0.000

Settlement Due to Desiccation = 0.492

Surface Elevation = 0.61

*****Current Conditions in Dredged Fill*****

***** Coordinates *****

***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
2.50	1.54	0.28	7.97	2.26	2.26	1
2.49	1.54	0.28	7.97	2.26	2.26	1
2.48	1.53	0.28	7.97	2.26	2.26	1
2.46	1.53	0.27	7.97	2.26	2.26	1
2.45	1.52	0.27	7.97	2.26	2.26	1
2.44	1.52	0.27	7.97	2.26	2.26	1
2.43	1.51	0.27	7.97	2.26	2.26	1
2.41	1.51	0.27	7.97	2.26	2.26	1
2.40	1.50	0.27	7.97	2.26	2.26	1
2.39	1.50	0.27	7.97	2.26	2.26	1
2.38	1.49	0.26	7.97	2.26	2.26	1
2.36	1.49	0.26	7.97	2.26	2.26	1
2.35	1.49	0.26	7.97	2.26	2.26	1
2.34	1.48	0.26	7.97	2.26	2.26	1
2.33	1.48	0.26	7.97	2.26	2.26	1
2.31	1.47	0.26	7.97	2.26	2.26	1
2.30	1.47	0.26	7.97	2.26	2.26	1
2.29	1.46	0.26	7.97	2.26	2.26	1
2.27	1.46	0.25	7.97	2.26	2.26	1
2.26	1.45	0.25	7.97	2.26	2.26	1
2.25	1.45	0.25	7.97	2.26	2.26	1
2.24	1.44	0.25	7.97	2.26	2.26	1
2.22	1.44	0.25	7.97	2.26	2.26	1
2.21	1.44	0.25	7.97	2.26	2.26	1
2.20	1.43	0.25	7.97	2.26	2.26	1
2.19	1.43	0.24	7.97	2.26	2.26	1
2.17	1.42	0.24	7.97	2.26	2.26	1
2.16	1.42	0.24	7.97	2.26	2.26	1
2.15	1.41	0.24	7.97	2.26	2.26	1
2.14	1.41	0.24	7.97	2.26	2.26	1
2.12	1.40	0.24	7.97	2.26	2.26	1
2.11	1.40	0.24	7.97	2.26	2.26	1
2.10	1.39	0.23	7.97	2.26	2.26	1
2.09	1.39	0.23	7.97	2.26	2.26	1
2.07	1.39	0.23	7.97	2.26	2.26	1
2.06	1.38	0.23	7.97	2.26	2.26	1
2.05	1.38	0.23	7.97	2.26	2.26	1
2.04	1.37	0.23	7.97	2.26	2.26	1
2.02	1.37	0.23	7.97	2.26	2.26	1
2.01	1.36	0.22	7.97	2.26	2.26	1
2.00	1.36	0.22	7.97	5.92	2.26	1
2.00	1.36	0.22	7.97	5.92	2.26	1

1.99	1.35	0.22	7.97	2.26	2.26	1
1.97	1.35	0.22	7.97	2.26	2.26	1
1.96	1.34	0.22	7.97	2.26	2.26	1
1.95	1.34	0.22	7.97	2.26	2.26	1
1.94	1.33	0.22	7.97	2.26	2.26	1
1.92	1.33	0.21	7.97	2.26	2.26	1
1.91	1.32	0.21	7.97	2.26	2.26	1
1.90	1.32	0.21	7.97	2.26	2.26	1
1.89	1.31	0.21	7.97	2.26	2.26	1
1.87	1.31	0.21	7.97	2.26	2.26	1
1.86	1.30	0.21	7.97	2.26	2.26	1
1.85	1.30	0.21	7.97	2.26	2.26	1
1.84	1.30	0.20	7.97	2.26	2.26	1
1.82	1.29	0.20	7.97	2.26	2.26	1
1.81	1.29	0.20	7.97	2.26	2.26	1
1.80	1.28	0.20	7.97	2.26	2.26	1
1.79	1.28	0.20	7.97	2.26	2.26	1
1.77	1.27	0.20	7.97	2.26	2.26	1
1.76	1.27	0.20	7.97	2.26	2.26	1
1.75	1.26	0.20	7.97	2.26	2.26	1
1.74	1.26	0.19	7.97	2.26	2.26	1
1.72	1.26	0.19	7.97	2.26	2.26	1
1.71	1.25	0.19	7.97	2.26	2.26	1
1.70	1.25	0.19	7.97	2.26	2.26	1
1.69	1.24	0.19	7.97	2.26	2.26	1
1.67	1.24	0.19	7.97	2.26	2.26	1
1.66	1.23	0.19	7.97	2.26	2.26	1
1.65	1.23	0.18	7.97	2.26	2.26	1
1.64	1.22	0.18	7.97	2.26	2.26	1
1.62	1.22	0.18	7.97	5.62	5.62	1
1.61	1.21	0.18	7.97	5.62	5.61	1
1.60	1.20	0.18	7.97	5.62	5.60	1
1.59	1.19	0.18	7.97	5.63	5.59	1
1.57	1.18	0.18	7.97	5.63	5.59	1
1.56	1.17	0.17	7.97	5.63	5.58	1
1.55	1.16	0.17	7.97	5.63	5.57	1
1.54	1.15	0.17	7.97	5.63	5.56	1
1.52	1.14	0.17	7.97	5.64	5.55	1
1.51	1.13	0.17	7.97	5.64	5.54	1
1.50	1.12	0.17	7.97	5.64	5.53	1
1.50	1.12	0.17	7.97	5.64	5.53	1
1.49	1.12	0.17	7.97	5.64	5.52	1
1.47	1.11	0.16	7.97	5.64	5.51	1
1.46	1.10	0.16	7.97	5.65	5.50	1
1.45	1.09	0.16	7.97	5.65	5.49	1
1.44	1.08	0.16	7.97	5.65	5.48	1
1.42	1.07	0.16	7.97	5.65	5.48	1
1.41	1.06	0.16	7.97	5.65	5.47	1
1.40	1.05	0.16	7.97	5.66	5.46	1
1.39	1.04	0.15	7.97	5.66	5.45	1
1.37	1.03	0.15	7.97	5.66	5.45	1
1.36	1.02	0.15	7.97	5.66	5.44	1
1.35	1.01	0.15	7.97	5.66	5.44	1
1.34	1.00	0.15	7.97	5.67	5.44	1

1.32	0.99	0.15	7.97	5.67	5.43	1
1.31	0.99	0.15	7.97	5.67	5.43	1
1.30	0.98	0.14	7.97	5.67	5.42	1
1.29	0.97	0.14	7.97	5.67	5.42	1
1.27	0.96	0.14	7.97	5.67	5.41	1
1.26	0.95	0.14	7.97	5.68	5.41	1
1.25	0.94	0.14	7.97	5.68	5.40	1
1.24	0.93	0.14	7.97	5.68	5.40	1
1.22	0.92	0.14	7.97	5.68	5.39	1
1.21	0.91	0.14	7.97	5.68	5.39	1
1.20	0.90	0.13	7.97	5.68	5.38	1
1.19	0.89	0.13	7.97	5.69	5.38	1
1.17	0.88	0.13	7.97	5.69	5.37	1
1.16	0.87	0.13	7.97	5.69	5.37	1
1.15	0.86	0.13	7.97	5.69	5.36	1
1.14	0.86	0.13	7.97	5.69	5.36	1
1.12	0.85	0.13	7.97	5.69	5.36	1
1.11	0.84	0.12	7.97	5.70	5.35	1
1.10	0.83	0.12	7.97	5.70	5.35	1
1.09	0.82	0.12	7.97	5.70	5.34	1
1.07	0.81	0.12	7.97	5.70	5.34	1
1.06	0.80	0.12	7.97	5.70	5.33	1
1.05	0.79	0.12	7.97	5.70	5.33	1
1.04	0.78	0.12	7.97	5.70	5.32	1
1.02	0.77	0.11	7.97	5.71	5.32	1
1.01	0.76	0.11	7.97	5.71	5.31	1
1.00	0.75	0.11	7.97	5.71	5.31	1
1.00	0.75	0.11	7.97	5.71	5.31	1
0.98	0.74	0.11	7.97	5.71	5.30	1
0.95	0.72	0.11	7.97	5.71	5.30	1
0.93	0.70	0.10	7.97	5.72	5.29	1
0.91	0.69	0.10	7.97	5.72	5.29	1
0.89	0.67	0.10	7.97	5.72	5.28	1
0.86	0.65	0.10	7.97	5.72	5.28	1
0.84	0.63	0.09	7.97	5.73	5.27	1
0.82	0.62	0.09	7.97	5.73	5.27	1
0.80	0.60	0.09	7.97	5.73	5.26	1
0.77	0.58	0.09	7.97	5.73	5.26	1
0.75	0.57	0.08	7.97	5.73	5.25	1
0.73	0.55	0.08	7.97	5.74	5.25	1
0.71	0.53	0.08	7.97	5.74	5.24	1
0.68	0.52	0.08	7.97	5.74	5.24	1
0.66	0.50	0.07	7.97	5.74	5.23	1
0.64	0.48	0.07	7.97	5.75	5.23	1
0.62	0.47	0.07	7.97	5.75	5.22	1
0.59	0.45	0.07	7.97	5.75	5.22	1
0.57	0.43	0.06	7.97	5.75	5.21	1
0.55	0.41	0.06	7.97	5.75	5.21	1
0.53	0.40	0.06	7.97	5.75	5.20	1
0.51	0.38	0.06	7.97	5.76	5.20	1
0.48	0.36	0.05	7.97	5.76	5.19	1
0.46	0.35	0.05	7.97	5.76	5.19	1
0.44	0.33	0.05	7.97	5.76	5.18	1
0.42	0.31	0.05	7.97	5.76	5.18	1

0.39	0.30	0.04	7.97	5.76	5.18	1
0.37	0.28	0.04	7.97	5.77	5.17	1
0.35	0.26	0.04	7.97	5.77	5.17	1
0.33	0.25	0.04	7.97	5.77	5.17	1
0.30	0.23	0.03	7.97	5.77	5.16	1
0.28	0.21	0.03	7.97	5.77	5.15	1
0.26	0.19	0.03	7.97	5.77	5.14	1
0.23	0.18	0.03	7.97	5.78	5.13	1
0.21	0.16	0.02	7.97	5.78	5.12	1
0.19	0.14	0.02	7.97	5.78	5.12	1
0.17	0.13	0.02	7.97	5.78	5.11	1
0.14	0.11	0.02	7.97	5.78	5.10	1
0.12	0.09	0.01	7.97	5.78	5.10	1
0.10	0.08	0.01	7.97	5.78	5.09	1
0.10	0.08	0.01	7.97	5.78	5.08	1
0.08	0.06	0.01	7.97	5.77	5.08	1
0.06	0.05	0.01	7.97	5.76	5.07	1
0.04	0.03	0.00	7.97	5.74	5.07	1
0.02	0.01	0.00	7.97	5.73	5.06	1
0.00	0.00	0.00	7.97	5.72	5.05	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
1.54	0.00	0.00	0.00	0.00	0.00	1
1.54	0.30	0.30	0.00	0.00	0.00	1
1.53	0.61	0.61	0.00	0.00	0.00	1
1.53	0.91	0.91	0.00	0.00	0.00	1
1.52	1.21	1.21	0.00	0.00	0.00	1
1.52	1.51	1.51	0.00	0.00	0.00	1
1.51	1.82	1.82	0.00	0.00	0.00	1
1.51	2.12	2.12	0.00	0.00	0.00	1
1.50	2.42	2.42	0.00	0.00	0.00	1
1.50	2.72	2.72	0.00	0.00	0.00	1
1.49	3.03	3.03	0.00	0.00	0.00	1
1.49	3.33	3.33	0.00	0.00	0.00	1
1.49	3.63	3.63	0.00	0.00	0.00	1
1.48	3.93	3.93	0.00	0.00	0.00	1
1.48	4.24	4.24	0.00	0.00	0.00	1
1.47	4.54	4.54	0.00	0.00	0.00	1
1.47	4.84	4.84	0.00	0.00	0.00	1
1.46	5.14	5.14	0.00	0.00	0.00	1
1.46	5.45	5.45	0.00	0.00	0.00	1
1.45	5.75	5.75	0.00	0.00	0.00	1
1.45	6.05	6.05	0.00	0.00	0.00	1
1.44	6.35	6.35	0.00	0.00	0.00	1
1.44	6.66	6.66	0.00	0.00	0.00	1
1.44	6.96	6.96	0.00	0.00	0.00	1
1.43	7.26	7.26	0.00	0.00	0.00	1
1.43	7.56	7.56	0.00	0.00	0.00	1
1.42	7.87	7.87	0.00	0.00	0.00	1
1.42	8.17	8.17	0.00	0.00	0.00	1
1.41	8.47	8.47	0.00	0.00	0.00	1

1.41	8.77	8.77	0.00	0.00	0.00	1
1.40	9.08	9.08	0.00	0.00	0.00	1
1.40	9.38	9.38	0.00	0.00	0.00	1
1.39	9.68	9.68	0.00	0.00	0.00	1
1.39	9.98	9.98	0.00	0.00	0.00	1
1.39	10.29	10.29	0.00	0.00	0.00	1
1.38	10.59	10.59	0.00	0.00	0.00	1
1.38	10.89	10.89	0.00	0.00	0.00	1
1.37	11.19	11.19	0.00	0.00	0.00	1
1.37	11.50	11.50	0.00	0.00	0.00	1
1.36	11.80	11.80	0.00	0.00	0.00	1
1.36	12.10	12.10	0.00	0.00	0.00	1
1.36	12.40	12.40	0.00	0.00	0.00	1
1.35	12.77	12.77	0.00	0.00	0.00	1
1.35	13.14	13.14	0.00	0.00	0.00	1
1.34	13.44	13.44	0.00	0.00	0.00	1
1.34	13.74	13.74	0.00	0.00	0.00	1
1.33	14.04	14.04	0.00	0.00	0.00	1
1.33	14.35	14.35	0.00	0.00	0.00	1
1.32	14.65	14.65	0.00	0.00	0.00	1
1.32	14.95	14.95	0.00	0.00	0.00	1
1.31	15.25	15.25	0.00	0.00	0.00	1
1.31	15.56	15.56	0.00	0.00	0.00	1
1.30	15.86	15.86	0.00	0.00	0.00	1
1.30	16.16	16.16	0.00	0.00	0.00	1
1.30	16.46	16.46	0.00	0.00	0.00	1
1.29	16.77	16.77	0.00	0.00	0.00	1
1.29	17.07	17.07	0.00	0.00	0.00	1
1.28	17.37	17.37	0.00	0.00	0.00	1
1.28	17.67	17.67	0.00	0.00	0.00	1
1.27	17.98	17.98	0.00	0.00	0.00	1
1.27	18.28	18.28	0.00	0.00	0.00	1
1.26	18.58	18.58	0.00	0.00	0.00	1
1.26	18.88	18.88	0.00	0.00	0.00	1
1.26	19.19	19.19	0.00	0.00	0.00	1
1.25	19.49	19.49	0.00	0.00	0.00	1
1.25	19.79	19.79	0.00	0.00	0.00	1
1.24	20.09	20.09	0.00	0.00	0.00	1
1.24	20.40	20.40	0.00	0.00	0.00	1
1.23	20.70	20.70	0.00	0.00	0.00	1
1.23	21.00	21.00	0.00	0.00	0.00	1
1.22	21.31	21.31	0.00	0.00	0.00	1
1.22	35.57	12.28	30.69	19.09	13.87	1
1.21	36.38	17.21	31.54	19.75	9.08	1
1.20	37.19	17.18	32.39	20.42	9.26	1
1.19	38.01	17.14	33.23	21.09	9.45	1
1.18	38.82	17.10	34.07	21.75	9.63	1
1.17	39.63	17.07	34.92	22.42	9.81	1
1.16	40.45	17.03	35.75	23.09	9.99	1
1.15	41.26	16.99	36.59	23.76	10.18	1
1.14	42.08	16.96	37.42	24.43	10.36	1
1.13	42.90	16.92	38.26	25.10	10.54	1
1.12	43.71	16.89	39.09	25.77	10.72	1
1.12	43.71	4.63	39.09	25.77	10.72	1

1.12	44.53	16.85	39.92	26.44	10.90	1
1.11	45.35	16.82	40.74	27.11	11.08	1
1.10	46.16	16.78	41.57	27.79	11.26	1
1.09	46.98	16.75	42.39	28.46	11.44	1
1.08	47.80	16.71	43.21	29.13	11.62	1
1.07	48.62	16.68	44.03	29.80	11.80	1
1.06	49.43	16.65	44.85	30.47	11.98	1
1.05	50.25	16.61	45.67	31.15	12.16	1
1.04	51.07	16.58	46.48	31.82	12.34	1
1.03	51.89	16.55	47.29	32.49	12.51	1
1.02	52.70	16.52	48.10	33.16	12.69	1
1.01	53.52	16.49	48.91	33.83	12.87	1
1.00	54.34	16.45	49.72	34.50	13.05	1
0.99	55.16	16.42	50.52	35.17	13.22	1
0.99	55.97	16.39	51.33	35.84	13.40	1
0.98	56.79	16.36	52.13	36.51	13.58	1
0.97	57.60	16.33	52.93	37.18	13.75	1
0.96	58.42	16.30	53.73	37.85	13.93	1
0.95	59.23	16.27	54.53	38.52	14.10	1
0.94	60.05	16.24	55.32	39.19	14.28	1
0.93	60.86	16.21	56.12	39.86	14.45	1
0.92	61.68	16.18	56.91	40.53	14.63	1
0.91	62.49	16.16	57.70	41.20	14.80	1
0.90	63.30	16.13	58.49	41.86	14.98	1
0.89	64.12	16.10	59.28	42.53	15.15	1
0.88	64.93	16.07	60.07	43.20	15.33	1
0.87	65.74	16.04	60.86	43.86	15.50	1
0.86	66.55	16.02	61.64	44.53	15.67	1
0.86	67.36	15.99	62.42	45.19	15.85	1
0.85	68.17	15.96	63.21	45.85	16.02	1
0.84	68.98	15.94	63.99	46.52	16.19	1
0.83	69.79	15.91	64.74	47.18	16.36	1
0.82	70.59	15.88	65.49	47.84	16.54	1
0.81	71.40	15.86	66.23	48.50	16.71	1
0.80	72.21	15.83	66.97	49.16	16.88	1
0.79	73.01	15.81	67.71	49.82	17.05	1
0.78	73.82	15.78	68.45	50.48	17.22	1
0.77	74.62	15.76	69.18	51.14	17.39	1
0.76	75.43	15.73	69.92	51.80	17.56	1
0.75	76.23	15.71	70.65	52.46	17.73	1
0.75	76.23	5.58	70.65	52.46	17.73	1
0.74	77.67	15.66	71.97	53.64	18.04	1
0.72	79.11	15.62	73.28	54.82	18.34	1
0.70	80.55	15.58	74.59	55.99	18.65	1
0.69	81.99	15.54	75.90	57.17	18.95	1
0.67	83.42	15.49	77.20	58.34	19.26	1
0.65	84.86	15.45	78.50	59.51	19.56	1
0.63	86.29	15.41	79.80	60.67	19.86	1
0.62	87.71	15.37	81.10	61.84	20.16	1
0.60	89.14	15.34	82.39	63.00	20.46	1
0.58	90.56	15.30	83.68	64.16	20.76	1
0.57	91.98	15.26	84.96	65.32	21.06	1
0.55	93.40	15.23	86.25	66.47	21.36	1
0.53	94.81	15.19	87.53	67.63	21.66	1

0.52	96.22	15.15	88.80	68.78	21.96	1
0.50	97.63	15.12	90.08	69.92	22.26	1
0.48	99.04	15.09	91.35	71.07	22.55	1
0.47	100.45	15.05	92.62	72.21	22.85	1
0.45	101.85	15.02	93.89	73.35	23.14	1
0.43	103.25	14.99	95.15	74.49	23.44	1
0.41	104.65	14.96	96.42	75.62	23.73	1
0.40	106.04	14.92	97.68	76.76	24.03	1
0.38	107.44	14.89	98.93	77.89	24.32	1
0.36	108.83	14.86	100.19	79.02	24.61	1
0.35	110.21	14.83	101.44	80.14	24.90	1
0.33	111.60	14.81	102.69	81.26	25.20	1
0.31	112.98	14.78	103.94	82.38	25.49	1
0.30	114.36	14.75	105.18	83.50	25.78	1
0.28	115.74	14.72	106.43	84.62	26.07	1
0.26	71.43	14.69	56.73	65.76	-9.02	1
0.25	72.56	14.67	57.90	66.82	-8.92	1
0.23	73.70	14.64	59.06	67.88	-8.82	1
0.21	74.84	14.62	60.22	68.94	-8.72	1
0.19	75.97	14.59	61.38	70.00	-8.62	1
0.18	77.11	14.57	62.54	71.06	-8.52	1
0.16	78.25	14.54	63.70	72.12	-8.41	1
0.14	79.38	14.52	64.87	73.18	-8.31	1
0.13	80.52	14.49	66.03	74.24	-8.22	1
0.11	81.66	14.47	67.19	75.30	-8.12	1
0.09	82.80	14.45	68.35	76.36	-8.02	1
0.08	83.93	14.43	69.51	77.43	-7.92	1
0.08	84.17	14.43	69.74	77.43	-7.69	1
0.06	85.20	14.67	70.54	78.37	-7.83	1
0.05	86.24	14.90	71.34	79.31	-7.97	1
0.03	87.27	15.13	72.14	80.25	-8.11	1
0.01	88.30	15.36	72.94	81.19	-8.25	1
0.00	89.33	15.59	73.74	82.12	0.00	1

Time = 7325. Degree of Consolidation = 45.0%

Total Settlement = 0.960

Settlement at End of Primary Consolidation = 1.041

Settlement caused by Primary Consolidation at time 7325. = 0.468

Settlement caused by Secondary Compression at time 7325. = 0.000

Settlement Due to Desiccation = 0.492

Surface Elevation = 0.61



Grand Chenier Marsh Creation
GeoEngineers, Inc.

Report Creation Date: 2023/02/24, 15:23:05

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Settle3 Analysis Information

Grand Chenier Marsh Creation

Project Settings

Document Name	Grand Chenier_MC340_MF+1.5
Project Title	Grand Chenier Marsh Creation
Analysis	ML -0.929 , MF +1.5
Author	DNF
Company	GeoEngineers, Inc.
Date Created	1/27/2023
Last saved with Settle3 version	5.017
Stress Computation Method	Boussinesq
Stress Units	Imperial, stress as ksf
Settlement Units	inches
Time-dependent Consolidation Analysis	
Time Units	days
Permeability Units	inches/year

Advanced Settings

Start of secondary consolidation (% of primary)	95
Min. stress for secondary consolidation (% of initial)	1
Reset time when load changes for secondary consolidation	No
Minimum settlement ratio for subgrade modulus	0.9
Use average poisson's ratio to calculate layered stresses	
Ignore negative effective stresses in settlement calculations	
Add field points to load edges	

Soil Profile

Layer Option	Horizontal Soil Layers
Vertical Axis	Depth below ground surface

Stage Settings

Stage #	Name	Time [days]
1	Stage 1	0
2	Stage 2	15
3	Stage 3	30
4	Stage 4	60
5	Stage 5	90
6	Stage 6	120
7	Stage 7	150
8	Stage 8	180
9	Stage 9	270
10	Stage 10	365
11	Stage 11	730
12	Stage 12	1095
13	Stage 13	2190
14	Stage 14	3650
15	Stage 15	7300

Results

Time taken to compute: 0 seconds

Stage: Stage 1 = 0 d

Data Type	Minimum	Maximum
Total Settlement [in]	0	0
Total Consolidation Settlement [in]	0	0
Virgin Consolidation Settlement [in]	0	0
Recompression Consolidation Settlement [in]	0	0
Immediate Settlement [in]	0	0
Secondary Settlement [in]	0	0
Loading Stress ZZ [ksf]	0.0273834	0.033858
Loading Stress XX [ksf]	0.00363475	0.0237006
Loading Stress YY [ksf]	0.00363475	0.0237006
Effective Stress ZZ [ksf]	0	1.64871
Effective Stress XX [ksf]	0.0237006	1.65235
Effective Stress YY [ksf]	0.0237006	1.65235
Total Stress ZZ [ksf]	0.033858	4.11413
Total Stress XX [ksf]	0.0575586	4.11776
Total Stress YY [ksf]	0.0575586	4.11776
Modulus of Subgrade Reaction (Total) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Immediate) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Consolidation) [ksf/ft]	0	0
Total Strain	0	0
Pore Water Pressure [ksf]	0.033858	2.46541
Excess Pore Water Pressure [ksf]	0.0273834	0.033858
Degree of Consolidation [%]	0	0
Pre-consolidation Stress [ksf]	0.272	1.64785
Over-consolidation Ratio	1	204.951
Void Ratio	0	3.38
Permeability [in/y]	0	53.1409
Coefficient of Consolidation [in ² /y]	0	1051
Hydroconsolidation Settlement [in]	0	0
Average Degree of Consolidation [%]	0	0
Undrained Shear Strength	0	0

Stage: Stage 2 = 15 d

Data Type	Minimum	Maximum
Total Settlement [in]	0	0.368991
Total Consolidation Settlement [in]	0	0.368991
Virgin Consolidation Settlement [in]	0	0.0986848
Recompression Consolidation Settlement [in]	0	0.270306
Immediate Settlement [in]	0	0
Secondary Settlement [in]	0	0
Loading Stress ZZ [ksf]	0.0273834	0.033858
Loading Stress XX [ksf]	0.00363475	0.0237006
Loading Stress YY [ksf]	0.00363475	0.0237006
Effective Stress ZZ [ksf]	0.033858	1.6761
Effective Stress XX [ksf]	0.0575586	1.67973
Effective Stress YY [ksf]	0.0575586	1.67973
Total Stress ZZ [ksf]	0.033858	4.11413
Total Stress XX [ksf]	0.0575586	4.11776
Total Stress YY [ksf]	0.0575586	4.11776
Modulus of Subgrade Reaction (Total) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Immediate) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Consolidation) [ksf/ft]	0	0
Total Strain	0	0.0422252
Pore Water Pressure [ksf]	0	2.43803
Excess Pore Water Pressure [ksf]	0	0.0337289
Degree of Consolidation [%]	0	98.9572
Pre-consolidation Stress [ksf]	0.272	1.67524
Over-consolidation Ratio	1	7.74439
Void Ratio	0	3.37999
Permeability [in/y]	0	53.1409
Coefficient of Consolidation [in ² /y]	0	1051
Hydroconsolidation Settlement [in]	0	0
Average Degree of Consolidation [%]	0	0
Undrained Shear Strength	0	0.00151258

Stage: Stage 3 = 30 d

Data Type	Minimum	Maximum
Total Settlement [in]	0	0.450145
Total Consolidation Settlement [in]	0	0.450145
Virgin Consolidation Settlement [in]	0	0.130925
Recompression Consolidation Settlement [in]	0	0.31922
Immediate Settlement [in]	0	0
Secondary Settlement [in]	0	0
Loading Stress ZZ [ksf]	0.0273834	0.033858
Loading Stress XX [ksf]	0.00363475	0.0237006
Loading Stress YY [ksf]	0.00363475	0.0237006
Effective Stress ZZ [ksf]	0.033858	1.6761
Effective Stress XX [ksf]	0.0575586	1.67973
Effective Stress YY [ksf]	0.0575586	1.67973
Total Stress ZZ [ksf]	0.033858	4.11413
Total Stress XX [ksf]	0.0575586	4.11776
Total Stress YY [ksf]	0.0575586	4.11776
Modulus of Subgrade Reaction (Total) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Immediate) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Consolidation) [ksf/ft]	0	0
Total Strain	0	0.0422353
Pore Water Pressure [ksf]	0	2.43803
Excess Pore Water Pressure [ksf]	0	0.0336698
Degree of Consolidation [%]	0	99.2517
Pre-consolidation Stress [ksf]	0.272	1.67524
Over-consolidation Ratio	1	7.73828
Void Ratio	0	3.37994
Permeability [in/y]	0	53.1409
Coefficient of Consolidation [in ² /y]	0	1051
Hydroconsolidation Settlement [in]	0	0
Average Degree of Consolidation [%]	0	0
Undrained Shear Strength	0	0.00151258

Stage: Stage 4 = 60 d

Data Type	Minimum	Maximum
Total Settlement [in]	0	0.55216
Total Consolidation Settlement [in]	0	0.55216
Virgin Consolidation Settlement [in]	0	0.170214
Recompression Consolidation Settlement [in]	0	0.381946
Immediate Settlement [in]	0	0
Secondary Settlement [in]	0	0
Loading Stress ZZ [ksf]	0.0273834	0.033858
Loading Stress XX [ksf]	0.00363475	0.0237006
Loading Stress YY [ksf]	0.00363475	0.0237006
Effective Stress ZZ [ksf]	0.033858	1.6761
Effective Stress XX [ksf]	0.0575586	1.67973
Effective Stress YY [ksf]	0.0575586	1.67973
Total Stress ZZ [ksf]	0.033858	4.11413
Total Stress XX [ksf]	0.0575586	4.11776
Total Stress YY [ksf]	0.0575586	4.11776
Modulus of Subgrade Reaction (Total) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Immediate) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Consolidation) [ksf/ft]	0	0
Total Strain	0	0.0422407
Pore Water Pressure [ksf]	0	2.43803
Excess Pore Water Pressure [ksf]	0	0.0332767
Degree of Consolidation [%]	0	99.4472
Pre-consolidation Stress [ksf]	0.272	1.67524
Over-consolidation Ratio	1	7.73508
Void Ratio	0	3.3797
Permeability [in/y]	0	53.1409
Coefficient of Consolidation [in ² /y]	0	1051
Hydroconsolidation Settlement [in]	0	0
Average Degree of Consolidation [%]	0	0
Undrained Shear Strength	0	0.00151258

Stage: Stage 5 = 90 d

Data Type	Minimum	Maximum
Total Settlement [in]	0	0.620484
Total Consolidation Settlement [in]	0	0.620484
Virgin Consolidation Settlement [in]	0	0.198068
Recompression Consolidation Settlement [in]	0	0.422416
Immediate Settlement [in]	0	0
Secondary Settlement [in]	0	0
Loading Stress ZZ [ksf]	0.0273834	0.033858
Loading Stress XX [ksf]	0.00363475	0.0237006
Loading Stress YY [ksf]	0.00363475	0.0237006
Effective Stress ZZ [ksf]	0.033858	1.6761
Effective Stress XX [ksf]	0.0575586	1.67973
Effective Stress YY [ksf]	0.0575586	1.67973
Total Stress ZZ [ksf]	0.033858	4.11413
Total Stress XX [ksf]	0.0575586	4.11776
Total Stress YY [ksf]	0.0575586	4.11776
Modulus of Subgrade Reaction (Total) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Immediate) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Consolidation) [ksf/ft]	0	0
Total Strain	0	0.0422436
Pore Water Pressure [ksf]	0	2.43803
Excess Pore Water Pressure [ksf]	0	0.0323377
Degree of Consolidation [%]	0	99.5433
Pre-consolidation Stress [ksf]	0.272	1.67524
Over-consolidation Ratio	1	7.73333
Void Ratio	0	3.3794
Permeability [in/y]	0	53.1409
Coefficient of Consolidation [in ² /y]	0	1051
Hydroconsolidation Settlement [in]	0	0
Average Degree of Consolidation [%]	0	0
Undrained Shear Strength	0	0.00151258

Stage: Stage 6 = 120 d

Data Type	Minimum	Maximum
Total Settlement [in]	0	0.670895
Total Consolidation Settlement [in]	0	0.670895
Virgin Consolidation Settlement [in]	0	0.220364
Recompression Consolidation Settlement [in]	0	0.450531
Immediate Settlement [in]	0	0
Secondary Settlement [in]	0	0
Loading Stress ZZ [ksf]	0.0273834	0.033858
Loading Stress XX [ksf]	0.00363475	0.0237006
Loading Stress YY [ksf]	0.00363475	0.0237006
Effective Stress ZZ [ksf]	0.033858	1.6761
Effective Stress XX [ksf]	0.0575586	1.67973
Effective Stress YY [ksf]	0.0575586	1.67973
Total Stress ZZ [ksf]	0.033858	4.11413
Total Stress XX [ksf]	0.0575586	4.11776
Total Stress YY [ksf]	0.0575586	4.11776
Modulus of Subgrade Reaction (Total) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Immediate) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Consolidation) [ksf/ft]	0	0
Total Strain	0	0.0422453
Pore Water Pressure [ksf]	0	2.43803
Excess Pore Water Pressure [ksf]	0	0.0309269
Degree of Consolidation [%]	0	99.6038
Pre-consolidation Stress [ksf]	0.272	1.67524
Over-consolidation Ratio	1	7.73227
Void Ratio	0	3.37921
Permeability [in/y]	0	53.1409
Coefficient of Consolidation [in ² /y]	0	1051
Hydroconsolidation Settlement [in]	0	0
Average Degree of Consolidation [%]	0	0
Undrained Shear Strength	0	0.00151258

Stage: Stage 7 = 150 d

Data Type	Minimum	Maximum
Total Settlement [in]	0	0.710391
Total Consolidation Settlement [in]	0	0.710391
Virgin Consolidation Settlement [in]	0	0.239265
Recompression Consolidation Settlement [in]	0	0.471125
Immediate Settlement [in]	0	0
Secondary Settlement [in]	0	0
Loading Stress ZZ [ksf]	0.0273834	0.033858
Loading Stress XX [ksf]	0.00363475	0.0237006
Loading Stress YY [ksf]	0.00363475	0.0237006
Effective Stress ZZ [ksf]	0.033858	1.6761
Effective Stress XX [ksf]	0.0575586	1.67973
Effective Stress YY [ksf]	0.0575586	1.67973
Total Stress ZZ [ksf]	0.033858	4.11413
Total Stress XX [ksf]	0.0575586	4.11776
Total Stress YY [ksf]	0.0575586	4.11776
Modulus of Subgrade Reaction (Total) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Immediate) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Consolidation) [ksf/ft]	0	0
Total Strain	0	0.0422464
Pore Water Pressure [ksf]	0	2.43803
Excess Pore Water Pressure [ksf]	0	0.0297496
Degree of Consolidation [%]	0	99.6455
Pre-consolidation Stress [ksf]	0.272	1.67524
Over-consolidation Ratio	1	7.73162
Void Ratio	0	3.37904
Permeability [in/y]	0	53.1409
Coefficient of Consolidation [in ² /y]	0	1051
Hydroconsolidation Settlement [in]	0	0
Average Degree of Consolidation [%]	0	0
Undrained Shear Strength	0	0.00151258

Stage: Stage 8 = 180 d

Data Type	Minimum	Maximum
Total Settlement [in]	0	0.742763
Total Consolidation Settlement [in]	0	0.742763
Virgin Consolidation Settlement [in]	0	0.255846
Recompression Consolidation Settlement [in]	0	0.486918
Immediate Settlement [in]	0	0
Secondary Settlement [in]	0	0
Loading Stress ZZ [ksf]	0.0273834	0.033858
Loading Stress XX [ksf]	0.00363475	0.0237006
Loading Stress YY [ksf]	0.00363475	0.0237006
Effective Stress ZZ [ksf]	0.033858	1.6761
Effective Stress XX [ksf]	0.0575586	1.67973
Effective Stress YY [ksf]	0.0575586	1.67973
Total Stress ZZ [ksf]	0.033858	4.11413
Total Stress XX [ksf]	0.0575586	4.11776
Total Stress YY [ksf]	0.0575586	4.11776
Modulus of Subgrade Reaction (Total) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Immediate) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Consolidation) [ksf/ft]	0	0
Total Strain	0	0.0422471
Pore Water Pressure [ksf]	0	2.43803
Excess Pore Water Pressure [ksf]	0	0.0285362
Degree of Consolidation [%]	0	99.6765
Pre-consolidation Stress [ksf]	0.272	1.67524
Over-consolidation Ratio	1	7.73121
Void Ratio	0	3.37889
Permeability [in/y]	0	53.1409
Coefficient of Consolidation [in ² /y]	0	1051
Hydroconsolidation Settlement [in]	0	0
Average Degree of Consolidation [%]	0	0
Undrained Shear Strength	0	0.00151258

Stage: Stage 9 = 270 d

Data Type	Minimum	Maximum
Total Settlement [in]	0	0.815193
Total Consolidation Settlement [in]	0	0.815193
Virgin Consolidation Settlement [in]	0	0.29649
Recompression Consolidation Settlement [in]	0	0.518703
Immediate Settlement [in]	0	0
Secondary Settlement [in]	0	0
Loading Stress ZZ [ksf]	0.0273834	0.033858
Loading Stress XX [ksf]	0.00363475	0.0237006
Loading Stress YY [ksf]	0.00363475	0.0237006
Effective Stress ZZ [ksf]	0.033858	1.6761
Effective Stress XX [ksf]	0.0575586	1.67973
Effective Stress YY [ksf]	0.0575586	1.67973
Total Stress ZZ [ksf]	0.033858	4.11413
Total Stress XX [ksf]	0.0575586	4.11776
Total Stress YY [ksf]	0.0575586	4.11776
Modulus of Subgrade Reaction (Total) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Immediate) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Consolidation) [ksf/ft]	0	0
Total Strain	0	0.042248
Pore Water Pressure [ksf]	0	2.43803
Excess Pore Water Pressure [ksf]	0	0.0246631
Degree of Consolidation [%]	0	99.7393
Pre-consolidation Stress [ksf]	0.272	1.67524
Over-consolidation Ratio	1	7.7307
Void Ratio	0	3.37852
Permeability [in/y]	0	53.1409
Coefficient of Consolidation [in ² /y]	0	1051
Hydroconsolidation Settlement [in]	0	0
Average Degree of Consolidation [%]	0	0
Undrained Shear Strength	0	0.00151258

Stage: Stage 10 = 365 d

Data Type	Minimum	Maximum
Total Settlement [in]	0	0.885413
Total Consolidation Settlement [in]	0	0.885413
Virgin Consolidation Settlement [in]	0	0.347519
Recompression Consolidation Settlement [in]	0	0.537894
Immediate Settlement [in]	0	0
Secondary Settlement [in]	0	0
Loading Stress ZZ [ksf]	0.0273834	0.033858
Loading Stress XX [ksf]	0.00363475	0.0237006
Loading Stress YY [ksf]	0.00363475	0.0237006
Effective Stress ZZ [ksf]	0.033858	1.6761
Effective Stress XX [ksf]	0.0575586	1.67973
Effective Stress YY [ksf]	0.0575586	1.67973
Total Stress ZZ [ksf]	0.033858	4.11413
Total Stress XX [ksf]	0.0575586	4.11776
Total Stress YY [ksf]	0.0575586	4.11776
Modulus of Subgrade Reaction (Total) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Immediate) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Consolidation) [ksf/ft]	0	0
Total Strain	0	0.0422482
Pore Water Pressure [ksf]	0	2.43803
Excess Pore Water Pressure [ksf]	0	0.0208167
Degree of Consolidation [%]	0	99.7846
Pre-consolidation Stress [ksf]	0.272	1.67524
Over-consolidation Ratio	1	7.73057
Void Ratio	0	3.37821
Permeability [in/y]	0	53.1409
Coefficient of Consolidation [in ² /y]	0	1051
Hydroconsolidation Settlement [in]	0	0
Average Degree of Consolidation [%]	0	0
Undrained Shear Strength	0	0.00151258

Stage: Stage 11 = 730 d

Data Type	Minimum	Maximum
Total Settlement [in]	0	1.0266
Total Consolidation Settlement [in]	0	1.0266
Virgin Consolidation Settlement [in]	0	0.452583
Recompression Consolidation Settlement [in]	0	0.574022
Immediate Settlement [in]	0	0
Secondary Settlement [in]	0	0
Loading Stress ZZ [ksf]	0.0273834	0.033858
Loading Stress XX [ksf]	0.00363475	0.0237006
Loading Stress YY [ksf]	0.00363475	0.0237006
Effective Stress ZZ [ksf]	0.033858	1.6761
Effective Stress XX [ksf]	0.0575586	1.67973
Effective Stress YY [ksf]	0.0575586	1.67973
Total Stress ZZ [ksf]	0.033858	4.11413
Total Stress XX [ksf]	0.0575586	4.11776
Total Stress YY [ksf]	0.0575586	4.11776
Modulus of Subgrade Reaction (Total) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Immediate) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Consolidation) [ksf/ft]	0	0
Total Strain	0	0.0422482
Pore Water Pressure [ksf]	0	2.43803
Excess Pore Water Pressure [ksf]	0	0.0105762
Degree of Consolidation [%]	0	99.8913
Pre-consolidation Stress [ksf]	0.272	1.67524
Over-consolidation Ratio	1	7.73054
Void Ratio	0	3.37748
Permeability [in/y]	0	53.1409
Coefficient of Consolidation [in ² /y]	0	1051
Hydroconsolidation Settlement [in]	0	0
Average Degree of Consolidation [%]	0	0
Undrained Shear Strength	0	0.00151258

Stage: Stage 12 = 1095 d

Data Type	Minimum	Maximum
Total Settlement [in]	0	1.08133
Total Consolidation Settlement [in]	0	1.08133
Virgin Consolidation Settlement [in]	0	0.494973
Recompression Consolidation Settlement [in]	0	0.586362
Immediate Settlement [in]	0	0
Secondary Settlement [in]	0	0
Loading Stress ZZ [ksf]	0.0273834	0.033858
Loading Stress XX [ksf]	0.00363475	0.0237006
Loading Stress YY [ksf]	0.00363475	0.0237006
Effective Stress ZZ [ksf]	0.033858	1.6761
Effective Stress XX [ksf]	0.0575586	1.67973
Effective Stress YY [ksf]	0.0575586	1.67973
Total Stress ZZ [ksf]	0.033858	4.11413
Total Stress XX [ksf]	0.0575586	4.11776
Total Stress YY [ksf]	0.0575586	4.11776
Modulus of Subgrade Reaction (Total) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Immediate) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Consolidation) [ksf/ft]	0	0
Total Strain	0	0.0422482
Pore Water Pressure [ksf]	0	2.43803
Excess Pore Water Pressure [ksf]	0	0.00535559
Degree of Consolidation [%]	0	99.9449
Pre-consolidation Stress [ksf]	0.272	1.67524
Over-consolidation Ratio	1	7.73053
Void Ratio	0	3.37713
Permeability [in/y]	0	53.1409
Coefficient of Consolidation [in ² /y]	0	1051
Hydroconsolidation Settlement [in]	0	0
Average Degree of Consolidation [%]	0	0
Undrained Shear Strength	0	0.00151258

Stage: Stage 13 = 2190 d

Data Type	Minimum	Maximum
Total Settlement [in]	0	1.12088
Total Consolidation Settlement [in]	0	1.12088
Virgin Consolidation Settlement [in]	0	0.527636
Recompression Consolidation Settlement [in]	0	0.593241
Immediate Settlement [in]	0	0
Secondary Settlement [in]	0	0
Loading Stress ZZ [ksf]	0.0273834	0.033858
Loading Stress XX [ksf]	0.00363475	0.0237006
Loading Stress YY [ksf]	0.00363475	0.0237006
Effective Stress ZZ [ksf]	0.033858	1.6761
Effective Stress XX [ksf]	0.0575586	1.67973
Effective Stress YY [ksf]	0.0575586	1.67973
Total Stress ZZ [ksf]	0.033858	4.11413
Total Stress XX [ksf]	0.0575586	4.11776
Total Stress YY [ksf]	0.0575586	4.11776
Modulus of Subgrade Reaction (Total) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Immediate) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Consolidation) [ksf/ft]	0	0
Total Strain	0	0.0422482
Pore Water Pressure [ksf]	0	2.43803
Excess Pore Water Pressure [ksf]	0	0.00069515
Degree of Consolidation [%]	0	99.9929
Pre-consolidation Stress [ksf]	0.272	1.67524
Over-consolidation Ratio	1	7.73053
Void Ratio	0	3.37681
Permeability [in/y]	0	53.1409
Coefficient of Consolidation [in ² /y]	0	1051
Hydroconsolidation Settlement [in]	0	0
Average Degree of Consolidation [%]	0	0
Undrained Shear Strength	0	0.00151258

Stage: Stage 14 = 3650 d

Data Type	Minimum	Maximum
Total Settlement [in]	0	1.12559
Total Consolidation Settlement [in]	0	1.12559
Virgin Consolidation Settlement [in]	0	0.531778
Recompression Consolidation Settlement [in]	0	0.593807
Immediate Settlement [in]	0	0
Secondary Settlement [in]	0	0
Loading Stress ZZ [ksf]	0.0273834	0.033858
Loading Stress XX [ksf]	0.00363475	0.0237006
Loading Stress YY [ksf]	0.00363475	0.0237006
Effective Stress ZZ [ksf]	0.033858	1.6761
Effective Stress XX [ksf]	0.0575586	1.67973
Effective Stress YY [ksf]	0.0575586	1.67973
Total Stress ZZ [ksf]	0.033858	4.11413
Total Stress XX [ksf]	0.0575586	4.11776
Total Stress YY [ksf]	0.0575586	4.11776
Modulus of Subgrade Reaction (Total) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Immediate) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Consolidation) [ksf/ft]	0	0
Total Strain	0	0.0422482
Pore Water Pressure [ksf]	0	2.43803
Excess Pore Water Pressure [ksf]	-5.05829e-26	4.56319e-05
Degree of Consolidation [%]	0	99.9995
Pre-consolidation Stress [ksf]	0.272	1.67524
Over-consolidation Ratio	1	7.73053
Void Ratio	0	3.37677
Permeability [in/y]	0	53.1409
Coefficient of Consolidation [in ² /y]	0	1051
Hydroconsolidation Settlement [in]	0	0
Average Degree of Consolidation [%]	0	0
Undrained Shear Strength	0	0.00151258

Stage: Stage 15 = 7300 d

Data Type	Minimum	Maximum
Total Settlement [in]	0	1.12591
Total Consolidation Settlement [in]	0	1.12591
Virgin Consolidation Settlement [in]	0	0.532064
Recompression Consolidation Settlement [in]	0	0.593842
Immediate Settlement [in]	0	0
Secondary Settlement [in]	0	0
Loading Stress ZZ [ksf]	0.0273834	0.033858
Loading Stress XX [ksf]	0.00363475	0.0237006
Loading Stress YY [ksf]	0.00363475	0.0237006
Effective Stress ZZ [ksf]	0.033858	1.6761
Effective Stress XX [ksf]	0.0575586	1.67973
Effective Stress YY [ksf]	0.0575586	1.67973
Total Stress ZZ [ksf]	0.033858	4.11413
Total Stress XX [ksf]	0.0575586	4.11776
Total Stress YY [ksf]	0.0575586	4.11776
Modulus of Subgrade Reaction (Total) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Immediate) [ksf/ft]	0	0
Modulus of Subgrade Reaction (Consolidation) [ksf/ft]	0	0
Total Strain	0	0.0422482
Pore Water Pressure [ksf]	0	2.43803
Excess Pore Water Pressure [ksf]	-9.42594e-27	4.9761e-08
Degree of Consolidation [%]	0	100
Pre-consolidation Stress [ksf]	0.272	1.67524
Over-consolidation Ratio	1	7.73053
Void Ratio	0	3.37677
Permeability [in/y]	0	53.1409
Coefficient of Consolidation [in ² /y]	0	1051
Hydroconsolidation Settlement [in]	0	0
Average Degree of Consolidation [%]	0	0
Undrained Shear Strength	0	0.00151258

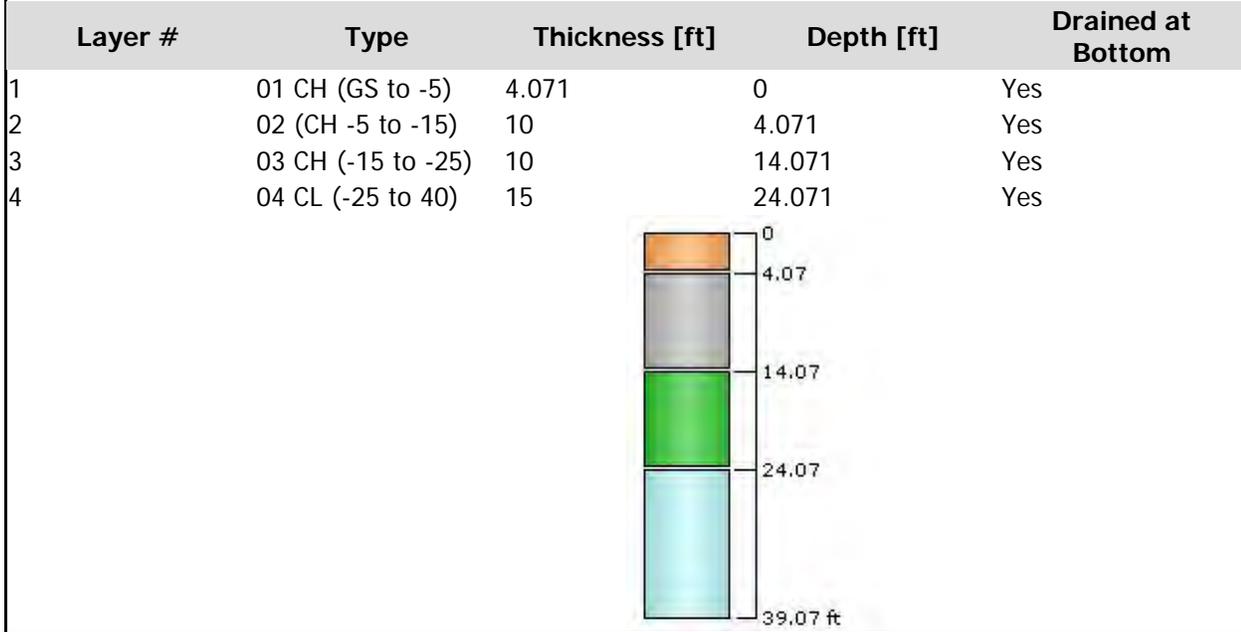
Embankments

1. Embankment: "Marsh Fill +3.5"

Label	Marsh Fill +3.5						
Center Line	(-50, 50) to (50, 50)						
Near End Angle	90 degrees						
Far End Angle	90 degrees						
Number of Layers	1						
Base Width	100						
Layer	Stage	Left Bench Width (ft)	Left Angle (deg)	Height (ft)	Unit Weight (kips/ft3)	Right Angle (deg)	Right Bench Width (ft)
1	Stage 1 = 0 d	0	90	1.539	0.022	90	0

Soil Layers

Ground Surface Drained: Yes



Soil Properties

Property	01 CH (GS to - 5)	02 (CH -5 to - 15)	03 CH (-15 to - 25)	04 CL (-25 to 40)
Color				
Unit Weight [kips/ft3]	0.095	0.095	0.095	0.12
Saturated Unit Weight [kips/ft3]	0.095	0.095	0.095	0.12
K0	1	1	1	1
Primary Consolidation	Enabled	Enabled	Enabled	Disabled
Material Type	Non-Linear	Non-Linear	Non-Linear	
Cc	1.19	1.19	1.19	-
Cr	0.13	0.13	0.13	-
e0	3.38	3.38	3.38	-
Pc [ksf]	0.272	0.408	0.654	-
Cv [in2/y]	1051	1051	1051	-
Cvr [in2/y]	1051	1051	1051	-
B-bar	1	1	1	-
Undrained Su A [kips/ft2]	0	0	0	0
Undrained Su S	0.2	0.2	0.2	0.2
Undrained Su m	0.8	0.8	0.8	0.8
Piezo Line ID	1	1	1	1

Groundwater

Groundwater method
Water Unit Weight

Piezometric Lines
0.0624 kips/ft³

Piezometric Line Entities

ID	Depth (ft)
1	0 ft

Query

Query Points

Point #	Query Point Name	(X,Y) Location	Number of Divisions
1	Query Point 1	0, 50	Auto: 65

APPENDIX J
Report Limitations and Guidelines for Use

APPENDIX J

REPORT LIMITATIONS AND GUIDELINES FOR USE

This appendix provides information to help you manage your risks with respect to the use of this report.

Geotechnical Services Are Performed for Specific Purposes, Persons and Projects

This report has been prepared exclusively for the ECM + MRD Joint Venture, the NRCS, and their authorized agents and regulatory agencies. The information contained herein is not applicable to other sites.

GeoEngineers, Inc. (GeoEngineers) structures our services to meet the specific needs of our clients. No party other than the ECM + MRD Joint Venture and the NRCS may rely on the product of our services unless we agree to such reliance in advance and in writing. This is to provide our firm with reasonable protection against open-ended liability claims by third parties with whom there would otherwise be no contractual limits to their actions. Within the limitations of scope, schedule and budget, our services have been executed in accordance with our Agreement with the Client and generally accepted geotechnical practices in this area at the time this report was prepared. Use of this report is not recommended for any purpose or project except the one originally contemplated.

A Geotechnical Engineering or Geologic Report Is Based on a Unique Set of Project-Specific Factors

This report has been prepared for the South Grand Chenier - Baker Marsh Creation (ME-32) project located in Cameron Parish, Louisiana. GeoEngineers considered a number of unique, project-specific factors when establishing the scope of services for this project and report. Unless GeoEngineers specifically indicates otherwise, it is important not to rely on this report if it was:

- not prepared for you,
- not prepared for your project,
- not prepared for the specific site explored, or
- completed before important project changes were made.

For example, changes that can affect the applicability of this report include those that affect:

- the function of the proposed structure;
- elevation, configuration, location, orientation or weight of the proposed structure;
- composition of the design team; or
- project ownership.

If important changes are made after the date of this report, we recommend that GeoEngineers be given the opportunity to review our interpretations and recommendations. Based on that review, we can provide written modifications or confirmation, as appropriate.

Subsurface Conditions Can Change

This geotechnical or geologic report is based on conditions that existed at the time the study was performed. The findings and conclusions of this report may be affected by the passage of time, by man-made events such as construction on or adjacent to the site, or by natural events such as floods, earthquakes, slope instability or groundwater fluctuations. If more than a few months have passed since issuance of our report or work product, or if any of the described events may have occurred, please contact GeoEngineers before applying this report for its intended purpose so that we may evaluate whether changed conditions affect the continued reliability or applicability of our conclusions and recommendations.

Most Geotechnical and Geologic Findings Are Professional Opinions

Our interpretations of subsurface conditions are based on field observations from widely spaced sampling locations at the site. Site exploration identifies the specific subsurface conditions only at those points where subsurface tests are conducted or samples are taken. GeoEngineers reviewed field and laboratory data and then applied our professional judgment to render an informed opinion about subsurface conditions throughout the site. Actual subsurface conditions may differ, sometimes significantly, from those indicated in this report. Our report, conclusions and interpretations should not be construed as a warranty of the subsurface conditions.

Geotechnical Engineering Report Recommendations Are Not Final

The construction recommendations included in this report are preliminary and should not be considered final. GeoEngineers' recommendations can be finalized only by observing actual subsurface conditions revealed during construction. GeoEngineers is unable to assume responsibility for the recommendations in this report without performing construction observation.

We recommend that you allow sufficient monitoring, testing and consultation during construction by GeoEngineers to confirm that the conditions encountered are consistent with those indicated by the explorations, to provide recommendations for design changes if the conditions revealed during the work differ from those anticipated, and to evaluate whether earthwork activities are completed in accordance with our recommendations. Retaining GeoEngineers for construction observation for this project is the most effective method of managing the risks associated with unanticipated conditions.

A Geotechnical Engineering or Geologic Report Could Be Subject to Misinterpretation

Misinterpretation of this report by members of the design team or by contractors can result in costly problems. GeoEngineers can help reduce the risks of misinterpretation by conferring with appropriate members of the design team after submitting the report, reviewing pertinent elements of the design team's plans and specifications, participating in pre-bid and preconstruction conferences, and providing construction observation.

Do Not Redraw the Exploration Logs

Geotechnical engineers and geologists prepare final boring and testing logs based upon their interpretation of field logs and laboratory data. The logs included in a geotechnical engineering or geologic report should never be redrawn for inclusion in architectural or other design drawings. Photographic or electronic reproduction is acceptable but separating logs from the report can create a risk of misinterpretation.

Give Contractors a Complete Report and Guidance

To help prevent costly problems associated with unanticipated subsurface conditions, we recommend giving contractors the complete geotechnical engineering or geologic report but preface it with a clearly written letter of transmittal. In that letter, advise contractors that the report's accuracy is limited. In addition, encourage them to confer with GeoEngineers and/or to conduct additional study to obtain the specific types of information they need or prefer.

Contractors Are Responsible for Site Safety on Their Own Construction Projects

Our geotechnical recommendations are not intended to direct the contractor's procedures, methods, schedule or management of the work site. The contractor is solely responsible for job site safety and for managing construction operations to minimize risks to on-site personnel and adjacent properties.

Read These Provisions Closely

It is important to recognize that the geoscience practices (geotechnical engineering, geology and environmental science) are less exact than other engineering and natural science disciplines. Without this understanding, there may be expectations that could lead to disappointments, claims and disputes. GeoEngineers includes these explanatory "limitations" provisions in our reports to help reduce such risks. Please confer with GeoEngineers if you need to know more how these "Report Limitations and Guidelines for Use" apply to your project or site.

Biological Pollutants

GeoEngineers' Scope of Work specifically excludes the investigation, detection, prevention or assessment of the presence of Biological Pollutants. Accordingly, this report does not include any interpretations, recommendations, findings or conclusions regarding the detecting, assessing, preventing or abating of Biological Pollutants, and no conclusions or inferences should be drawn regarding Biological Pollutants as they may relate to this project. The term "Biological Pollutants" includes, but is not limited to, molds, fungi, spores, bacteria and viruses, and/or any of their byproducts.

