



Engineering  
and Testing

# Geotechnical Engineering Data Report

**Breton Landbridge Marsh Creation (West)**  
**Plaquemines Parish, Louisiana**  
APS File No: 2008-G063

Presented to:  
**Coastal Protection and Restoration Authority**  
150 Terrace Avenue  
Baton Rouge, LA 70802

Prepared by:  
**APS Engineering and Testing, LLC**  
1645 Nicolson Drive  
Baton Rouge, LA 70802.

January 4, 2021

## Table of Contents

<b>1.0</b>	<b>INTRODUCTION</b>	<b>4</b>
<b>2.0</b>	<b>FIELD EXPLORATION</b>	<b>4</b>
<b>3.0</b>	<b>LABORATORY TESTING</b>	<b>6</b>
<b>4.0</b>	<b>CPT SOUNDING RESULTS</b>	<b>6</b>
<b>5.0</b>	<b>SITE CONDITIONS</b>	<b>7</b>
<b>6.0</b>	<b>SUB-SURFACE MATERIALS</b>	<b>7</b>
<b>7.0</b>	<b>VARIATIONS</b>	<b>7</b>
<b>8.0</b>	<b>LIMITATIONS</b>	<b>7</b>

### **APPENDIX A**

Error! Bookmark not defined.

**A: Boring Location Map**

**B: Boring Logs**

**C: Unconsolidated Undrained Test Reports**

**D: Grain-Size Curves**

**E: Consolidation and Specific Gravity Data Summary**

**F: Consolidation Test Reports**

**G: CPT Probe Logs**

**H: CPT Raw Data**

**I: Settling Column Report**

**J: Low Stress Consolidation Test Report**

**K: Survey Report**

**Coastal Protection and Restoration Authority**  
150 Terrace Avenue  
Baton Rouge, LA 70802.

**Attention:** **Jessica Diez**  
Coastal Protection and Restoration Authority  
Project Manager  
Project Management Division  
The Water Campus

**Re:** **Breton Landbridge Marsh Creation (West)**  
Plaquemines Parish, Louisiana  
APS File No.: 2008-G063

**Dear Ms. Diez:**

A P S Engineering and Testing, LLC is pleased to submit our project data report for the above referenced project.

If you have any questions pertaining to this report, or if we may be of further service, please contact our office.


Respectfully submitted,  
**A P S ENGINEERING AND TESTING, LLC**



Sairam Eddanapudi, M.E., P.E.  
Chief Engineer



Sergio Aviles, P.E., M. ASCE  
President 1/19/2021



Suraj Mani Perabathula, M.E.  
Staff Engineer

## 1.0 INTRODUCTION

A P S Engineering and Testing, LLC (A P S) is pleased to present this Geotechnical Data Report for the Breton Landbridge Marsh Creation Project (West) to Costal Protection and Restoration Authority (CPRA). The project site is located in Plaquemines Parish approximately 3.6 miles southwest from Delacroix Island. A map showing the boring locations and CPTs are attached in Appendix A. Our geotechnical engineering services were performed in general accordance with our APS Proposal No.:APS 2007-G027 dated May 6, 2020 and NTP was given on July 29,2020.

## 2.0 FIELD EXPLORATION

Field exploration for the Breton Landbridge Marsh Creation (West) Project included drilling 14 soil borings (B-1 through B-14) and 11 CPT's (C-1 through C-11). Drilling was completed from August 12, 2020 through August 18, 2020. Borings B-1 to B-14 were drilled using a piston sampler mounted on airboat and C-1 to C-11 were explored with CPT rig mounted on airboat.

The depth of the explorations varied from 25 to 40 feet below existing mudline. CPRA provided the required permits to A P S Engineering and Testing, LLC for conducting the field exploration and the locations were staked in the field by our sub-contractor C.H. Fenstermaker and Associates, LLC.

A survey of field exploration locations including mudline elevation and location coordinates was provided by our sub-contractor C.H. Fenstermaker and Associates, LLC. prior to A P S Engineering and Testing, LLC mobilizing on-site. A copy of the survey report is provided in Appendix B.

A summary of boring locations, including latitude, longitude, bottom elevation and boring depth, are shown on Table 1, Table 2 and Table 3.

**TABLE 1.0: MARSH CREATION AREA**

SOIL BORING NUMBER	LATITUDE	LONGITUDE	BOTTOM ELEVATION (ft)	BORING DEPTH (ft)
B-1	29°42'57.47"N	89°49'0.21"W	-2.028	40
B-2	29°42'48.83"N	89°49'46.78"W	-4.056	40
B-3	29°42'15.06"N	89°49'34.35"W	-2.205	30
B-4	29°41'58.07"N	89°50'26.16"W	-2.693	30
B-5	29°41'55.20"N	89°50'44.41"W	-4.902	30
B-6	29°41'32.59"N	89°51'20.45"W	-3.727	30



**TABLE 2.0: BORROW MATERIAL AREA**

SOIL BORING NUMBER	LATITUDE	LONGITUDE	BOTTOM ELEVATION (ft)	BORING DEPTH (ft)
B-7	29°42'47.50"N	89°50'46.88"W	-6.238	25
B-8	29°42'57.82"N	89°50'58.05"W	-6.52	25
B-9	29°42'49.26"N	89°50'58.64"W	-6.594	25
B-10	29°42'45.69"N	89°51'9.24"W	-5.921	25
B-11	29°42'37.99"N	89°51'14.67"W	-5.952	25
B-12	29°42'29.61"N	89°51'4.86"W	-5.606	25
B-13	29°42'38.83"N	89°51'2.19"W	-6.628	25
B-14	29°42'38.09"N	89°50'51.86"W	-6.09	25

**TABLE 3.0: CPTs in the Marsh Creation Area**

CPT NUMBER	LATITUDE	LONGITUDE	BOTTOM ELEVATION (ft)	BORING DEPTH (ft)
C-1	29°42'59.94"N	89°49'0.17"W	-2.328	44
C-2	29°42'37.67"N	89°49'12.75"W	-3.063	33
C-3	29°42'41.02"N	89°49'36.68"W	-8.421	32
C-4	29°42'48.83"N	89°49'46.78"W	-4.056	41
C-5	29°42'19.22"N	89°49'29.91"W	-1.314	32
C-6	29°42'9.81"N	89°49'53.96"W	-2.814	34
C-7	29°42'14.24"N	89°50'20.99"W	-4.189	40
C-8	29°41'58.07"N	89°50'26.16"W	-2.693	27
C-9	29°41'57.30"N	89°51'1.91"W	-4.191	41
C-10	29°41'50.55"N	89°51'28.30"W	-2.052	30
C-11	29°41'32.59"N	89°51'20.45"W	-3.727	31

### 3.0 LABORATORY TESTING

A laboratory testing program was conducted to determine pertinent engineering characteristics of the selected soil samples of subsurface materials. This program included:

- Visual description and classification and determination of the moisture content (ASTM D2216 Standard Test Method for Laboratory Determination of Water (Moisture) Content of Soil and Rock by Mass) on all soil samples;
- ASTM D4318 Standard Test Methods for Liquid Limit, Plastic Limit and Plasticity Index of Soils;
- Standard Test Methods for Determining the Amount of Material Finer than 75- $\mu\text{m}$  (No. 200) Sieve in Soils by Washing;
- ASTM D2850 Standard Test Method for Unconsolidated-Undrained Triaxial Compression test of Cohesive Soils;
- ASTM D854 Standard Test Methods for Specific Gravity of Soil Solids by Water Pycnometer, Low Stress Consolidation Test, Settling Properties of Fine-Grained Sediments (US Army Corps of Engineers Manual No. 1110-2-5027);
- ASTM D422 Standard Test Method for particle size analysis of soils;
- ASTM D2974 Standard Test Methods for Determining the Water (Moisture) Content, Ash Content, and Organic Material of Peat and Other Organic Soils; and
- ASTM D2435 Standard Test Method for One Dimensional Consolidation of Soil using Incremental Loading.

These test results are presented in the boring logs attached in Appendix B, C, D, E, H and I of this report.

### 4.0 CPT SOUNDING RESULTS

CPT Sounding data were processed using Dataforensics Rapid CPT, an add-in to the soil information database and presentation software gINT. Soil types were identified using the Robertson and Campanella (1986) cone tip pressure ( $q_t$ ) versus friction ratio (FR) non-normalized soil behavior type (SBT) correlation. This correlation generally provides a reasonable estimate of soil types as we observed them in our soil borings; however, published correlations do not always accurately reflect in-situ materials, especially for organic soils and sand/clay/silt mixtures. The Robertson and Campanella correlation (1986) was chosen because the results were reasonably consistent with our soil borings, and it relies on measurements that are consistent for each sounding. The  $N_{kt}$  value of 15 and  $N_c$  value of

20 was used to determine the soil profile. Shear strengths based on CPT tip pressure will be provided under separate cover and in our Geotechnical Engineering Report.

## 5.0 SITE CONDITIONS

Based on observations during our field exploration, the marsh creation area is predominantly marsh with access channels across the site. During the field exploration we measured water levels varying from 2-8 feet at the boring and CPT locations above the mudline.

## 6.0 SUB-SURFACE MATERIALS

The materials encountered at the borrow area exploration are primarily clay with silt and fine sand present from the mudline to a depth of about 25 feet, the material also consists of peat layers and organics.

The Marsh creation area exploration primarily consists of clays with interbedded sand and silt layers of varying thicknesses. The marsh area consists of peat and clay with high organic content in the top 2-6 feet from the mudline. The material consistency ranged from very soft to medium stiff to the termination depth of the boring.

## 7.0 VARIATIONS

Interpretations of soil conditions, as described in the soil boring logs are based on field and laboratory data described in this report. Variations in soil conditions are likely to exist between the boring locations, and also change in water elevations may occur with seasonal variations.

## 8.0 LIMITATIONS

The information presented in this report is based on field explorations completed for this study and judgments made by the A P S Engineering and Testing, LLC. This report is specific to this site and should not be used other than for the design of the Breton Landbridge Marsh Creation (West) project located in Plaquemines Parish, Louisiana. Within the limitations of scope, schedule, and budget, our services have been executed in accordance with generally accepted practices in the field of geotechnical engineering in this area at the time this report was prepared. No warranty or other conditions expressed or implied should be understood

**APPENDIX A**  
**(Boring Location Map)**



**Breton Landbridge Marsh Creation (West)**  
**(BS-0038)**  
**Plaquemines Parish, Louisiana**

**APS Engineering and Testing, LLC**  
*Geotechnical, Environmental, & Construction Materials Testing*

**Figure 1**  
**Boring Location Plan**

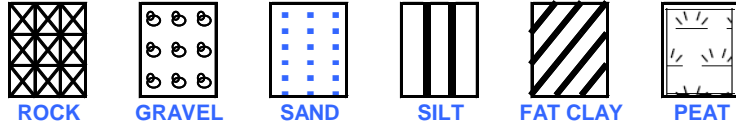
# **APPENDIX B**

## **( Boring Logs)**



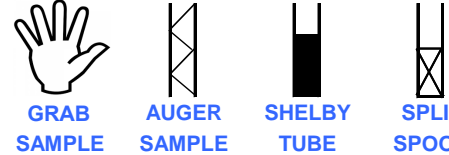
# KEY TO TERMS AND SYMBOLS USED ON LOGS

## SOIL TYPE



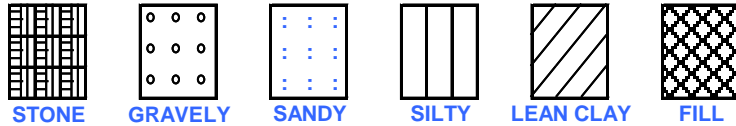
ROCK      GRAVEL      SAND      SILT      FAT CLAY      PEAT

## SAMPLER TYPE



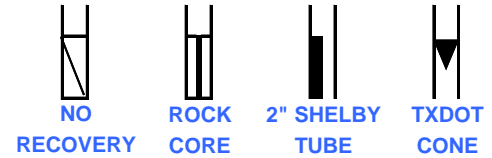
GRAB SAMPLE      AUGER SAMPLE      SHELBY TUBE      SPLIT SPOON

## MODIFIERS



STONE or CONCRETE      GRAVELY      SANDY      SILTY      LEAN CLAY      FILL

or CONCRETE



NO RECOVERY      ROCK CORE      2" SHELBY TUBE      TXDOT CONE

## UNIFIED SOIL CLASSIFICATION SYSTEM - ASTM D 2487 (1980)

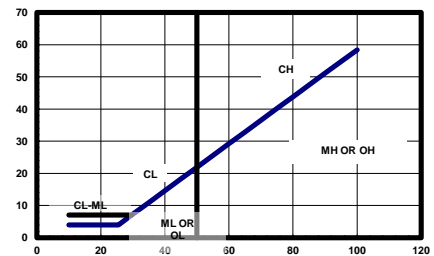
MAJOR DIVISIONS			LETTER SYMBOL	TYPICAL DESCRIPTIONS	
COARSE GRAINED SOILS LESS THAN 50% PASSING NO. 4 SIEVE	GRAVEL & GRAVELY SOILS LESS THAN 50% PASSING NO. 4 SIEVE	CLEAN GRAVEL (LITTLE OR NO FINES)	<b>GW</b>	WELL GRADED GRAVEL, GRAVEL-SAND MIXTURES WITH LITTLE OR NO FINES	
		GRAVEL (LITTLE OR NO FINES)	<b>GP</b>	POORLY GRADED GRAVEL, GRAVEL-SAND MIXTURES WITH LITTLE OR NO FINES	
	SANDS MORE THAN 50% PASSING NO. 4 SIEVE	W/ APPRECIABLE FINES	<b>GM</b>	SILTY GRAVEL, GRAVEL-SAND-SILT MIXTURES	
		CLEAN SANDS LITTLE FINES	<b>SW</b>	WELL GRADED SAND, GRAVELY SAND (LITTLE FINES)	
	SANDS WITH APPRECIABLE FINES	SANDS WITH LITTLE FINES	<b>SP</b>	POORLY GRADED SANDS, GRAVELY SAND (L.FINES)	
		SANDS WITH APPRECIABLE FINES	<b>SM</b>	SILTY SANDS, SAND-SILT MIXTURES	
	FINE GRAINED SOILS MORE THAN 50% PASSING NO. 200 SIEVE	SILTS AND CLAYS LIQUID LIMIT LESS THAN 50	CLAYEY SANDS, SAND-CLAY MIXTURES	<b>SC</b>	CLAYEY SANDS, SAND-CLAY MIXTURES
			WELL GRADED SAND, GRAVELY SAND (LITTLE FINES)	<b>ML</b>	INORGANIC SILTS & VERY FINE SANDS, ROCK FLOUR SILTY OR CLAYEY FINE SANDS OR CLAYEY SILT W/ LOW PI
			GRAVELY CLAYS, SANDY CLAYS, SILTY CLAYS	<b>CL</b>	INORGANIC CLAY OF LOW TO MEDIUM PI LEAN CLAY
		SILTS AND CLAYS LIQUID LIMIT GREATER THAN 50	ORGANIC SILTS & ORGANIC SILTY CLAYS OF LOW PI	<b>OL</b>	ORGANIC SILTS & ORGANIC SILTY CLAYS OF LOW PI
FINE SANDY OR SILTY SOILS, ELASTIC SILTS	<b>MH</b>		INORGANIC SILTS, MICACEOUS OR DIATOMACEOUS FINE SANDY OR SILTY SOILS, ELASTIC SILTS		
INORGANIC CLAYS OF HIGH PLASTICITY FAT CLAYS	<b>CH</b>		INORGANIC CLAYS OF HIGH PLASTICITY FAT CLAYS		
		ORGANIC CLAYS OF MED TO HIGH PI, ORGANIC SILT	<b>OH</b>	ORGANIC CLAYS OF MED TO HIGH PI, ORGANIC SILT	
HIGHLY ORGANIC SOIL		PEAT AND OTHER HIGHLY ORGANIC SOILS	<b>PT</b>	PEAT AND OTHER HIGHLY ORGANIC SOILS	
UNCLASSIFIED FILL MATERIALS		ARTIFICIALLY DEPOSITED AND OTHER UNCLASSIFIED SOILS AND MAN-MADE SOIL MIXTURES			

## CONSISTENCY OF COHESIVE SOILS

CONSISTENCY	UNCONFINED COMPRESSIVE STRENGTH IN TONS/FT <sup>2</sup>
VERY SOFT	0.0 TO 0.25
SOFT	0.25 TO 0.50
MEDIUM	0.50 TO 1.0
STIFF	1.0 TO 2.0
VERY STIFF	2.0 TO 4.0
HARD	> 4.0 OR 4.0+

## RELATIVE DENSITY - GRANULAR SOILS

CONSISTENCY	N-VALUE (BLOWS/FOOT)
VERY LOOSE	0-4
LOOSE	4-9
MEDIUM DENSE	10-29
DENSE	30-49
VERY DENSE	> 50 OR 50+



## ABBREVIATIONS

HP - HAND PENETROMETER      UC - UNCONFINED COMPRESSION TEST  
 TV - TORVANE      UU - UNCONSOLIDATED UNDRAINED TRIAXIAL  
 MV - MINIATURE VANE      CU - CONSOLIDATED UNDRAINED

▼ GROUNDWATER FIRST ENCOUNTERED  
 ▽ 24-HOUR GROUNDWATER READING

## CLASSIFICATION OF GRANULAR SOILS

U.S. STANDARD SIEVE SIZE(S)

	6"	3"	3/4"	4	10	40	200	
<b>BOUL- -DERS</b>	<b>COBBLES</b>	<b>GRAVEL</b>		<b>SAND</b>			<b>SILT OR CLAY</b>	<b>CLAY</b>
		<b>COARSE</b>	<b>FINE</b>	<b>COARSE</b>	<b>MEDIUM</b>	<b>FINE</b>		
	152	76.2	19.1	4.76	2.0	0.42	0.074	0.002
<b>GRAIN SIZE IN MM</b>								



APS Engineering and Testing, LLC.

# SUBSURFACE DIAGRAM

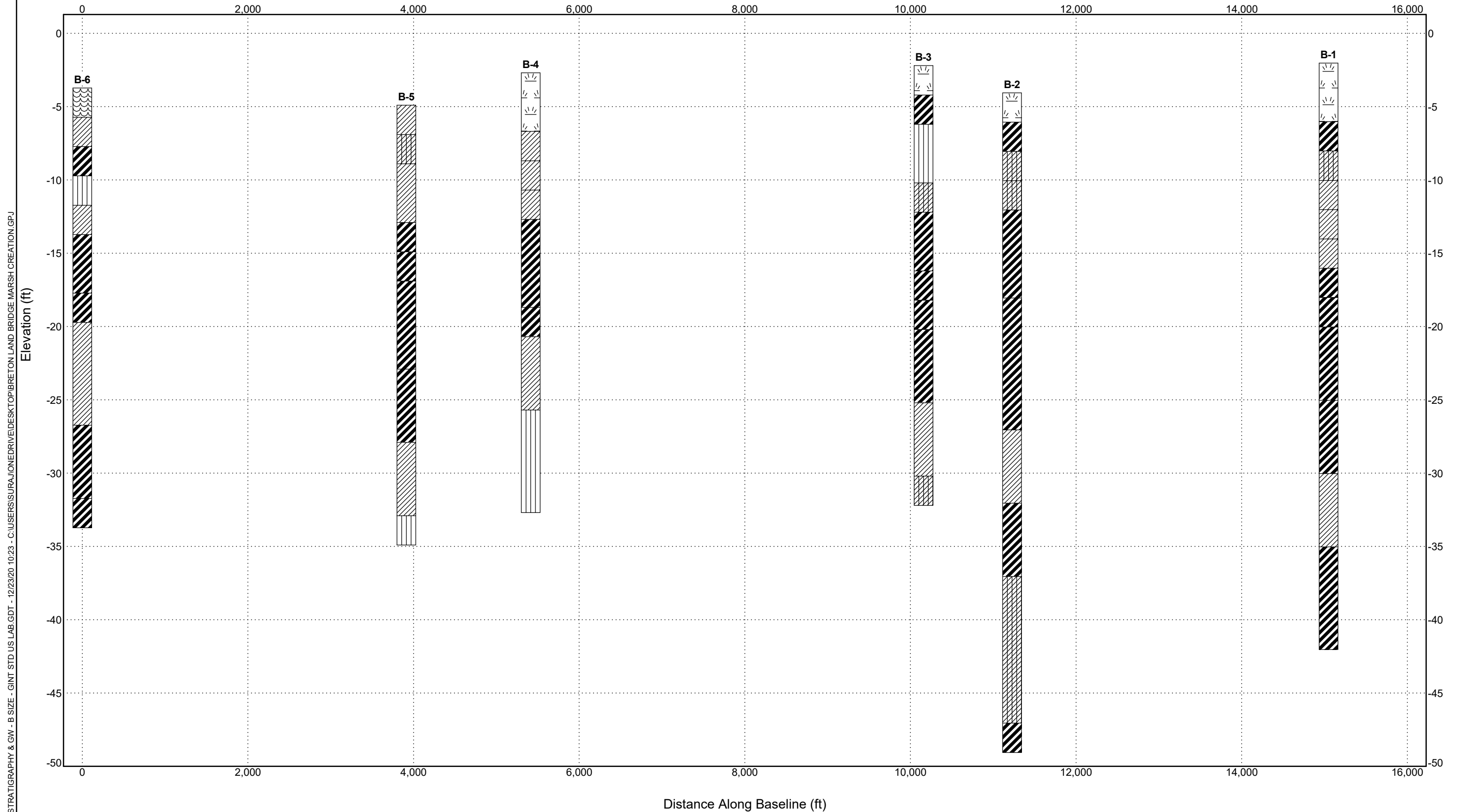
- USCS Peat
- USCS High Plasticity Clay
- USCS Low Plasticity Silty Clay
- USCS Silt
- USCS Low Plasticity Clay
- USCS High Plasticity Organic silt or clay

CLIENT CPRA

PROJECT NUMBER APS2008-G063

PROJECT NAME Breton Land Bridge Marsh Creation

PROJECT LOCATION Plaquemines parish



STRATIGRAPHY & GW - B SIZE - GINT STD US LAB.GDT - 12/23/20 10:23 - C:\USERS\SURAJ\ONE\DRIVE\DESKTOP\BRETON LAND BRIDGE MARSH CREATION.GPJ



APS Engineering and Testing, LLC.

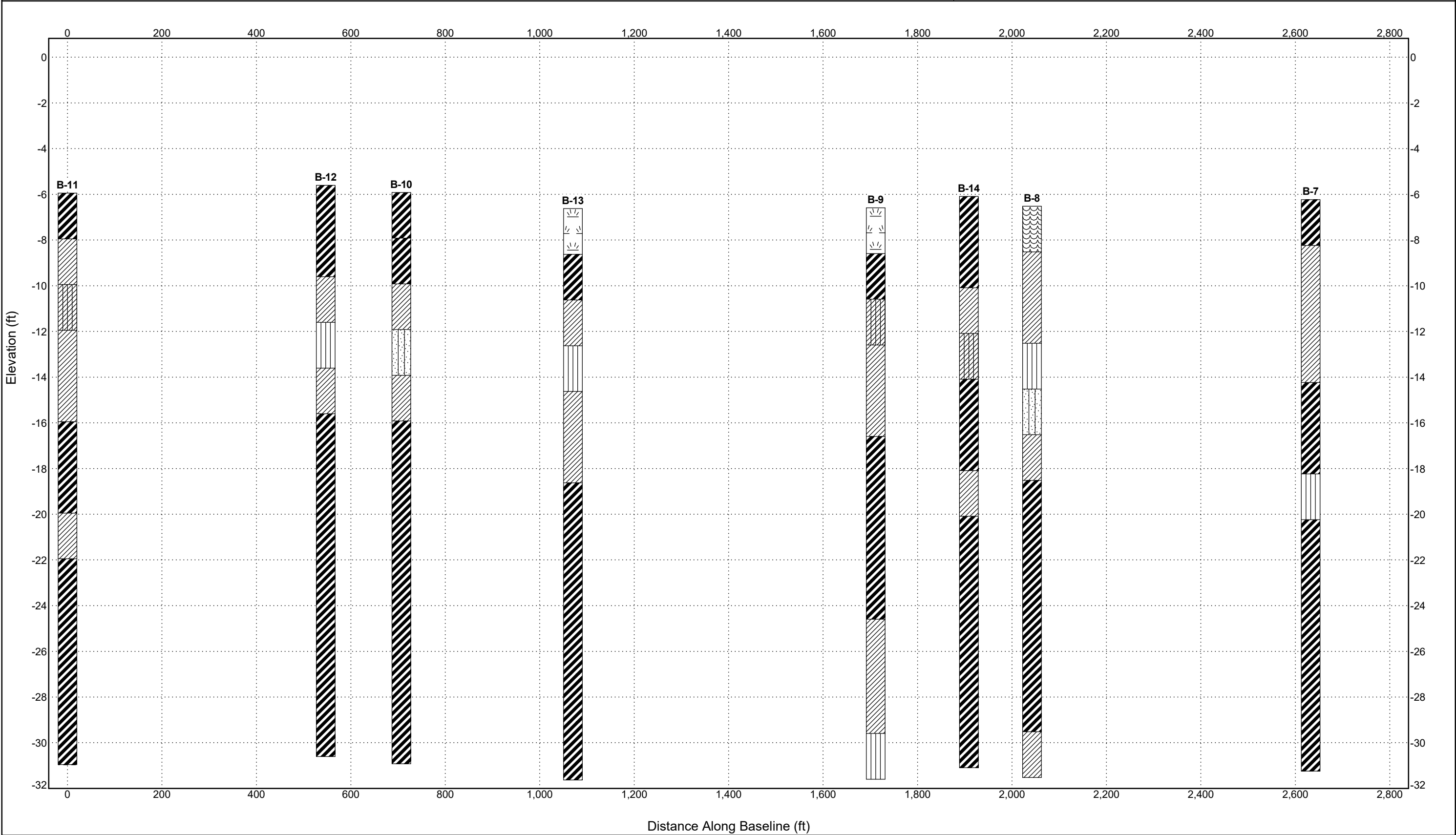
# SUBSURFACE DIAGRAM

CLIENT CPRA  
PROJECT NUMBER APS2008-G063

PROJECT NAME Breton Land Bridge Marsh Creation  
PROJECT LOCATION Plaquemines parish

- USCS High Plasticity Clay
- USCS Low Plasticity Clay
- USCS Silty Sand
- USCS Low Plasticity Silty Clay
- USCS Silt
- USCS Peat
- USCS High Plasticity Organic silt or clay

STRATIGRAPHY & GW - B SIZE - GINT STD US LAB.GDT - 12/23/20 10:22 - C:\USERS\JURAJ\ONE\DRIVE\DESKTOP\BRETON LAND BRIDGE MARSH CREATION.GPJ



# BORING LOG

**BORING NO.:** B-1

**PROJECT:** Breton Land Bridge Marsh Creation

**PROJECT LOCATION:** Plaquemines parish

**BORING LOCATION:** N445387.631 E3762240.514

**DATE DRILLED:** 8/12/2020

**WATER HEIGHT:** 1'3" feet

**GEOL/ENGR:** SMP

**PROJECT NO.:** APS2008-G063

**METHOD:** WET DRILLING

**BORING ELEVATION:** -2.028 feet

**DATE COMPLETED:** 08/12/2020

**WATER LEVEL DATE:** 08/12/2020

**DRILLER:** SC

DEPTH (FEET)	SAMPLE	COHESION (PSF)	Confining Pressure (PSI)	Moisture Content (%)	Dry Unit Weight (PCF)	LL	PI	Symbol	MATERIAL CLASSIFICATION
		68	0.8	879	6	980	298		Black Peat (PT) -@0.0'-2.0': Organics=74.6%
		270	1.6	756	7	873	315		Very Soft Gray Fat Clay (CH)
5		227	2.4	43	62	57	33		Soft Gray Silty Clay (CL-ML) -@ 6.0'-8.0': -200=85.7%
		323	3.2	38	86	31	5		Soft Gray Lean Clay (CL) -with fine sand
10		247	4.0	49	75	42	19		Medium Stiff Gray Lean Clay (CL) -with intermittent fine sand layers -@10.0'-12.0': Organics=2.9% -@10.0'-12.0': -200=95.8%
		540	4.8	66	63	43	22		Very Soft Gray Lean Clay (CL) -with fine sand -@12.0'-14.0': Organics=3.2% -@12.0'-14.0': -200=99.3%
		165	5.6	54	65	46	24		Very Soft Gray Fat Clay (CH) -@14.0'-16.0': Organics=3.9%
15		192	6.4	85	53	66	41		Soft Gray Fat Clay (CH) -@16.0'-18.0': Organics = 4.8%
		269	7.2	97	48	115	82		Very Soft Gray Fat Clay (CH) @18.0'-20.0': Organics = 4.2%
		185	8	94	49	89	65		Very Soft Gray Fat Clay (CH) @18.0'-20.0': Organics = 4.2%
20									

**COMMENTS:**

Shelby Tube

# BORING LOG

**BORING NO.:** B-1

**PROJECT:** Breton Land Bridge Marsh Creation

**PROJECT LOCATION:** Plaquemines parish

**BORING LOCATION:** N445387.631 E3762240.514

**DATE DRILLED:** 8/12/2020

**WATER HEIGHT:** 1'3" feet

**GEOL/ENGR:** SMP

**PROJECT NO.:** APS2008-G063

**METHOD:** WET DRILLING

**BORING ELEVATION:** -2.028 feet

**DATE COMPLETED:** 08/12/2020

**WATER LEVEL DATE:** 08/12/2020

**DRILLER:** SC

DEPTH (FEET)	SAMPLE	COHESION (PSF)	Confining Pressure (PSI)	Moisture Content (%)	Dry Unit Weight (PCF)	LL	PI	Symbol	MATERIAL CLASSIFICATION
25		291	10	111	44	165	135		Soft Gray Fat Clay (CH) -@23.0'-25.0': Organics = 5.7%
30		501	12	32	89	38	16		Medium Stiff Gray Lean Clay (CL) -with fine sand -@28.0'-30.0':-200=98.0%
35		306	14	50	72	61	35		Soft Gray Fat Clay (CH)  -@38.0'-40.0': Organics = 4.8%
40		325	16	65	61	94	65		
45									Boring terminated at 40 ft. Boring grouted on completion.

**COMMENTS:**

Shelby Tube

# BORING LOG

**BORING NO.:** B-2  
**PROJECT:** Breton Land Bridge Marsh Creation  
**PROJECT LOCATION:** Plaquemines parish  
**BORING LOCATION:** N444503.188 E3758202.135  
**DATE DRILLED:** 8/12/2020  
**WATER HEIGHT:** 3'6" feet  
**GEOL/ENGR:** SMP

**PROJECT NO.:** APS2008-G063  
**METHOD:** WET DRILLING  
**BORING ELEVATION:** -4.056 feet  
**DATE COMPLETED:** 08/12/2020  
**WATER LEVEL DATE:** 08/12/2020  
**DRILLER:** SC

DEPTH (FEET)	SAMPLE	COHESION (PSF)	Confining Pressure (PSI)	Moisture Content (%)	Dry Unit Weight (PCF)	LL	PI	Symbol	MATERIAL CLASSIFICATION
		179	0.8	594	10	621	462		Black Peat (PT) -@0.0'-2.0': Organics = 43.7%
		113	1.6	99	46	73	51		Very Soft Gray Fat Clay (CH)
5		279	2.4	46	75	31	6		Soft Gray Silty Clay (CL-ML) -@ 4.0'-6.0': -200=86.0%
		341	3.2	34	82	30	6		Soft Gray Silty Clay with Fine sand (CL-ML) -@ 6.0'-8.0': -200 = 80.3%
10		107	4.0	47	67	80	60		Very Soft Gray Fat Clay (CH) -with sand pockets -@ 8.0'-10.0': Organics = 3.4%
		213	4.8	50	70	53	29		
		193	5.6	99	46	77	58		-with sand lenses
15		274	6.4	105	46	101	72		Soft Gray Fat Clay (CH) -@14.0'-16.0': Organics = 3.2%
		288	7.2	92	49	129	93		-@ 16.0'-18.0': Organics = 3.6%
		395	8	86	48	103	80		-@ 18.0'-20.0': Organics = 8.7%
20									
25		380	10	56	69	40	21		Soft Gray Lean Clay (CL) -with intermittent fine sand layers -@ 23.0'-25.0': Organics=2.3%

**COMMENTS:**

Shelby Tube



# BORING LOG

**BORING NO.:** B-2

**PROJECT:** Breton Land Bridge Marsh Creation

**PROJECT LOCATION:** Plaquemines parish

**BORING LOCATION:** N444503.188 E3758202.135

**DATE DRILLED:** 8/12/2020

**WATER HEIGHT:** 3'6" feet

**GEOL/ENGR:** SMP

**PROJECT NO.:** APS2008-G063

**METHOD:** WET DRILLING

**BORING ELEVATION:** -4.056 feet

**DATE COMPLETED:** 08/12/2020

**WATER LEVEL DATE:** 08/12/2020

**DRILLER:** SC

DEPTH (FEET)	SAMPLE	COHESION (PSF)	Confining Pressure (PSI)	Moisture Content (%)	Dry Unit Weight (PCF)	LL	PI	Symbol	MATERIAL CLASSIFICATION
30		396	12	46	77	50	28		Soft Gray Fat Clay (CH) -with sand lenses -@ 28.0'-30.0': Organics=2.3% -@ 28.0'-30.0': -200 = 84.1%
35		593	14	30	91	NP	NP		Gray Silt (ML) -@33.0'-35.0': -200=91.3%
45		341	18	72	57	96	65		Soft Gray Fat Clay (CH) -@43.0'-45.0': Organics = 4.7 %
									Boring terminated at 45 ft. Boring grouted on completion.

**COMMENTS:**

Shelby Tube

# BORING LOG

**BORING NO.:** B-3

**PROJECT:** Breton Land Bridge Marsh Creation

**PROJECT LOCATION:** Plaquemines parish

**BORING LOCATION:** N441063.646 E3759287.337

**DATE DRILLED:** 8/15/2020

**WATER HEIGHT:** 1'2" feet

**GEOL/ENGR:** SMP

**PROJECT NO.:** APS2008-G063

**METHOD:** WET DRILLING

**BORING ELEVATION:** -2.205 feet

**DATE COMPLETED:** 08/15/2020

**WATER LEVEL DATE:** 08/15/2020

**DRILLER:** SC

DEPTH (FEET)	SAMPLE	COHESION (PSF)	Confining Pressure (PSI)	Moisture Content (%)	Dry Unit Weight (PCF)	LL	PI	Symbol	MATERIAL CLASSIFICATION
		88	0.8	476	12	533	406		Black Peat (PT) -@0.0'-2.0': Organics= 75.2%
		166	1.6	53	61	57	30		Very Soft Dark Gray Fat Clay (CH) -with sand pocket
5		363	2.4	33	88	NP	NP		Gray Silt with Sand (ML) -@4.0'-6.0': -200=77.9%
		1855	3.2	29	97	NP	NP		-@6.0'-8.0': -200=63.1%
		109	4.0	40	69	34	5		Very Soft Gray Sandy Silty Clay (CL-ML) -@8.0'-10.0': -200=65%
10		261	4.8	90	49	99	72		Soft Gray Fat Clay (CH) -@10.0'-12.0': Organics=3.7%
		297	5.6	67	57	110	79		-@12.0'-14.0': Organics=5.3%
15		239	6.4	85	51	114	82		Very Soft Gray fat Clay (CH) -@14.0'-16.0': Organics = 4.3%
		611	7.2	32	89	60	37		Medium Stiff Gray Fat Clay (CH) -with sand layer -@16.0'-18.0': Organics=2.0%
		289	8	50	71	81	58		Soft Gray Fat Clay (CH) -with sand layers and lenses -@18.0'-20.0': Organics=3.1%
20									

**COMMENTS:**

Shelby Tube

# BORING LOG

**BORING NO.:** B-3

**PROJECT:** Breton Land Bridge Marsh Creation

**PROJECT LOCATION:** Plaquemines parish

**BORING LOCATION:** N441063.646 E3759287.337

**DATE DRILLED:** 8/15/2020

**WATER HEIGHT:** 1'2" feet

**GEOL/ENGR:** SMP

**PROJECT NO.:** APS2008-G063

**METHOD:** WET DRILLING

**BORING ELEVATION:** -2.205 feet

**DATE COMPLETED:** 08/15/2020

**WATER LEVEL DATE:** 08/15/2020

**DRILLER:** SC

DEPTH (FEET)	SAMPLE	COHESION (PSF)	Confining Pressure (PSI)	Moisture Content (%)	Dry Unit Weight (PCF)	LL	PI	Symbol	MATERIAL CLASSIFICATION
25		352	10	40	78	44	24		Soft Gray Lean Clay (CL) -with fine sand and sand lenses -@23.0'-25.0': Organics=3.5% -@23.0'-25.0': -200=98.8%
30		1965	12	24	104	30	7		Very Stiff Gray Silty Clay (CL-ML) -with fine sand
35									Boring terminated at 30 ft. Boring grouted on completion.
40									
45									

**COMMENTS:**

Shelby Tube

# BORING LOG

**BORING NO.:** B-4

**PROJECT:** Breton Land Bridge Marsh Creation

**PROJECT LOCATION:** Plaquemines parish

**BORING LOCATION:** N439297.659 E3754741.153

**DATE DRILLED:** 8/15/2020

**WATER HEIGHT:** 2'9" feet

**GEOL/ENGR:** SMP

**PROJECT NO.:** APS2008-G063











**METHOD:** WET DRILLING

**BORING ELEVATION:** -2.693 feet

**DATE COMPLETED:** 08/15/2020

**WATER LEVEL DATE:** 08/15/2020

**DRILLER:** SC

DEPTH (FEET)	SAMPLE	COHESION (PSF)	Confining Pressure (PSI)	Moisture Content (%)	Dry Unit Weight (PCF)	LL	PI	Symbol	MATERIAL CLASSIFICATION
		149	0.8	692	9	574	385	 Black Peat (PT) - @0.0'-2.0': Organics=44.8%	
		56	1.6	618	9	478	349	 - @2.0'-4.0': Organics=42.9%	
5		191	2.4	50	69	49	29	 Very Soft Gray Lean Clay (CL) -with intermittent fine sand layers - @4.0'-6.0': Organics=2.7% - @4.0'-6.0': -200=98.0%	
		532	3.2	38	82	39	21	 Medium Stiff Gray Lean Clay (CL) -with intermittent fine sand layers - @6.0'-8.0': Organics=1.1% - @6.0'-8.0': -200=94.0%	
		248	4.0	51	73	36	18	 Very Soft Gray Lean Clay (CL) -with fine sand - @8.0'-10.0': Organics=2.7% - @8.0'-10.0': -200=94.1%	
10		244	4.8	48	68	52	31	 Very Soft Gray Fat Clay (CH) -@10.0'-12.0': Organics=2.8%	
		210	5.6	104	46	96	74	 -with sand lenses - @12.0'-14.0': Organics = 2.3%	
15		225	6.4	125	40	152	114	 - @14.0'-16.0': Organics = 5.5%	
		263	7.2	77	54	89	61	 Soft Gray Fat Clay (CH) - @16.0'-18.0': Organics=4.2%	
		591	8	30	90	38	19	 Medium Stiff Gray Lean Clay (CL) -with fine sand -@ 18.0'-20.0': Organics=2.0% -@ 18.0'-20.0': -200=90.4%	
20									

**COMMENTS:**

 Shelby Tube

# BORING LOG

**BORING NO.:** B-4

**PROJECT:** Breton Land Bridge Marsh Creation

**PROJECT LOCATION:** Plaquemines parish

**BORING LOCATION:** N439297.659 E3754741.153

**DATE DRILLED:** 8/15/2020

**WATER HEIGHT:** 2'9" feet

**GEOL/ENGR:** SMP

**PROJECT NO.:** APS2008-G063

**METHOD:** WET DRILLING

**BORING ELEVATION:** Surface Elevation: -2.693 feet

**DATE COMPLETED:** 08/15/2020

**WATER LEVEL DATE:** 08/15/2020

**DRILLER:** SC

DEPTH (FEET)	SAMPLE	COHESION (PSF)	Confining Pressure (PSI)	Moisture Content (%)	Dry Unit Weight (PCF)	LL	PI	Symbol	MATERIAL CLASSIFICATION
25		3264	10	26	97	NP	NP		Sandy Silt (ML) -@23.0'-25.0': Organics=1.0%
30		3428	12	29	95	NP	NP		-@28.0'-30.0': -200=69.0%
35									Boring terminated at 30 ft. Boring grouted on completion.
40									
45									

**COMMENTS:**

Shelby Tube

# BORING LOG

**BORING NO.:** B-5

**PROJECT:** Breton Land Bridge Marsh Creation

**PROJECT LOCATION:** Plaquemines parish

**BORING LOCATION:** N438977.843 E3753133.859

**DATE DRILLED:** 8/14/2020

**WATER HEIGHT:** 4' feet

**GEOL/ENGR:** SMP

**PROJECT NO.:** APS2008-G063











**METHOD:** WET DRILLING

**BORING ELEVATION:** -4.902 feet

**DATE COMPLETED:** 08/14/2020

**WATER LEVEL DATE:** 08/14/2020

**DRILLER:** SC

DEPTH (FEET)	SAMPLE	COHESION (PSF)	Confining Pressure (PSI)	Moisture Content (%)	Dry Unit Weight (PCF)	LL	PI	Symbol	MATERIAL CLASSIFICATION
		195	0.8	44	71	40	22		Very Soft Gray Lean Clay (CL) -with peat and fine sand -@0.0'-2.0': -200=96.3%
		1941	1.6	33	88	29	7		Very Stiff Gray Silty Clay (CL-ML) -with sand lenses -@2.0'-4.0': -200=87.6%
5		368	2.4	51	73	36	14		Soft Gray Lean Clay (CL) -with intermittent fine sand layers -@4.0'-6.0': -200=97.0%
		454	3.2	42	81	31	9		-with sand layers -@6.0'-8.0': -200=90.4%
		396	4.0	48	73	55	34		Soft Gray Fat Clay (CH) -with sand lenses
10		224	4.8	99	51	103	79		Very Soft Gray Fat Clay (CH) -@10.0'-12.0': Organics=4.9%
		341	5.6	78	52	95	67		Soft Gray Fat Clay (CH) -with sand lenses -@12.0'-14.0': Organics=5.0%
15		347	6.4	93	50	140	105		-@14.0'-16.0': Organics=4.1%
		374	7.2	58	67	76	50		
		84	8	65	63	88	62		Very Soft Gray Fat Clay (CH) -@18.0'-20.0': Organics=3.2%
20									

**COMMENTS:**

 Shelby Tube



# BORING LOG

**BORING NO.:** B-5

**PROJECT:** Breton Land Bridge Marsh Creation

**PROJECT LOCATION:** Plaquemines parish

**BORING LOCATION:** N438977.843 E3753133.859

**DATE DRILLED:** 8/14/2020

**WATER HEIGHT:** 4' feet

**GEOL/ENGR:** SMP

**PROJECT NO.:** APS2008-G063

**METHOD:** WET DRILLING

**BORING ELEVATION:** -4.902 feet

**DATE COMPLETED:** 08/14/2020

**WATER LEVEL DATE:** 08/14/2020

**DRILLER:** SC

DEPTH (FEET)	SAMPLE	COHESION (PSF)	Confining Pressure (PSI)	Moisture Content (%)	Dry Unit Weight (PCF)	LL	PI	Symbol	MATERIAL CLASSIFICATION
25		621	10	33	91	42	21		Medium Stiff Gray Lean Clay (CL) -with fine sand
30		1809	12	26	101	NP	NP		Very Stiff Gray Silt (ML) -@28.0'-30.0':-200=86.4%
35									Boring terminated at 30 ft. Boring grouted on completion.
40									
45									

**COMMENTS:**

Shelby Tube

# BORING LOG

**BORING NO.:** B-6

**PROJECT:** Breton Land Bridge Marsh Creation

**PROJECT LOCATION:** Plaquemines parish

**BORING LOCATION:** N436651.606 E3749986.02

**DATE DRILLED:** 8/14/2020

**WATER HEIGHT:** 3'10" feet

**GEOL/ENGR:** SMP

**PROJECT NO.:** APS2008-G063

**METHOD:** WET DRILLING

**BORING ELEVATION:** -3.727 feet

**DATE COMPLETED:** 08/14/2020

**WATER LEVEL DATE:** 08/14/2020

**DRILLER:** SC

DEPTH (FEET)	SAMPLE	COHESION (PSF)	Confining Pressure (PSI)	Moisture Content (%)	Dry Unit Weight (PCF)	LL	PI	Symbol	MATERIAL CLASSIFICATION
		116	0.8	203	23	173	134		Very Soft Dark Gray Organic Clay (OH) -@0.0'-2.0': Organics = 20.2%
		383	1.6	33	89	40	20		Soft Gray Lean Clay (CL) -with intermittent fine sand layers -@2.0'-4.0': -200=95.2%
5				82		76	55		Gray Fat Clay (CH) -with fine sand pockets
		311	3.2	42	80	NP	NP		Gray Silt with Sand (ML) -@6.0'-8.0': -200=77.0%
		248	4.0	30	83	47	23		Soft Gray Lean Clay (CL) -with fine sand and sand lenses
10		186	4.8	79	53	108	74		Very Soft Gray Fat Clay (CH) -with sand pocket -@10.0'-12.0': Organics = 2.4%
		220	5.6	71	55	113	76		-@12.0'-14.0': Organics = 4.2%
15		277	6.4	85	50	119	85		Soft Gray Fat Clay (CH)
		337	7.2	78	52	32	7		Soft Gray Lean Clay (CL) -with fine sand and sand layer -@16.0'-18.0': Organics=2.4% -@16.0'-18.0': -200=94.5%
20		428	8	32	84	38	17		-@18.0'-20.0': -200= 98.8%

**COMMENTS:**

Shelby Tube

# BORING LOG

**BORING NO.:** B-6

**PROJECT:** Breton Land Bridge Marsh Creation

**PROJECT LOCATION:** Plaquemines parish

**BORING LOCATION:** N436651.606 E3749986.02

**DATE DRILLED:** 8/14/2020

**WATER HEIGHT:** 3'10" feet

**GEOL/ENGR:** SMP

**PROJECT NO.:** APS2008-G063

**METHOD:** WET DRILLING

**BORING ELEVATION:** -3.727 feet

**DATE COMPLETED:** 08/14/2020

**WATER LEVEL DATE:** 08/14/2020

**DRILLER:** SC

DEPTH (FEET)	SAMPLE	COHESION (PSF)	Confining Pressure (PSI)	Moisture Content (%)	Dry Unit Weight (PCF)	LL	PI	Symbol	MATERIAL CLASSIFICATION
25		424	10	71	57	96	65		Soft Gray Fat Clay (CH) -with fine sand pockets -@23.0'-25.0': Organics=3.1%
30		202	12	69	60	81	56		Very Soft Gray Fat Clay (CH) -@28.0'-30.0': Organics=4.4%
35									Boring terminated at 30 ft. Boring grouted upon completion.
40									
45									

**COMMENTS:**

Shelby Tube

# BORING LOG

**BORING NO.:** B-7

**PROJECT:** Breton Land Bridge Marsh Creation

**PROJECT LOCATION:** Plaquemines parish

**BORING LOCATION:** N444258.877 E3752848.071

**DATE DRILLED:** 8/13/2020

**WATER HEIGHT:** 5'11" feet

**GEOL/ENGR:** SMP

**PROJECT NO.:** APS2008-G063

**METHOD:** WET DRILLING

**BORING ELEVATION:** -6.238 feet

**DATE COMPLETED:** 08/13/2020

**WATER LEVEL DATE:** 08/13/2020

**DRILLER:** SC

DEPTH (FEET)	SAMPLE	Moisture Content (%)	LL	PI	Symbol	MATERIAL CLASSIFICATION
		128	146	110		Gray Fat Clay (CH) -@0.0'-2.0': sand=6.1% ; silt = 69.4% ; clay=24.5% -@0.0'-2.0': Organics=6.4%
		36	37	19		Gray Lean Clay (CL) -with Fine Sand -@2.0'-4.0' : Sand = 2.6% ; Silt = 66.7% ; Clay = 30.7% -@4.0'-6.0' : Sand = 8.8% ; Silt = 78.8% ; Clay = 12.4%
5		37	39	20		-@6.0'-8.0' : Sand = 1.7% ; Silt = 66.1% ; Clay = 32.2%
		51	39	14		
		80	71	43		Gray Fat Clay (CH) -@8.0'-10.0' : Sand = 0.2% ; Silt = 39.5% ; Clay = 60.3%
10		37				
		28	NP	NP		Gray Silt with Sand (ML) -@12.0'-14.0': Sand=16.2% ; Silt = 67.4% ; Clay = 16.4 %
15		56	67	43		Gray Fat Clay (CH) -@14.0'-16.0' : Sand = 0.4% ; Silt = 35.8% ; Clay = 63.8%
		59	115	84		-@16.0'-18.0': Sand = 0.3% ; Silt = 23.0% ; Clay = 76.7% -@16.0'-18.0': Organics = 5.0%
		64	138	101		-@18.0'-20.0': Sand = 8.6% ; Silt = 41.5% ; Clay = 49.9% -@18.0'-20.0': Organics = 3.5 %
20						
		40	63	41		-@23.0'-25.0': Sand = 0.5% ; Silt = 51.9% ; Clay = 47.6%
25						
30						

**COMMENTS:**

Shelby Tube

# BORING LOG

**BORING NO.:** B-8

**PROJECT:** Breton Land Bridge Marsh Creation

**PROJECT LOCATION:** Plaquemines parish

**BORING LOCATION:** N445286.602 E3751849.341

**DATE DRILLED:** 8/13/2020

**WATER HEIGHT:** 6' feet

**GEOL/ENGR:** SMP

**PROJECT NO.:** APS2008-G063

**METHOD:** WET DRILLING

**BORING ELEVATION:** -6.52 feet

**DATE COMPLETED:** 08/13/2020

**WATER LEVEL DATE:** 08/13/2020

**DRILLER:** SC

DEPTH (FEET)	SAMPLE	Moisture Content (%)	LL	PI	Symbol	MATERIAL CLASSIFICATION
		96	150	113		Dark Gray Organic Clay (OH) -@0.0'-2.0': sand=7.7% ; silt = 49.4% ; clay=42.9% -@0.0'-2.0': Organics = 7.0%
		27	35	10		Gray Lean Clay (CL) -with fine sand -@2.0'-4.0' : Sand = 6.9% ; Silt =73.3% ; Clay = 19.8% -@2.0'-4.0': Organics=2.0% -@4.0'-6.0' : Sand = 15.8% ; Silt = 68.6% ; Clay = 15.6% -@4.0'-6.0':Organics=1.9%
5		50	31	8		
		27	28	NP		Gray Silt with Fine Sand (ML) -@6.0'-8.0' : Sand = 16.9% ; Silt = 68.7% ; Clay = 14.4%
		32	29	2		Gray Silty Sand (SM) -@8.0'-10.0' : Sand = 55.4% ; Silt = 38.1% ; Clay = 6.5% -@8.0'-10.0':Organics=0.8%
10		43	41	15		Gray Lean Clay (CL) -with fine sand -@10.0'-12.0' : Sand = 20.4% ; Silt = 63.1% ; Clay = 16.5%
		115	102	77		Gray Fat Clay (CH) -with fine sand ( hydro was performed on clay sand pocket) -@12.0'-14.0': Sand = 17.0% ; Silt = 43.1% ; Clay = 39.9 % -@12.0'-14.0':Organics=5.7% -@14.0'-16.0' : Sand = 0.7% ; Silt = 41.7% ; Clay = 57.6% - @14.0'-16.0':Organics=3.0%
15		63	81	57		
		68	128	96		-@16.0'-18.0': Sand = 0.6% ; Silt = 19.2% ; Clay = 80.2% - @16.0'-18.0':Organics=5.8%
		68	98	64		-@18.0'-20.0': Sand = 0.9% ; Silt = 27.7% ; Clay = 71.4% - @18.0'-20.0':Organics=3.3%
20						
		51	46	26		Gray Lean Clay (CL) -with Fine Sand -@23.0'-25.0': Sand = 1.9% ; Silt =26.7% ; Clay = 71.4%
25						
30						

**COMMENTS:**

Shelby Tube

# BORING LOG

**BORING NO.:** B-9

**PROJECT:** Breton Land Bridge Marsh Creation

**PROJECT LOCATION:** Plaquemines parish

**BORING LOCATION:** N444421.615 E3751809.854

**DATE DRILLED:** 8/13/2020

**WATER HEIGHT:** 6' feet

**GEOL/ENGR:** SMP

**PROJECT NO.:** APS2008-G063

**METHOD:** WET DRILLING

**BORING ELEVATION:** -6.594 feet

**DATE COMPLETED:** 08/13/2020

**WATER LEVEL DATE:** 08/13/2020

**DRILLER:** SC

DEPTH (FEET)	SAMPLE	Moisture Content (%)	LL	PI	Symbol	MATERIAL CLASSIFICATION
		122	476	390		Black Peat (PT) -@0.0'-2.0': Sand = 1.5% ; Silt = 62.0% ; Clay = 36.5% -@0.0'-2.0':Organics=29.2%
		52	91	64		Gray Fat Clay (CH) -@2.0'-4.0': Sand = 1.4% ; Silt = 50.1% ; Clay = 48.5% -@2.0'-4.0':Organics=3.8%
5		26	27	4		Gray Silty Clay with Sand (CL-ML) -@4.0'-6.0' : Sand = 24% ; Silt = 60.5 % ; Clay = 15.5 %
		29	33	8		Gray Lean Clay (CL) -with fine sand -@6.0'-8.0': Sand = 15.5% ; Silt = 65.0 % ; Clay = 19.5% -@8.0'-10.0': Sand = 1.2% ; Silt = 64.1% ; Clay = 34.7 %
10		63	120	85		Gray Fat Clay (CH) -@10.0'-12.0': Sand = 7.8% ; Silt = 26.7% ; Clay = 65.5% -@10.0'-12.0': Organics=3.7% -@12.0'-14.0': Sand = 0.8% ; Silt = 62.9% ; Clay = 36.3%
		64	57	36		
15		67	98	70		-@14.0'-16.0': Sand = 0.2% ; Silt = 20.3% ; Clay = 79.5% -@14.0'-16.0':Organics=4.5%
		59	91	63		-@16.0'-18.0': Sand = 0.2% ; Silt =24.6% ; Clay = 75.2% -@16.0'-18.0':Organics=3.5%
20		45	43	22		Gray Lean Clay(CL) -@18.0'-20.0': Sand = 0.3% ; Silt = 20.2% ; Clay =79.5%
25		27	NP	NP		Gray Silt with Sand (ML) -@23.0'-25.0': Sand = 23.4% ; Silt = 64.4% ; Clay = 12.2%
30						

**COMMENTS:**

Shelby Tube

# BORING LOG

**BORING NO.:** B-10

**PROJECT:** Breton Land Bridge Marsh Creation

**PROJECT LOCATION:** Plaquemines parish

**BORING LOCATION:** N444047.405 E3750877.04

**DATE DRILLED:** 8/14/2020

**WATER HEIGHT:** 5'9" feet

**GEOL/ENGR:** SMP

**PROJECT NO.:** APS2008-G063












**METHOD:** WET DRILLING

**BORING ELEVATION:** -5.921 feet

**DATE COMPLETED:** 08/14/2020

**WATER LEVEL DATE:** 08/14/2020

**DRILLER:** SC

DEPTH (FEET)	SAMPLE	Moisture Content (%)	LL	PI	Symbol	MATERIAL CLASSIFICATION
		215	146	110		Dark Gray Fat Clay (CH) -@0.0'-2.0': Sand = 3.2% ; Silt = 40.1% ; Clay = 56.7% -@0.0'-2.0': Organics = 12.6%
		54	52	29		Gray Fat Clay (CH) -@2.0'-4.0': Sand = 1.3% ; Silt = 62.5% ; Clay = 36.2% -@2.0'-4.0': Organics = 2.7%
5		57	32	10		Gray Lean Clay (CL) -@4.0'-6.0': Sand = 2.5% ; Silt = 81.8% ; Clay = 15.7% -@4.0'-6.0': Organics = 1.6%
		52	NP	NP		Silty Sand (SM) -@6.0'-8.0': Sand = 80.6% ; Silt = 14.6% ; Clay = 4.8% -@6.0'-8.0': Organics = 0.7%
10		53	48	26		Gray Lean Clay (CL) - with Fine Sand -@8.0'-10.0': Sand = 19.1% ; Silt = 69.1% ; Clay = 11.8% -@8.0'-10.0': Organics = 2.9%
		62	99	67		Gray Fat Clay (CH) -@10.0'-12.0': Sand = 11.0% ; Silt = 40.3% ; Clay = 48.7% -@10.0'-12.0': Organics = 3.3%
		116	205	157		-@12.0'-14.0': Sand = 0.2% ; Silt = 67.6% ; Clay = 32.2% -@12.0'-14.0': Organics = 11.1%
15		90	101	67		-@14.0'-16.0': Sand = 0.3% ; Silt = 28.6% ; Clay = 71.1% -@14.0'-16.0': Organics = 4.6%
		82	103	67		-@16.0'-18.0': Sand = 0.8% ; Silt = 25.9% ; Clay = 73.3% -@16.0'-18.0': Organics = 6.1%
20		64	93	64		-@18.0'-20.0': Sand = 0.1% ; Silt = 24.6% ; Clay = 75.3% -@18.0'-20.0': Organics = 4.2%
25		52	61	45		-@23.0'-25.0': Sand = 0.1% ; Silt = 49.7% ; Clay = 50.2%

**COMMENTS:**  
 Shelby Tube

# BORING LOG

**BORING NO.:** B-11

**PROJECT:** Breton Land Bridge Marsh Creation

**PROJECT LOCATION:** Plaquemines parish

**BORING LOCATION:** N443266.916 E3750407.228

**DATE DRILLED:** 8/14/2020

**WATER HEIGHT:** 6' feet

**GEOL/ENGR:** SMP

**PROJECT NO.:** APS2008-G063












**METHOD:** WET DRILLING

**BORING ELEVATION:** -5.952 feet

**DATE COMPLETED:** 08/14/2020

**WATER LEVEL DATE:** 08/14/2020

**DRILLER:** SC

DEPTH (FEET)	SAMPLE	Moisture Content (%)	LL	PI	Symbol	MATERIAL CLASSIFICATION
		175	95	63		Black Sandy Fat Clay (CH) -@0.0'-2.0': Sand = 37.5% ; Silt = 46.1% ; Clay = 16.4% -@0.0'-2.0': Organics = 5.0%
		38	37	15		Gray Lean Clay (CL) -with Fine Sand -@2.0'-4.0': Sand = 8.8% ; Silt = 61.6% ; Clay =29.6% -@2.0'-4.0':Organics=2.9%
5		34	29	7		Gray Sity clay (CL-ML) -@4.0'-6.0':Organics=2.4% -@4.0'-6.0':-200=82.7%
		36	43	22		Gray Lean Clay (CL) -with Fine Sand -@6.0'-8.0': Sand = 9.1% ; Silt = 59% ; Clay= 31.9% -@6.0'-8.0':Organics=2.5%
		21	40	17		-@8.0'-10.0': Sand = 1% ; Silt = 40.8% ; Clay= 58.2% -@8.0'-10.0':Organics=2.5%
10		67	99	67		Gray Fat Clay (CH) -with Fine Sand -@10.0'-12.0': Sand = 9.6% ; Silt = 46.4% ; Clay= 44% -@10.0'-12.0':Organics=4.1%
		70	115	82		-@12.0'-14.0': Sand = 0.4% ; Silt = 20.2% ; Clay= 79.4% -@12.0'-14.0':Organics=4.3%
15		44	49	27		Gray Sandy Lean Clay (CL) -@14.0'-16.0': Sand = 38.8% ; Silt = 36.3% ; Clay= 24.9% -@14.0'-16.0':Organics=2.2%
		51	98	75		Gray Fat Clay (CH) -with Fine Sand -@16.0'-18.0': Sand = 6.5% ; Silt = 57.9% ; Clay= 35.6% -@16.0'-18.0':Organics=3.0%
		53	93	72		-@18.0'-20.0': Sand = 0.6% ; Silt =75.9% ; Clay= 23.5% -@18.0'-20.0'= Organics=5.3%
20						
		48	99	67		-@23.0'-25.0': Sand = 0.3% ; Silt = 18.4% ; Clay = 81.3%
25						
30						

**COMMENTS:**  
 Shelby Tube



# BORING LOG

**BORING NO.:** B-12

**PROJECT:** Breton Land Bridge Marsh Creation

**PROJECT LOCATION:** Plaquemines parish

**BORING LOCATION:** N442431.991 E3751290.054

**DATE DRILLED:** 8/14/2020

**WATER HEIGHT:** 5'7" feet

**GEOL/ENGR:** SMP

**PROJECT NO.:** APS2008-G063

**METHOD:** WET DRILLING

**BORING ELEVATION:** -5.606 feet

**DATE COMPLETED:** 08/14/2020

**WATER LEVEL DATE:** 08/14/2020

**DRILLER:** SC

DEPTH (FEET)	SAMPLE	Moisture Content (%)	LL	PI	Symbol	MATERIAL CLASSIFICATION
		106	115	82		Gray Fat Clay (CH) -@0.0'-2.0': Sand = 1.5% ; Silt = 47.7% ; Clay = 50.8% -@0.0'-2.0': Organics = 11.2%
		67	91	59		-@2.0'-4.0': Sand = 1.0% ; Silt = 28% ; Clay = 71% -@2.0'-4.0': Organics=2.9%
5		35	34	10		Gray Lean Clay (CL) -with fine sand -@4.0'-6.0': Sand = 26.3% ; Silt = 57.9% ; Clay= 15.8% -@4.0'-6.0': Organics=1.4%
		28	NP	NP		Gray Silt with Sand (ML) -@6.0'-8.0': Sand = 29.2% ; Silt = 58.4% ; Clay= 12.4% -@6.0'-8.0': Organics=2.4 %
10		51	31	11		Gray Lean Clay (CL) -with Fine Sand -@8.0'-10.0': Sand = 9.7% ; Silt = 68.9% ; Clay= 21.4% -@8.0'-10.0': Organics=2.0%
		55	52	29		Gray Fat Clay (CH) -@10.0'-12.0': Sand = 0.5% ; Silt = 59.1% ; Clay= 40.4% -@10.0'-12.0': Organics=2.9%
		64	82	57		-@12.0'-14.0': Sand =13.1% ; Silt =24.7% ; Clay= 62.2% -@12.0'-14.0': Organics=4.4%
15		68	98	70		-@14.0'-16.0': Sand =0.9% ; Silt = 58.3% ; Clay= 40.8% -@14.0'-16.0': Organics=3.9%
		64	124	87		-@16.0'-18.0': Sand = 0.1% ; Silt = 25.6% ; Clay= 74.3% -@16.0'-18.0': Organics=6.0%
20		59	95	65		-@18.0'-20.0': Sand = 0.1% ; Silt =36.4% ; Clay= 63.5% -@18.0'-20.0'= Organics=10.6%
		61	89	59		-@23.0'-25.0': Sand = 0% ; Silt = 26% ; Clay = 74% -@23.0'-25.0': Organics=4.4%
30						

**COMMENTS:**

Shelby Tube

# BORING LOG

**BORING NO.:** B-13

**PROJECT:** Breton Land Bridge Marsh Creation

**PROJECT LOCATION:** Plaquemines parish

**BORING LOCATION:** N443363.505 E3751510.453

**DATE DRILLED:** 8/13/2020

**WATER HEIGHT:** 6'6" feet

**GEOL/ENGR:** SMP

**PROJECT NO.:** APS2008-G063

**METHOD:** WET DRILLING

**BORING ELEVATION:** -6.628 feet

**DATE COMPLETED:** 08/13/2020

**WATER LEVEL DATE:** 08/13/2020

**DRILLER:** SC

DEPTH (FEET)	SAMPLE	Moisture Content (%)	LL	PI	Symbol	MATERIAL CLASSIFICATION
		391	432	122		Black Peat (PT) -@0.0'-2.0': Sand = 4.9% ; Silt = 76.6% ; Clay = 18.5% -@0.0'-2.0': Organics = 13.1%
		104	93	67		Gray Fat Clay (CH) -@2.0'-4.0': Sand = 0.4% ; Silt = 41.2% ; Clay = 58.4% -@2.0'-4.0': Organics=5.0%
5		36	47	27		Gray Lean Clay (CL) -with Fine Sand -@4.0'-6.0': Sand =7.8% ; Silt = 52.5% ; Clay= 39.7% -@4.0'-6.0':Organics=2.3%
		26	NP	NP		Gray Sandy Silt (ML) -@6.0'-8.0': Sand = 31% ; Silt =41.6% ; Clay= 27.4% -@6.0'-8.0':Organics=0.6 %
10		38	40	21		Gray Lean Clay (CL) -with Fine Sand -@8.0'-10.0': Sand =3.4% ; Silt =57.1% ; Clay= 39.5% -@8.0'-10.0':Organics=1.8% -@10.0'-12.0': Sand = 1.2% ; Silt =82% ; Clay=16.8% -@10.0'-12.0':Organics=1.8%
		52	47	21		
15		94	106	74		Gray Fat Clay (CH) -@12.0'-14.0': Sand =4.3% ; Silt =34.3% ; Clay= 61.4% -@12.0'-14.0':Organics=3.4%
		65	94	62		-@14.0'-16.0': Sand =0.4% ; Silt = 62% ; Clay= 37.6% -@14.0'-16.0':Organics=9.0%
		102	128	95		-@16.0'-18.0': Sand = 2.5% ; Silt = 23.9% ; Clay= 73.6% -@16.0'-18.0':Organics=3.7%
20		80	57	39		-@18.0'-20.0': Sand = 0.4% ; Silt =15.4% ; Clay= 84.2% -@18.0'-20.0'= Organics=3.0%
		68	94	70		-@23.0'-25.0': Sand = 0.4% ; Silt = 36.4% ; Clay = 63.2% -@23.0'-25.0':Organics=3.6%
30						











**COMMENTS:**

Shelby Tube

# BORING LOG

**BORING NO.:** B-14  
**PROJECT:** Breton Land Bridge Marsh Creation  
**PROJECT LOCATION:** Plaquemines parish  
**BORING LOCATION:** N443301.969 E3752423.841  
**DATE DRILLED:** 8/14/2020  
**WATER HEIGHT:** 7'4" feet  
**GEOL/ENGR:** SMP

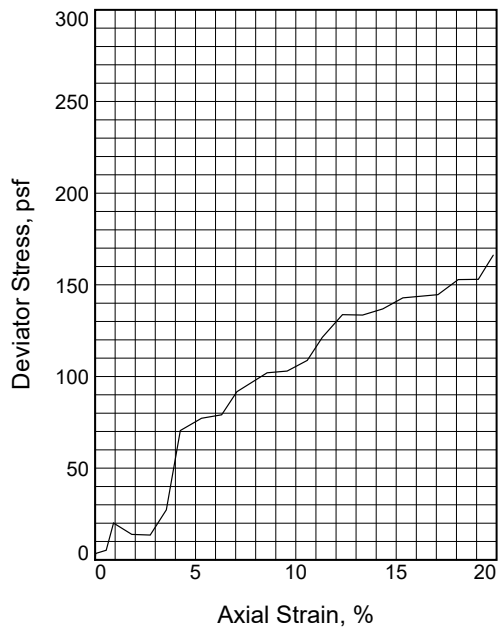
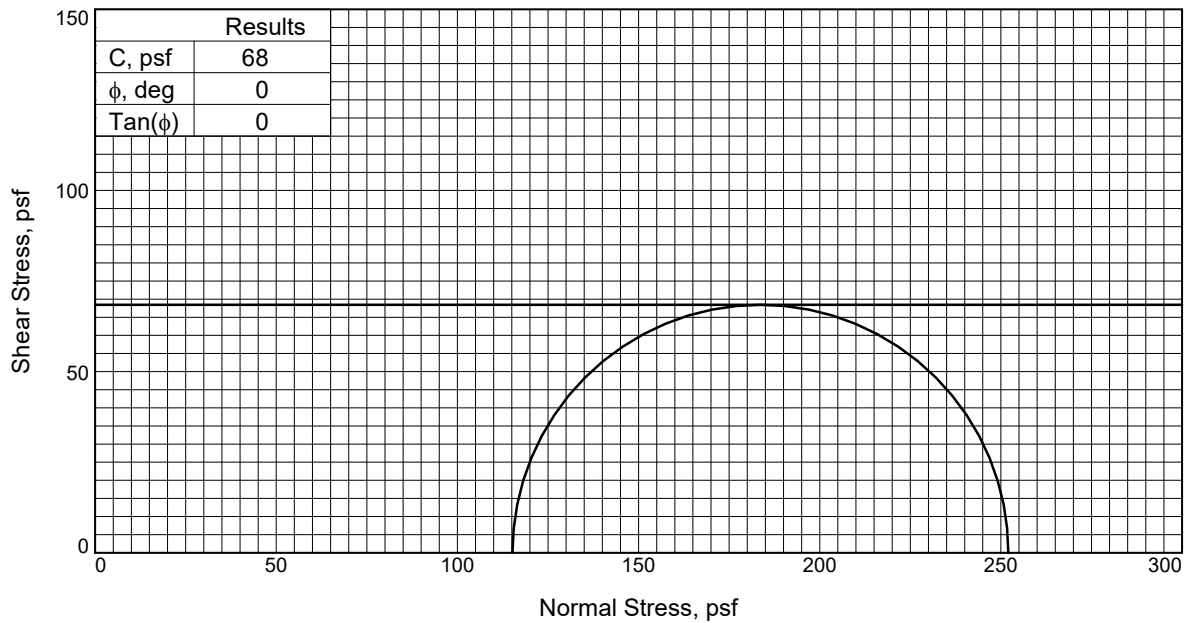
**PROJECT NO.:** APS2008-G063  
**METHOD:** WET DRILLING  
**BORING ELEVATION:** -6.09 feet  
**DATE COMPLETED:** 08/14/2020  
**WATER LEVEL DATE:** 08/14/2020  
**DRILLER:** SC

DEPTH (FEET)	SAMPLE	Moisture Content (%)	LL	PI	Symbol	MATERIAL CLASSIFICATION
		87	90	54		Gray Fat Clay (CL) -@0.0'-2.0': Sand = 20.3% ; Silt =68% ; Clay = 11.7% -@0.0'-2.0': Organics = 9.2% -@2.0'-4.0': Sand = 0.4% ; Silt = 47% ; Clay =52.6% -@2.0'-4.0':Organics=3.1%
		51	93	65		Gray Lean Clay (CL) -with Fine Sand -@4.0'-6.0': Sand =9.8% ; Silt = 73.9% ; Clay= 16.3% -@4.0'-6.0':Organics=2.1%
5		37	28	9		Gray Silty Clay with Sand (CL-ML) -@6.0'-8.0': Sand =23.5% ; Silt =67.4% ; Clay= 9.1% -@6.0'-8.0':Organics=1.0%
		45	30	5		Gray Fat Clay (CH) -@8.0'-10.0': Sand =6.6% ; Silt =50.2% ; Clay= 43.2% -@8.0'-10.0':Organics=3.0%
10		90	104	70		-@10.0'-12.0': Sand = 3.7% ; Silt =78.4% ; Clay=17.9% -@10.0'-12.0':Organics=2.8%
		53	60	36		Gray Lean Clay (CL) -with Fine Sand -@12.0'-14.0': Sand =9.7% ; Silt =70.2% ; Clay= 20.1% -@12.0'-14.0':Organics=2.6%
15		67	83	62		Gray Fat Clay (CH) -@14.0'-16.0': Sand =0.2% ; Silt =21.7% ; Clay= 78.1% -@14.0'-16.0':Organics=4.4%
		73	98	69		-@16.0'-18.0': Sand = 0.5% ; Silt = 31.8% ; Clay= 67.7% -@16.0'-18.0':Organics=4.6%
		77	134	95		-@18.0'-20.0': Sand = 0.5% ; Silt =42.2% ; Clay= 57.3% -@18.0'-20.0': Organics=3.9%
20						
		60	76	56		-@23.0'-25.0': Sand = 0.1% ; Silt = 72.2% ; Clay = 27.7% -@23.0'-25.0':Organics=3.1%
25						
30						

**COMMENTS:**

 Shelby Tube

**APPENDIX C**  
**( Unconsolidated**  
**Undrained Test Reports)**



Sample No.	1	
Initial	Water Content, %	879.1
	Dry Density, pcf	6.4
	Saturation, %	98.6
	Void Ratio	10.7910
	Diameter, in.	2.72
At Test	Height, in.	6.11
	Water Content, %	879.1
	Dry Density, pcf	6.4
	Saturation, %	98.6
	Void Ratio	10.7910
Diameter, in.	2.72	
Height, in.	6.11	
Strain at peak, %	14.3	
Back Pressure, psi	0.00	
Cell Pressure, psi	0.80	
Fail. Stress, psf	137	
Ult. Stress, psf	137	
$\sigma_1$ Failure, psf	252	
$\sigma_3$ Failure, psf	115	

**Type of Test:**

Unconsolidated Undrained

**Sample Type:** Undisturbed

**Description:** Very soft black peat

**LL= 980      PL= 682      PI= 298**

**Specific Gravity= 1.21**

**Remarks:** Failure type : Bulge  
Failure limit to 15%

**Client:** CPRA

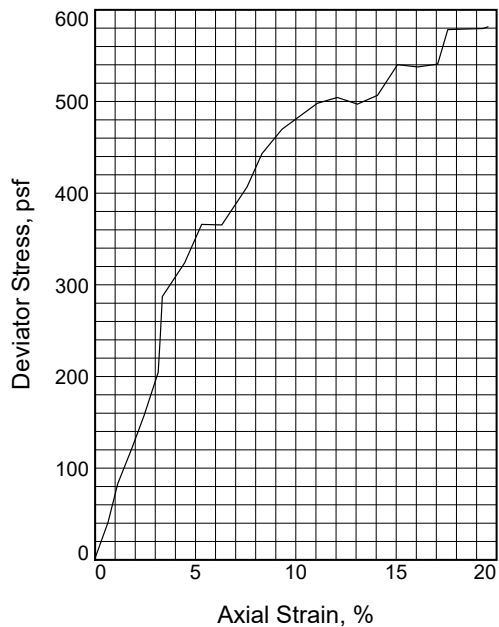
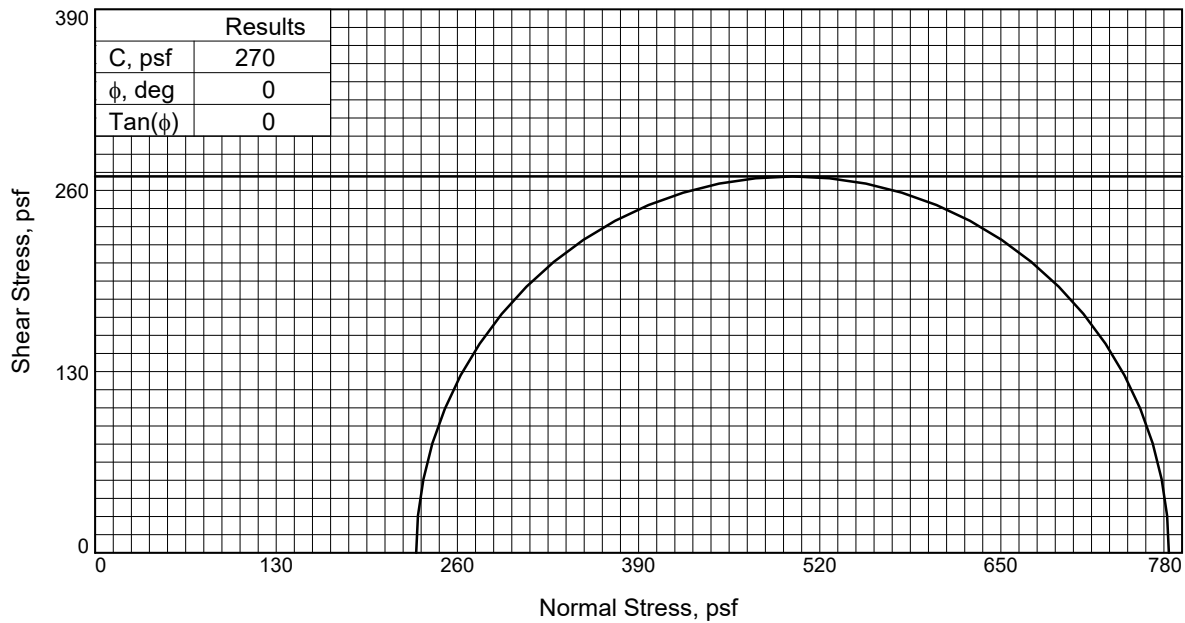
**Project:** BRETON LANDBRIDGE MARSH CREATION

**Source of Sample:** B-1      **Depth:** 0-2

**Sample Number:** 1

**Proj. No.:** APS2008-G063      **Date Sampled:** 8-12-2020





Sample No.	1	
Initial	Water Content, %	755.6
	Dry Density, pcf	7.4
	Saturation, %	94.0
	Void Ratio	21.6955
	Diameter, in.	2.75
At Test	Height, in.	5.73
	Water Content, %	755.6
	Dry Density, pcf	7.4
	Saturation, %	94.0
	Void Ratio	21.6955
Diameter, in.	2.75	
Height, in.	5.73	
Strain at peak, %	15.1	
Back Pressure, psi	0.00	
Cell Pressure, psi	1.60	
Fail. Stress, psf	540	
Ult. Stress, psf	540	
$\sigma_1$ Failure, psf	771	
$\sigma_3$ Failure, psf	230	

**Type of Test:**

Unconsolidated Undrained

**Sample Type:** Undisturbed

**Description:** Soft black peat

LL= 873      PL= 558      PI= 315

**Assumed Specific Gravity=** 2.7

**Remarks:** Failure type : Bulge

Failure limit to 15%

**Client:** CPRA

**Project:** BRETON LANDBRIDGE MARSH CREATION

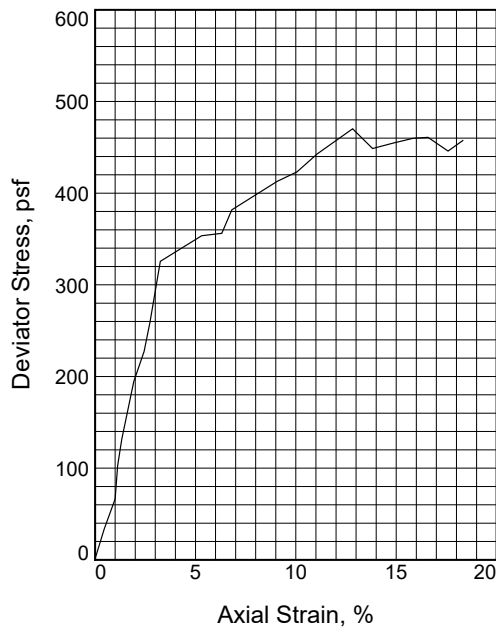
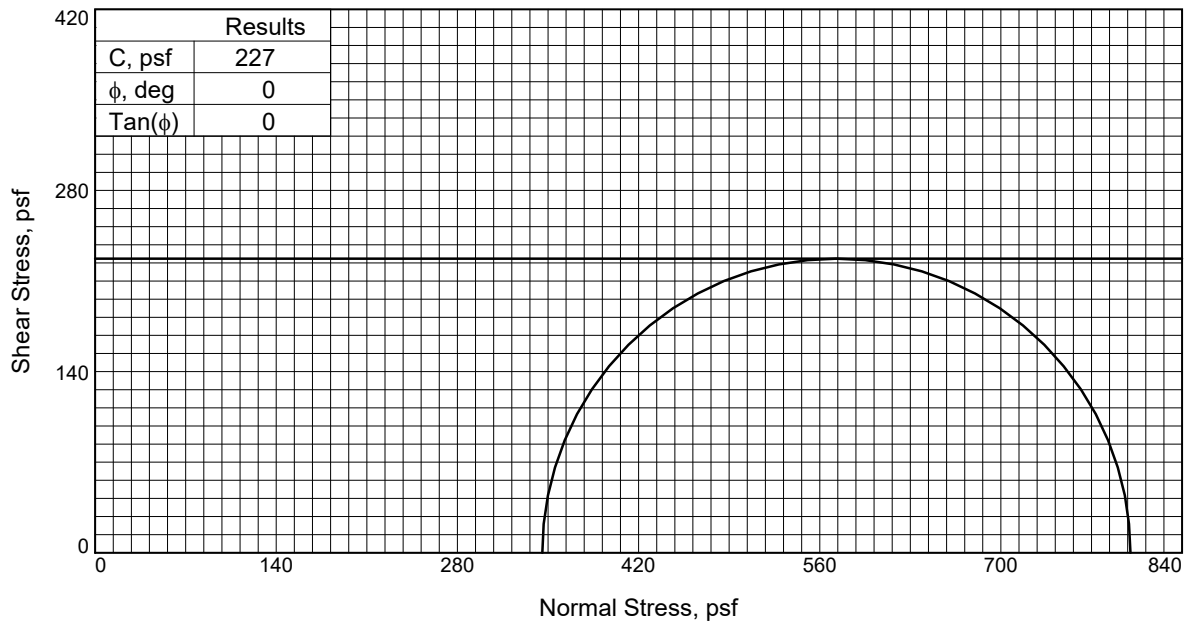
**Source of Sample:** B-1      **Depth:** 2-4

**Sample Number:** 2

**Proj. No.:** APS2008-G063

**Date Sampled:** 8-12-2020





Sample No.	1	
Initial	Water Content, %	43.4
	Dry Density, pcf	62.4
	Saturation, %	72.3
	Void Ratio	1.5015
	Diameter, in.	2.72
	Height, in.	5.78
At Test	Water Content, %	43.4
	Dry Density, pcf	62.4
	Saturation, %	72.3
	Void Ratio	1.5015
	Diameter, in.	2.72
	Height, in.	5.78
Strain at peak, %	14.8	
Back Pressure, psi	0.00	
Cell Pressure, psi	2.40	
Fail. Stress, psf	455	
Ult. Stress, psf	455	
$\sigma_1$ Failure, psf	800	
$\sigma_3$ Failure, psf	346	

**Type of Test:**

Unconsolidated Undrained

**Sample Type:** Undisturbed

**Description:** Very Soft Gray Fat Clay (CH)

**LL= 57      PL= 24      PI= 33**

**Specific Gravity= 2.5**

**Remarks:** Failure type : Bulge

Failure limit to 15%

**Client:** CPRA

**Project:** BRETON LANDBRIDGE MARSH CREATION

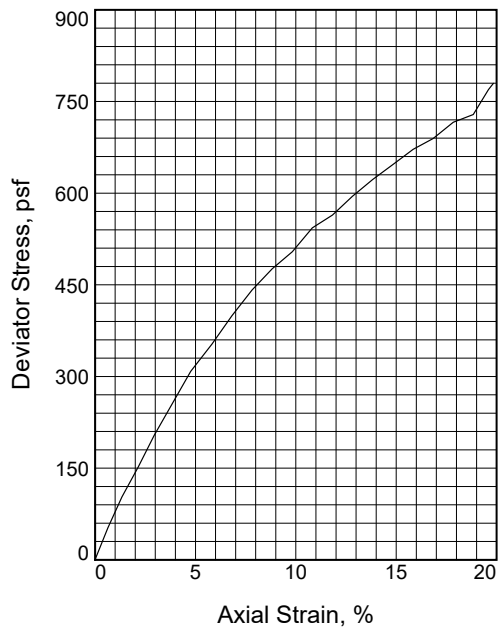
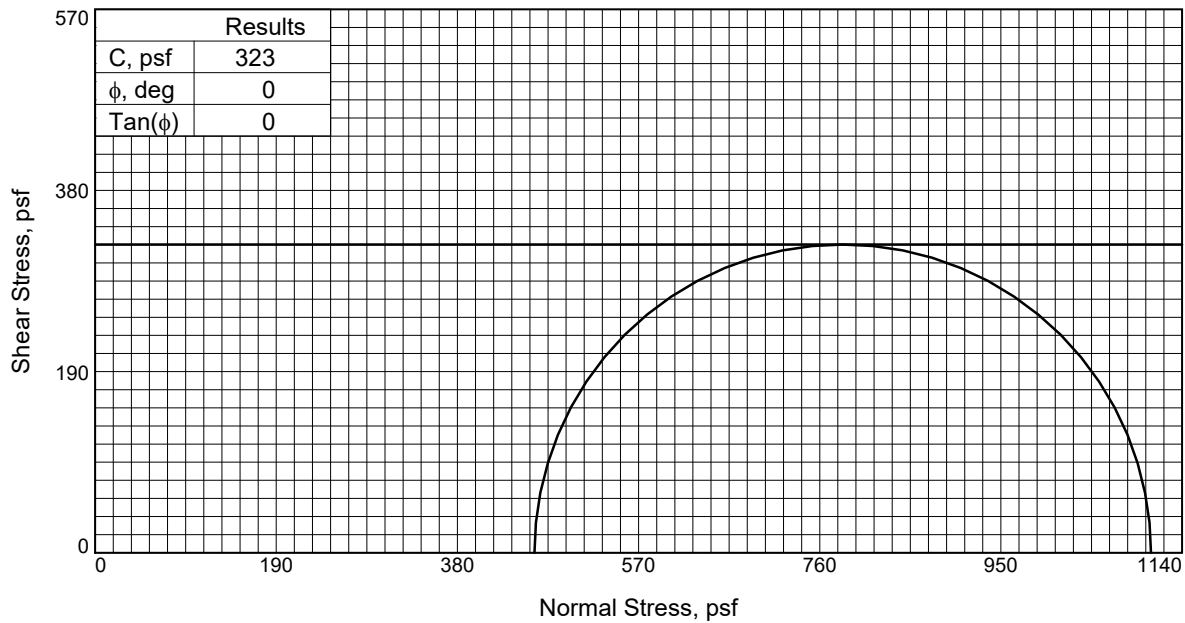
**Source of Sample:** B-1      **Depth:** 4-6

**Sample Number:** 3

**Proj. No.:** APS2008-G063

**Date Sampled:** 8-12-2020





Sample No.	1	
Initial	Water Content, %	37.5
	Dry Density, pcf	85.8
	Saturation, %	105.0
	Void Ratio	0.9637
	Diameter, in.	2.74
	Height, in.	5.89
At Test	Water Content, %	37.5
	Dry Density, pcf	85.8
	Saturation, %	105.0
	Void Ratio	0.9637
	Diameter, in.	2.74
	Height, in.	5.89
Strain at peak, %	14.8	
Back Pressure, psi	0.00	
Cell Pressure, psi	3.20	
Fail. Stress, psf	647	
Ult. Stress, psf	647	
$\sigma_1$ Failure, psf	1107	
$\sigma_3$ Failure, psf	461	

**Type of Test:**

Unconsolidated Undrained

**Sample Type:** Undisturbed

**Description:** Soft Gray Silty Clay (CL-ML)

LL= 31      PL= 26      PI= 5

**Assumed Specific Gravity=** 2.7

**Remarks:** Failure type : Bulge

Failure limit to 15%

**Client:** CPRA

**Project:** BRETON LANDBRIDGE MARSH CREATION

**Source of Sample:** B-1      **Depth:** 6-8

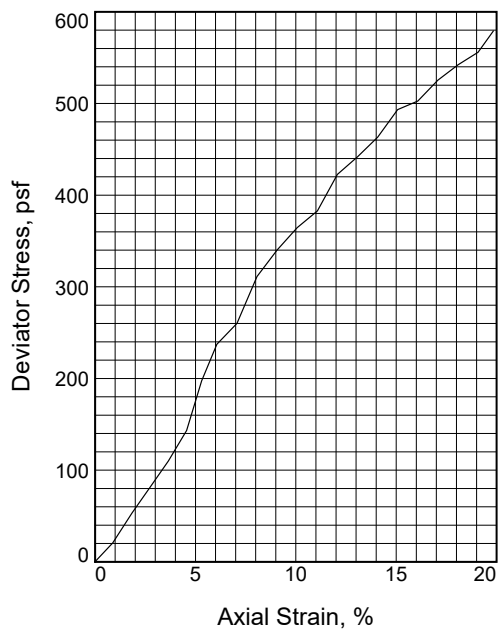
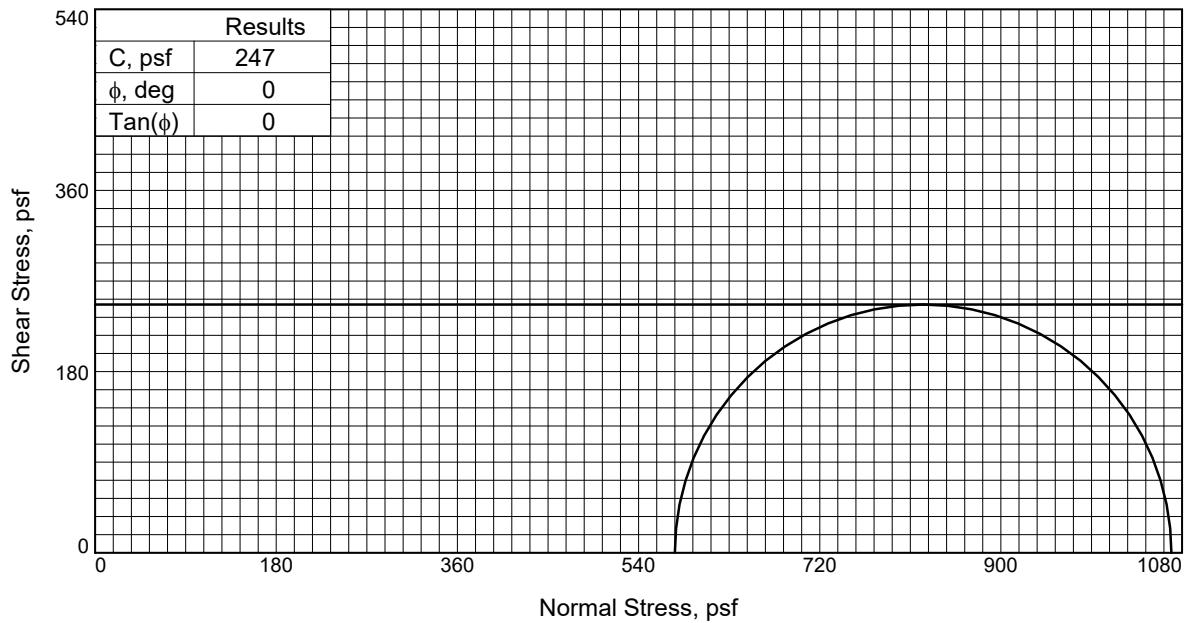
**Sample Number:** 4

**Proj. No.:** APS2008-G063

**Date Sampled:** 8-12-2020







Sample No.	1	
Initial	Water Content, %	48.5
	Dry Density, pcf	74.9
	Saturation, %	104.8
	Void Ratio	1.2499
	Diameter, in.	2.82
	Height, in.	5.81
At Test	Water Content, %	48.5
	Dry Density, pcf	74.9
	Saturation, %	104.8
	Void Ratio	1.2499
	Diameter, in.	2.82
	Height, in.	5.81
Strain at peak, %	15.1	
Back Pressure, psi	0.00	
Cell Pressure, psi	4.00	
Fail. Stress, psf	493	
Ult. Stress, psf	493	
$\sigma_1$ Failure, psf	1069	
$\sigma_3$ Failure, psf	576	

**Type of Test:**

Unconsolidated Undrained

**Sample Type:** Undisturbed

**Description:** Soft Gray Lean Clay (CL)-with fine sand

**LL= 42      PL= 23      PI= 19**

**Assumed Specific Gravity= 2.7**

**Remarks:** Failure type : Bulge  
Failure limit to 15%

**Client:** CPRA

**Project:** BRETON LANDBRIDGE MARSH CREATION

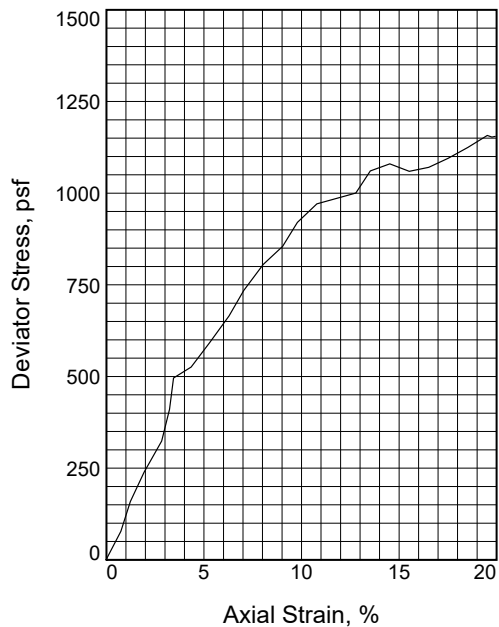
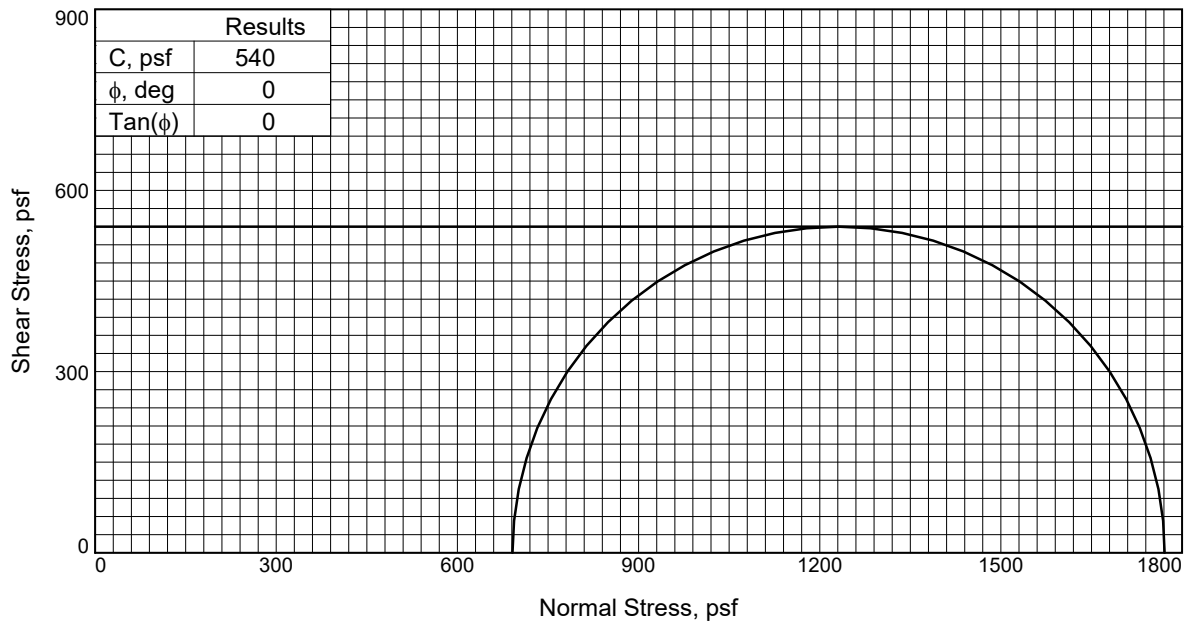
**Source of Sample:** B-1      **Depth:** 8-10

**Sample Number:** 5

**Proj. No.:** APS2008-G063

**Date Sampled:** 8-12-2020





Sample No.	1	
Initial	Water Content, %	65.9
	Dry Density, pcf	62.5
	Saturation, %	104.9
	Void Ratio	1.6970
	Diameter, in.	2.81
At Test	Height, in.	5.75
	Water Content, %	65.9
	Dry Density, pcf	62.5
	Saturation, %	104.9
	Void Ratio	1.6970
Diameter, in.	2.81	
Height, in.	5.75	
Strain at peak, %	14.5	
Back Pressure, psi	0.00	
Cell Pressure, psi	4.80	
Fail. Stress, psf	1080	
Ult. Stress, psf	1080	
$\sigma_1$ Failure, psf	1771	
$\sigma_3$ Failure, psf	691	

**Type of Test:**

Unconsolidated Undrained

**Sample Type:** Undisturbed

**Description:** Soft Gray Lean Clay (CL)-with fine sand

**LL= 43      PL= 21      PI= 22**

**Assumed Specific Gravity= 2.7**

**Remarks:** Failure type : Bulge

Failure limit to 15%

**Client:** CPRA

**Project:** BRETON LANDBRIDGE MARSH CREATION

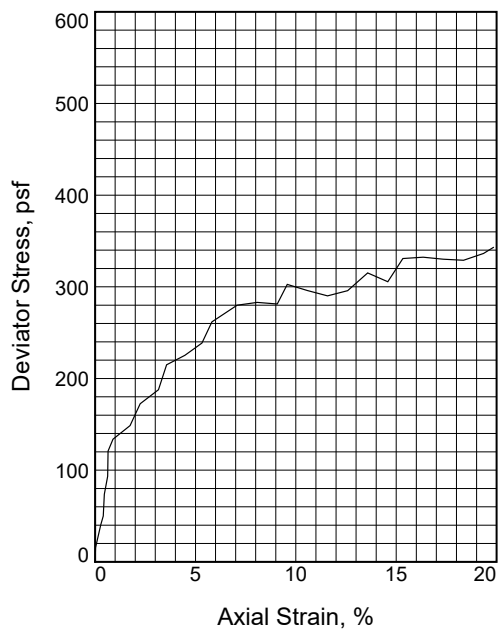
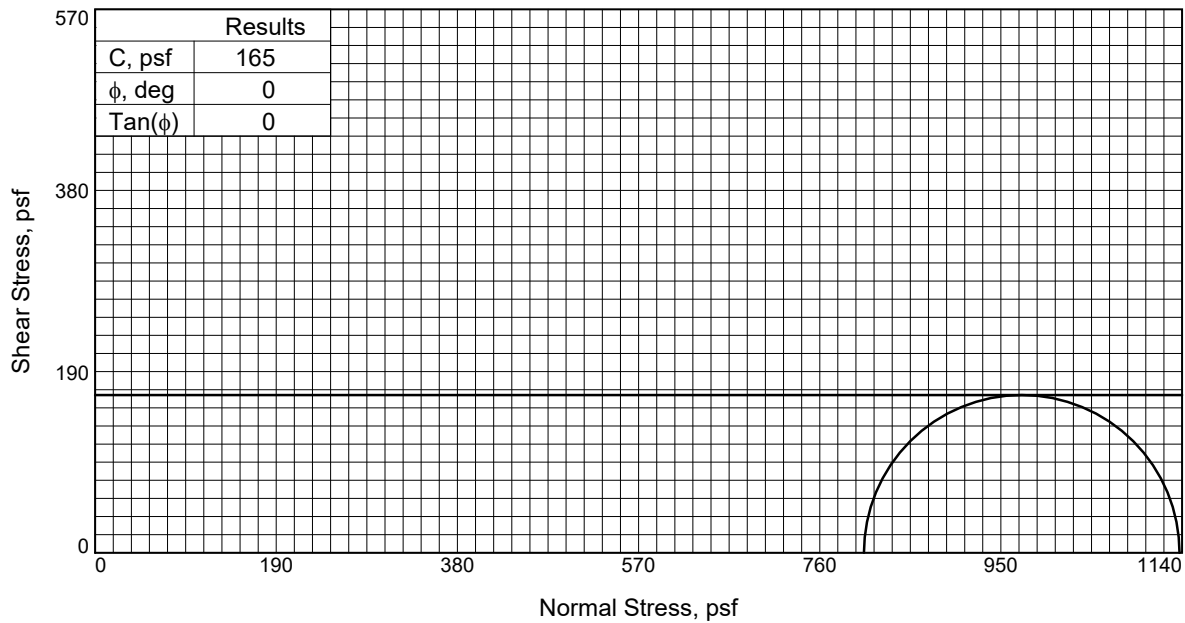
**Source of Sample:** B-1      **Depth:** 10-12

**Sample Number:** 6

**Proj. No.:** APS2008-G063

**Date Sampled:** 8-12-2020





Sample No.	1	
Initial	Water Content, %	53.9
	Dry Density, pcf	65.4
	Saturation, %	92.2
	Void Ratio	1.5773
	Diameter, in.	2.83
At Test	Height, in.	6.00
	Water Content, %	53.9
	Dry Density, pcf	65.4
	Saturation, %	92.2
	Void Ratio	1.5773
Diameter, in.	2.83	
Height, in.	6.00	
Strain at peak, %	15.3	
Back Pressure, psi	0.00	
Cell Pressure, psi	5.60	
Fail. Stress, psf	331	
Ult. Stress, psf	331	
$\sigma_1$ Failure, psf	1137	
$\sigma_3$ Failure, psf	806	

**Type of Test:**

Unconsolidated Undrained

**Sample Type:** Undisturbed

**Description:** Very Soft Gray Lean Clay (CL)-  
with fine sand

**LL= 46      PL= 22      PI= 24**

**Assumed Specific Gravity= 2.7**

**Remarks:** Failure type : Bulge  
Failure limit to 15%

**Client:** CPRA

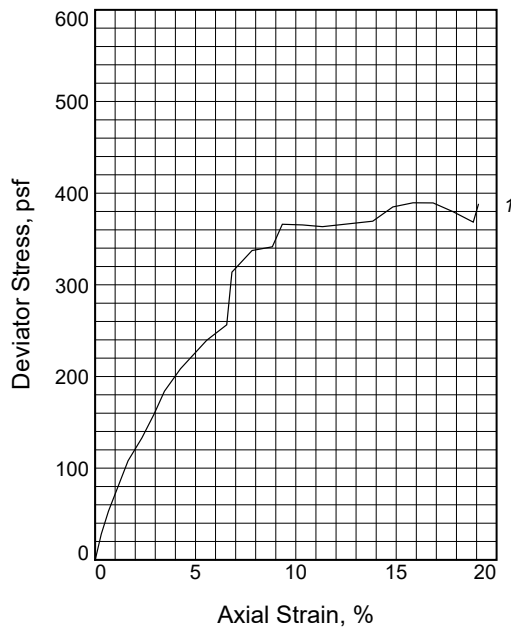
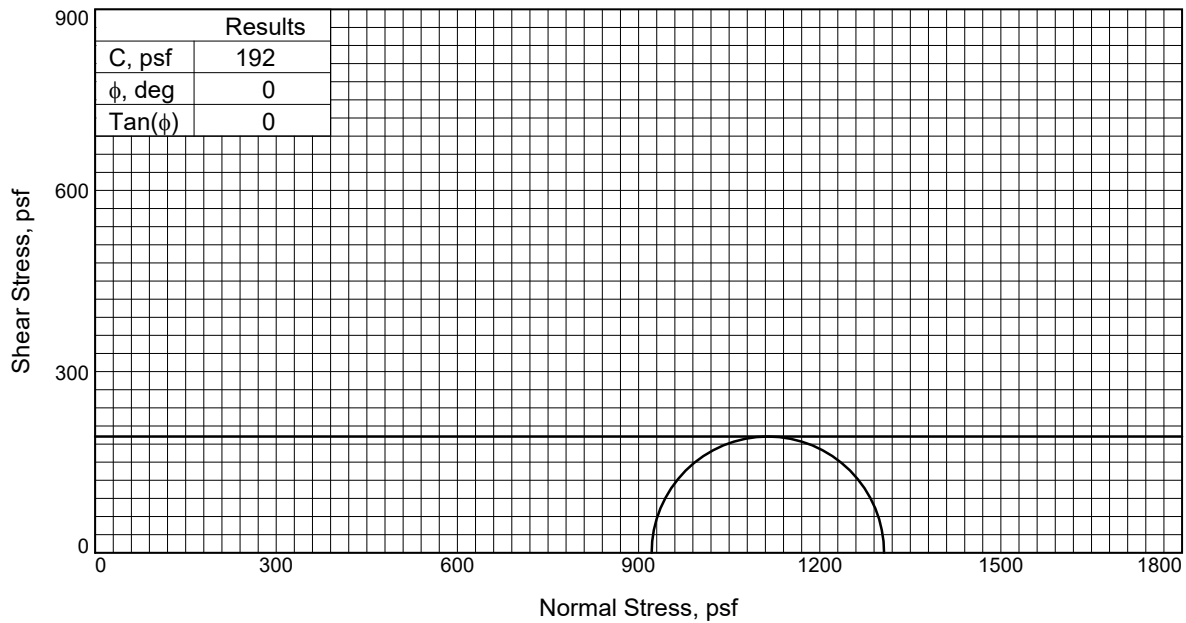
**Project:** BRETON LANDBRIDGE MARSH CREATION

**Source of Sample:** B-1      **Depth:** 12-14

**Sample Number:** 7

**Proj. No.:** APS2008-G063      **Date Sampled:** 8-12-2020





Sample No.	1	
Initial	Water Content, %	85.0
	Dry Density, pcf	52.9
	Saturation, %	104.9
	Void Ratio	2.1876
	Diameter, in.	2.81
At Test	Height, in.	5.80
	Water Content, %	85.0
	Dry Density, pcf	52.9
	Saturation, %	104.9
	Void Ratio	2.1876
Diameter, in.	2.81	
Height, in.	5.80	
Strain at peak, %	14.8	
Back Pressure, psi	0.00	
Cell Pressure, psi	6.40	
Fail. Stress, psf	385	
Ult. Stress, psf	385	
$\sigma_1$ Failure, psf	1307	
$\sigma_3$ Failure, psf	922	

**Type of Test:**

Unconsolidated Undrained

**Sample Type:** Undisturbed

**Description:** Very Soft Gray Fat Clay (CH)

**LL=** 66      **PL=** 25      **PI=** 41

**Assumed Specific Gravity=** 2.7

**Remarks:** Failure type : Bulge

Failure limit to 15%

**Client:** CPRA

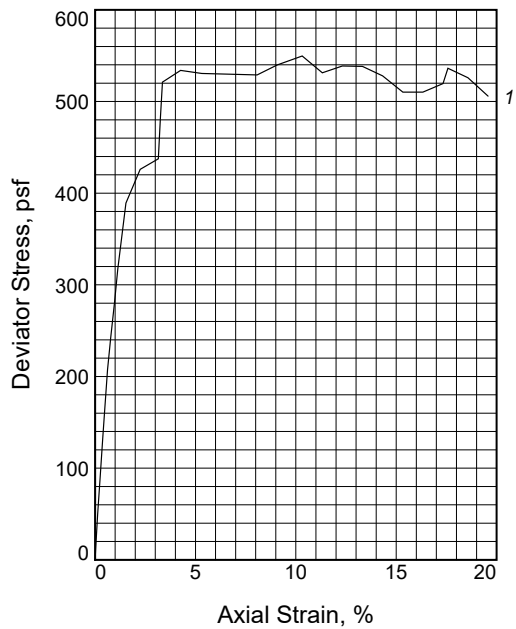
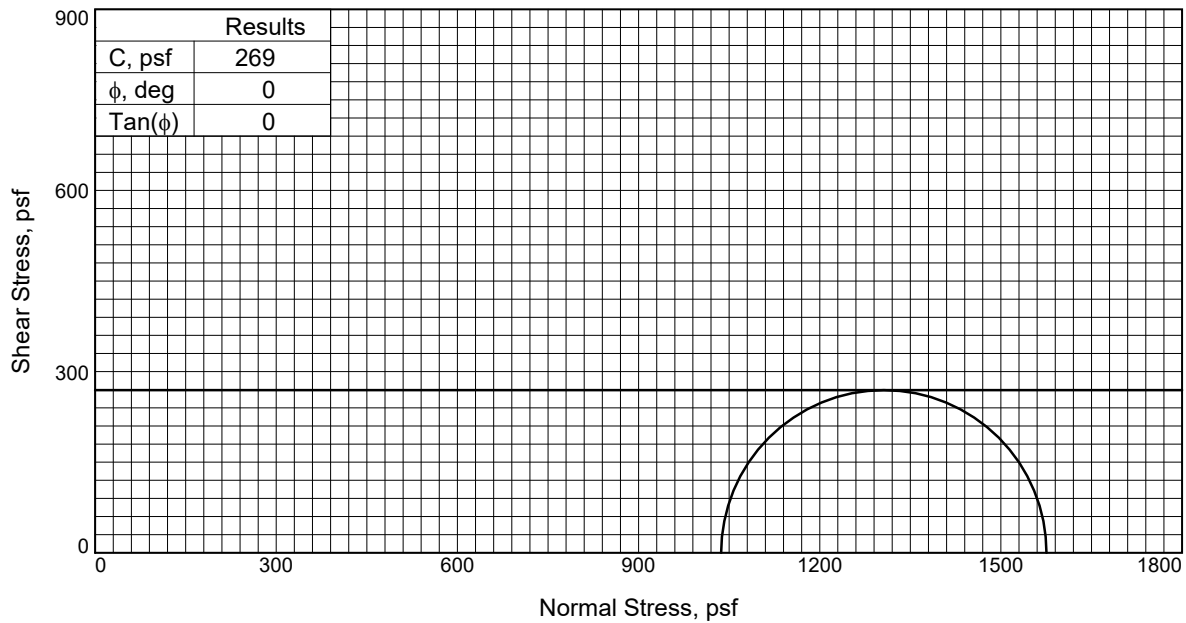
**Project:** BRETON LANDBRIDGE MARSH CREATION

**Source of Sample:** B-1      **Depth:** 14-16

**Sample Number:** 8

**Proj. No.:** APS2008-G063      **Date Sampled:** 8-12-2020





Sample No.	1	
Initial	Water Content, %	96.8
	Dry Density, pcf	47.7
	Saturation, %	104.4
	Void Ratio	2.4303
	Diameter, in.	2.81
At Test	Height, in.	5.80
	Water Content, %	96.8
	Dry Density, pcf	47.7
	Saturation, %	104.4
	Void Ratio	2.4303
Diameter, in.	2.81	
Height, in.	5.80	
Strain at peak, %	12.3	
Back Pressure, psi	0.00	
Cell Pressure, psi	7.20	
Fail. Stress, psf	539	
Ult. Stress, psf	539	
$\sigma_1$ Failure, psf	1575	
$\sigma_3$ Failure, psf	1037	

**Type of Test:**

Unconsolidated Undrained

**Sample Type:** Undisturbed

**Description:** Very Soft Gray Fat Clay (CH)

LL= 115      PL= 33      PI= 82

**Specific Gravity=** 2.62

**Remarks:** Failure type : Bulge

**Client:** CPRA

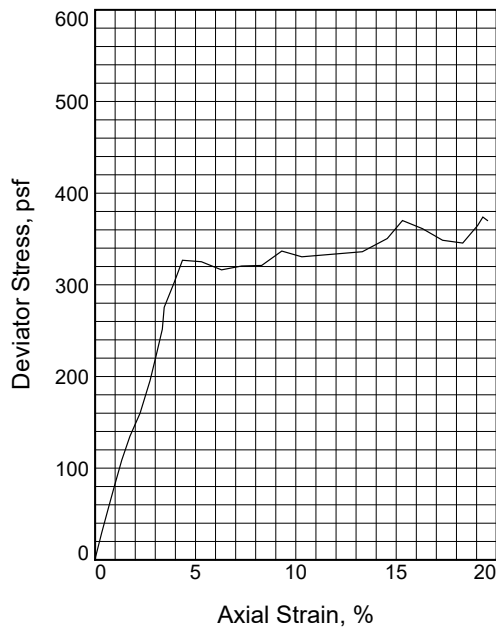
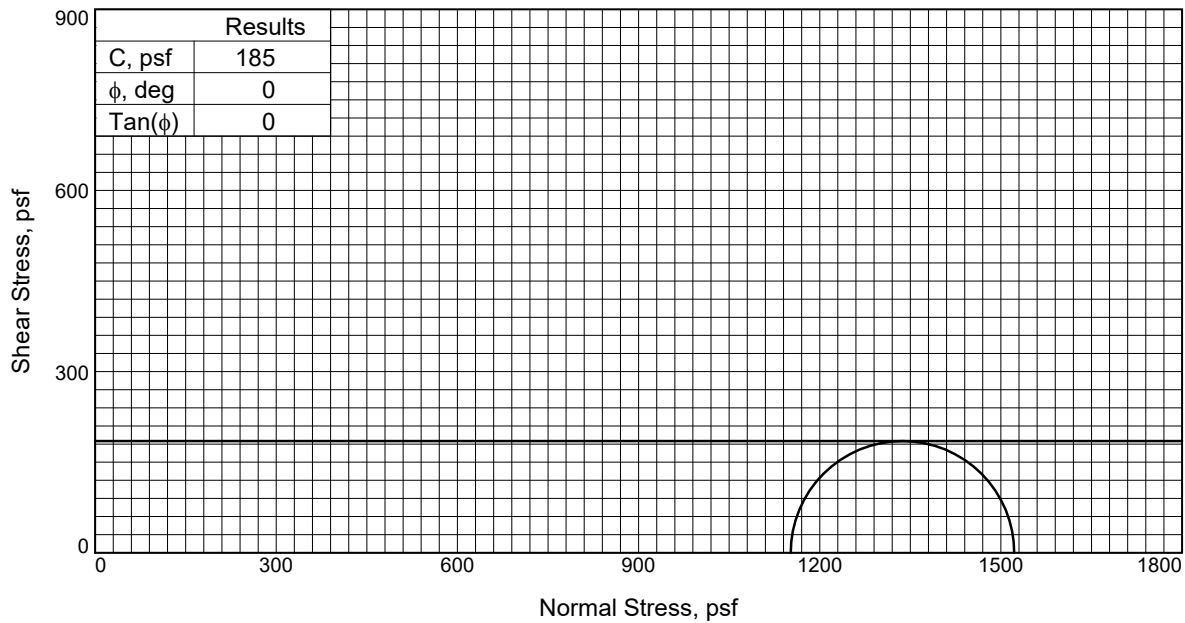
**Project:** BRETON LANDBRIDGE MARSH CREATION

**Source of Sample:** B-1      **Depth:** 16-18

**Sample Number:** 9

**Proj. No.:** APS2008-G063      **Date Sampled:** 8-12-2020





Sample No.	1	
Initial	Water Content, %	93.8
	Dry Density, pcf	49.3
	Saturation, %	104.7
	Void Ratio	2.4192
	Diameter, in.	2.78
At Test	Height, in.	5.76
	Water Content, %	93.8
	Dry Density, pcf	49.3
	Saturation, %	104.7
	Void Ratio	2.4192
Diameter, in.	2.78	
Height, in.	5.76	
Strain at peak, %	15.3	
Back Pressure, psi	0.00	
Cell Pressure, psi	8.00	
Fail. Stress, psf	370	
Ult. Stress, psf	370	
$\sigma_1$ Failure, psf	1522	
$\sigma_3$ Failure, psf	1152	

**Type of Test:**

Unconsolidated Undrained

**Sample Type:** Undisturbed

**Description:** Very Soft Gray Fat Clay (CH)

**LL= 89      PL= 24      PI= 65**

**Specific Gravity= 2.7**

**Remarks:** Failure type : Bulge  
Failure limit to 15%

**Client:** CPRA

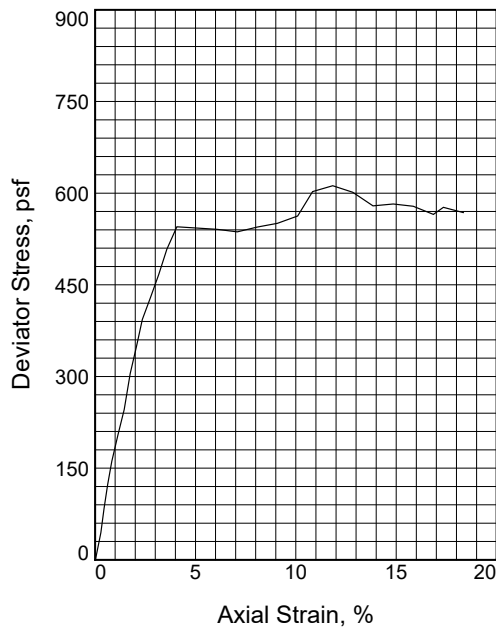
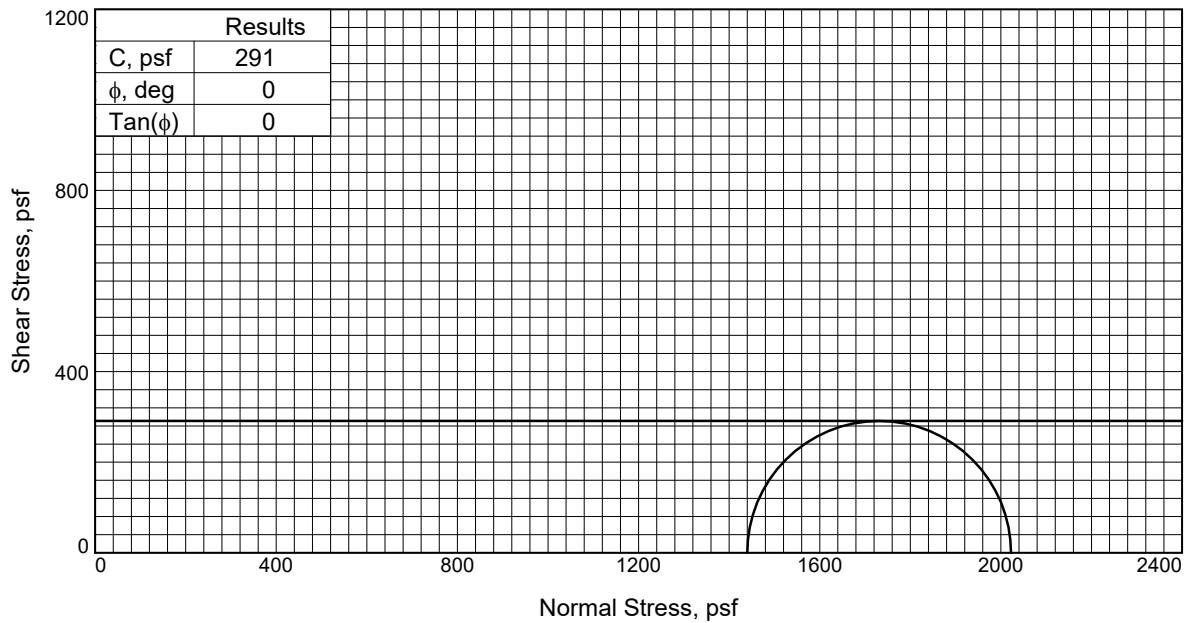
**Project:** BRETON LANDBRIDGE MARSH CREATION

**Source of Sample:** B-1      **Depth:** 18-20

**Sample Number:** 10

**Proj. No.:** APS2008-G063      **Date Sampled:** 8-12-2020





Sample No.	1	
Initial	Water Content, %	111.4
	Dry Density, pcf	43.5
	Saturation, %	104.8
	Void Ratio	2.8714
	Diameter, in.	2.83
At Test	Height, in.	5.80
	Water Content, %	111.4
	Dry Density, pcf	43.5
	Saturation, %	104.8
	Void Ratio	2.8714
Diameter, in.	2.83	
Height, in.	5.80	
Strain at peak, %	14.9	
Back Pressure, psi	0.00	
Cell Pressure, psi	10.00	
Fail. Stress, psf	582	
Ult. Stress, psf	582	
$\sigma_1$ Failure, psf	2022	
$\sigma_3$ Failure, psf	1440	

**Type of Test:**

Unconsolidated Undrained

**Sample Type:** Undisturbed

**Description:** Soft Gray Fat Clay (CH)

**LL=** 165      **PL=** 30      **PI=** 135

**Assumed Specific Gravity=** 2.7

**Remarks:** Failure type : Bulge

Failure limit to 15%

**Client:** CPRA

**Project:** BRETON LANDBRIDGE MARSH CREATION

**Source of Sample:** B-1

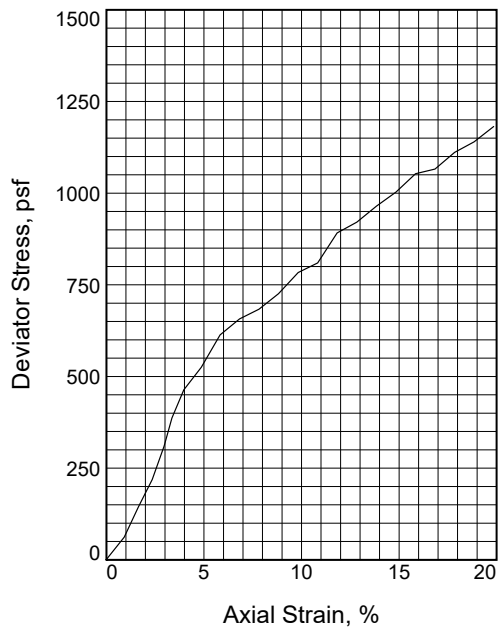
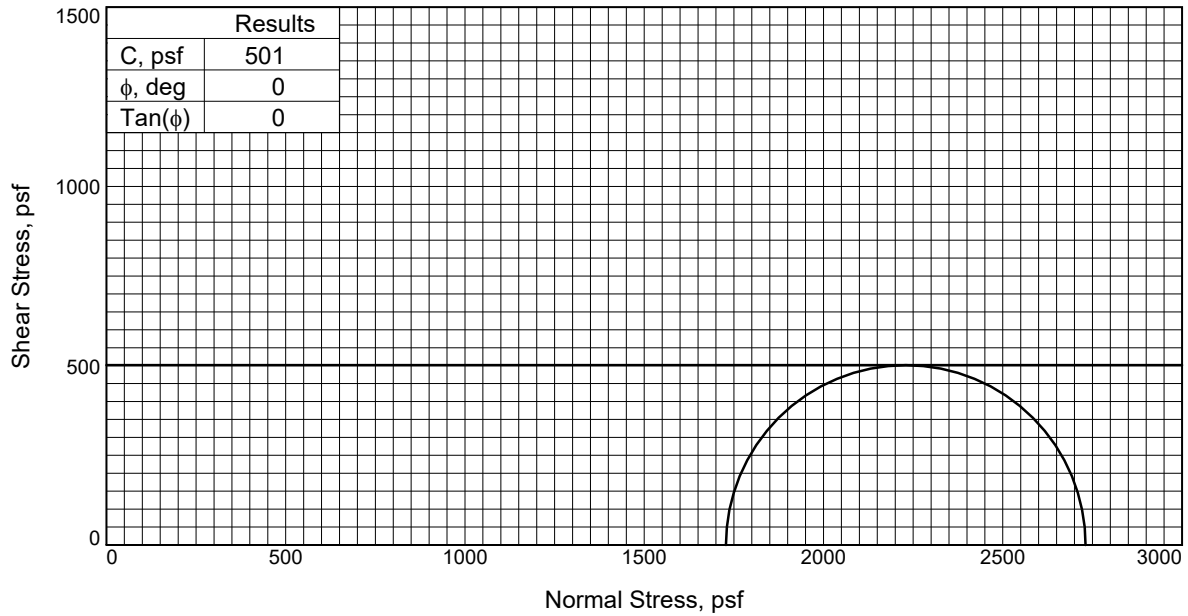
**Depth:** 23-25

**Sample Number:** 11

**Proj. No.:** APS2008-G063

**Date Sampled:** 8-12-2020





Sample No.	1	
Initial	Water Content, %	32.2
	Dry Density, pcf	88.7
	Saturation, %	96.4
	Void Ratio	0.9008
	Diameter, in.	2.78
	Height, in.	5.87
At Test	Water Content, %	32.2
	Dry Density, pcf	88.7
	Saturation, %	96.4
	Void Ratio	0.9008
	Diameter, in.	2.78
	Height, in.	5.87
Strain at peak, %	14.8	
Back Pressure, psi	0.00	
Cell Pressure, psi	12.00	
Fail. Stress, psf	1003	
Ult. Stress, psf	1003	
$\sigma_1$ Failure, psf	2731	
$\sigma_3$ Failure, psf	1728	

**Type of Test:**

Unconsolidated Undrained

**Sample Type:** Undisturbed

**Description:** Medium Stiff Gray Lean Clay (CL)-with fine sand

**LL= 38      PL= 22      PI= 16**

**Assumed Specific Gravity= 2.7**

**Remarks:** Failure type : Bulge  
Failure limit to 15%

**Client:** CPRA

**Project:** BRETON LANDBRIDGE MARSH CREATION

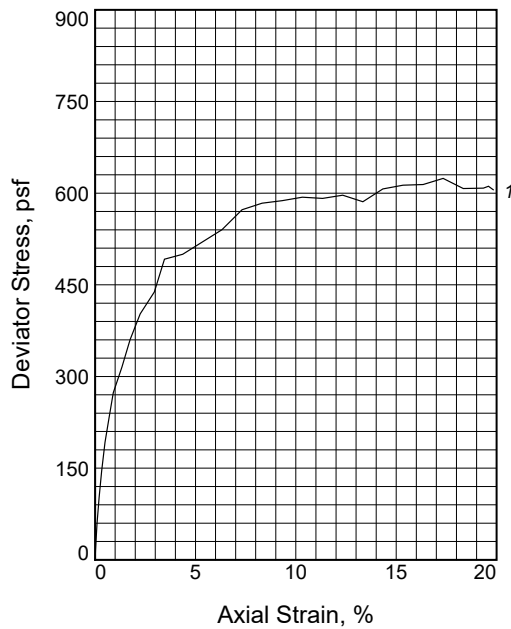
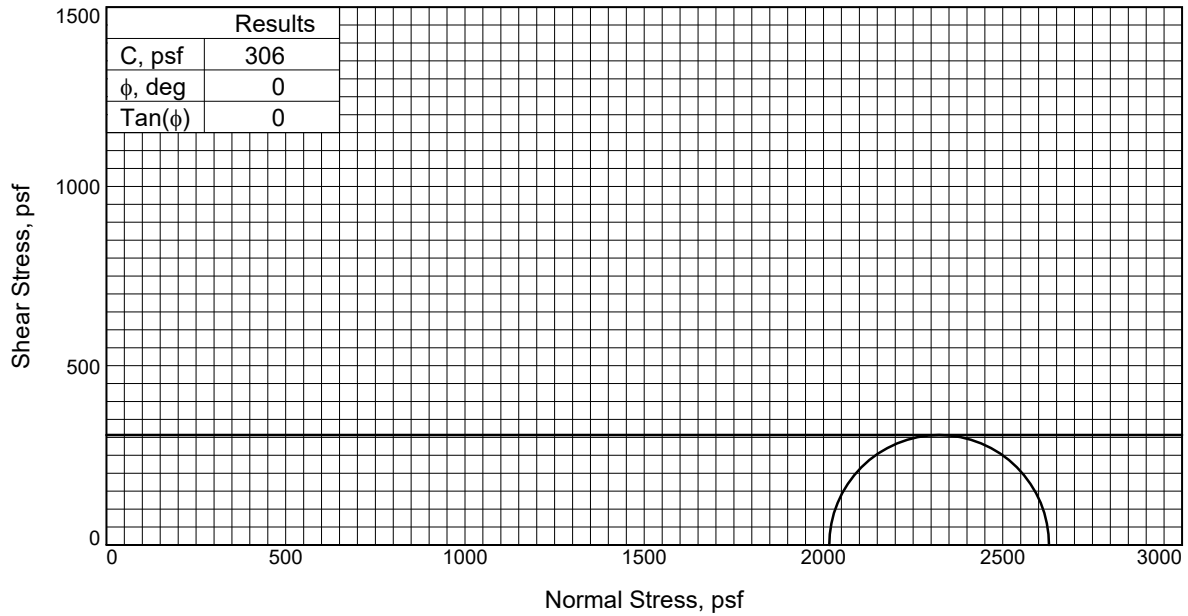
**Source of Sample:** B-1      **Depth:** 28-30

**Sample Number:** 12

**Proj. No.:** APS2008-G063      **Date Sampled:** 8-12-2020







Sample No.	1	
Initial	Water Content, %	49.9
	Dry Density, pcf	72.1
	Saturation, %	100.8
	Void Ratio	1.3377
	Diameter, in.	2.78
At Test	Height, in.	5.81
	Water Content, %	49.9
	Dry Density, pcf	72.1
	Saturation, %	100.8
	Void Ratio	1.3377
Diameter, in.	2.78	
Height, in.	5.81	
Strain at peak, %	15.3	
Back Pressure, psi	0.00	
Cell Pressure, psi	14.00	
Fail. Stress, psf	613	
Ult. Stress, psf	613	
$\sigma_1$ Failure, psf	2629	
$\sigma_3$ Failure, psf	2016	

**Type of Test:**

Unconsolidated Undrained

**Sample Type:** Undisturbed

**Description:** Soft Gray Fat Clay (CH)

**LL=** 61      **PL=** 26      **PI=** 35

**Assumed Specific Gravity=** 2.7

**Remarks:** Failure Type : Bulge

Failure limit to 15%

**Client:** CPRA

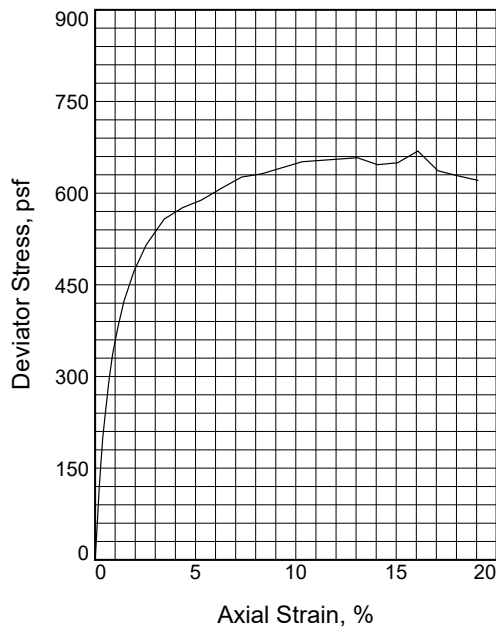
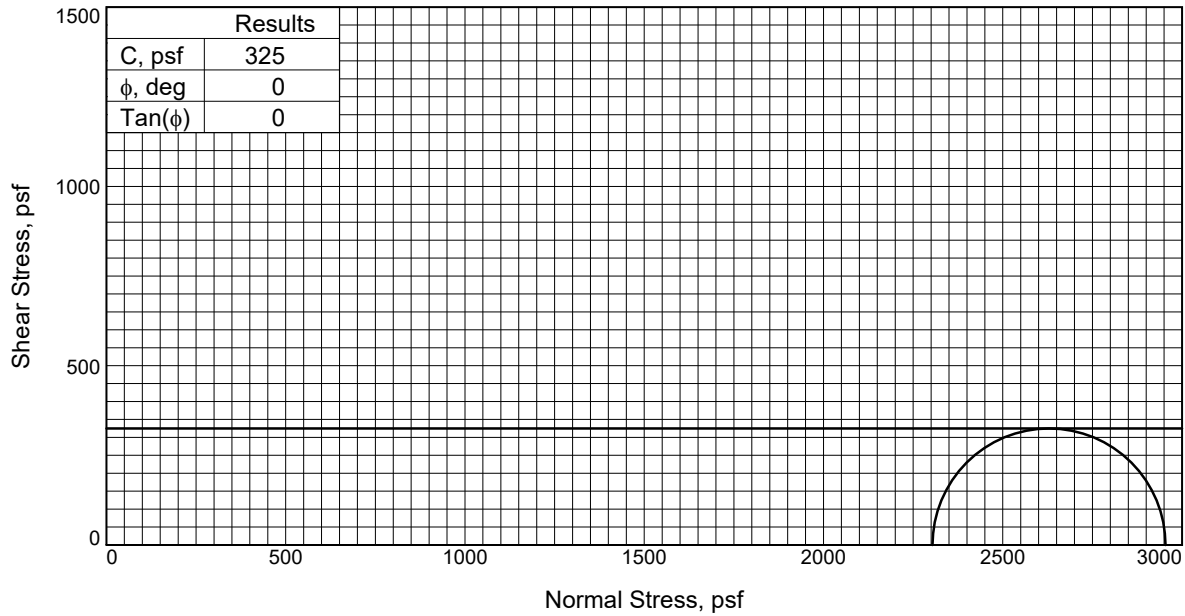
**Project:** BRETON LANDBRIDGE MARSH CREATION

**Source of Sample:** B-1      **Depth:** 33-35

**Sample Number:** 13

**Proj. No.:** APS2008-G063      **Date Sampled:** 8-12-2020





Sample No.	1	
Initial	Water Content, %	64.9
	Dry Density, pcf	60.8
	Saturation, %	98.9
	Void Ratio	1.7726
	Diameter, in.	2.77
	Height, in.	5.79
At Test	Water Content, %	64.9
	Dry Density, pcf	60.8
	Saturation, %	98.9
	Void Ratio	1.7726
	Diameter, in.	2.77
	Height, in.	5.79
Strain at peak, %	15.1	
Back Pressure, psi	0.00	
Cell Pressure, psi	16.00	
Fail. Stress, psf	650	
Ult. Stress, psf	650	
$\sigma_1$ Failure, psf	2954	
$\sigma_3$ Failure, psf	2304	

**Type of Test:**

Unconsolidated Undrained

**Sample Type:** Undisturbed

**Description:** Soft gray fat clay (CH)

**LL= 94      PL= 29      PI= 65**

**Assumed Specific Gravity= 2.7**

**Remarks:** Failure Type : Multi Shear

Failure limit to 15%

**Client:** CPRA

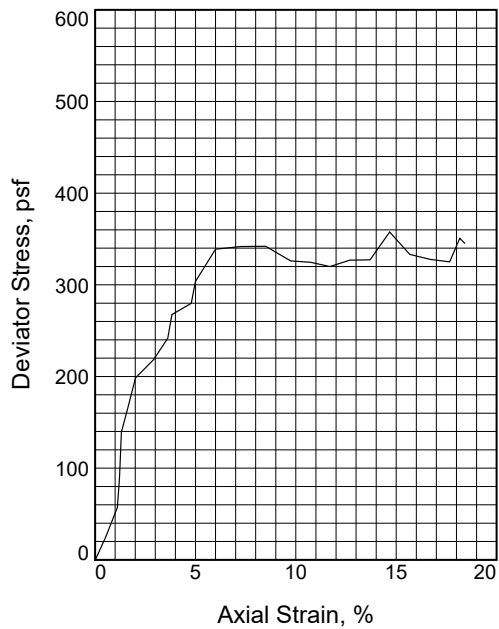
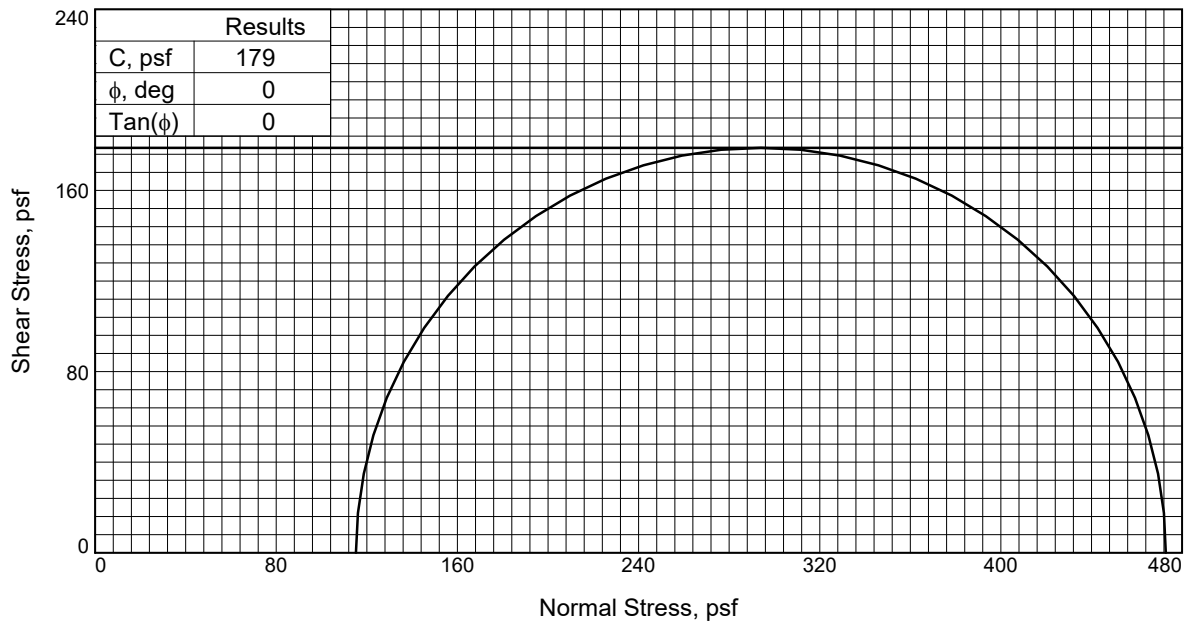
**Project:** BRETON LANDBRIDGE MARSH CREATION

**Source of Sample:** B-1      **Depth:** 38-40

**Sample Number:** 14

**Proj. No.:** APS2008-G063      **Date Sampled:** 8-12-2020





Sample No.	1	
Initial	Water Content, %	594.5
	Dry Density, pcf	10.3
	Saturation, %	104.9
	Void Ratio	15.3034
	Diameter, in.	2.76
At Test	Height, in.	5.71
	Water Content, %	566.8
	Dry Density, pcf	10.3
	Saturation, %	100.0
	Void Ratio	15.3034
Diameter, in.	2.76	
Height, in.	5.71	
Strain at peak, %	14.7	
Back Pressure, psi	0.00	
Cell Pressure, psi	0.80	
Fail. Stress, psf	358	
Ult. Stress, psf	358	
$\sigma_1$ Failure, psf	473	
$\sigma_3$ Failure, psf	115	

**Type of Test:**

Unconsolidated Undrained

**Sample Type:** Undisturbed

**Description:** Very Soft Black Organic Clay (OH)

**LL=** 621      **PL=** 159      **PI=** 462

**Assumed Specific Gravity=** 2.7

**Remarks:** Failure Type : Bulge

Failure limit to 15%

**Client:** CPRA

**Project:** BRETON LANDBRIDGE MARSH CREATION

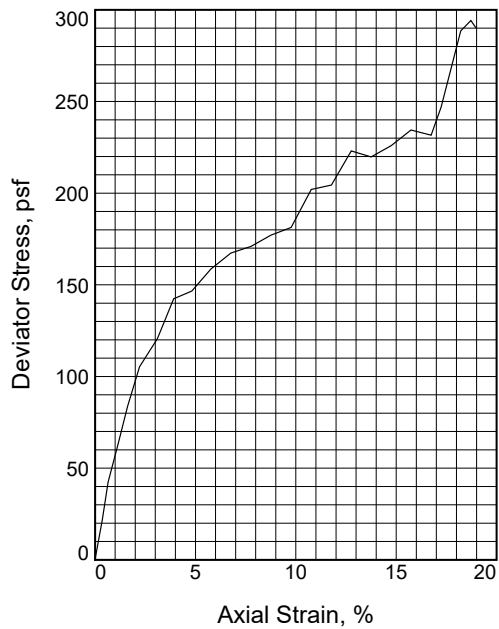
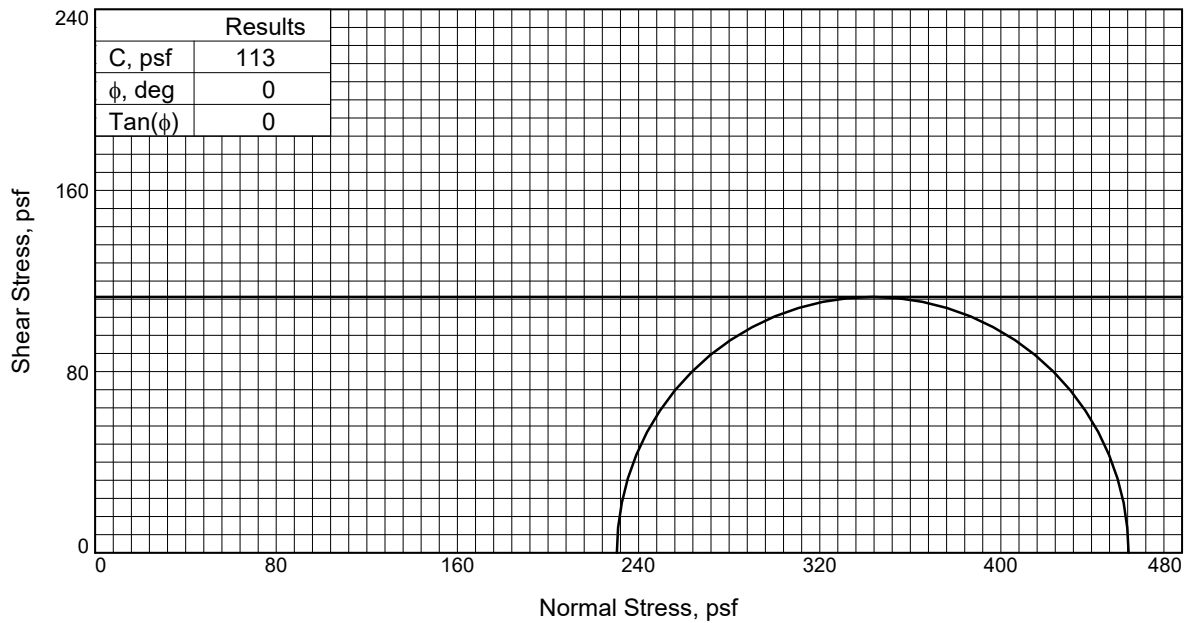
**Source of Sample:** B-2      **Depth:** 0-2

**Sample Number:** 1

**Proj. No.:** APS2008-G063

**Date Sampled:** 8-12-2020





Sample No.	1	
Initial	Water Content, %	98.8
	Dry Density, pcf	45.5
	Saturation, %	98.7
	Void Ratio	2.7036
	Diameter, in.	2.78
At Test	Height, in.	6.17
	Water Content, %	98.8
	Dry Density, pcf	45.5
	Saturation, %	98.7
	Void Ratio	2.7036
Diameter, in.	2.78	
Height, in.	6.17	
Strain at peak, %	14.8	
Back Pressure, psi	0.00	
Cell Pressure, psi	1.60	
Fail. Stress, psf	226	
Ult. Stress, psf	226	
$\sigma_1$ Failure, psf	456	
$\sigma_3$ Failure, psf	230	

**Type of Test:**

Unconsolidated Undrained

**Sample Type:** Undisturbed

**Description:** Very Soft Gray Fat Clay (CH)

LL= 73      PL= 22      PI= 51

**Assumed Specific Gravity=** 2.7

**Remarks:** Failure Type : Bulge

Failure limit to 15%

**Client:** CPRA

**Project:** BRETON LANDBRIDGE MARSH CREATION

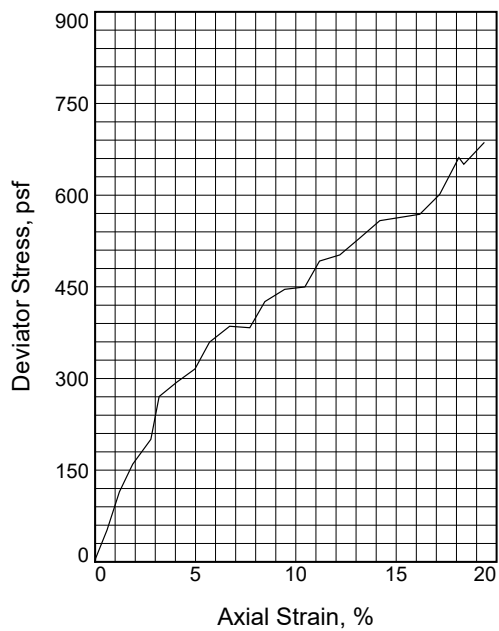
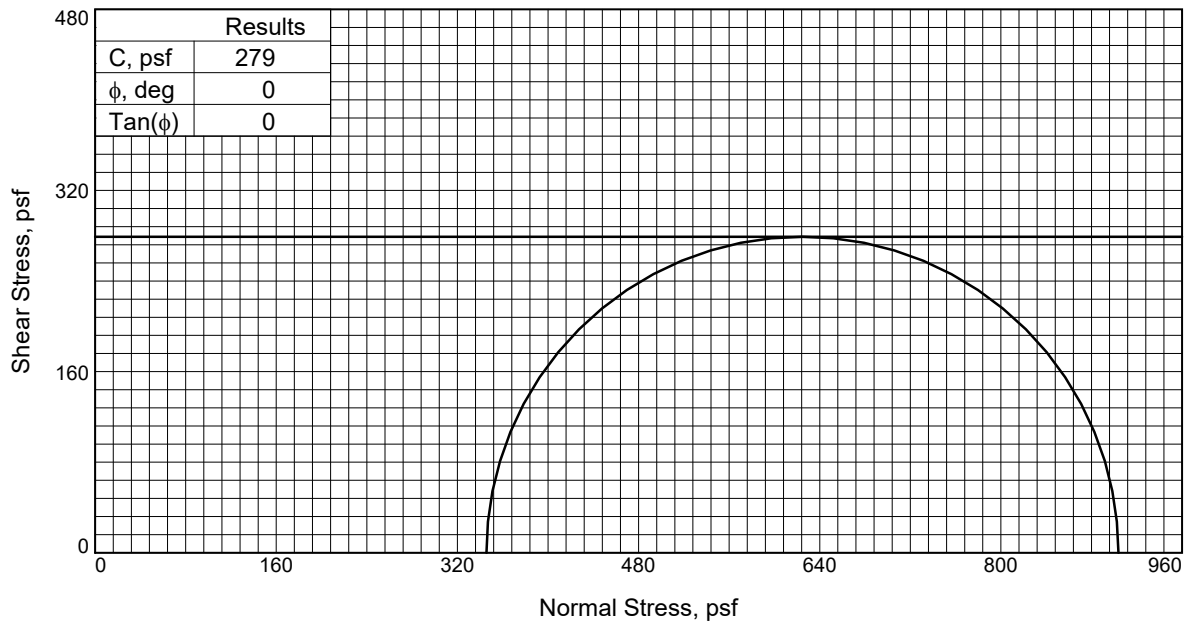
**Source of Sample:** B-2      **Depth:** 2-4

**Sample Number:** 2

**Proj. No.:** APS2008-G063

**Date Sampled:** 8-12-2020





Sample No.	1	
Initial	Water Content, %	46.0
	Dry Density, pcf	75.0
	Saturation, %	99.6
	Void Ratio	1.2474
	Diameter, in.	2.94
	Height, in.	5.94
At Test	Water Content, %	46.0
	Dry Density, pcf	75.0
	Saturation, %	99.6
	Void Ratio	1.2474
	Diameter, in.	2.94
	Height, in.	5.94
Strain at peak, %	14.2	
Back Pressure, psi	0.00	
Cell Pressure, psi	2.40	
Fail. Stress, psf	558	
Ult. Stress, psf	558	
$\sigma_1$ Failure, psf	904	
$\sigma_3$ Failure, psf	346	

**Type of Test:**

Unconsolidated Undrained

**Sample Type:** Undisturbed

**Description:** Soft Gray Silty Clay(CL-ML)

**LL= 31      PL= 25      PI= 6**

**Assumed Specific Gravity= 2.7**

**Remarks:** Failure Type : Bulge

Failure limit to 15%

**Client:** CPRA

**Project:** BRETON LANDBRIDGE MARSH CREATION

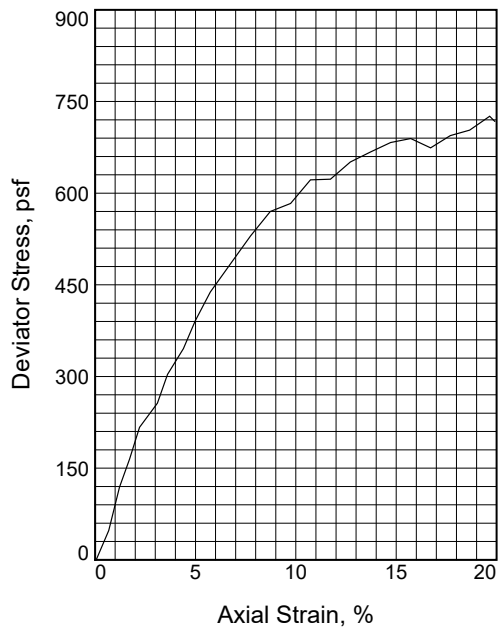
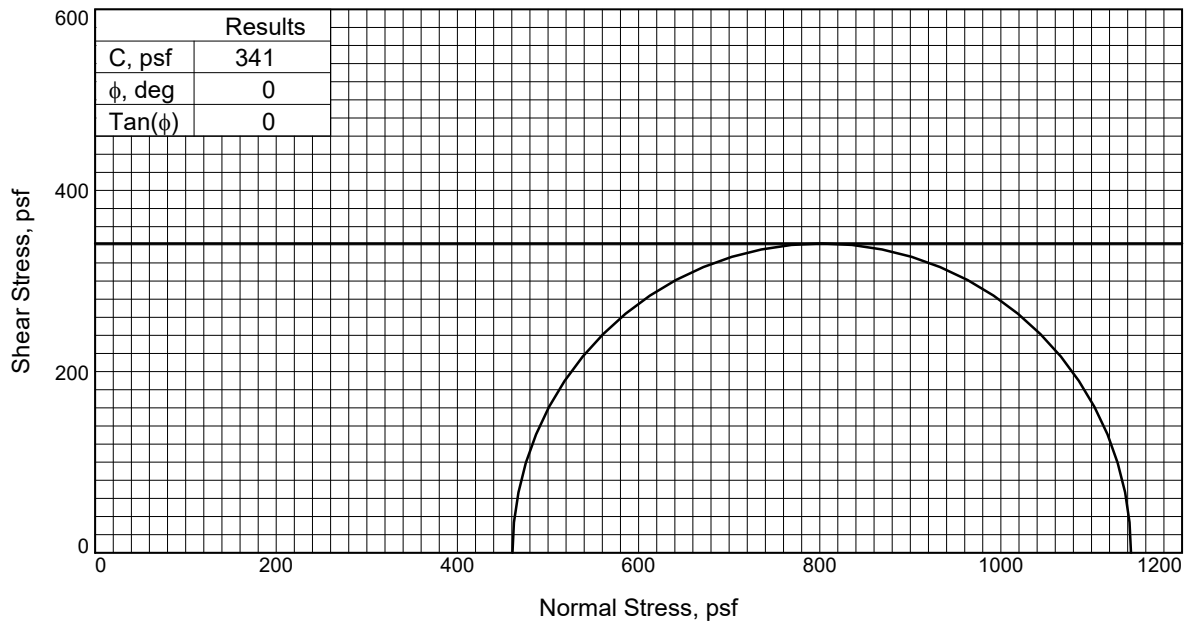
**Source of Sample:** B-2      **Depth:** 4-6

**Sample Number:** 3

**Proj. No.:** APS2008-G063

**Date Sampled:** 8-12-2020





Sample No.	1	
Initial	Water Content, %	34.0
	Dry Density, pcf	81.7
	Saturation, %	86.3
	Void Ratio	1.0643
	Diameter, in.	2.95
	Height, in.	5.98
At Test	Water Content, %	34.0
	Dry Density, pcf	81.7
	Saturation, %	86.3
	Void Ratio	1.0643
	Diameter, in.	2.95
	Height, in.	5.98
Strain at peak, %	14.7	
Back Pressure, psi	0.00	
Cell Pressure, psi	3.20	
Fail. Stress, psf	683	
Ult. Stress, psf	683	
$\sigma_1$ Failure, psf	1144	
$\sigma_3$ Failure, psf	461	

**Type of Test:**

Unconsolidated Undrained

**Sample Type:** Undisturbed

**Description:** Soft Gray Silty Clay with sand  
(CL-ML)

**LL= 30      PL= 24      PI= 6**

**Assumed Specific Gravity= 2.7**

**Remarks:** Failure Type : Bulge  
Failure limit to 15%

**Client:** CPRA

**Project:** BRETON LANDBRIDGE MARSH CREATION

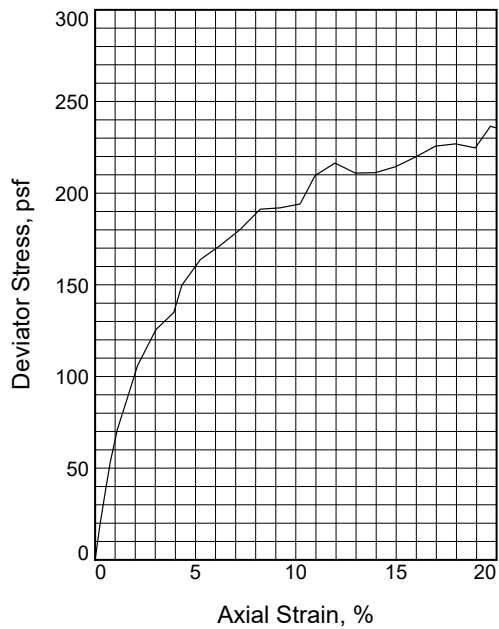
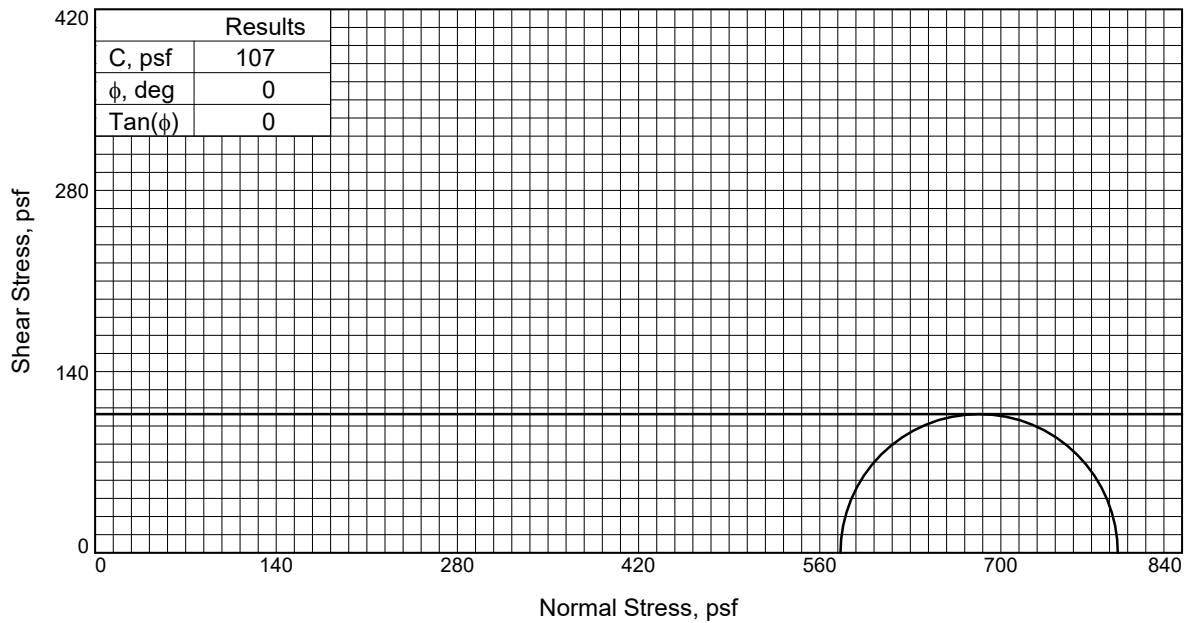
**Source of Sample:** B-2      **Depth:** 6-8

**Sample Number:** 4

**Proj. No.:** APS2008-G063

**Date Sampled:** 8-12-2020





Sample No.	1	
Initial	Water Content, %	47.3
	Dry Density, pcf	67.5
	Saturation, %	85.3
	Void Ratio	1.4987
	Diameter, in.	2.86
	Height, in.	5.88
At Test	Water Content, %	47.3
	Dry Density, pcf	67.5
	Saturation, %	85.3
	Void Ratio	1.4987
	Diameter, in.	2.86
	Height, in.	5.88
Strain at peak, %	15.0	
Back Pressure, psi	0.00	
Cell Pressure, psi	4.00	
Fail. Stress, psf	214	
Ult. Stress, psf	214	
$\sigma_1$ Failure, psf	790	
$\sigma_3$ Failure, psf	576	

**Type of Test:**

Unconsolidated Undrained

**Sample Type:** Undisturbed

**Description:** Soft Gray Silty Clay with sand (CL-ML)

**LL= 80      PL= 20      PI= 60**

**Assumed Specific Gravity= 2.7**

**Remarks:** Failure Type : Bulge  
Failure limit to 15%

**Client:** CPRA

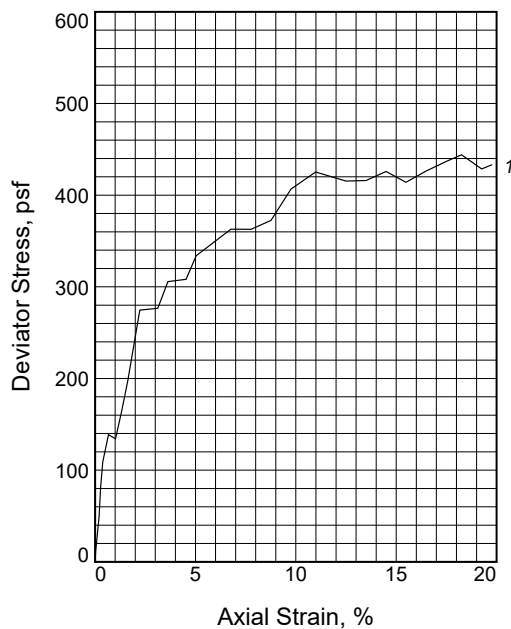
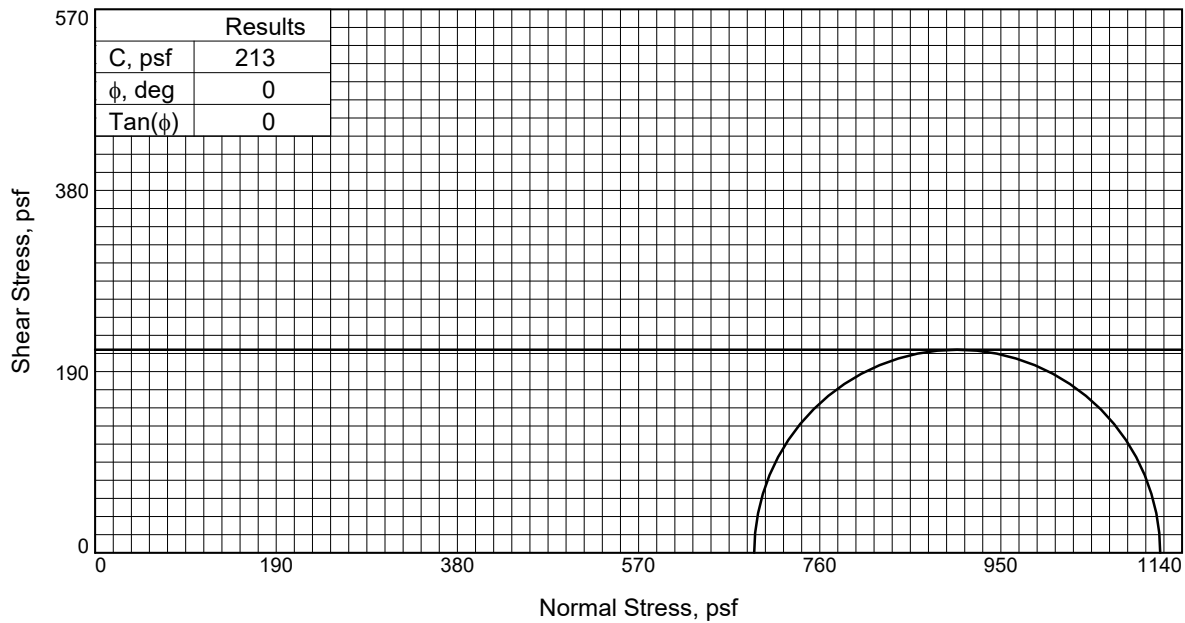
**Project:** BRETON LANDBRIDGE MARSH CREATION

**Source of Sample:** B-2      **Depth:** 8-10

**Sample Number:** 5

**Proj. No.:** APS2008-G063      **Date Sampled:** 8-12-2020





Sample No.	1	
Initial	Water Content, %	49.5
	Dry Density, pcf	70.3
	Saturation, %	95.6
	Void Ratio	1.3990
	Diameter, in.	2.82
	Height, in.	5.77
At Test	Water Content, %	49.5
	Dry Density, pcf	70.3
	Saturation, %	95.6
	Void Ratio	1.3990
	Diameter, in.	2.82
	Height, in.	5.77
Strain at peak, %	14.5	
Back Pressure, psi	0.00	
Cell Pressure, psi	4.80	
Fail. Stress, psf	426	
Ult. Stress, psf	426	
$\sigma_1$ Failure, psf	1117	
$\sigma_3$ Failure, psf	691	

**Type of Test:**

Unconsolidated Undrained

**Sample Type:** Undisturbed

**Description:** Very Soft Gray Fat Clay (CH)

**LL= 53      PL= 24      PI= 29**

**Assumed Specific Gravity= 2.7**

**Remarks:** Failure Type : Bulge

Failure limit to 15%

**Client:** CPRA

**Project:** BRETON LANDBRIDGE MARSH CREATION

**Source of Sample:** B-2      **Depth:** 10-12

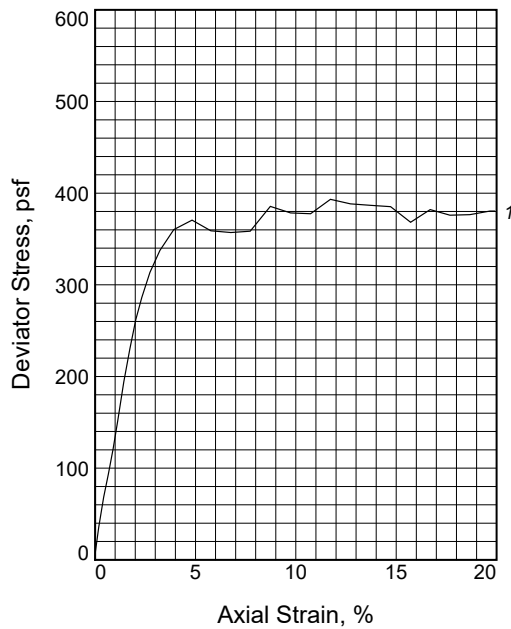
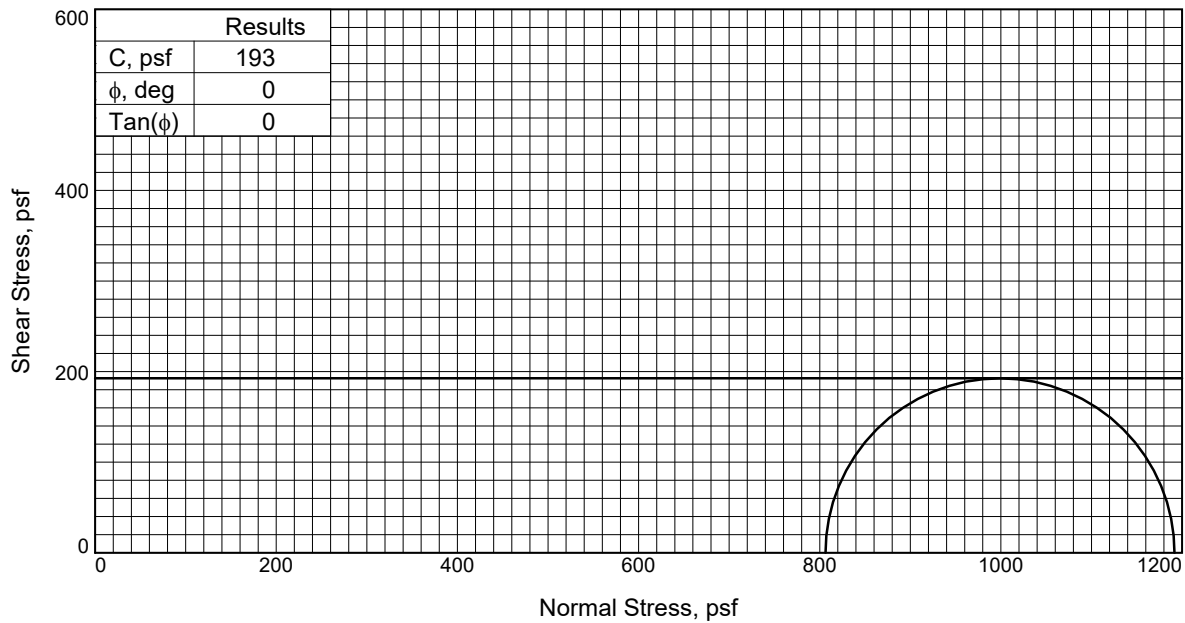
**Sample Number:** 6

**Proj. No.:** APS2008-G063

**Date Sampled:** 8-12-2020







Sample No.	1	
Initial	Water Content, %	98.6
	Dry Density, pcf	46.0
	Saturation, %	100.0
	Void Ratio	2.6625
	Diameter, in.	2.84
At Test	Height, in.	5.75
	Water Content, %	98.6
	Dry Density, pcf	46.0
	Saturation, %	100.0
	Void Ratio	2.6625
Diameter, in.	2.84	
Height, in.	5.75	
Strain at peak, %	14.7	
Back Pressure, psi	0.00	
Cell Pressure, psi	5.60	
Fail. Stress, psf	385	
Ult. Stress, psf	385	
$\sigma_1$ Failure, psf	1192	
$\sigma_3$ Failure, psf	806	

**Type of Test:**

Unconsolidated Undrained

**Sample Type:** Undisturbed

**Description:** Very Soft Gray Fat Clay (CH)

**LL= 77      PL= 19      PI= 58**

**Assumed Specific Gravity= 2.7**

**Remarks:** Failure Type : Bulge

Failure limit to 15%

**Client:** CPRA

**Project:** BRETON LANDBRIDGE MARSH CREATION

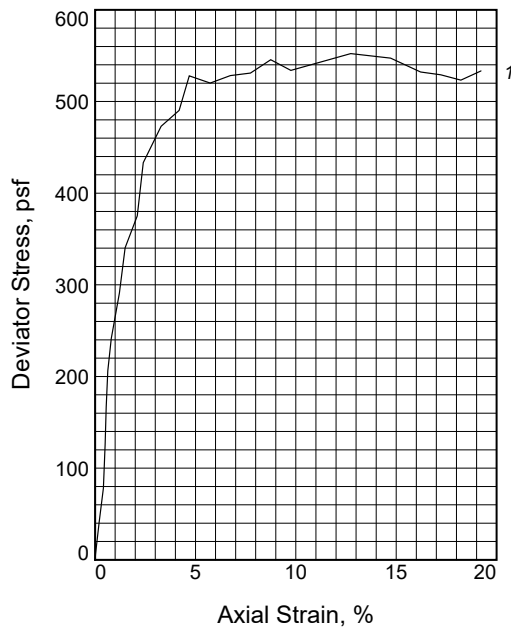
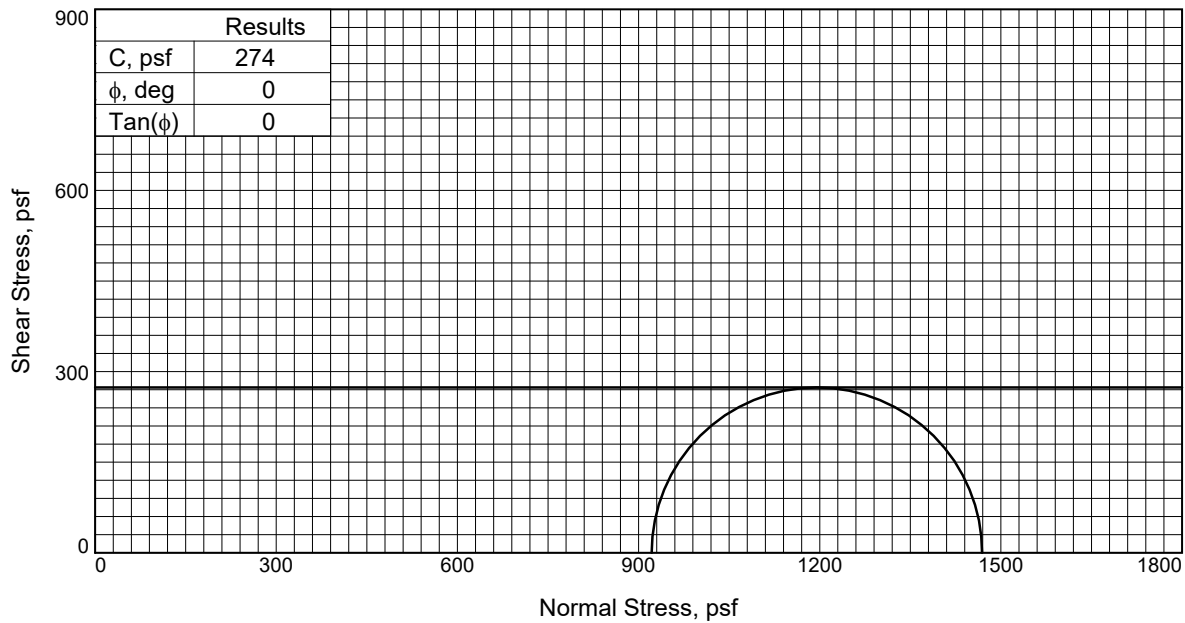
**Source of Sample:** B-2      **Depth:** 12-14

**Sample Number:** 7

**Proj. No.:** APS2008-G063

**Date Sampled:** 8-12-2020





Sample No.	1	
Initial	Water Content, %	104.7
	Dry Density, pcf	45.6
	Saturation, %	104.9
	Void Ratio	2.6936
	Diameter, in.	2.81
At Test	Height, in.	5.75
	Water Content, %	104.7
	Dry Density, pcf	45.6
	Saturation, %	104.9
	Void Ratio	2.6936
Diameter, in.	2.81	
Height, in.	5.75	
Strain at peak, %	14.7	
Back Pressure, psi	0.00	
Cell Pressure, psi	6.40	
Fail. Stress, psf	547	
Ult. Stress, psf	547	
$\sigma_1$ Failure, psf	1469	
$\sigma_3$ Failure, psf	922	

**Type of Test:**

Unconsolidated Undrained

**Sample Type:** Undisturbed

**Description:** Soft Gray Fat Clay (CH)

**LL=** 101      **PL=** 29      **PI=** 72

**Assumed Specific Gravity=** 2.7

**Remarks:** Failure Type : Bulge

Failure limit to 15%

**Client:** CPRA

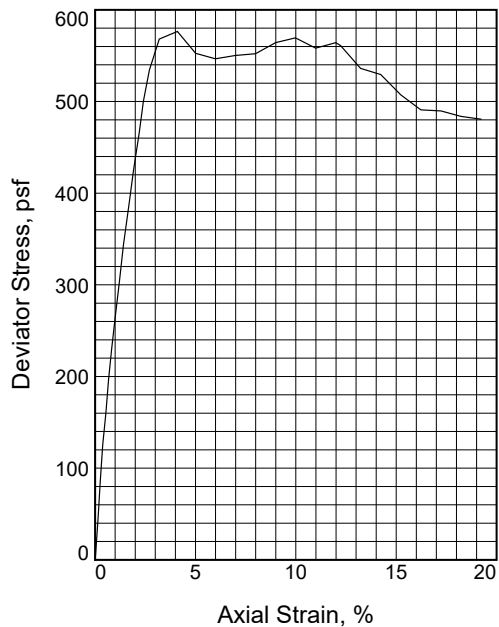
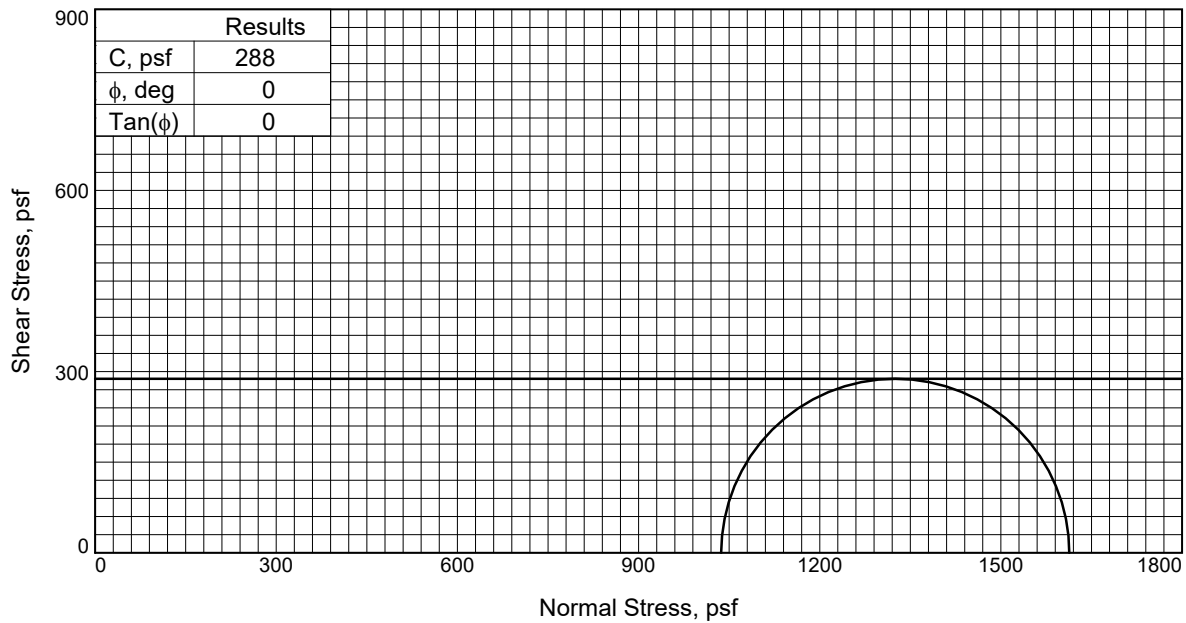
**Project:** BRETON LANDBRIDGE MARSH CREATION

**Source of Sample:** B-2      **Depth:** 14-16

**Sample Number:** 8

**Proj. No.:** APS2008-G063      **Date Sampled:** 8-12-2020





Sample No.	1	
Initial	Water Content, %	92.1
	Dry Density, pcf	49.1
	Saturation, %	102.3
	Void Ratio	2.4294
	Diameter, in.	2.83
	Height, in.	5.76
At Test	Water Content, %	92.1
	Dry Density, pcf	49.1
	Saturation, %	102.3
	Void Ratio	2.4294
	Diameter, in.	2.83
	Height, in.	5.76
Strain at peak, %	4.1	
Back Pressure, psi	0.00	
Cell Pressure, psi	7.20	
Fail. Stress, psf	576	
Ult. Stress, psf	576	
$\sigma_1$ Failure, psf	1613	
$\sigma_3$ Failure, psf	1037	

**Type of Test:**

Unconsolidated Undrained

**Sample Type:** Undisturbed

**Description:** Soft Gray Fat Clay (CH)

**LL=** 129      **PL=** 36      **PI=** 93

**Assumed Specific Gravity=** 2.7

**Remarks:** Failure Type : Bulge and Muti shear  
Failure limit to 15%

**Client:** CPRA

**Project:** BRETON LANDBRIDGE MARSH CREATION

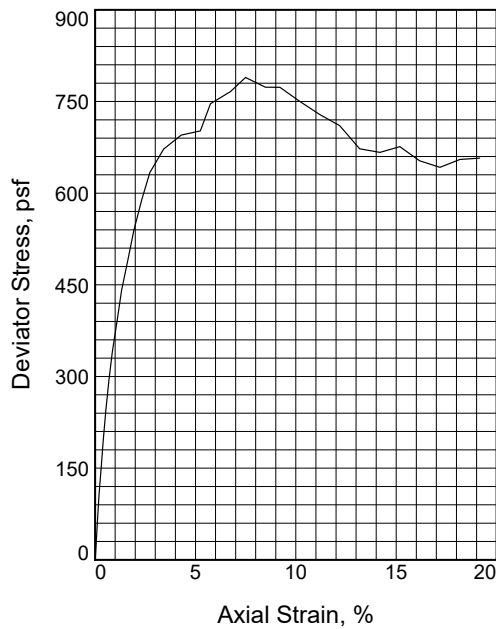
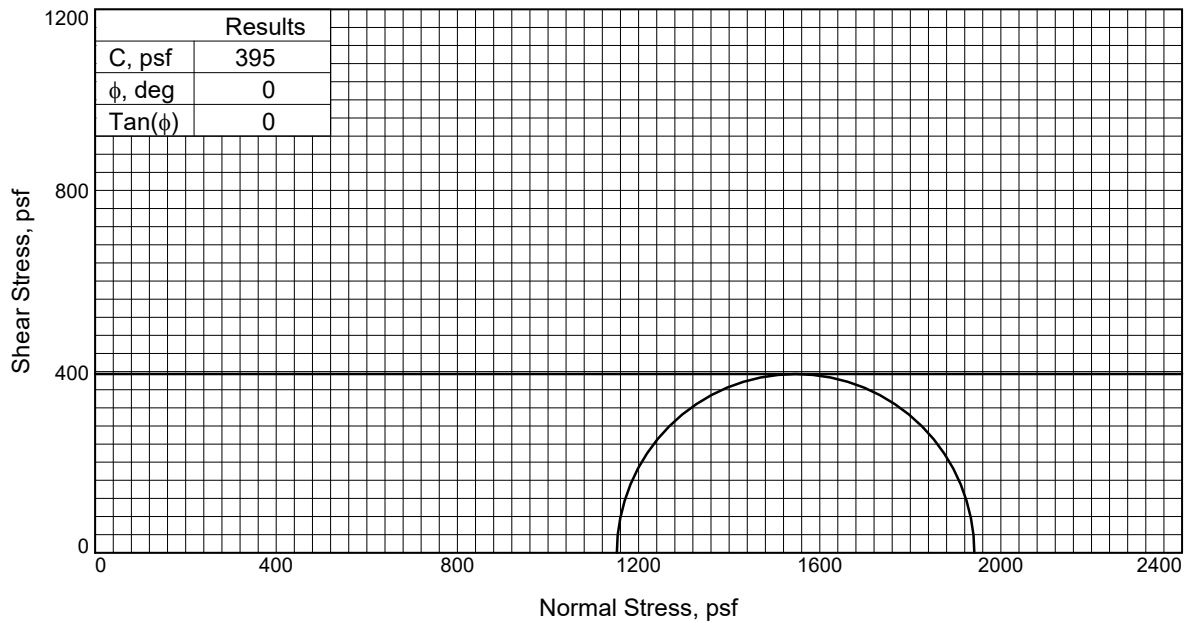
**Source of Sample:** B-2      **Depth:** 16-18

**Sample Number:** 9

**Proj. No.:** APS2008-G063

**Date Sampled:** 8-12-2020





Sample No.	1	
Initial	Water Content, %	85.8
	Dry Density, pcf	47.7
	Saturation, %	91.4
	Void Ratio	2.5360
	Diameter, in.	2.82
	Height, in.	5.77
At Test	Water Content, %	85.8
	Dry Density, pcf	47.7
	Saturation, %	91.4
	Void Ratio	2.5360
	Diameter, in.	2.82
	Height, in.	5.77
Strain at peak, %	7.5	
Back Pressure, psi	0.00	
Cell Pressure, psi	8.00	
Fail. Stress, psf	789	
Ult. Stress, psf	789	
$\sigma_1$ Failure, psf	1941	
$\sigma_3$ Failure, psf	1152	

**Type of Test:**

Unconsolidated Undrained

**Sample Type:** Undisturbed

**Description:** Soft Gray Fat Clay (CH)

**LL=** 103      **PL=** 23      **PI=** 80

**Assumed Specific Gravity=** 2.7

**Remarks:** Failure Type : Bulge

**Client:** CPRA

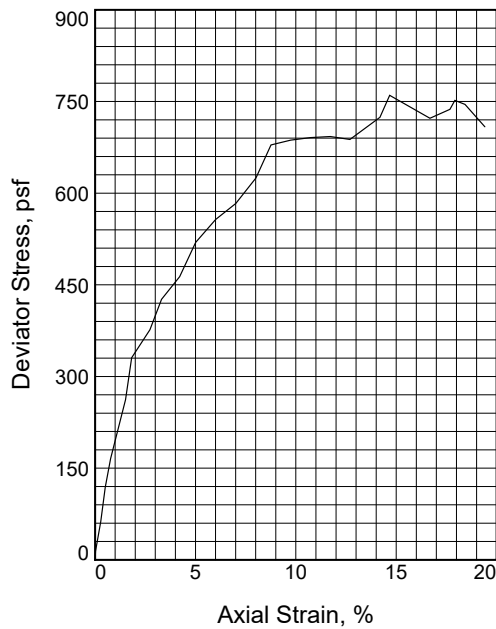
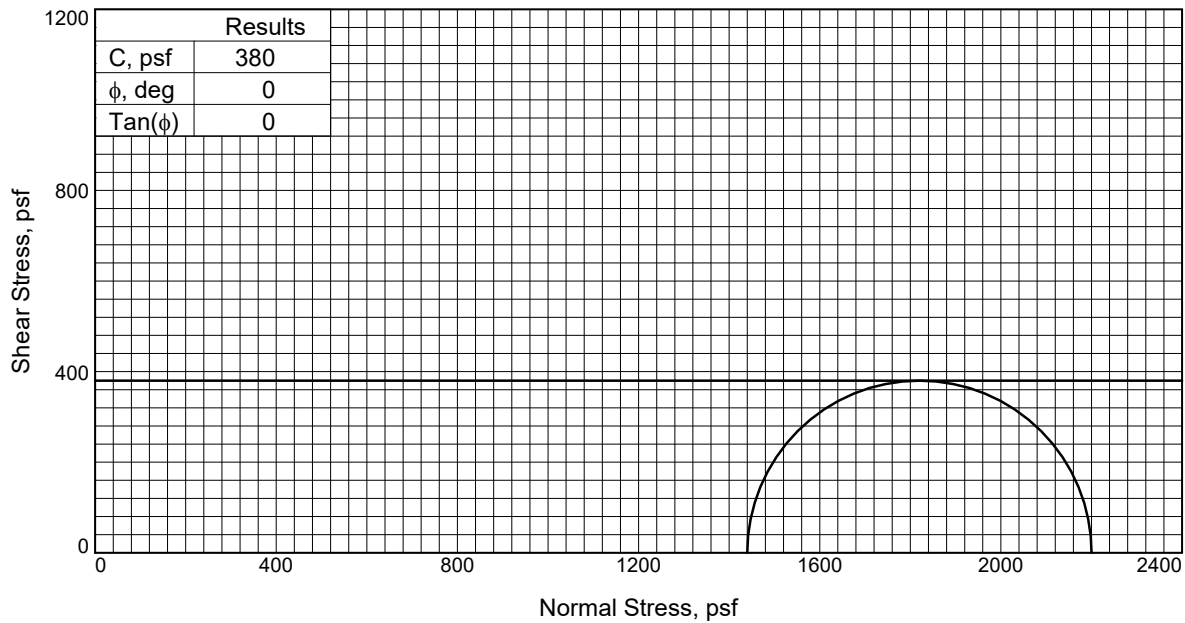
**Project:** BRETON LANDBRIDGE MARSH CREATION

**Source of Sample:** B-2      **Depth:** 18-20

**Sample Number:** 10

**Proj. No.:** APS2008-G063      **Date Sampled:** 8-12-2020





Sample No.	1	
Initial	Water Content, %	56.0
	Dry Density, pcf	69.1
	Saturation, %	104.9
	Void Ratio	1.4410
	Diameter, in.	2.78
	Height, in.	5.80
At Test	Water Content, %	56.0
	Dry Density, pcf	69.1
	Saturation, %	104.9
	Void Ratio	1.4410
	Diameter, in.	2.78
	Height, in.	5.80
Strain at peak, %	14.7	
Back Pressure, psi	0.00	
Cell Pressure, psi	10.00	
Fail. Stress, psf	760	
Ult. Stress, psf	760	
$\sigma_1$ Failure, psf	2200	
$\sigma_3$ Failure, psf	1440	

**Type of Test:**

Unconsolidated Undrained

**Sample Type:** Undisturbed

**Description:** Soft Gray Lean Clay (CL)-with fine sand

**LL= 40      PL= 19      PI= 21**

**Assumed Specific Gravity= 2.7**

**Remarks:** Failure Type : Bulge

Failure limit to 15%

**Client:** CPRA

**Project:** BRETON LANDBRIDGE MARSH CREATION

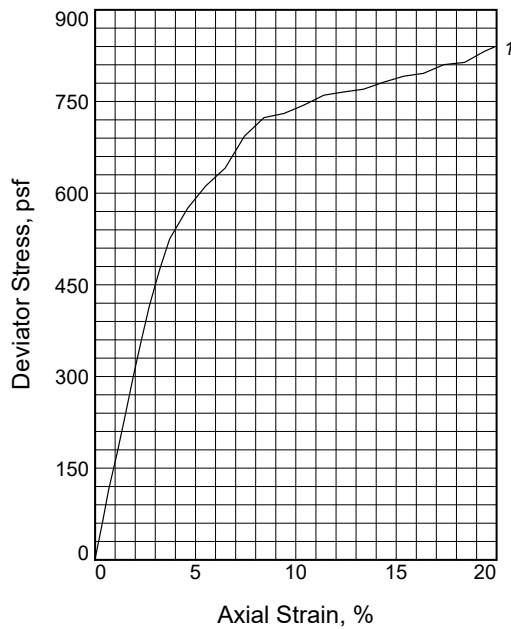
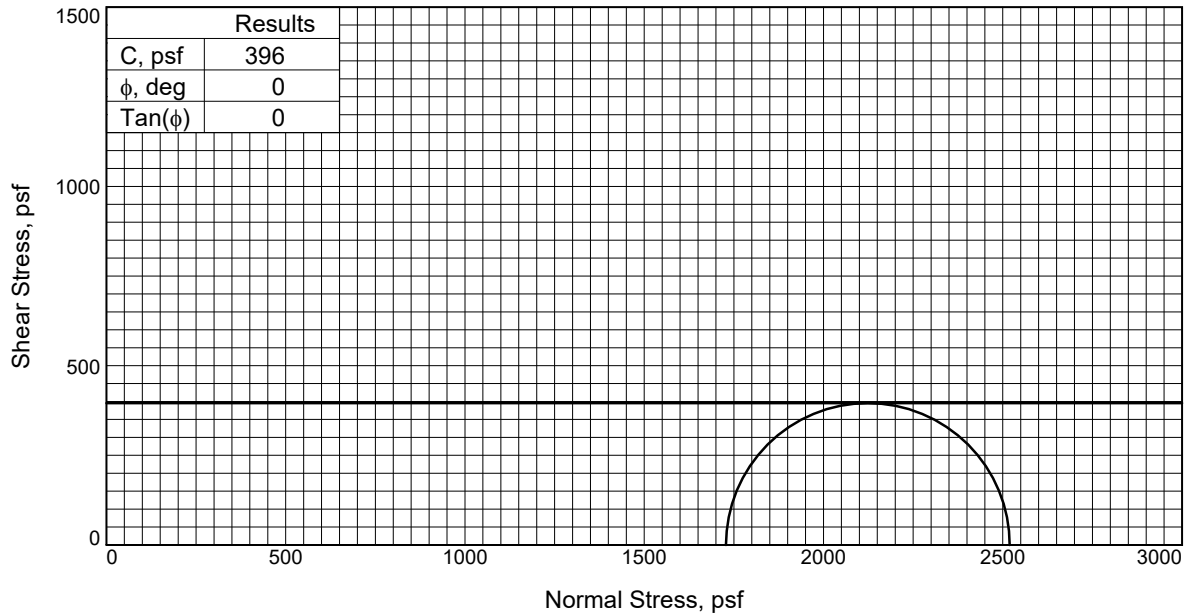
**Source of Sample:** B-2      **Depth:** 23-25

**Sample Number:** 11

**Proj. No.:** APS2008-G063

**Date Sampled:** 8-12-2020





Sample No.	1	
Initial	Water Content, %	46.4
	Dry Density, pcf	76.7
	Saturation, %	104.7
	Void Ratio	1.1980
	Diameter, in.	2.79
At Test	Height, in.	5.76
	Water Content, %	46.4
	Dry Density, pcf	76.7
	Saturation, %	104.7
	Void Ratio	1.1980
Diameter, in.	2.79	
Height, in.	5.76	
Strain at peak, %	15.4	
Back Pressure, psi	0.00	
Cell Pressure, psi	12.00	
Fail. Stress, psf	791	
Ult. Stress, psf	791	
$\sigma_1$ Failure, psf	2519	
$\sigma_3$ Failure, psf	1728	

**Type of Test:**

Unconsolidated Undrained

**Sample Type:** Undisturbed

**Description:** Soft Gray Fat Clay (CH)

**LL= 50      PL= 22      PI= 28**

**Assumed Specific Gravity= 2.7**

**Remarks:** Failure Type : Bulge

Failure limit to 15%

**Client:** CPRA

**Project:** BRETON LANDBRIDGE MARSH CREATION

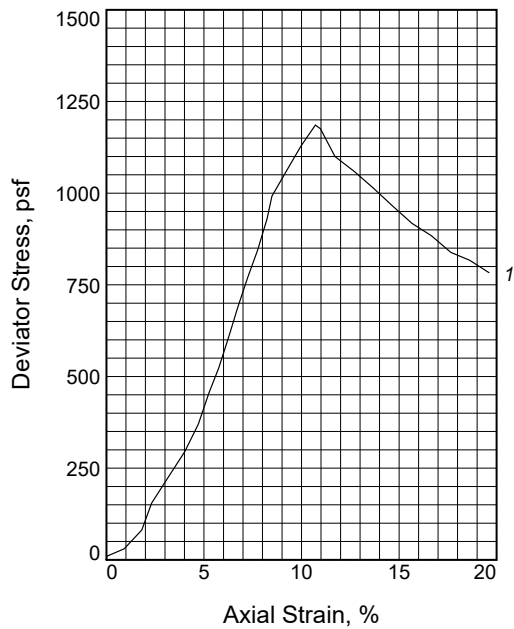
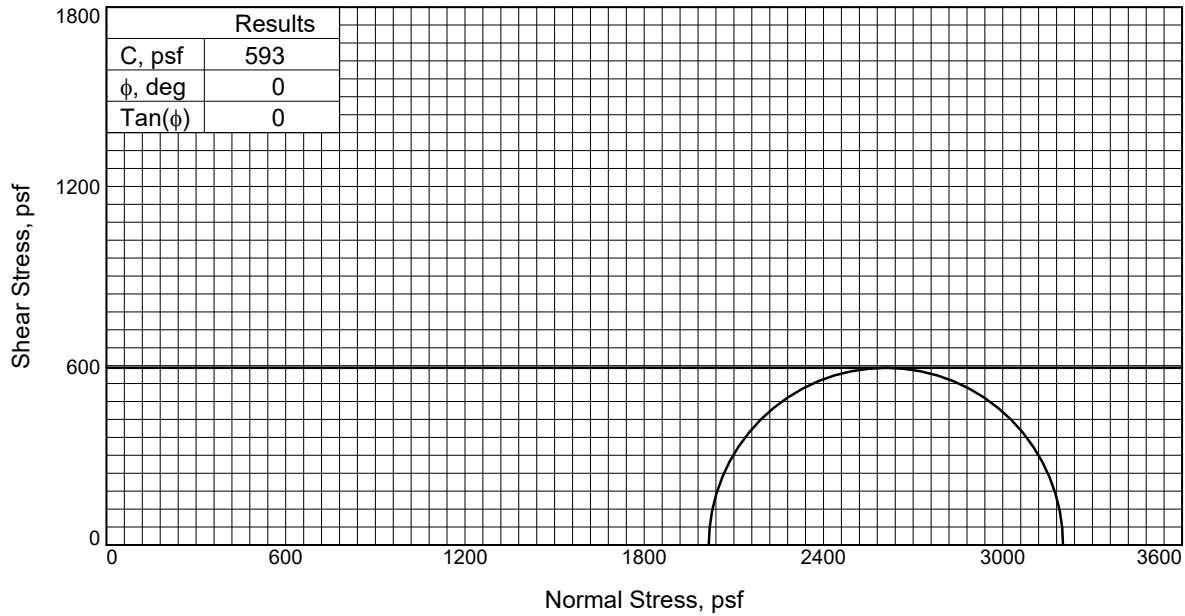
**Source of Sample:** B-2      **Depth:** 28-30

**Sample Number:** 12

**Proj. No.:** APS2008-G063

**Date Sampled:** 8-12-2020





Sample No.	1	
Initial	Water Content, %	590.9
	Dry Density, pcf	17.2
	Saturation, %	181.2
	Void Ratio	8.8066
	Diameter, in.	2.81
	Height, in.	5.65
At Test	Water Content, %	30.2
	Dry Density, pcf	17.2
	Saturation, %	9.3
	Void Ratio	8.8066
	Diameter, in.	2.81
	Height, in.	5.65
Strain at peak, %	10.7	
Back Pressure, psi	0.00	
Cell Pressure, psi	14.00	
Fail. Stress, psf	1186	
Ult. Stress, psf	1186	
$\sigma_1$ Failure, psf	3202	
$\sigma_3$ Failure, psf	2016	

**Type of Test:**

Unconsolidated Undrained

**Sample Type:** Undisturbed

**Description:** Gray Silty Clay (CL-ML)

**LL=** NP

**PI=** NP

**Assumed Specific Gravity=** 2.7

**Remarks:** Failure Type : Bulge

**Client:** CPRA

**Project:** BRETON LANDBRIDGE MARSH CREATION

**Source of Sample:** B-2

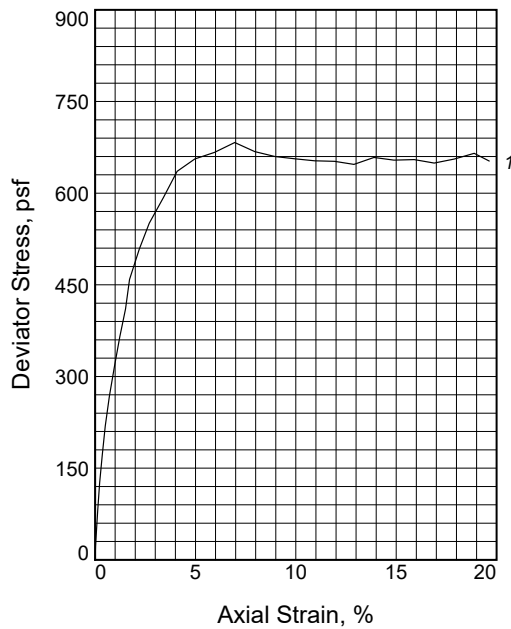
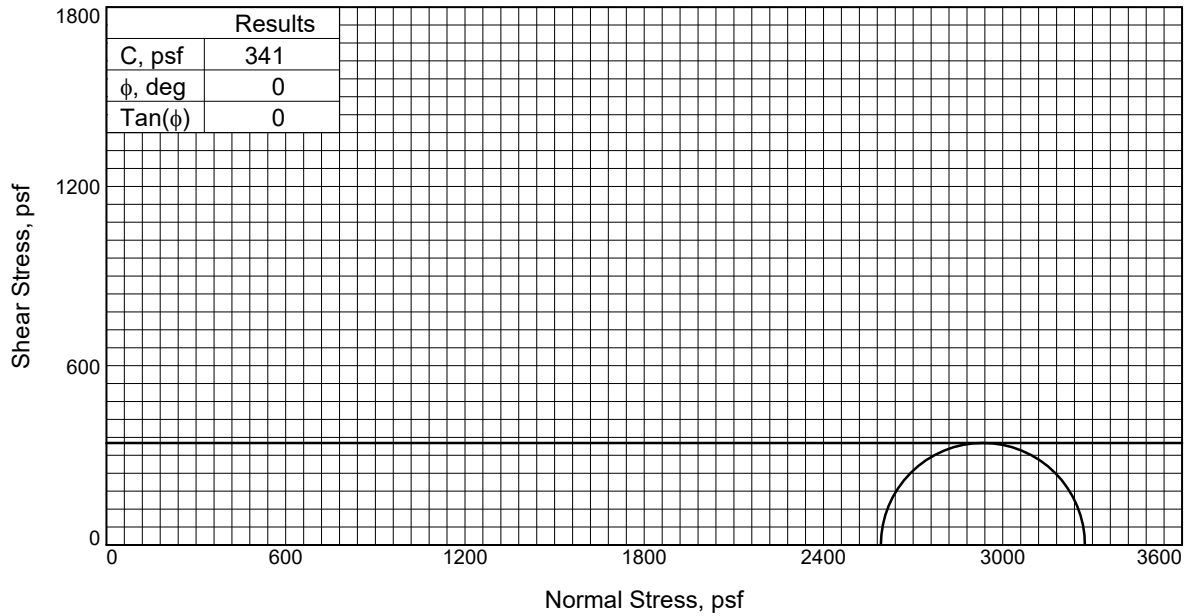
**Depth:** 33-35

**Sample Number:** 13

**Proj. No.:** APS2008-G063

**Date Sampled:** 8-12-2020





Sample No.	1	
Initial	Water Content, %	72.4
	Dry Density, pcf	57.1
	Saturation, %	100.3
	Void Ratio	1.9495
	Diameter, in.	2.85
	Height, in.	5.82
At Test	Water Content, %	72.4
	Dry Density, pcf	57.1
	Saturation, %	100.3
	Void Ratio	1.9495
	Diameter, in.	2.85
	Height, in.	5.82
Strain at peak, %	7.0	
Back Pressure, psi	0.00	
Cell Pressure, psi	18.00	
Fail. Stress, psf	683	
Ult. Stress, psf	683	
$\sigma_1$ Failure, psf	3275	
$\sigma_3$ Failure, psf	2592	

**Type of Test:**  
Unconsolidated Undrained

**Sample Type:** Undisturbed

**Description:** Soft Gray Fat Clay(CH)

**LL= 96      PL= 31      PI= 65**

**Assumed Specific Gravity= 2.7**

**Remarks:** Failure Type : Bulge

**Client:** CPRA

**Project:** BRETON LANDBRIDGE MARSH CREATION

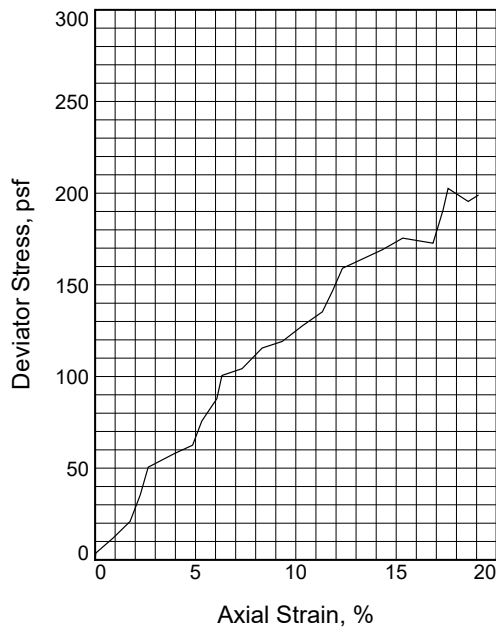
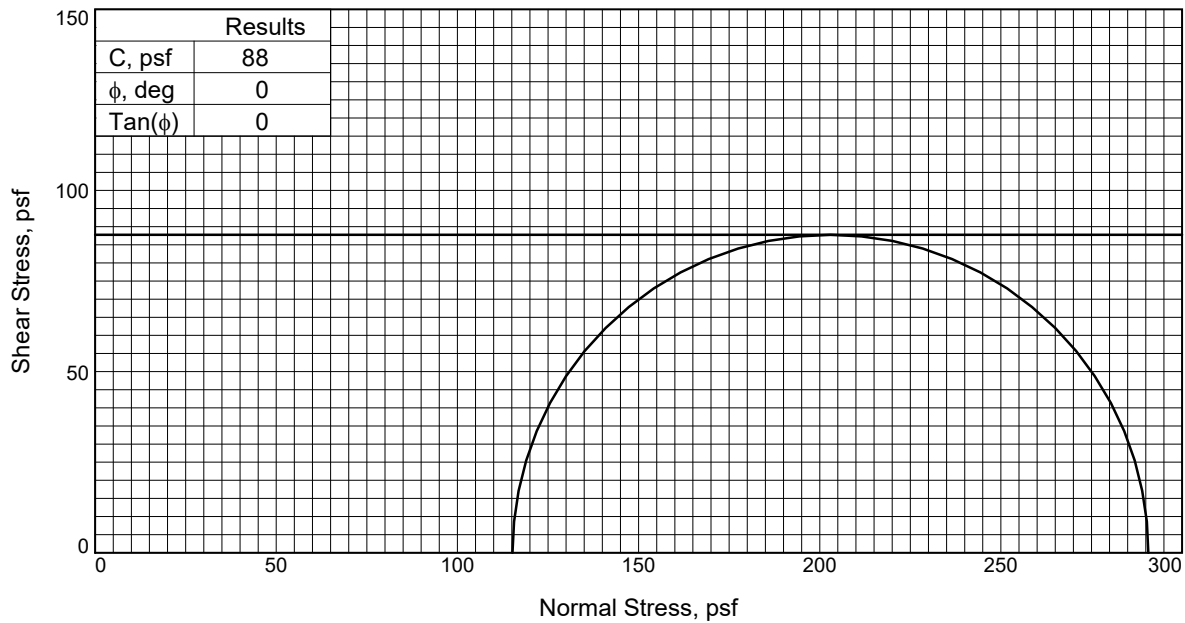
**Source of Sample:** B-2      **Depth:** 43-45

**Sample Number:** 15

**Proj. No.:** APS2008-G063      **Date Sampled:** 8-12-2020







Sample No.	1	
Initial	Water Content, %	475.7
	Dry Density, pcf	11.9
	Saturation, %	101.2
	Void Ratio	8.6489
	Diameter, in.	2.72
At Test	Height, in.	5.91
	Water Content, %	475.7
	Dry Density, pcf	11.9
	Saturation, %	101.2
	Void Ratio	8.6489
Diameter, in.	2.72	
Height, in.	5.91	
Strain at peak, %	15.3	
Back Pressure, psi	0.00	
Cell Pressure, psi	0.80	
Fail. Stress, psf	176	
Ult. Stress, psf	176	
$\sigma_1$ Failure, psf	291	
$\sigma_3$ Failure, psf	115	

**Type of Test:**

Unconsolidated Undrained

**Sample Type:** Undisturbed

**Description:** Black Peat (PT)

**LL=** 538      **PL=** 127      **PI=** 411

**Specific Gravity=** 1.84

**Remarks:** Failure Type : Bulge  
Failure limit to 15%

**Client:** CPRA

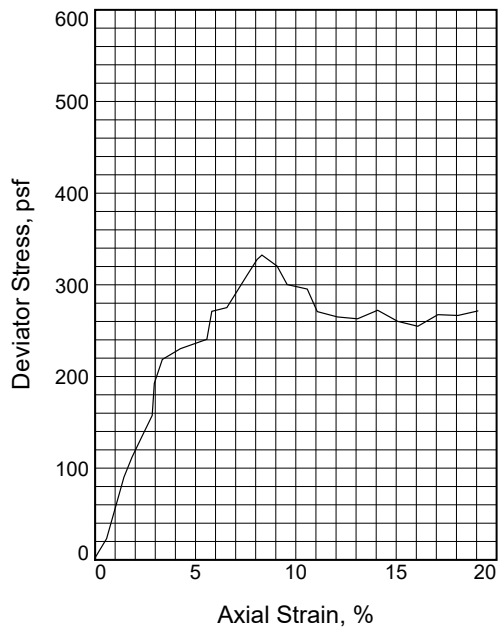
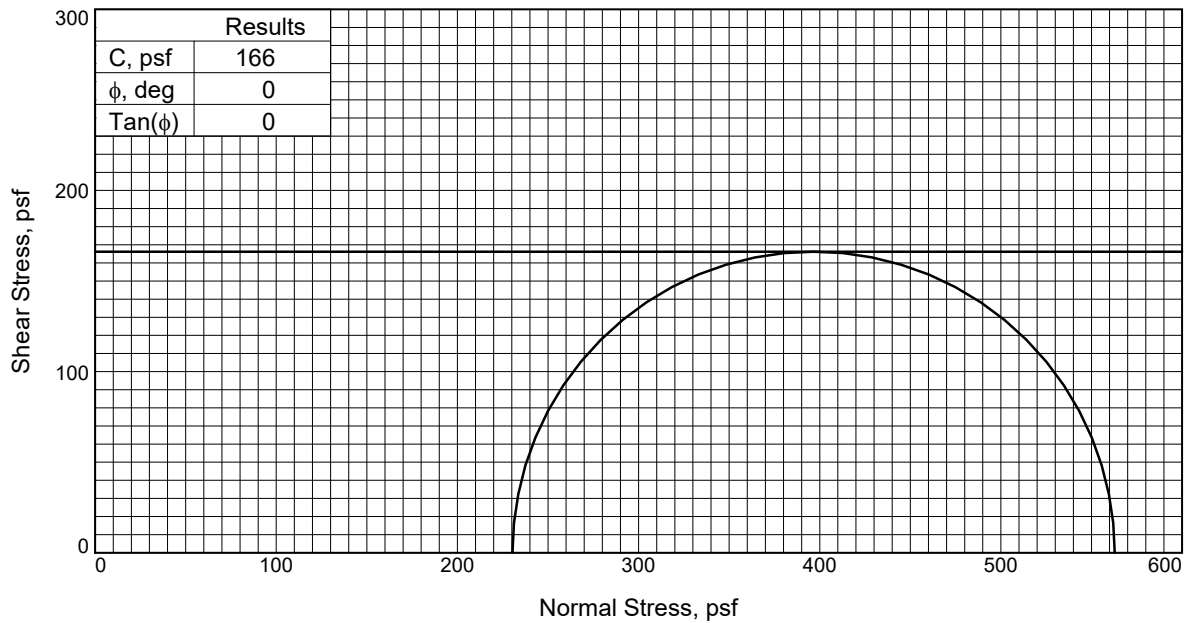
**Project:** BRETON LANDBRIDGE MARSH CREATION

**Source of Sample:** B-3      **Depth:** 0-2

**Sample Number:** 1

**Proj. No.:** APS2008-G063      **Date Sampled:** 8-15-2020





Sample No.	1	
Initial	Water Content, %	52.6
	Dry Density, pcf	61.2
	Saturation, %	81.1
	Void Ratio	1.7532
	Diameter, in.	2.68
At Test	Height, in.	5.94
	Water Content, %	52.6
	Dry Density, pcf	61.2
	Saturation, %	81.1
	Void Ratio	1.7532
Diameter, in.	2.68	
Height, in.	5.94	
Strain at peak, %	8.3	
Back Pressure, psi	0.00	
Cell Pressure, psi	1.60	
Fail. Stress, psf	332	
Ult. Stress, psf	332	
$\sigma_1$ Failure, psf	563	
$\sigma_3$ Failure, psf	230	

**Type of Test:**

Unconsolidated Undrained

**Sample Type:** Undisturbed

**Description:** Very Soft Dark Gray Fat Clay (CH)

LL= 57      PL= 27      PI= 30

**Assumed Specific Gravity=** 2.7

**Remarks:** Failure Type : Bulge

**Client:** CPRA

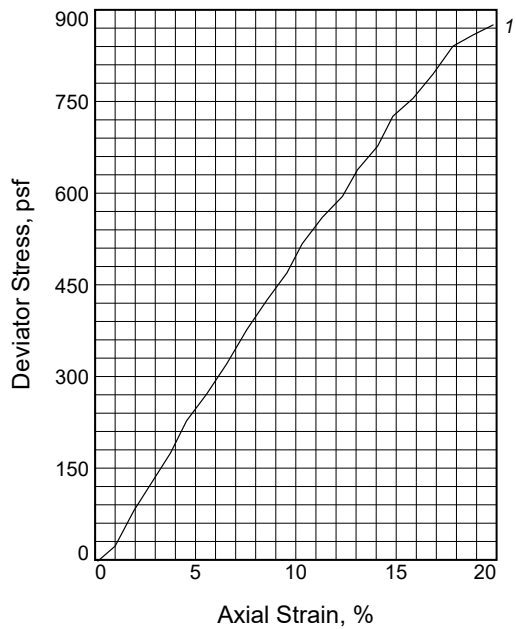
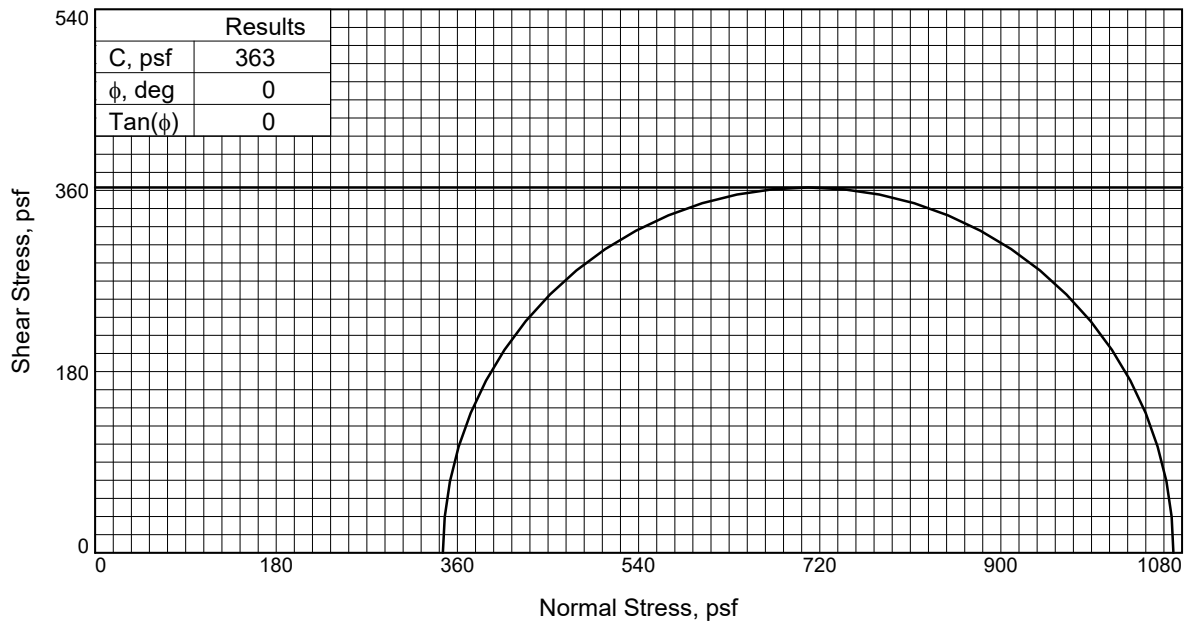
**Project:** BRETON LANDBRIDGE MARSH CREATION

**Source of Sample:** B-3      **Depth:** 2-4

**Sample Number:** 2

**Proj. No.:** APS2008-G063      **Date Sampled:** 8-15-2020





Sample No.	1	
Initial	Water Content, %	32.5
	Dry Density, pcf	87.8
	Saturation, %	95.4
	Void Ratio	0.9199
	Diameter, in.	2.75
At Test	Height, in.	5.86
	Water Content, %	32.5
	Dry Density, pcf	87.8
	Saturation, %	95.4
	Void Ratio	0.9199
Diameter, in.	2.75	
Height, in.	5.86	
Strain at peak, %	14.8	
Back Pressure, psi	0.00	
Cell Pressure, psi	2.40	
Fail. Stress, psf	726	
Ult. Stress, psf	726	
$\sigma_1$ Failure, psf	1071	
$\sigma_3$ Failure, psf	346	

**Type of Test:**

Unconsolidated Undrained

**Sample Type:** Undisturbed

**Description:** Gray Silt with Sand(ML)

LL= NV

PI= NP

**Assumed Specific Gravity=** 2.7

**Remarks:** Failure Type : Bulge and Multi

Shear

Failure limit to 15%

**Client:** CPRA

**Project:** BRETON LANDBRIDGE MARSH CREATION

**Source of Sample:** B-3

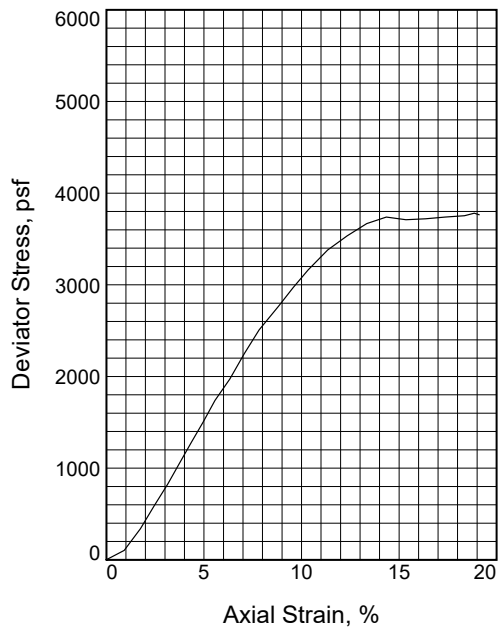
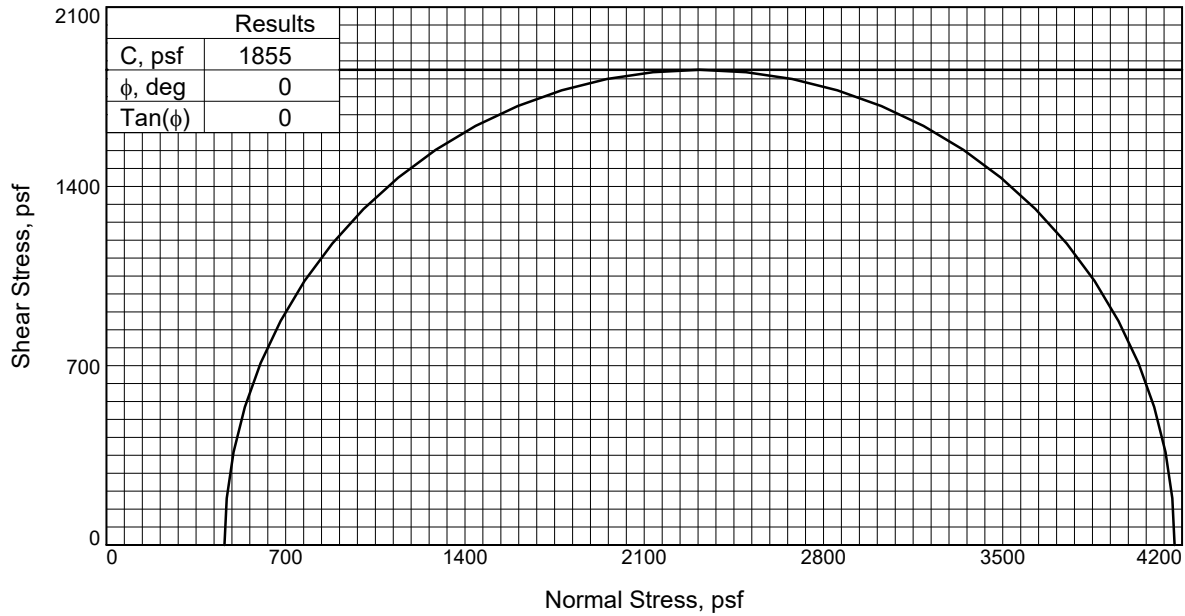
**Depth:** 4-6

**Sample Number:** 3

**Proj. No.:** APS2008-G063

**Date Sampled:** 8-15-2020





Sample No.	1	
Initial	Water Content, %	28.6
	Dry Density, pcf	96.8
	Saturation, %	104.1
	Void Ratio	0.7413
	Diameter, in.	2.82
At Test	Height, in.	5.66
	Water Content, %	28.6
	Dry Density, pcf	96.8
	Saturation, %	104.1
	Void Ratio	0.7413
Diameter, in.	2.82	
Height, in.	5.66	
Strain at peak, %	15.4	
Back Pressure, psi	0.00	
Cell Pressure, psi	3.20	
Fail. Stress, psf	3710	
Ult. Stress, psf	3710	
$\sigma_1$ Failure, psf	4171	
$\sigma_3$ Failure, psf	461	

**Type of Test:**

Unconsolidated Undrained

**Sample Type:** Undisturbed

**Description:** Gray Silt with Sand(ML)

LL= NV

PI= NP

**Assumed Specific Gravity=** 2.7

**Remarks:** Failure Type : Bulge

Failure limit to 15%

**Client:** CPRA

**Project:** BRETON LANDBRIDGE MARSH CREATION

**Source of Sample:** B-3

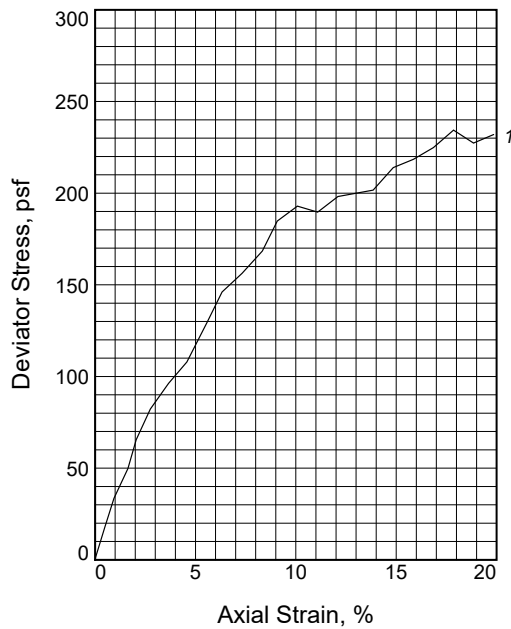
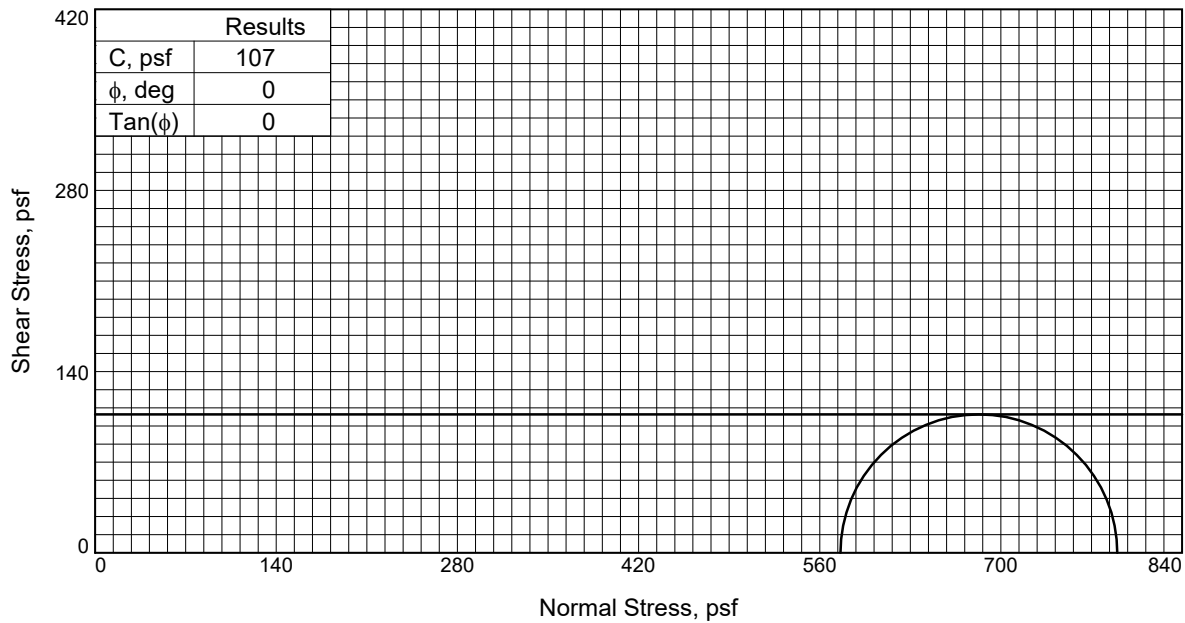
**Depth:** 6-8

**Sample Number:** 4

**Proj. No.:** APS2008-G063

**Date Sampled:** 8-15-2020





Sample No.	1	
Initial	Water Content, %	40.3
	Dry Density, pcf	68.8
	Saturation, %	75.0
	Void Ratio	1.4487
	Diameter, in.	2.89
	Height, in.	5.96
At Test	Water Content, %	40.3
	Dry Density, pcf	68.8
	Saturation, %	75.0
	Void Ratio	1.4487
	Diameter, in.	2.89
	Height, in.	5.96
Strain at peak, %	14.9	
Back Pressure, psi	0.00	
Cell Pressure, psi	4.00	
Fail. Stress, psf	214	
Ult. Stress, psf	214	
$\sigma_1$ Failure, psf	790	
$\sigma_3$ Failure, psf	576	

**Type of Test:**

Unconsolidated Undrained

**Sample Type:** Undisturbed

**Description:** Very Soft Gray Sandy Silty Clay (CL-ML)

**LL= 34      PL= 29      PI= 5**

**Assumed Specific Gravity= 2.7**

**Remarks:** Failure Type : Bulge  
Failure limit to 15%

**Client:** CPRA

**Project:** BRETON LANDBRIDGE MARSH CREATION

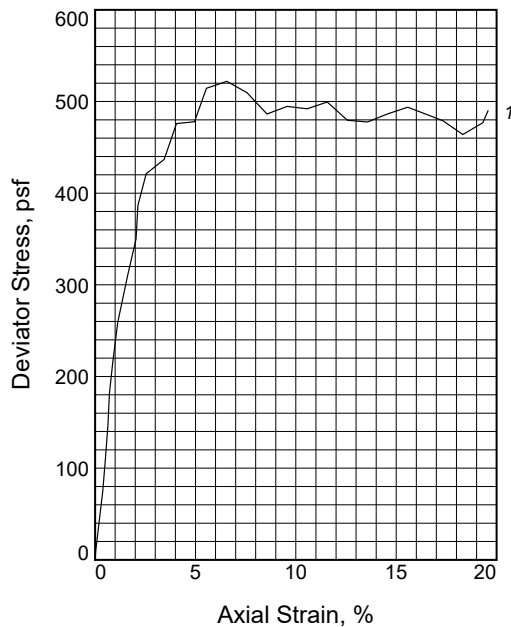
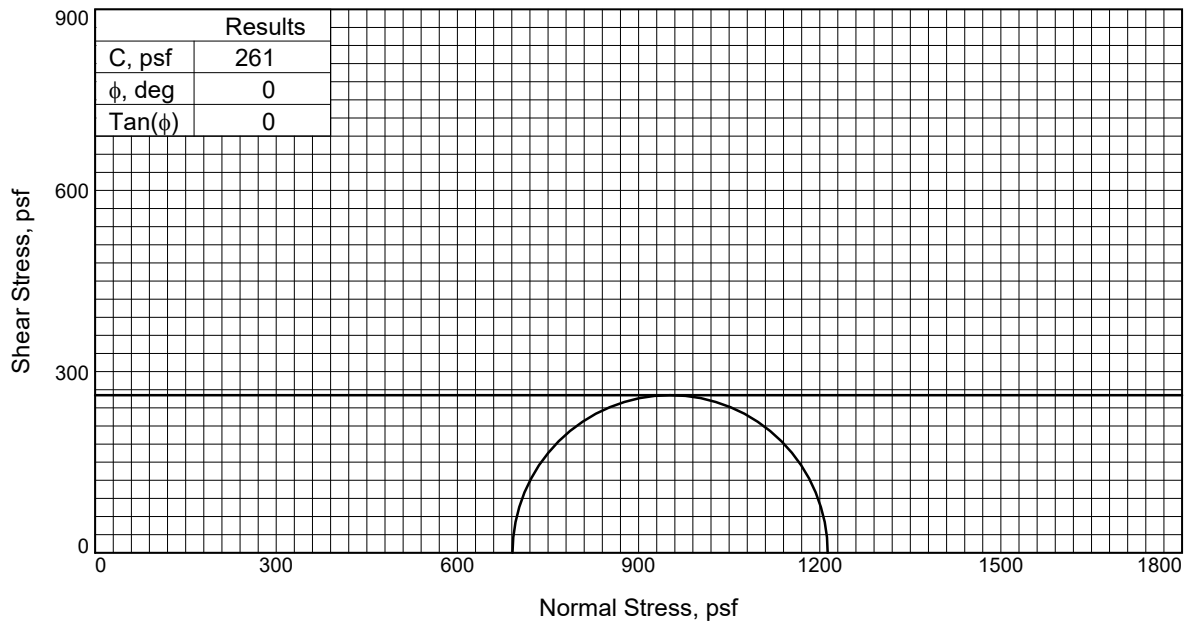
**Source of Sample:** B-3      **Depth:** 8-10

**Sample Number:** 5

**Proj. No.:** APS2008-G063

**Date Sampled:** 8-15-2020





Sample No.	1	
Initial	Water Content, %	90.4
	Dry Density, pcf	48.8
	Saturation, %	100.6
	Void Ratio	2.3546
	Diameter, in.	2.81
	Height, in.	5.83
At Test	Water Content, %	90.4
	Dry Density, pcf	48.8
	Saturation, %	100.6
	Void Ratio	2.3546
	Diameter, in.	2.81
	Height, in.	5.83
Strain at peak, %	6.6	
Back Pressure, psi	0.00	
Cell Pressure, psi	4.80	
Fail. Stress, psf	522	
Ult. Stress, psf	522	
$\sigma_1$ Failure, psf	1213	
$\sigma_3$ Failure, psf	691	

**Type of Test:**

Unconsolidated Undrained

**Sample Type:** Undisturbed

**Description:** Soft gray fat clay (CH)

LL= 99      PL= 27      PI= 72

**Specific Gravity=** 2.62

**Remarks:** Failure Type : Bulge

**Client:** CPRA

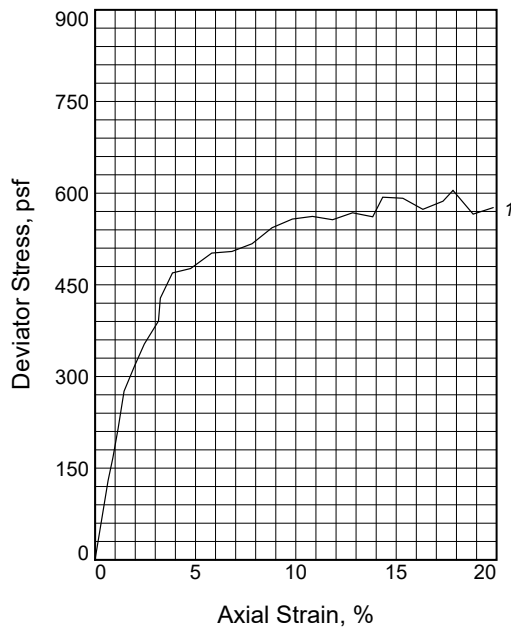
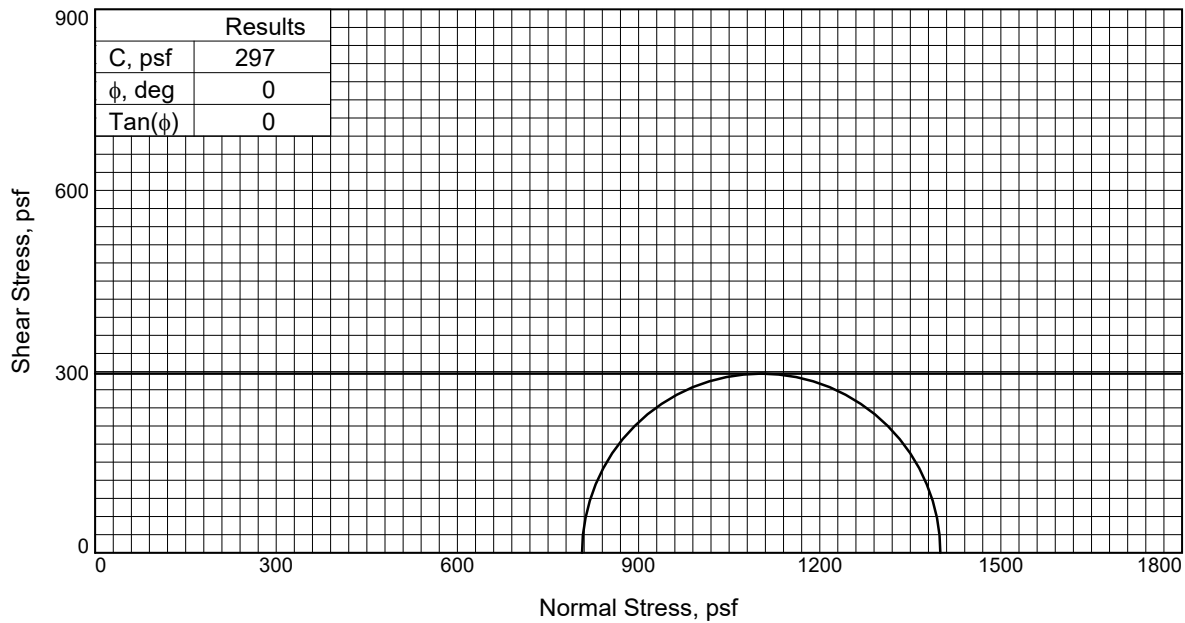
**Project:** BRETON LANDBRIDGE MARSH CREATION

**Source of Sample:** B-3      **Depth:** 10-12

**Sample Number:** 6

**Proj. No.:** APS2008-G063      **Date Sampled:** 8-15-2020





Sample No.	1	
Initial	Water Content, %	67.1
	Dry Density, pcf	56.6
	Saturation, %	91.6
	Void Ratio	1.9785
	Diameter, in.	2.83
	Height, in.	5.78
At Test	Water Content, %	67.1
	Dry Density, pcf	56.6
	Saturation, %	91.6
	Void Ratio	1.9785
	Diameter, in.	2.83
	Height, in.	5.78
Strain at peak, %	14.3	
Back Pressure, psi	0.00	
Cell Pressure, psi	5.60	
Fail. Stress, psf	593	
Ult. Stress, psf	593	
$\sigma_1$ Failure, psf	1400	
$\sigma_3$ Failure, psf	806	

**Type of Test:**

Unconsolidated Undrained

**Sample Type:** Undisturbed

**Description:** Soft Gray Fat Clay (CH)

**LL=** 110      **PL=** 31      **PI=** 79

**Assumed Specific Gravity=** 2.7

**Remarks:** Failure Type : Bulge

Failure limit to 15%

**Client:** CPRA

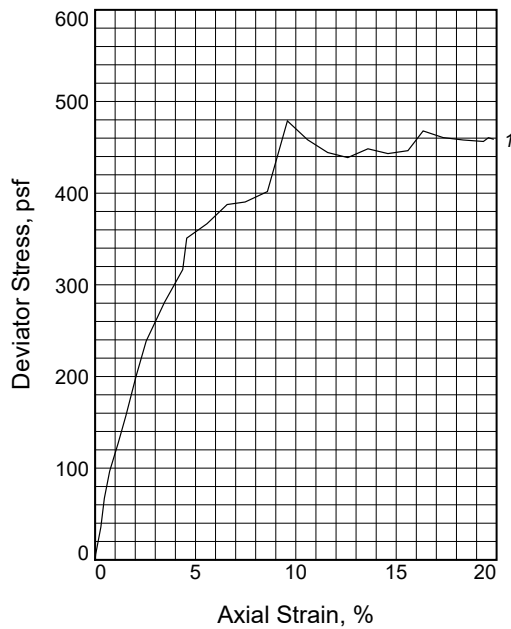
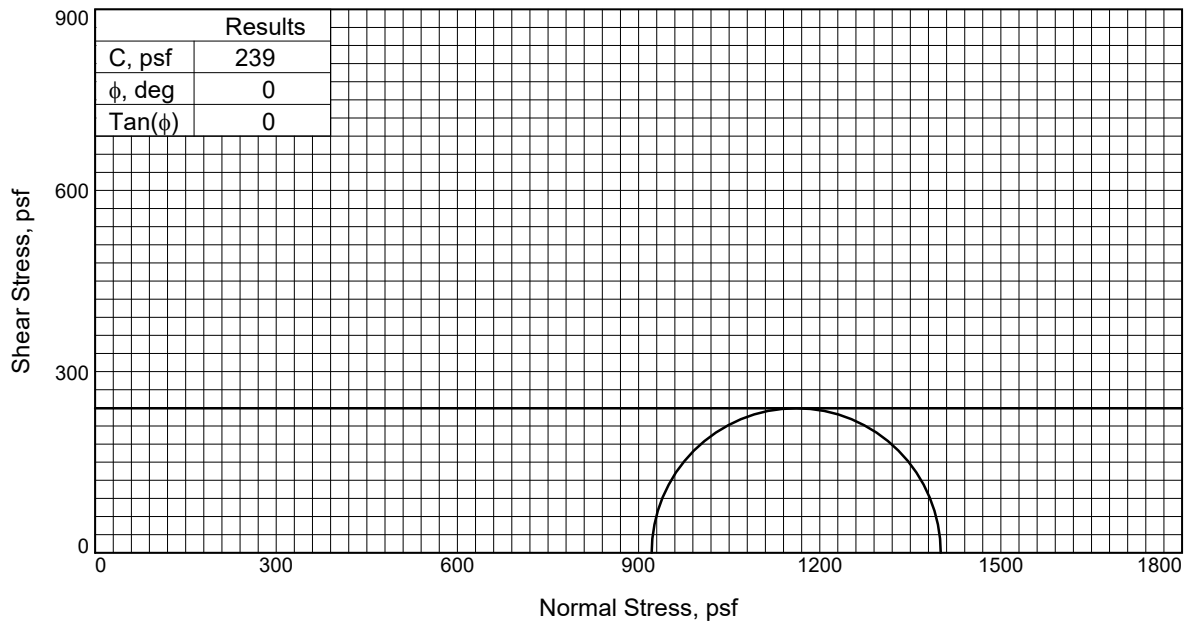
**Project:** BRETON LANDBRIDGE MARSH CREATION

**Source of Sample:** B-3      **Depth:** 12-14

**Sample Number:** 7

**Proj. No.:** APS2008-G063      **Date Sampled:** 8-15-2020





Sample No.	1	
Initial	Water Content, %	84.7
	Dry Density, pcf	51.5
	Saturation, %	102.6
	Void Ratio	2.1300
	Diameter, in.	2.77
	Height, in.	5.80
At Test	Water Content, %	84.7
	Dry Density, pcf	51.5
	Saturation, %	102.6
	Void Ratio	2.1300
	Diameter, in.	2.77
	Height, in.	5.80
Strain at peak, %	9.6	
Back Pressure, psi	0.00	
Cell Pressure, psi	6.40	
Fail. Stress, psf	479	
Ult. Stress, psf	479	
$\sigma_1$ Failure, psf	1400	
$\sigma_3$ Failure, psf	922	

**Type of Test:**

Unconsolidated Undrained

**Sample Type:** Undisturbed

**Description:** Very Soft Gray fat Clay (CH)

**LL=** 114      **PL=** 32      **PI=** 82

**Specific Gravity=** 2.58

**Remarks:** Failure Type : Bulge

**Client:** CPRA

**Project:** BRETON LANDBRIDGE MARSH CREATION

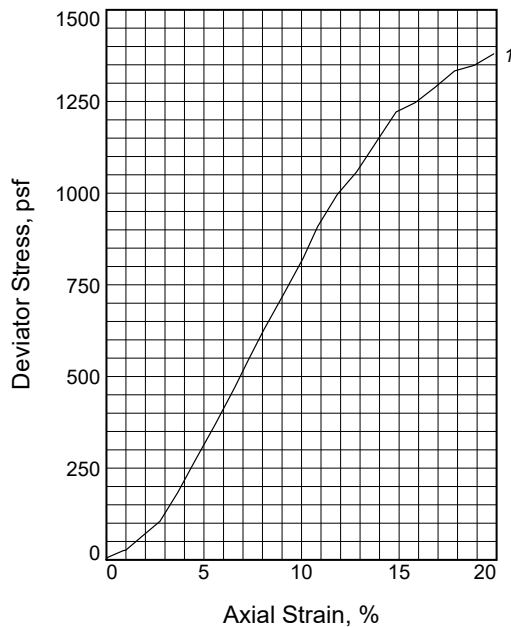
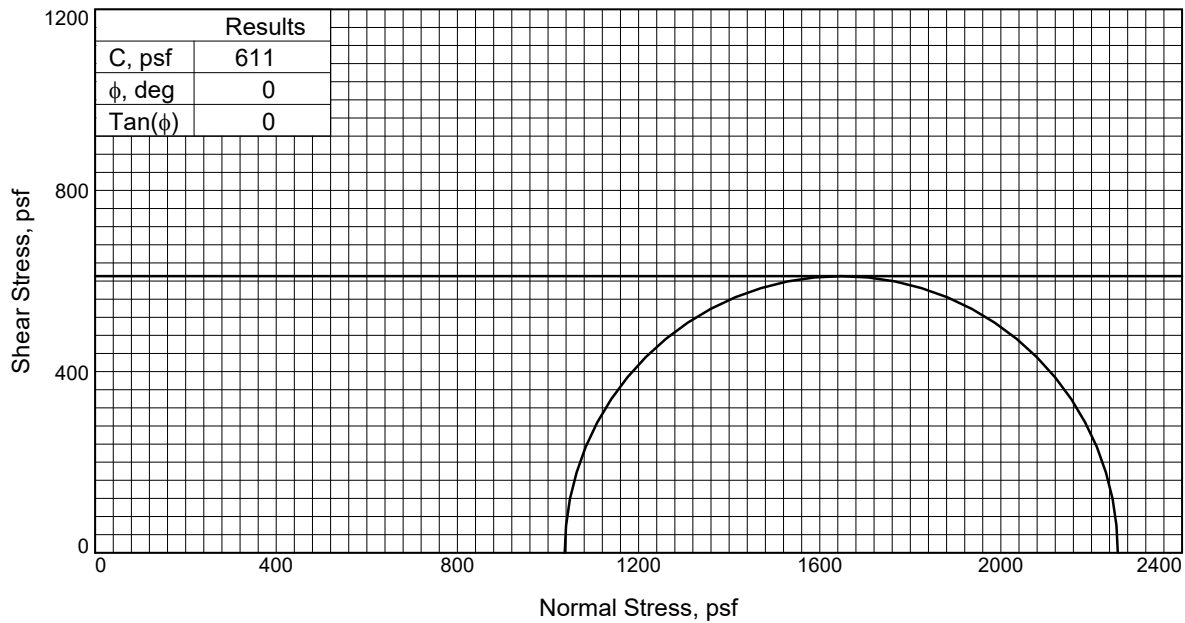
**Source of Sample:** B-3      **Depth:** 14-16

**Sample Number:** 8

**Proj. No.:** APS2008-G063      **Date Sampled:** 8-15-2020







Sample No.	1	
Initial	Water Content, %	31.6
	Dry Density, pcf	89.2
	Saturation, %	96.1
	Void Ratio	0.8889
	Diameter, in.	2.80
	Height, in.	5.86
At Test	Water Content, %	31.6
	Dry Density, pcf	89.2
	Saturation, %	96.1
	Void Ratio	0.8889
	Diameter, in.	2.80
	Height, in.	5.86
Strain at peak, %	14.8	
Back Pressure, psi	0.00	
Cell Pressure, psi	7.20	
Fail. Stress, psf	1221	
Ult. Stress, psf	1221	
$\sigma_1$ Failure, psf	2258	
$\sigma_3$ Failure, psf	1037	

**Type of Test:**

Unconsolidated Undrained

**Sample Type:** Undisturbed

**Description:** Medium Stiff Gray Fat Clay (CH)

**LL= 60      PL= 23      PI= 37**

**Assumed Specific Gravity= 2.7**

**Remarks:** Failure Type : Bulge & Multi Shear  
Failure limit to 15%

**Client:** CPRA

**Project:** BRETON LANDBRIDGE MARSH CREATION

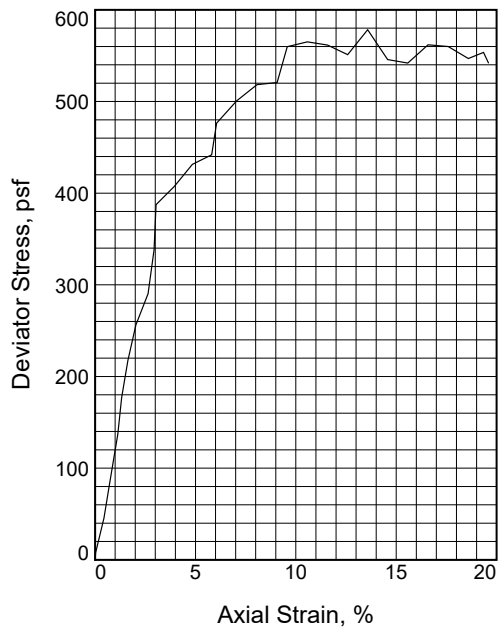
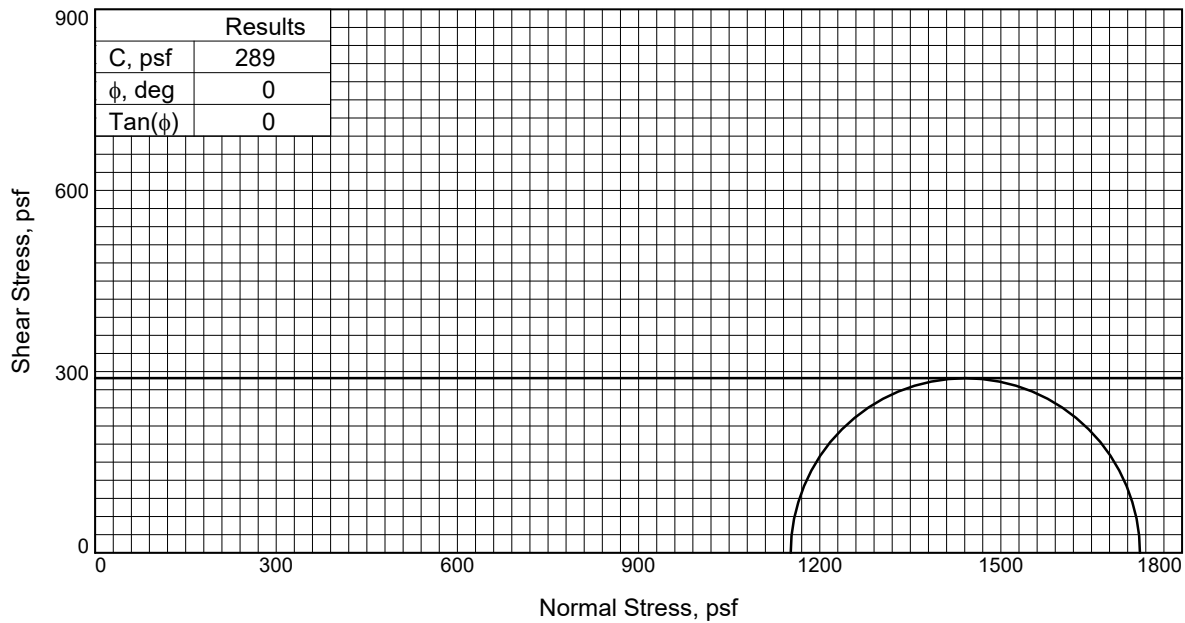
**Source of Sample:** B-3      **Depth:** 16-18

**Sample Number:** 9

**Proj. No.:** APS2008-G063

**Date Sampled:** 8-15-2020





Sample No.	1	
Initial	Water Content, %	49.9
	Dry Density, pcf	70.8
	Saturation, %	104.8
	Void Ratio	1.1771
	Diameter, in.	2.77
At Test	Water Content, %	49.9
	Dry Density, pcf	70.8
	Saturation, %	104.8
	Void Ratio	1.1771
	Diameter, in.	2.77
Height, in.	5.80	
Strain at peak, %	13.6	
Back Pressure, psi	0.00	
Cell Pressure, psi	8.00	
Fail. Stress, psf	578	
Ult. Stress, psf	578	
$\sigma_1$ Failure, psf	1730	
$\sigma_3$ Failure, psf	1152	

**Type of Test:**  
Unconsolidated Undrained

**Sample Type:** Undisturbed

**Description:** Soft Gray Fat Clay (CH)

LL= 81      PL= 23      PI= 58

**Assumed Specific Gravity=** 2.47

**Remarks:** Failure Type : Bulge

**Client:** CPRA

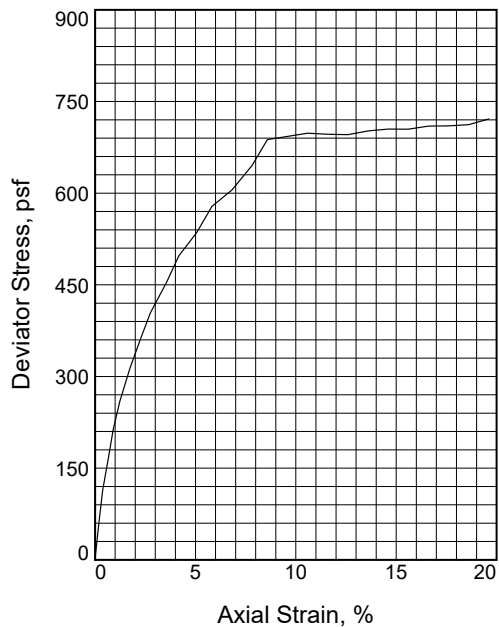
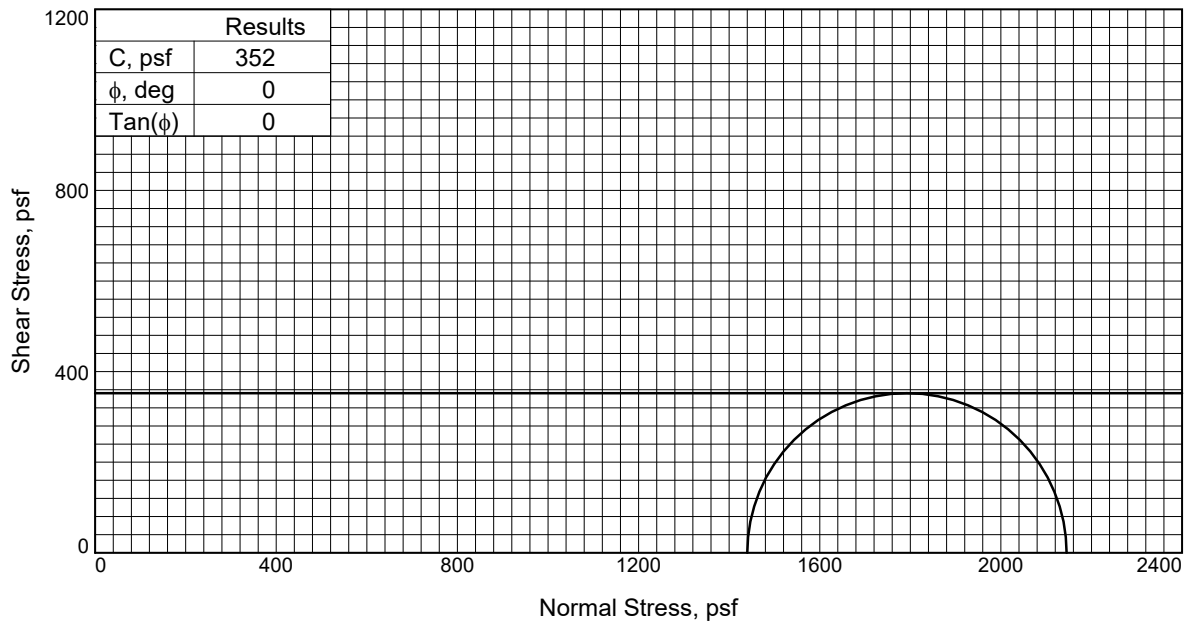
**Project:** BRETON LANDBRIDGE MARSH CREATION

**Source of Sample:** B-3      **Depth:** 18-20

**Sample Number:** 10

**Proj. No.:** APS2008-G063      **Date Sampled:** 8-15-2020





Sample No.	1	
Initial	Water Content, %	40.1
	Dry Density, pcf	78.3
	Saturation, %	94.0
	Void Ratio	1.1517
	Diameter, in.	2.80
	Height, in.	5.86
At Test	Water Content, %	40.1
	Dry Density, pcf	78.3
	Saturation, %	94.0
	Void Ratio	1.1517
	Diameter, in.	2.80
	Height, in.	5.86
Strain at peak, %	14.6	
Back Pressure, psi	0.00	
Cell Pressure, psi	10.00	
Fail. Stress, psf	705	
Ult. Stress, psf	705	
$\sigma_1$ Failure, psf	2145	
$\sigma_3$ Failure, psf	1440	

**Type of Test:**

Unconsolidated Undrained

**Sample Type:** Undisturbed

**Description:** Soft Gray Lean Clay (CL)-with fine sand

**LL= 44      PL= 20      PI= 24**

**Assumed Specific Gravity= 2.7**

**Remarks:** Failure Type : Bulge and Multi

Shear

Failure limit to 15%

**Client:** CPRA

**Project:** BRETON LANDBRIDGE MARSH CREATION

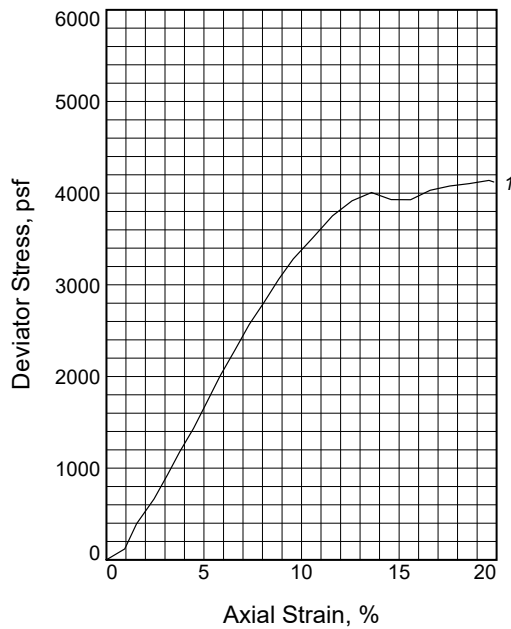
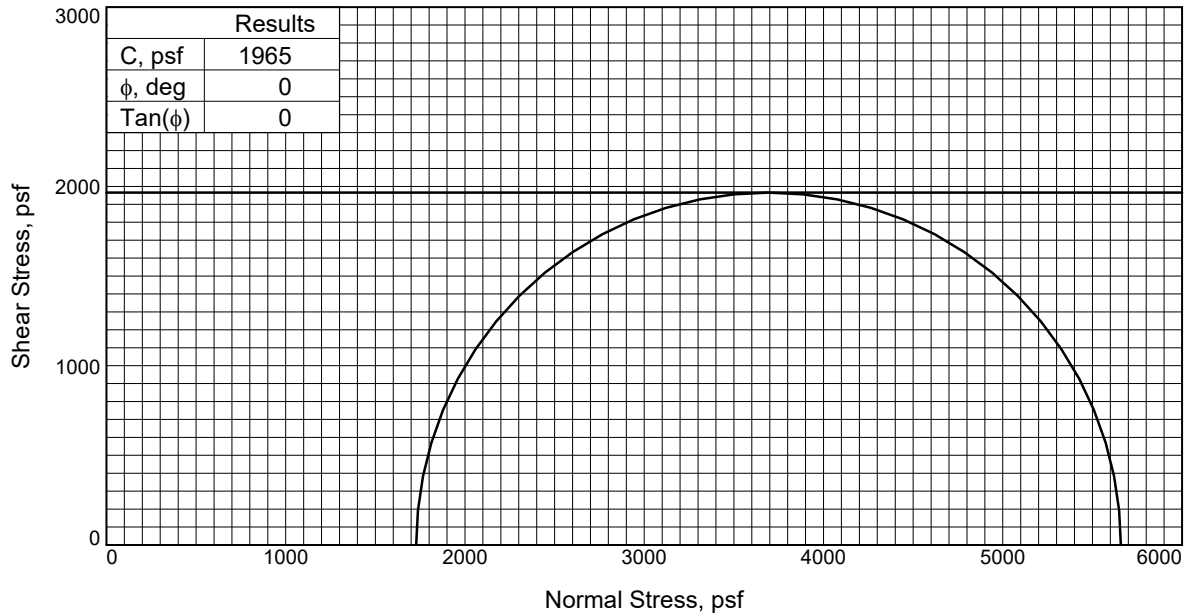
**Source of Sample:** B-3      **Depth:** 23-25

**Sample Number:** 11

**Proj. No.:** APS2008-G063

**Date Sampled:** 8-15-2020





Sample No.	1	
Initial	Water Content, %	24.1
	Dry Density, pcf	104.0
	Saturation, %	104.8
	Void Ratio	0.6203
	Diameter, in.	2.75
	Height, in.	5.72
At Test	Water Content, %	24.1
	Dry Density, pcf	104.0
	Saturation, %	104.8
	Void Ratio	0.6203
	Diameter, in.	2.75
	Height, in.	5.72
Strain at peak, %	14.6	
Back Pressure, psi	0.00	
Cell Pressure, psi	12.00	
Fail. Stress, psf	3930	
Ult. Stress, psf	3930	
$\sigma_1$ Failure, psf	5658	
$\sigma_3$ Failure, psf	1728	

**Type of Test:**

Unconsolidated Undrained

**Sample Type:** Undisturbed

**Description:** Very Stiff Gray Silty Clay (CL-ML) -with fine sand

**LL= 30      PL= 23      PI= 7**

**Assumed Specific Gravity= 2.7**

**Remarks:** Failure Type : Bulge

Failure limit to 15%

**Client:** CPRA

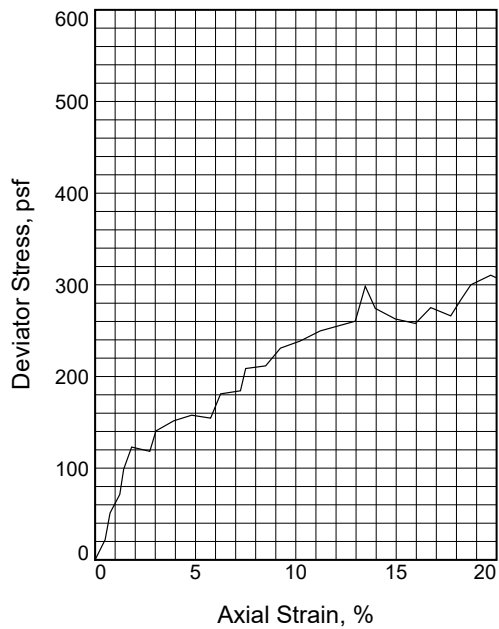
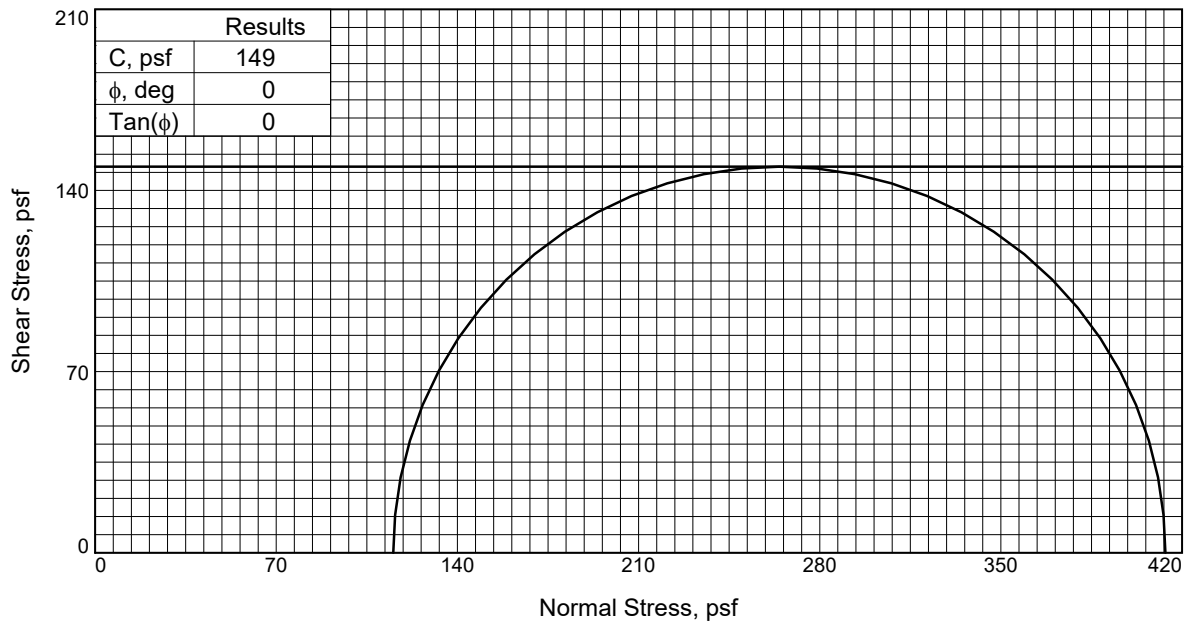
**Project:** BRETON LANDBRIDGE MARSH CREATION

**Source of Sample:** B-3      **Depth:** 28-30

**Sample Number:** 12

**Proj. No.:** APS2008-G063      **Date Sampled:** 8-15-2020





Sample No.	1	
Initial	Water Content, %	691.6
	Dry Density, pcf	8.7
	Saturation, %	102.2
	Void Ratio	18.2801
	Diameter, in.	2.69
	Height, in.	6.00
At Test	Water Content, %	691.6
	Dry Density, pcf	8.7
	Saturation, %	102.2
	Void Ratio	18.2801
	Diameter, in.	2.69
	Height, in.	6.00
Strain at peak, %	13.5	
Back Pressure, psi	0.00	
Cell Pressure, psi	0.80	
Fail. Stress, psf	298	
Ult. Stress, psf	298	
$\sigma_1$ Failure, psf	414	
$\sigma_3$ Failure, psf	115	

**Type of Test:**

Unconsolidated Undrained

**Sample Type:** Undisturbed

**Description:** Black Peat (PT)

**LL=** 574      **PL=** 189      **PI=** 385

**Assumed Specific Gravity=** 2.7

**Remarks:** Failure Type : Bulge

**Client:** CPRA

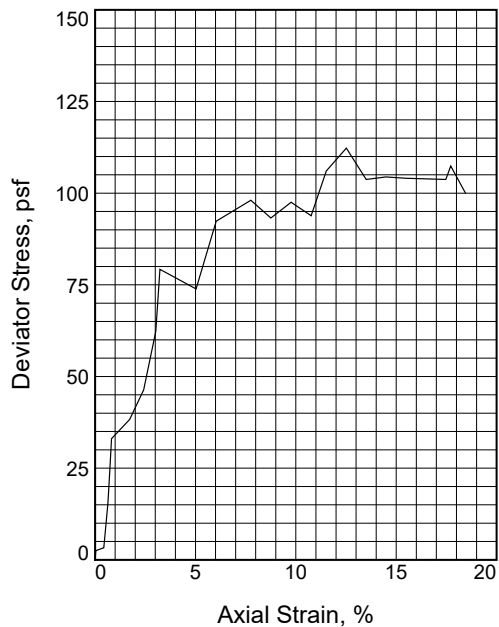
**Project:** BRETON LANDBRIDGE MARSH CREATION

**Source of Sample:** B-4      **Depth:** 0-2

**Sample Number:** 1

**Proj. No.:** APS2008-G063      **Date Sampled:** 8-12-2020





Sample No.	1	
Initial	Water Content, %	617.7
	Dry Density, pcf	9.4
	Saturation, %	98.3
	Void Ratio	16.9605
	Diameter, in.	2.74
At Test	Height, in.	5.79
	Water Content, %	617.7
	Dry Density, pcf	9.4
	Saturation, %	98.3
	Void Ratio	16.9605
Diameter, in.	2.74	
Height, in.	5.79	
Strain at peak, %	12.5	
Back Pressure, psi	0.00	
Cell Pressure, psi	1.60	
Fail. Stress, psf	112	
Ult. Stress, psf	112	
$\sigma_1$ Failure, psf	343	
$\sigma_3$ Failure, psf	230	

**Type of Test:**

Unconsolidated Undrained

**Sample Type:** Undisturbed

**Description:** Black Peat (PT)

LL= 483      PL= 129      PI= 354

**Assumed Specific Gravity=** 2.7

**Remarks:** Failure Type : Bulge

**Client:** CPRA

**Project:** BRETON LANDBRIDGE MARSH CREATION

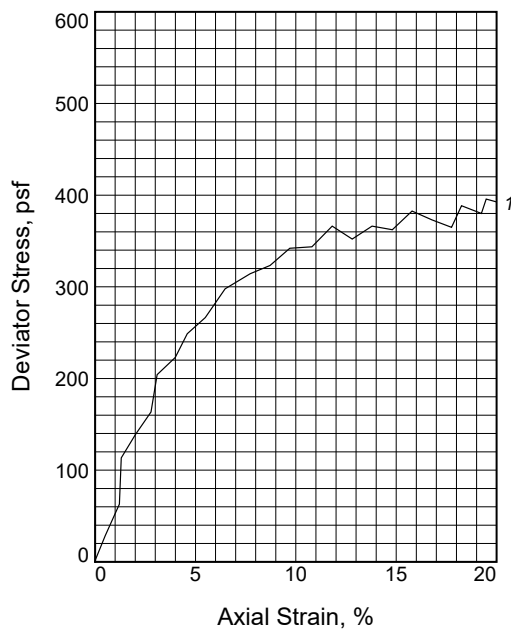
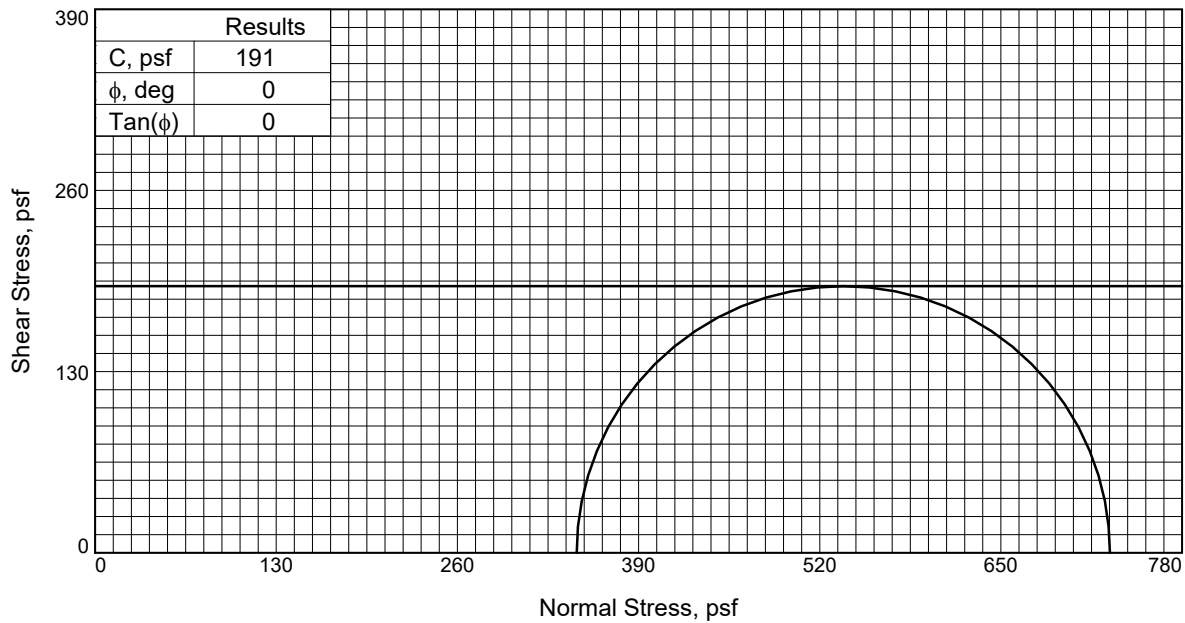
**Source of Sample:** B-4      **Depth:** 2-4

**Sample Number:** 2

**Proj. No.:** APS2008-G063

**Date Sampled:** 8-12-2020





Sample No.	1	
Initial	Water Content, %	50.1
	Dry Density, pcf	68.8
	Saturation, %	93.3
	Void Ratio	1.4511
	Diameter, in.	2.90
	Height, in.	5.74
At Test	Water Content, %	50.1
	Dry Density, pcf	68.8
	Saturation, %	93.3
	Void Ratio	1.4511
	Diameter, in.	2.90
	Height, in.	5.74
Strain at peak, %	15.8	
Back Pressure, psi	0.00	
Cell Pressure, psi	2.40	
Fail. Stress, psf	383	
Ult. Stress, psf	383	
$\sigma_1$ Failure, psf	728	
$\sigma_3$ Failure, psf	346	

**Type of Test:**

Unconsolidated Undrained

**Sample Type:** Undisturbed

**Description:** Very Soft Gray Lean Clay (CL) -  
with fine sand

**LL= 49      PL= 20      PI= 29**

**Assumed Specific Gravity= 2.7**

**Remarks:** Failure Type : Bulge

Failure limit to 15%

**Client:** CPRA

**Project:** BRETON LANDBRIDGE MARSH CREATION

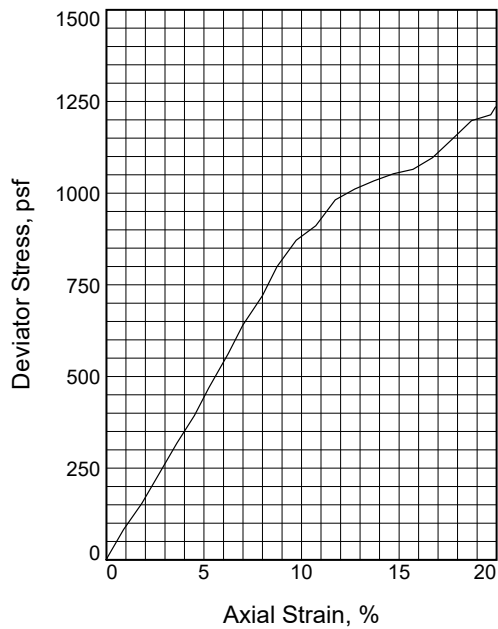
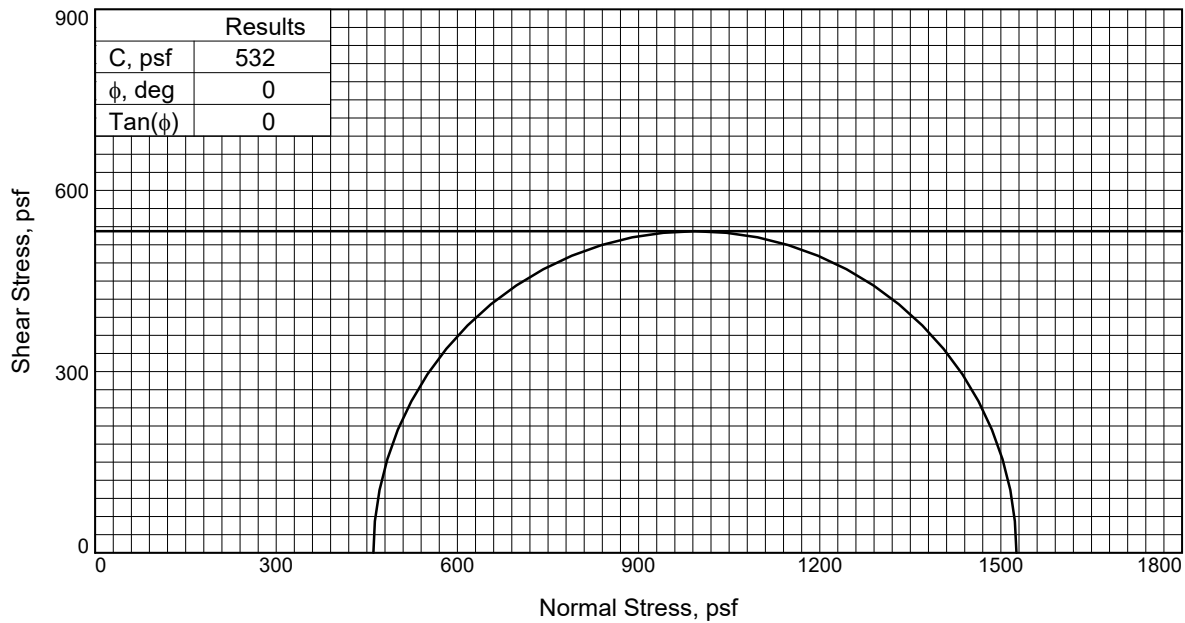
**Source of Sample:** B-4      **Depth:** 4-6

**Sample Number:** 3

**Proj. No.:** APS2008-G063

**Date Sampled:** 8-12-2020





Sample No.	1	
Initial	Water Content, %	37.7
	Dry Density, pcf	81.6
	Saturation, %	95.5
	Void Ratio	1.0660
	Diameter, in.	2.89
	Height, in.	5.78
At Test	Water Content, %	37.7
	Dry Density, pcf	81.6
	Saturation, %	95.5
	Void Ratio	1.0660
	Diameter, in.	2.89
	Height, in.	5.78
Strain at peak, %	15.7	
Back Pressure, psi	0.00	
Cell Pressure, psi	3.20	
Fail. Stress, psf	1065	
Ult. Stress, psf	1065	
$\sigma_1$ Failure, psf	1526	
$\sigma_3$ Failure, psf	461	

**Type of Test:**

Unconsolidated Undrained

**Sample Type:** Undisturbed

**Description:** Medium Stiff Gray Lean Clay (CL) -with fine sand

**LL= 39      PL= 18      PI= 21**

**Assumed Specific Gravity= 2.7**

**Remarks:** Failure Type : Bulge  
Failure limit to 15%

**Client:** CPRA

**Project:** BRETON LANDBRIDGE MARSH CREATION

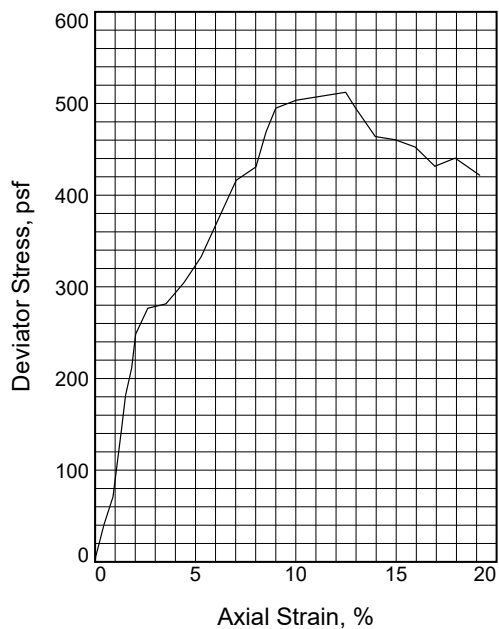
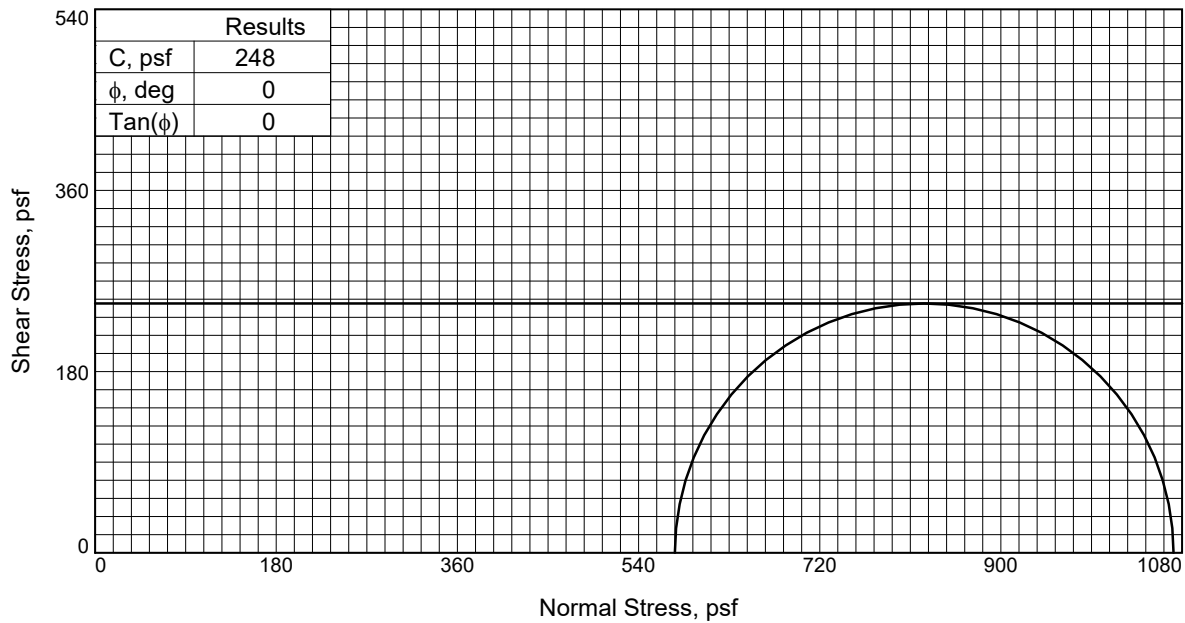
**Source of Sample:** B-4      **Depth:** 6-8

**Sample Number:** 4

**Proj. No.:** APS2008-G063      **Date Sampled:** 8-12-2020







Sample No.	1	
Initial	Water Content, %	50.8
	Dry Density, pcf	73.0
	Saturation, %	104.8
	Void Ratio	1.3096
	Diameter, in.	2.76
	Height, in.	5.77
At Test	Water Content, %	50.8
	Dry Density, pcf	73.0
	Saturation, %	104.8
	Void Ratio	1.3096
	Diameter, in.	2.76
	Height, in.	5.77
Strain at peak, %	13.0	
Back Pressure, psi	0.00	
Cell Pressure, psi	4.00	
Fail. Stress, psf	496	
Ult. Stress, psf	496	
$\sigma_1$ Failure, psf	1072	
$\sigma_3$ Failure, psf	576	

**Type of Test:**

Unconsolidated Undrained

**Sample Type:** Undisturbed

**Description:** Very Soft Gray Fat Clay (CH)

**LL= 36      PL= 18      PI= 18**

**Assumed Specific Gravity= 2.7**

**Remarks:** Failure Type : Bulge

**Client:** CPRA

**Project:** BRETON LANDBRIDGE MARSH CREATION

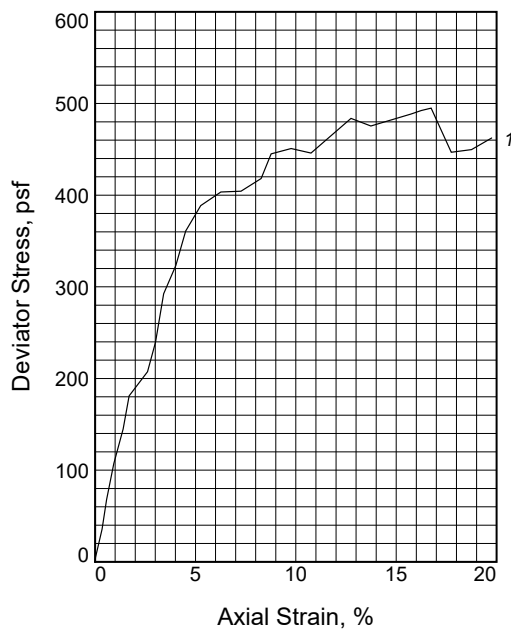
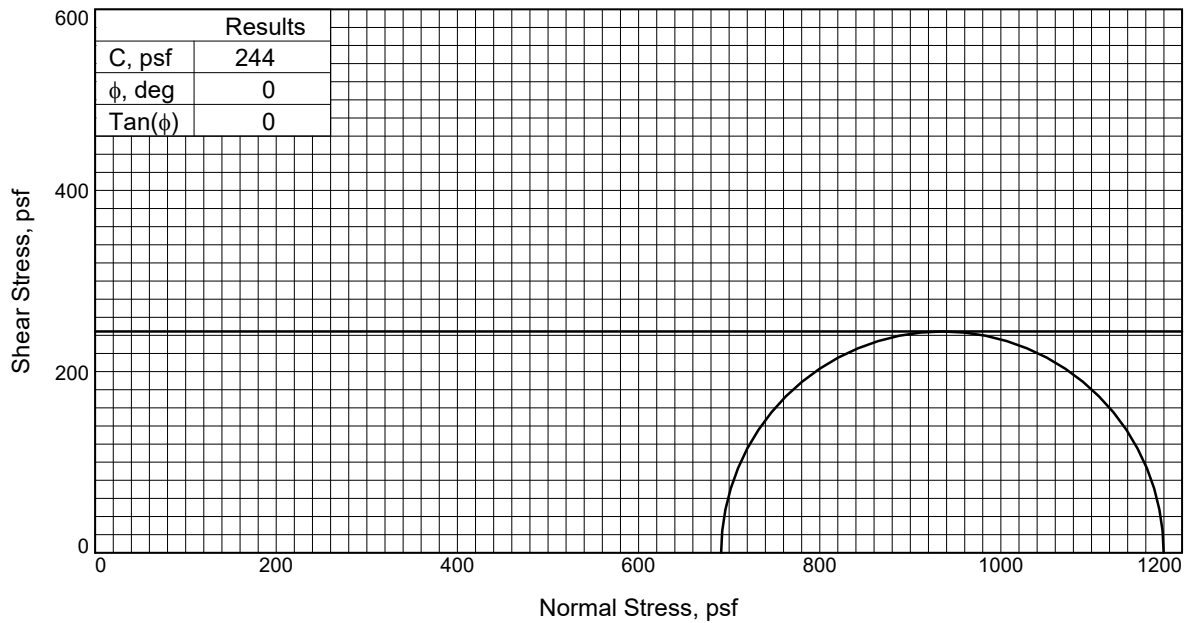
**Source of Sample:** B-4      **Depth:** 8-10

**Sample Number:** 5

**Proj. No.:** APS2008-G063

**Date Sampled:** 8-12-2020





Sample No.	1	
Initial	Water Content, %	47.5
	Dry Density, pcf	68.1
	Saturation, %	86.9
	Void Ratio	1.4769
	Diameter, in.	2.84
	Height, in.	5.85
At Test	Water Content, %	47.5
	Dry Density, pcf	68.1
	Saturation, %	86.9
	Void Ratio	1.4769
	Diameter, in.	2.84
	Height, in.	5.85
Strain at peak, %	15.7	
Back Pressure, psi	0.00	
Cell Pressure, psi	4.80	
Fail. Stress, psf	489	
Ult. Stress, psf	489	
$\sigma_1$ Failure, psf	1180	
$\sigma_3$ Failure, psf	691	

**Type of Test:**

Unconsolidated Undrained

**Sample Type:** Undisturbed

**Description:** Very Soft Gray Fat Clay (CH)

**LL= 52      PL= 21      PI= 31**

**Assumed Specific Gravity= 2.7**

**Remarks:** Failure Type : Bulge

Failure limit to 15%

**Client:** CPRA

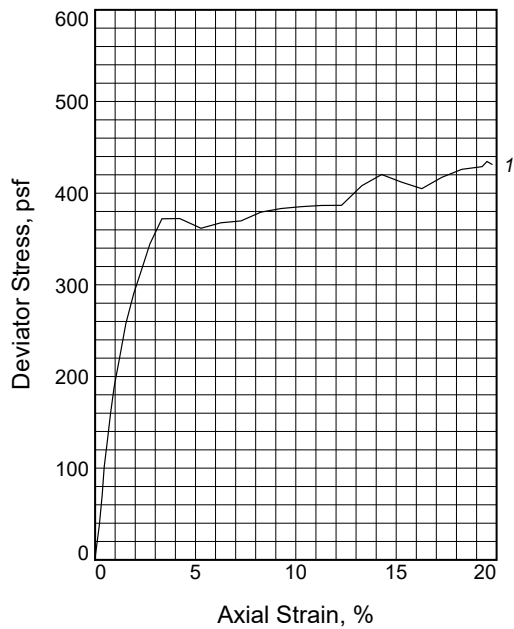
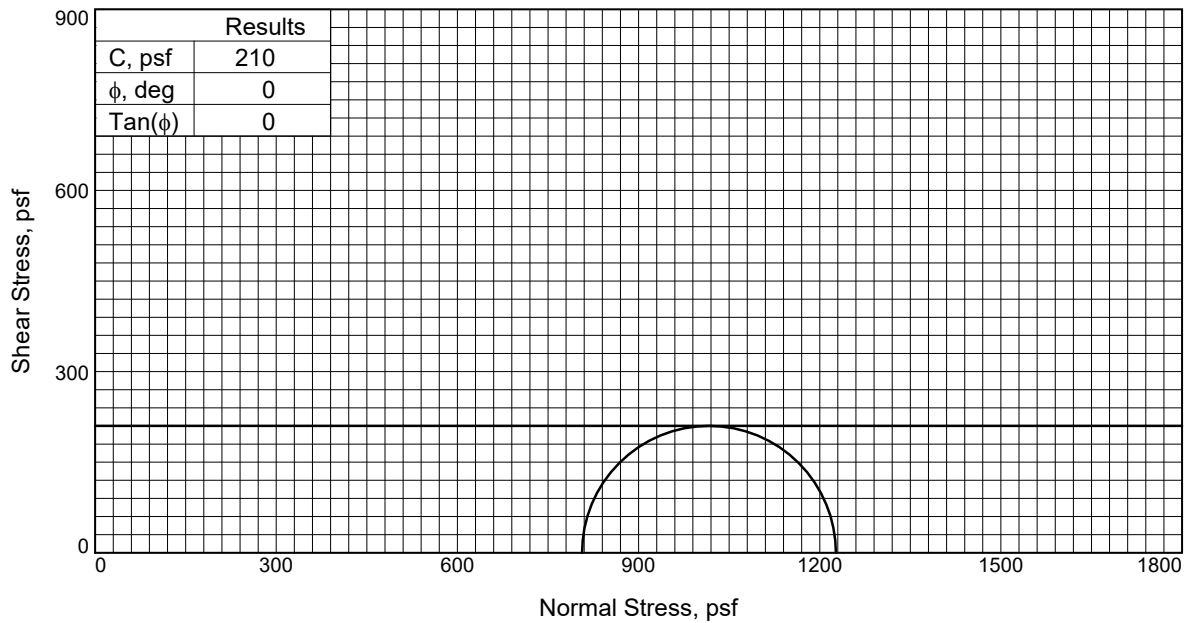
**Project:** BRETON LANDBRIDGE MARSH CREATION

**Source of Sample:** B-4      **Depth:** 10-12

**Sample Number:** 6

**Proj. No.:** APS2008-G063      **Date Sampled:** 8-12-2020





Sample No.	1	
Initial	Water Content, %	103.8
	Dry Density, pcf	45.9
	Saturation, %	105.0
	Void Ratio	2.6696
	Diameter, in.	2.84
At Test	Height, in.	5.78
	Water Content, %	103.8
	Dry Density, pcf	45.9
	Saturation, %	105.0
	Void Ratio	2.6696
Diameter, in.	2.84	
Height, in.	5.78	
Strain at peak, %	14.3	
Back Pressure, psi	0.00	
Cell Pressure, psi	5.60	
Fail. Stress, psf	420	
Ult. Stress, psf	420	
$\sigma_1$ Failure, psf	1227	
$\sigma_3$ Failure, psf	806	

**Type of Test:**

Unconsolidated Undrained

**Sample Type:** Undisturbed

**Description:** Very Soft Gray Fat Clay (CH)

LL= 96      PL= 22      PI= 74

**Assumed Specific Gravity=** 2.7

**Remarks:** Failure Type : Bulge

Failure limit to 15%

**Client:** CPRA

**Project:** BRETON LANDBRIDGE MARSH CREATION

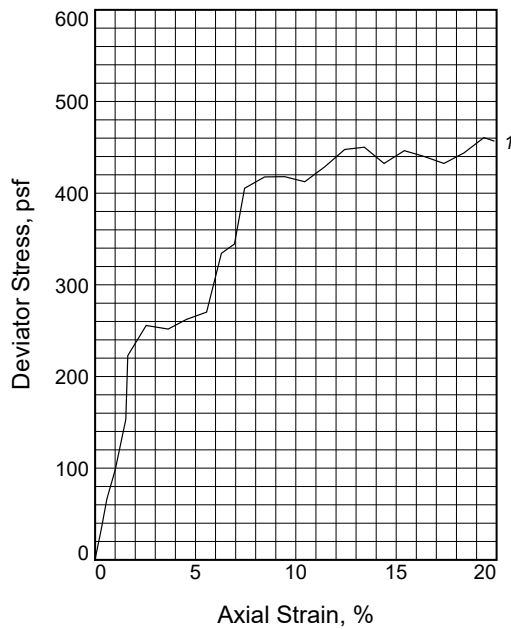
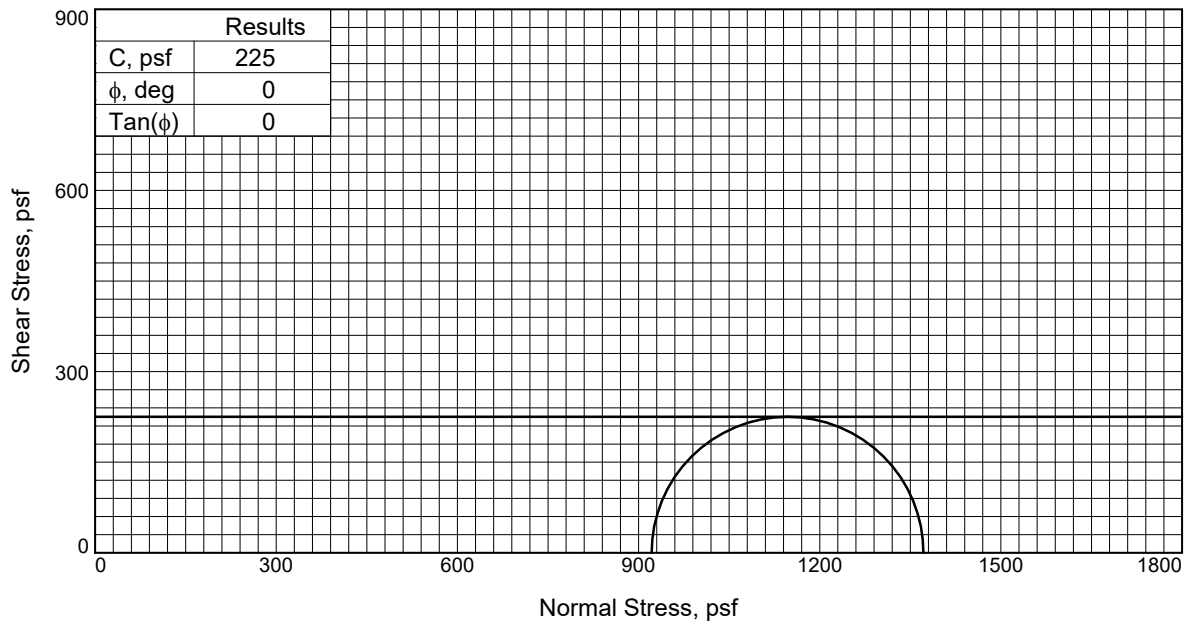
**Source of Sample:** B-4      **Depth:** 12-14

**Sample Number:** 7

**Proj. No.:** APS2008-G063

**Date Sampled:** 8-12-2020





Sample No.	1	
Initial	Water Content, %	125.4
	Dry Density, pcf	39.8
	Saturation, %	104.7
	Void Ratio	3.2326
	Diameter, in.	2.79
	Height, in.	5.82
At Test	Water Content, %	125.4
	Dry Density, pcf	39.8
	Saturation, %	104.7
	Void Ratio	3.2326
	Diameter, in.	2.79
	Height, in.	5.82
Strain at peak, %	13.4	
Back Pressure, psi	0.00	
Cell Pressure, psi	6.40	
Fail. Stress, psf	450	
Ult. Stress, psf	450	
$\sigma_1$ Failure, psf	1372	
$\sigma_3$ Failure, psf	922	

**Type of Test:**

Unconsolidated Undrained

**Sample Type:** Undisturbed

**Description:** Very Soft Gray Fat Clay (CH)

LL= 149      PL= 38      PI= 111

**Assumed Specific Gravity=** 2.7

**Remarks:** Failure Type : Bulge

**Client:** CPRA

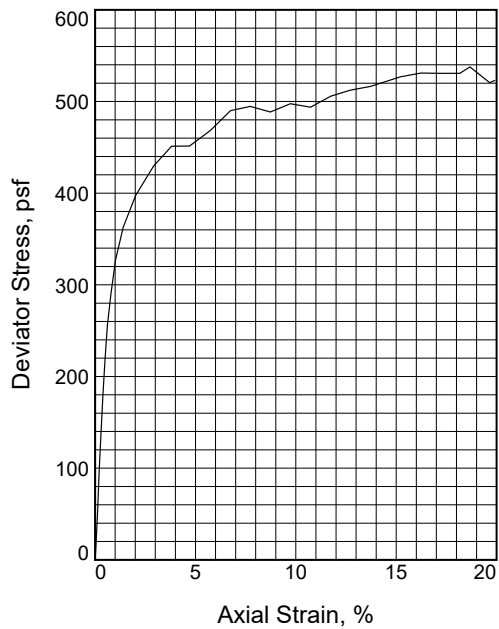
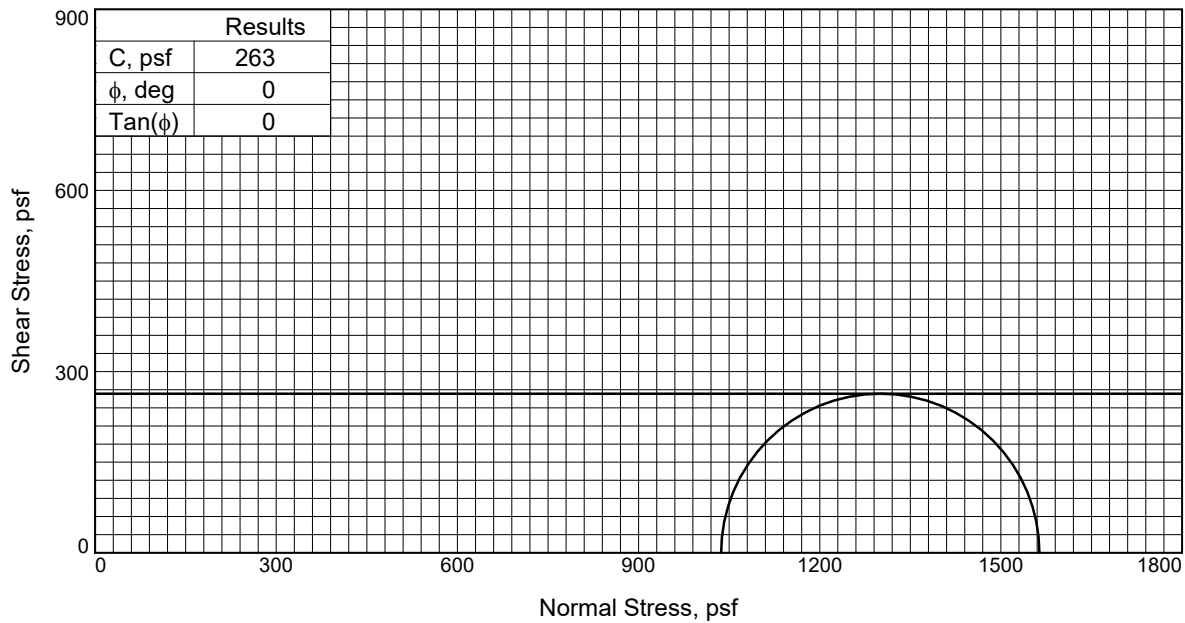
**Project:** BRETON LANDBRIDGE MARSH CREATION

**Source of Sample:** B-4      **Depth:** 14-16

**Sample Number:** 8

**Proj. No.:** APS2008-G063      **Date Sampled:** 8-12-2020





Sample No.	1	
Initial	Water Content, %	77.1
	Dry Density, pcf	54.3
	Saturation, %	98.8
	Void Ratio	2.1061
	Diameter, in.	2.83
At Test	Height, in.	5.78
	Water Content, %	77.1
	Dry Density, pcf	54.3
	Saturation, %	98.8
	Void Ratio	2.1061
Diameter, in.	2.83	
Height, in.	5.78	
Strain at peak, %	15.2	
Back Pressure, psi	0.00	
Cell Pressure, psi	7.20	
Fail. Stress, psf	527	
Ult. Stress, psf	527	
$\sigma_1$ Failure, psf	1564	
$\sigma_3$ Failure, psf	1037	

**Type of Test:**

Unconsolidated Undrained

**Sample Type:** Undisturbed

**Description:** Soft Gray Fat Clay (CH)

**LL=** 89      **PL=** 28      **PI=** 61

**Assumed Specific Gravity=** 2.7

**Remarks:** Failure Type : Bulge

Failure limit to 15%

**Client:** CPRA

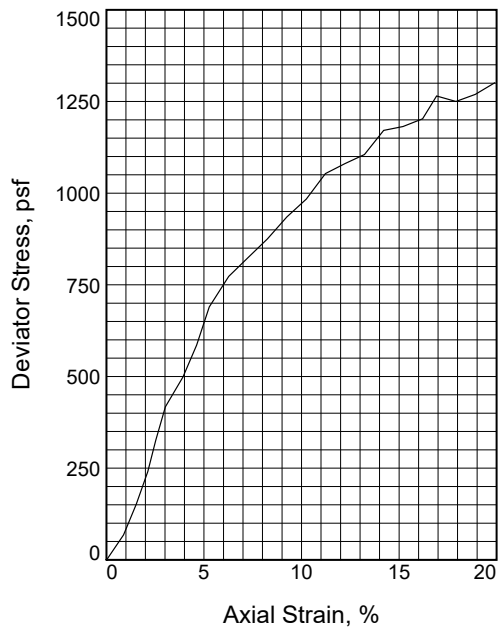
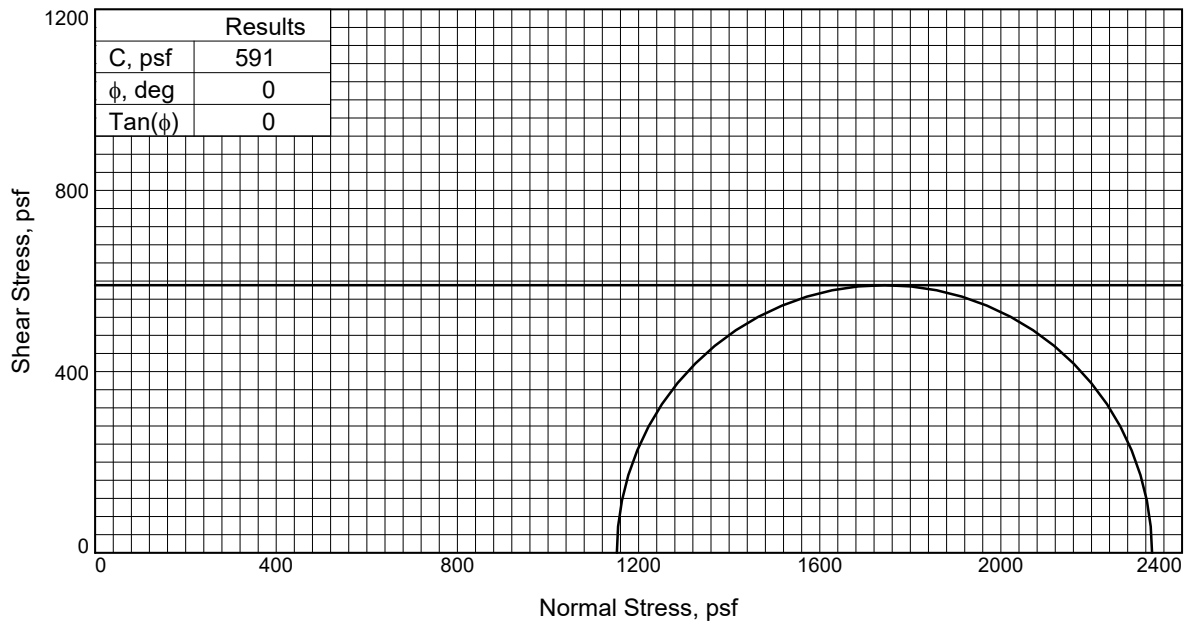
**Project:** BRETON LANDBRIDGE MARSH CREATION

**Source of Sample:** B-4      **Depth:** 16-18

**Sample Number:** 9

**Proj. No.:** APS2008-G063      **Date Sampled:** 8-12-2020





Sample No.	1	
Initial	Water Content, %	30.1
	Dry Density, pcf	89.7
	Saturation, %	92.5
	Void Ratio	0.8789
	Diameter, in.	2.91
	Height, in.	6.03
At Test	Water Content, %	30.1
	Dry Density, pcf	89.7
	Saturation, %	92.5
	Void Ratio	0.8789
	Diameter, in.	2.91
	Height, in.	6.03
Strain at peak, %	15.2	
Back Pressure, psi	0.00	
Cell Pressure, psi	8.00	
Fail. Stress, psf	1182	
Ult. Stress, psf	1182	
$\sigma_1$ Failure, psf	2334	
$\sigma_3$ Failure, psf	1152	

**Type of Test:**

Unconsolidated Undrained

**Sample Type:** Undisturbed

**Description:** Medium Stiff Gray Lean Clay (CL) -with fine sand

**LL= 38      PL= 19      PI= 19**

**Assumed Specific Gravity= 2.7**

**Remarks:** Failure Type : Bulge  
Failure limit to 15%

**Client:** CPRA

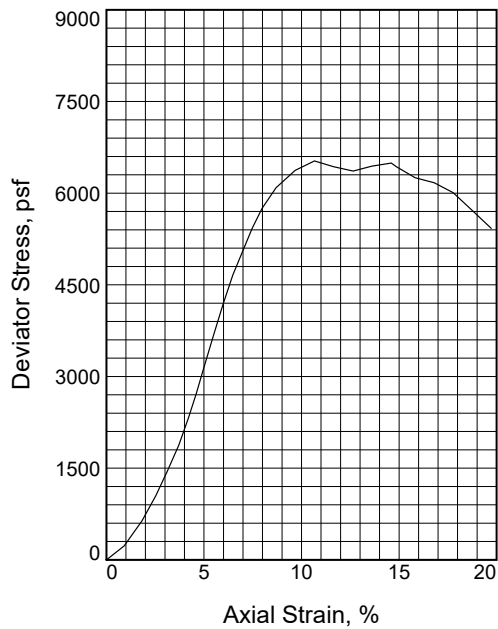
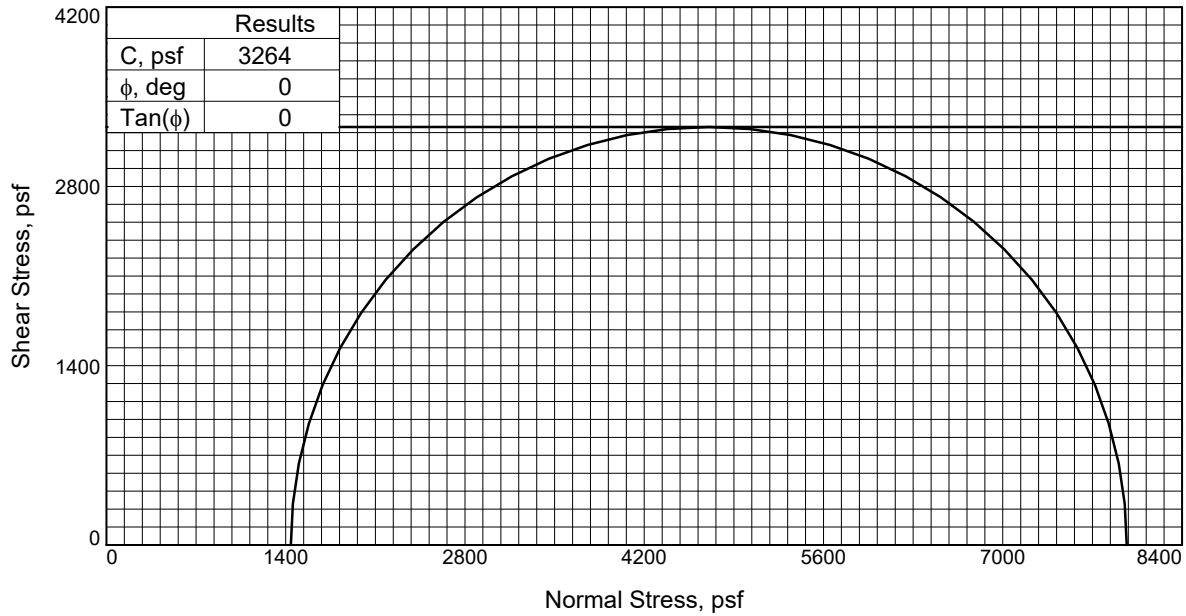
**Project:** BRETON LANDBRIDGE MARSH CREATION

**Source of Sample:** B-4      **Depth:** 18-20

**Sample Number:** 10

**Proj. No.:** APS2008-G063      **Date Sampled:** 8-12-2020





Sample No.	1	
Initial	Water Content, %	26.1
	Dry Density, pcf	96.7
	Saturation, %	94.6
	Void Ratio	0.7432
	Diameter, in.	2.83
At Test	Height, in.	5.80
	Water Content, %	26.1
	Dry Density, pcf	96.7
	Saturation, %	94.6
	Void Ratio	0.7432
	Diameter, in.	2.83
	Height, in.	5.80
	Strain at peak, %	10.7
	Back Pressure, psi	0.00
	Cell Pressure, psi	10.00
	Fail. Stress, psf	6528
	Ult. Stress, psf	6528
	$\sigma_1$ Failure, psf	7968
	$\sigma_3$ Failure, psf	1440

**Type of Test:**

Unconsolidated Undrained

**Sample Type:** Undisturbed

**Description:** Sandy silt (ML)

**LL=** NP

**PI=** NP

**Assumed Specific Gravity=** 2.7

**Remarks:** Failure Type : Bulge

**Client:** CPRA

**Project:** BRETON LANDBRIDGE MARSH CREATION

**Source of Sample:** B-4

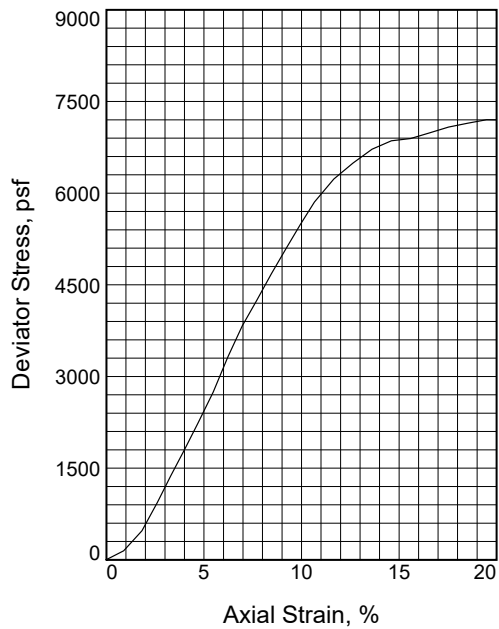
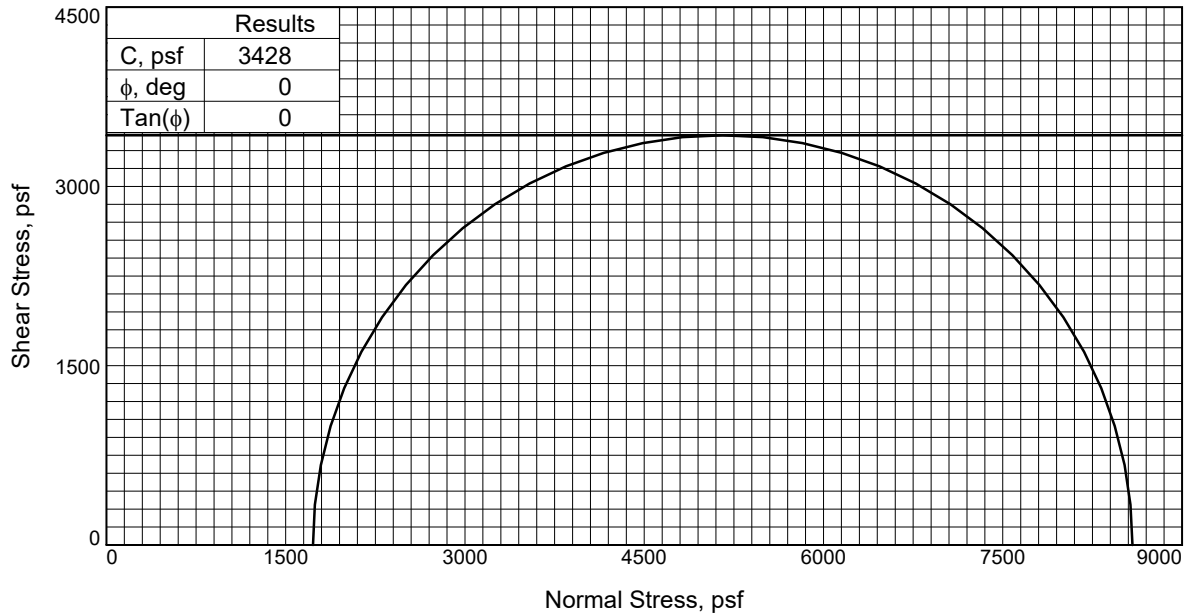
**Depth:** 23-25

**Sample Number:** 11

**Proj. No.:** APS2008-G063

**Date Sampled:** 8-12-2020





Sample No.	1	
Initial	Water Content, %	28.7
	Dry Density, pcf	94.8
	Saturation, %	99.7
	Void Ratio	0.7778
	Diameter, in.	2.77
	Height, in.	5.87
At Test	Water Content, %	28.7
	Dry Density, pcf	94.8
	Saturation, %	99.7
	Void Ratio	0.7778
	Diameter, in.	2.77
	Height, in.	5.87
Strain at peak, %	14.6	
Back Pressure, psi	0.00	
Cell Pressure, psi	12.00	
Fail. Stress, psf	6857	
Ult. Stress, psf	6857	
$\sigma_1$ Failure, psf	8585	
$\sigma_3$ Failure, psf	1728	

**Type of Test:**

Unconsolidated Undrained

**Sample Type:** Undisturbed

**Description:** Sandy silt (ML)

**LL=** NP

**PI=** NP

**Assumed Specific Gravity=** 2.7

**Remarks:** Failure Type : Bulge

Failure limit to 15%

**Client:** CPRA

**Project:** BRETON LANDBRIDGE MARSH CREATION

**Source of Sample:** B-4

**Depth:** 28-30

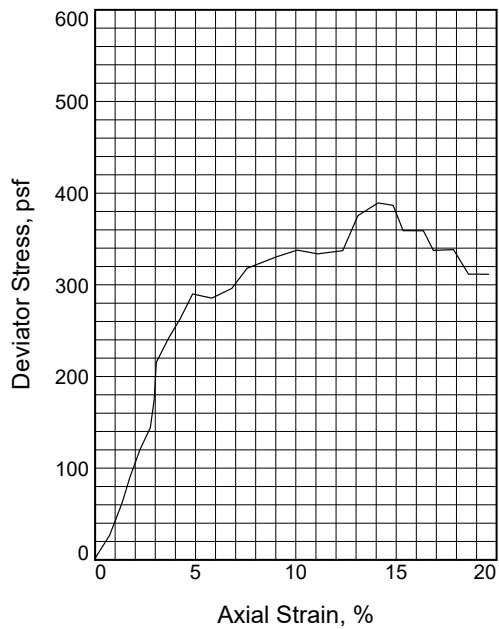
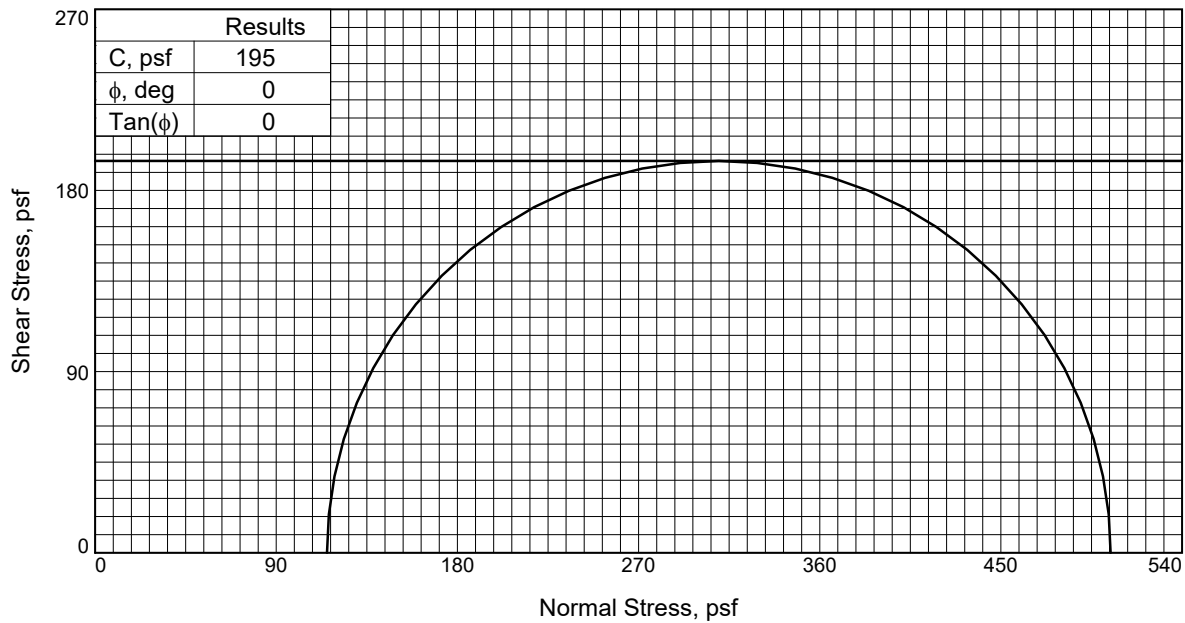
**Sample Number:** 12

**Proj. No.:** APS2008-G063

**Date Sampled:** 8-12-2020







Sample No.	1	
Initial	Water Content, %	44.3
	Dry Density, pcf	71.4
	Saturation, %	94.0
	Void Ratio	1.1677
	Diameter, in.	2.70
At Test	Height, in.	5.81
	Water Content, %	44.3
	Dry Density, pcf	71.4
	Saturation, %	94.0
	Void Ratio	1.1677
	Diameter, in.	2.70
	Height, in.	5.81
Strain at peak, %	14.1	
Back Pressure, psi	0.00	
Cell Pressure, psi	0.80	
Fail. Stress, psf	389	
Ult. Stress, psf	389	
$\sigma_1$ Failure, psf	504	
$\sigma_3$ Failure, psf	115	

**Type of Test:**

Unconsolidated Undrained

**Sample Type:** Undisturbed

**Description:** Very Soft Gray Lean Clay(CL)-  
with peat and fine sand

**LL= 43      PL= 18      PI= 25**

**Specific Gravity= 2.48**

**Remarks:** Failure Type : Bulge  
Failure limit to 15%

**Client:** CPRA

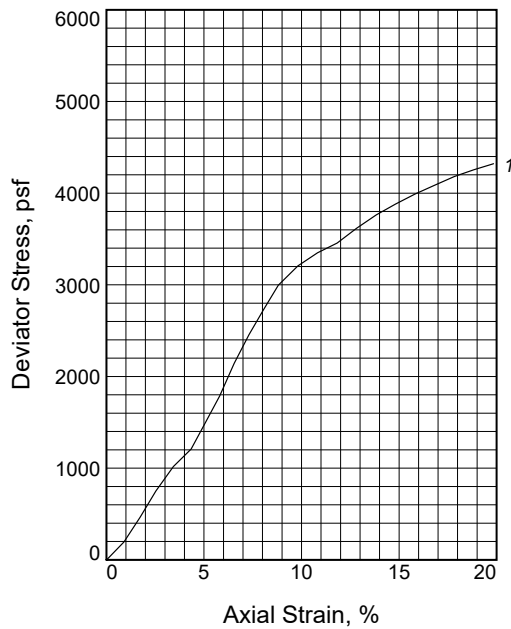
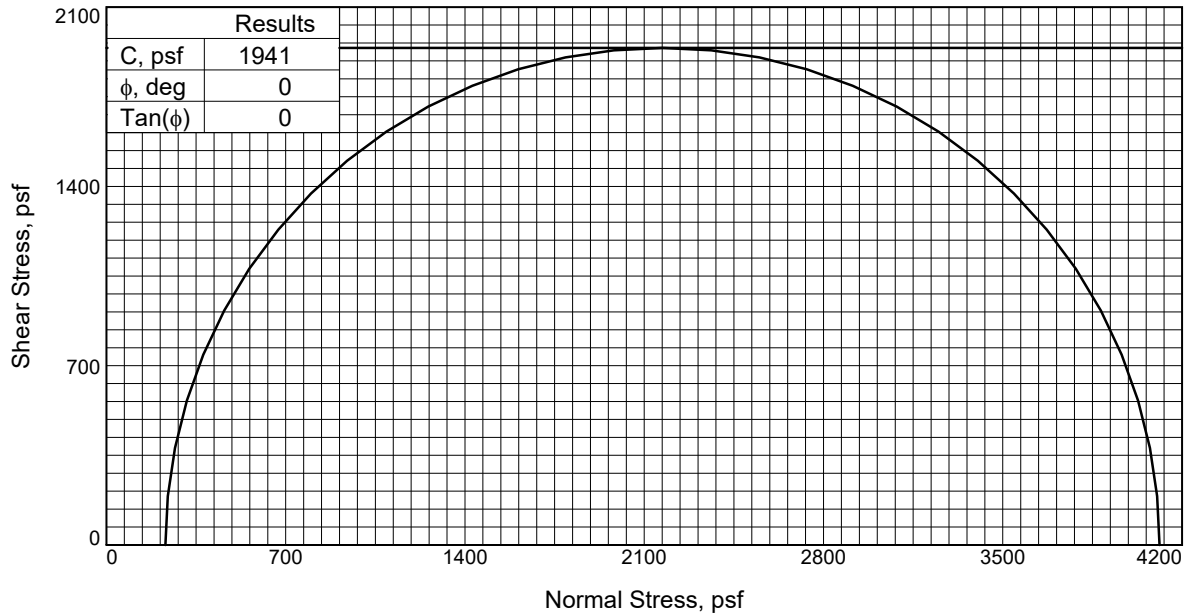
**Project:** BRETON LANDBRIDGE MARSH CREATION

**Source of Sample:** B-5      **Depth:** 0-2

**Sample Number:** 1

**Proj. No.:** APS2008-G063      **Date Sampled:** 8-14-2020





Sample No.		1
Initial	Water Content, %	33.3
	Dry Density, pcf	88.2
	Saturation, %	98.7
	Void Ratio	0.9100
	Diameter, in.	2.81
	Height, in.	5.89
At Test	Water Content, %	33.3
	Dry Density, pcf	88.2
	Saturation, %	98.7
	Void Ratio	0.9100
	Diameter, in.	2.81
	Height, in.	5.89
Strain at peak, %		14.8
Back Pressure, psi		0.00
Cell Pressure, psi		1.60
Fail. Stress, psf		3882
Ult. Stress, psf		3882
$\sigma_1$ Failure, psf		4112
$\sigma_3$ Failure, psf		230

**Type of Test:**

Unconsolidated Undrained

**Sample Type:** Undisturbed

**Description:** Very Stiff Gray Silty Clay (CL-ML)

**LL= 29      PL= 22      PI= 7**

**Assumed Specific Gravity= 2.7**

**Remarks:** Failure Type : Bulge  
Failure limit to 15%

**Client:** CPRA

**Project:** BRETON LANDBRIDGE MARSH CREATION

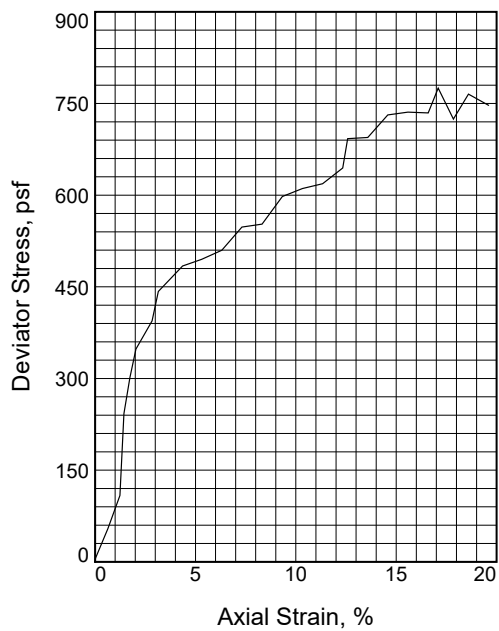
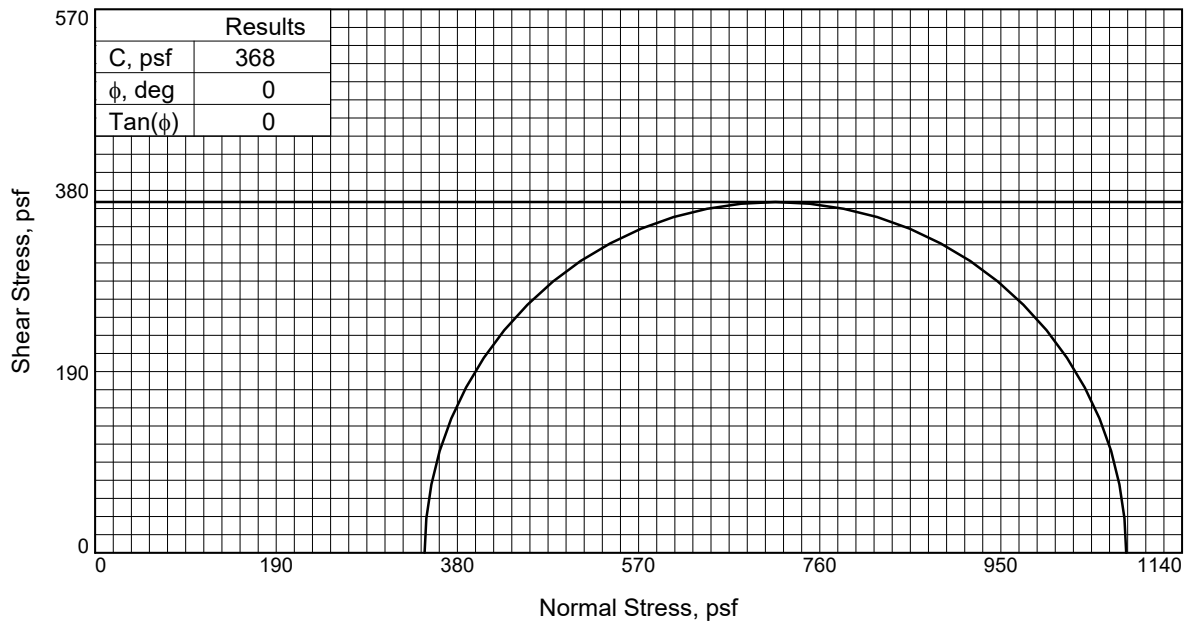
**Source of Sample:** B-5      **Depth:** 2-4

**Sample Number:** 2

**Proj. No.:** APS2008-G063

**Date Sampled:** 8-14-2020





Sample No.	1	
Initial	Water Content, %	51.4
	Dry Density, pcf	72.6
	Saturation, %	105.0
	Void Ratio	1.3226
	Diameter, in.	2.71
	Height, in.	5.76
At Test	Water Content, %	51.4
	Dry Density, pcf	72.6
	Saturation, %	105.0
	Void Ratio	1.3226
	Diameter, in.	2.71
	Height, in.	5.76
Strain at peak, %	15.6	
Back Pressure, psi	0.00	
Cell Pressure, psi	2.40	
Fail. Stress, psf	736	
Ult. Stress, psf	736	
$\sigma_1$ Failure, psf	1081	
$\sigma_3$ Failure, psf	346	

**Type of Test:**

Unconsolidated Undrained

**Sample Type:** Undisturbed

**Description:** Soft Gray Lean Clay(CL) -with fine sand

**LL= 36      PL= 22      PI= 14**

**Assumed Specific Gravity= 2.7**

**Remarks:** Failure Type : Bulge

Failure limit to 15%

**Client:** CPRA

**Project:** BRETON LANDBRIDGE MARSH CREATION

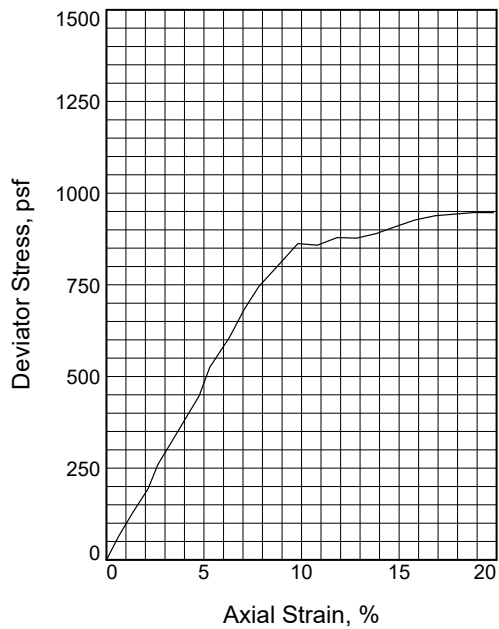
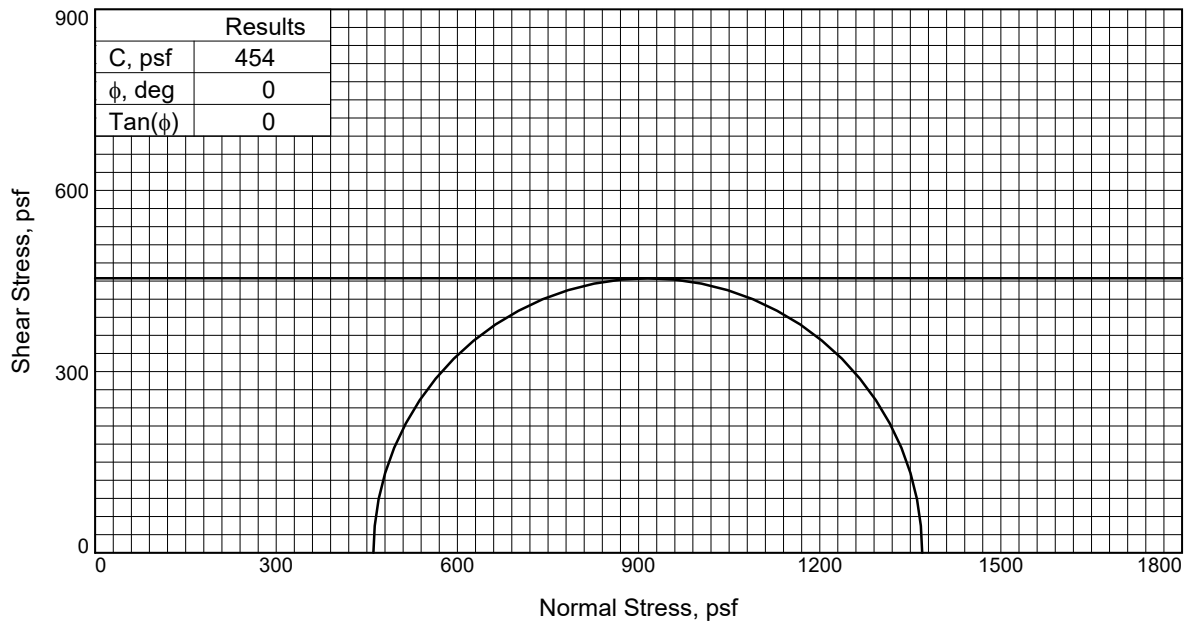
**Source of Sample:** B-5      **Depth:** 4-6

**Sample Number:** 3

**Proj. No.:** APS2008-G063

**Date Sampled:** 8-14-2020





Sample No.	1	
Initial	Water Content, %	42.3
	Dry Density, pcf	80.7
	Saturation, %	104.8
	Void Ratio	1.0894
	Diameter, in.	2.81
At Test	Height, in.	5.81
	Water Content, %	42.3
	Dry Density, pcf	80.7
	Saturation, %	104.8
	Void Ratio	1.0894
Diameter, in.	2.81	
Height, in.	5.81	
Strain at peak, %	14.8	
Back Pressure, psi	0.00	
Cell Pressure, psi	3.20	
Fail. Stress, psf	909	
Ult. Stress, psf	909	
$\sigma_1$ Failure, psf	1370	
$\sigma_3$ Failure, psf	461	

**Type of Test:**

Unconsolidated Undrained

**Sample Type:** Undisturbed

**Description:** Soft Gray Lean Clay(CL)-with fine sand

**LL= 31      PL= 22      PI= 9**

**Assumed Specific Gravity= 2.7**

**Remarks:** Failure Type : Bulge  
Failure limit to 15%

**Client:** CPRA

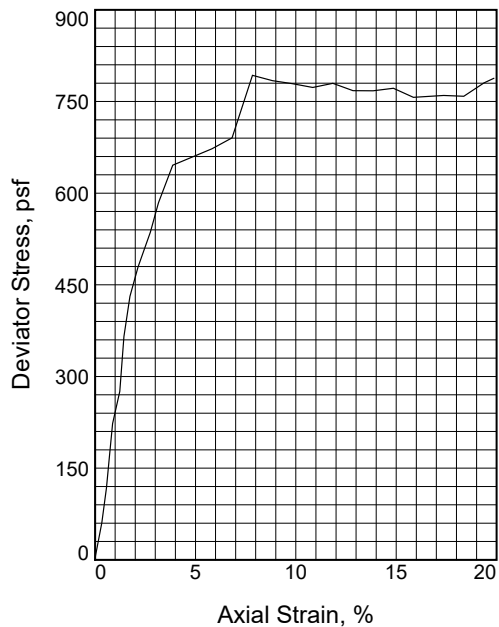
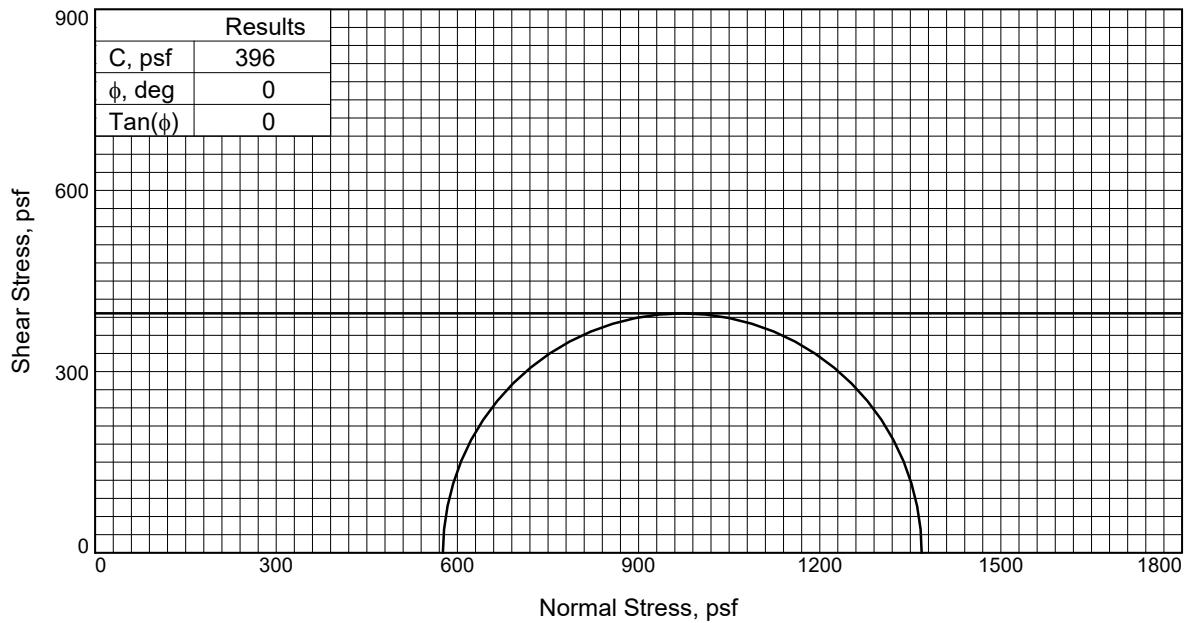
**Project:** BRETON LANDBRIDGE MARSH CREATION

**Source of Sample:** B-5      **Depth:** 6-8

**Sample Number:** 4

**Proj. No.:** APS2008-G063      **Date Sampled:** 8-14-2020





Sample No.	1	
Initial	Water Content, %	47.7
	Dry Density, pcf	73.1
	Saturation, %	98.6
	Void Ratio	1.3045
	Diameter, in.	2.75
	Height, in.	5.80
At Test	Water Content, %	47.7
	Dry Density, pcf	73.1
	Saturation, %	98.6
	Void Ratio	1.3045
	Diameter, in.	2.75
	Height, in.	5.80
Strain at peak, %	7.8	
Back Pressure, psi	0.00	
Cell Pressure, psi	4.00	
Fail. Stress, psf	793	
Ult. Stress, psf	793	
$\sigma_1$ Failure, psf	1369	
$\sigma_3$ Failure, psf	576	

**Type of Test:**

Unconsolidated Undrained

**Sample Type:** Undisturbed

**Description:** Soft Gray Fat CLay(CH)

**LL= 55      PL= 21      PI= 34**

**Assumed Specific Gravity= 2.7**

**Remarks:** Failure Type : Bulge

**Client:** CPRA

**Project:** BRETON LANDBRIDGE MARSH CREATION

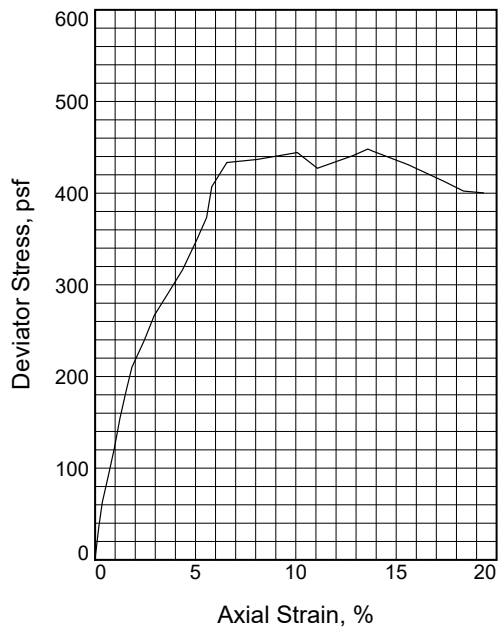
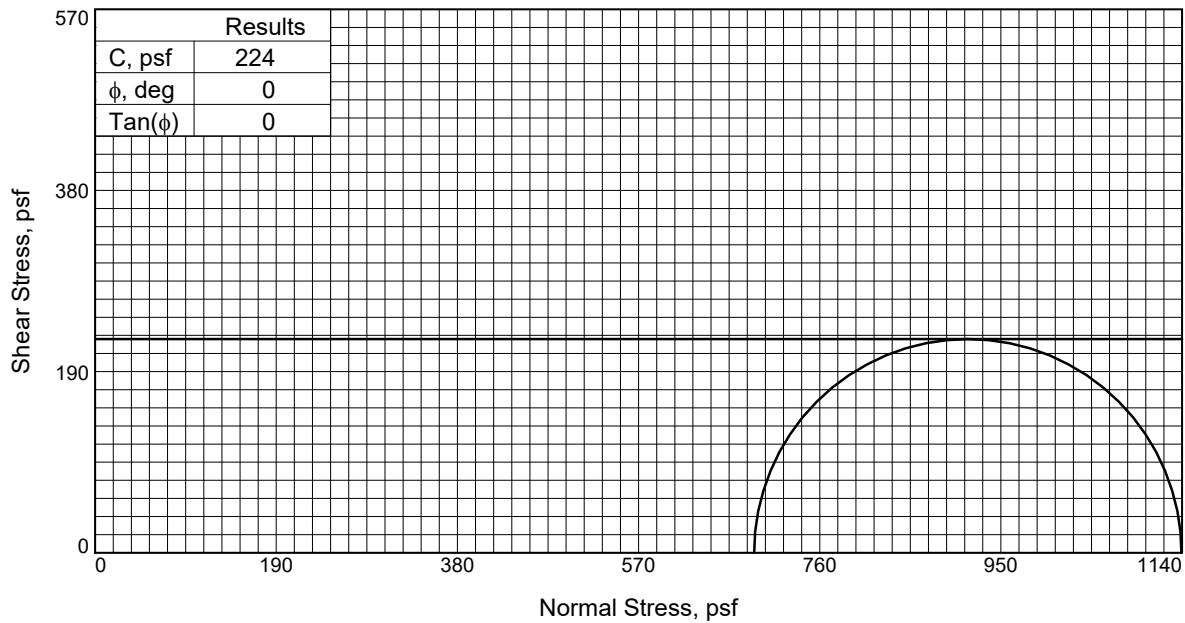
**Source of Sample:** B-5      **Depth:** 8-10

**Sample Number:** 5

**Proj. No.:** APS2008-G063

**Date Sampled:** 8-14-2020





Sample No.	1	
Initial	Water Content, %	29.3
	Dry Density, pcf	78.3
	Saturation, %	68.6
	Void Ratio	1.1525
	Diameter, in.	2.76
	Height, in.	5.76
At Test	Water Content, %	29.3
	Dry Density, pcf	78.3
	Saturation, %	68.6
	Void Ratio	1.1525
	Diameter, in.	2.76
	Height, in.	5.76
Strain at peak, %	13.6	
Back Pressure, psi	0.00	
Cell Pressure, psi	4.80	
Fail. Stress, psf	448	
Ult. Stress, psf	448	
$\sigma_1$ Failure, psf	1139	
$\sigma_3$ Failure, psf	691	

**Type of Test:**

Unconsolidated Undrained

**Sample Type:** Undisturbed

**Description:** Very Soft Gray Fat Clay (CH)

**LL=** 103      **PL=** 24      **PI=** 79

**Assumed Specific Gravity=** 2.7

**Remarks:** Failure Type : Bulge

**Client:** CPRA

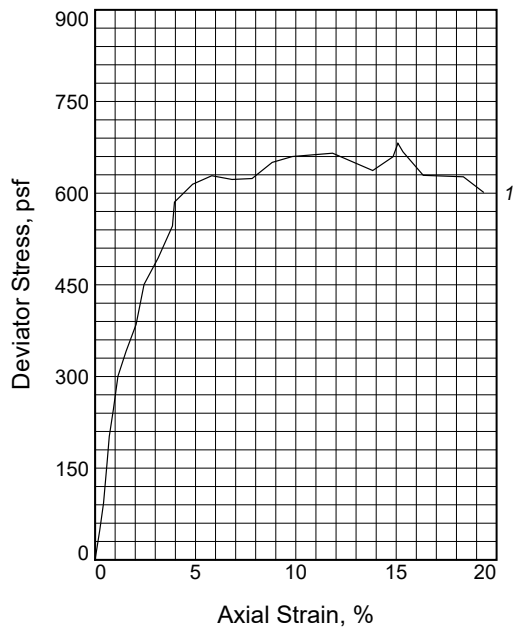
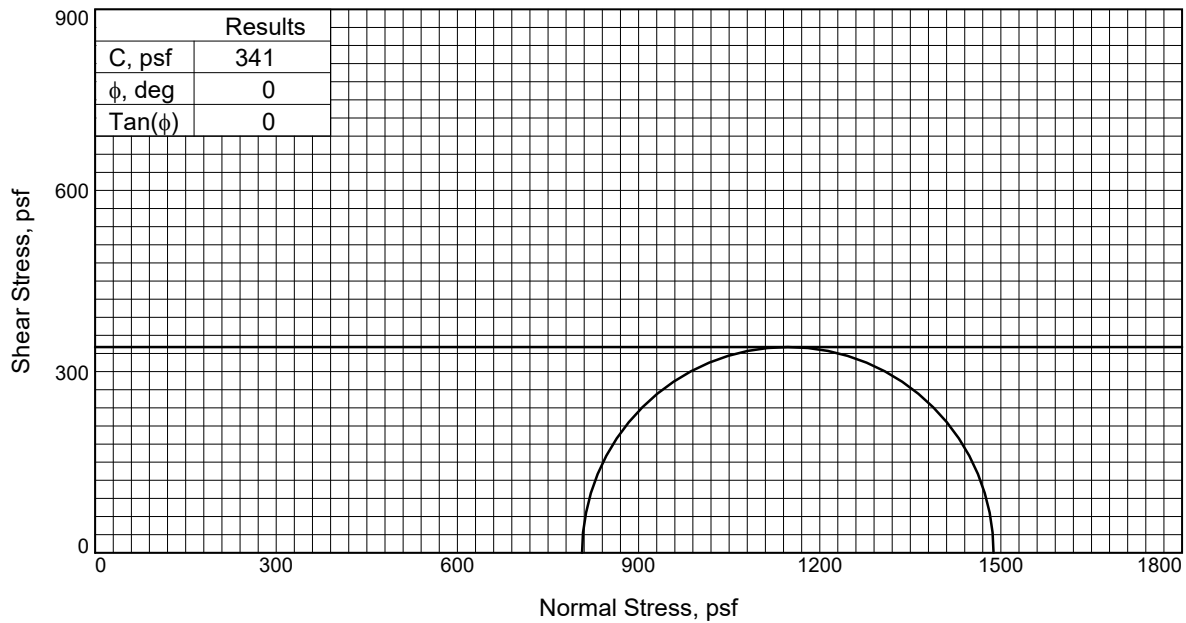
**Project:** BRETON LANDBRIDGE MARSH CREATION

**Source of Sample:** B-5      **Depth:** 10-12

**Sample Number:** 6

**Proj. No.:** APS2008-G063      **Date Sampled:** 8-14-2020





Sample No.	1	
Initial	Water Content, %	78.1
	Dry Density, pcf	52.3
	Saturation, %	94.9
	Void Ratio	2.2218
	Diameter, in.	2.79
At Test	Height, in.	5.78
	Water Content, %	78.1
	Dry Density, pcf	52.3
	Saturation, %	94.9
	Void Ratio	2.2218
Diameter, in.	2.78	
Height, in.	5.78	
Strain at peak, %	15.1	
Back Pressure, psi	0.00	
Cell Pressure, psi	5.60	
Fail. Stress, psf	681	
Ult. Stress, psf	681	
$\sigma_1$ Failure, psf	1488	
$\sigma_3$ Failure, psf	806	

**Type of Test:**

Unconsolidated Undrained

**Sample Type:** Undisturbed

**Description:** Soft Gray Fat Clay(CH)

LL= 95      PL= 28      PI= 67

**Assumed Specific Gravity=** 2.7

**Remarks:** Failure Type : Bulge and Multi

Shear

Failure limit to 15%

**Client:** CPRA

**Project:** BRETON LANDBRIDGE MARSH CREATION

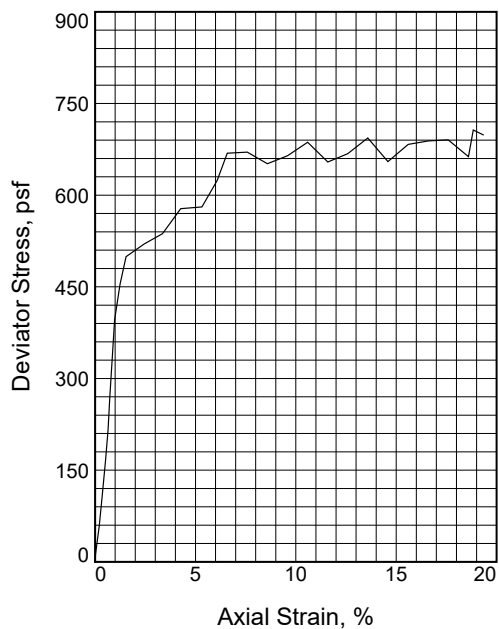
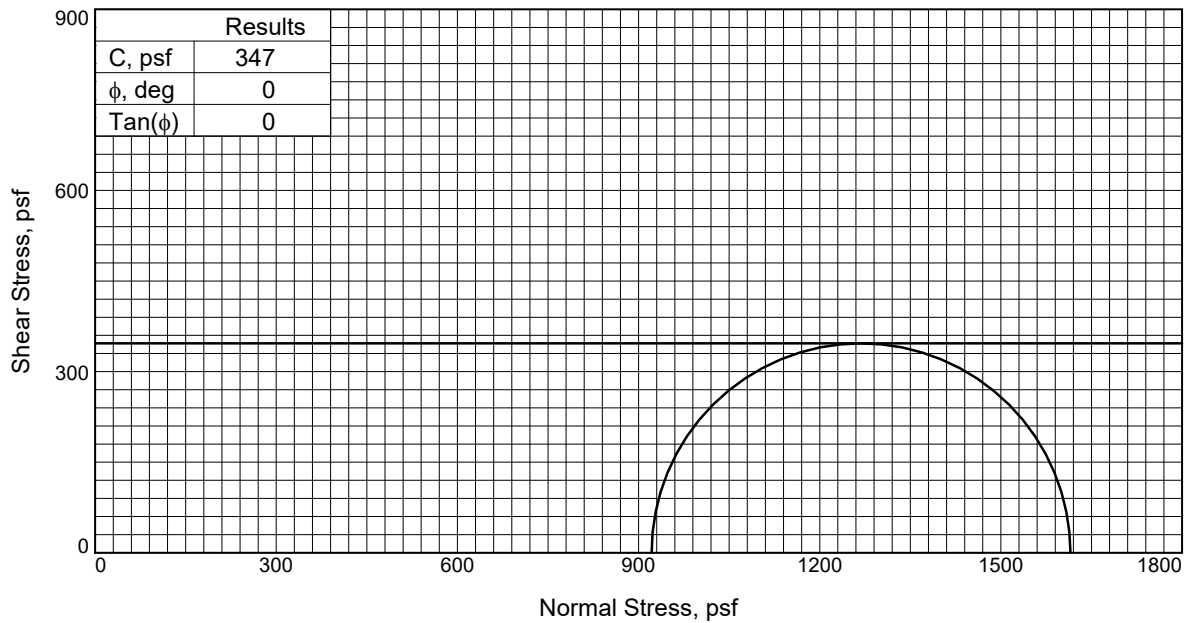
**Source of Sample:** B-5      **Depth:** 12-14

**Sample Number:** 7

**Proj. No.:** APS2008-G063

**Date Sampled:** 8-14-2020





Sample No.	1	
Initial	Water Content, %	92.9
	Dry Density, pcf	49.0
	Saturation, %	104.9
	Void Ratio	2.2753
	Diameter, in.	2.79
	Height, in.	5.80
At Test	Water Content, %	92.9
	Dry Density, pcf	49.0
	Saturation, %	104.9
	Void Ratio	2.2753
	Diameter, in.	2.79
	Height, in.	5.80
Strain at peak, %	13.6	
Back Pressure, psi	0.00	
Cell Pressure, psi	6.40	
Fail. Stress, psf	694	
Ult. Stress, psf	694	
$\sigma_1$ Failure, psf	1615	
$\sigma_3$ Failure, psf	922	

**Type of Test:**

Unconsolidated Undrained

**Sample Type:** Undisturbed

**Description:** Soft gray fat clay (CH)

**LL=** 140      **PL=** 35      **PI=** 105

**Specific Gravity=** 2.57

**Remarks:** Failure Type : Bulge and Multi Shear

**Client:** CPRA

**Project:** BRETON LANDBRIDGE MARSH CREATION

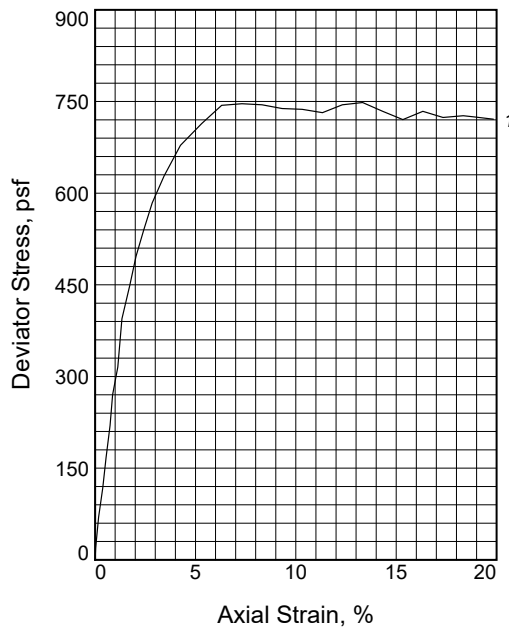
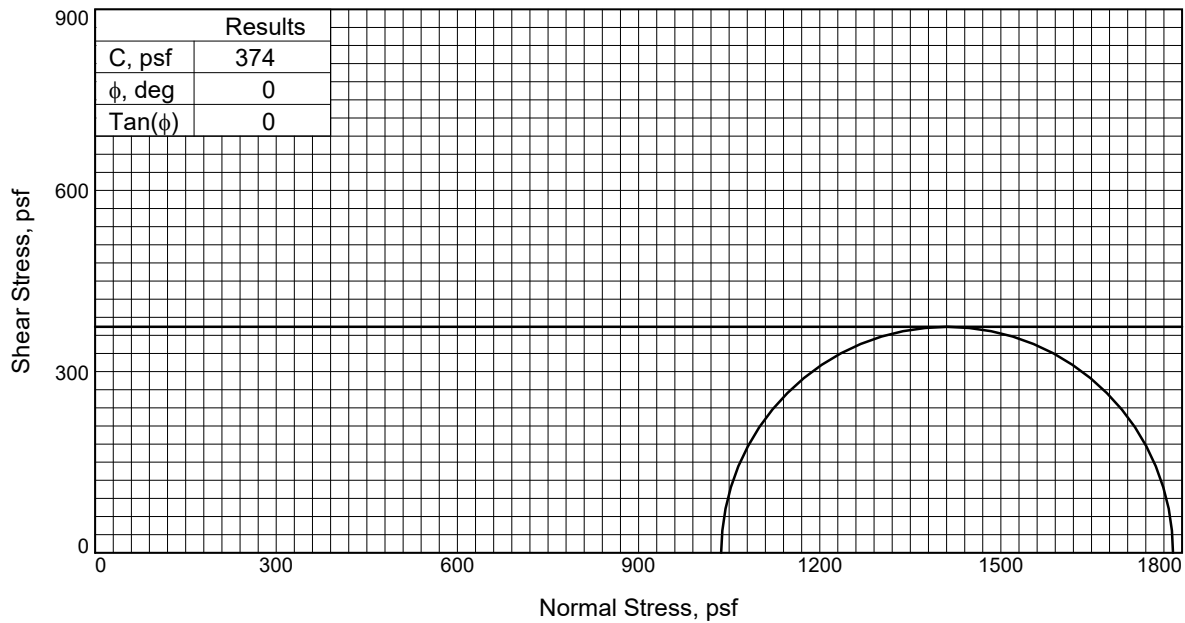
**Source of Sample:** B-5      **Depth:** 14-16

**Sample Number:** 8

**Proj. No.:** APS2008-G063      **Date Sampled:** 8-14-2020







Sample No.	1	
Initial	Water Content, %	58.3
	Dry Density, pcf	67.4
	Saturation, %	104.8
	Void Ratio	1.5024
	Diameter, in.	2.76
	Height, in.	5.83
At Test	Water Content, %	58.3
	Dry Density, pcf	67.4
	Saturation, %	104.8
	Void Ratio	1.5024
	Diameter, in.	2.76
	Height, in.	5.83
Strain at peak, %	13.3	
Back Pressure, psi	0.00	
Cell Pressure, psi	7.20	
Fail. Stress, psf	748	
Ult. Stress, psf	748	
$\sigma_1$ Failure, psf	1785	
$\sigma_3$ Failure, psf	1037	

**Type of Test:**

Unconsolidated Undrained

**Sample Type:** Undisturbed

**Description:** Soft gray fat clay (CH)

**LL= 76      PL= 26      PI= 50**

**Assumed Specific Gravity= 2.7**

**Remarks:** Failure Type : Bulge and Multi Shear

**Client:** CPRA

**Project:** BRETON LANDBRIDGE MARSH CREATION

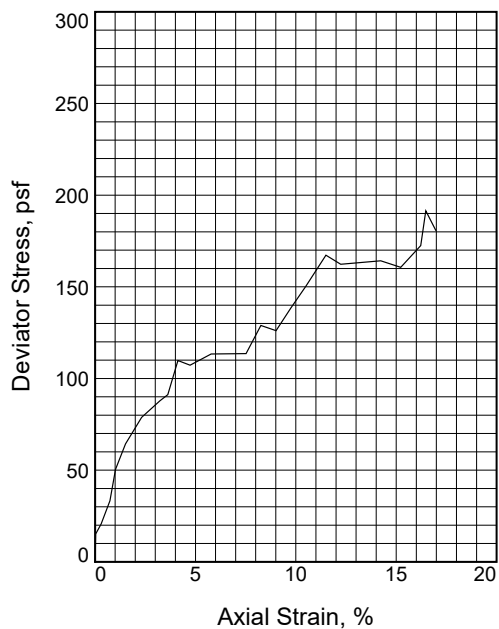
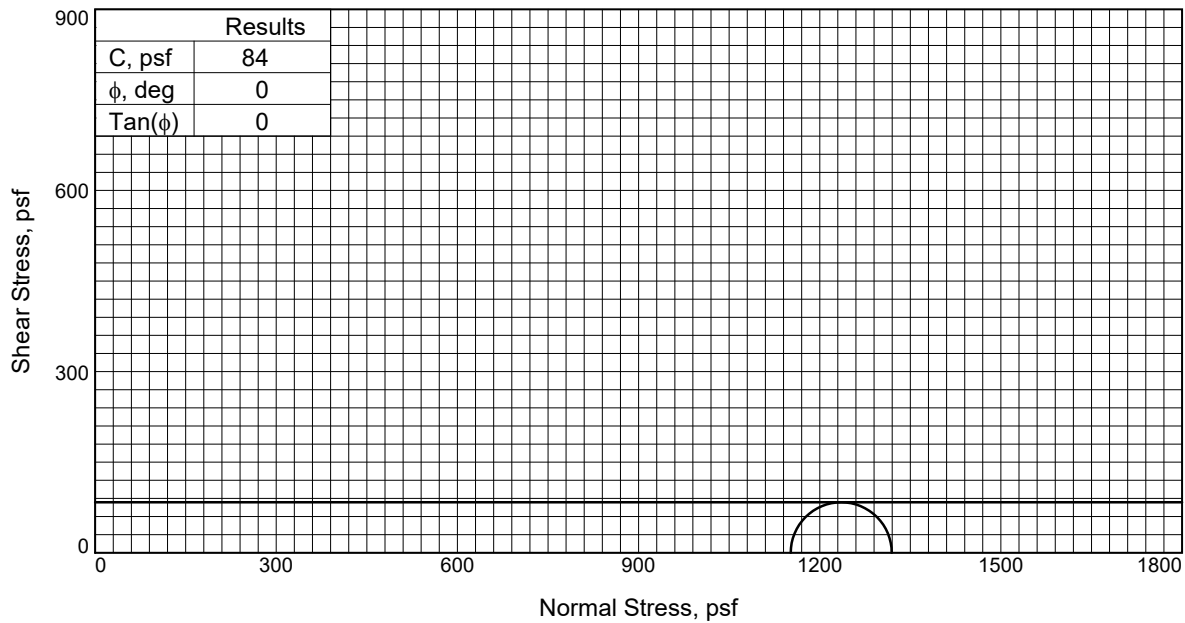
**Source of Sample:** B-5      **Depth:** 16-18

**Sample Number:** 9

**Proj. No.:** APS2008-G063

**Date Sampled:** 8-14-2020





Sample No.	1	
Initial	Water Content, %	64.7
	Dry Density, pcf	61.6
	Saturation, %	104.0
	Void Ratio	1.5928
	Diameter, in.	2.83
At Test	Height, in.	5.80
	Water Content, %	64.7
	Dry Density, pcf	61.6
	Saturation, %	104.0
	Void Ratio	1.5928
	Diameter, in.	2.82
	Height, in.	5.80
Strain at peak, %	11.5	
Back Pressure, psi	0.00	
Cell Pressure, psi	8.00	
Fail. Stress, psf	167	
Ult. Stress, psf	167	
$\sigma_1$ Failure, psf	1319	
$\sigma_3$ Failure, psf	1152	

**Type of Test:**

Unconsolidated Undrained

**Sample Type:** Undisturbed

**Description:** Very soft gray fat clay (CH)

LL= 88

PL= 26

PI= 62

**Specific Gravity=** 2.56

**Remarks:** Failure Type : Bulge

**Client:** CPRA

**Project:** BRETON LANDBRIDGE MARSH CREATION

**Source of Sample:** B-5

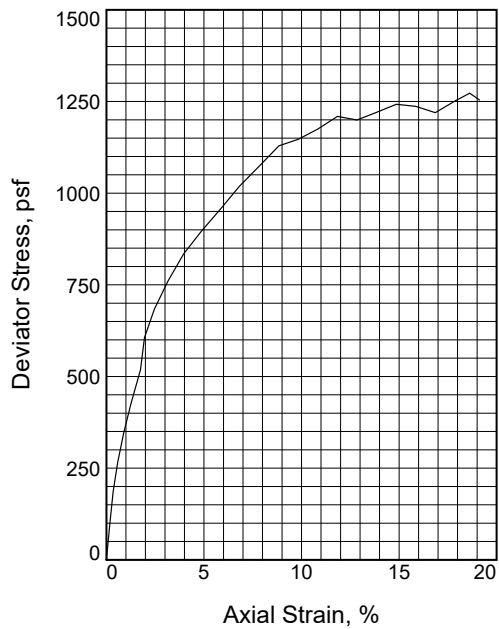
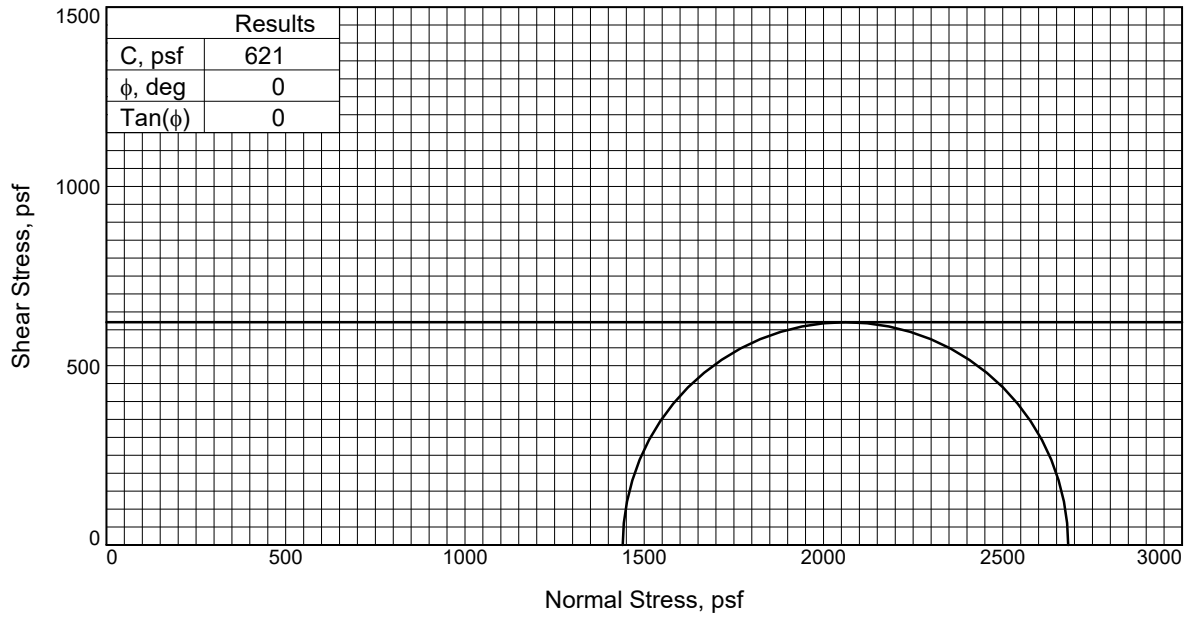
**Depth:** 18-20

**Sample Number:** 10

**Proj. No.:** APS2008-G063

**Date Sampled:** 8-14-2020





Sample No.	1	
Initial	Water Content, %	32.9
	Dry Density, pcf	90.8
	Saturation, %	103.8
	Void Ratio	0.8563
	Diameter, in.	2.75
	Height, in.	5.74
At Test	Water Content, %	32.9
	Dry Density, pcf	90.8
	Saturation, %	103.8
	Void Ratio	0.8563
	Diameter, in.	2.75
	Height, in.	5.74
Strain at peak, %	14.9	
Back Pressure, psi	0.00	
Cell Pressure, psi	10.00	
Fail. Stress, psf	1242	
Ult. Stress, psf	1242	
$\sigma_1$ Failure, psf	2682	
$\sigma_3$ Failure, psf	1440	

**Type of Test:**

Unconsolidated Undrained

**Sample Type:** Undisturbed

**Description:** Medium Stiff Gray Lean Clay (CL) -with fine sand

**LL= 42      PL= 21      PI= 21**

**Assumed Specific Gravity= 2.7**

**Remarks:** Failure Type : Bulge  
Failure limit to 15%

**Client:** CPRA

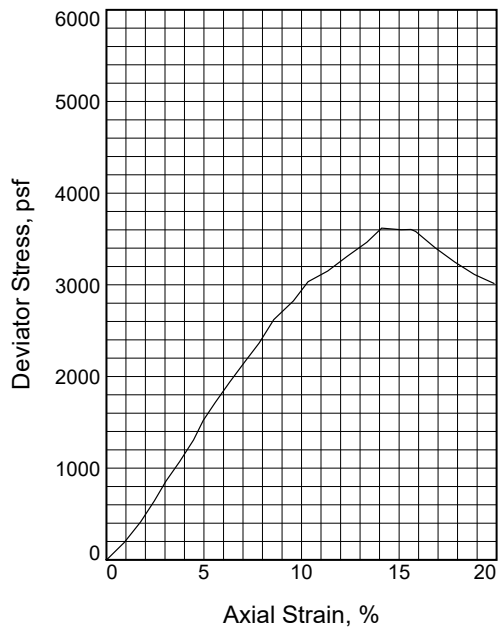
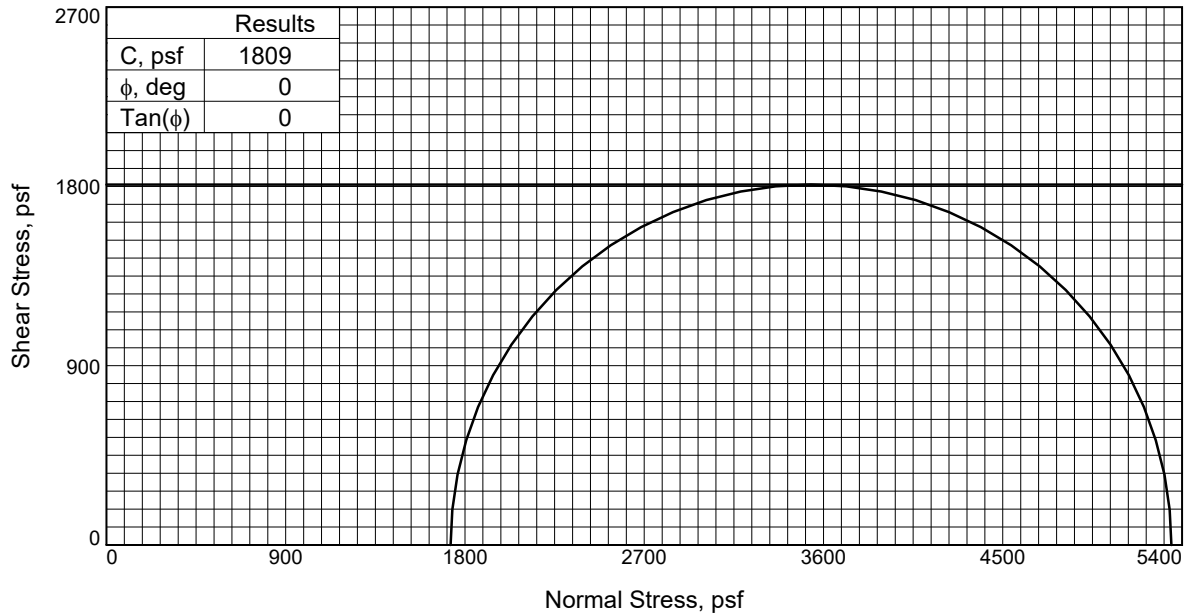
**Project:** BRETON LANDBRIDGE MARSH CREATION

**Source of Sample:** B-5      **Depth:** 23-25

**Sample Number:** 11

**Proj. No.:** APS2008-G063      **Date Sampled:** 8-14-2020





Sample No.	1	
Initial	Water Content, %	25.6
	Dry Density, pcf	101.2
	Saturation, %	104.0
	Void Ratio	0.6655
	Diameter, in.	2.71
At Test	Height, in.	5.70
	Water Content, %	25.6
	Dry Density, pcf	101.2
	Saturation, %	104.0
	Void Ratio	0.6655
Diameter, in.	2.71	
Height, in.	5.70	
Strain at peak, %	14.1	
Back Pressure, psi	0.00	
Cell Pressure, psi	12.00	
Fail. Stress, psf	3618	
Ult. Stress, psf	3618	
$\sigma_1$ Failure, psf	5346	
$\sigma_3$ Failure, psf	1728	

**Type of Test:**

Unconsolidated Undrained

**Sample Type:** Undisturbed

**Description:** Very Stiff Gray Silty Clay (CL-ML)

LL= NV

PI= NP

**Assumed Specific Gravity=** 2.7

**Remarks:** Failure Type : Bulge

Failure limit to 15%

**Client:** CPRA

**Project:** BRETON LANDBRIDGE MARSH CREATION

**Source of Sample:** B-5

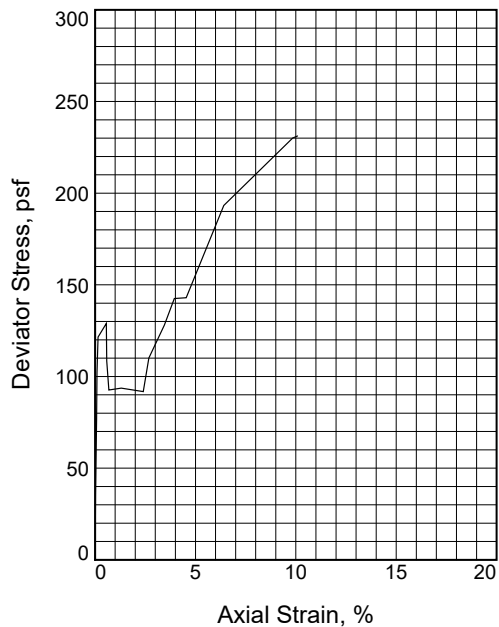
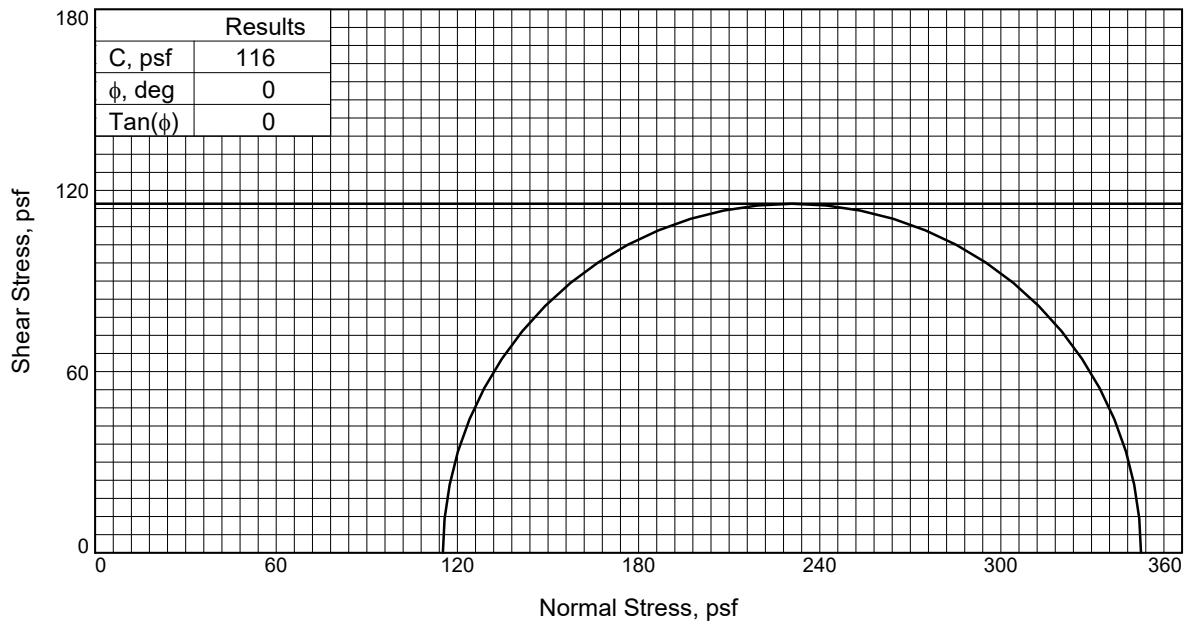
**Depth:** 28-30

**Sample Number:** 12

**Proj. No.:** APS2008-G063

**Date Sampled:** 8-14-2020





Sample No.	1	
Initial	Water Content, %	203.4
	Dry Density, pcf	22.6
	Saturation, %	86.6
	Void Ratio	5.6350
	Diameter, in.	2.79
	Height, in.	5.26
At Test	Water Content, %	203.4
	Dry Density, pcf	22.6
	Saturation, %	86.6
	Void Ratio	5.6350
	Diameter, in.	2.79
	Height, in.	5.26
Strain at peak, %	10.1	
Back Pressure, psi	0.00	
Cell Pressure, psi	0.80	
Fail. Stress, psf	231	
Ult. Stress, psf	231	
$\sigma_1$ Failure, psf	346	
$\sigma_3$ Failure, psf	115	

**Type of Test:**

Unconsolidated Undrained

**Sample Type:** Undisturbed

**Description:** Very Soft Dark Gray Fat Clay (CH)

**LL=** 173      **PL=** 39      **PI=** 134

**Specific Gravity=** 2.4

**Remarks:** Failure Type : Bulge

**Client:** CPRA

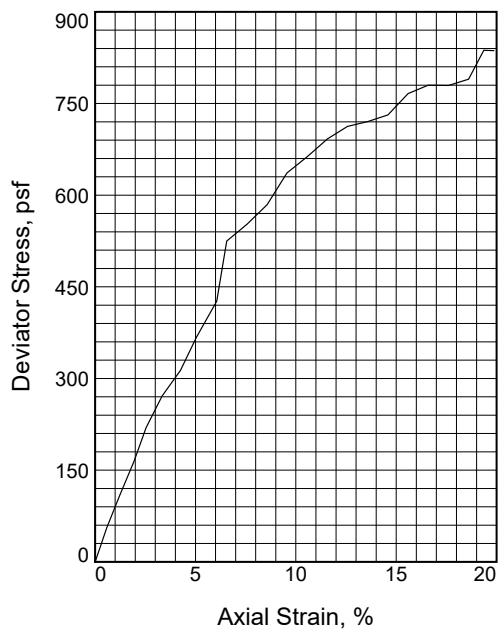
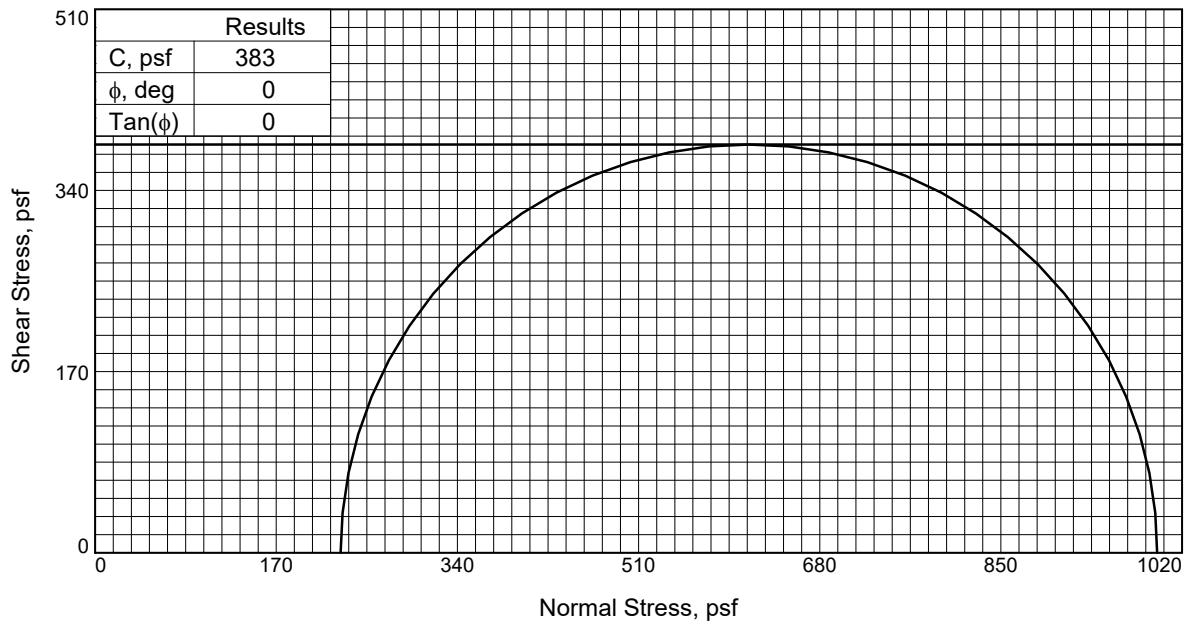
**Project:** BRETON LANDBRIDGE MARSH CREATION

**Source of Sample:** B-6      **Depth:** 0-2

**Sample Number:** 1

**Proj. No.:** APS2008-G063      **Date Sampled:** 8-14-2020





Sample No.	1	
Initial	Water Content, %	32.9
	Dry Density, pcf	89.4
	Saturation, %	100.4
	Void Ratio	0.8860
	Diameter, in.	2.81
	Height, in.	5.78
At Test	Water Content, %	32.9
	Dry Density, pcf	89.4
	Saturation, %	100.4
	Void Ratio	0.8860
	Diameter, in.	2.81
	Height, in.	5.78
Strain at peak, %	15.6	
Back Pressure, psi	0.00	
Cell Pressure, psi	1.60	
Fail. Stress, psf	766	
Ult. Stress, psf	766	
$\sigma_1$ Failure, psf	997	
$\sigma_3$ Failure, psf	230	

**Type of Test:**

Unconsolidated Undrained

**Sample Type:** Undisturbed

**Description:** Soft Gray Lean Clay(CL)-with fine sand

**LL= 40      PL= 20      PI= 20**

**Assumed Specific Gravity= 2.7**

**Remarks:** Failure Type : Bulge  
Failure limit to 15%

**Client:** CPRA

**Project:** BRETON LANDBRIDGE MARSH CREATION

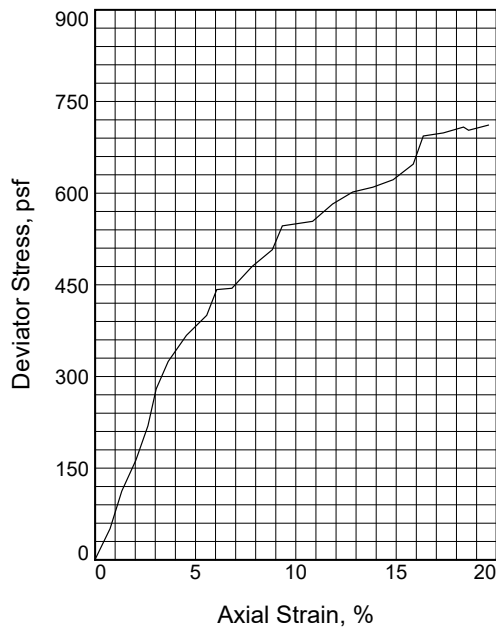
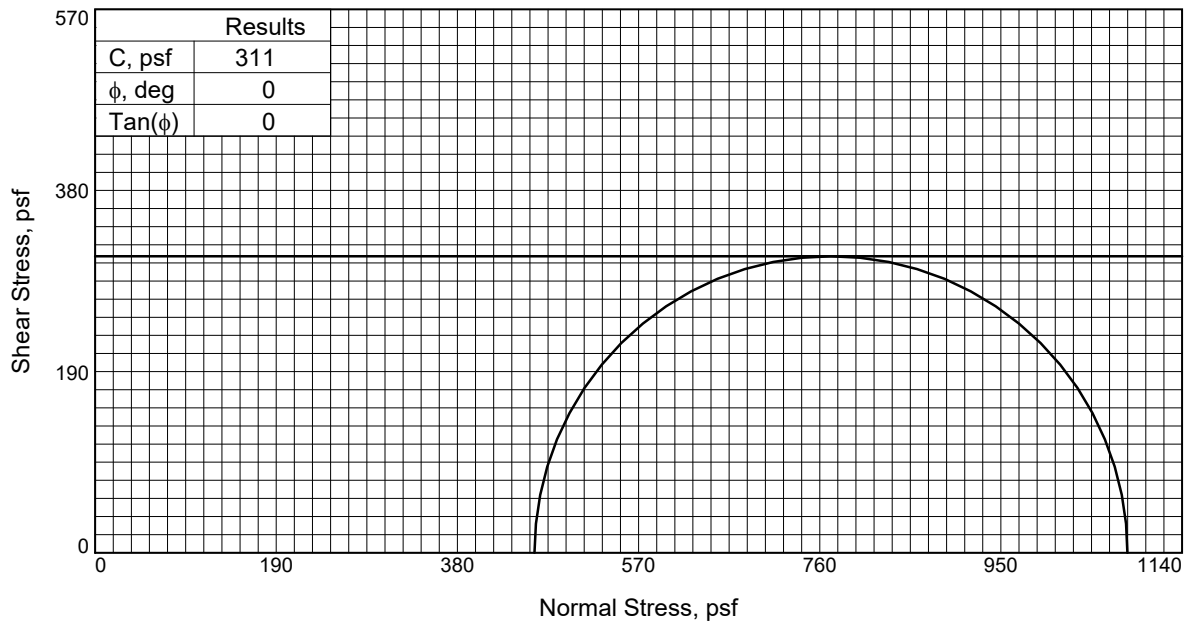
**Source of Sample:** B-6      **Depth:** 2-4

**Sample Number:** 2

**Proj. No.:** APS2008-G063

**Date Sampled:** 8-14-2020





Sample No.	1	
Initial	Water Content, %	42.1
	Dry Density, pcf	79.7
	Saturation, %	102.1
	Void Ratio	1.1148
	Diameter, in.	2.90
	Height, in.	5.75
At Test	Water Content, %	42.1
	Dry Density, pcf	79.7
	Saturation, %	102.1
	Void Ratio	1.1148
	Diameter, in.	2.90
	Height, in.	5.75
Strain at peak, %	14.8	
Back Pressure, psi	0.00	
Cell Pressure, psi	3.20	
Fail. Stress, psf	622	
Ult. Stress, psf	622	
$\sigma_1$ Failure, psf	1083	
$\sigma_3$ Failure, psf	461	

**Type of Test:**

Unconsolidated Undrained

**Sample Type:** Undisturbed

**Description:** Gray Silt with Sand (ML)

**LL=** 29

**PI=** NP

**Assumed Specific Gravity=** 2.7

**Remarks:** Failure Type : Bulge

Failure limit to 15%

**Client:** CPRA

**Project:** BRETON LANDBRIDGE MARSH CREATION

**Source of Sample:** B-6

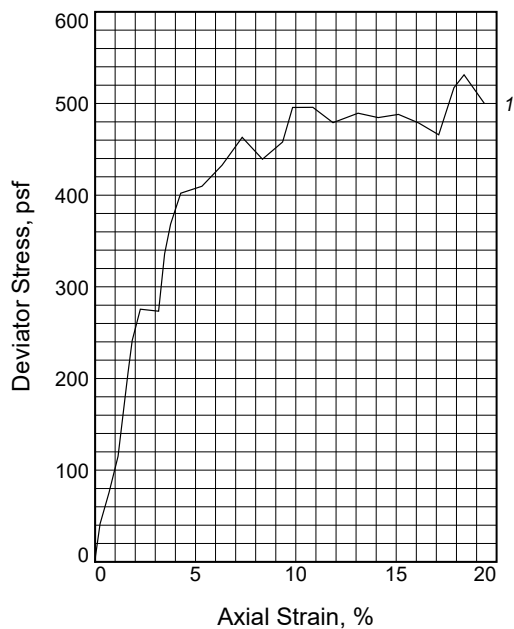
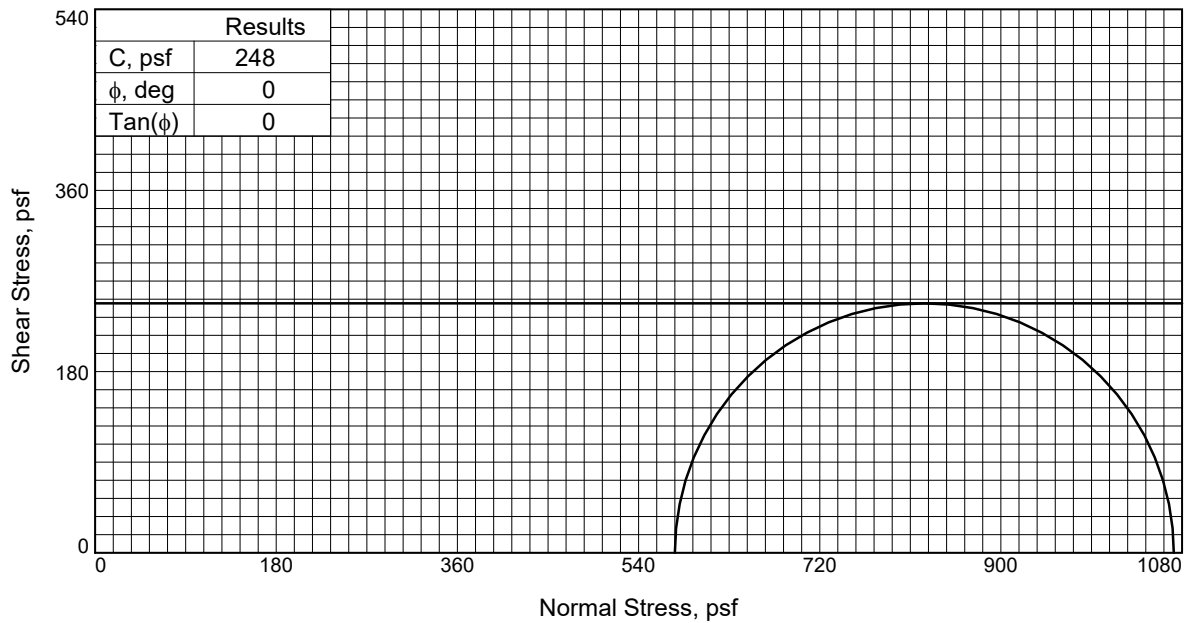
**Depth:** 6-8

**Sample Number:** 4

**Proj. No.:** APS2008-G063

**Date Sampled:** 8-14-2020





Sample No.	1	
Initial	Water Content, %	45.4
	Dry Density, pcf	74.6
	Saturation, %	97.2
	Void Ratio	1.2604
	Diameter, in.	2.83
	Height, in.	5.84
At Test	Water Content, %	45.4
	Dry Density, pcf	74.6
	Saturation, %	97.2
	Void Ratio	1.2604
	Diameter, in.	2.83
	Height, in.	5.84
Strain at peak, %	10.8	
Back Pressure, psi	0.00	
Cell Pressure, psi	4.00	
Fail. Stress, psf	496	
Ult. Stress, psf	496	
$\sigma_1$ Failure, psf	1072	
$\sigma_3$ Failure, psf	576	

**Type of Test:**

Unconsolidated Undrained

**Sample Type:** Undisturbed

**Description:** Soft Gray Lean Clay (CL) -with fine sand

**LL= 48      PL= 24      PI= 24**

**Assumed Specific Gravity= 2.7**

**Remarks:** Failure Type : Bulge

**Client:** CPRA

**Project:** BRETON LANDBRIDGE MARSH CREATION

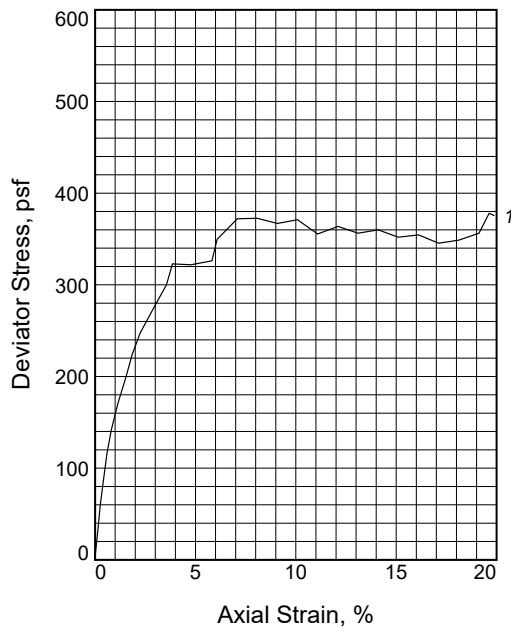
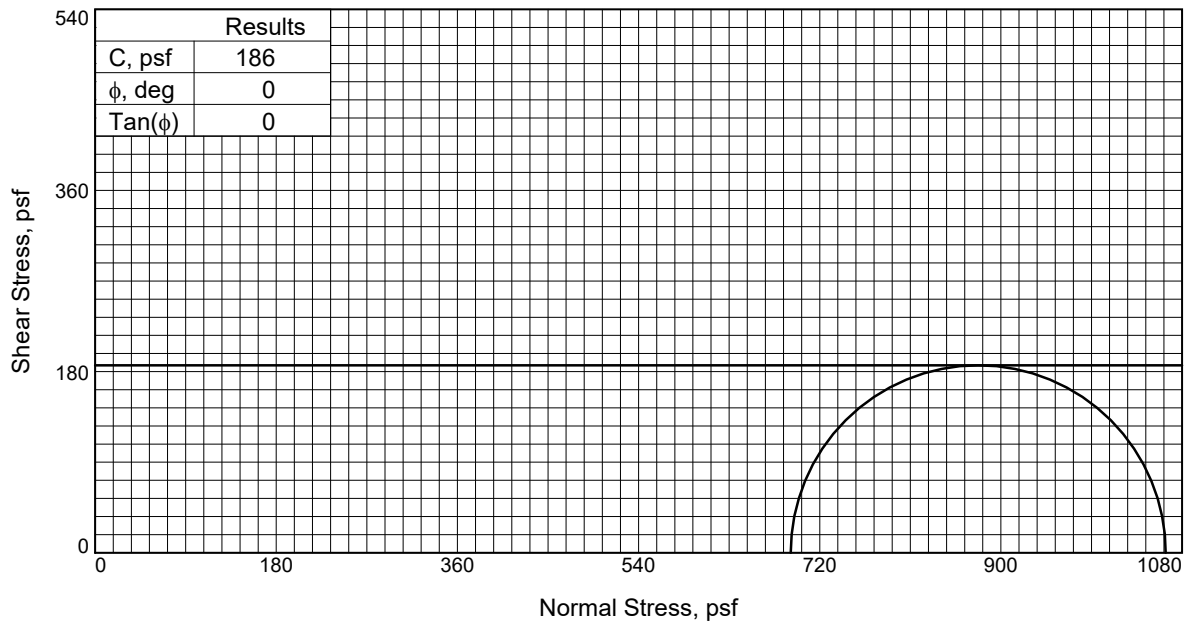
**Source of Sample:** B-6      **Depth:** 8-10

**Sample Number:** 5

**Proj. No.:** APS2008-G063      **Date Sampled:** 8-14-2020







Sample No.	1	
Initial	Water Content, %	79.0
	Dry Density, pcf	53.3
	Saturation, %	98.6
	Void Ratio	2.1638
	Diameter, in.	2.80
At Test	Height, in.	5.82
	Water Content, %	79.0
	Dry Density, pcf	53.3
	Saturation, %	98.6
	Void Ratio	2.1638
Diameter, in.	2.80	
Height, in.	5.82	
Strain at peak, %	8.1	
Back Pressure, psi	0.00	
Cell Pressure, psi	4.80	
Fail. Stress, psf	373	
Ult. Stress, psf	373	
$\sigma_1$ Failure, psf	1064	
$\sigma_3$ Failure, psf	691	

**Type of Test:**

Unconsolidated Undrained

**Sample Type:** Undisturbed

**Description:** Soft Gray Lean Clay (CL) -with fine sand

**LL= 108      PL= 34      PI= 74**

**Assumed Specific Gravity= 2.7**

**Remarks:** Failure Type : Bulge

**Client:** CPRA

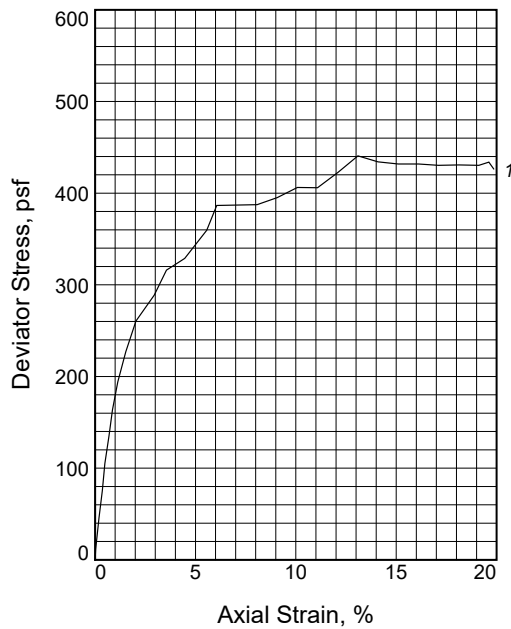
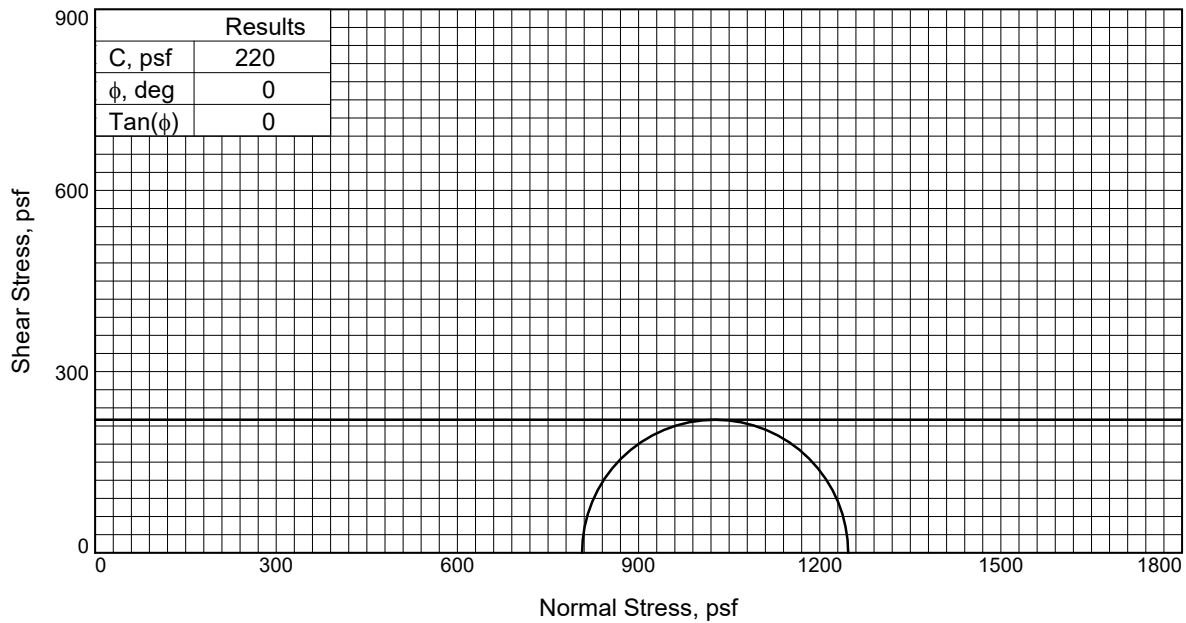
**Project:** BRETON LANDBRIDGE MARSH CREATION

**Source of Sample:** B-6      **Depth:** 10-12

**Sample Number:** 6

**Proj. No.:** APS2008-G063      **Date Sampled:** 8-14-2020





Sample No.	1	
Initial	Water Content, %	71.1
	Dry Density, pcf	54.7
	Saturation, %	94.2
	Void Ratio	1.9555
	Diameter, in.	2.84
	Height, in.	5.82
At Test	Water Content, %	71.1
	Dry Density, pcf	54.7
	Saturation, %	94.2
	Void Ratio	1.9555
	Diameter, in.	2.84
	Height, in.	5.82
Strain at peak, %	13.1	
Back Pressure, psi	0.00	
Cell Pressure, psi	5.60	
Fail. Stress, psf	441	
Ult. Stress, psf	441	
$\sigma_1$ Failure, psf	1247	
$\sigma_3$ Failure, psf	806	

**Type of Test:**

Unconsolidated Undrained

**Sample Type:** Undisturbed

**Description:** Very Soft Gray Fat Clay (CH)

**LL=** 113      **PL=** 37      **PI=** 76

**Assumed Specific Gravity=** 2.59

**Remarks:** Failure Type : Bulge

**Client:** CPRA

**Project:** BRETON LANDBRIDGE MARSH CREATION

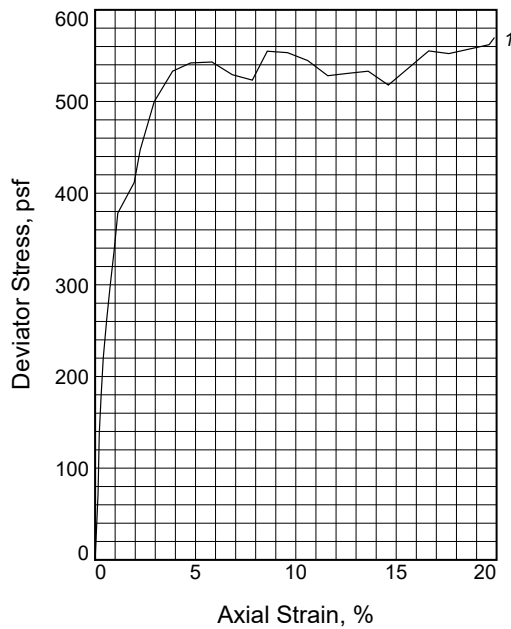
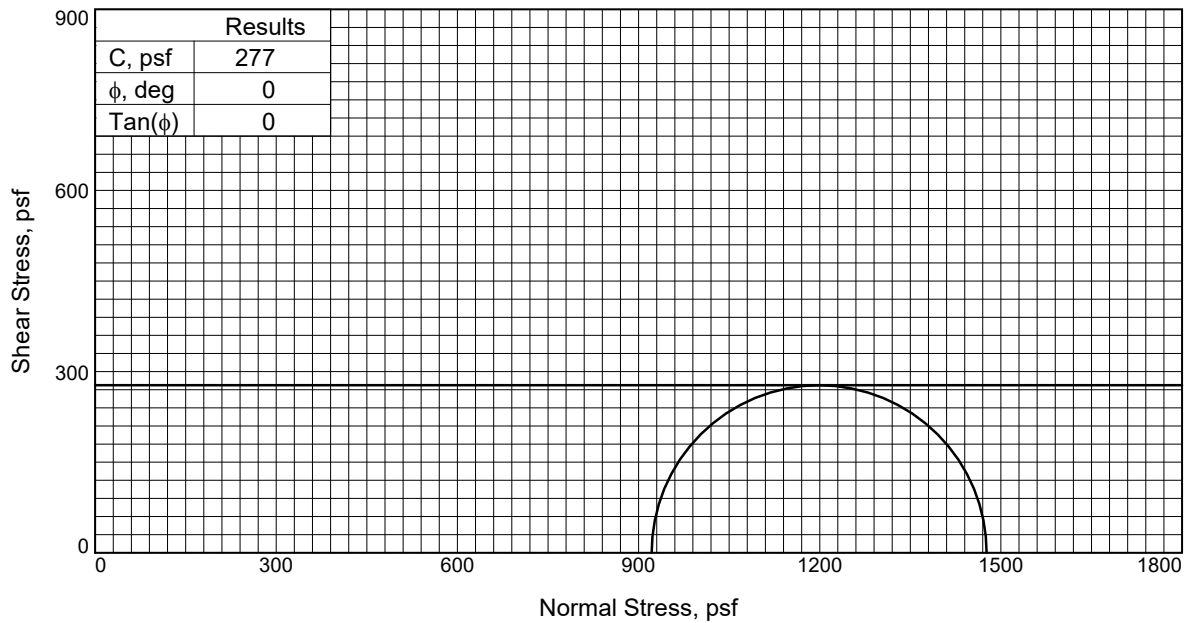
**Source of Sample:** B-6      **Depth:** 12-14

**Sample Number:** 7

**Proj. No.:** APS2008-G063

**Date Sampled:** 8-14-2020





Sample No.	1	
Initial	Water Content, %	85.4
	Dry Density, pcf	50.1
	Saturation, %	97.5
	Void Ratio	2.3655
	Diameter, in.	2.85
At Test	Height, in.	5.84
	Water Content, %	85.4
	Dry Density, pcf	50.1
	Saturation, %	97.5
	Void Ratio	2.3655
Diameter, in.	2.85	
Height, in.	5.84	
Strain at peak, %	8.6	
Back Pressure, psi	0.00	
Cell Pressure, psi	6.40	
Fail. Stress, psf	555	
Ult. Stress, psf	555	
$\sigma_1$ Failure, psf	1476	
$\sigma_3$ Failure, psf	922	

**Type of Test:**

Unconsolidated Undrained

**Sample Type:** Undisturbed

**Description:** Soft Gray Fat Clay (CH)

**LL=** 119      **PL=** 34      **PI=** 85

**Assumed Specific Gravity=** 2.7

**Remarks:** Failure Type : Bulge

**Client:** CPRA

**Project:** BRETON LANDBRIDGE MARSH CREATION

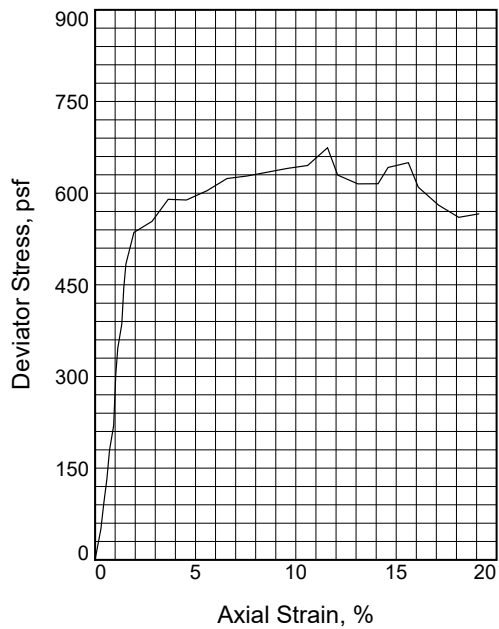
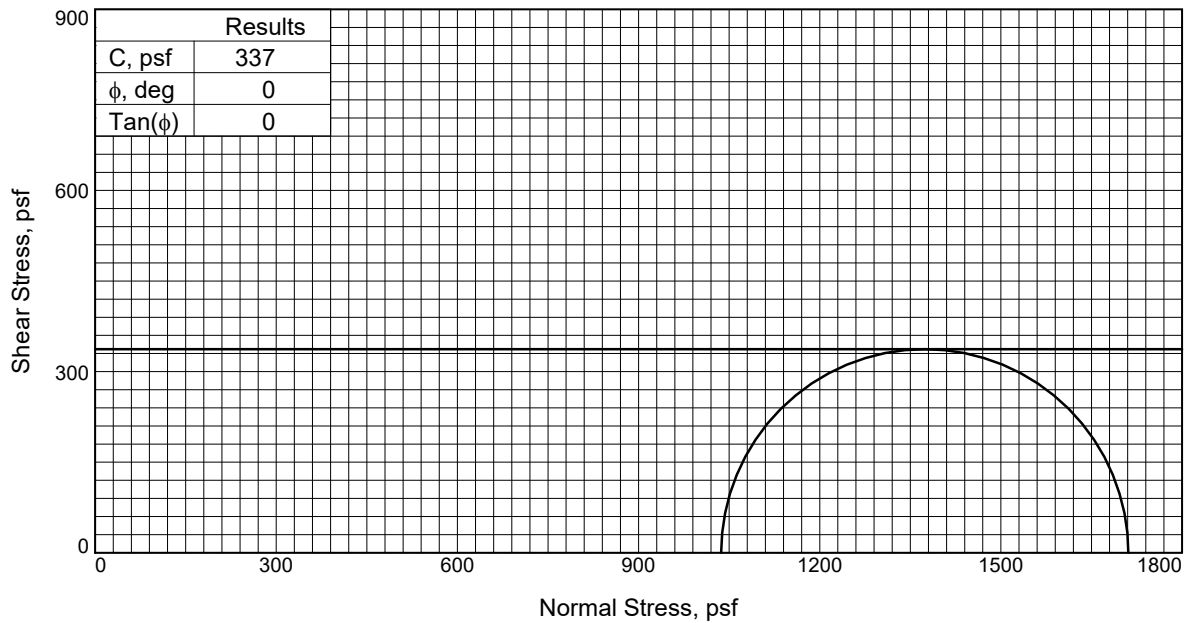
**Source of Sample:** B-6      **Depth:** 14-16

**Sample Number:** 8

**Proj. No.:** APS2008-G063

**Date Sampled:** 8-14-2020





Sample No.	1	
Initial	Water Content, %	78.4
	Dry Density, pcf	52.4
	Saturation, %	95.4
	Void Ratio	2.2174
	Diameter, in.	2.85
At Test	Height, in.	5.78
	Water Content, %	78.4
	Dry Density, pcf	52.4
	Saturation, %	95.4
	Void Ratio	2.2174
Diameter, in.	2.85	
Height, in.	5.78	
Strain at peak, %	11.6	
Back Pressure, psi	0.00	
Cell Pressure, psi	7.20	
Fail. Stress, psf	674	
Ult. Stress, psf	674	
$\sigma_1$ Failure, psf	1711	
$\sigma_3$ Failure, psf	1037	

**Type of Test:**

Unconsolidated Undrained

**Sample Type:** Undisturbed

**Description:** Soft Gray Lean Clay (CL)-with fine sand

**LL= 32      PL= 24      PI= 8**

**Assumed Specific Gravity= 2.7**

**Remarks:** Failure Type : Bulge

**Client:** CPRA

**Project:** BRETON LANDBRIDGE MARSH CREATION

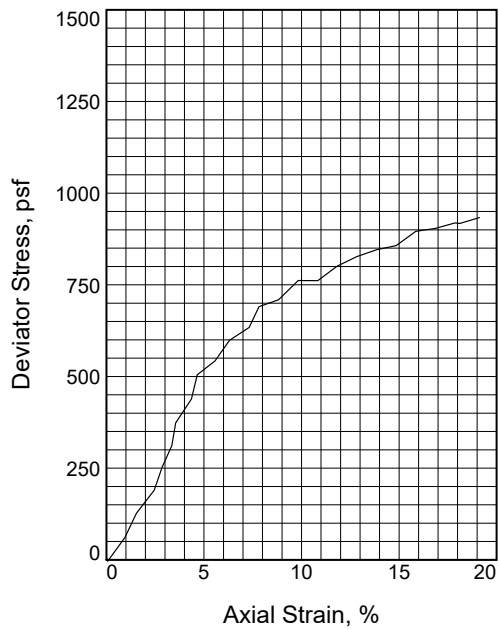
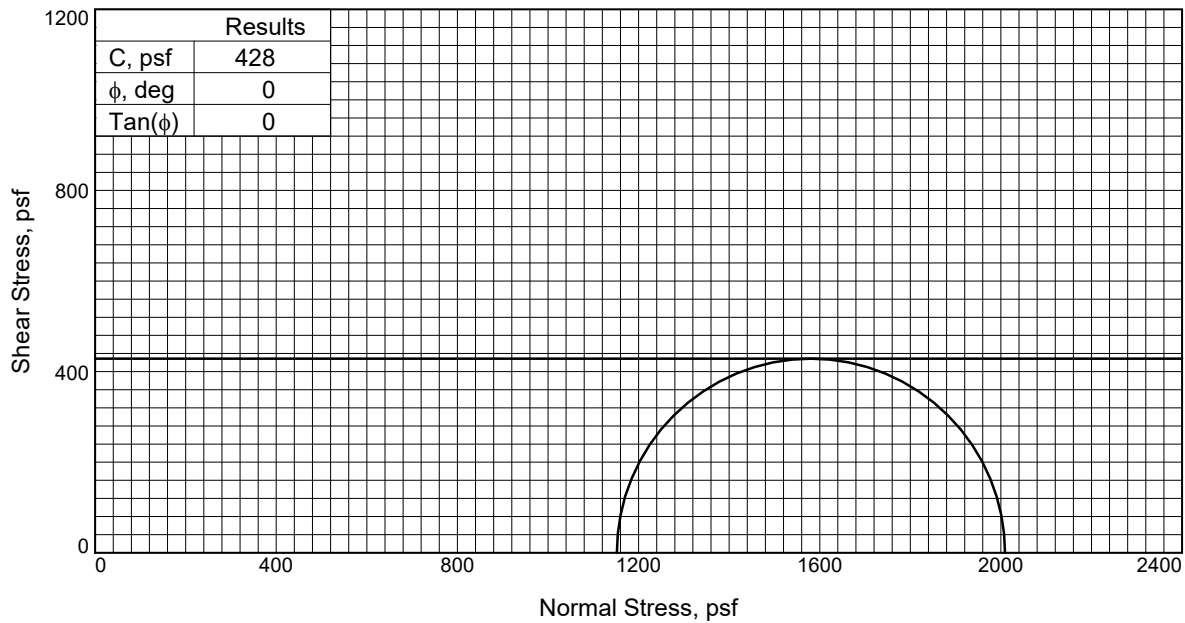
**Source of Sample:** B-6      **Depth:** 16-18

**Sample Number:** 9

**Proj. No.:** APS2008-G063

**Date Sampled:** 8-14-2020





Sample No.	1	
Initial	Water Content, %	32.0
	Dry Density, pcf	84.2
	Saturation, %	86.3
	Void Ratio	1.0015
	Diameter, in.	2.87
At Test	Height, in.	5.79
	Water Content, %	32.0
	Dry Density, pcf	84.2
	Saturation, %	86.3
	Void Ratio	1.0015
Diameter, in.	2.87	
Height, in.	5.79	
Strain at peak, %	14.9	
Back Pressure, psi	0.00	
Cell Pressure, psi	8.00	
Fail. Stress, psf	857	
Ult. Stress, psf	857	
$\sigma_1$ Failure, psf	2009	
$\sigma_3$ Failure, psf	1152	

**Type of Test:**

Unconsolidated Undrained

**Sample Type:** Undisturbed

**Description:** Soft Gray Lean Clay (CL)-with fine sand

**LL= 38      PL= 21      PI= 17**

**Assumed Specific Gravity= 2.7**

**Remarks:** Failure Type : Bulge

Failure limit to 15%

**Client:** CPRA

**Project:** BRETON LANDBRIDGE MARSH CREATION

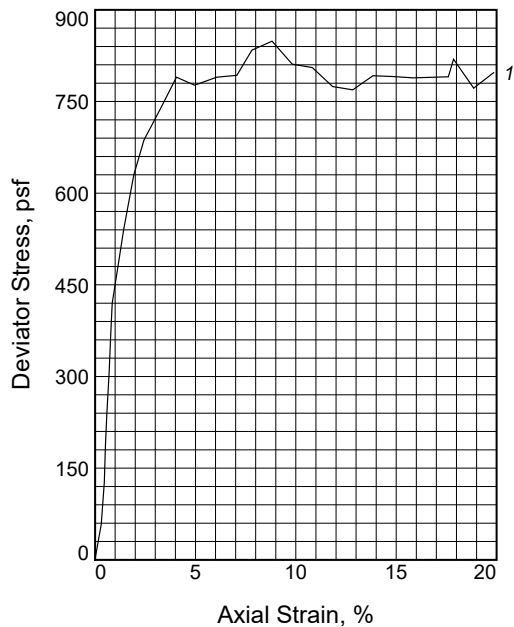
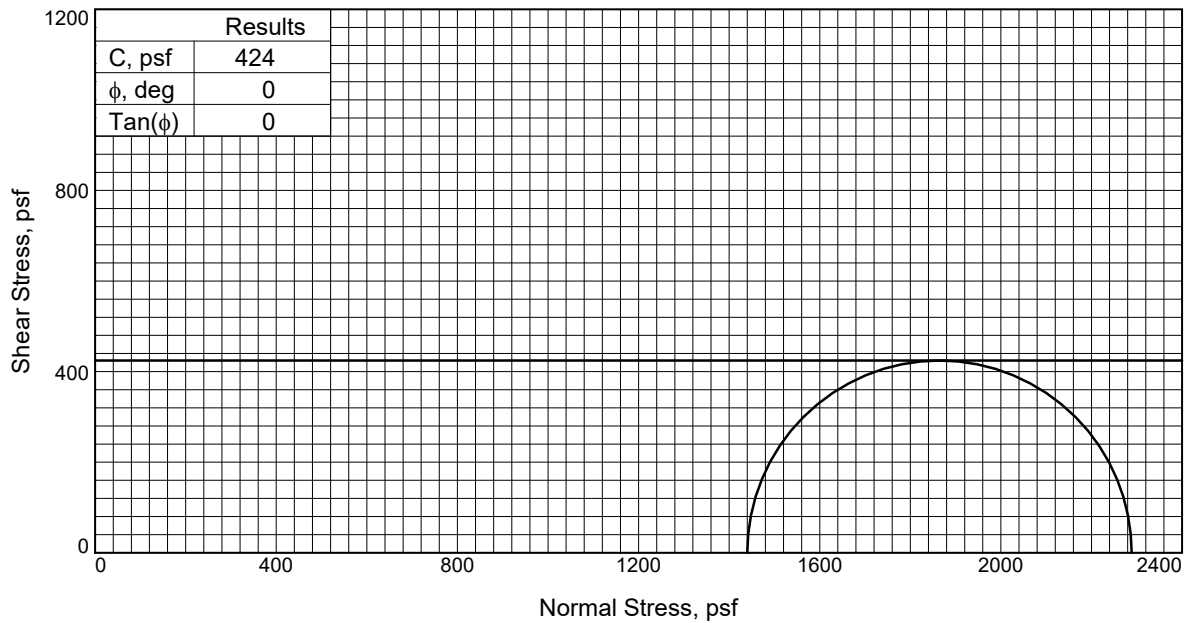
**Source of Sample:** B-6      **Depth:** 18-20

**Sample Number:** 10

**Proj. No.:** APS2008-G063

**Date Sampled:** 8-14-2020





Sample No.	1	
Initial	Water Content, %	71.3
	Dry Density, pcf	57.2
	Saturation, %	98.9
	Void Ratio	1.9461
	Diameter, in.	2.83
	Height, in.	5.81
At Test	Water Content, %	71.3
	Dry Density, pcf	57.2
	Saturation, %	98.9
	Void Ratio	1.9461
	Diameter, in.	2.83
	Height, in.	5.81
Strain at peak, %	8.8	
Back Pressure, psi	0.00	
Cell Pressure, psi	10.00	
Fail. Stress, psf	849	
Ult. Stress, psf	849	
$\sigma_1$ Failure, psf	2289	
$\sigma_3$ Failure, psf	1440	

**Type of Test:**

Unconsolidated Undrained

**Sample Type:** Undisturbed

**Description:** Soft Gray Fat Clay (CH)

LL= 96      PL= 31      PI= 65

**Assumed Specific Gravity=** 2.7

**Remarks:** Failure Type : Bulge

**Client:** CPRA

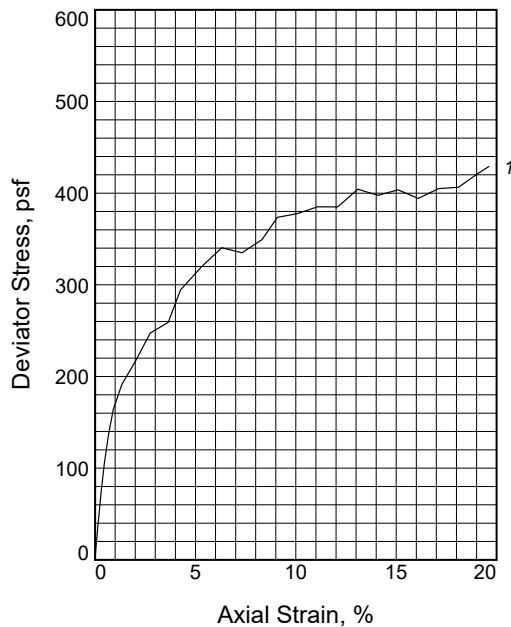
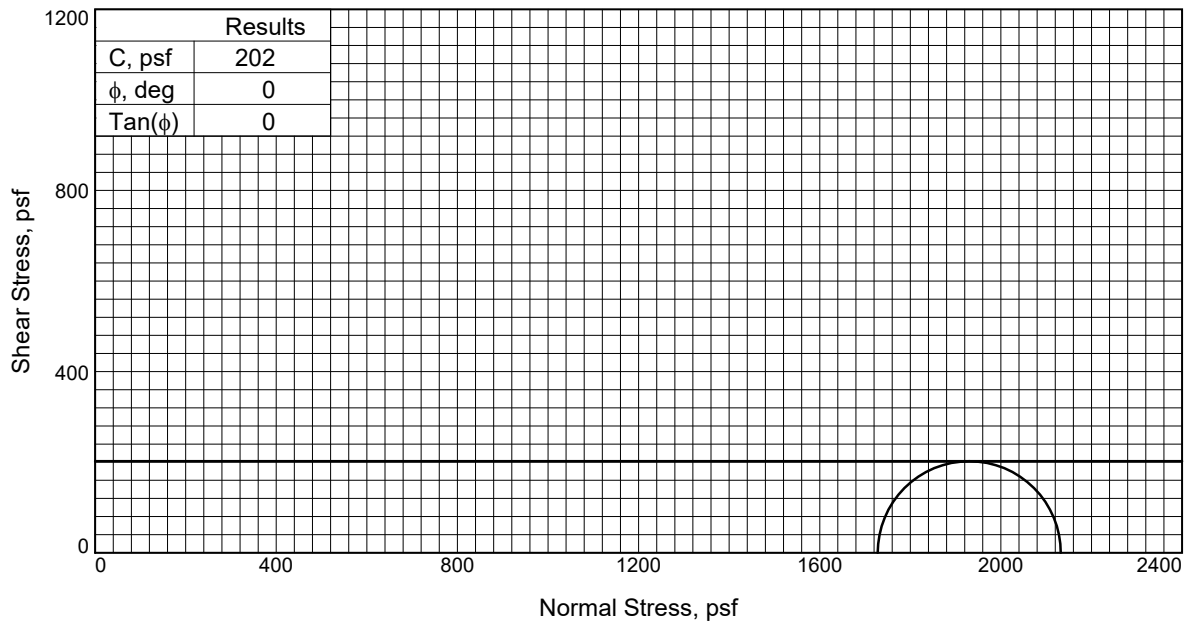
**Project:** BRETON LANDBRIDGE MARSH CREATION

**Source of Sample:** B-6      **Depth:** 23-25

**Sample Number:** 11

**Proj. No.:** APS2008-G063      **Date Sampled:** 8-14-2020





Sample No.	1	
Initial	Water Content, %	69.3
	Dry Density, pcf	59.6
	Saturation, %	103.9
	Void Ratio	1.7541
	Diameter, in.	2.79
At Test	Height, in.	5.83
	Water Content, %	69.3
	Dry Density, pcf	59.6
	Saturation, %	103.9
	Void Ratio	1.7541
Diameter, in.	2.79	
Height, in.	5.83	
Strain at peak, %	13.1	
Back Pressure, psi	0.00	
Cell Pressure, psi	12.00	
Fail. Stress, psf	404	
Ult. Stress, psf	404	
$\sigma_1$ Failure, psf	2132	
$\sigma_3$ Failure, psf	1728	

**Type of Test:**

Unconsolidated Undrained

**Sample Type:** Undisturbed

**Description:** Very soft gray fat clay (CH)

LL= 81      PL= 25      PI= 56

**Specific Gravity=** 2.63

**Remarks:** Failure Type : Bulge

**Client:** CPRA

**Project:** BRETON LANDBRIDGE MARSH CREATION

**Source of Sample:** B-6      **Depth:** 28-30

**Sample Number:** 12

**Proj. No.:** APS2008-G063

**Date Sampled:** 8-14-2020

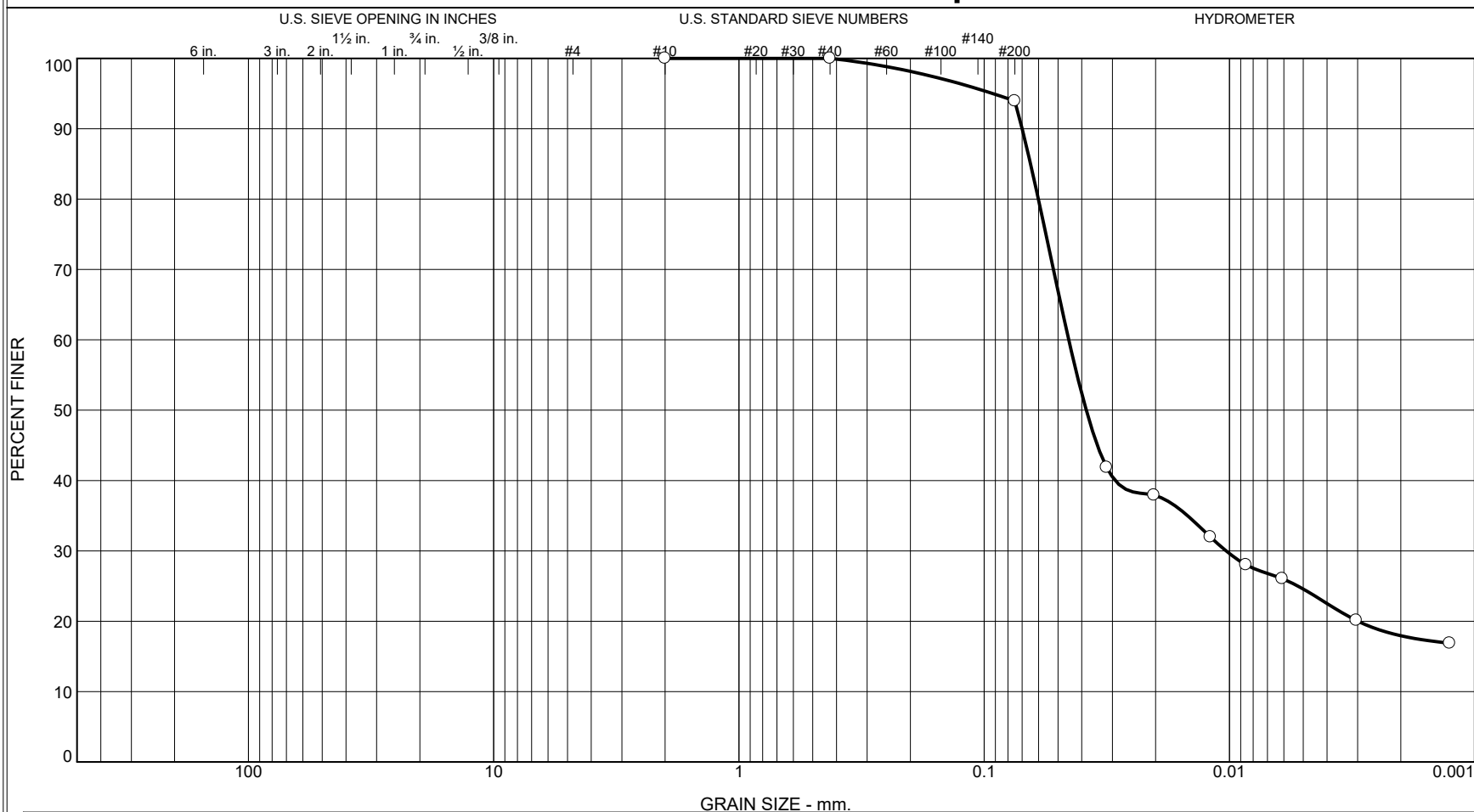


## **APPENDIX D**

### **(Grain-Size Curves)**




# Particle Size Distribution Report

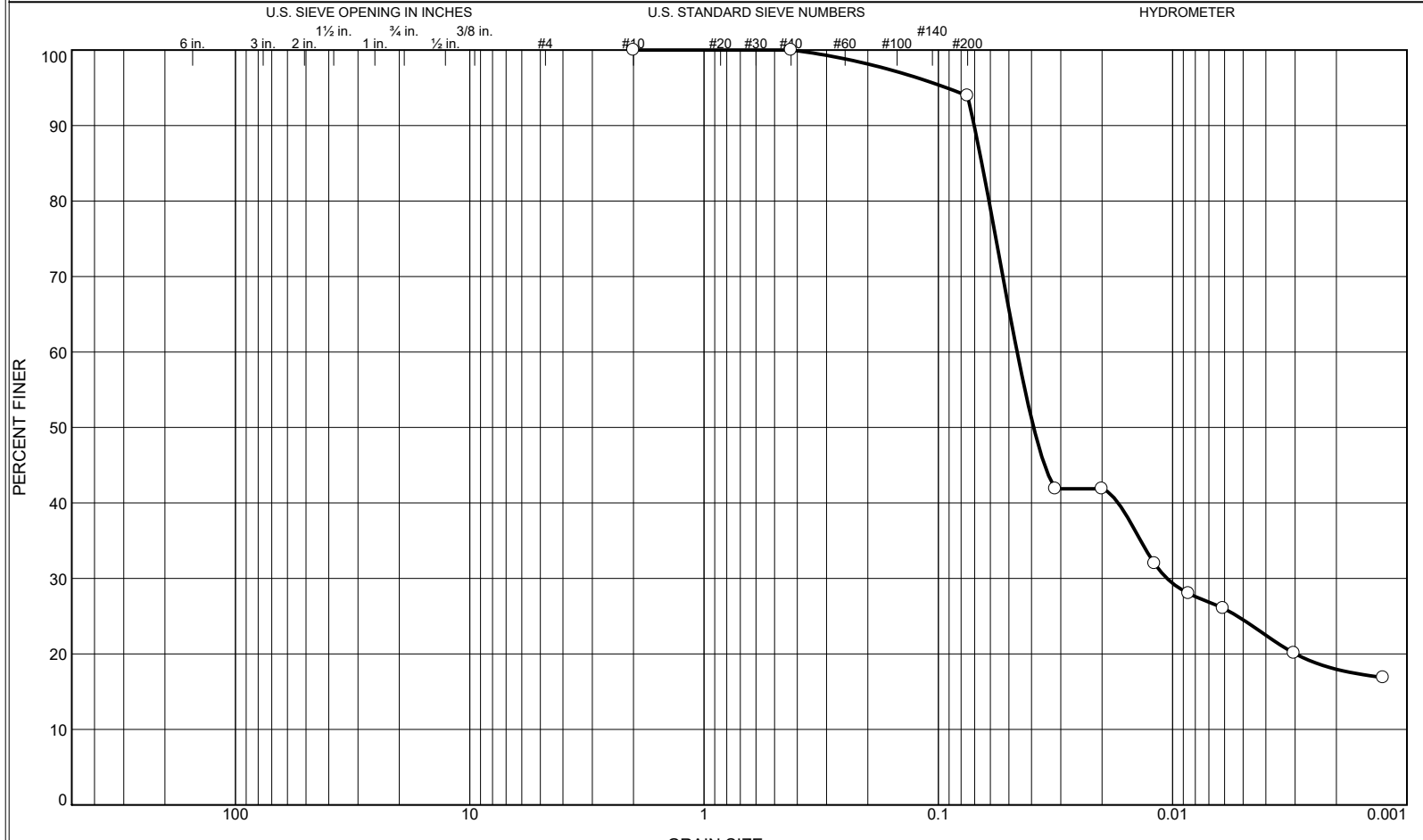


% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	6.1	69.3	24.6

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-7	Depth: 0-2	Sample Number: 1			


Client CPRA		
Project Breton Landbridge Marsh Creation(West)		
Project No. APS2008-G063		Figure

# Particle Size Distribution Report

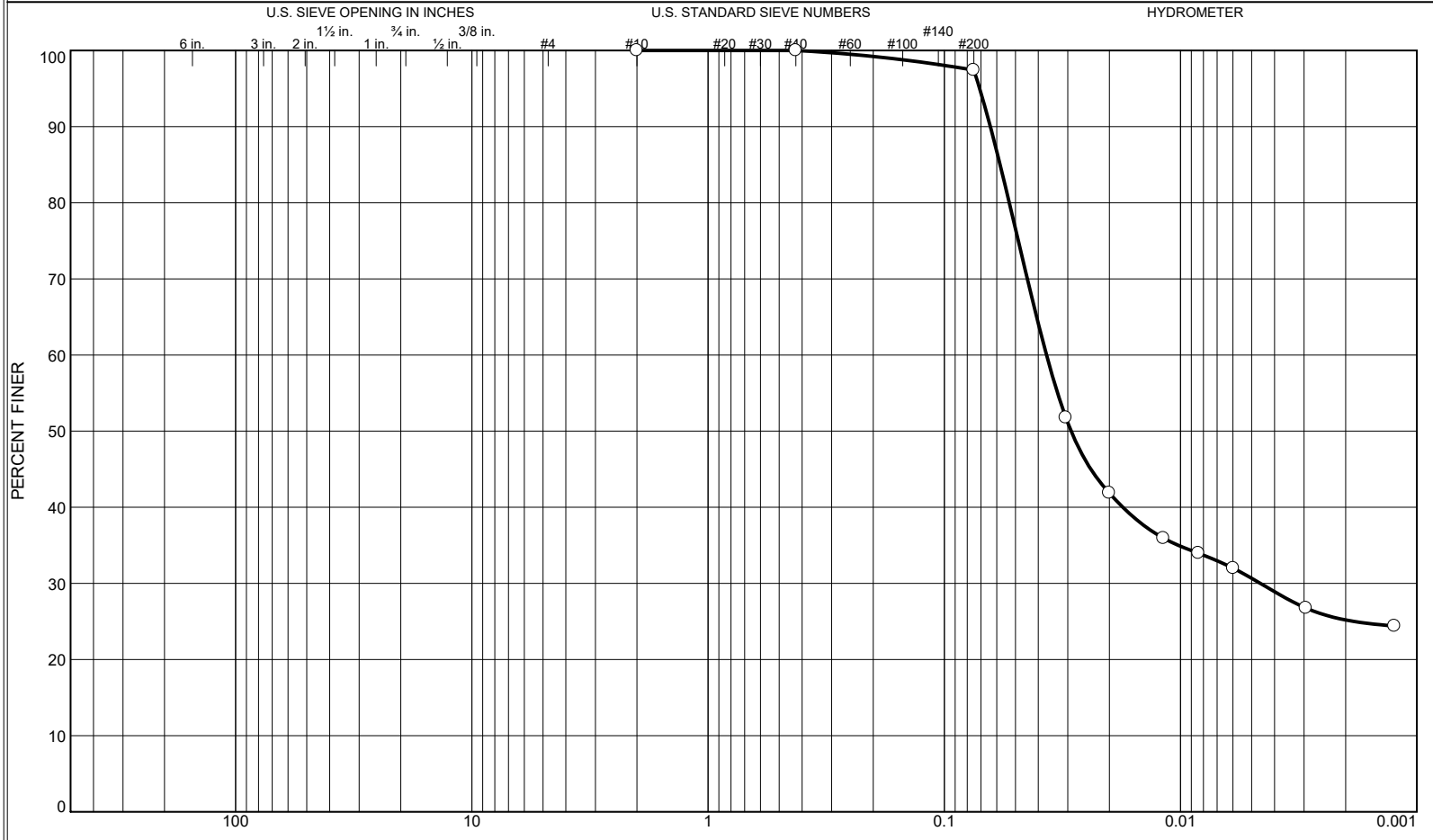


% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	6.1	69.4	24.5

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-7	Depth: 0-2	Sample Number: 1			

Client CPRA		
Project Breton Landbridge Marsh Creation(West)		
Project No. APS2008-G063		

# Particle Size Distribution Report



% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	2.6	66.7	30.7

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-7	Depth: 2-4	Sample Number: 2			


Client CPRA		
Project Breton Landbridge Marsh Creation(West)		
Project No. APS2008-G063		

# Particle Size Distribution Report

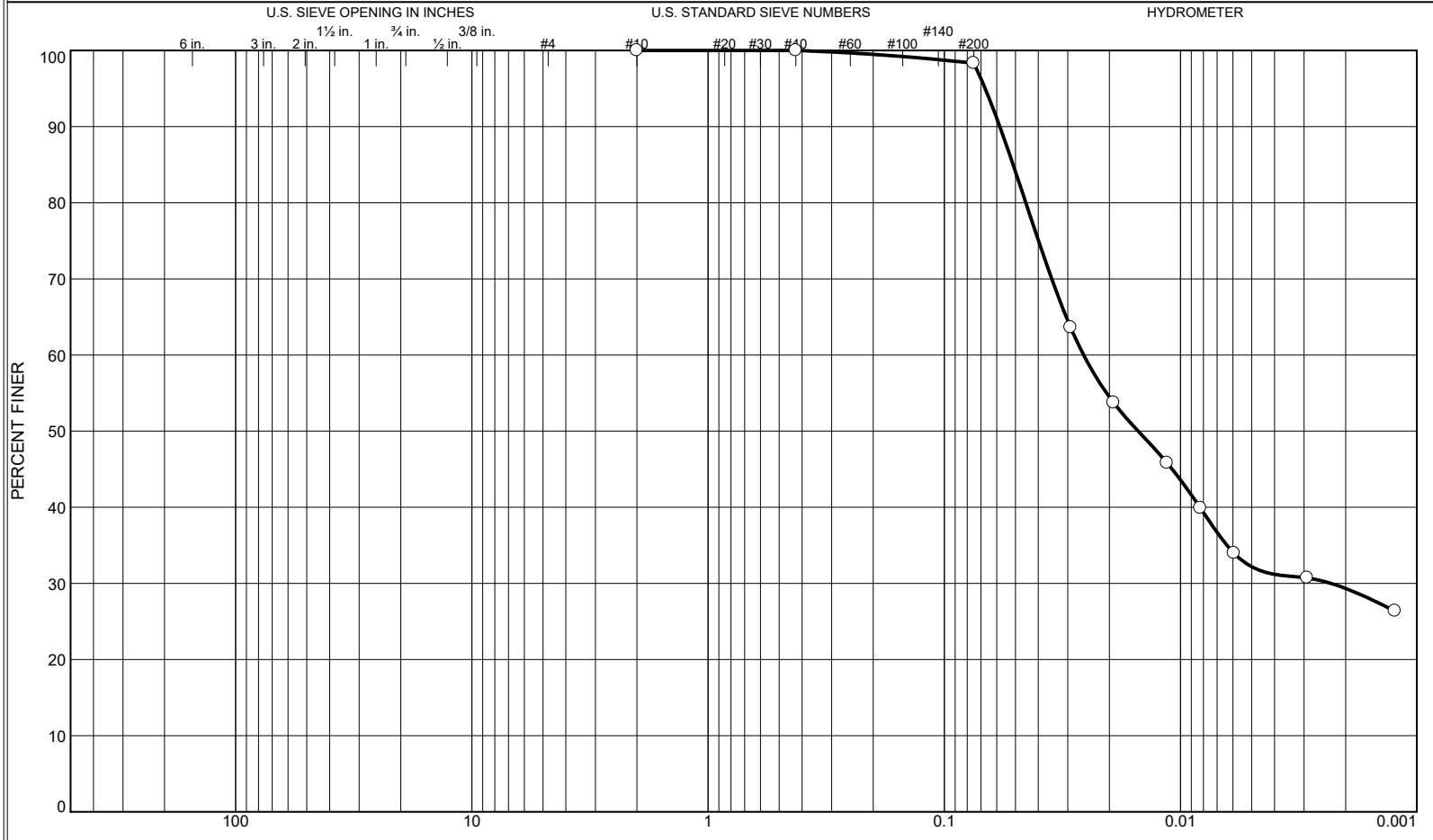


% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	8.8	78.8	12.4

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-7	Depth: 4-6	Sample Number: 3			

Client CPRA		
Project Breton Landbridge Marsh Creation(West)		
Project No. APS2008-G063		

# Particle Size Distribution Report

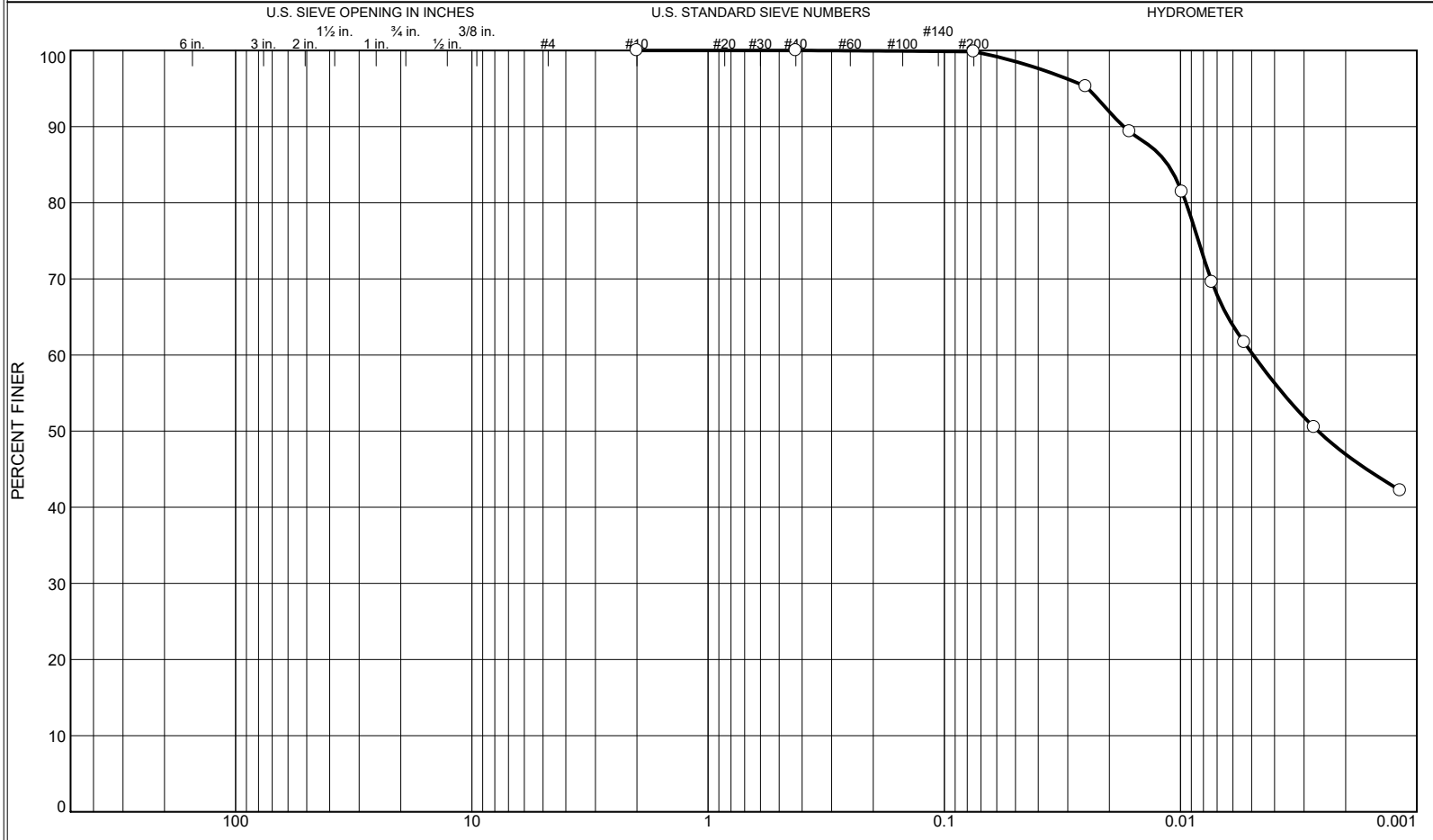


% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	1.7	66.1	32.2

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-7	Depth: 6-8	Sample Number: 4			

Client CPRA		
Project Breton Landbridge Marsh Creation(West)		
Project No. APS2008-G063		

# Particle Size Distribution Report

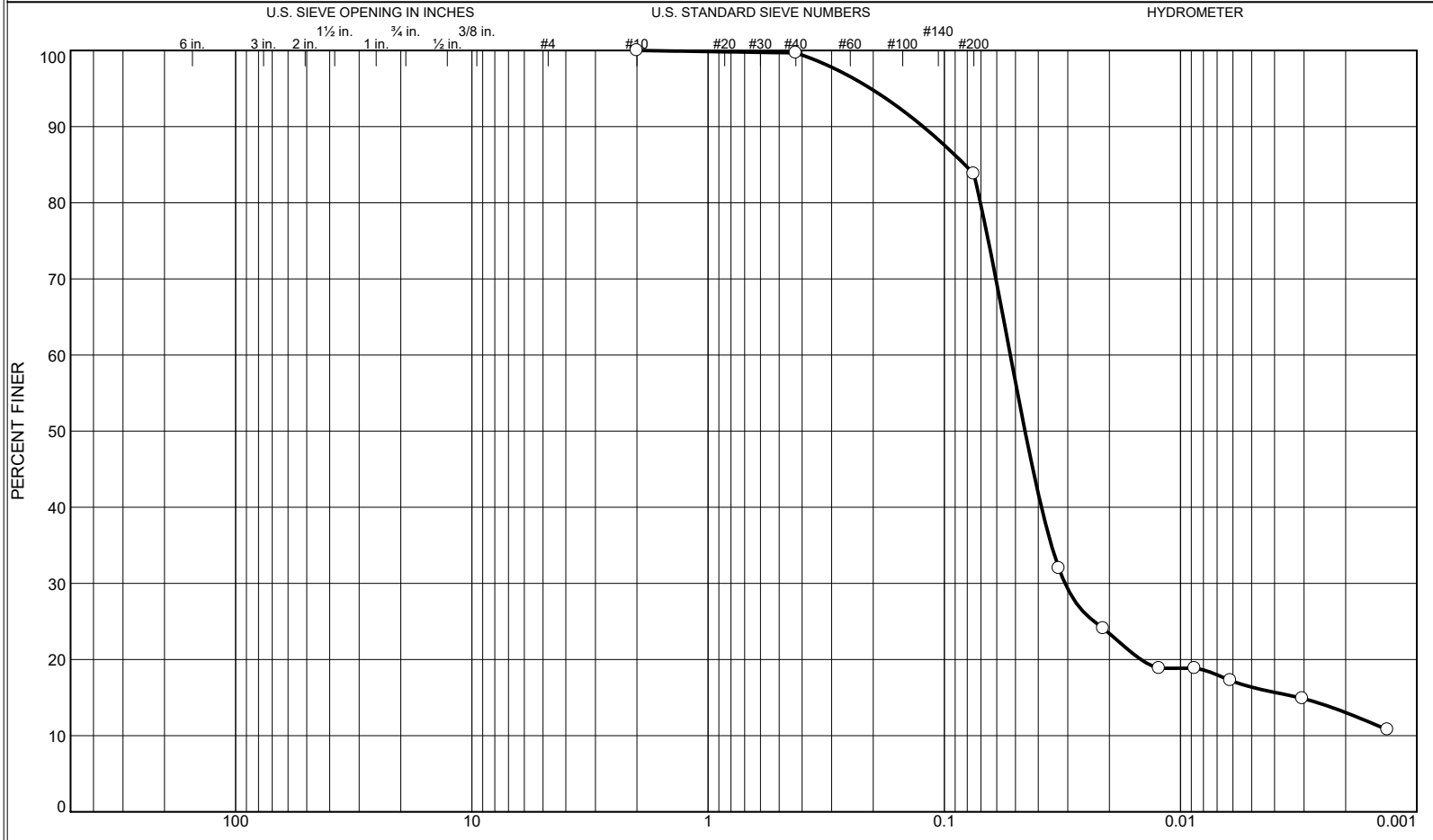


% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	0.2	39.5	60.3

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-7	Depth: 8-10	Sample Number: 5			

Client CPRA		
Project Breton Landbridge Marsh Creation(West)		
Project No. APS2008-G063		

# Particle Size Distribution Report

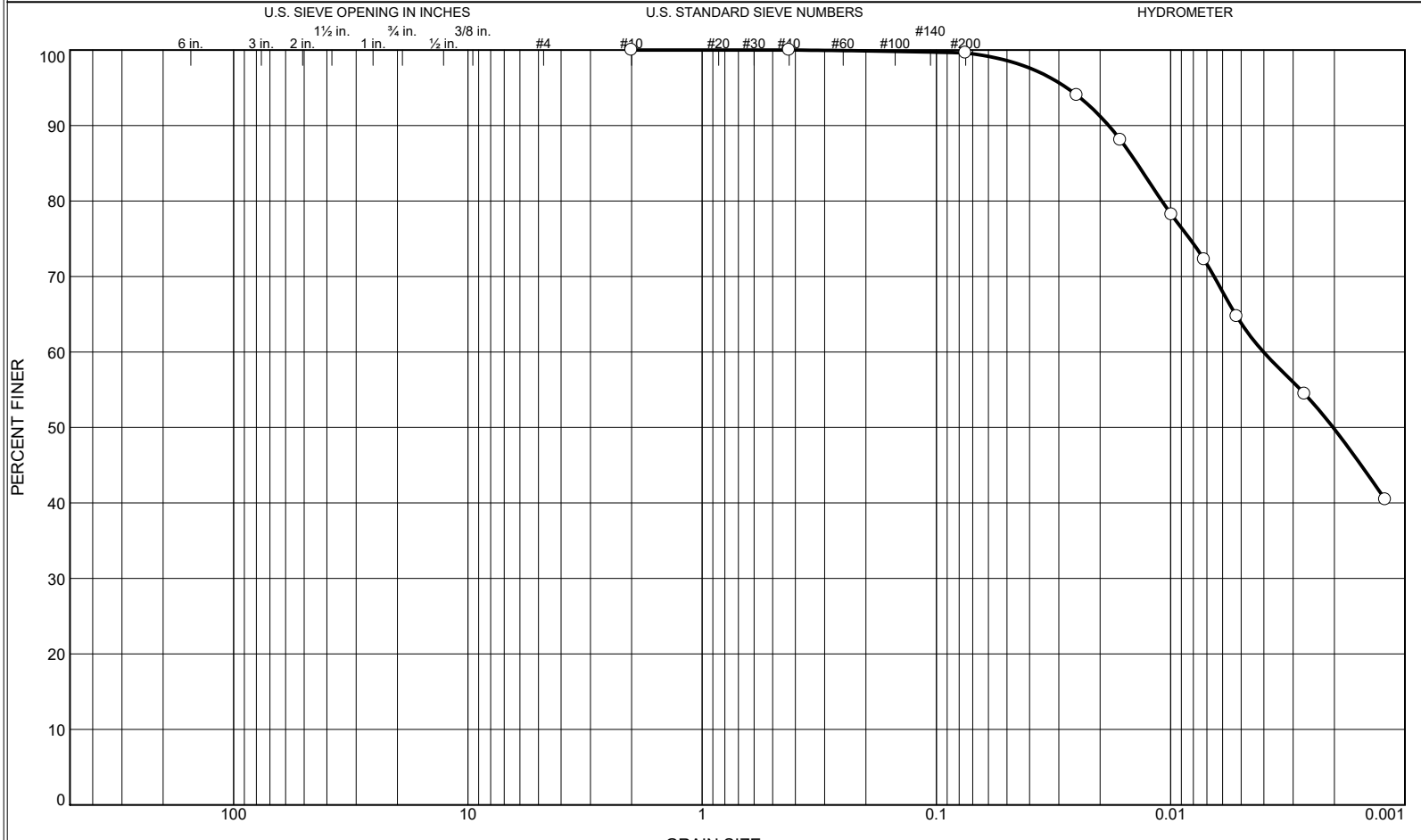


% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.3	15.9	67.4	16.4

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-7	Depth: 12-14	Sample Number: 7			

Client CPRA		
Project Breton Landbridge Marsh Creation(West)		
Project No. APS2008-G063		

# Particle Size Distribution Report



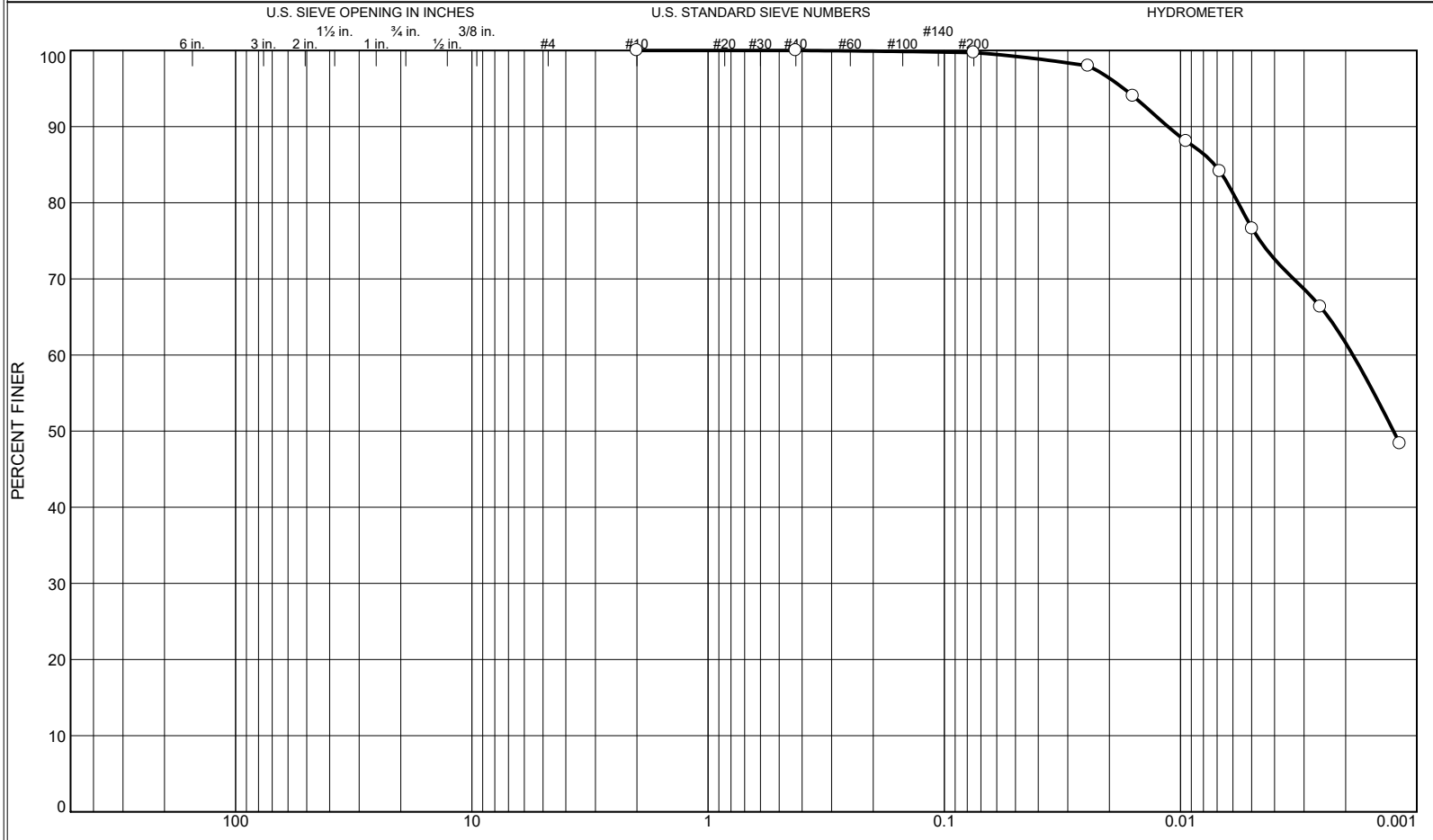
% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	0.4	35.8	63.8

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-7	Depth: 14-16	Sample Number: 8			

Client CPRA		
Project Breton Landbridge Marsh Creation(West)		
Project No. APS2008-G063		



# Particle Size Distribution Report

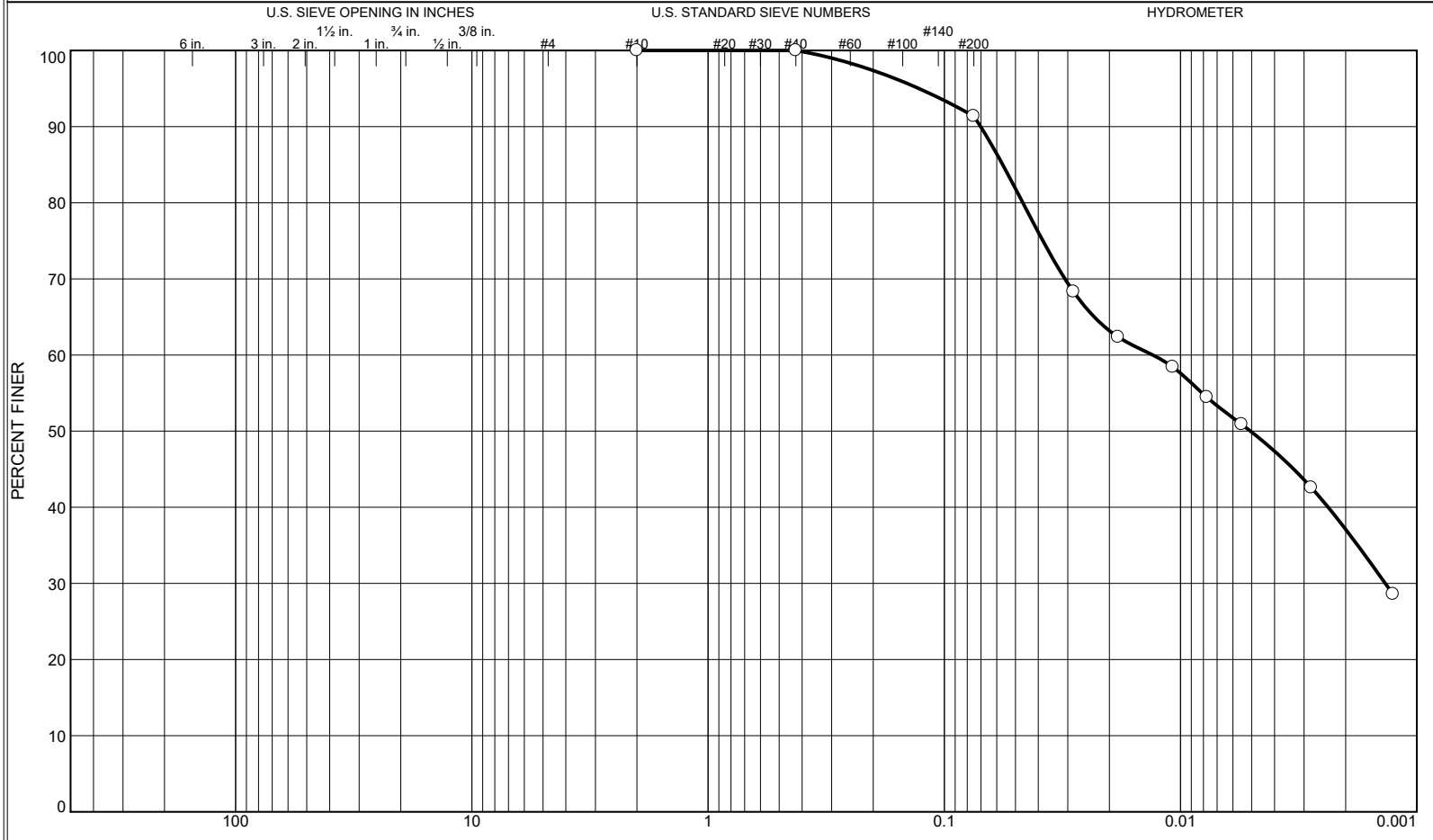


% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	0.3	23.0	76.7

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-7	Depth: 16-18	Sample Number: 9			

Client CPRA		
Project Breton Landbridge Marsh Creation(West)		
Project No. APS2008-G063		

# Particle Size Distribution Report

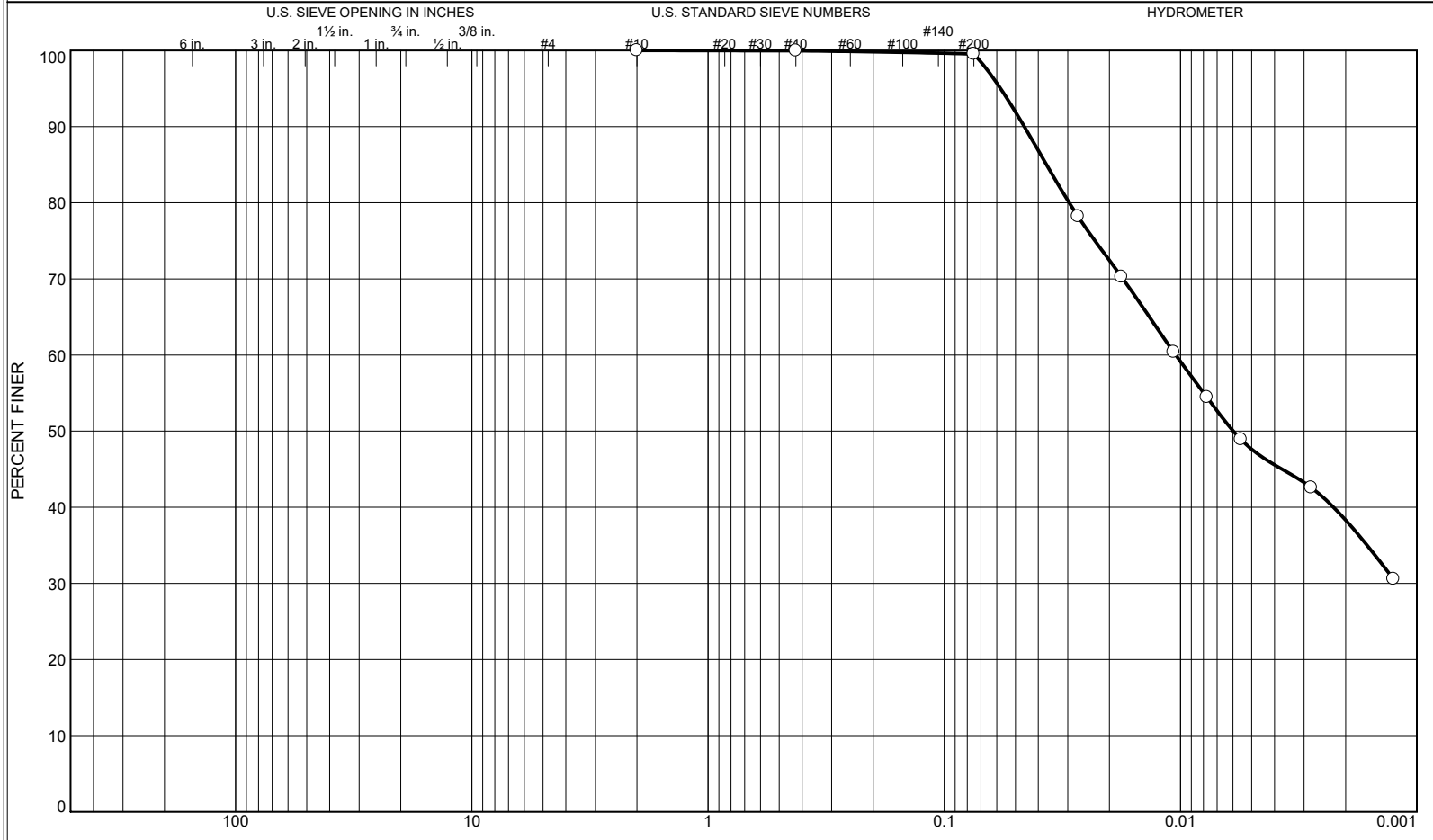


% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	8.6	41.5	49.9

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-7	Depth: 18-20	Sample Number: 10			

Client CPRA		
Project Breton Landbridge Marsh Creation(West)		
Project No. APS2008-G063		

# Particle Size Distribution Report

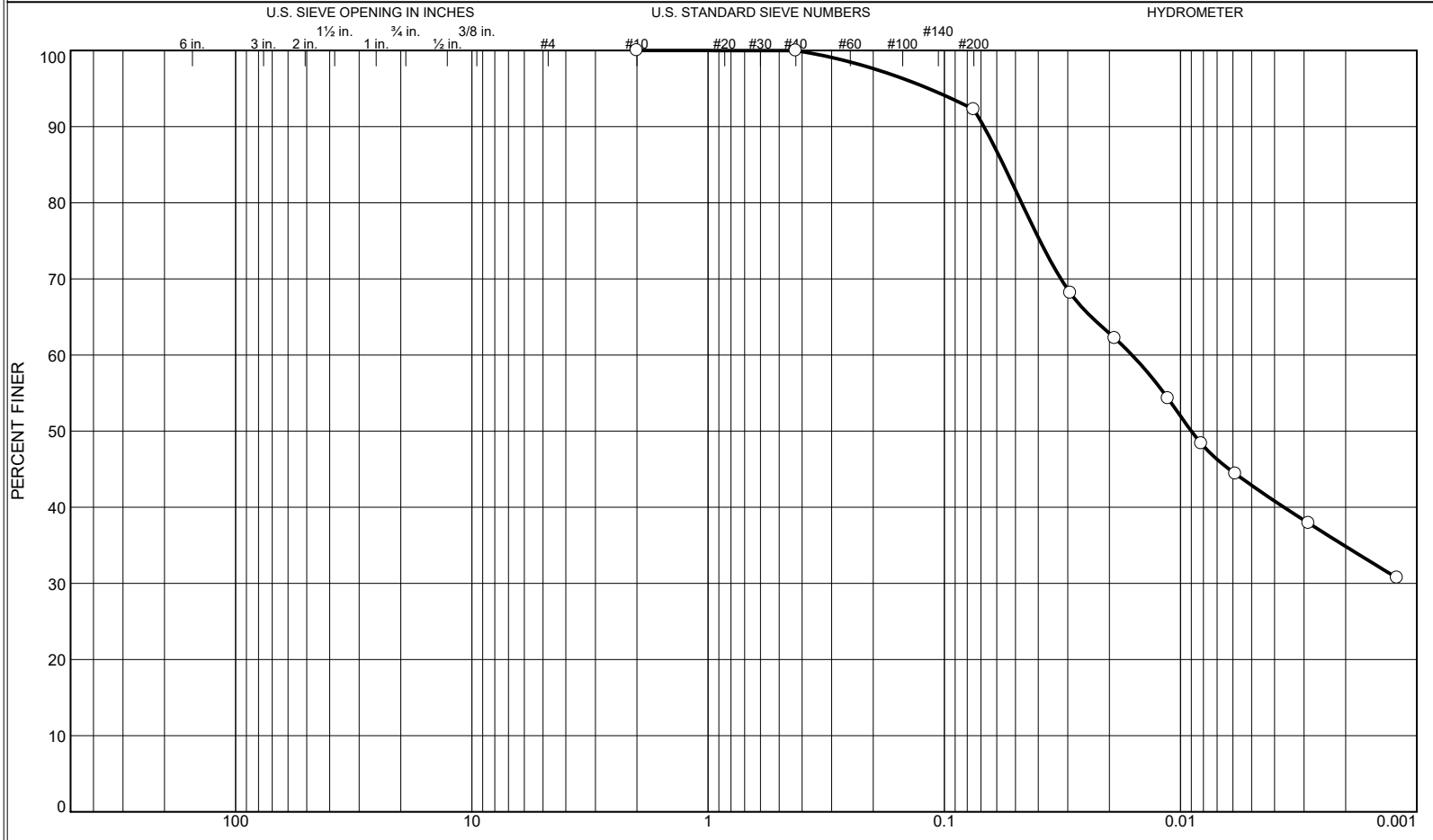


% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	0.5	51.9	47.6

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-7	Depth: 23-25	Sample Number: 11			


Client CPRA	
Project Breton Landbridge Marsh Creation(West)	
Project No. APS2008-G063	

# Particle Size Distribution Report

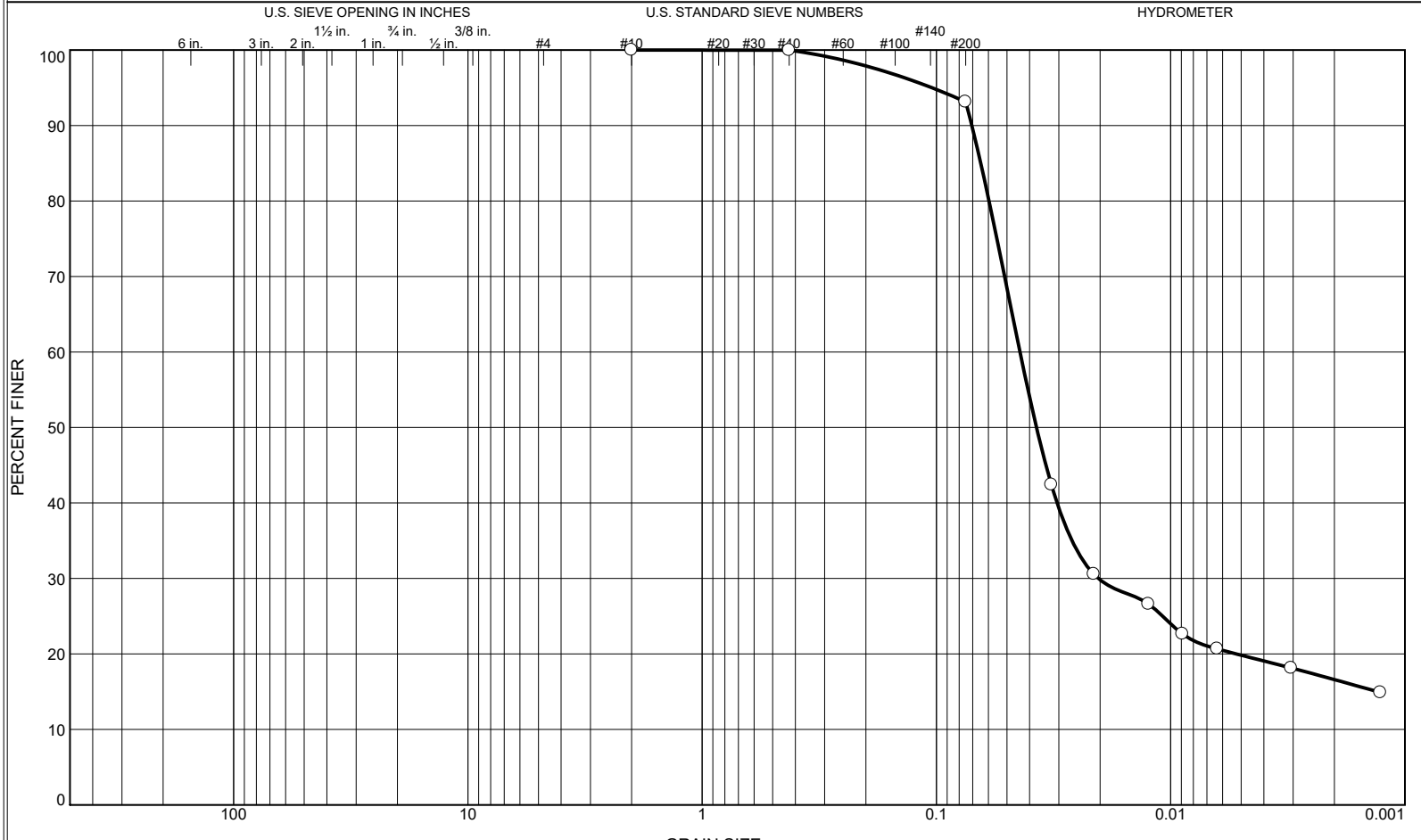


% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	7.7	49.4	42.9

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-8	Depth: 0-2	Sample Number: 1			

Client CPRA		
Project Breton Landbridge Marsh Creation(West)		
Project No. APS2008-G063		

# Particle Size Distribution Report

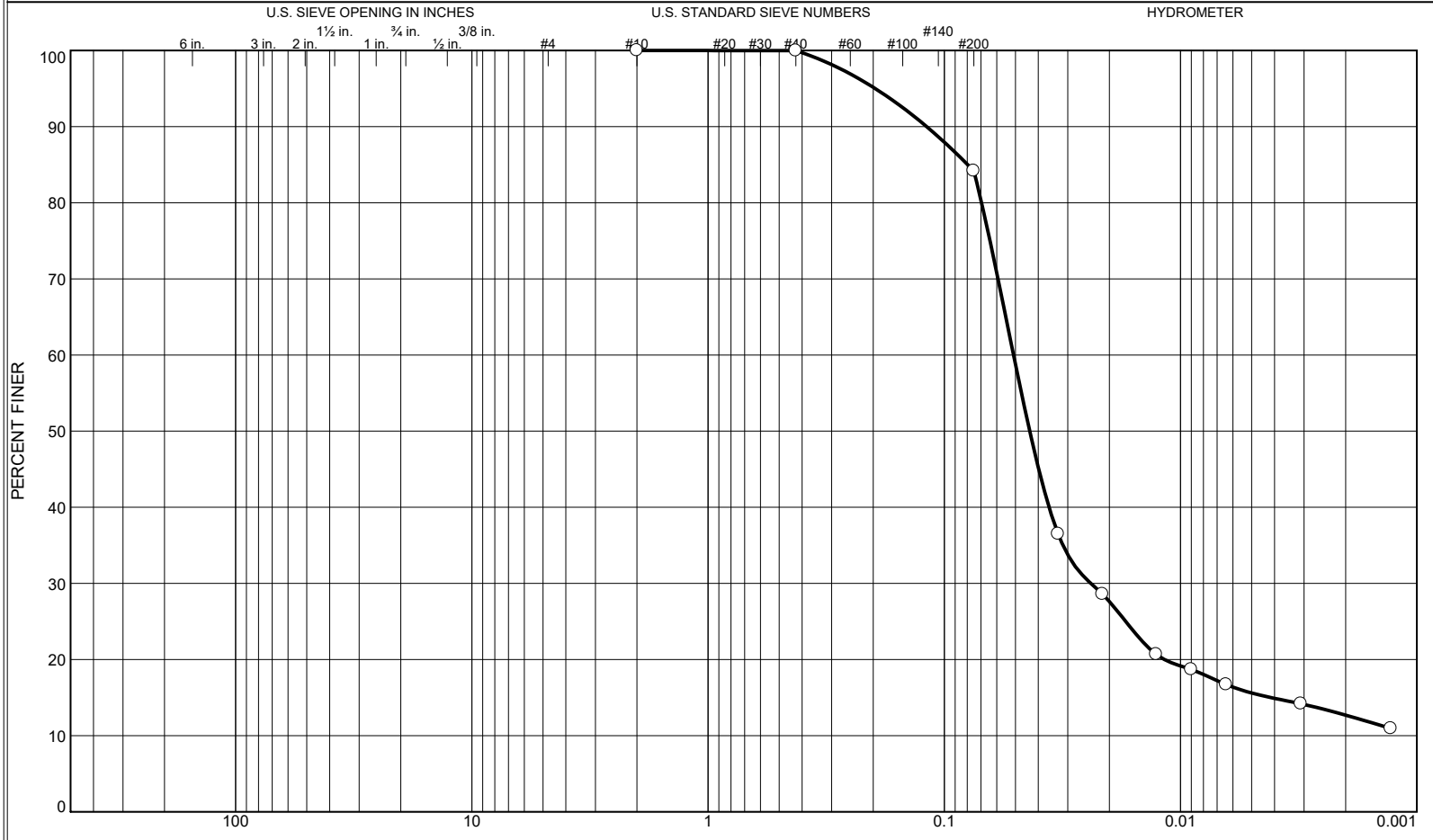


% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	6.9	73.3	19.8

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-8	Depth: 2-4	Sample Number: 2			

Client CPRA	
Project Breton Landbridge Marsh Creation(West)	
Project No. APS2008-G063	

# Particle Size Distribution Report

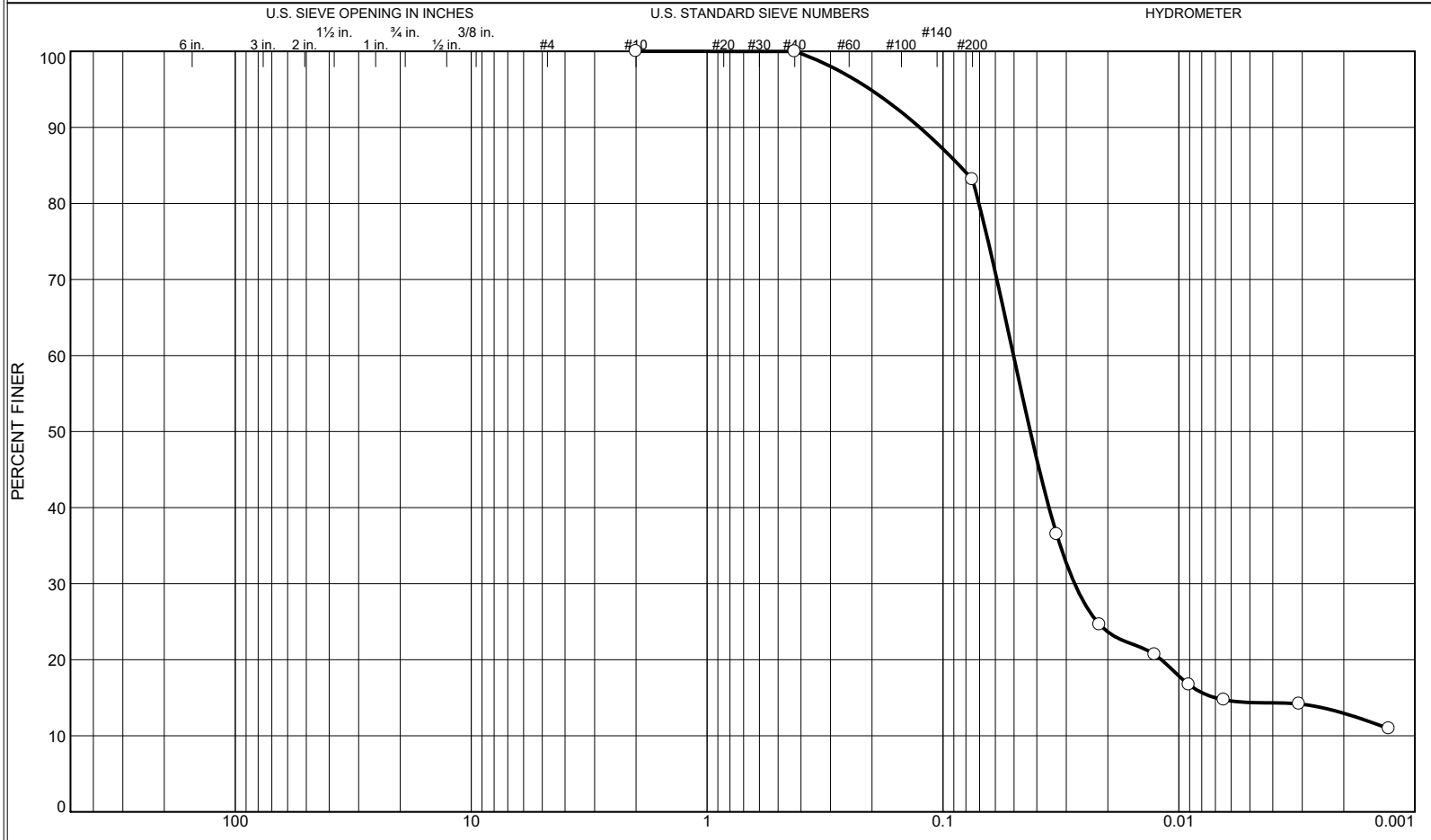


% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	15.8	68.6	15.6

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-8	Depth: 4-6	Sample Number: 3			

Client CPRA	
Project Breton Landbridge Marsh Creation(West)	
Project No. APS2008-G063	

# Particle Size Distribution Report

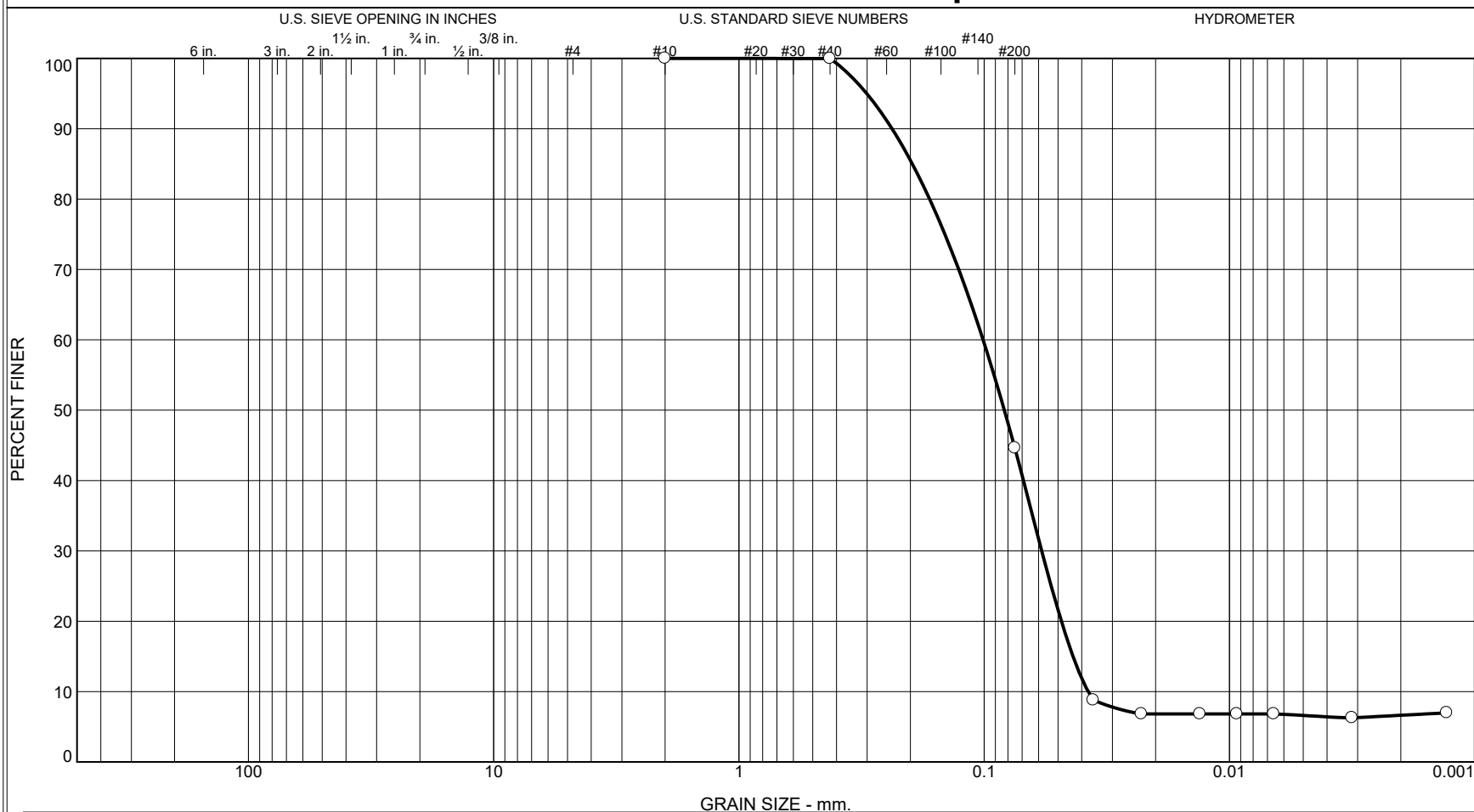


% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	16.9	68.7	14.4

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-8	Depth: 6-8	Sample Number: 4			

Client CPRA		
Project Breton Landbridge Marsh Creation(West)		
Project No. APS2008-G063		

# Particle Size Distribution Report



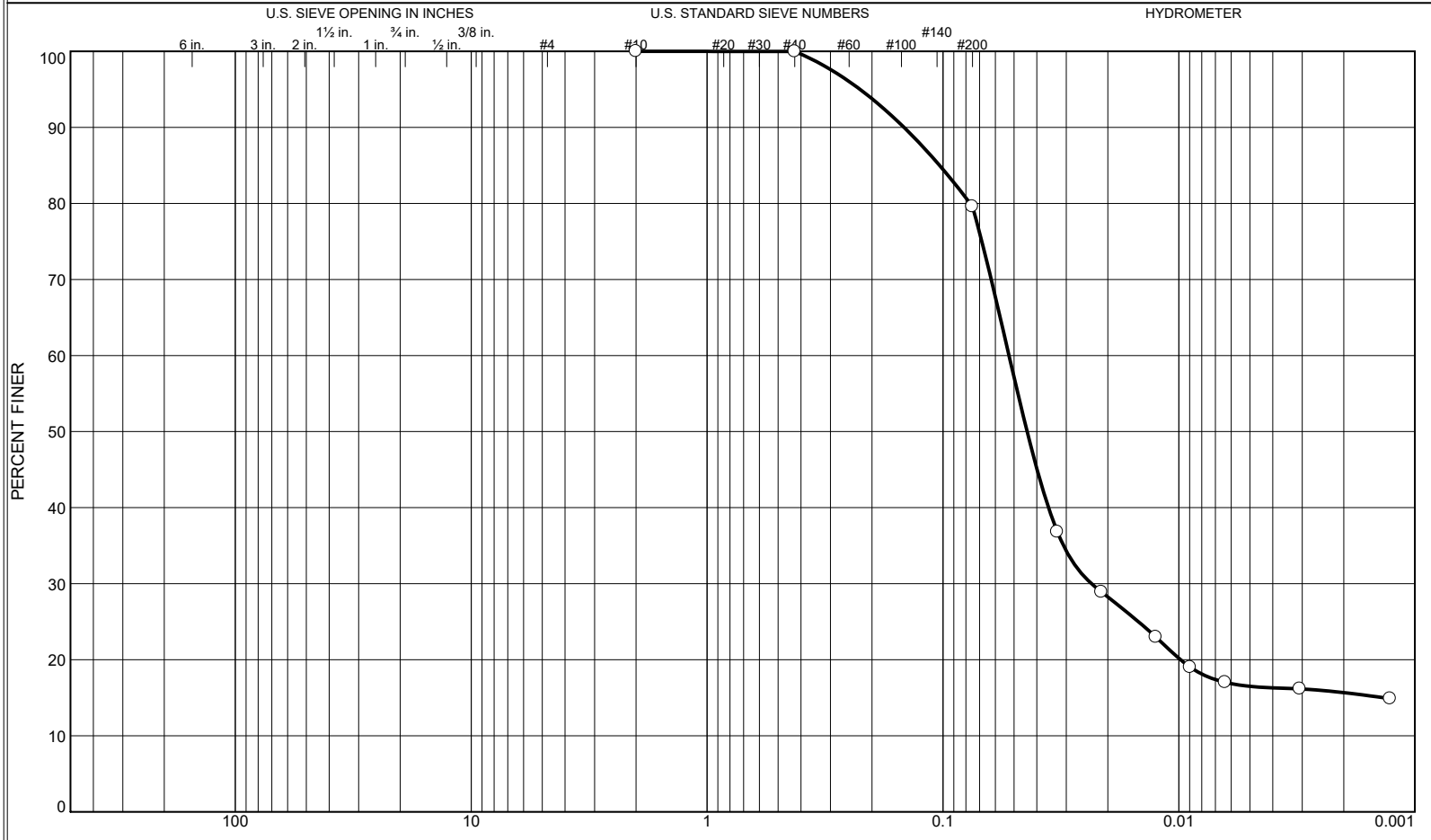
% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	55.4	38.0	6.6

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-8	Depth: 8-10	Sample Number: 5			

Client		
Project		
Project No.		Figure



# Particle Size Distribution Report

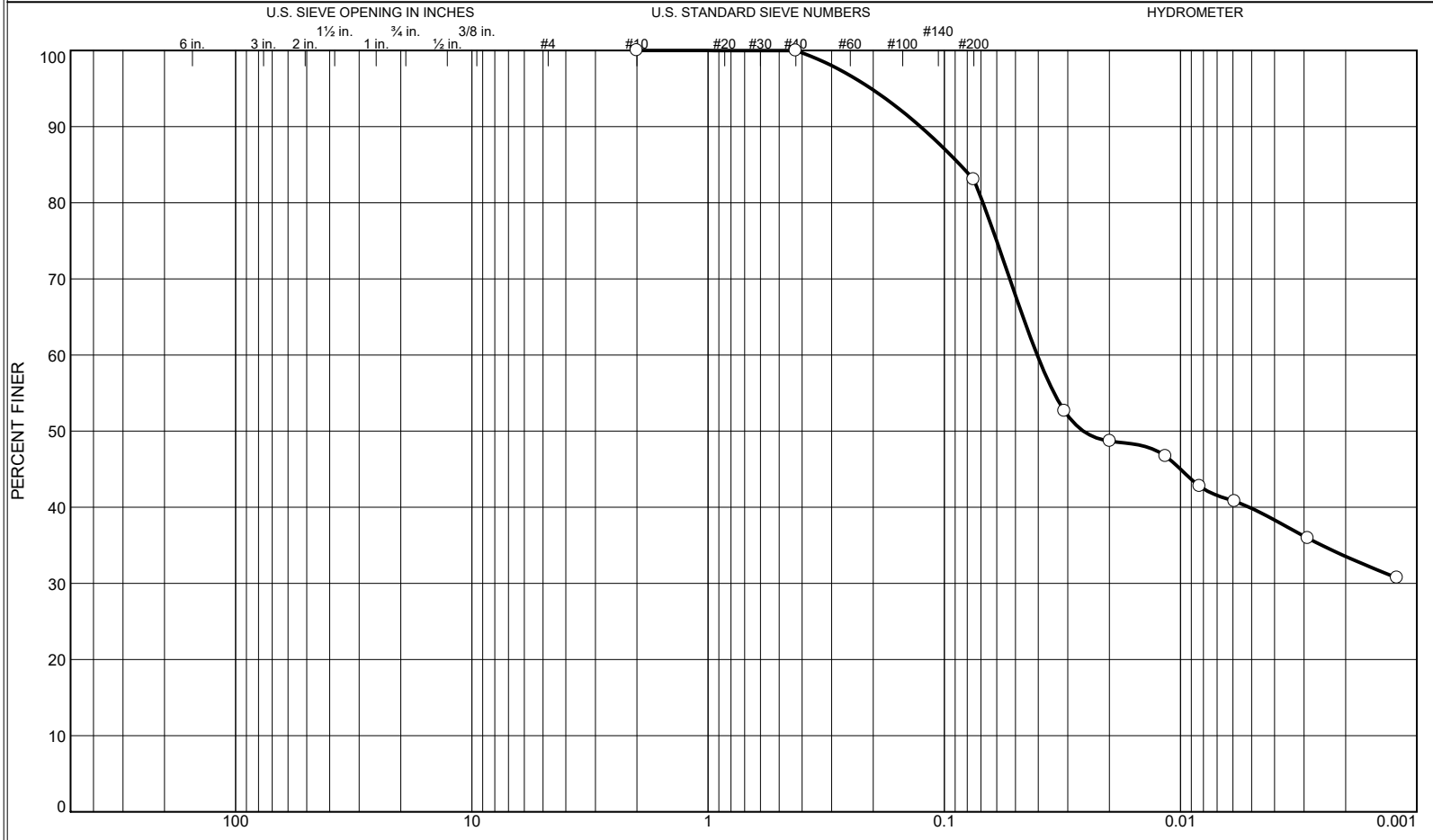


% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	20.4	63.1	16.5

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-8	Depth: 10-12	Sample Number: 6			

Client CPRA		
Project Breton Landbridge Marsh Creation(West)		
Project No. APS2008-G063		

# Particle Size Distribution Report

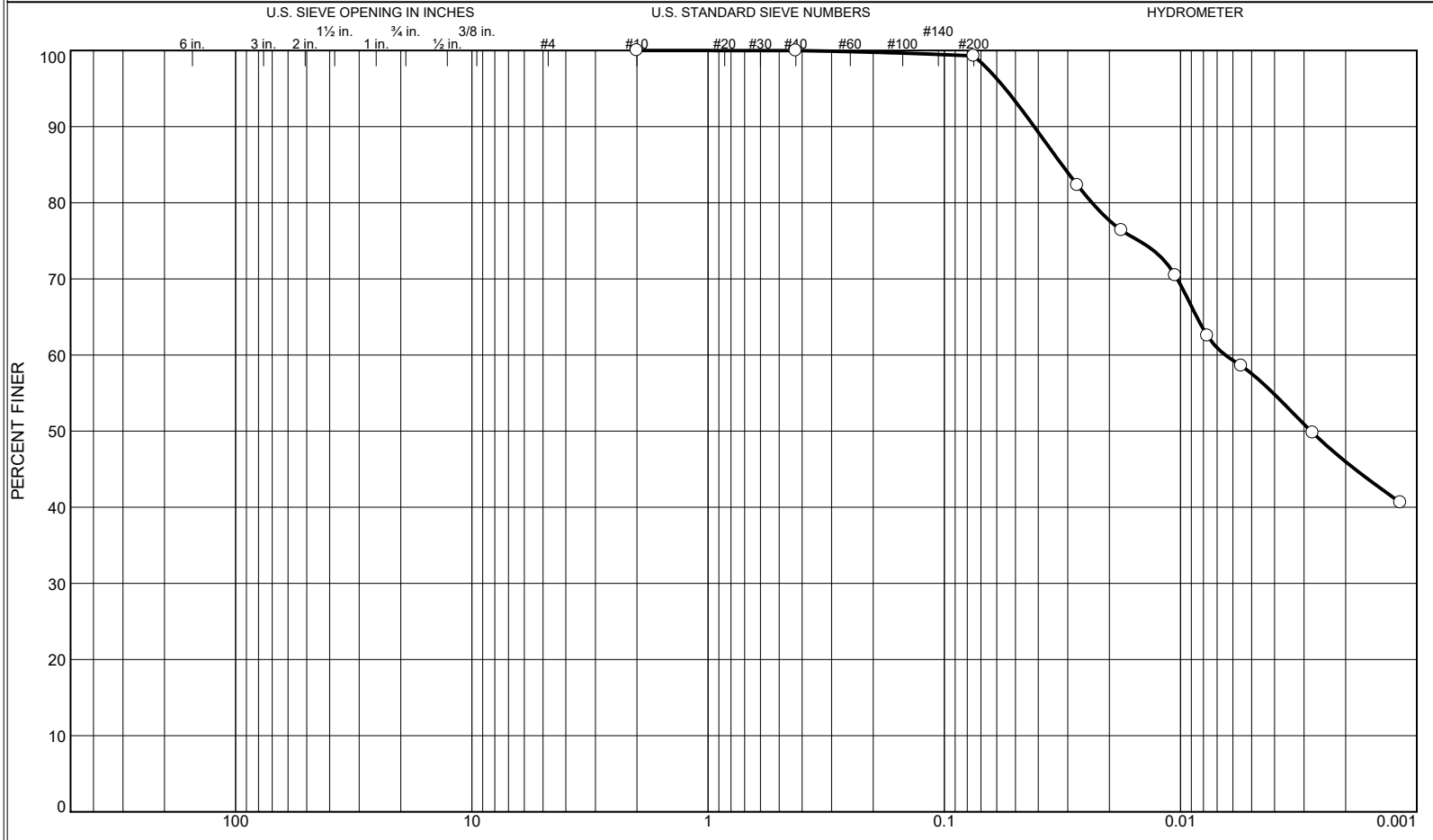


% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	17.0	43.1	39.9

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-8	Depth: 12-14	Sample Number: 7			

Client CPRA	
Project Breton Landbridge Marsh Creation(West)	
Project No. APS2008-G063	

# Particle Size Distribution Report

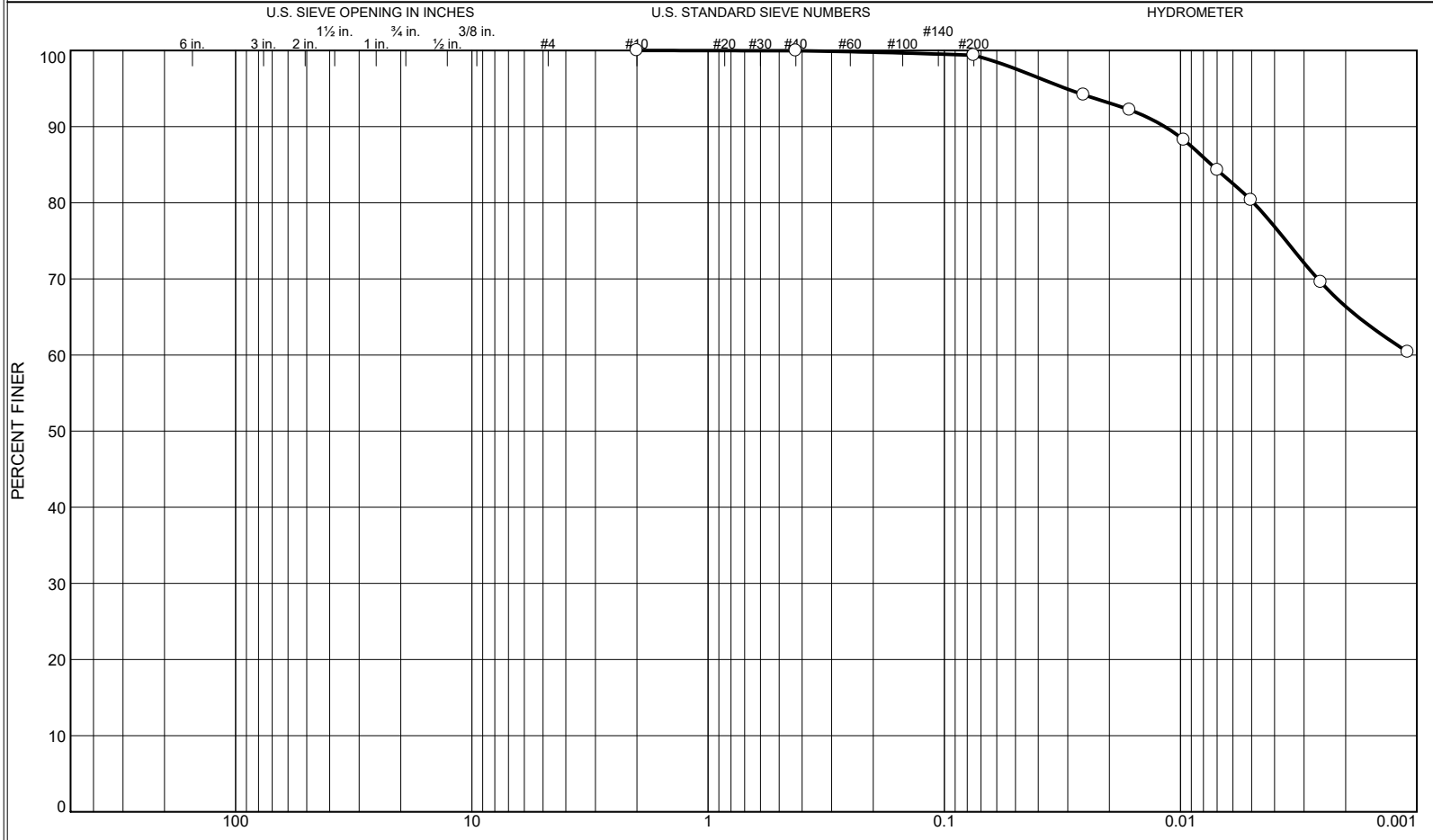


% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	0.7	41.7	57.6

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-8	Depth: 14-16	Sample Number: 8			


Client CPRA	
Project Breton Landbridge Marsh Creation(West)	
Project No. APS2008-G063	

# Particle Size Distribution Report

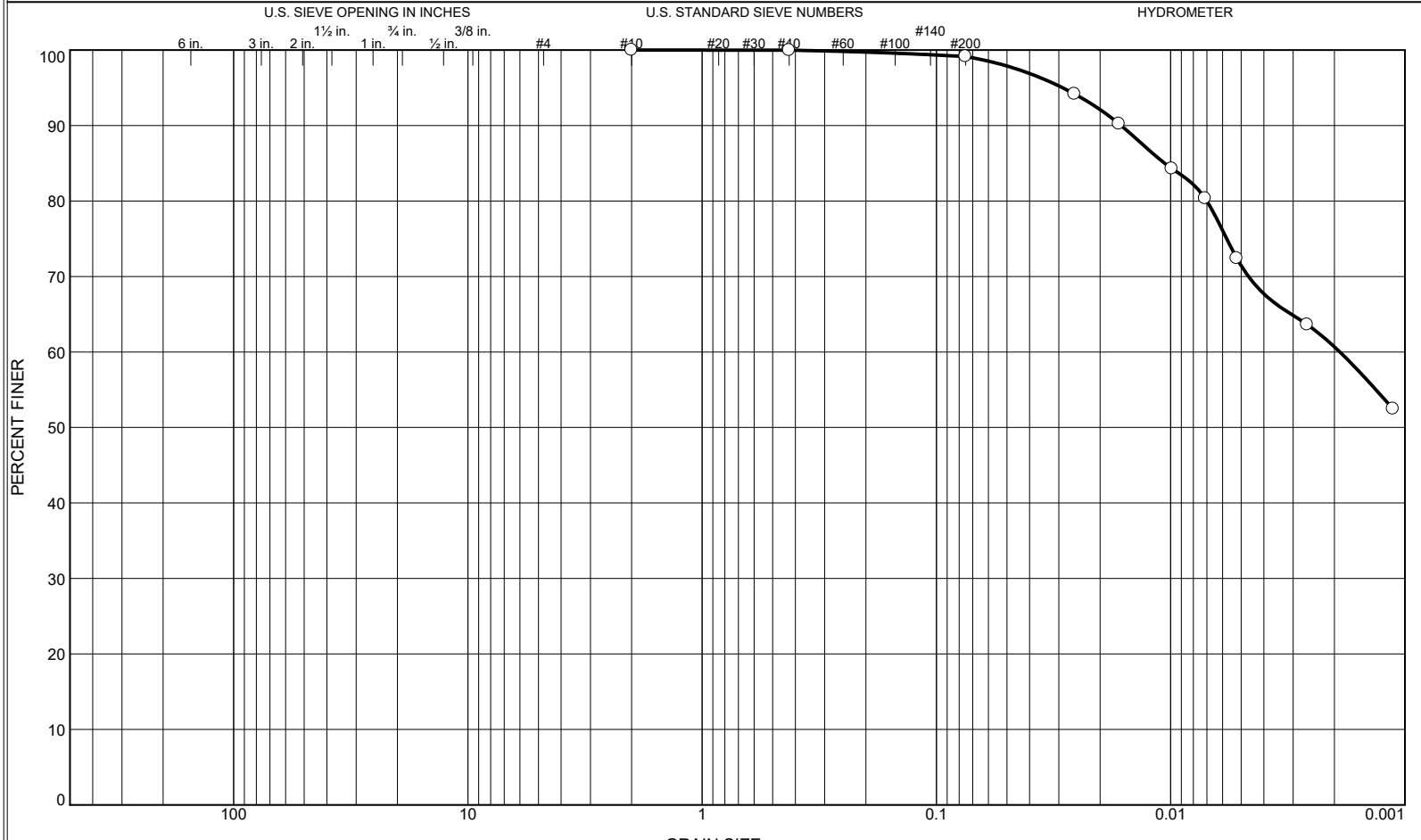


% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	0.6	19.2	80.2

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-8	Depth: 16-18	Sample Number: 9			

Client CPRA		
Project Breton Landbridge Marsh Creation(West)		
Project No. APS2008-G063		

# Particle Size Distribution Report



% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	0.9	27.7	71.4

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-8	Depth: 18-20	Sample Number: 10			

Client CPRA		
Project Breton Landbridge Marsh Creation(West)		
Project No. APS2008-G063		

# Particle Size Distribution Report

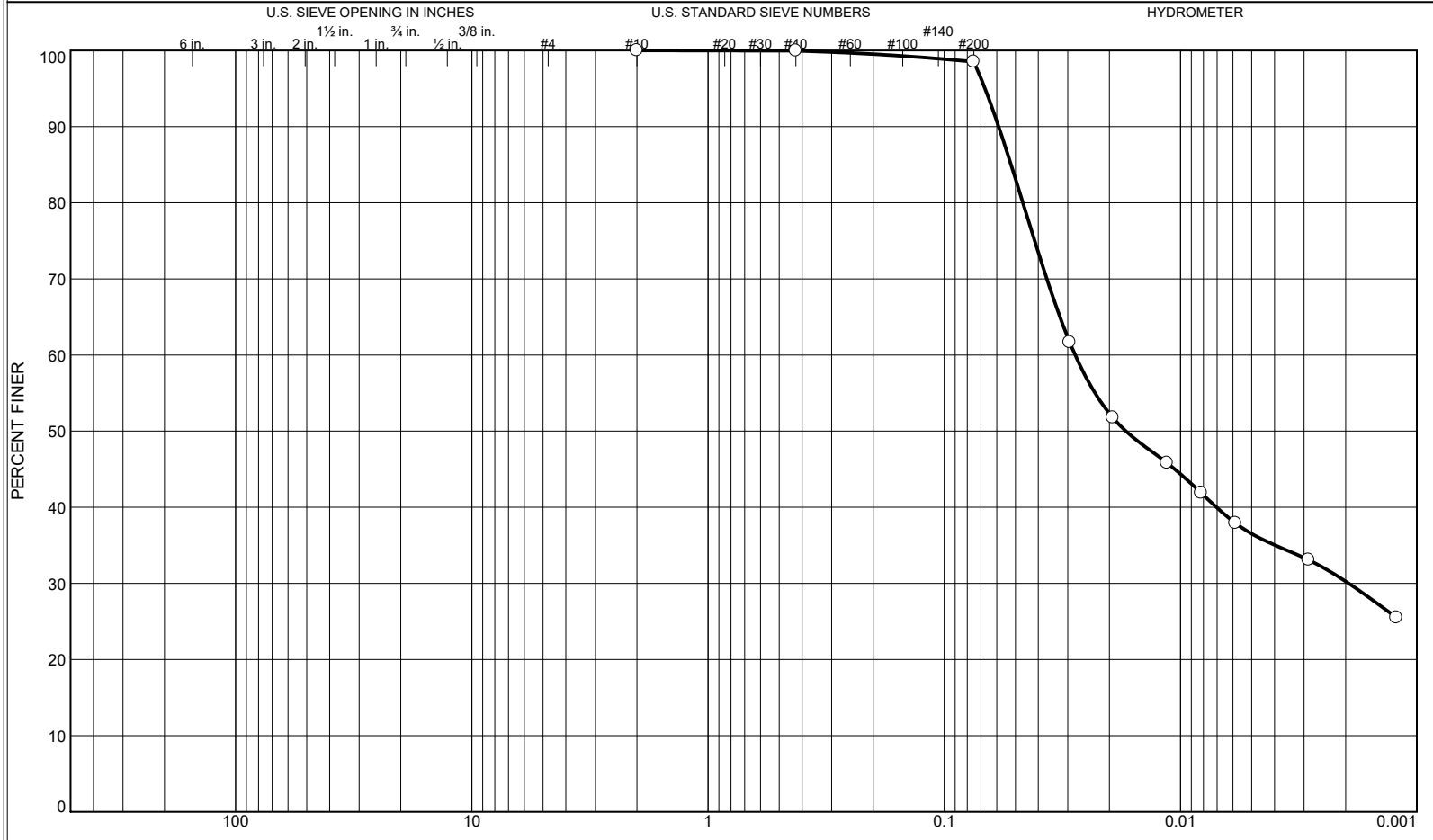


% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	1.9	26.7	71.4

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-8	Depth: 23-25	Sample Number: 11			

Client CPRA		
Project Breton Landbridge Marsh Creation(West)		
Project No. APS2008-G063		

# Particle Size Distribution Report

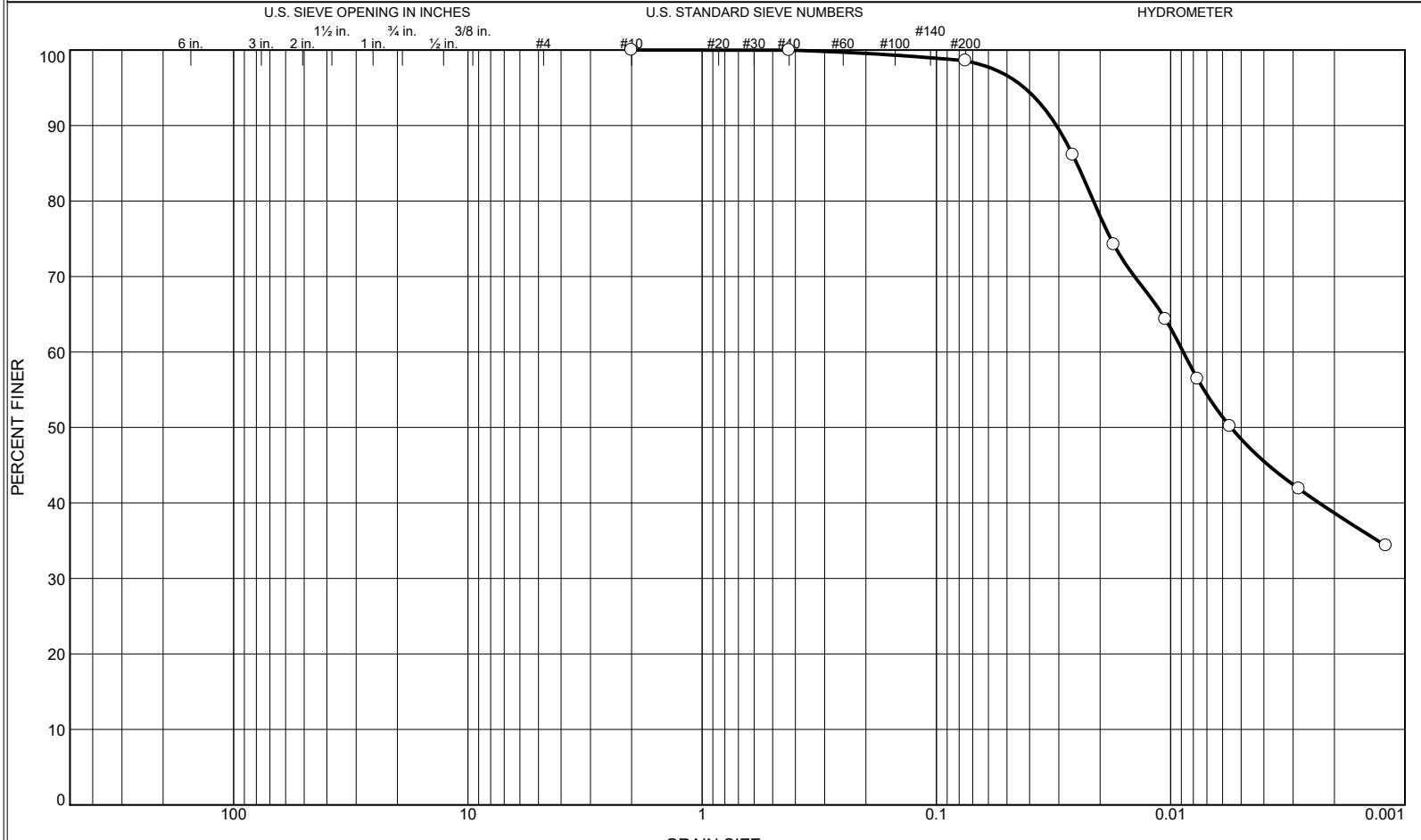


% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	1.5	62.0	36.5

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-9	Depth: 0-2	Sample Number: 1			

Client CPRA		
Project Breton Landbridge Marsh Creation(West)		
Project No. APS2008-G063		

# Particle Size Distribution Report



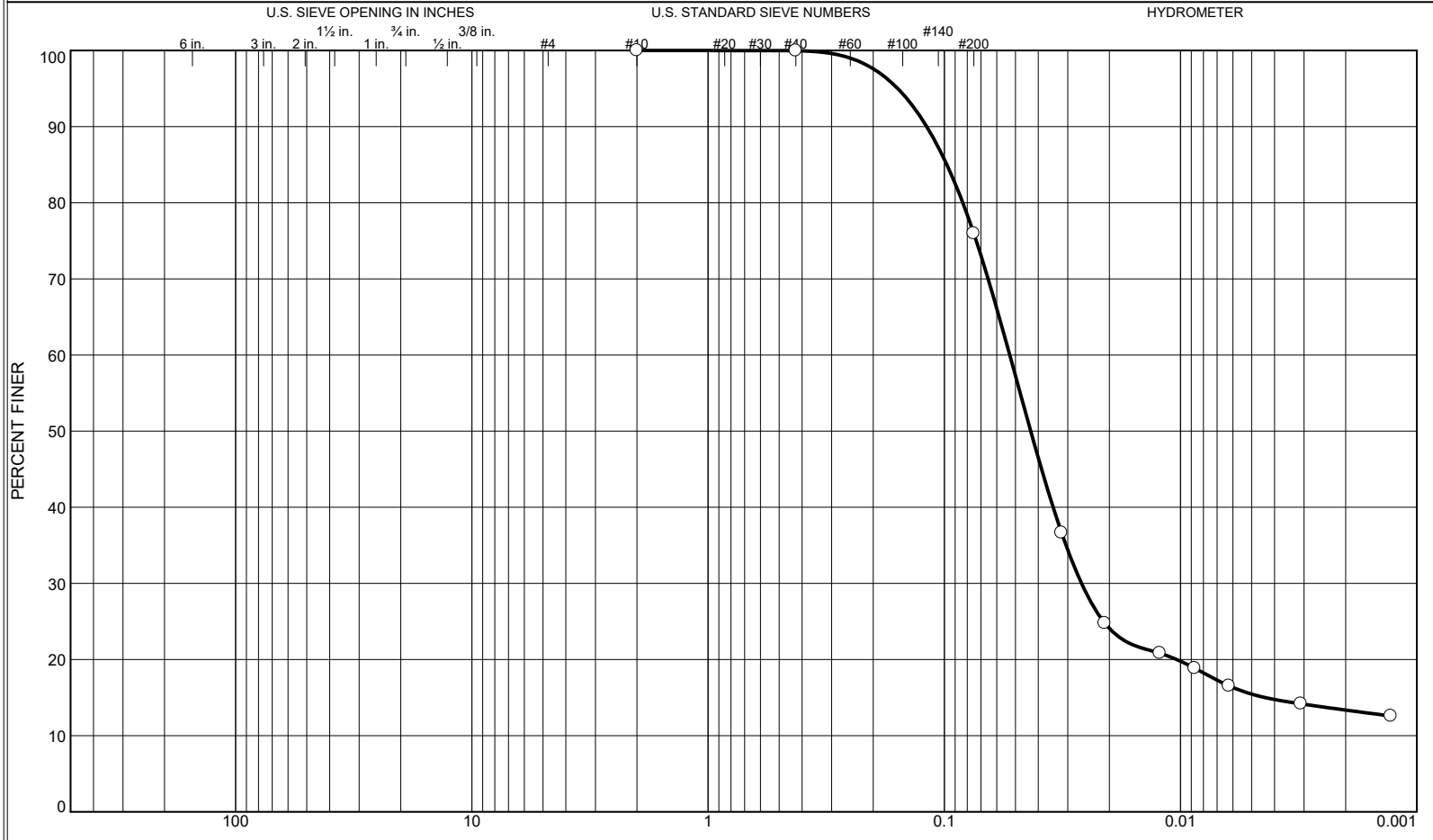
% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	1.4	50.1	48.5

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-9	Depth: 2-4	Sample Number: 2			

Client CPRA	
Project Breton Landbridge Marsh Creation(West)	
Project No. APS2008-G063	



# Particle Size Distribution Report

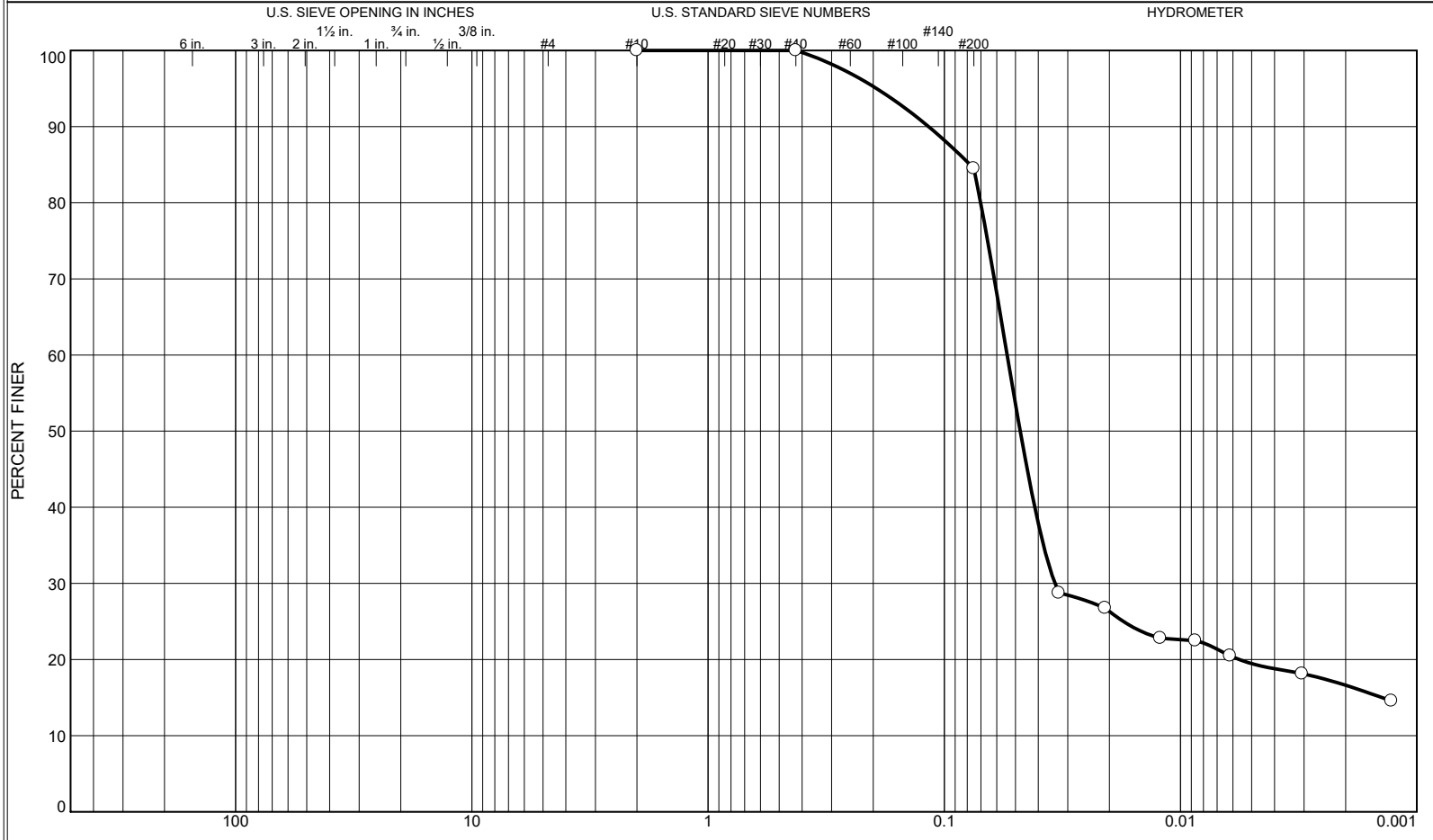


% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	24.0	60.5	15.5

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-9	Depth: 4-6	Sample Number: 3			

Client CPRA	 <b>APS</b> Engineering and Testing	
Project Breton Landbridge Marsh Creation(West)		
Project No. APS2008-G063		

# Particle Size Distribution Report

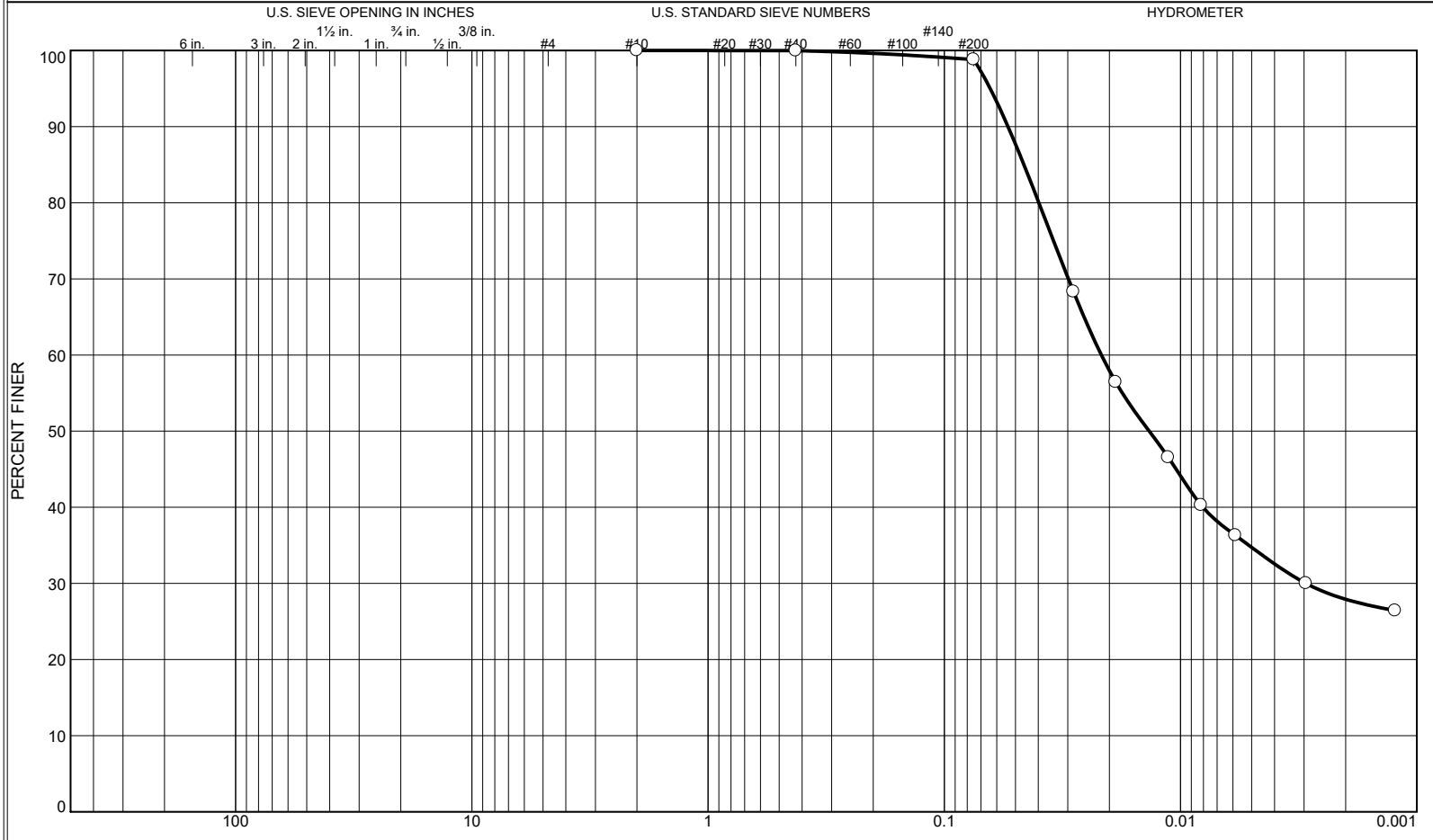


% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	15.5	65.0	19.5

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-9	Depth: 6-8	Sample Number: 4			

Client CPRA		
Project Breton Landbridge Marsh Creation(West)		
Project No. APS2008-G063		

# Particle Size Distribution Report

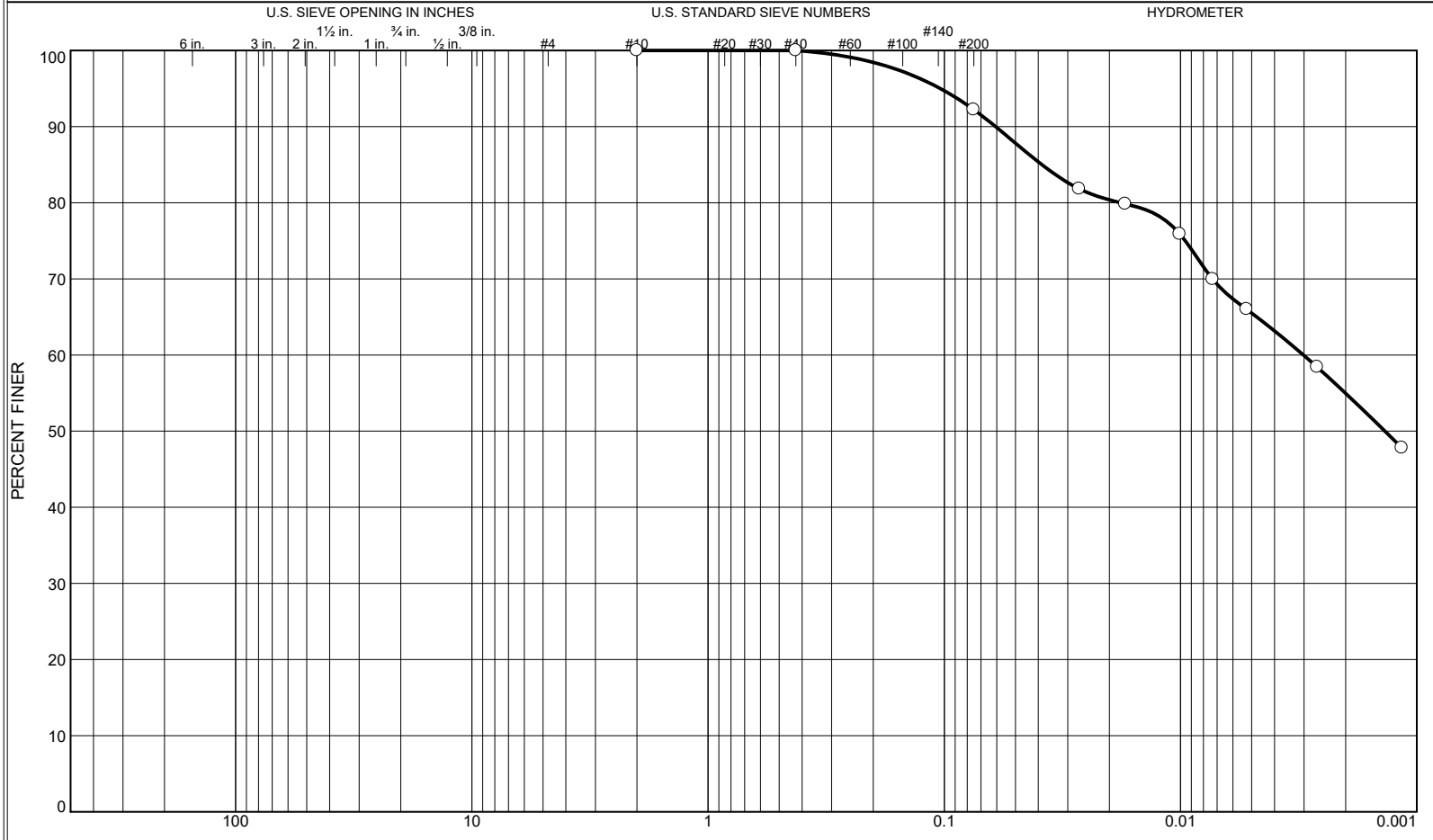


% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	1.2	64.1	34.7

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-9	Depth: 8-10	Sample Number: 5			


Client CPRA		
Project Breton Landbridge Marsh Creation(West)		
Project No. APS2008-G063		

# Particle Size Distribution Report

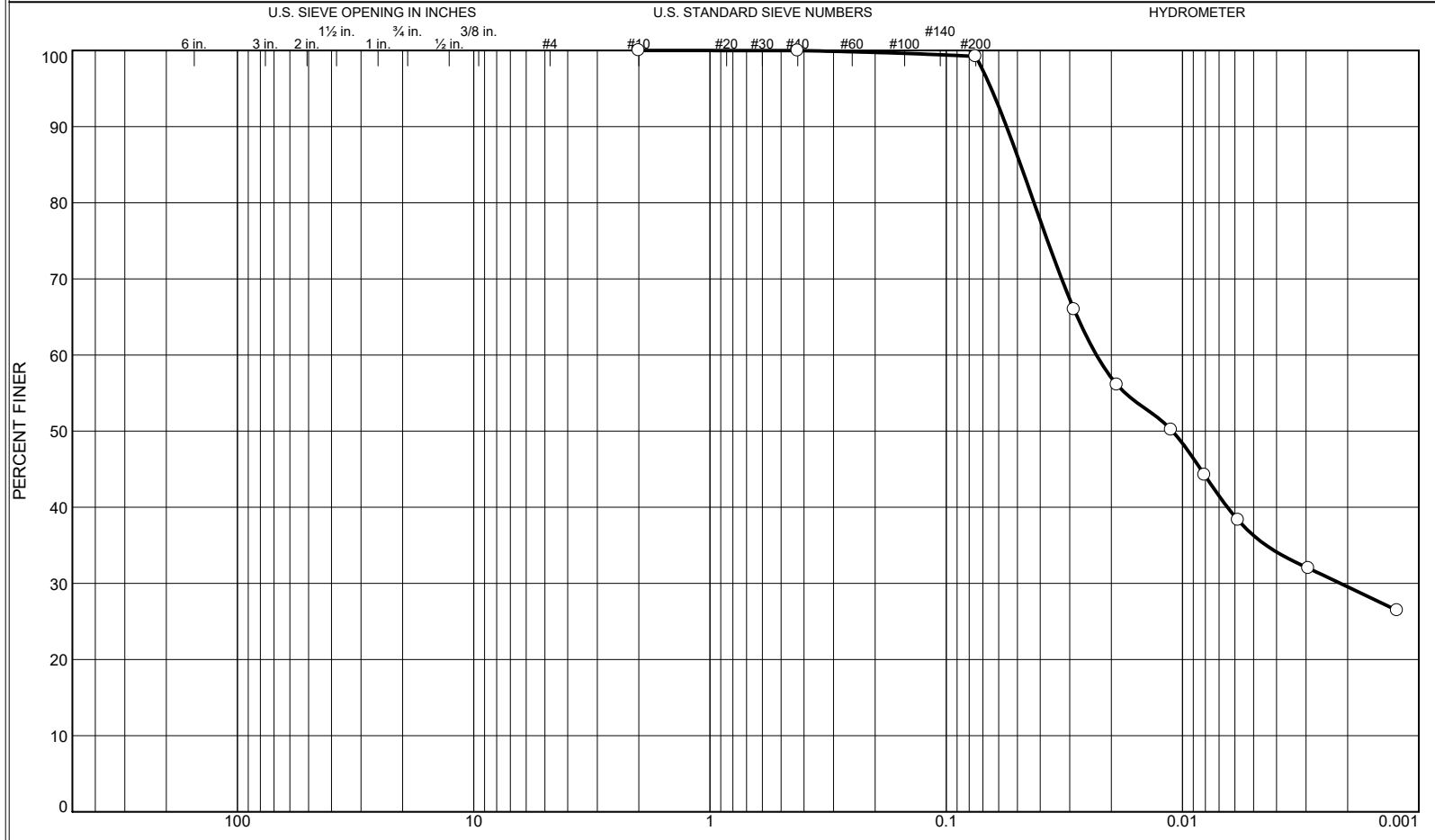


% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	7.8	26.7	65.5

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-9	Depth: 10-12	Sample Number: 6			


Client CPRA		
Project Breton Landbridge Marsh Creation(West)		
Project No. APS2008-G063		

# Particle Size Distribution Report

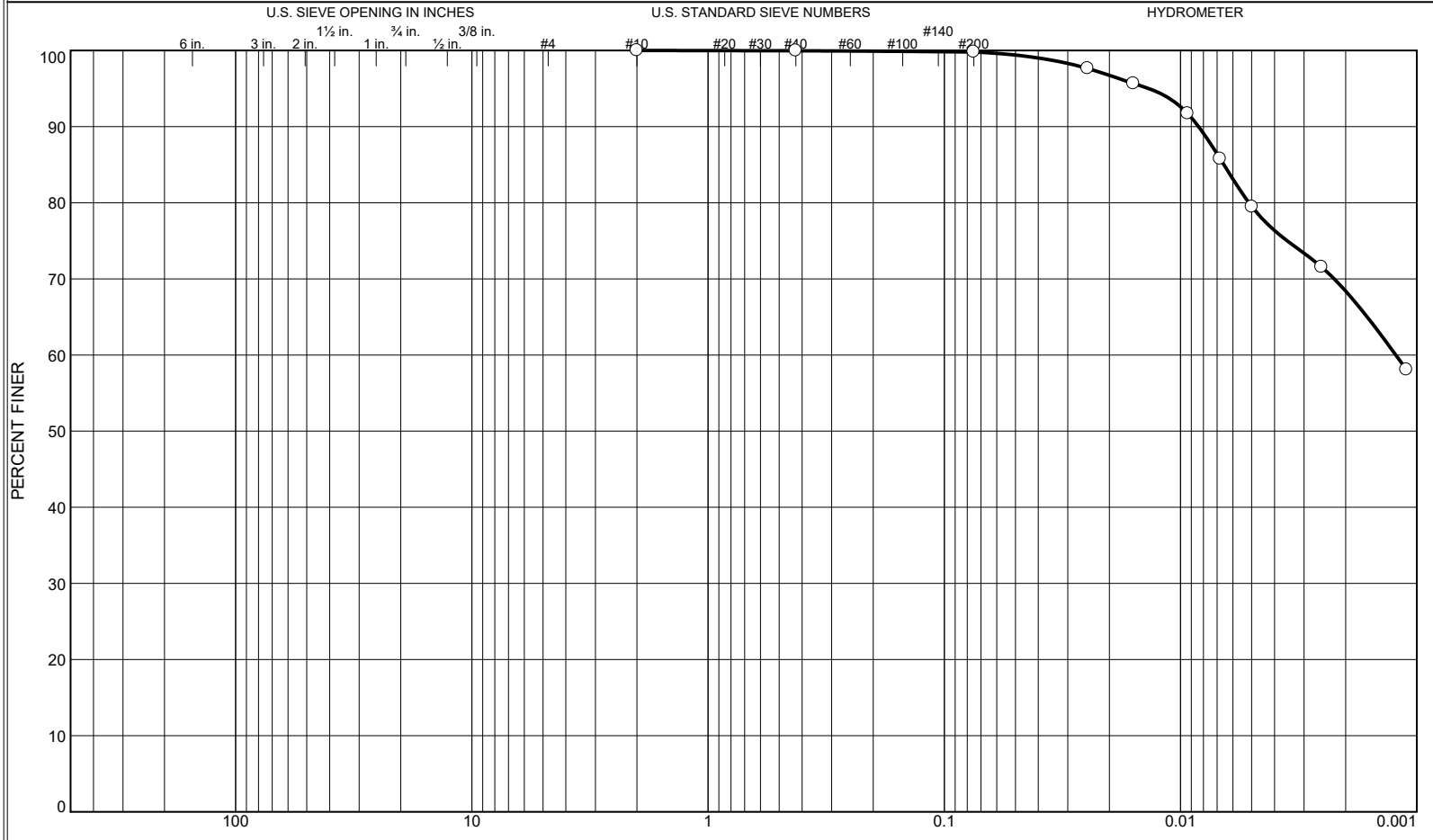


% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	0.8	62.9	36.3

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-9	Depth: 12-14	Sample Number: 7			

Client CPRA		
Project Breton Landbridge Marsh Creation(West)		
Project No. APS2008-G063		

# Particle Size Distribution Report

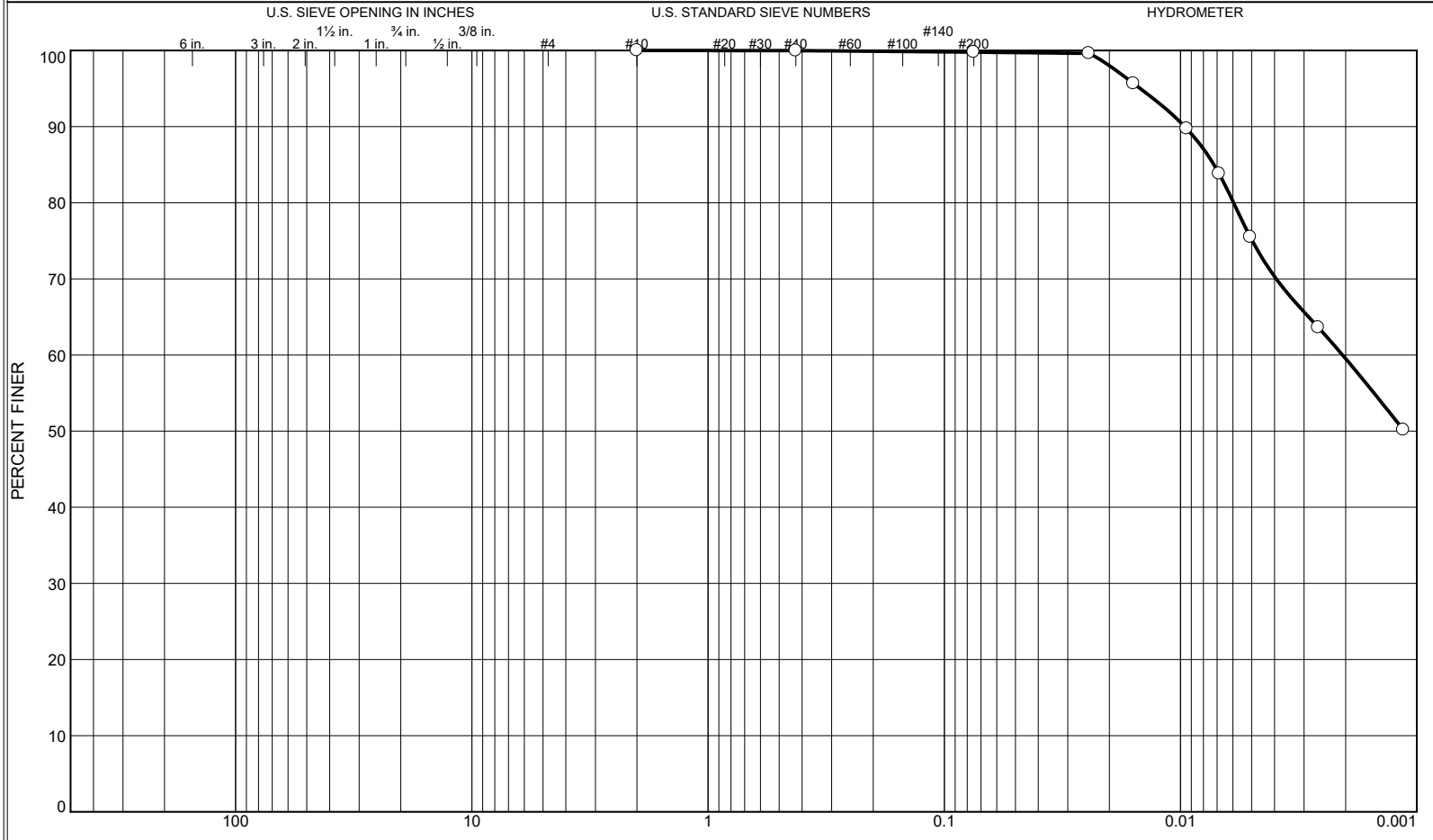


% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	0.2	20.3	79.5

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-9	Depth: 14-16	Sample Number: 8			

Client CPRA		
Project Breton Landbridge Marsh Creation(West)		
Project No. APS2008-G063		

# Particle Size Distribution Report

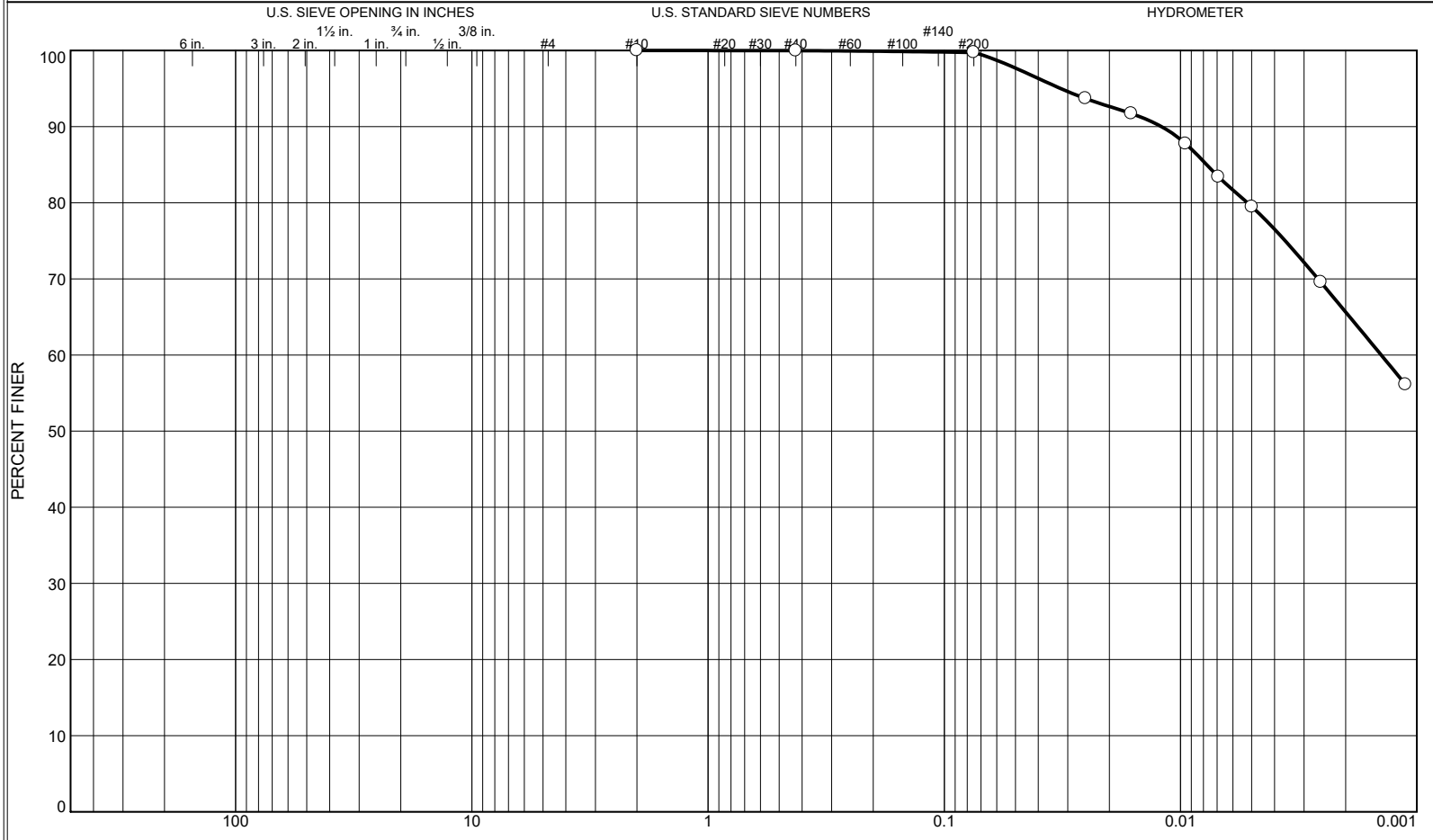


% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	0.2	24.6	75.2

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-9	Depth: 16-18	Sample Number: 9			

Client CPRA		
Project Breton Landbridge Marsh Creation(West)		
Project No. APS2008-G063		

# Particle Size Distribution Report



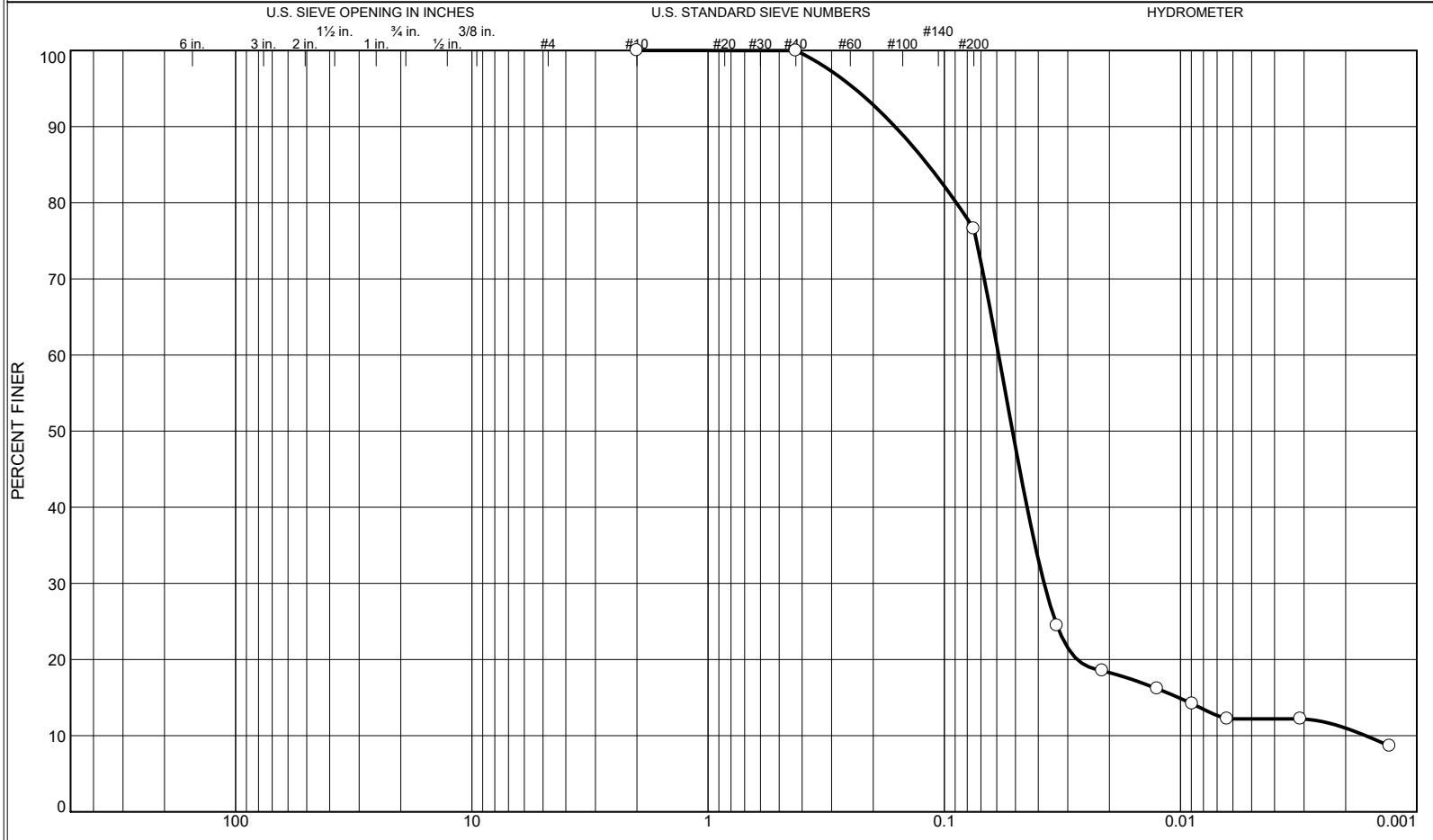
% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	0.3	20.2	79.5

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-9	Depth: 18-20	Sample Number: 10			

Client CPRA		
Project Breton Landbridge Marsh Creation(West)		
Project No. APS2008-G063		



# Particle Size Distribution Report

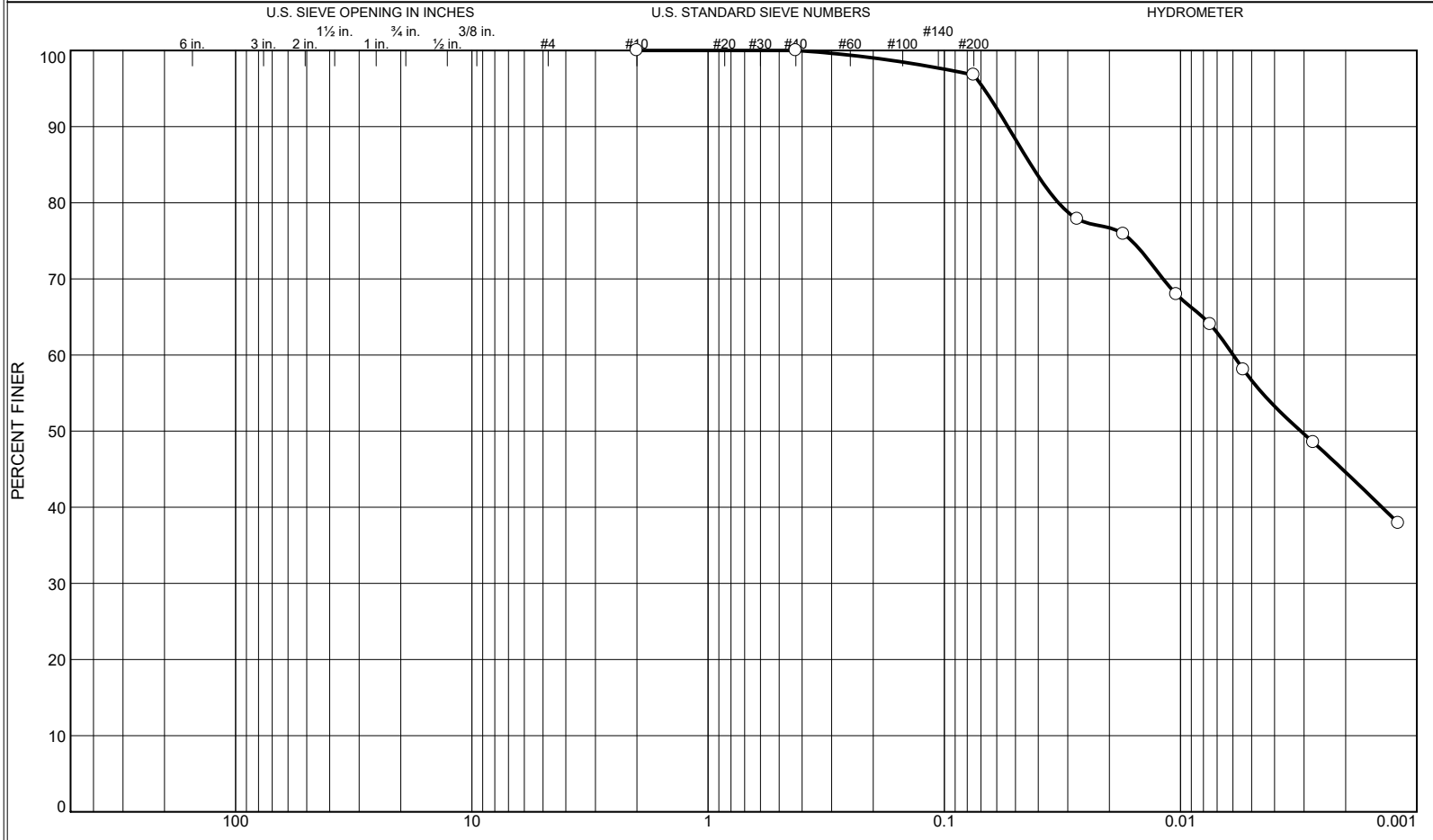


% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	23.4	64.4	12.2

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-9	Depth: 23-25	Sample Number: 11			

Client CPRA	
Project Breton Landbridge Marsh Creation(West)	
Project No. APS2008-G063	

# Particle Size Distribution Report

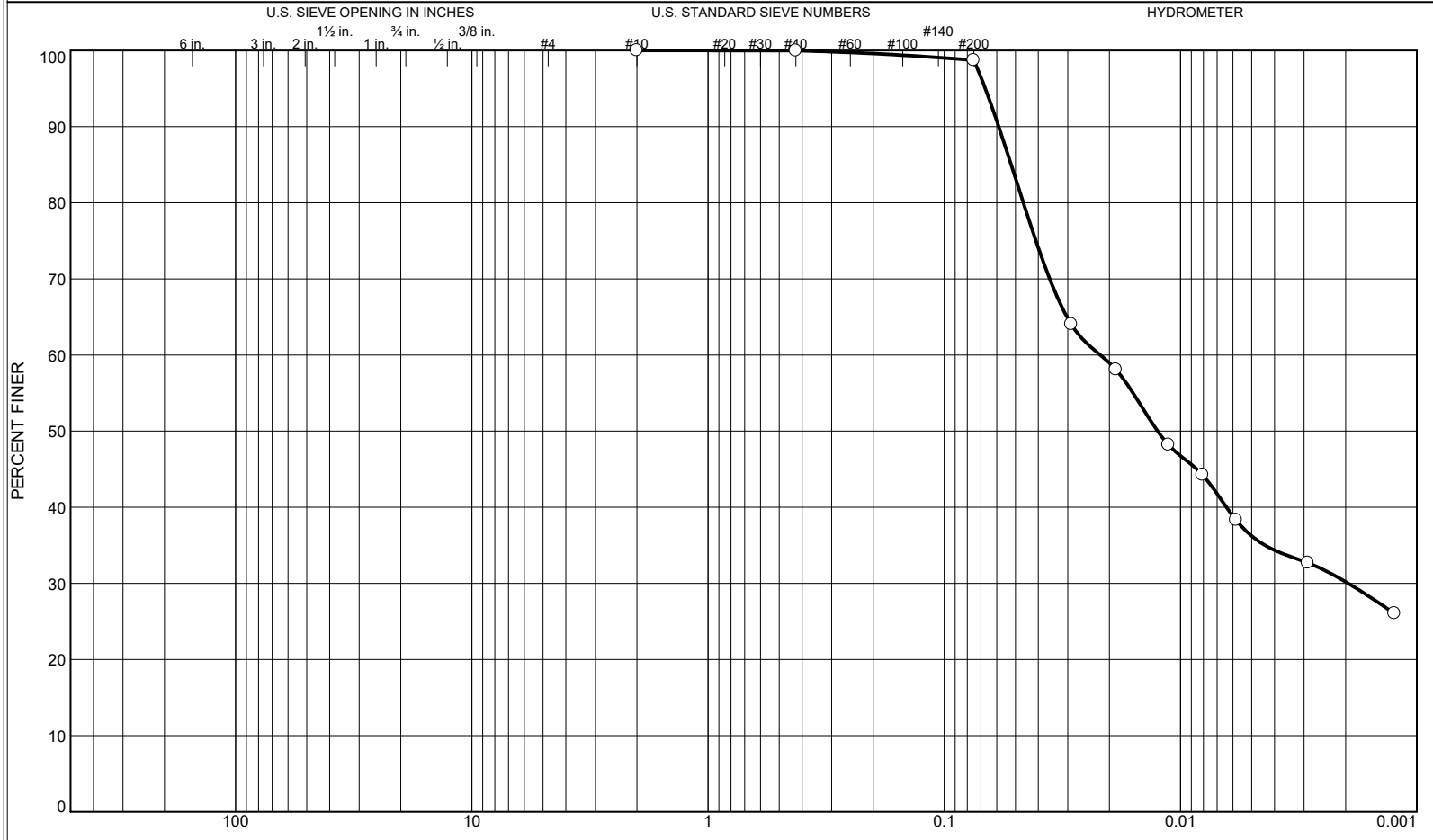


% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	3.2	40.1	56.7

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-10	Depth: 0-2	Sample Number: 1			

Client CPRA		
Project Breton Landbridge Marsh Creation(West)		
Project No. APS2008-G063		

# Particle Size Distribution Report

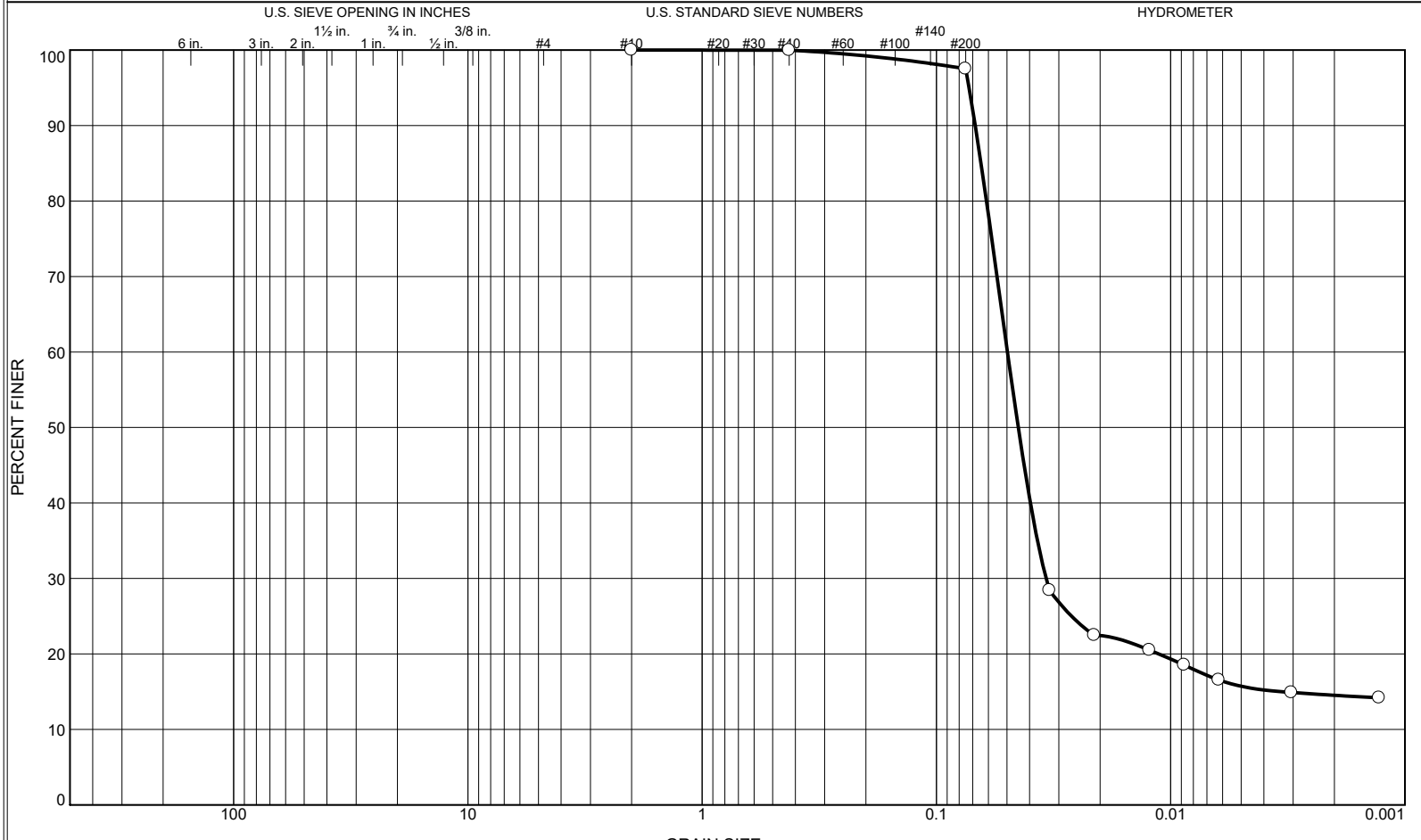


% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	1.3	62.5	36.2

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-10	Depth: 2-4	Sample Number: 2			


Client CPRA		
Project Breton Landbridge Marsh Creation(West)		
Project No. APS2008-G063		

# Particle Size Distribution Report

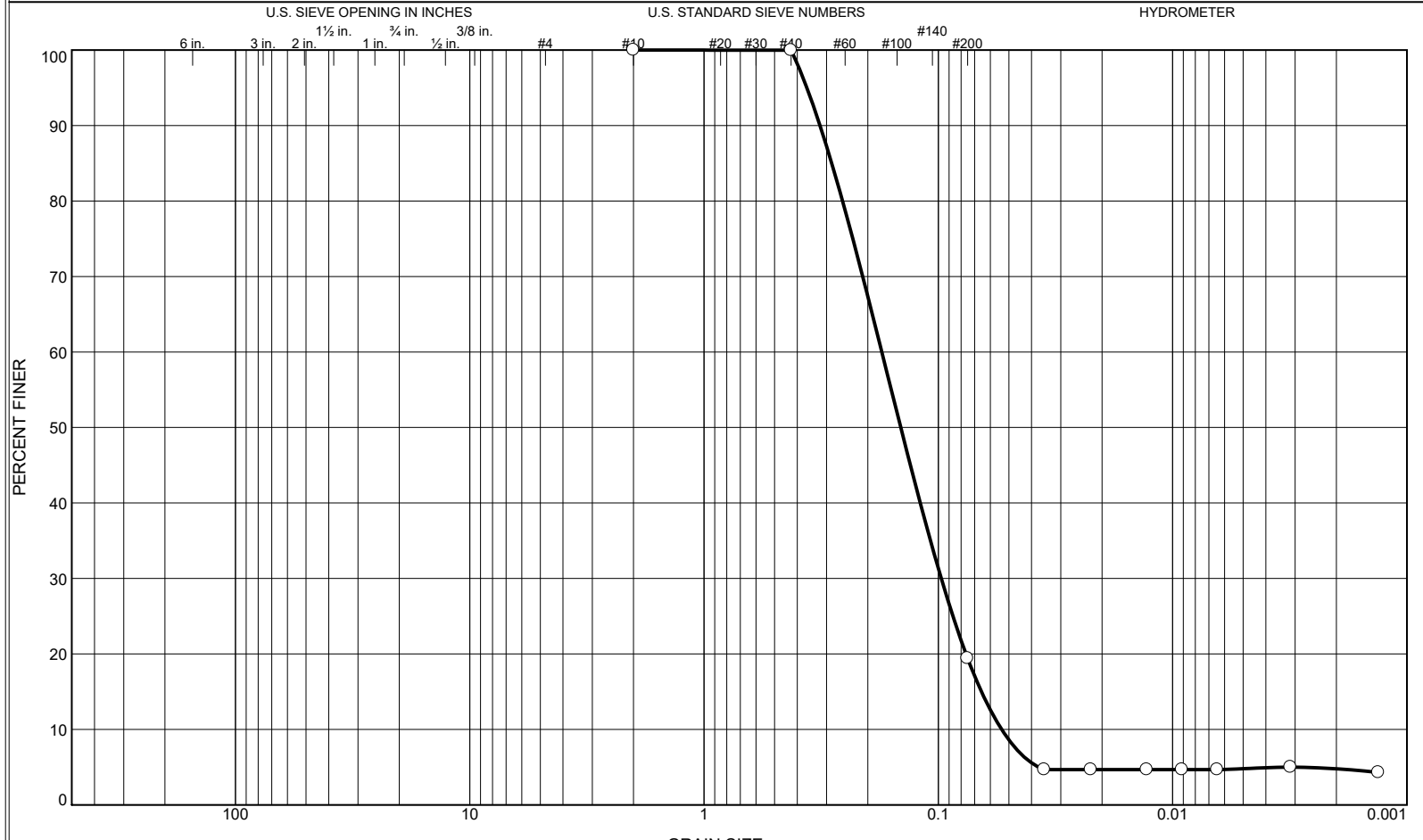


% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	2.5	81.8	15.7

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-10	Depth: 4-6	Sample Number: 3			


Client CPRA		
Project Breton Landbridge Marsh Creation(West)		
Project No. APS2008-G063		

# Particle Size Distribution Report

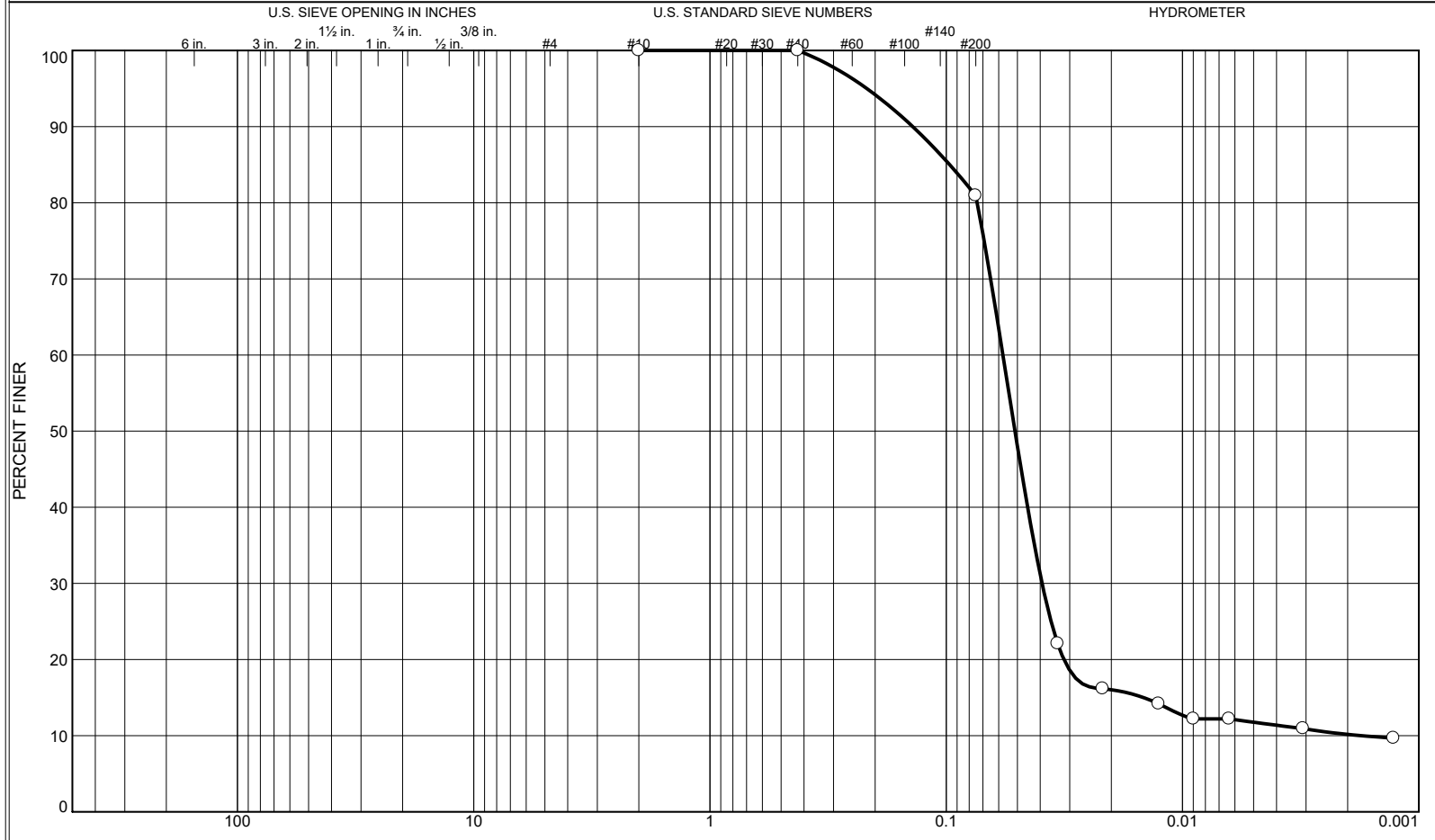


% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	80.6	14.6	4.8

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-10	Depth: 6-8	Sample Number: 4			


Client CPRA		
Project Breton Landbridge Marsh Creation(West)		
Project No. APS2008-G063		

# Particle Size Distribution Report

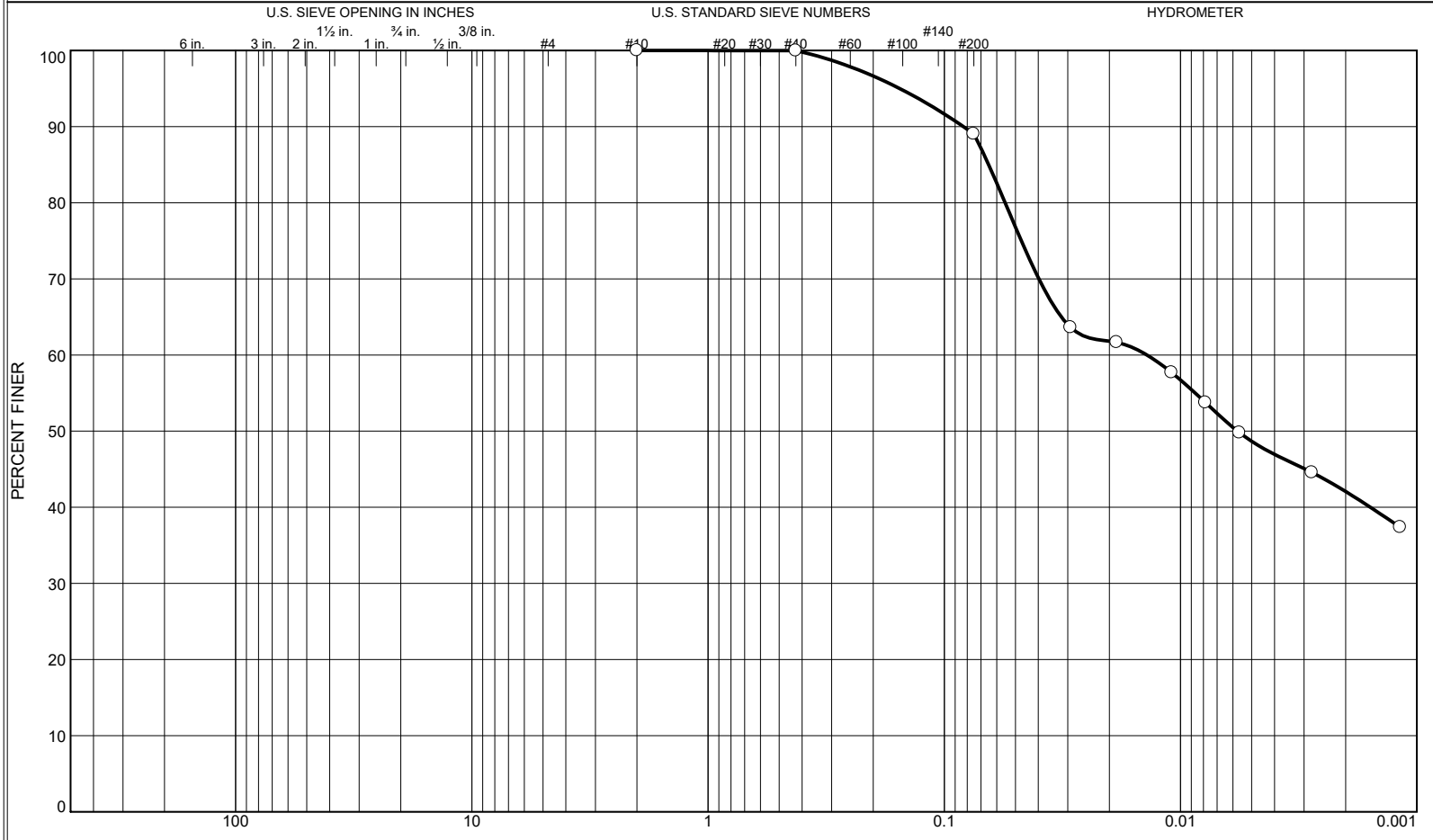


% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	19.1	69.1	11.8

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-10	Depth: 8-10	Sample Number: 5			

Client CPRA		
Project Breton Landbridge Marsh Creation(West)		
Project No. APS2008-G063		

# Particle Size Distribution Report

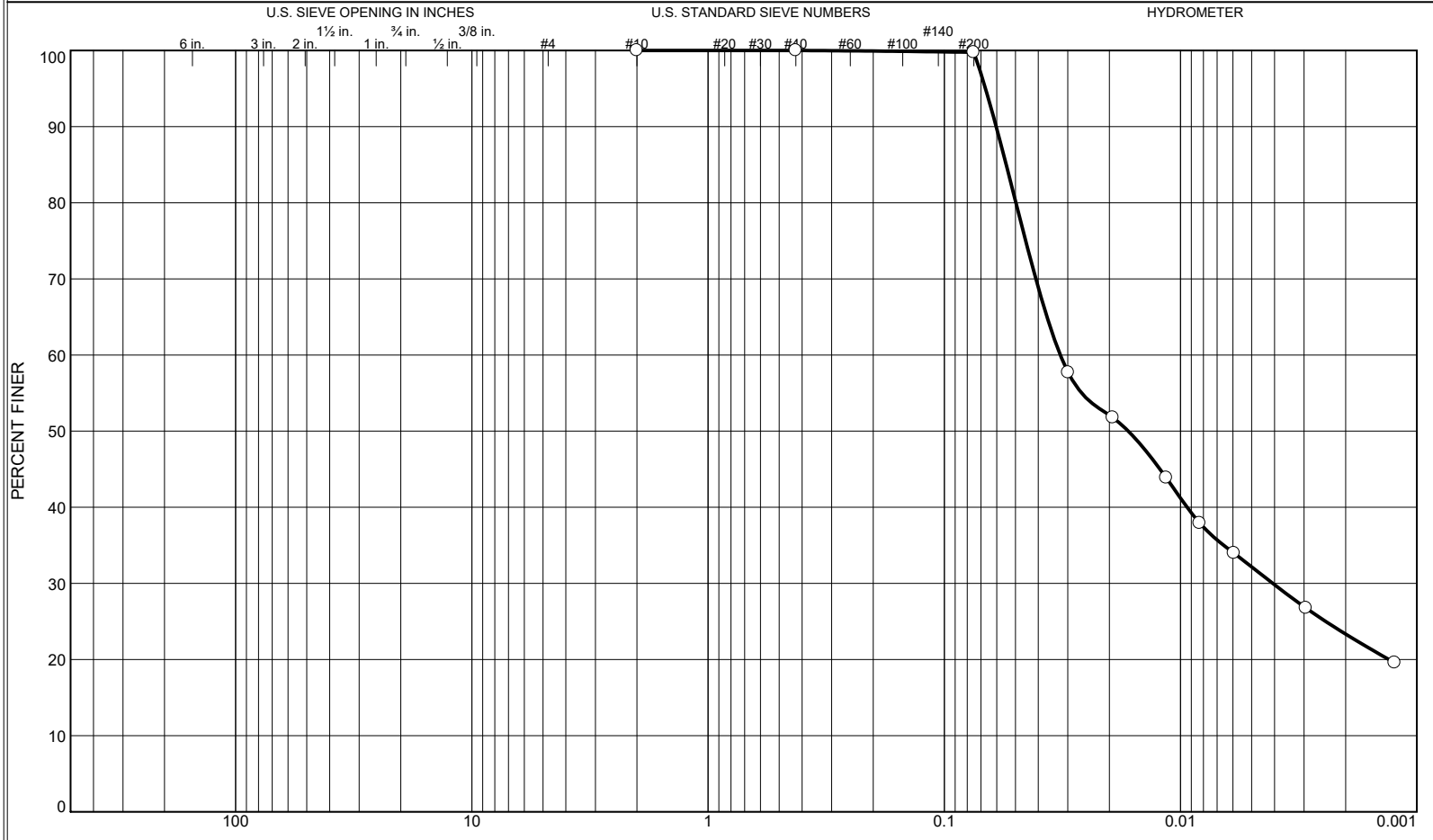


% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	11.0	40.3	48.7

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-10	Depth: 10-12	Sample Number: 6			

Client CPRA		
Project Breton Landbridge Marsh Creation(West)		
Project No. APS2008-G063		

# Particle Size Distribution Report



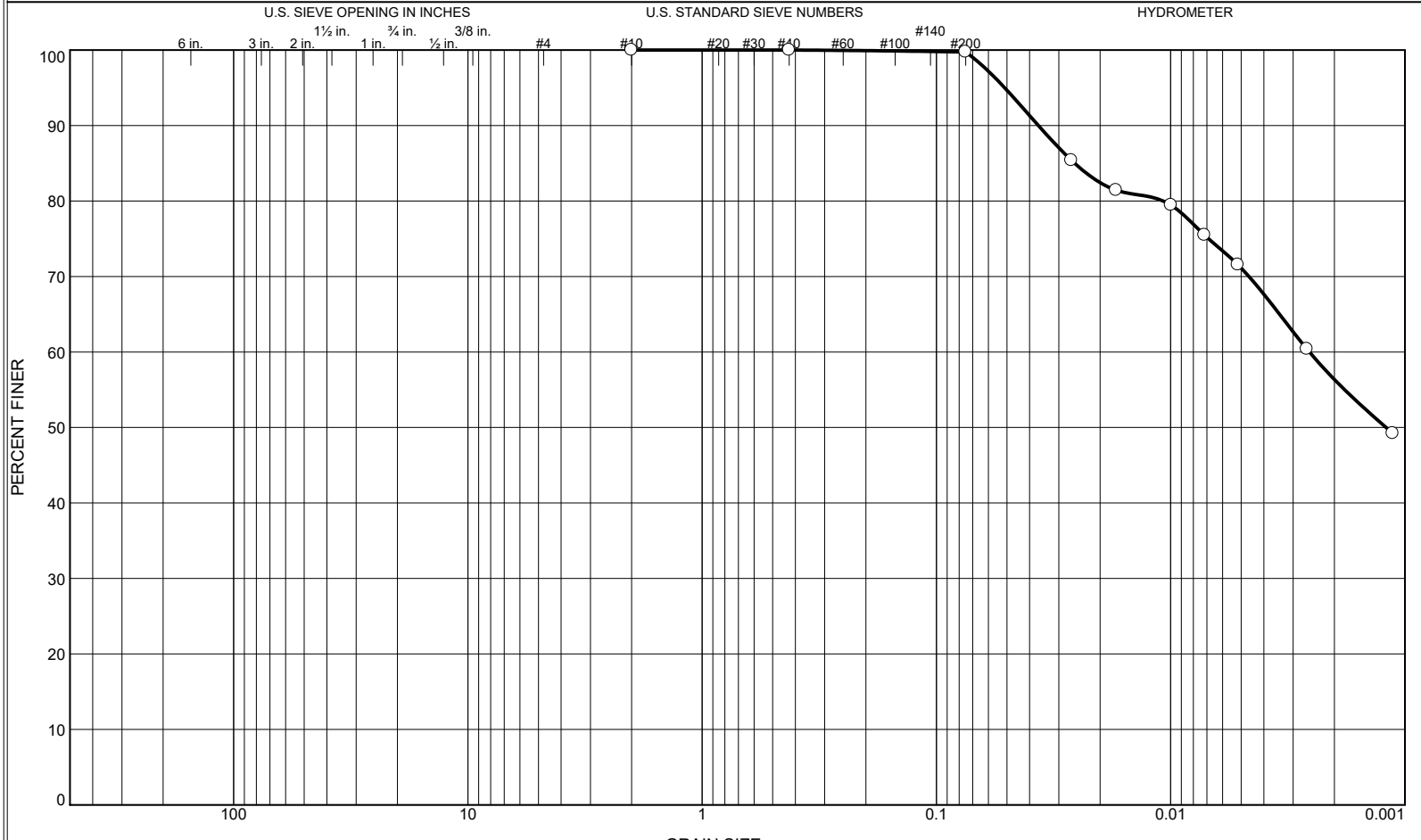
% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	0.2	67.6	32.2

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-10	Depth: 12-14	Sample Number: 7			

Client CPRA		
Project Breton Landbridge Marsh Creation(West)		
Project No. APS2008-G063		



# Particle Size Distribution Report

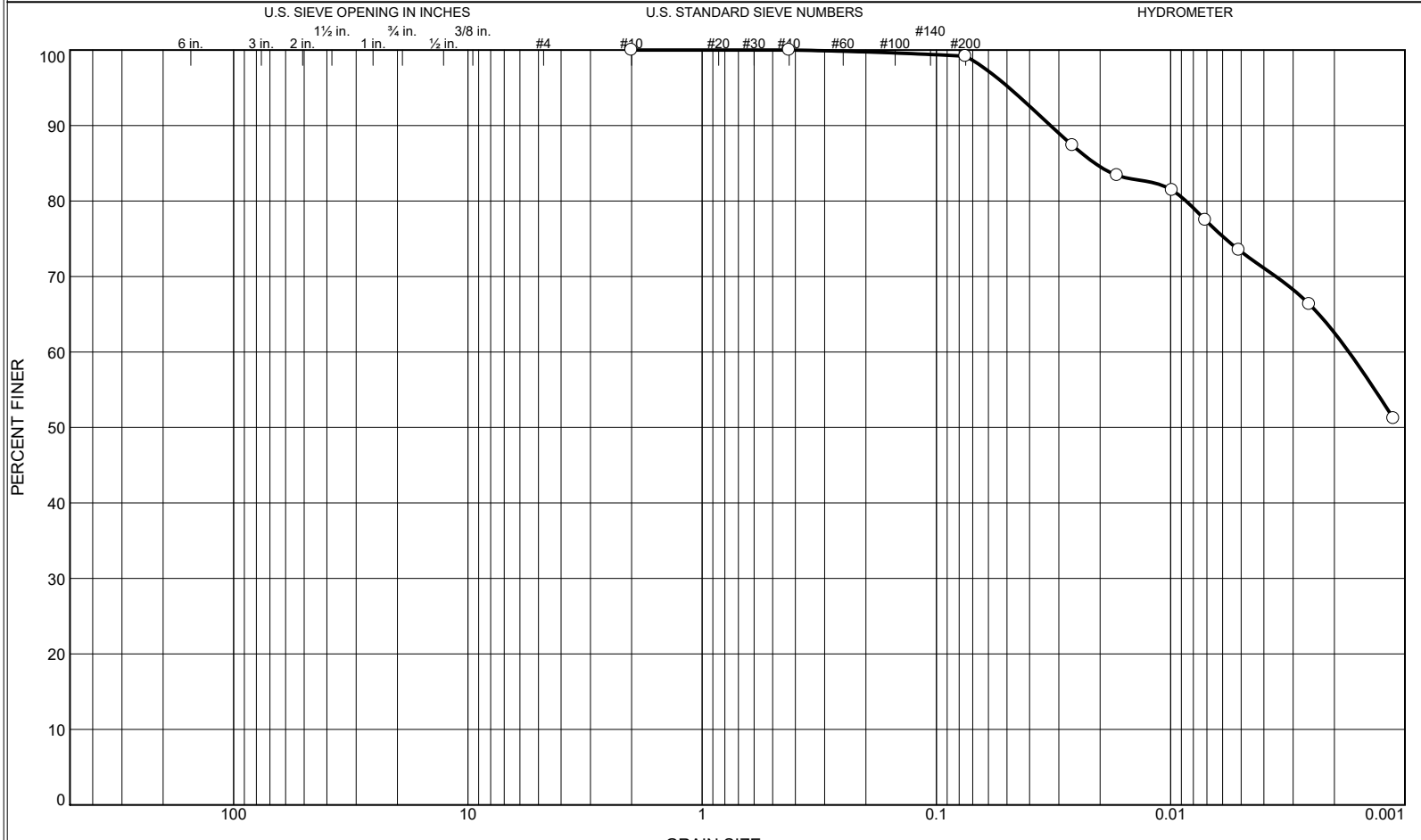


% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	0.3	28.6	71.1

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-10	Depth: 14-16	Sample Number: 8			

Client CPRA		
Project Breton Landbridge Marsh Creation(West)		
Project No. APS2008-G063		

# Particle Size Distribution Report

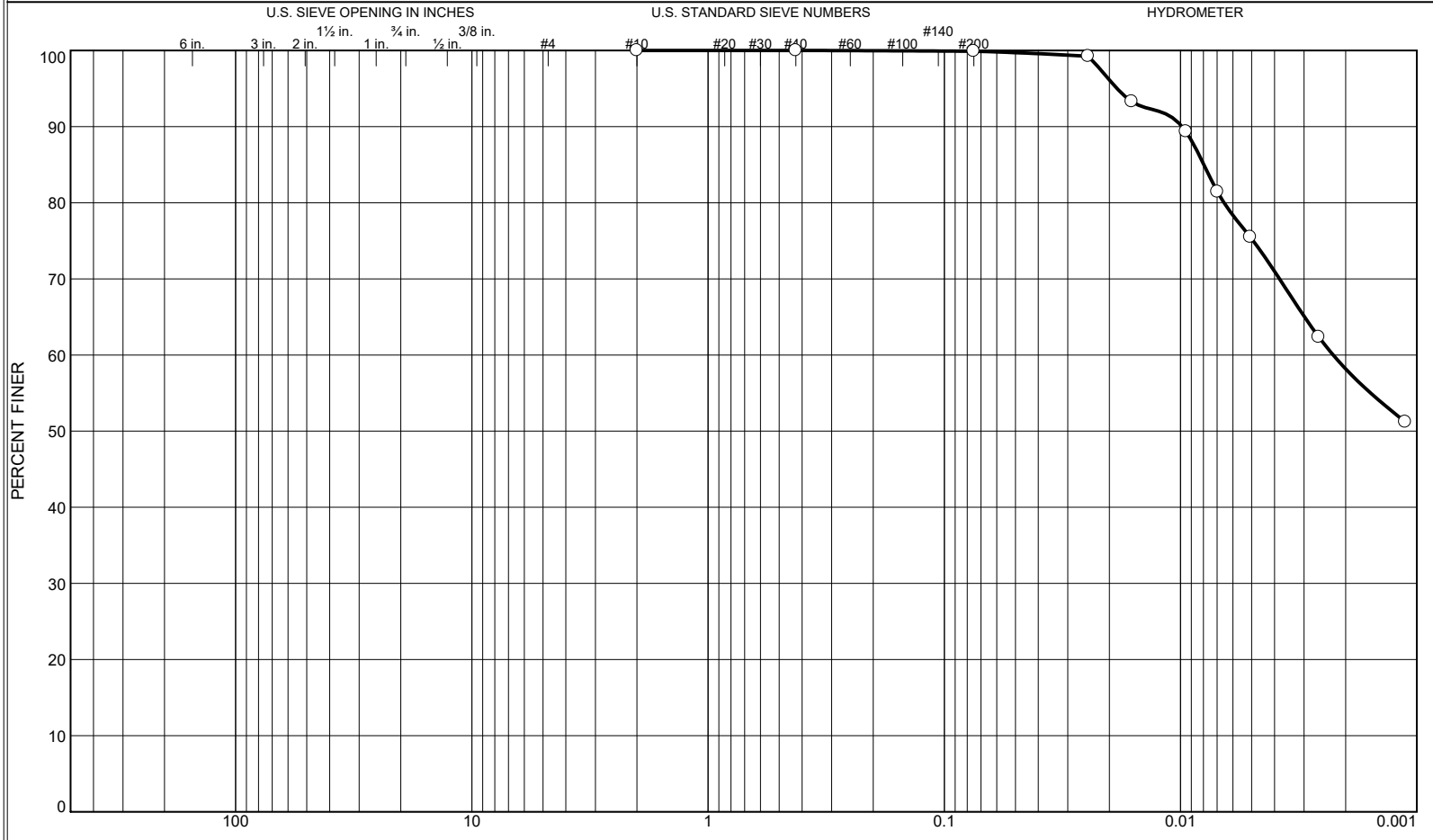


% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	0.8	25.9	73.3

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-10	Depth: 16-18	Sample Number: 9			

Client CPRA		
Project Breton Landbridge Marsh Creation(West)		
Project No. APS2008-G063		

# Particle Size Distribution Report

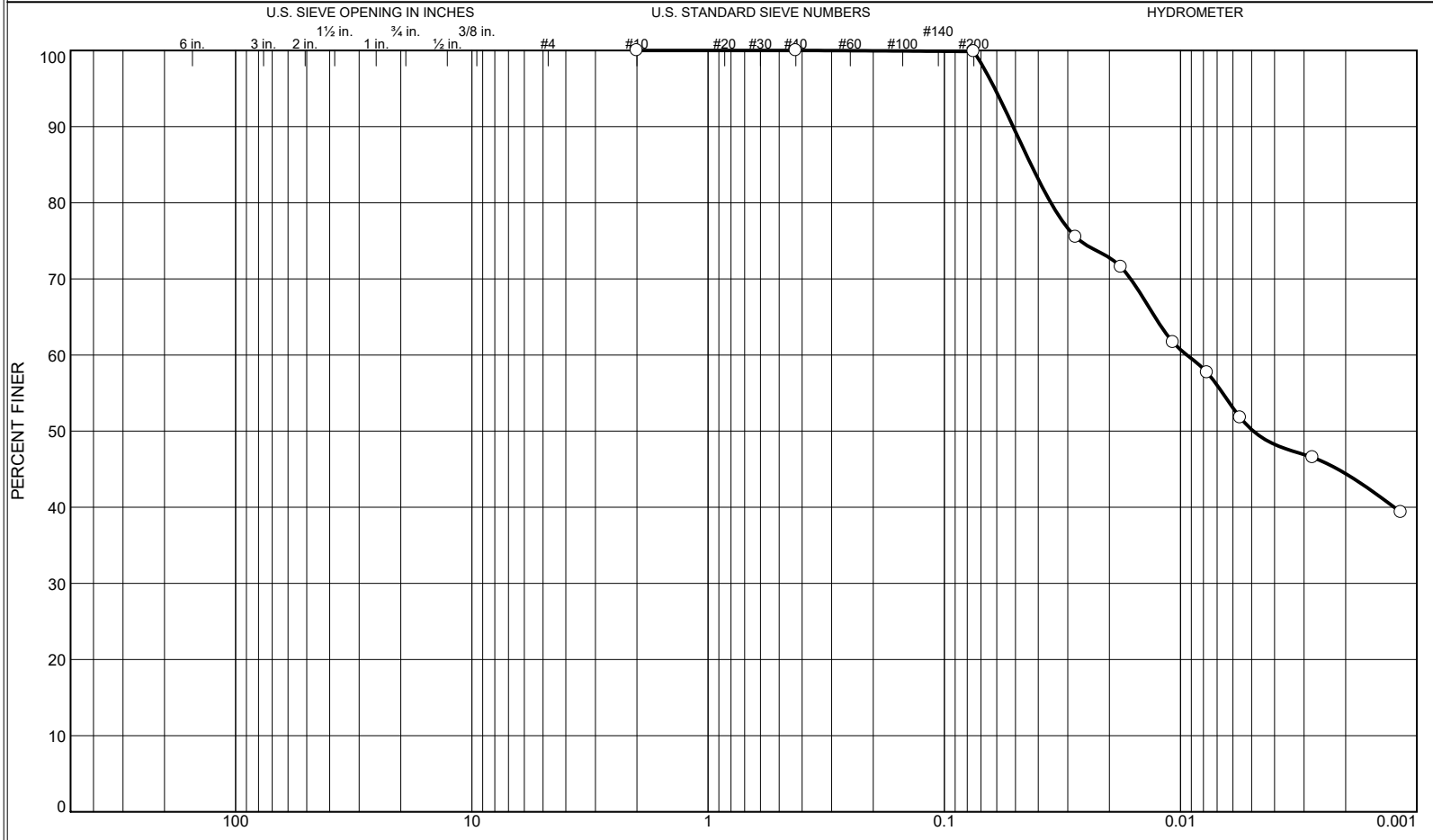


% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	0.1	24.6	75.3

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-10	Depth: 18-20	Sample Number: 10			


Client CPRA		
Project Breton Landbridge Marsh Creation(West)		
Project No. APS2008-G063		

# Particle Size Distribution Report

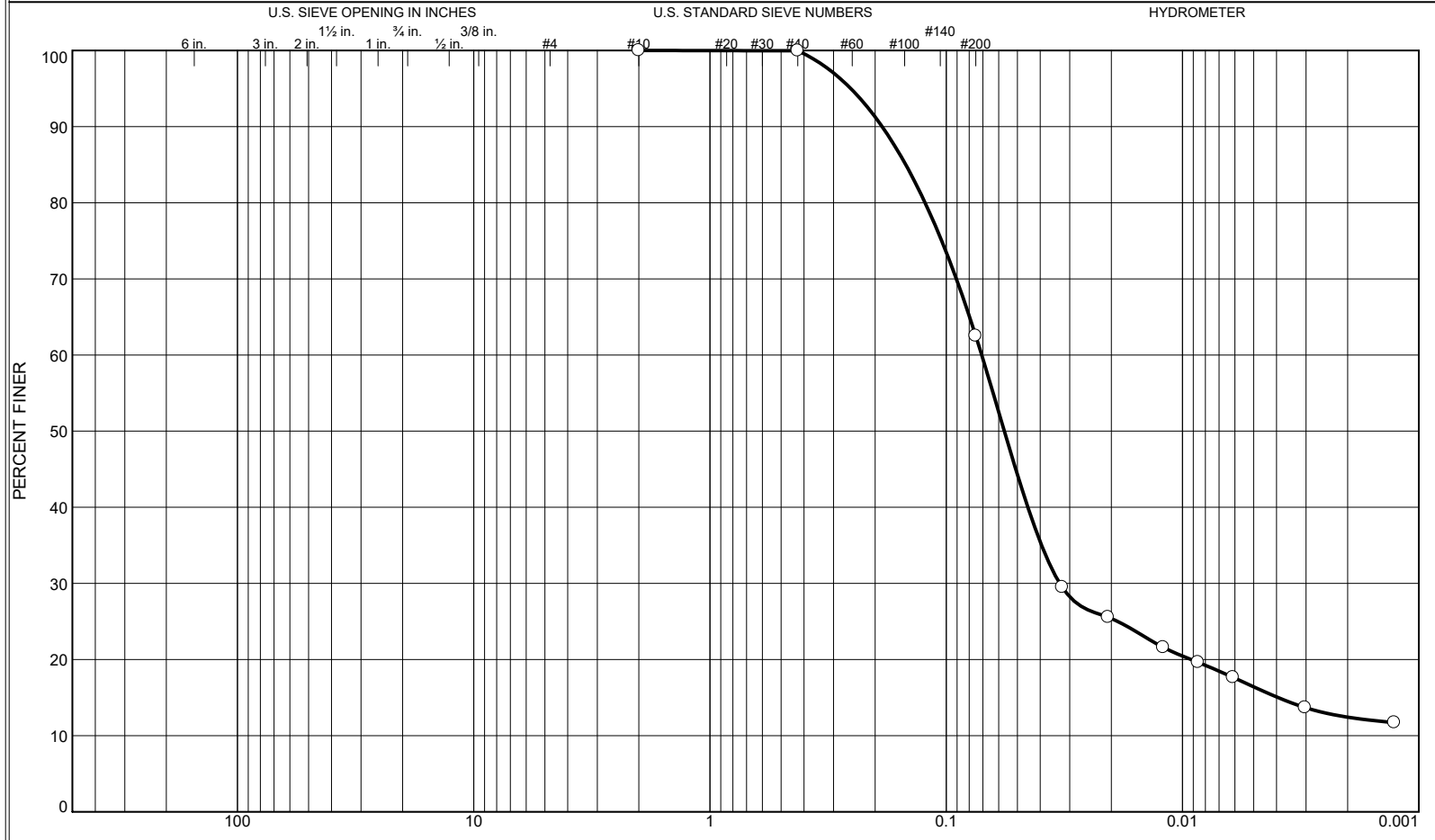


% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	0.1	49.7	50.2

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-10	Depth: 23-25	Sample Number: 11			


Client CPRA		
Project Breton Landbridge Marsh Creation(West)		
Project No. APS2008-G063		

# Particle Size Distribution Report

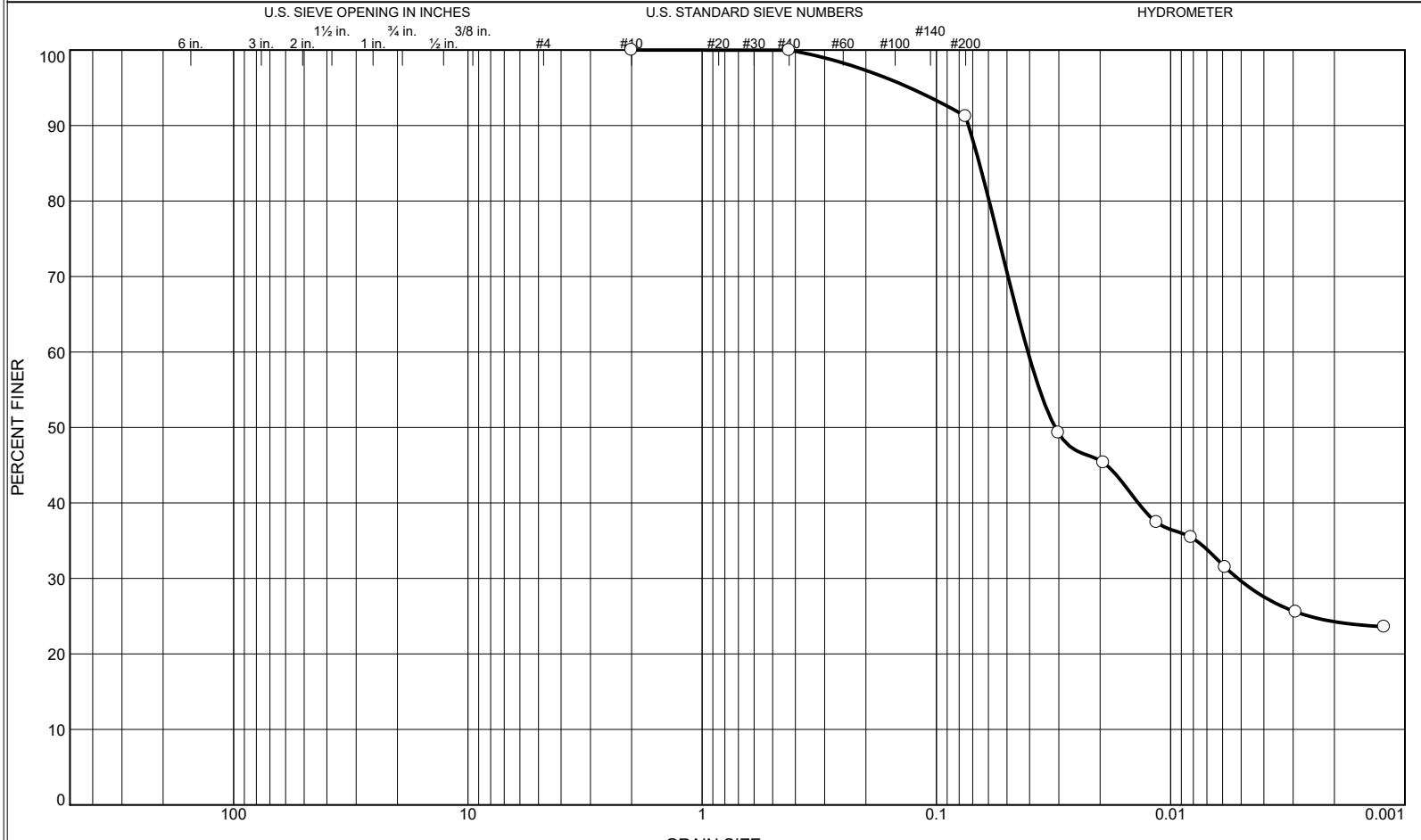


% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	37.5	46.1	16.4

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-11	Depth: 0-2	Sample Number: 1			

Client CPRA		
Project Breton Landbridge Marsh Creation(West)		
Project No. APS2008-G063		

# Particle Size Distribution Report

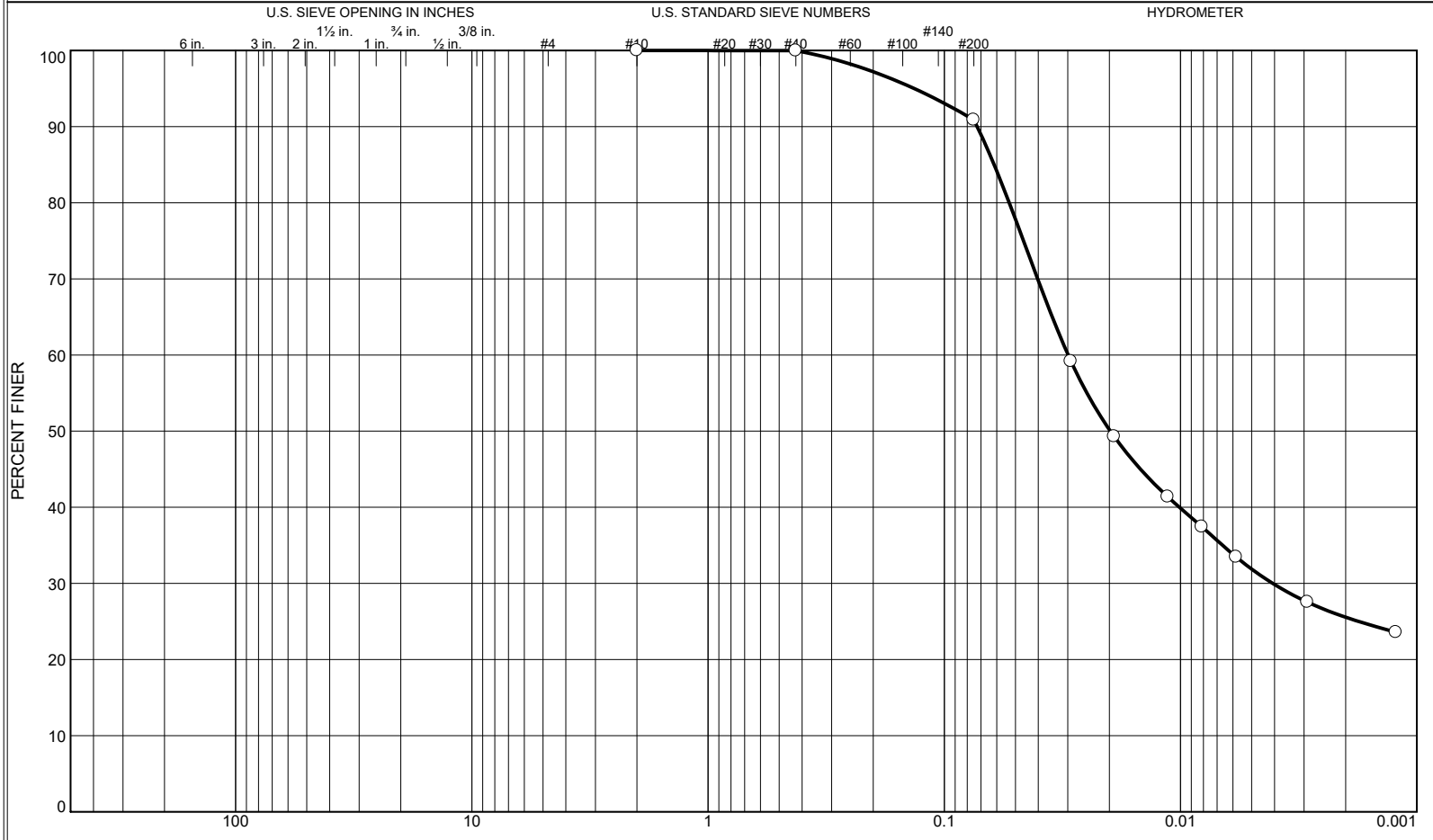


% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	8.8	61.6	29.6

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-11	Depth: 2-4	Sample Number: 2			

Client CPRA		
Project Breton Landbridge Marsh Creation(West)		
Project No. APS2008-G063		

# Particle Size Distribution Report

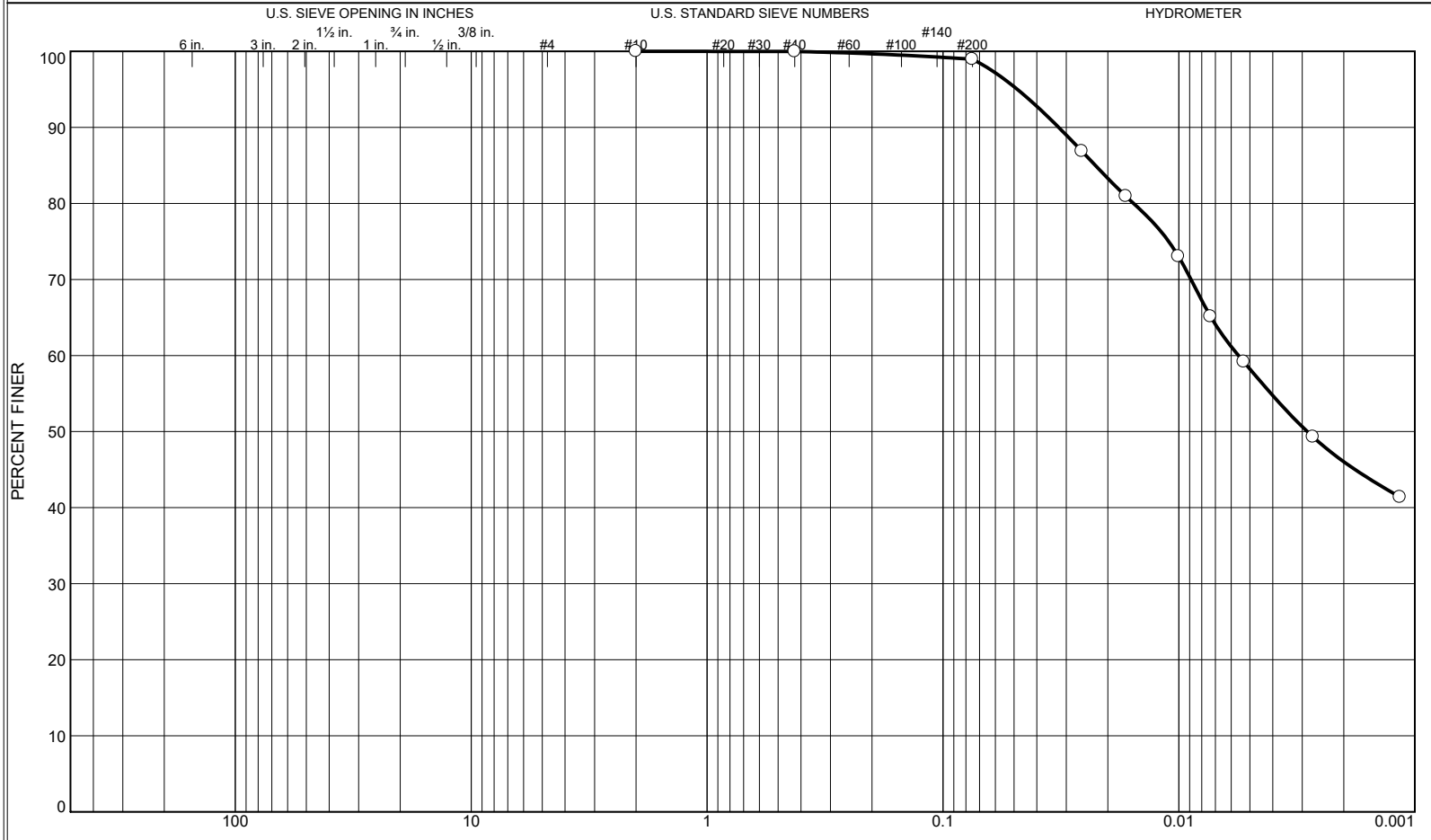


% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	9.1	59.0	31.9

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-11	Depth: 6-8	Sample Number: 4			

Client CPRA		
Project Breton Landbridge Marsh Creation(West)		
Project No. APS2008-G063		

# Particle Size Distribution Report



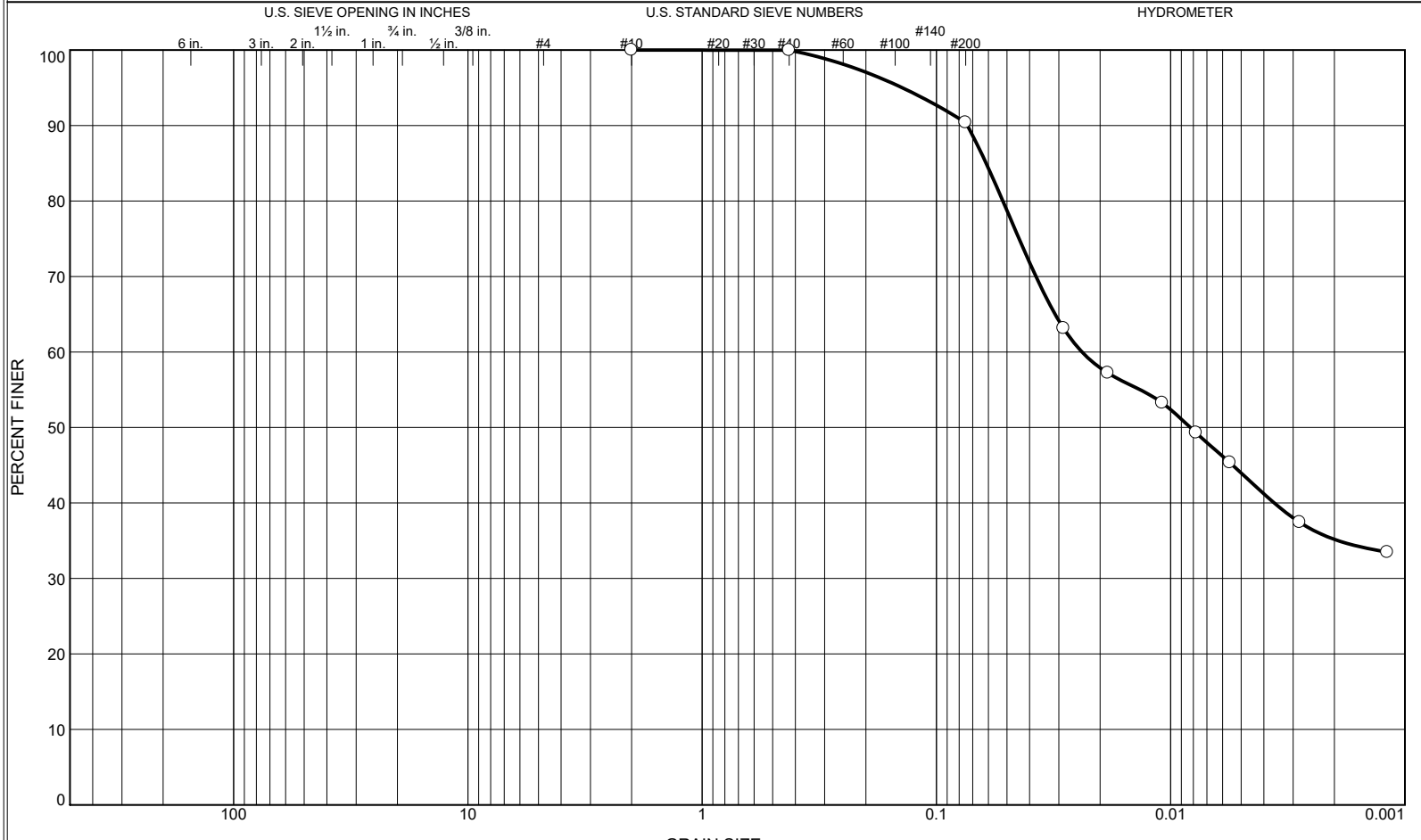
% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	1.0	40.8	58.2

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-11	Depth: 8-10	Sample Number: 5			

Client CPRA		
Project Breton Landbridge Marsh Creation(West)		
Project No. APS2008-G063		



# Particle Size Distribution Report

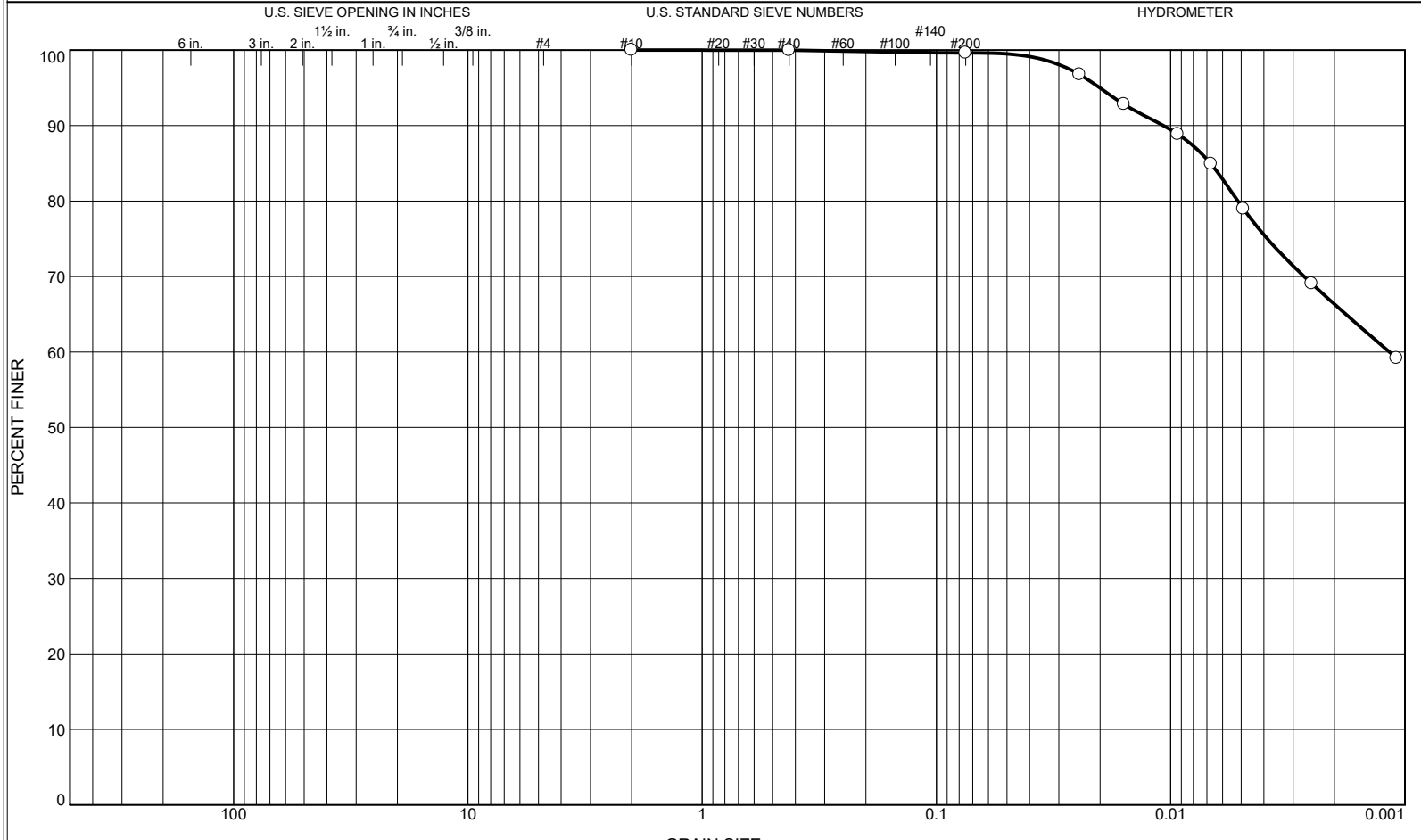


% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	9.6	46.4	44.0

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-11	Depth: 10-12	Sample Number: 6			

Client CPRA		
Project Breton Landbridge Marsh Creation(West)		
Project No. APS2008-G063		

# Particle Size Distribution Report

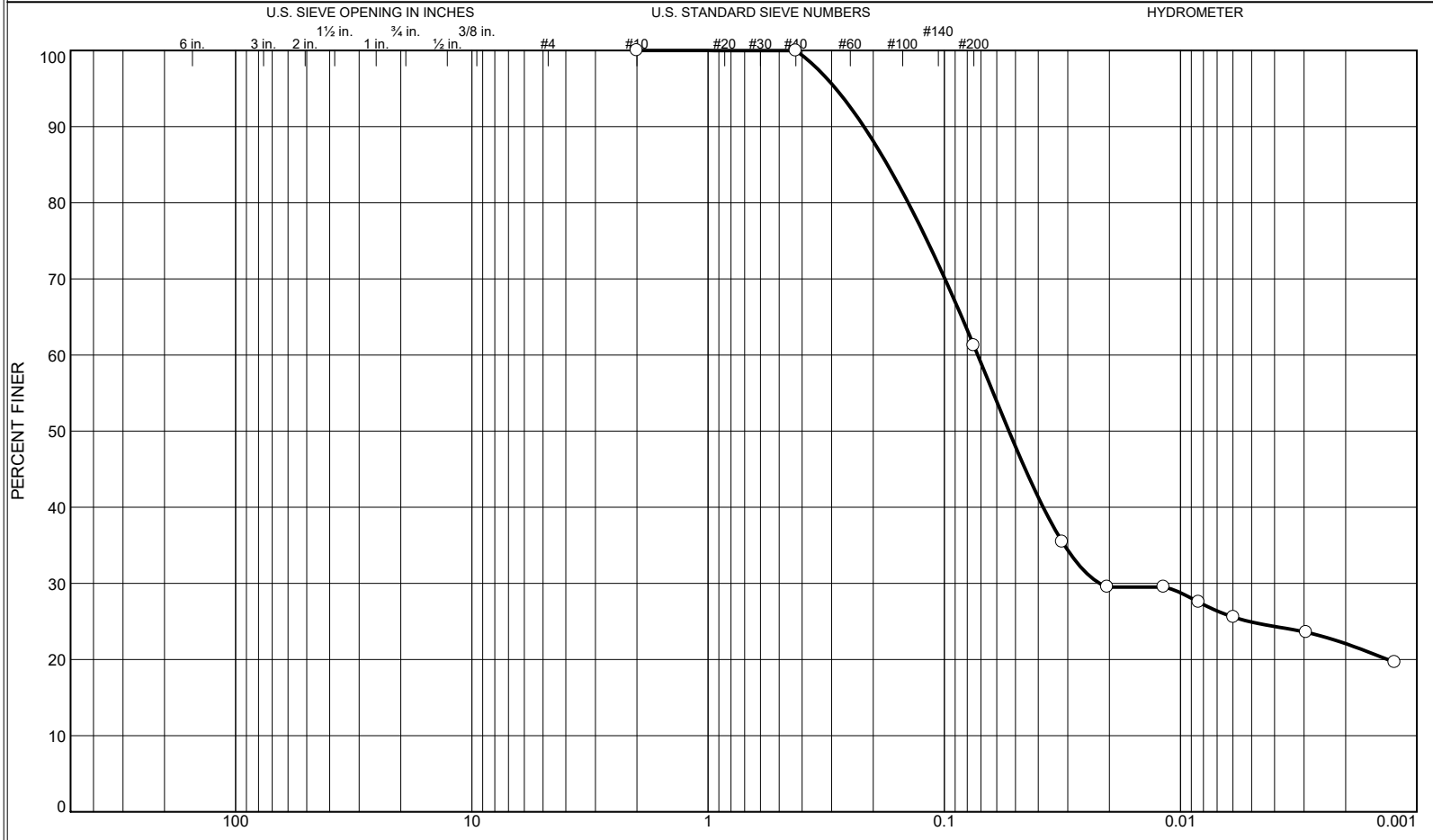


% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	0.4	20.2	79.4

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-11	Depth: 12-14	Sample Number: 7			

Client CPRA		
Project Breton Landbridge Marsh Creation(West)		
Project No. APS2008-G063		

# Particle Size Distribution Report

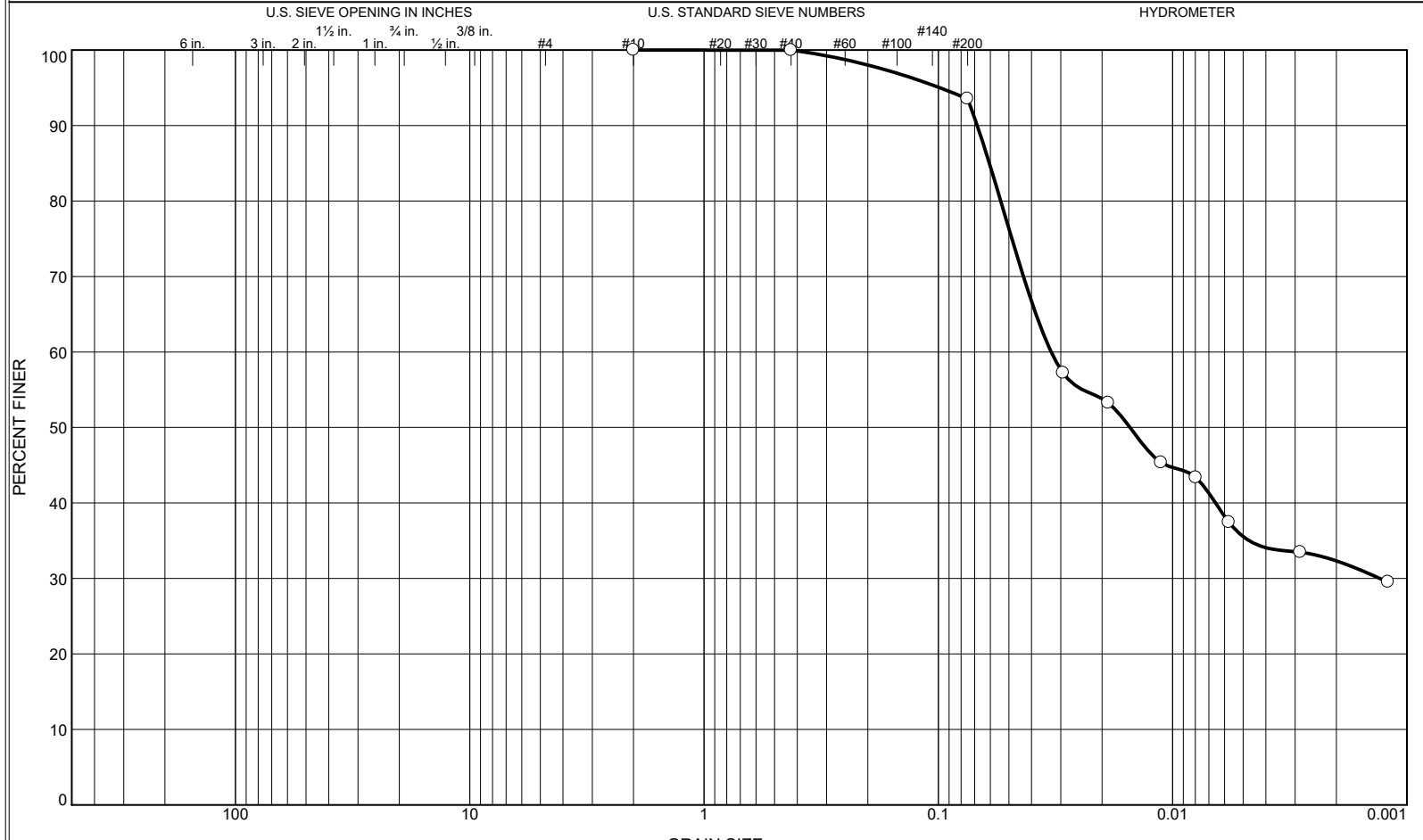


% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	38.8	36.3	24.9

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-11	Depth: 14-16	Sample Number: 8			


Client CPRA		
Project Breton Landbridge Marsh Creation(West)		
Project No. APS2008-G063		

# Particle Size Distribution Report

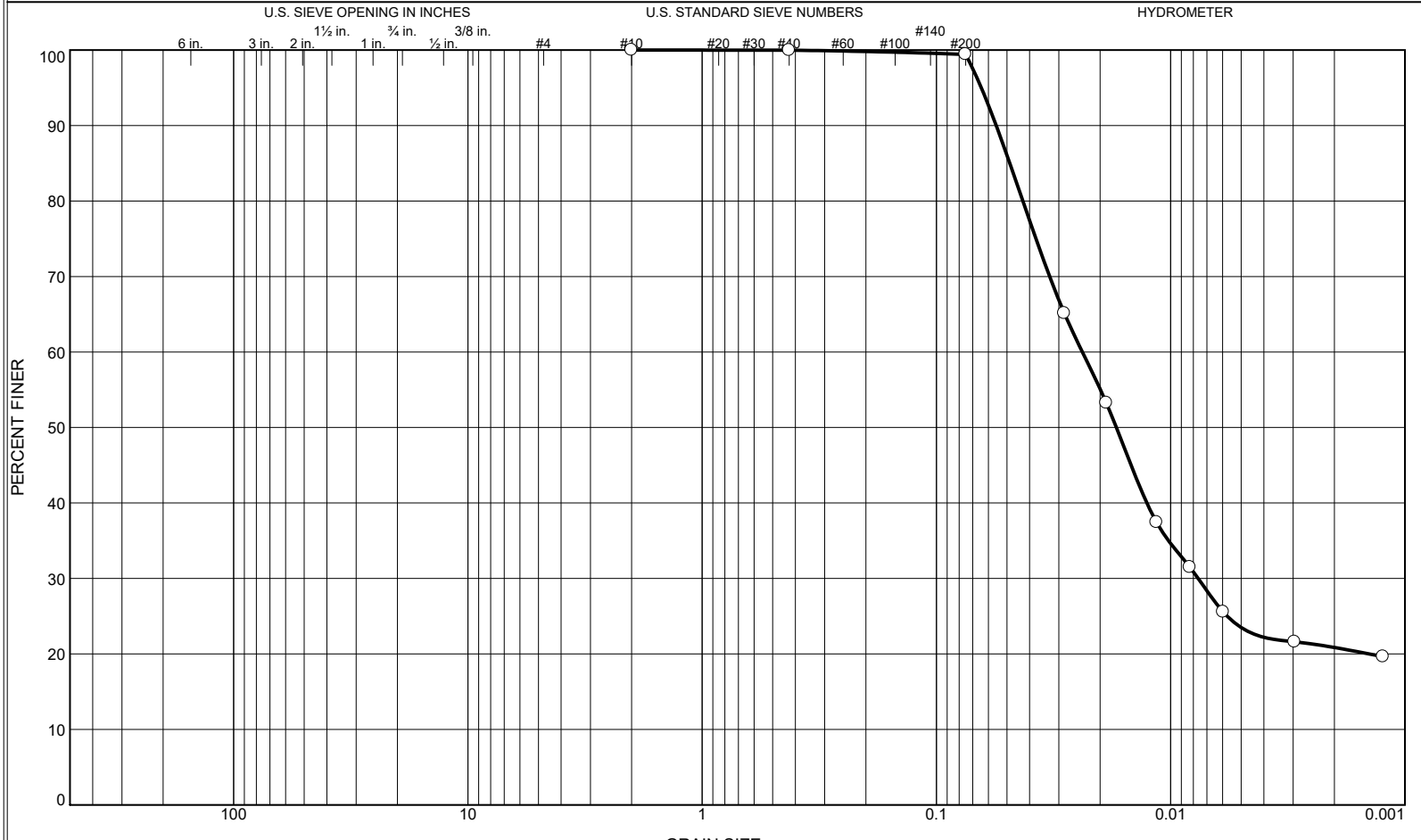


% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	6.5	57.9	35.6

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-11	Depth: 16-18	Sample Number: 9			

Client CPRA		
Project Breton Landbridge Marsh Creation(West)		
Project No. APS2008-G063		

# Particle Size Distribution Report

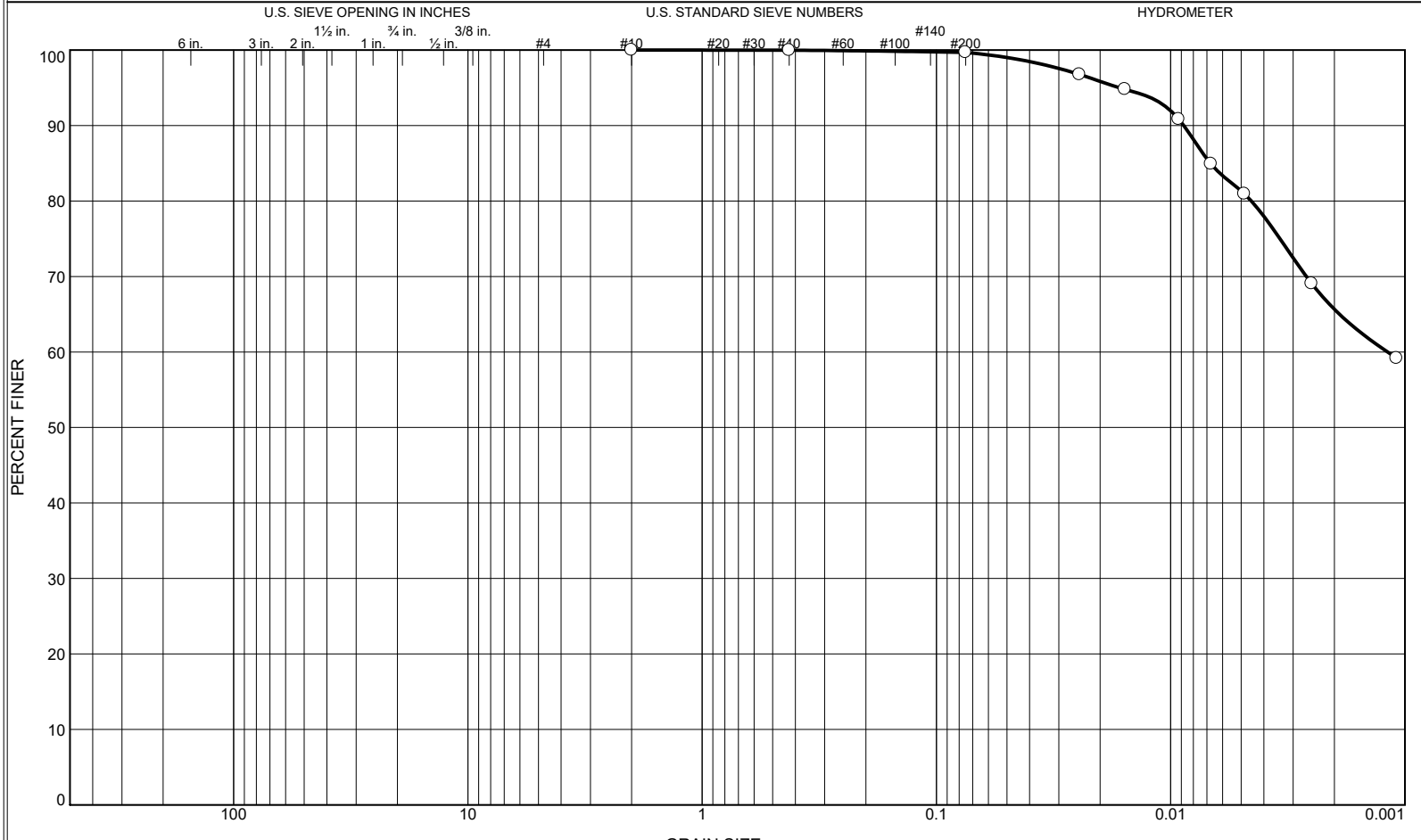


% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	0.6	75.9	23.5

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-11	Depth: 18-20	Sample Number: 10			

Client CPRA		
Project Breton Landbridge Marsh Creation(West)		
Project No. APS2008-G063		

# Particle Size Distribution Report

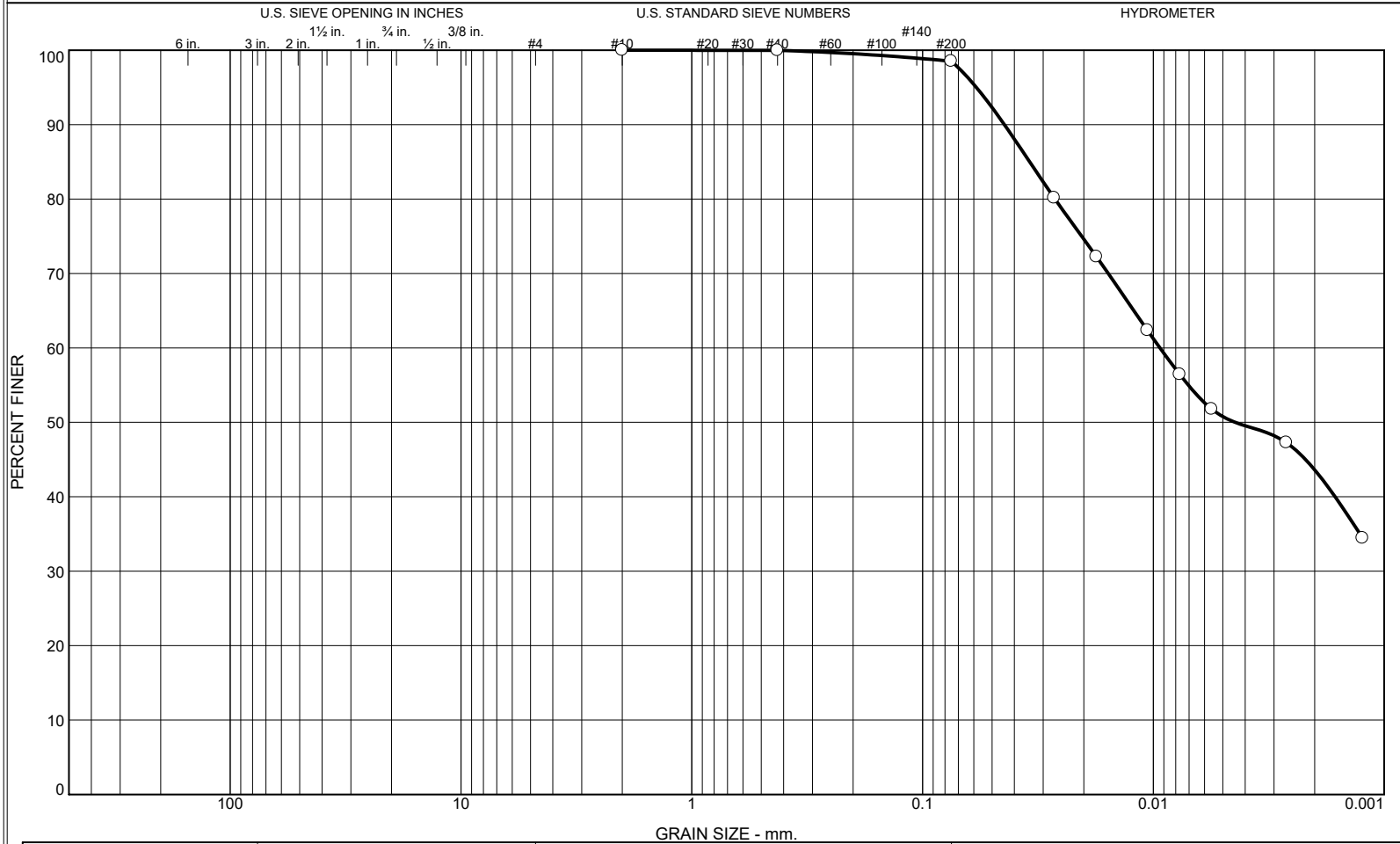


% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	0.3	18.4	81.3

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-11	Depth: 23-25	Sample Number: 11			

Client CPRA		
Project Breton Landbridge Marsh Creation(West)		
Project No. APS2008-G063		

# Particle Size Distribution Report

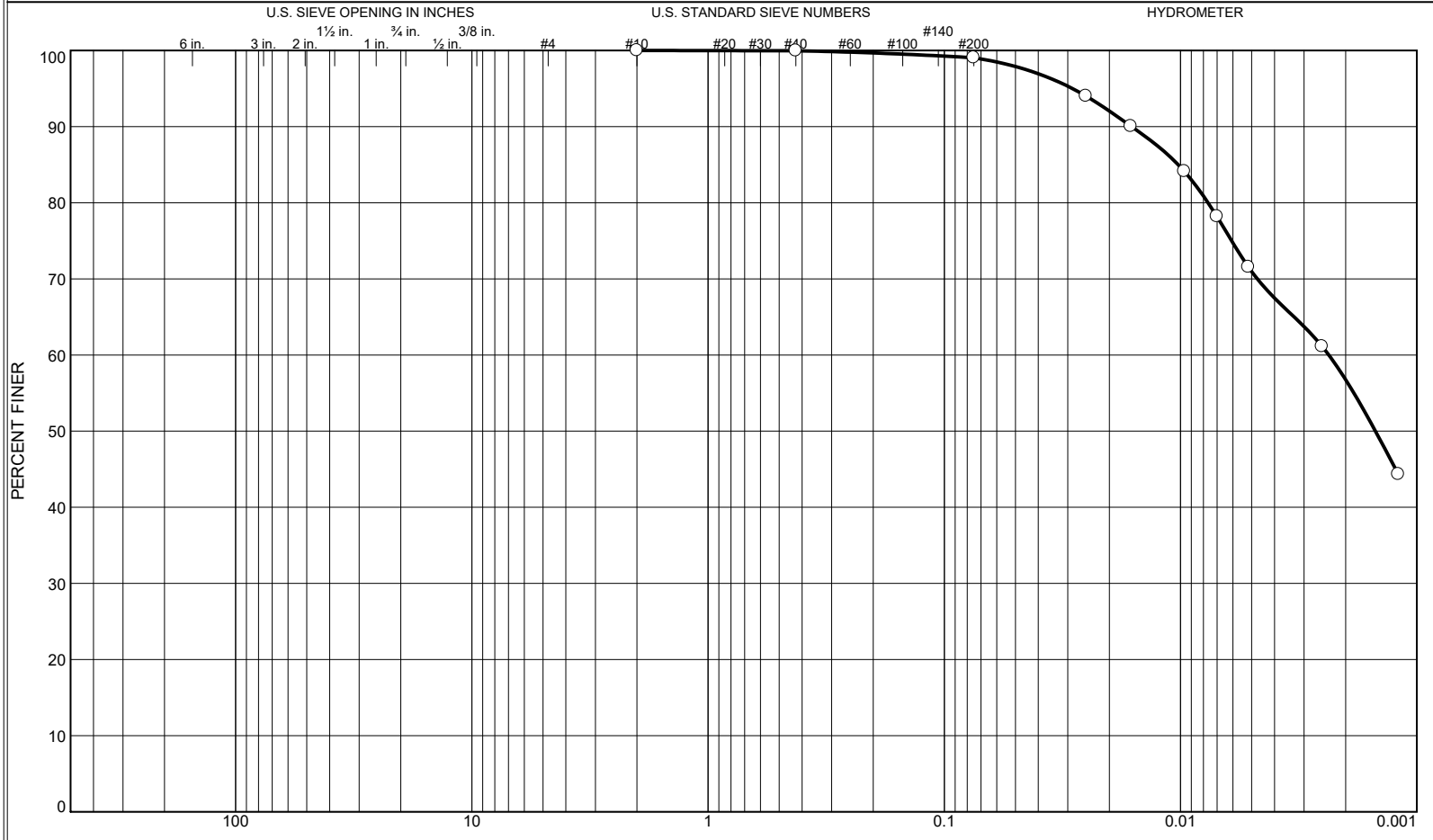


% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	1.5	47.7	50.8

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-12	Depth: 0-2	Sample Number: 1			

Client CPRA		
Project Breton Landbridge Marsh Creation(West)		
Project No. APS2008-G063		

# Particle Size Distribution Report



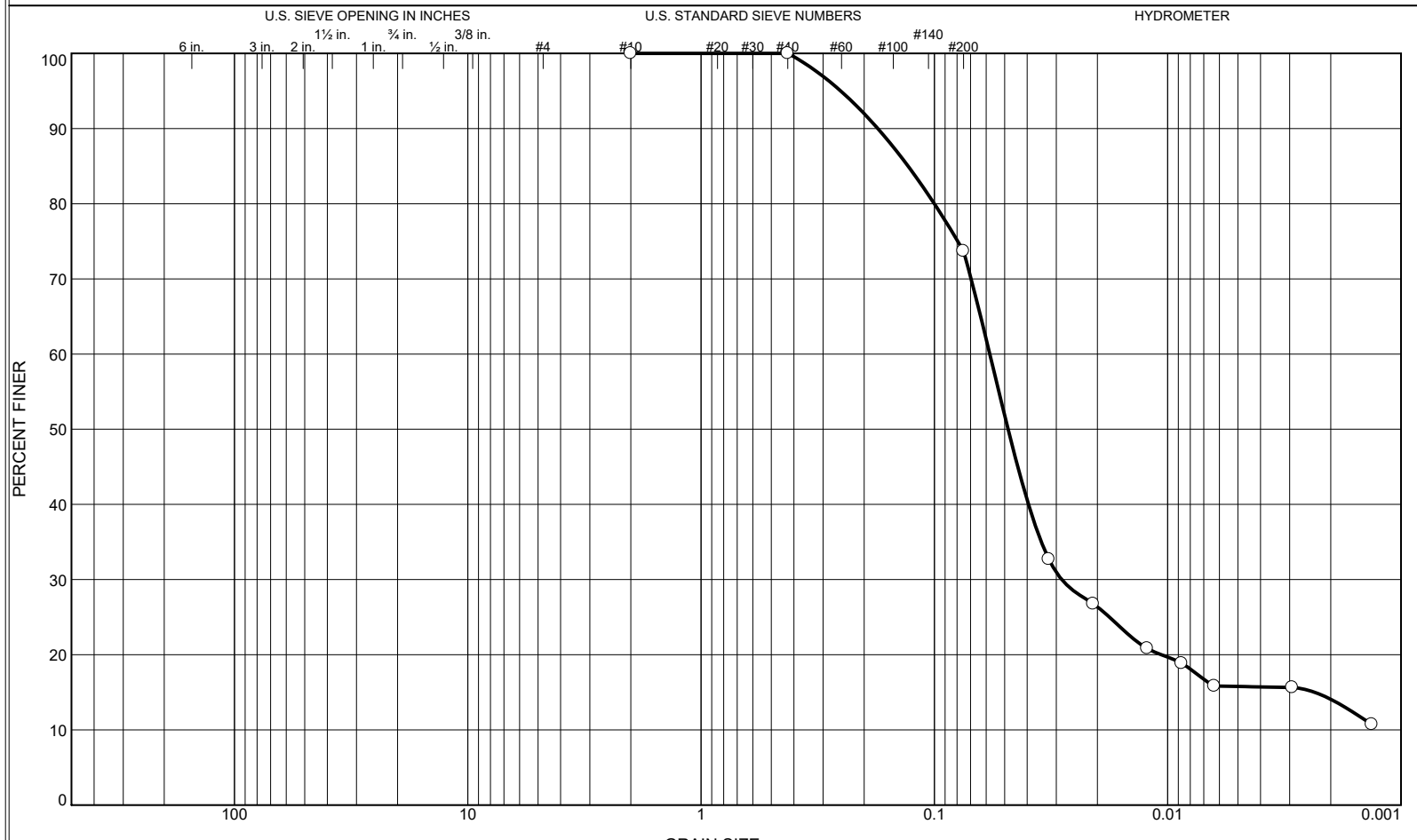
% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	1.0	28.0	71.0

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-12	Depth: 2-4	Sample Number: 2			

Client CPRA		
Project Breton Landbridge Marsh Creation(West)		
Project No. APS2008-G063		




# Particle Size Distribution Report

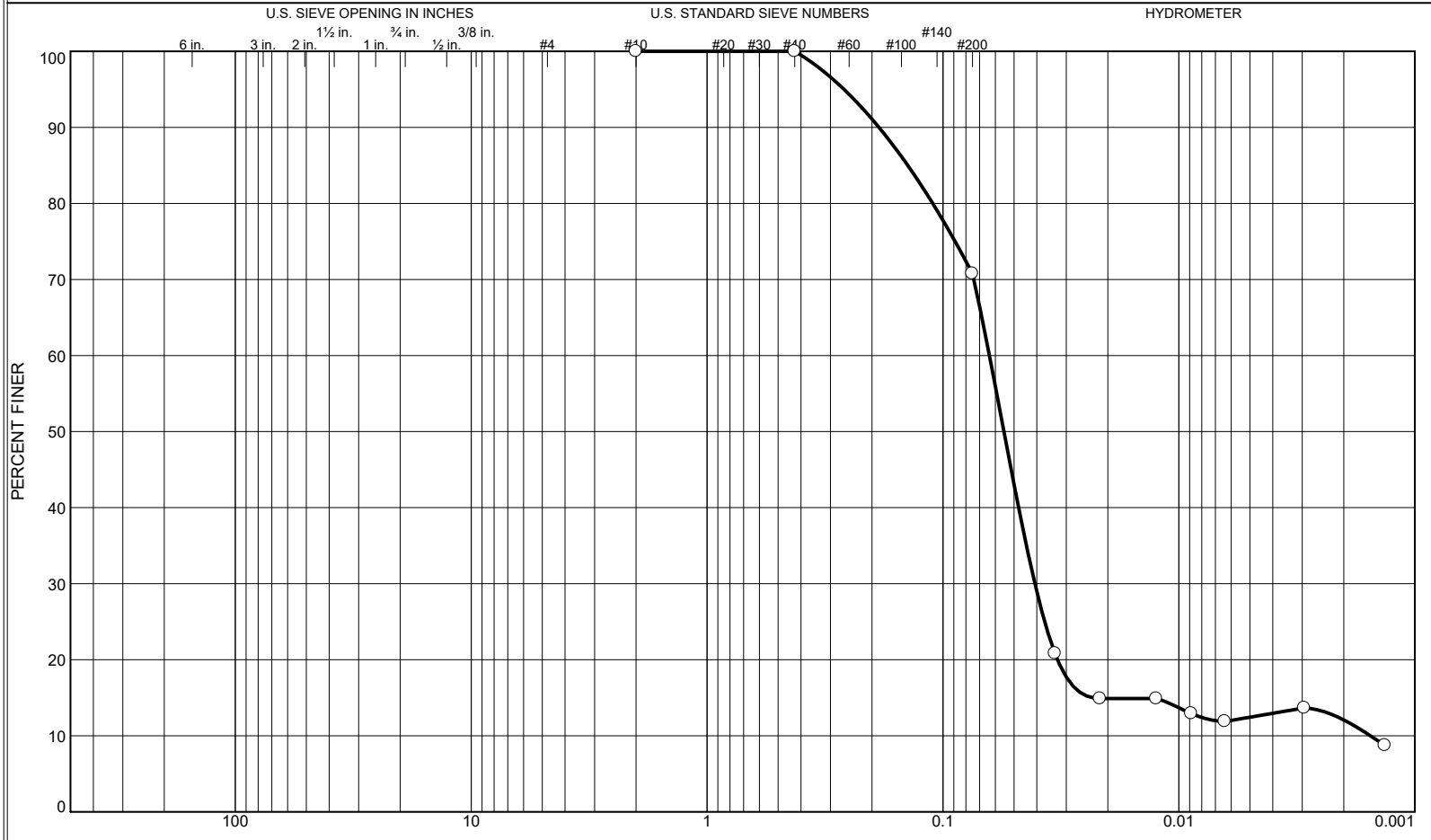


% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	26.3	57.9	15.8

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-12	Depth: 4-6	Sample Number: 3			

Client CPRA		
Project Breton Landbridge Marsh Creation(West)		
Project No. APS2008-G063		

# Particle Size Distribution Report

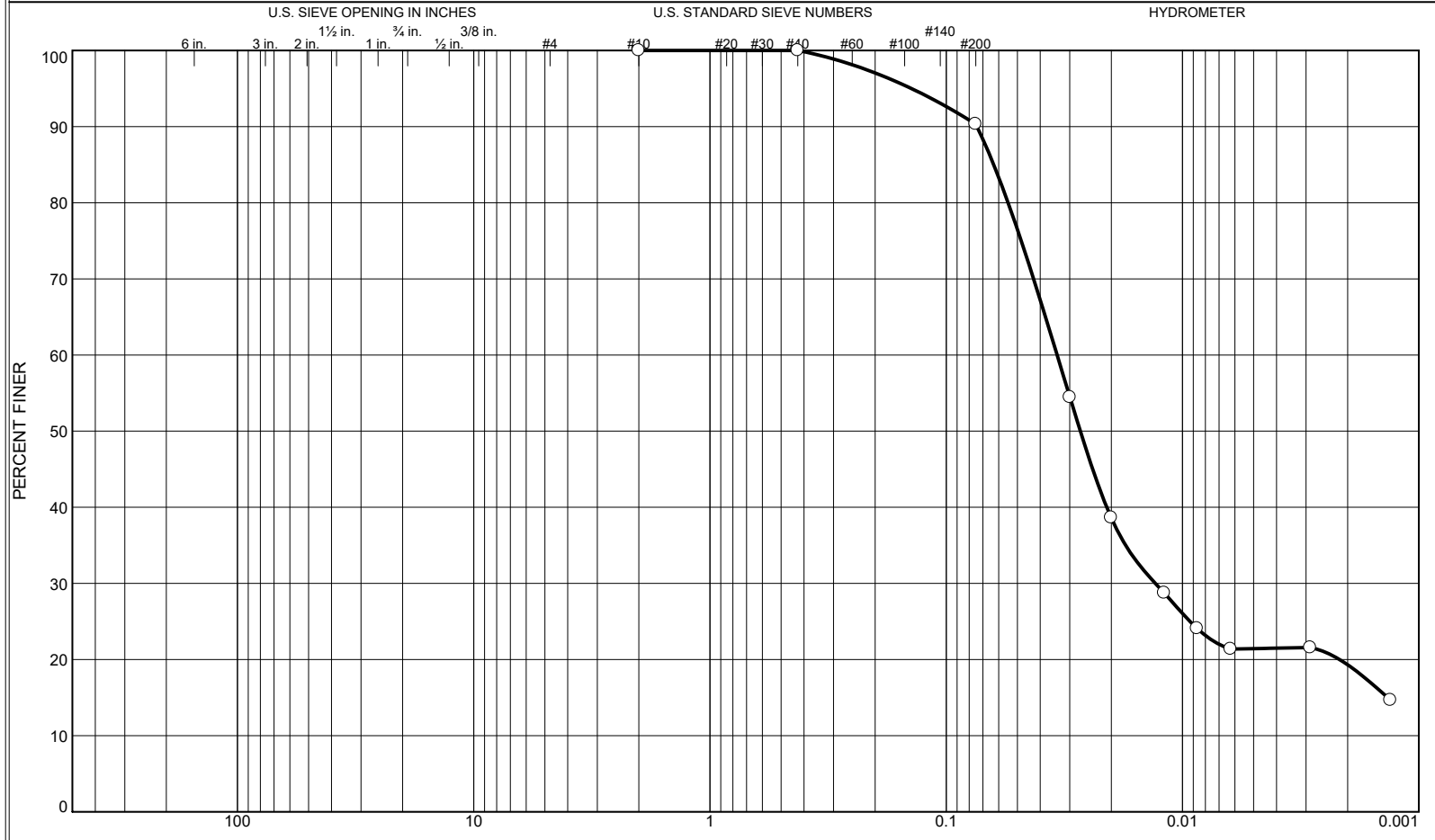


% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	29.2	58.4	12.4

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-12	Depth: 6-8	Sample Number: 4			


Client CPRA		
Project Breton Landbridge Marsh Creation(West)		
Project No. APS2008-G063		

# Particle Size Distribution Report

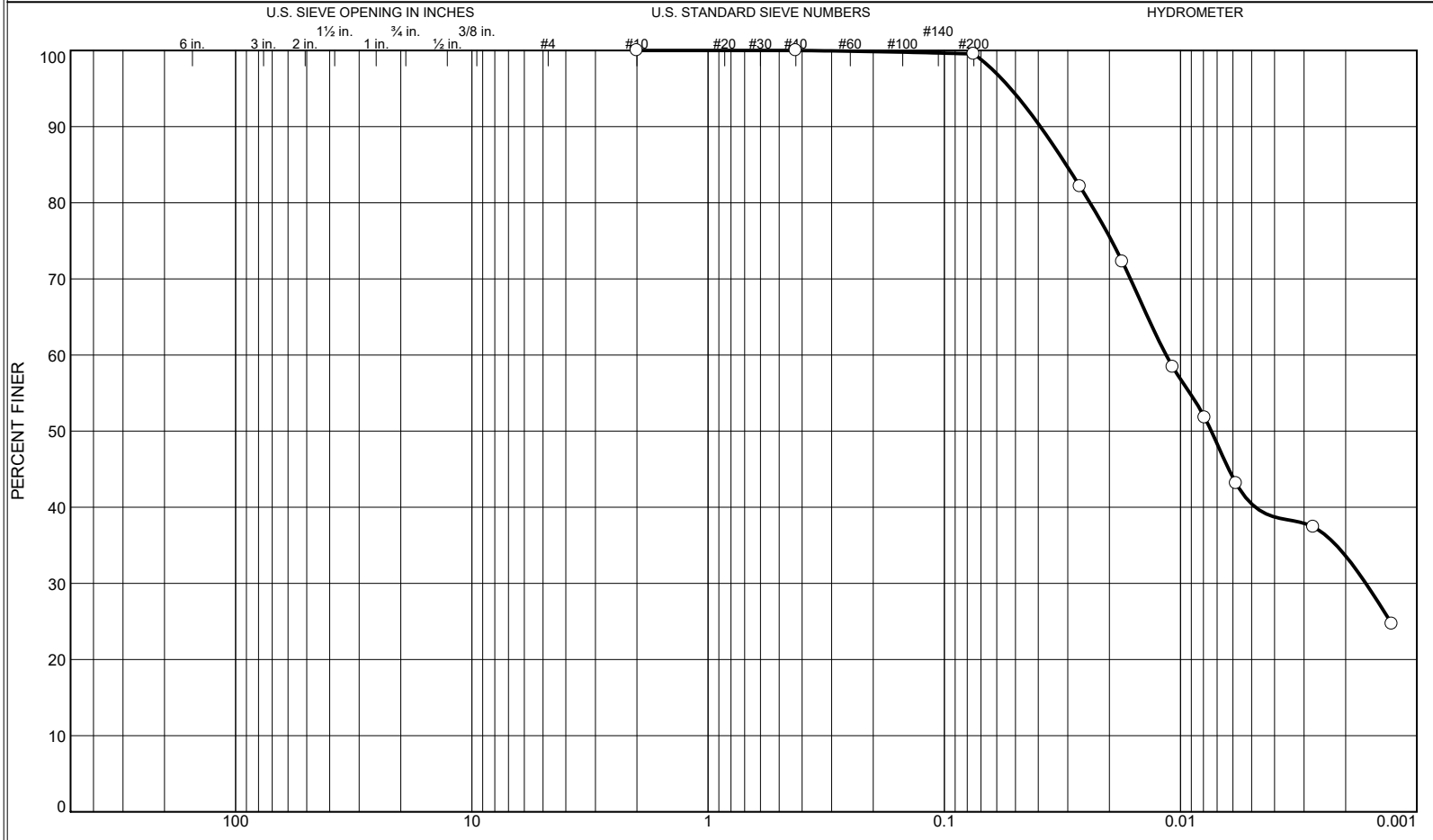


% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	9.7	68.9	21.4

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-12	Depth: 8-10	Sample Number: 5			


Client CPRA		
Project Breton Landbridge Marsh Creation(West)		
Project No. APS2008-G063		

# Particle Size Distribution Report

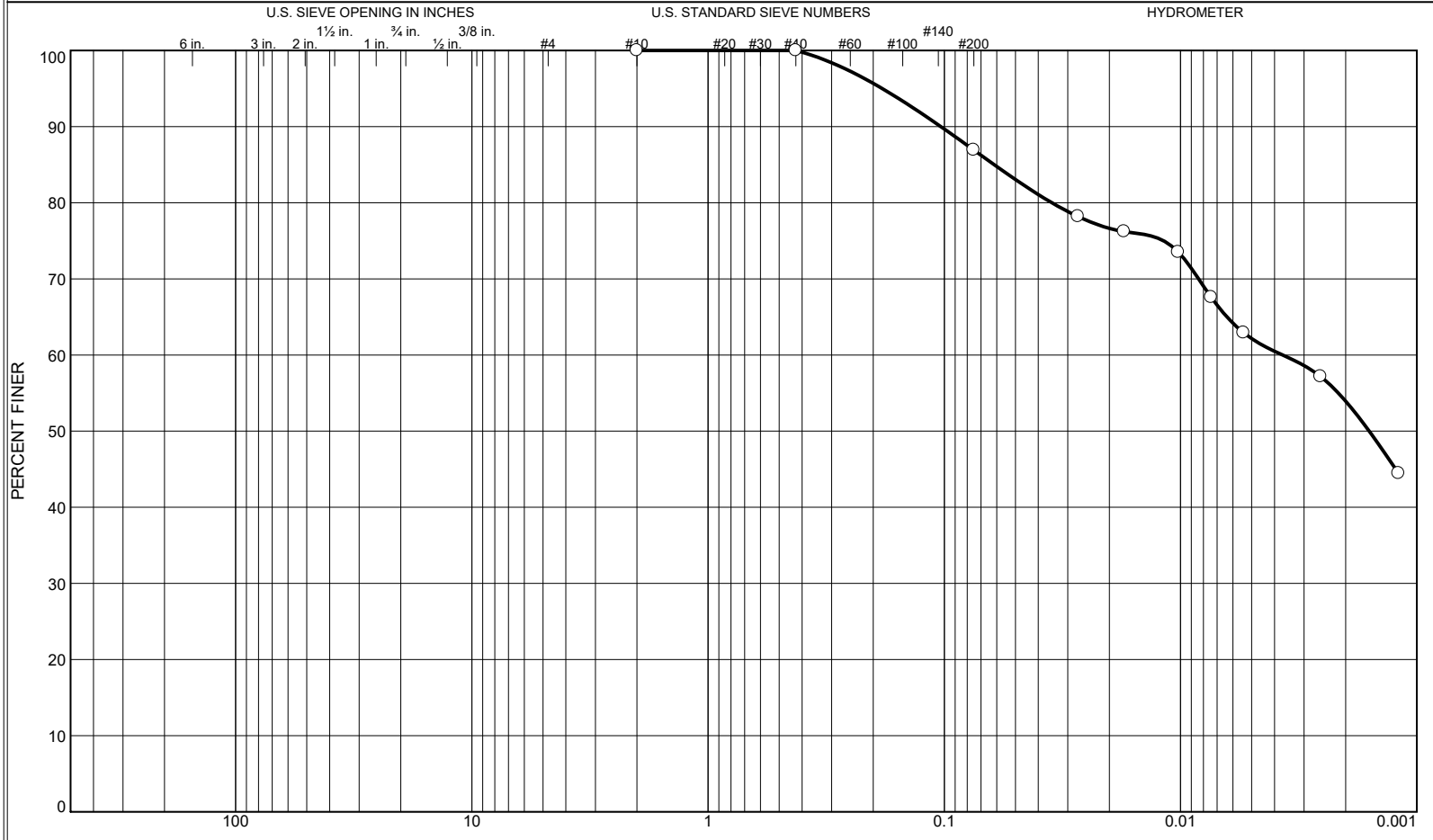


% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	0.5	59.1	40.4

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-12	Depth: 10-12	Sample Number: 6			

Client CPRA		
Project Breton Landbridge Marsh Creation(West)		
Project No. APS2008-G063		

# Particle Size Distribution Report

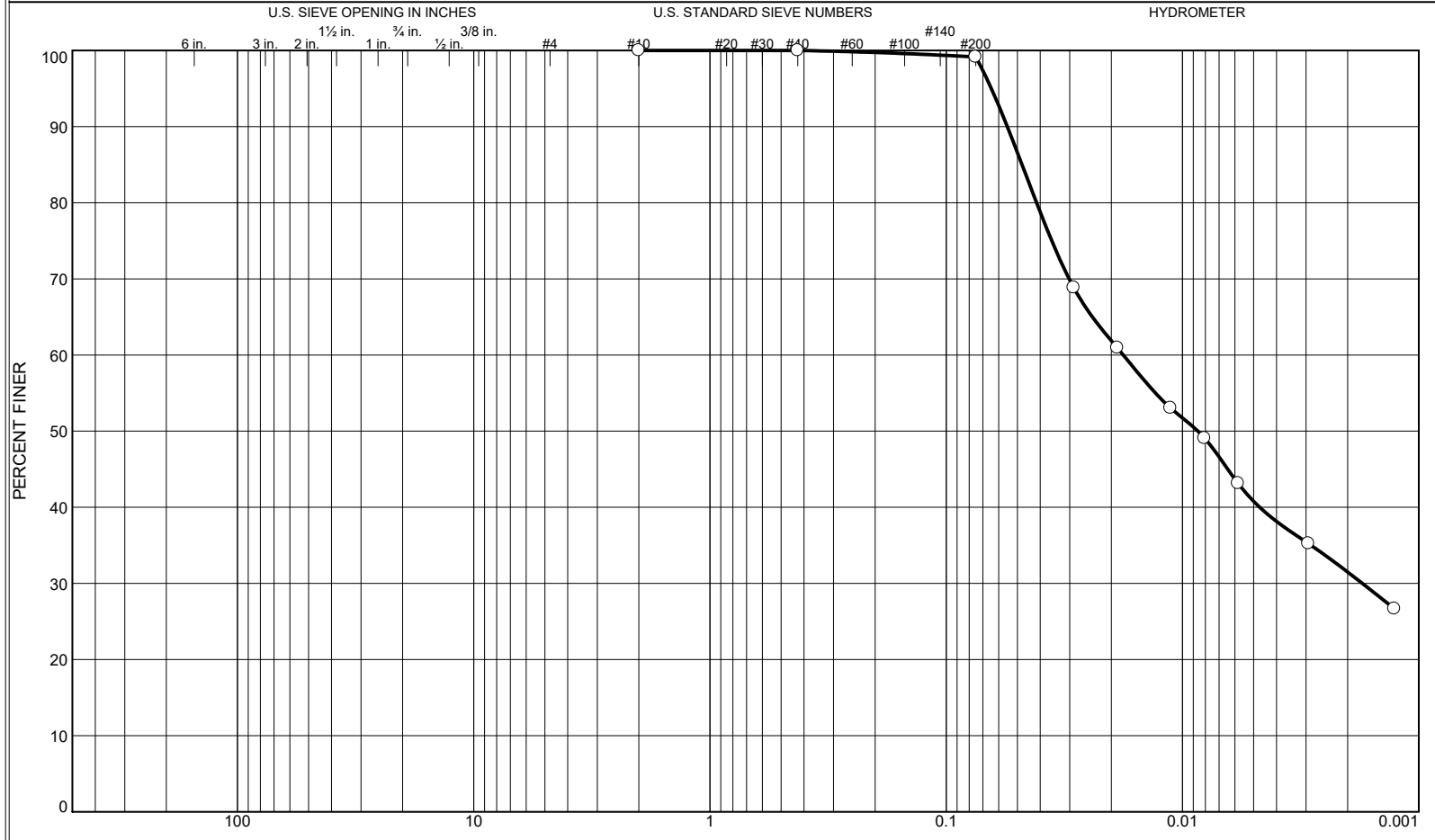


% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	13.1	24.7	62.2

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-12	Depth: 12-14	Sample Number: 7			

Client CPRA		
Project Breton Landbridge Marsh Creation(West)		
Project No. APS2008-G063		

# Particle Size Distribution Report

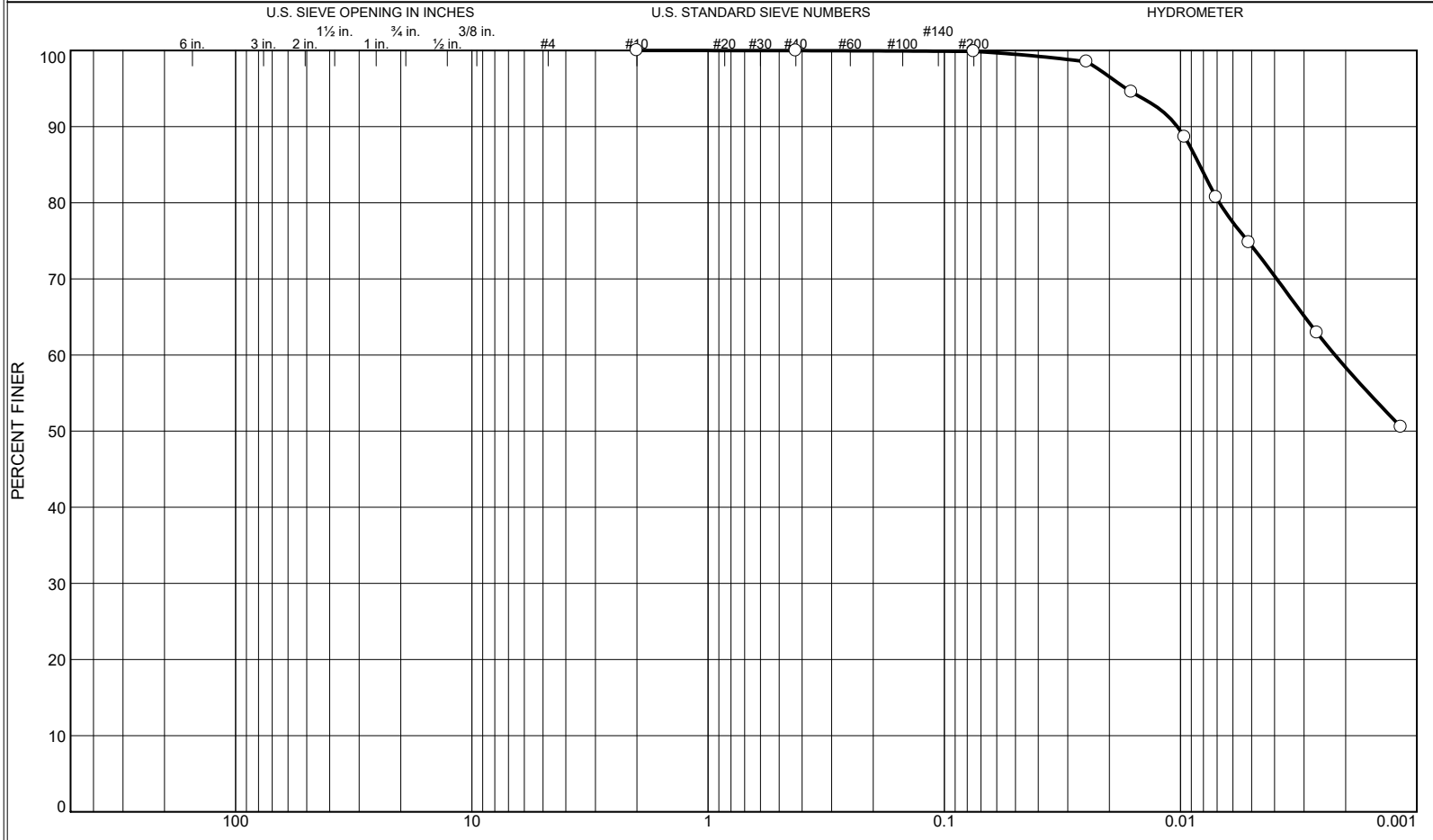


% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	0.9	58.3	40.8

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-12	Depth: 14-16	Sample Number: 8			

Client CPRA		
Project Breton Landbridge Marsh Creation(West)		
Project No. APS2008-G063		

# Particle Size Distribution Report

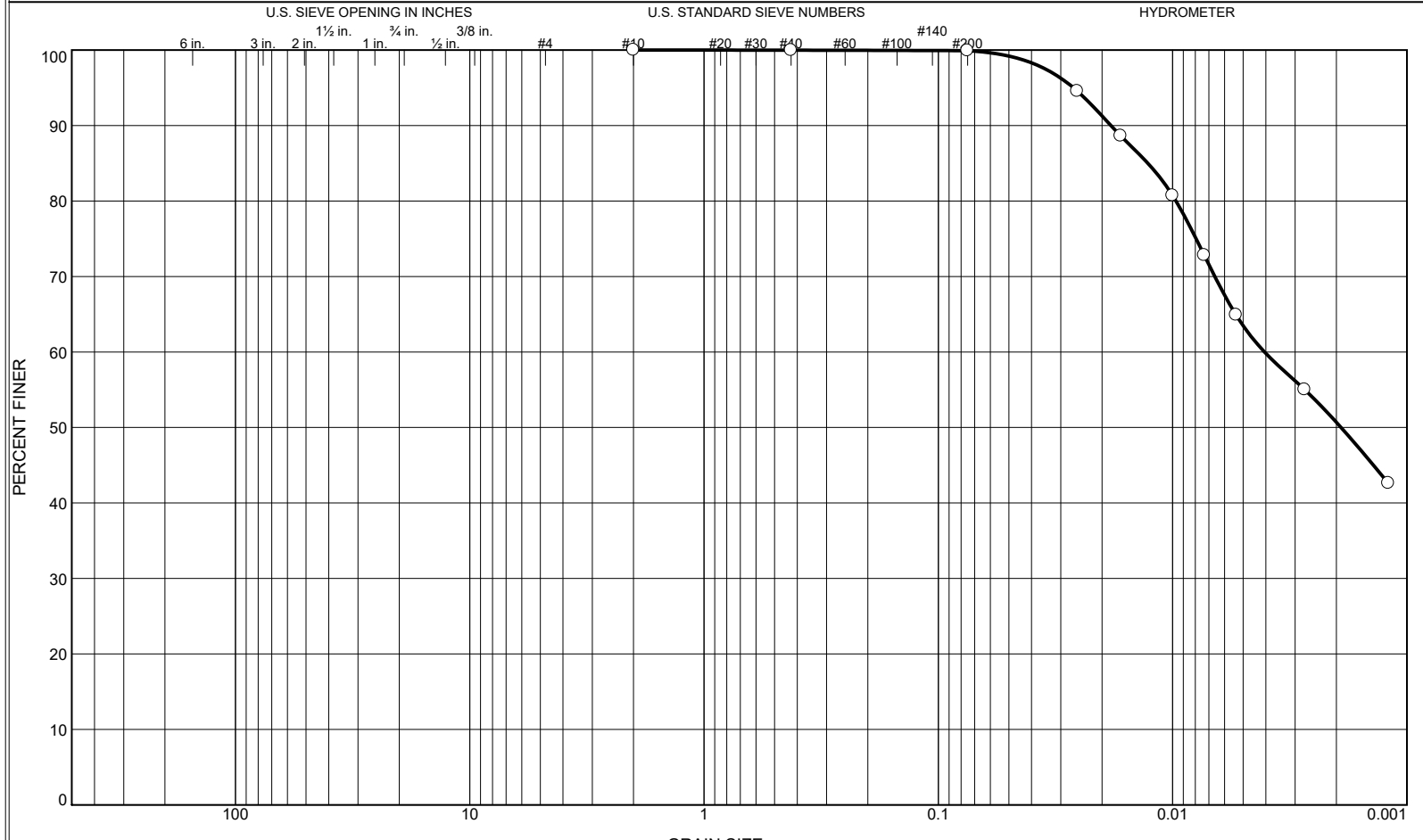


% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	0.1	25.6	74.3

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-12	Depth: 16-18	Sample Number: 9			


Client CPRA		
Project Breton Landbridge Marsh Creation(West)		
Project No. APS2008-G063		

# Particle Size Distribution Report



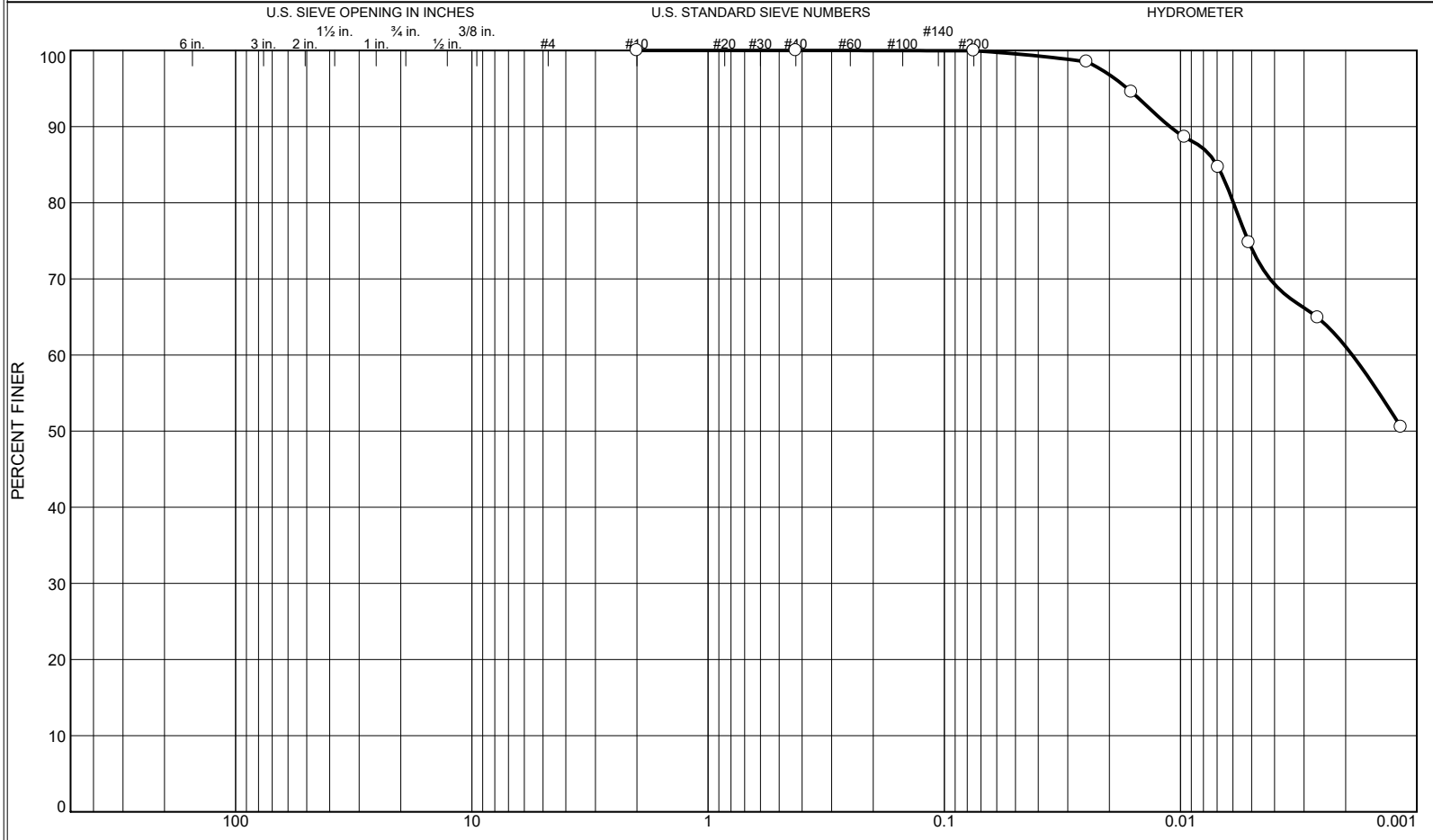
% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	0.1	36.4	63.5

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-12	Depth: 18-20	Sample Number: 10			

Client CPRA		
Project Breton Landbridge Marsh Creation(West)		
Project No. APS2008-G063		



# Particle Size Distribution Report



% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	0.0	26.0	74.0

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-12	Depth: 23-25	Sample Number: 11			

Client CPRA		
Project Breton Landbridge Marsh Creation(West)		
Project No. APS2008-G063		

# Particle Size Distribution Report

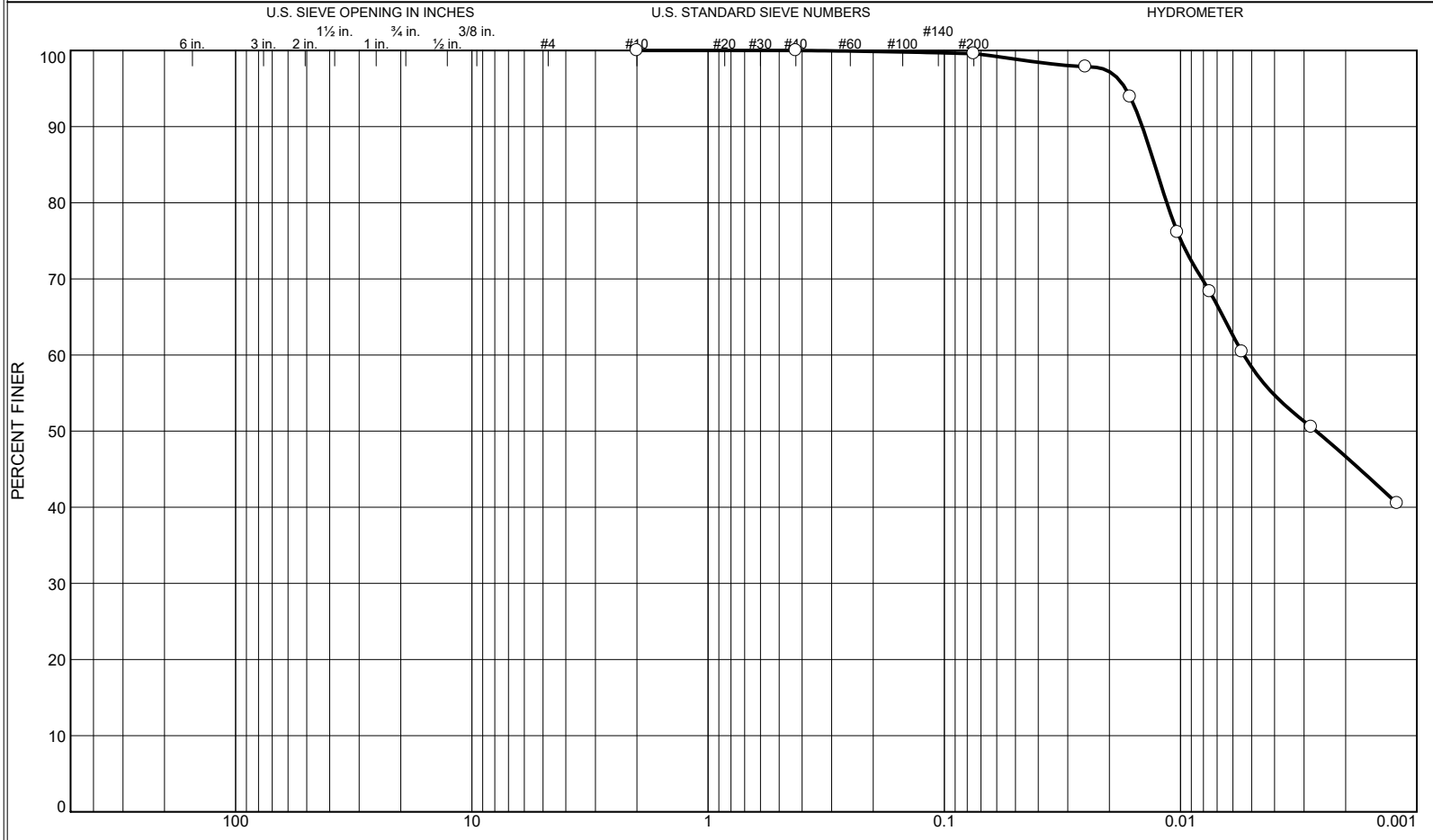


% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	4.9	76.6	18.5

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-13	Depth: 0-2	Sample Number: 1			

Client CPRA		
Project Breton Landbridge Marsh Creation(West)		
Project No. APS2008-G063		

# Particle Size Distribution Report

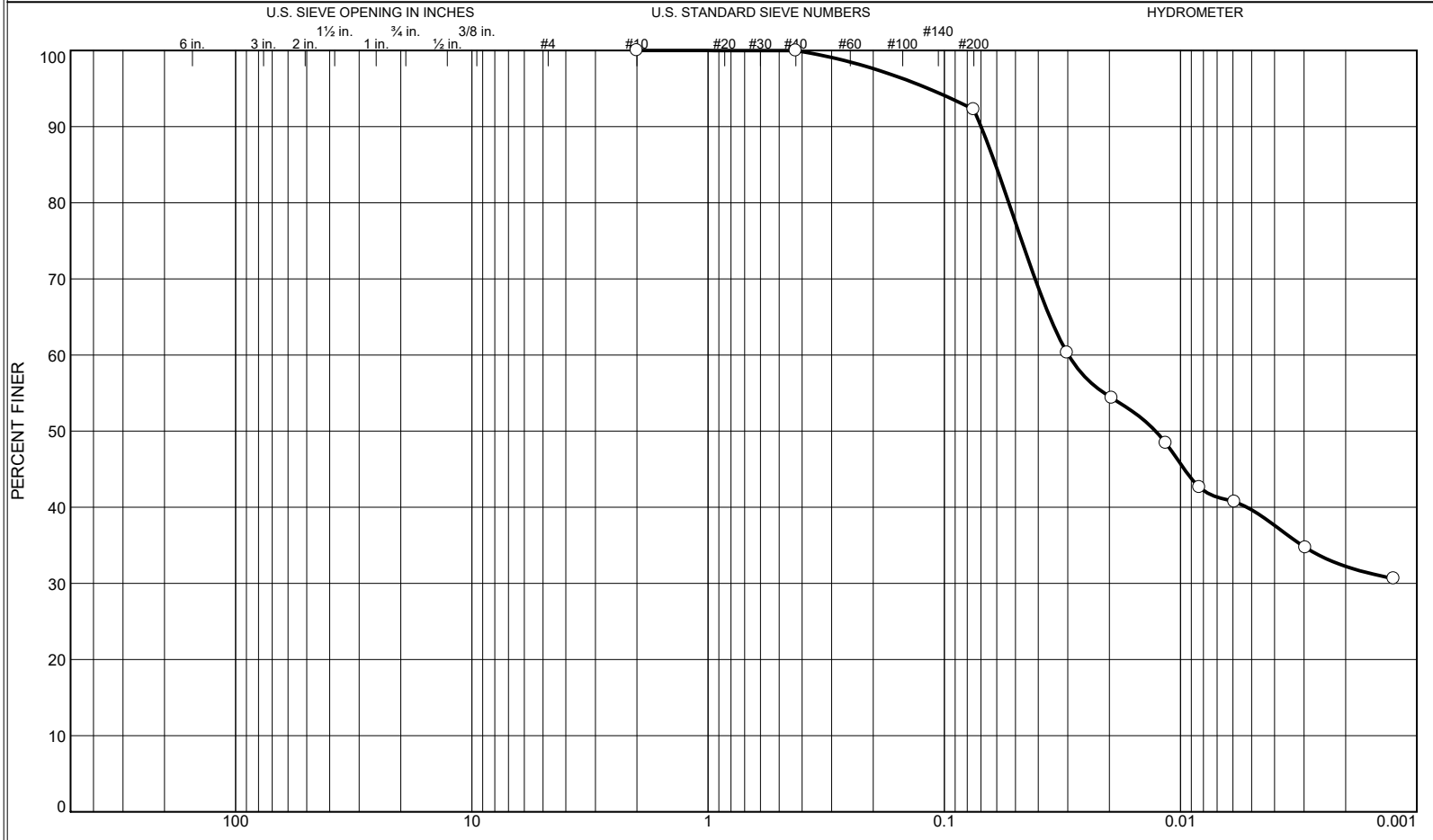


% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	0.4	41.2	58.4

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-13	Depth: 2-4	Sample Number: 2			


Client CPRA		
Project Breton Landbridge Marsh Creation(West)		
Project No. APS2008-G063		

# Particle Size Distribution Report

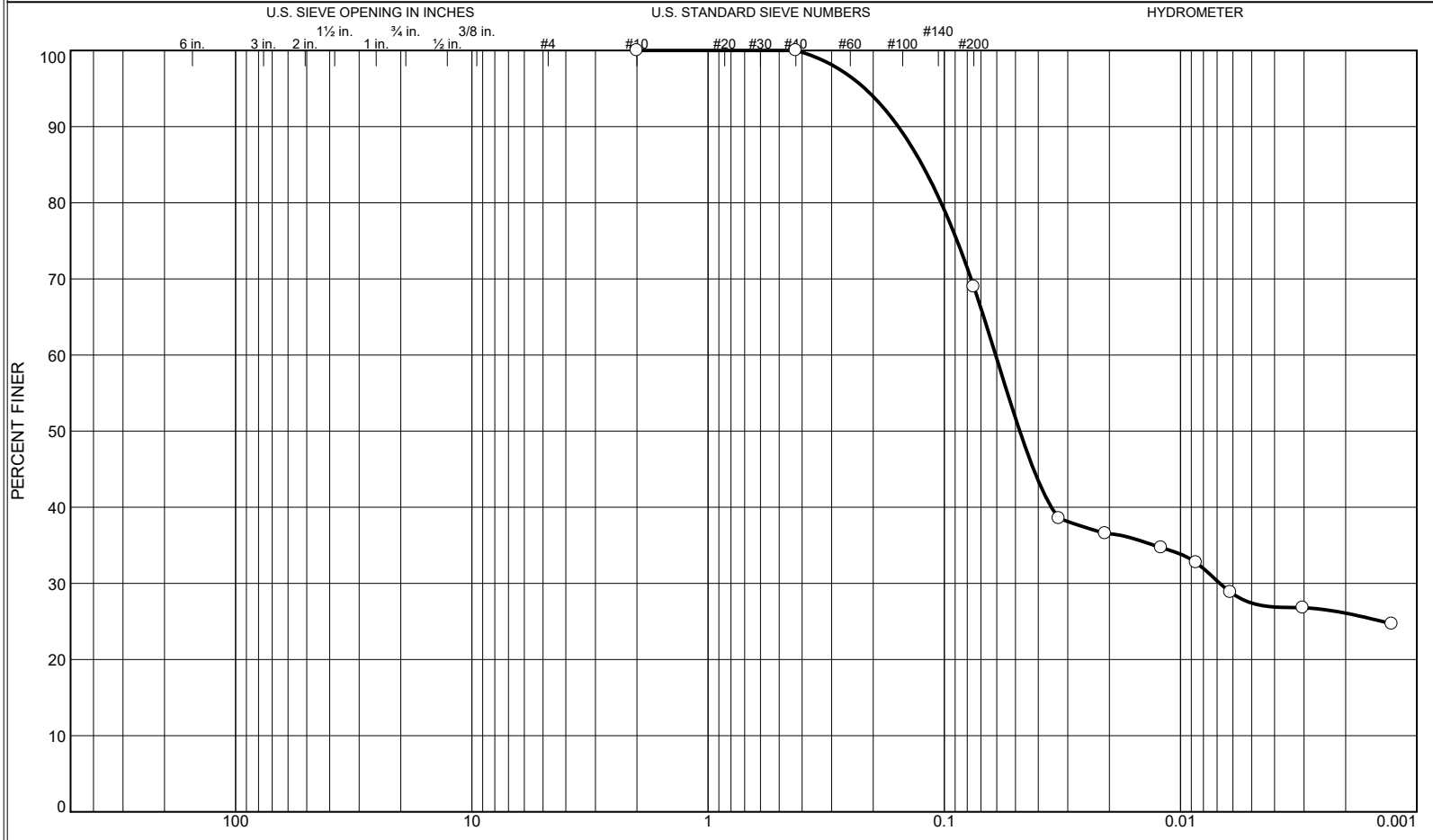


% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	7.8	52.5	39.7

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-13	Depth: 4-6	Sample Number: 3			

Client CPRA		
Project Breton Landbridge Marsh Creation(West)		
Project No. APS2008-G063		

# Particle Size Distribution Report

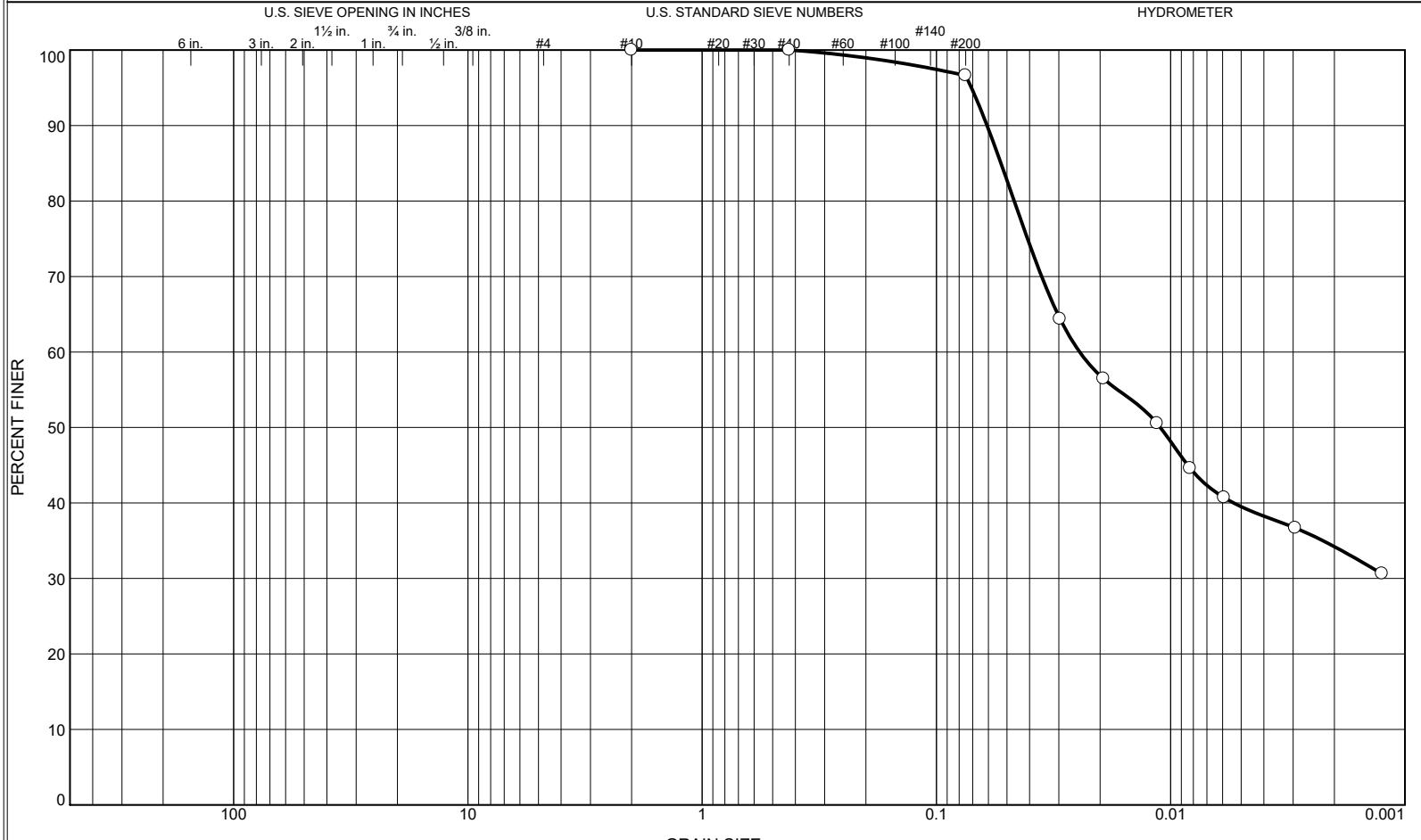


% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	31.0	41.6	27.4

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-13	Depth: 6-8	Sample Number: 4			

Client CPRA		
Project Breton Landbridge Marsh Creation(West)		
Project No. APS2008-G063		

# Particle Size Distribution Report

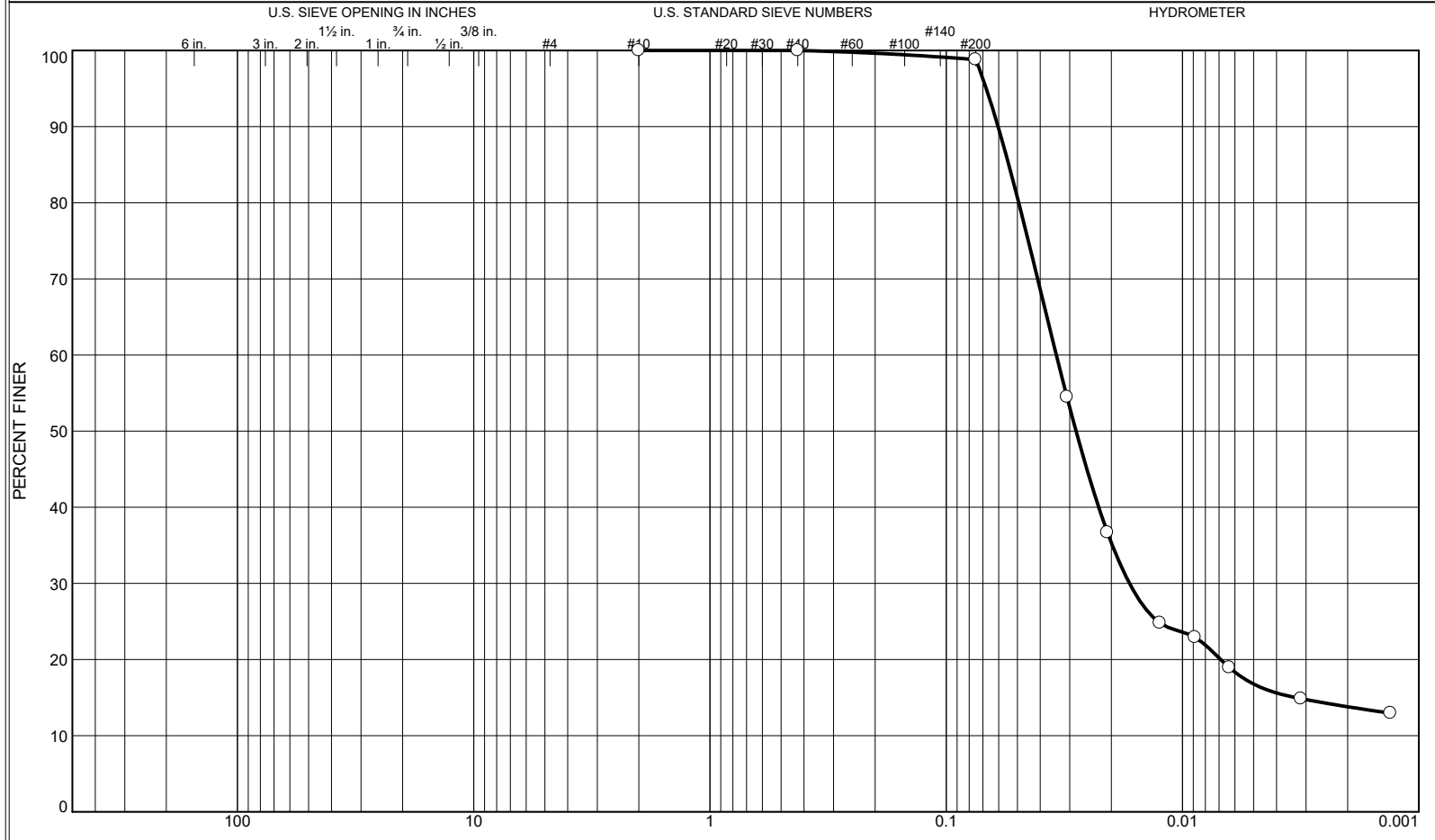


% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	3.4	57.1	39.5

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-13	Depth: 8-10	Sample Number: 5			


Client CPRA		
Project Breton Landbridge Marsh Creation(West)		
Project No. APS2008-G063		

# Particle Size Distribution Report

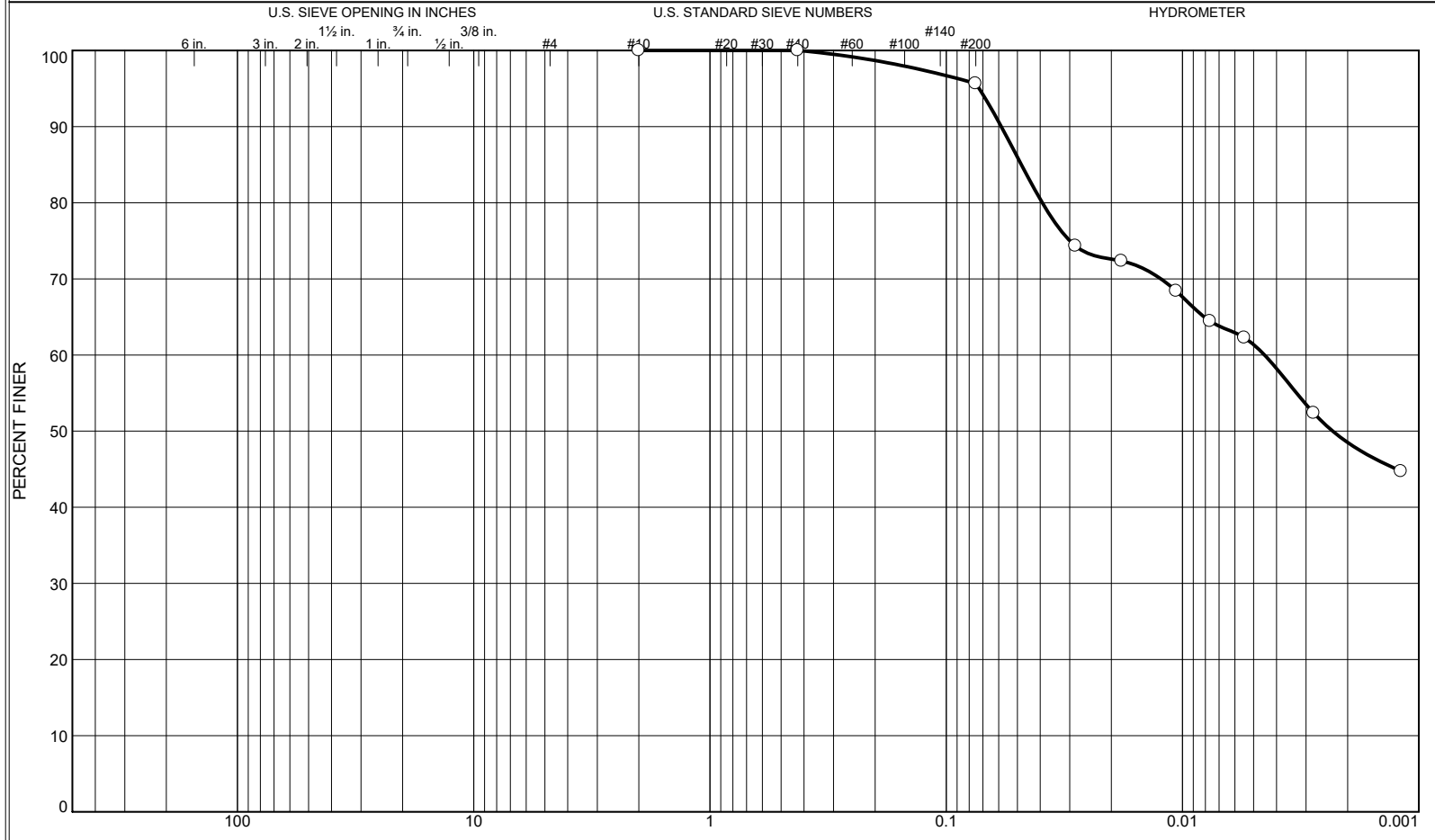


% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	1.2	82.0	16.8

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-13	Depth: 10-12	Sample Number: 6			


Client CPRA		
Project Breton Landbridge Marsh Creation(West)		
Project No. APS2008-G063		

# Particle Size Distribution Report



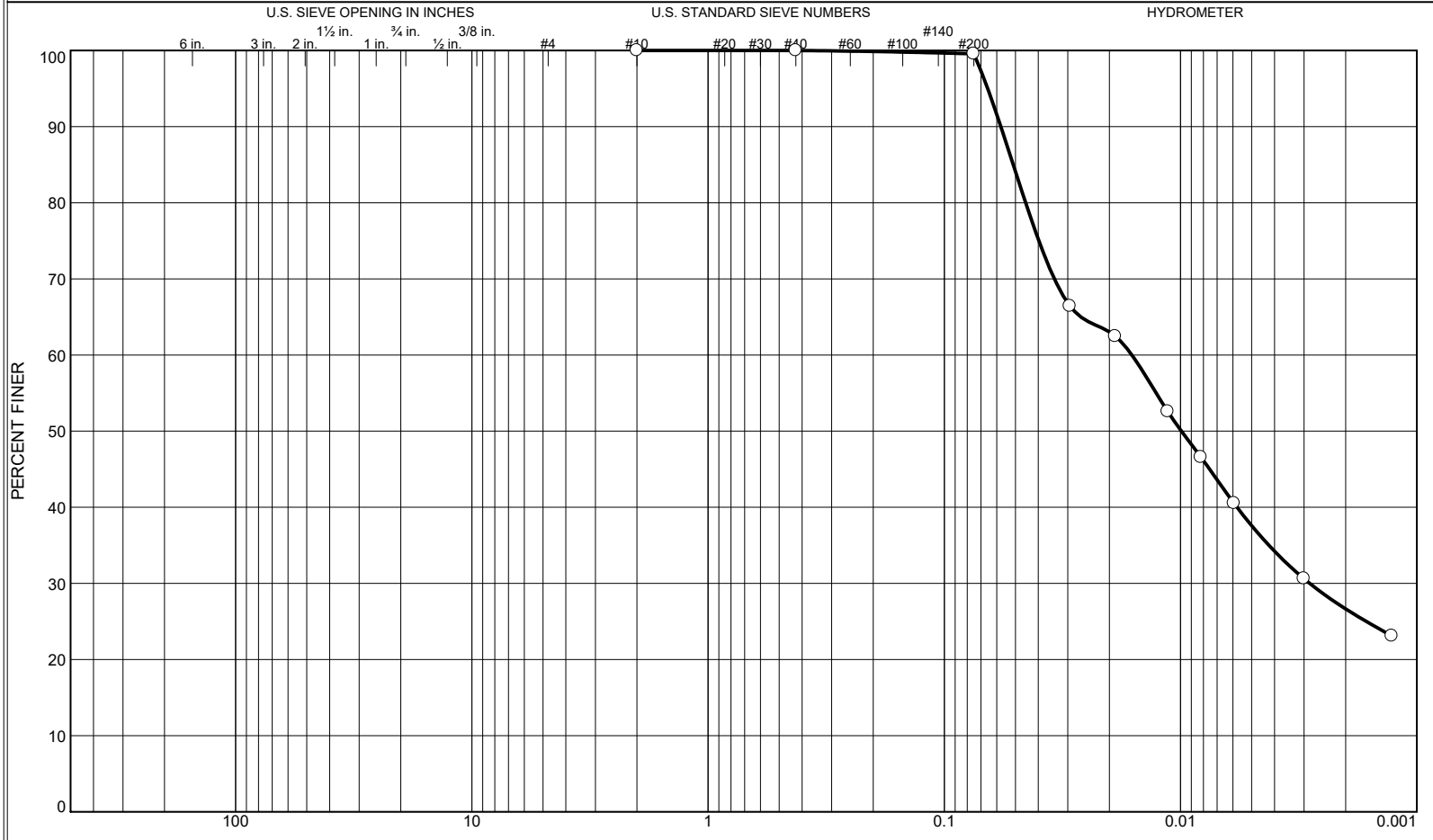
% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	4.3	34.3	61.4

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-13	Depth: 12-14	Sample Number: 7			

Client CPRA		
Project Breton Landbridge Marsh Creation(West)		
Project No. APS2008-G063		



# Particle Size Distribution Report

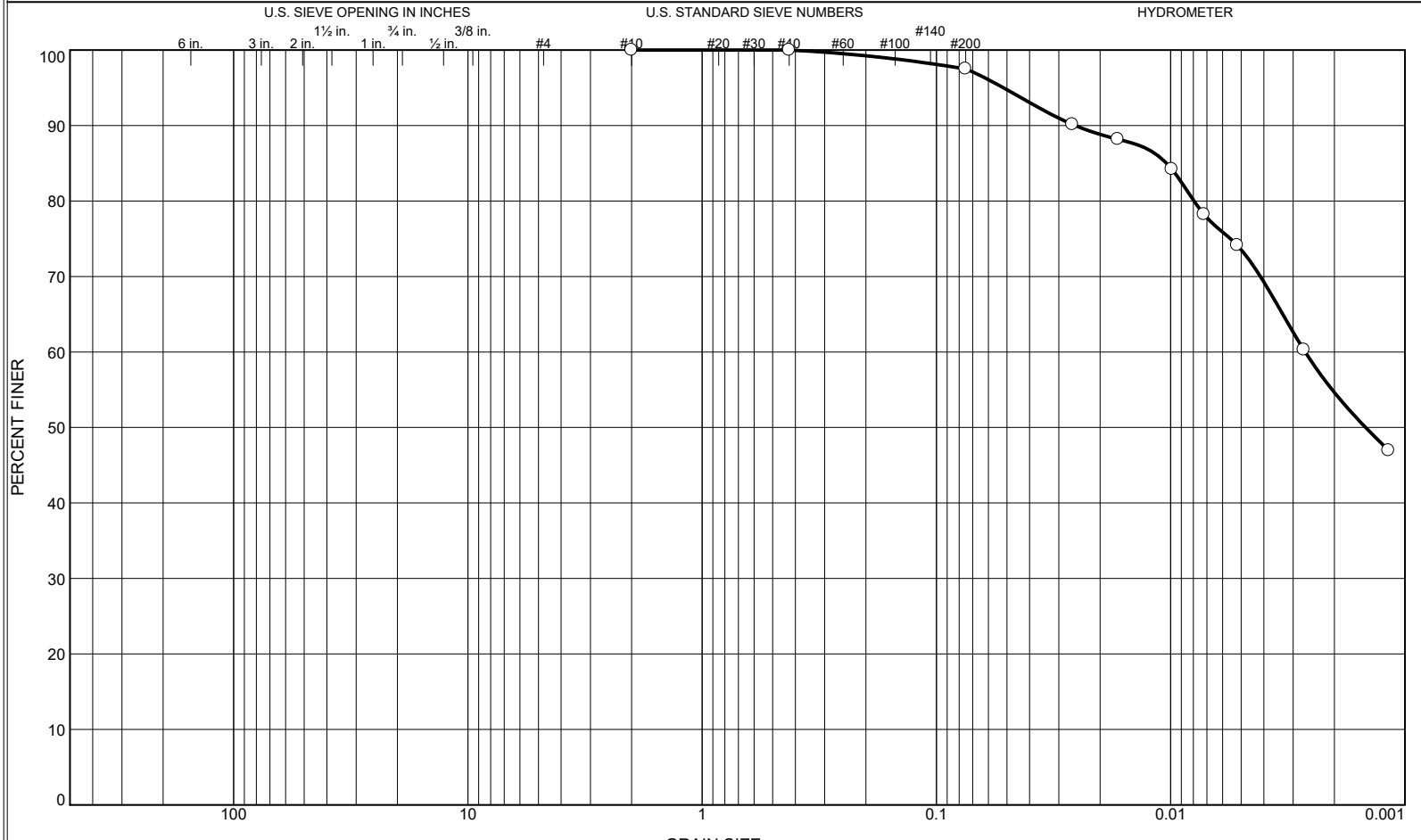


% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	0.4	62.0	37.6

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-13	Depth: 14-16	Sample Number: 8			

Client CPRA		
Project Breton Landbridge Marsh Creation(West)		
Project No. APS2008-G063		

# Particle Size Distribution Report



% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	2.5	23.9	73.6

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-13	Depth: 16-18	Sample Number: 9			

Client CPRA		
Project Breton Landbridge Marsh Creation(West)		
Project No. APS2008-G063		

# Particle Size Distribution Report

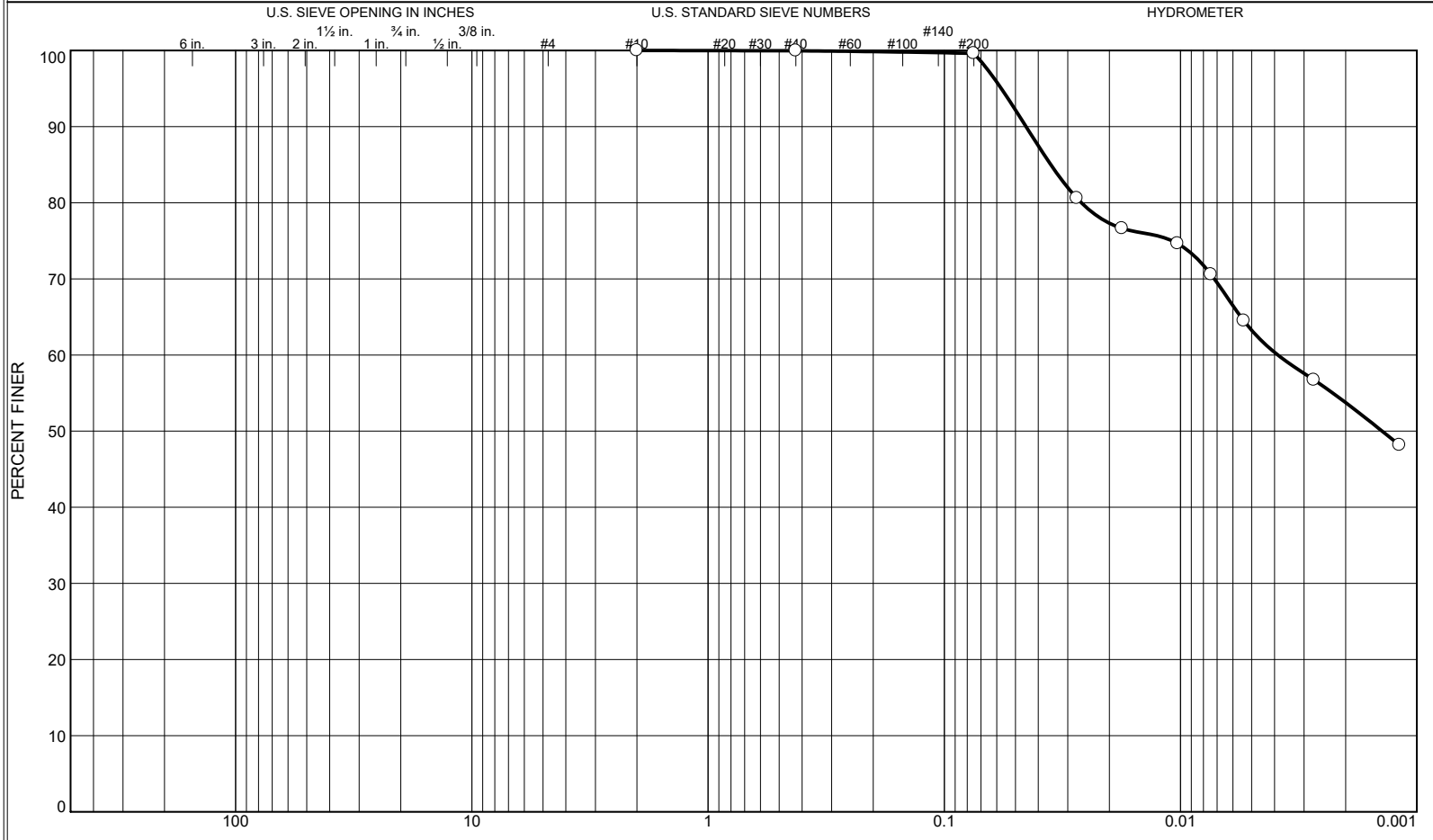


% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	0.4	15.4	84.2

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-13	Depth: 18-20	Sample Number: 10			


Client CPRA		
Project Breton Landbridge Marsh Creation(West)		
Project No. APS2008-G063		

# Particle Size Distribution Report

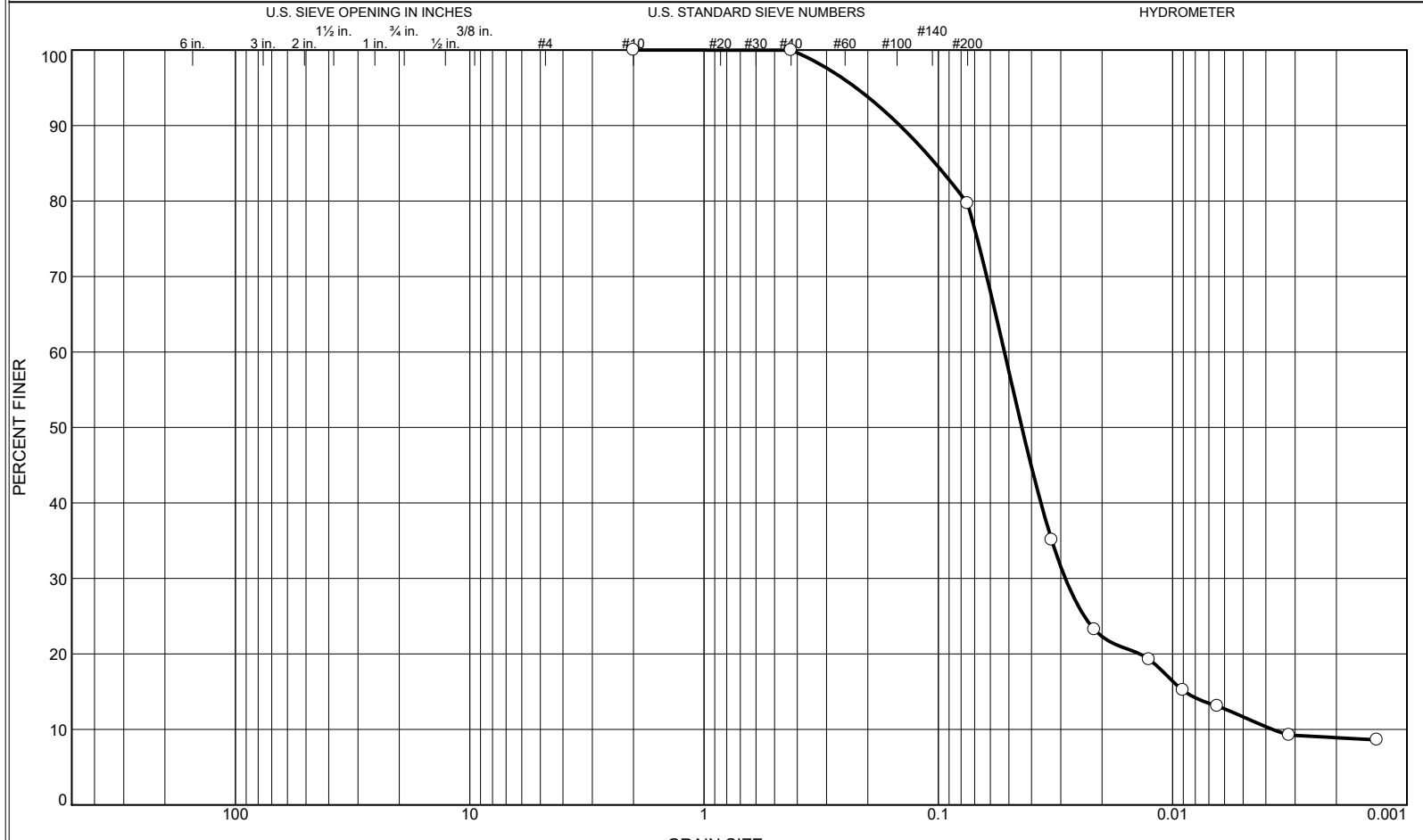


% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	0.4	36.4	63.2

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-13	Depth: 23-25	Sample Number: 11			


Client CPRA		
Project Breton Landbridge Marsh Creation(West)		
Project No. APS2008-G063		

# Particle Size Distribution Report

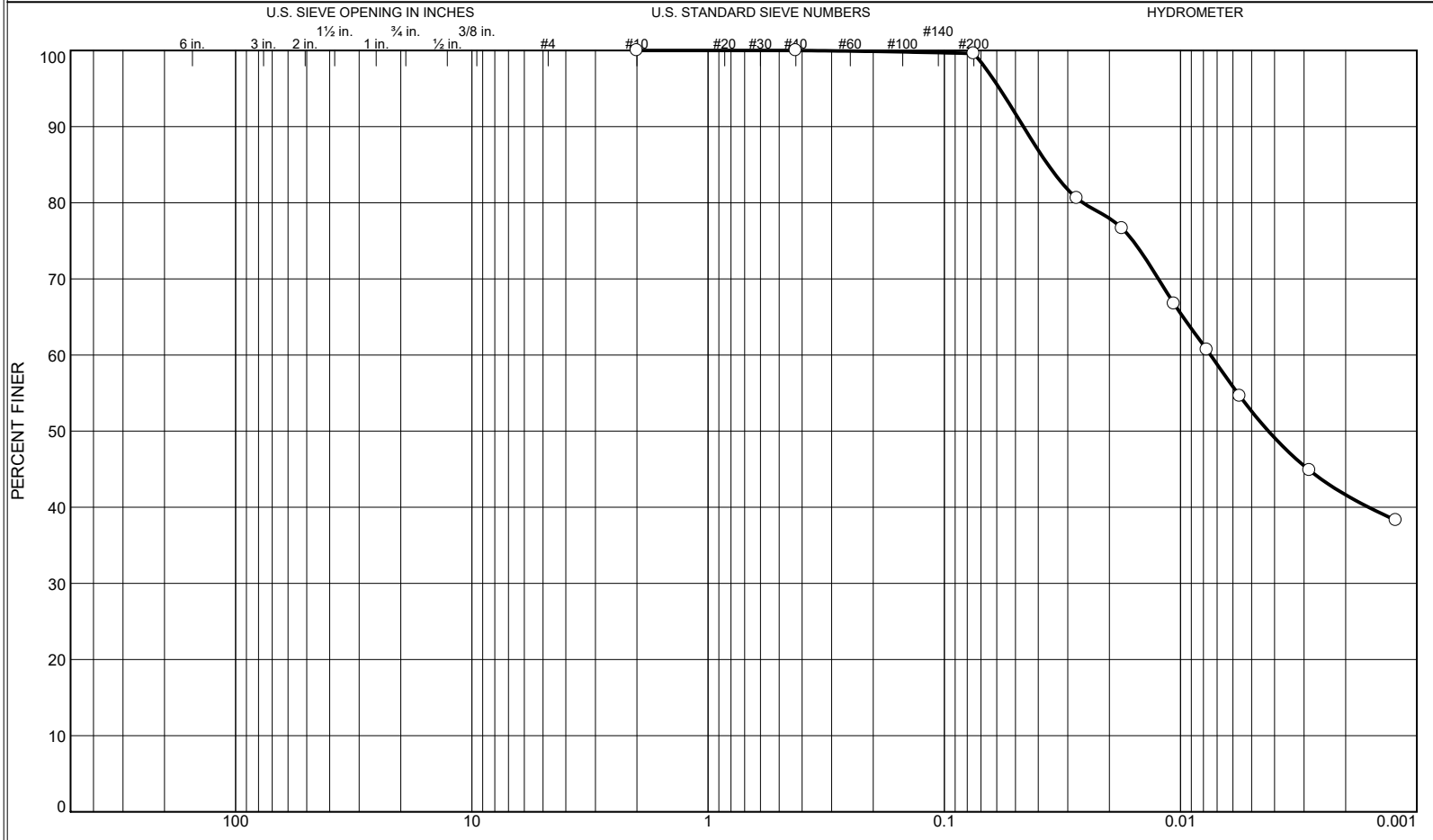


% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	20.3	68.0	11.7

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-14	Depth: 0-2	Sample Number: 1			

Client CPRA		
Project Breton Landbridge Marsh Creation(West)		
Project No. APS2008-G063		

# Particle Size Distribution Report

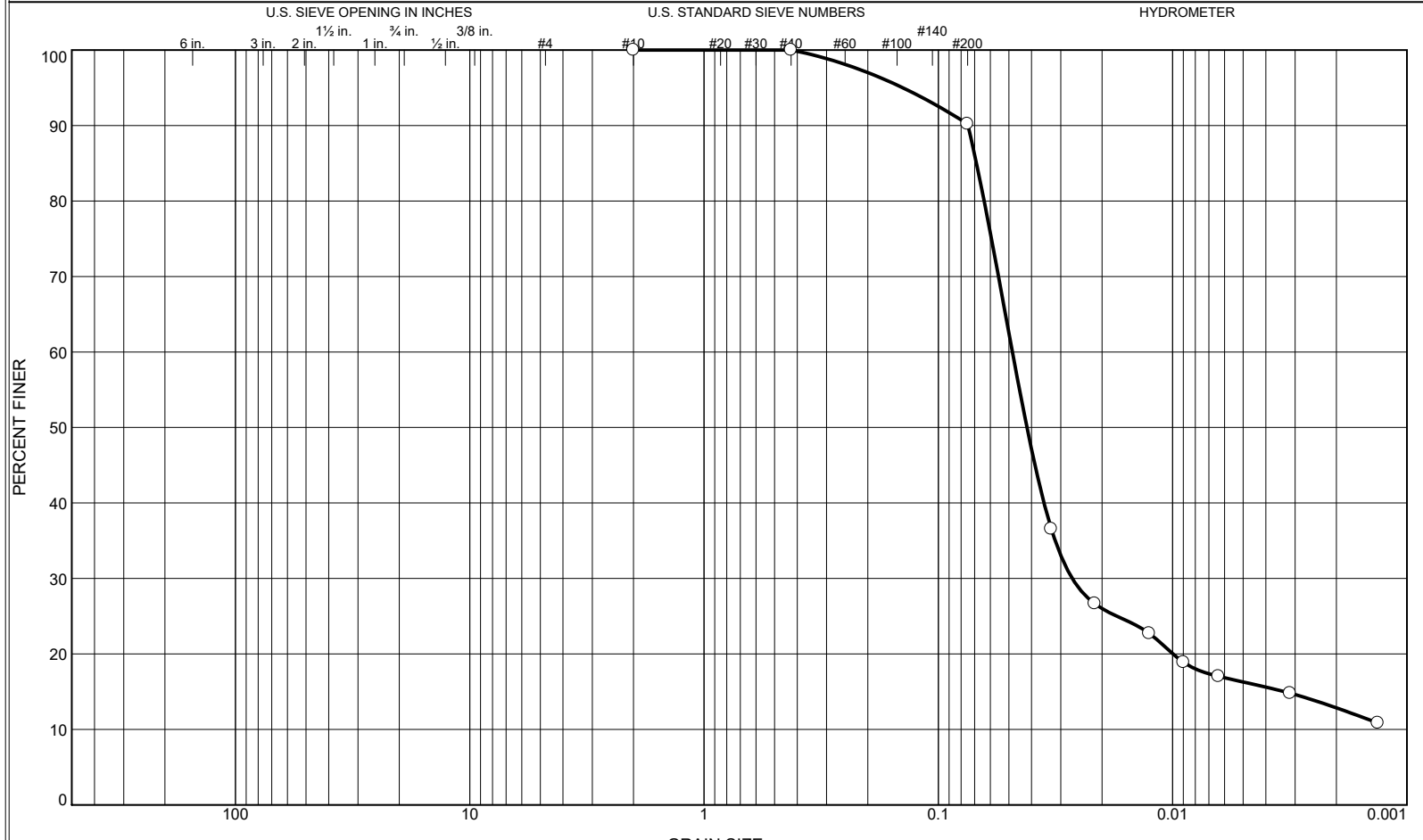


% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	0.4	47.0	52.6

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-14	Depth: 2-4	Sample Number: 2			


Client CPRA		
Project Breton Landbridge Marsh Creation(West)		
Project No. APS2008-G063		

# Particle Size Distribution Report

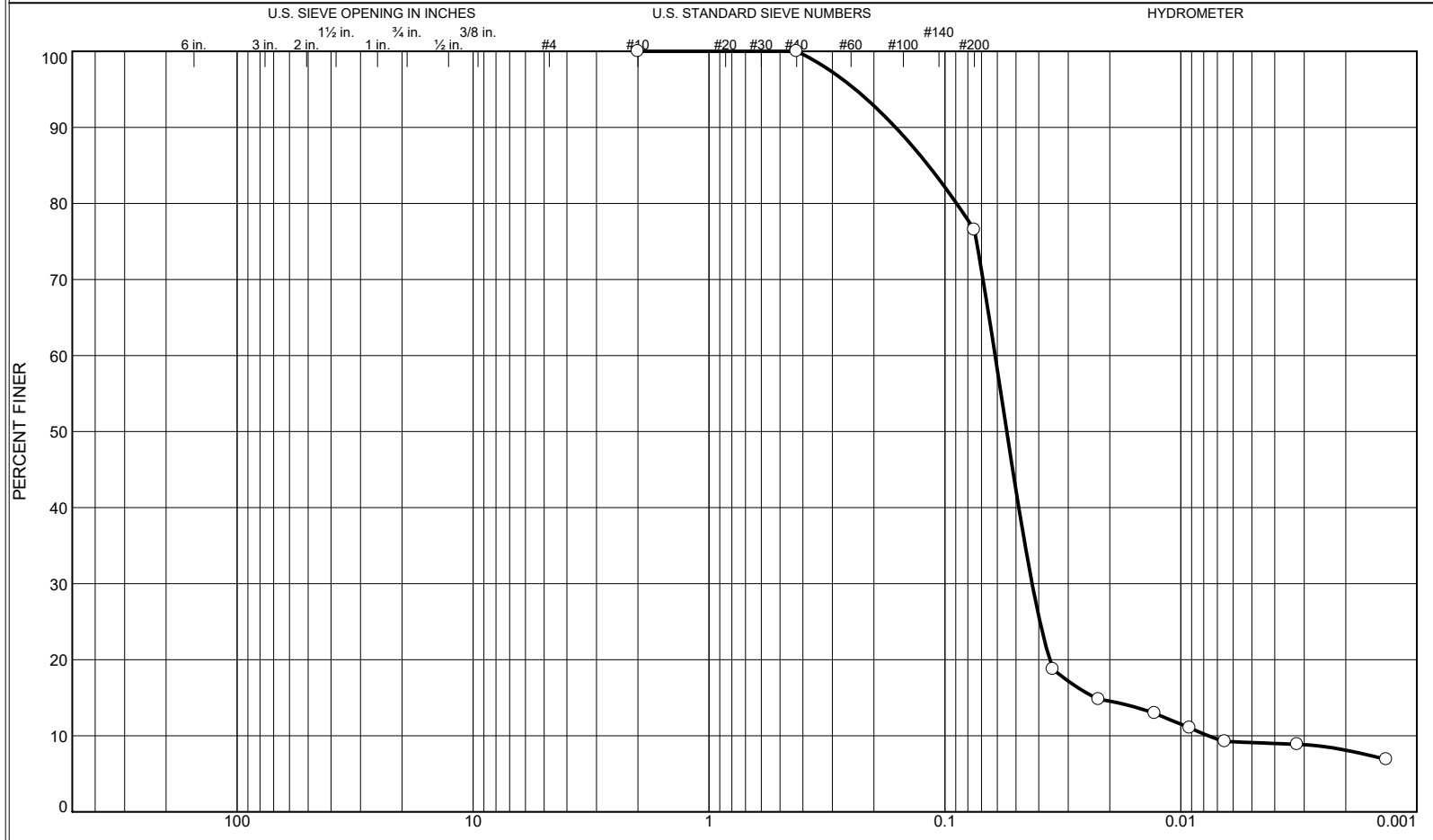


% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	9.8	73.9	16.3

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-14	Depth: 4-6	Sample Number: 3			


Client CPRA		
Project Breton Landbridge Marsh Creation(West)		
Project No. APS2008-G063		

# Particle Size Distribution Report



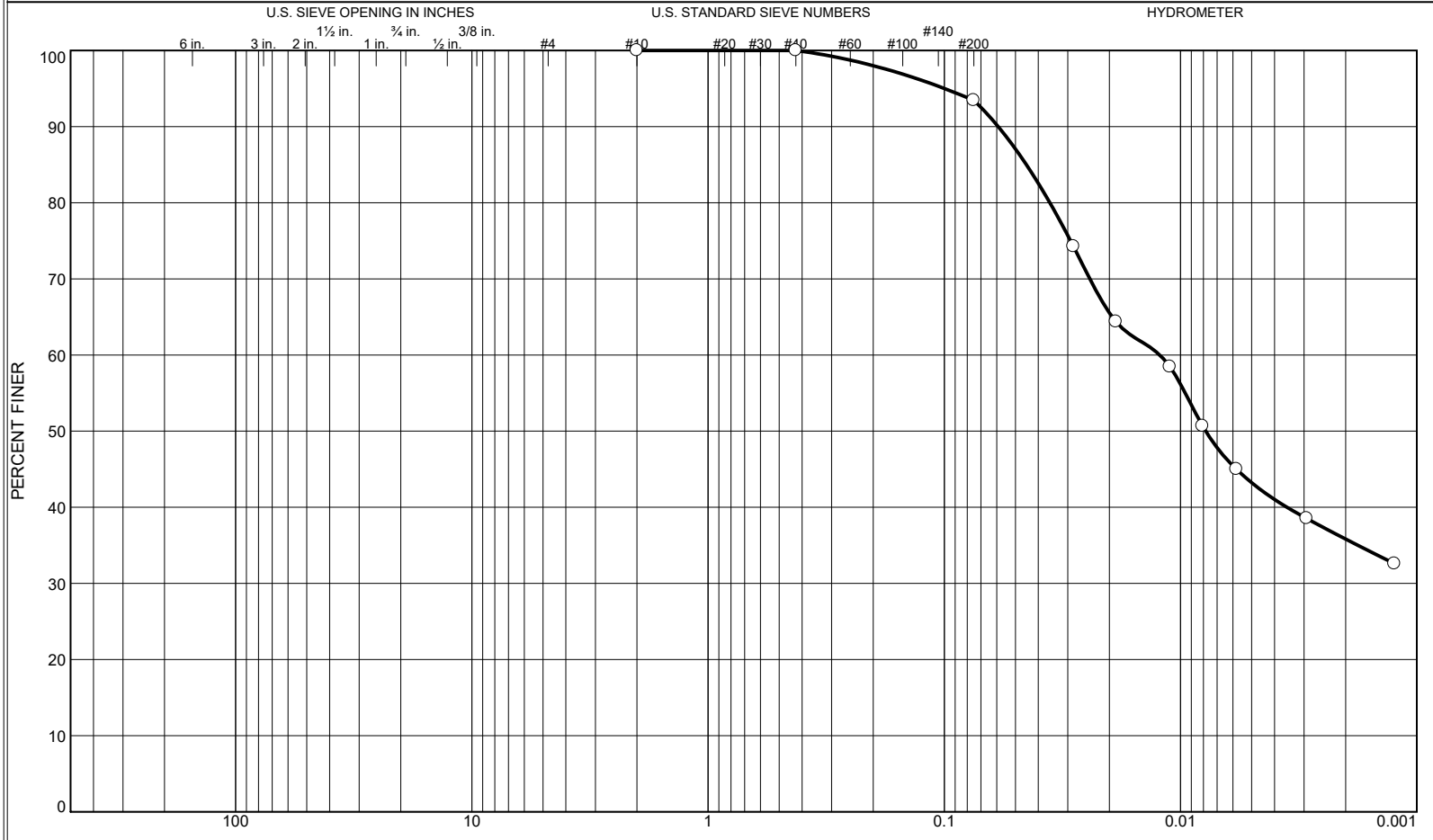
% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	23.5	67.4	9.1

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-14	Depth: 6-8	Sample Number: 4			

Client CPRA		
Project Breton Landbridge Marsh Creation(West)		
Project No. APS2008-G063		



# Particle Size Distribution Report

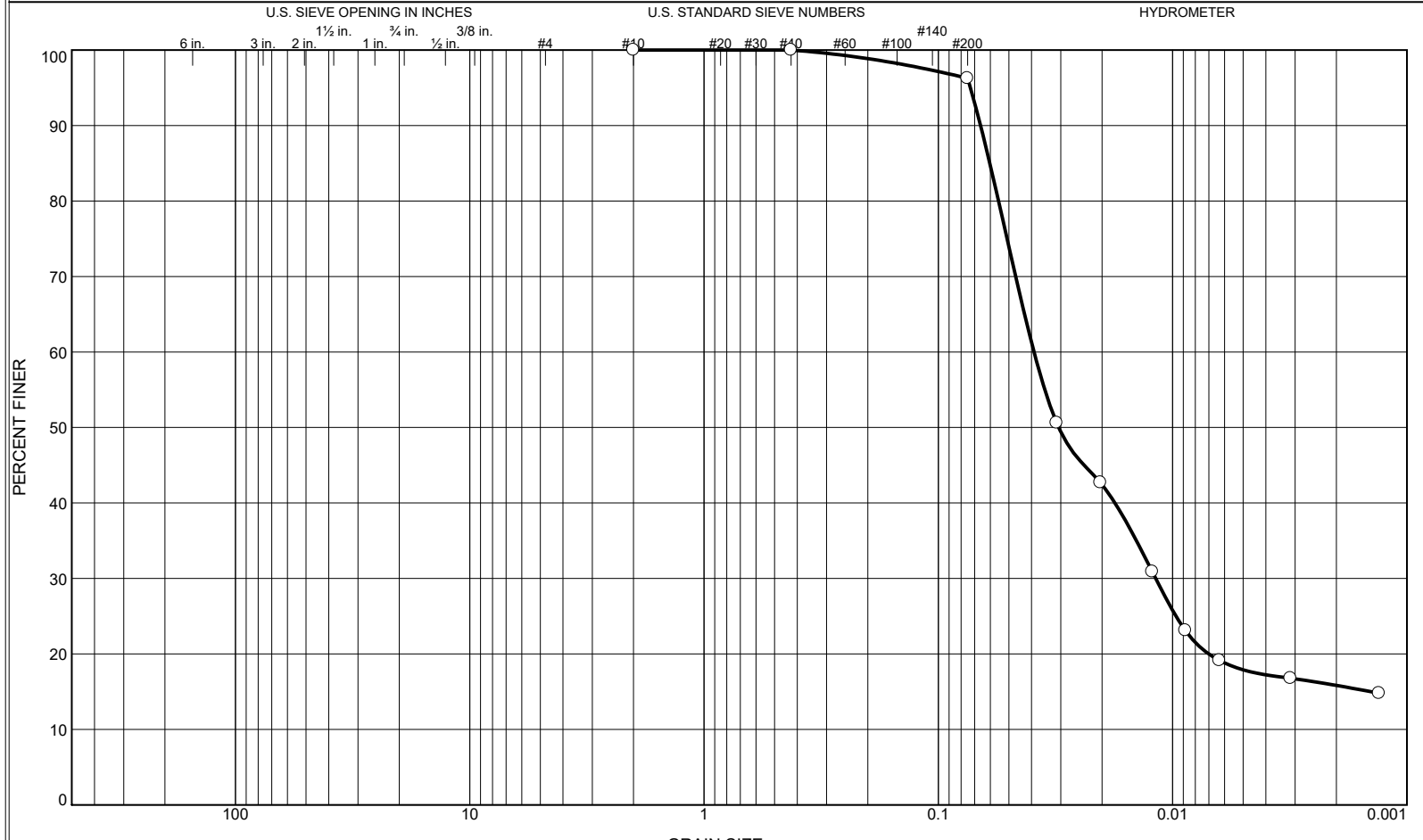


% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	6.6	50.2	43.2

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-14	Depth: 8-10	Sample Number: 5			


Client CPRA		
Project Breton Landbridge Marsh Creation(West)		
Project No. APS2008-G063		

# Particle Size Distribution Report

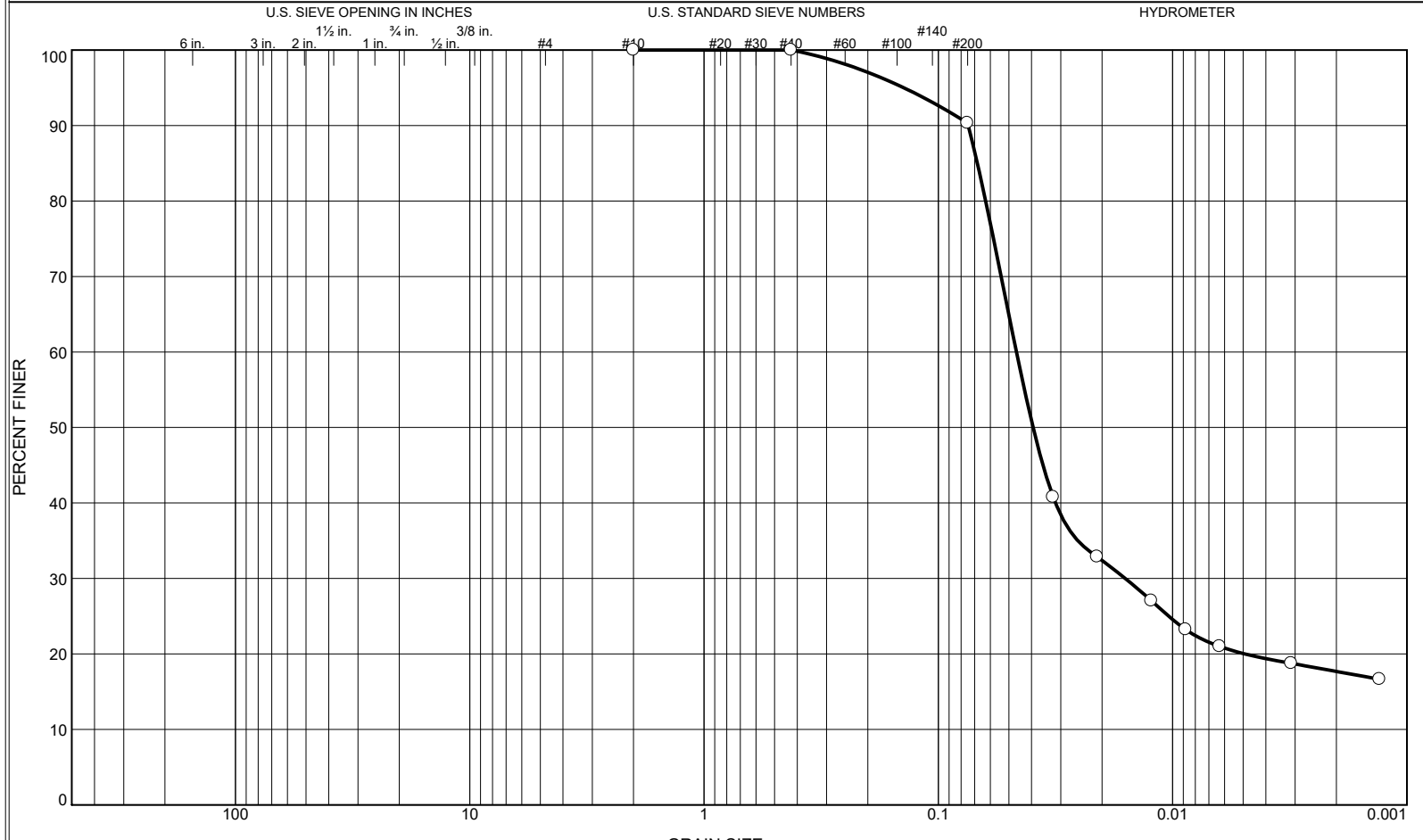


% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	3.7	78.4	17.9

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-14	Depth: 10-12	Sample Number: 6			


Client CPRA		
Project Breton Landbridge Marsh Creation(West)		
Project No. APS2008-G063		

# Particle Size Distribution Report

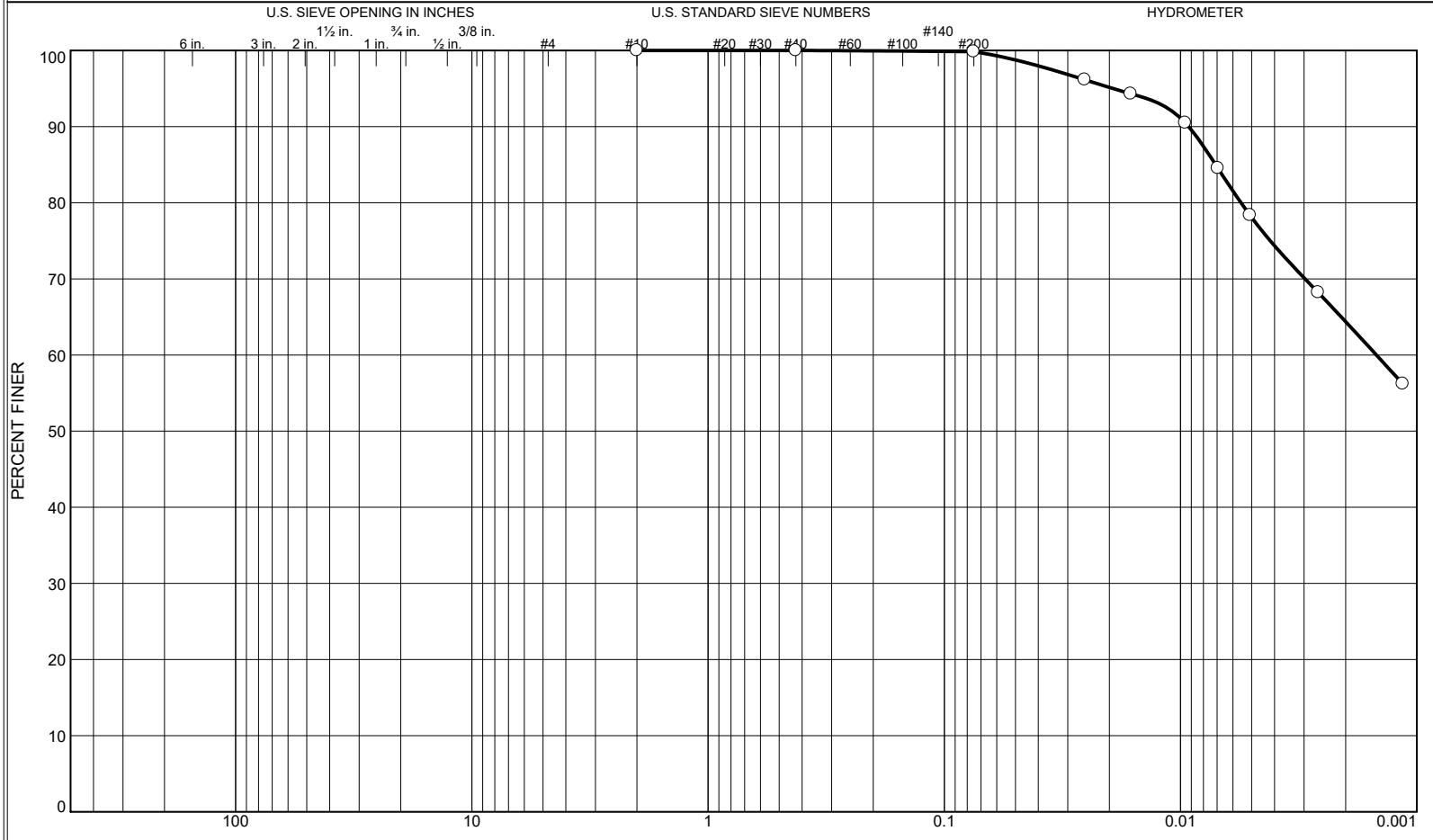


% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	9.7	70.2	20.1

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-14	Depth: 12-14	Sample Number: 7			


Client CPRA		
Project Breton Landbridge Marsh Creation(West)		
Project No. APS2008-G063		

# Particle Size Distribution Report

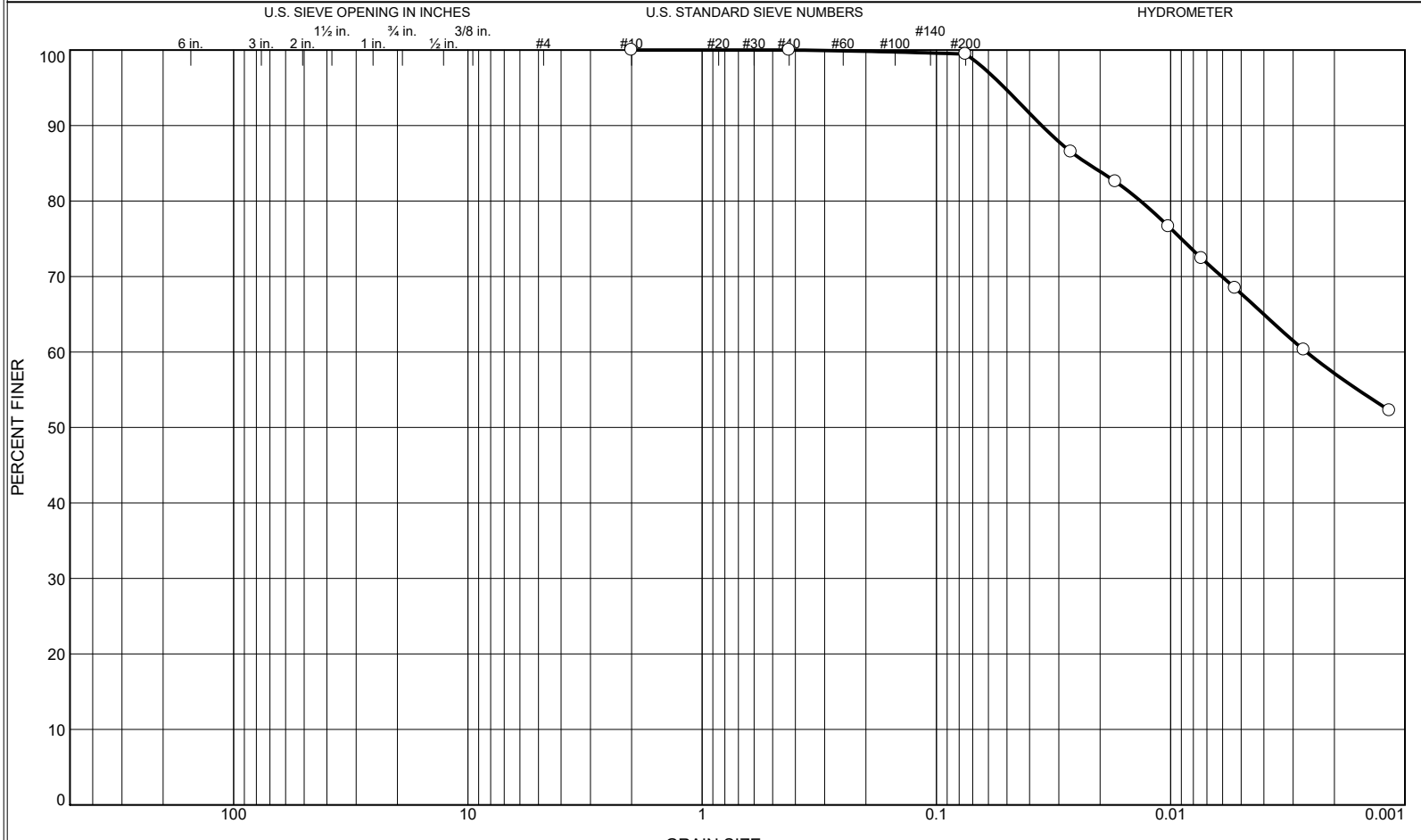


% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	0.2	21.7	78.1

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-14	Depth: 14-16	Sample Number: 8			

Client CPRA		
Project Breton Landbridge Marsh Creation(West)		
Project No. APS2008-G063		

# Particle Size Distribution Report



% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	0.5	31.8	67.7

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-14	Depth: 16-18	Sample Number: 9			

Client CPRA		
Project Breton Landbridge Marsh Creation(West)		
Project No. APS2008-G063		

# Particle Size Distribution Report

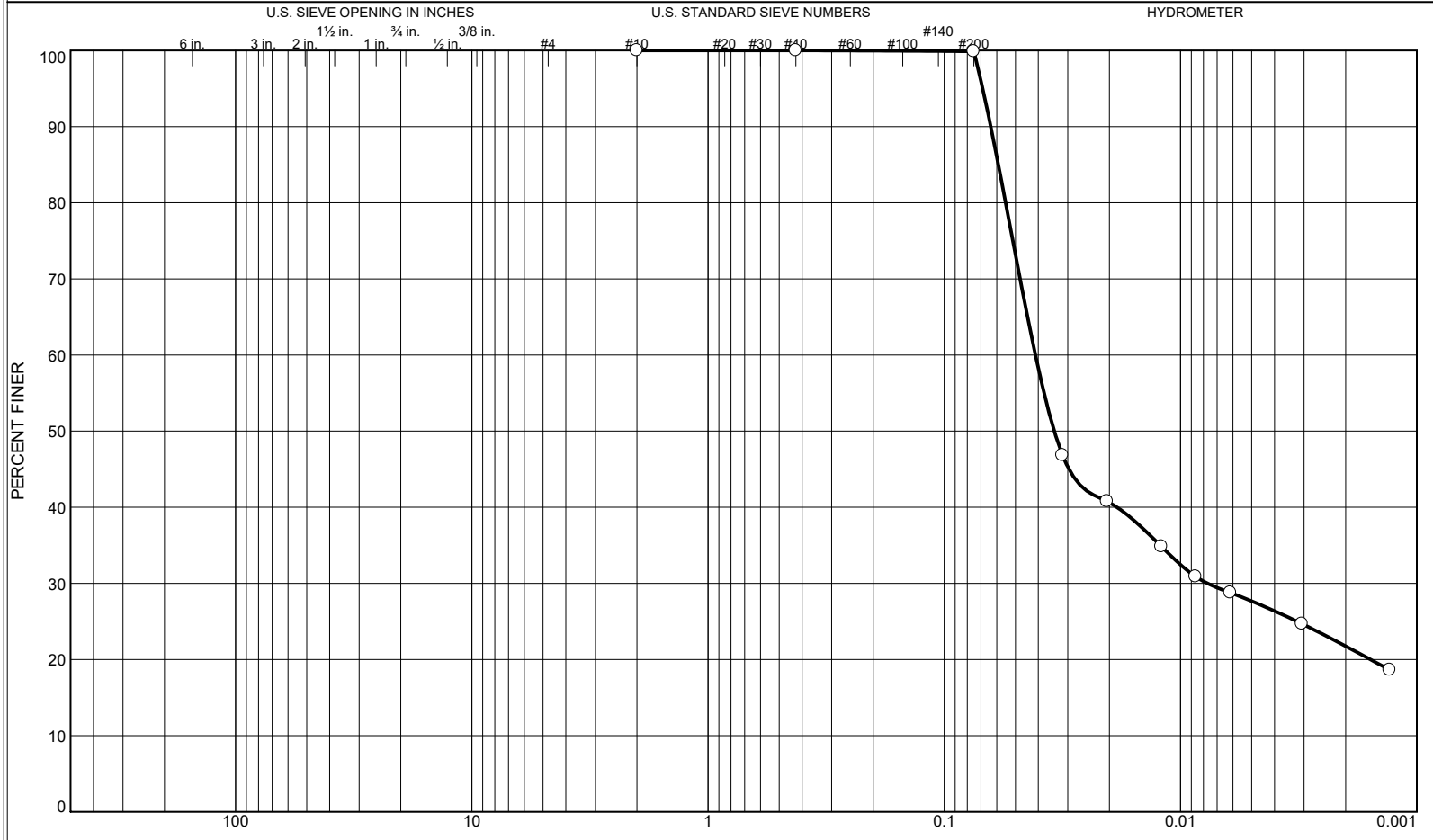


% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	0.5	42.2	57.3

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-14	Depth: 18-20	Sample Number: 10			

Client CPRA		
Project Breton Landbridge Marsh Creation(West)		
Project No. APS2008-G063		

# Particle Size Distribution Report



% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.0	0.1	72.2	27.7

Identification			Date Sampled	Date Received	Date Tested
Source of Sample: B-14	Depth: 23-25	Sample Number: 11			

Client CPRA		
Project Breton Landbridge Marsh Creation(West)		
Project No. APS2008-G063		

**APPENDIX E**  
**(Consolidation and Specific Gravity Data Summary)**



BRETON LANDBRIDGE MARSH CREATION - CONSOLIDATION AND SPECIFIC GRAVITY RESULTS SUMMARY														
Boring No.	Depth (ft)	Laboratory Classification	$P_c^1$ (psf)	$C_c^2$	$C_r^3$	$e_o$	Specific Gravity <sup>4</sup>	w %	LL	PL	PI	$\gamma_{wet}$ (pcf)	$\gamma_{dry}$ (pcf)	UUc (psf)
B-1	0-2	Black Peat(PT)	280	4.60	0.66	10.70	1.21	879.10	980	682	298	63	6	68
B-1	4-6	Very Soft Gray Fat Clay (CH)	310	0.94	0.13	3.00	2.50	43.40	57	24	33	90	62	227
B-1	16-18	Soft Gray Fat Clay (CH)	650	0.42	0.06	1.90	2.62	96.80	115	33	82	95	48	269
B-3	0-2	Black Peat(PT)	210	5.76	0.82	12.50	1.84	475.70	533	127	406	69	12	88
B-3	10-12	Soft Gray Fat Clay (CH)	650	0.35	0.05	1.77	2.62	90.04	99	27	72	93	49	261
B-3	14-16	Very Soft Gray Fat Clay (CH)	350	0.15	0.02	1.74	2.58	84.70	114	32	82	95	51	239
B-5	0-2	Very Soft Gray Lean Clay (CH) -w/ peat and fine sand	310	0.77	0.11	2.05	2.48	44.30	40	18	22	103	71	195
B-5	14-16	Soft Gray Fat Clay (CH)	550	0.24	0.03	1.60	2.57	92.90	140	35	105	96	50	347
B-5	18-20	Very Soft Gray Fat Clay (CH)	580	0.17	0.02	0.90	2.56	64.70	87	26	61	104	63	84
B-6	0-2	Very Soft Gray Fat Clay (CH) w/ peat	300	2.11	0.30	4.91	2.40	203.40	173	39	134	69	23	116
B-6	12-14	Very Soft Gray Fat Clay (CH)	670	0.33	0.05	2.15	2.59	71.10	113	37	76	94	55	220
B-6	28-30	Very Soft Gray Fat Clay (CH)	550	0.19	0.03	1.36	2.63	69.30	81	25	56	101	60	202

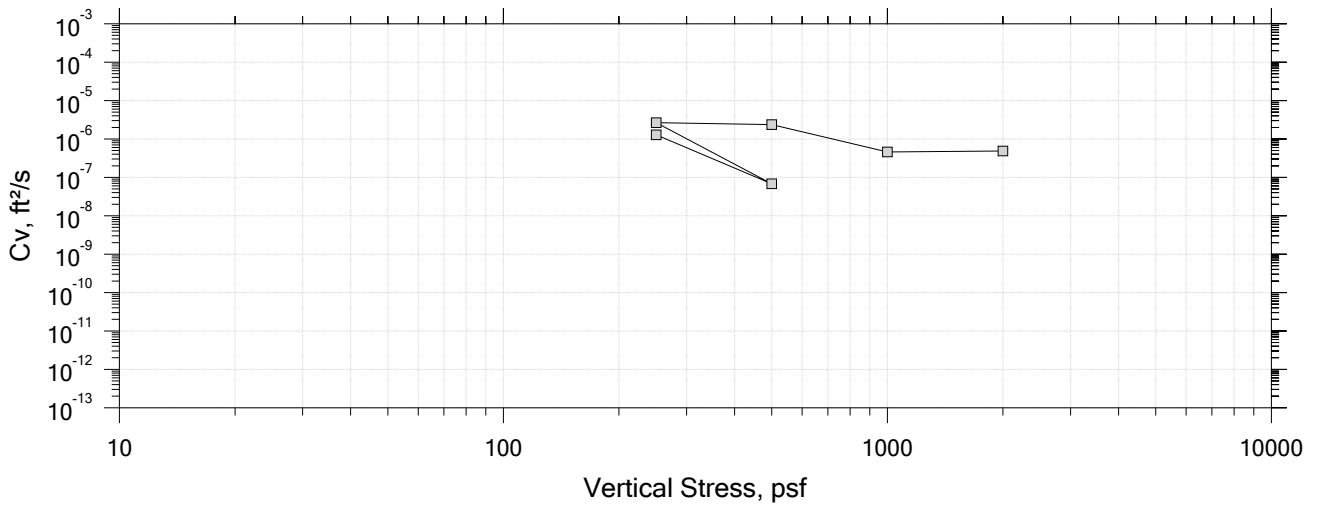
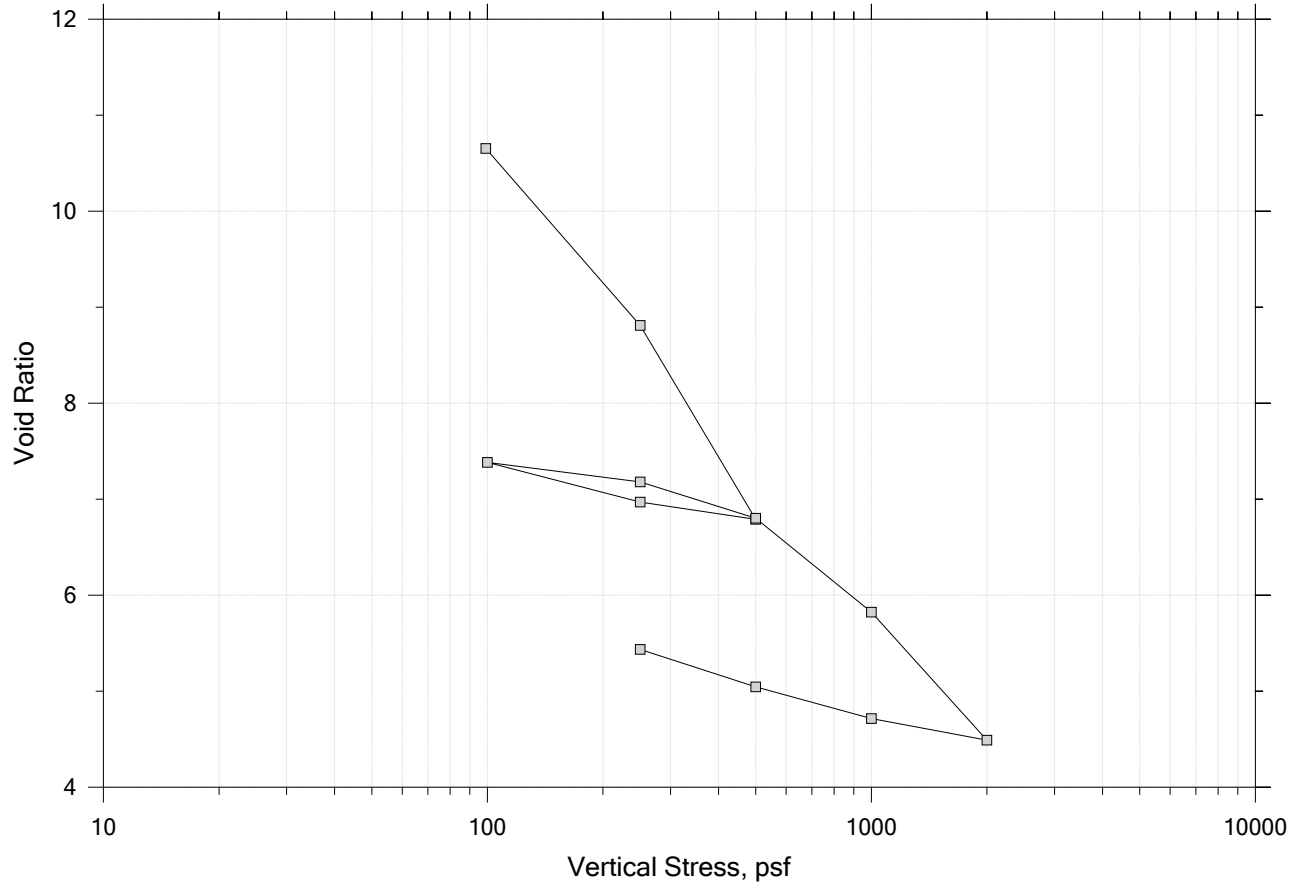
**NOTE:**


1. Preconsolidation Pressure
2. Compression Index
3. Recompression Index
4. Measured as per ASTM D854

**APPENDIX F**  
**(Consolidation Test Reports)**

# One-Dimensional Consolidation by ASTM D2435 - Method B

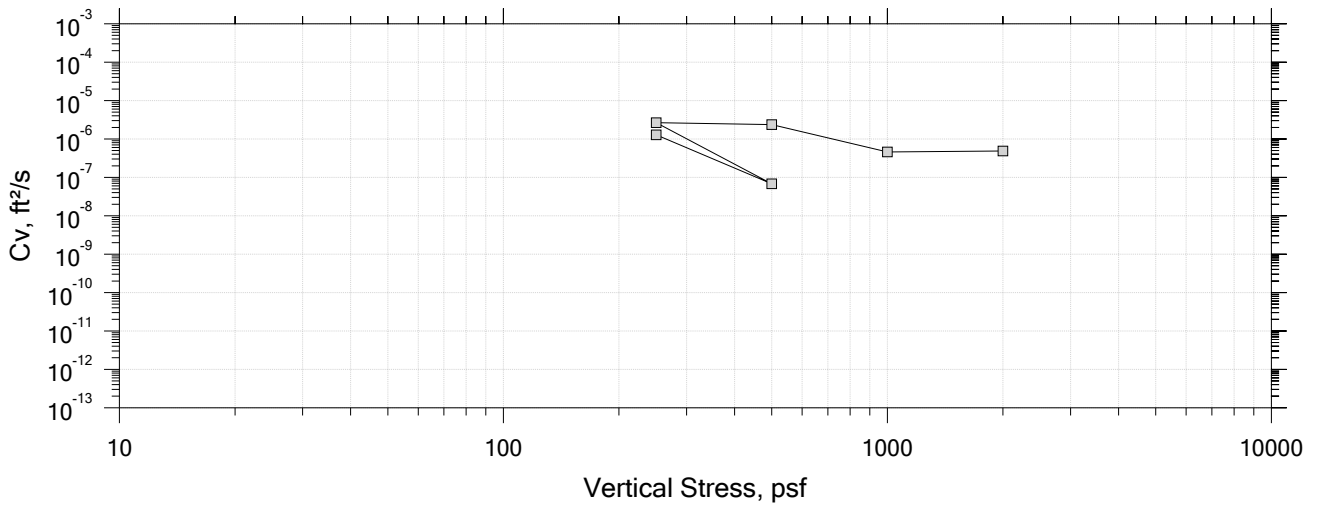
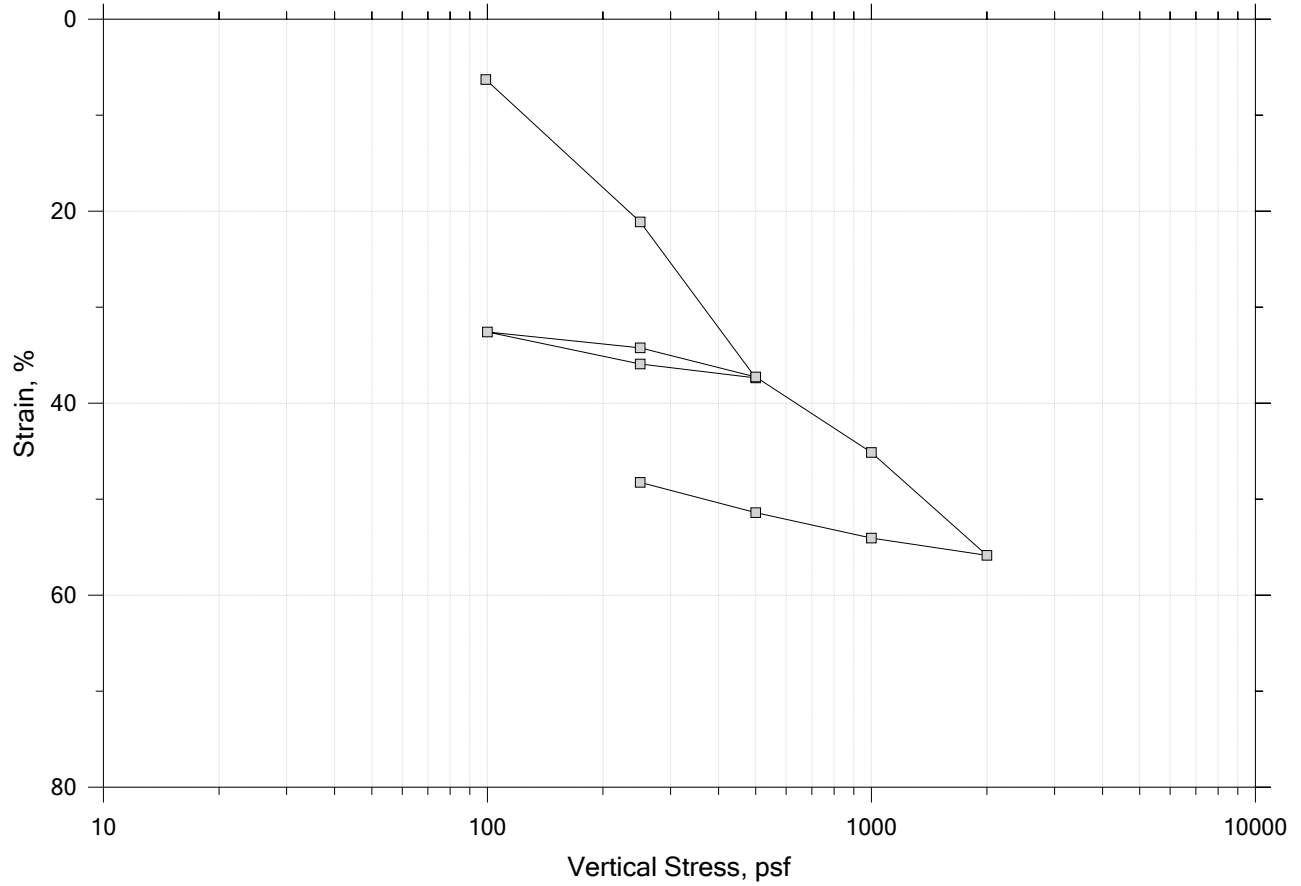
## Summary Report




 <p>APS Engineering and Testing</p>	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-1	Tested By: jm	Checked By: mcm
	Sample No.: 1	Test Date: 10/7/20	Depth: 0-2 ft
	Test No.: IP-1	Sample Type: intact	Elevation: ---
	Description: Moist, black peat(PT)	Measured specific gravity: 1.21	

# One-Dimensional Consolidation by ASTM D2435 - Method B

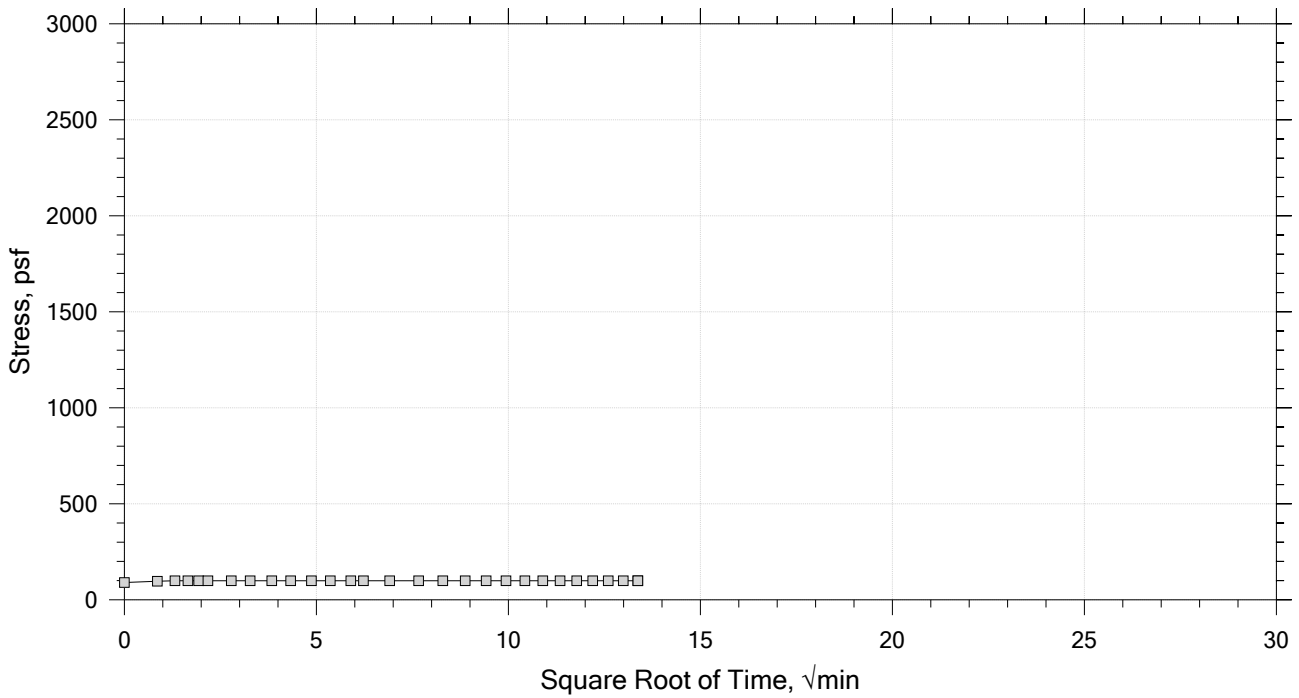
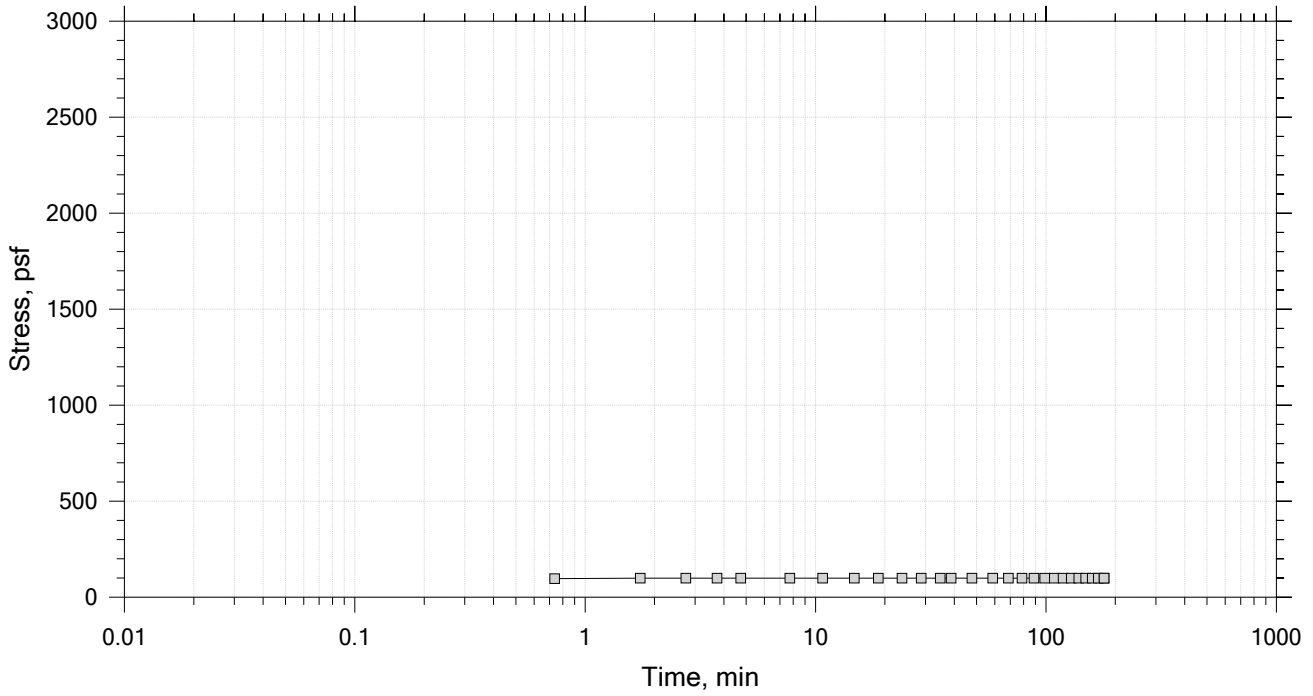
## Summary Report




 <p>Engineering and Testing</p>	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-1	Tested By: jm	Checked By: mcm
	Sample No.: 1	Test Date: 10/7/20	Depth: 0-2 ft
	Test No.: IP-1	Sample Type: intact	Elevation: ---
	Description: Moist, black peat (PT)		

# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 1 of 12  
 Constant Volume Step  
 Stress: 99 psf



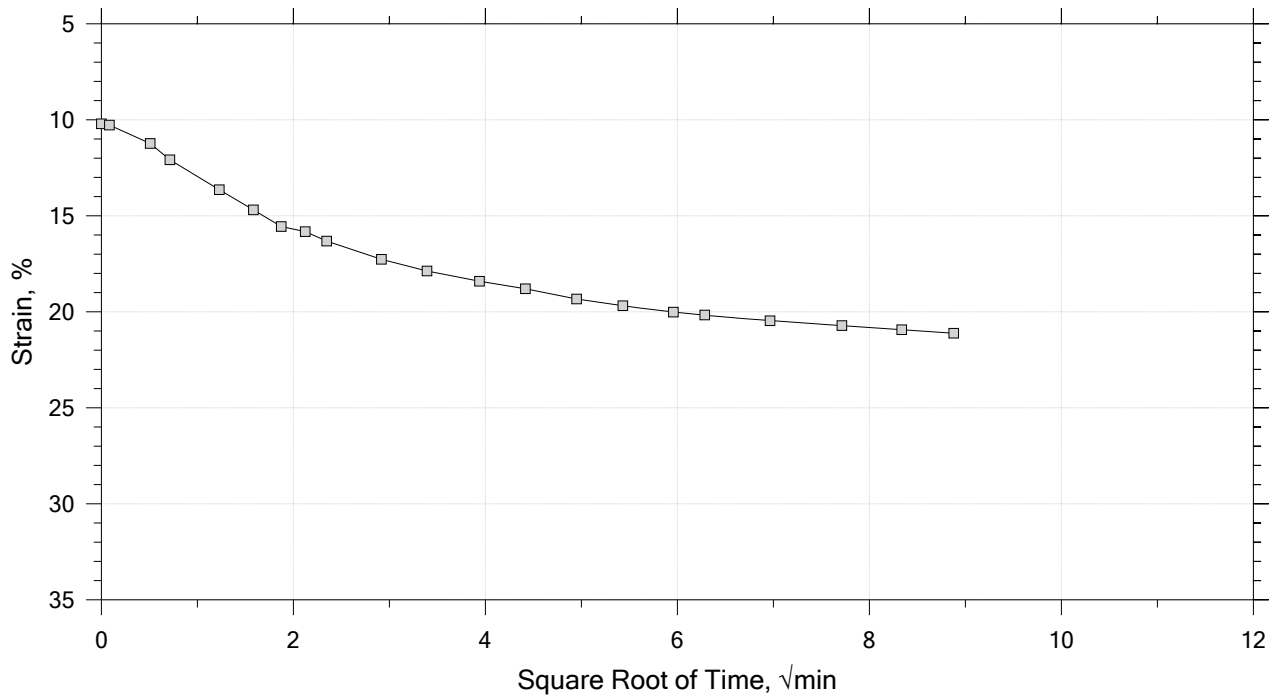
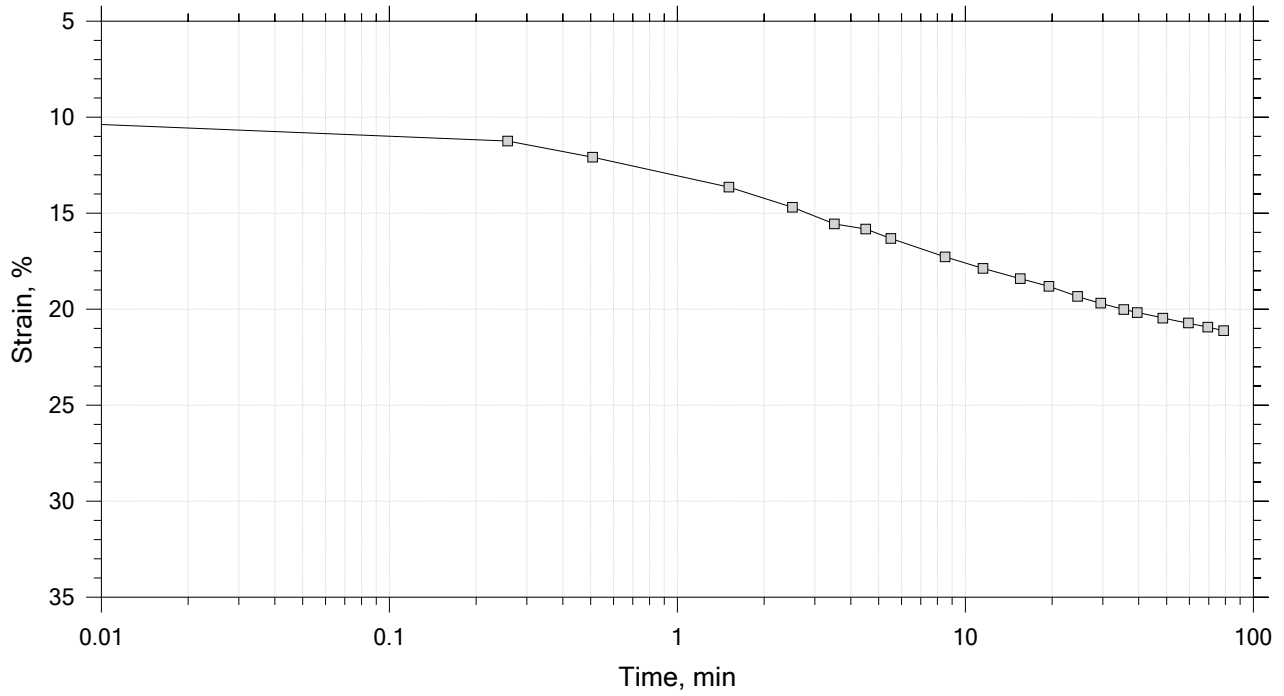
 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-1	Tested By: jm	Checked By: mcm
	Sample No.: 1	Test Date: 10/7/20	Depth: 0-2 ft
	Test No.: IP-1	Sample Type: intact	Elevation: ---
	Description: Moist, black peat (PT)		


# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 2 of 12

Constant Load Step

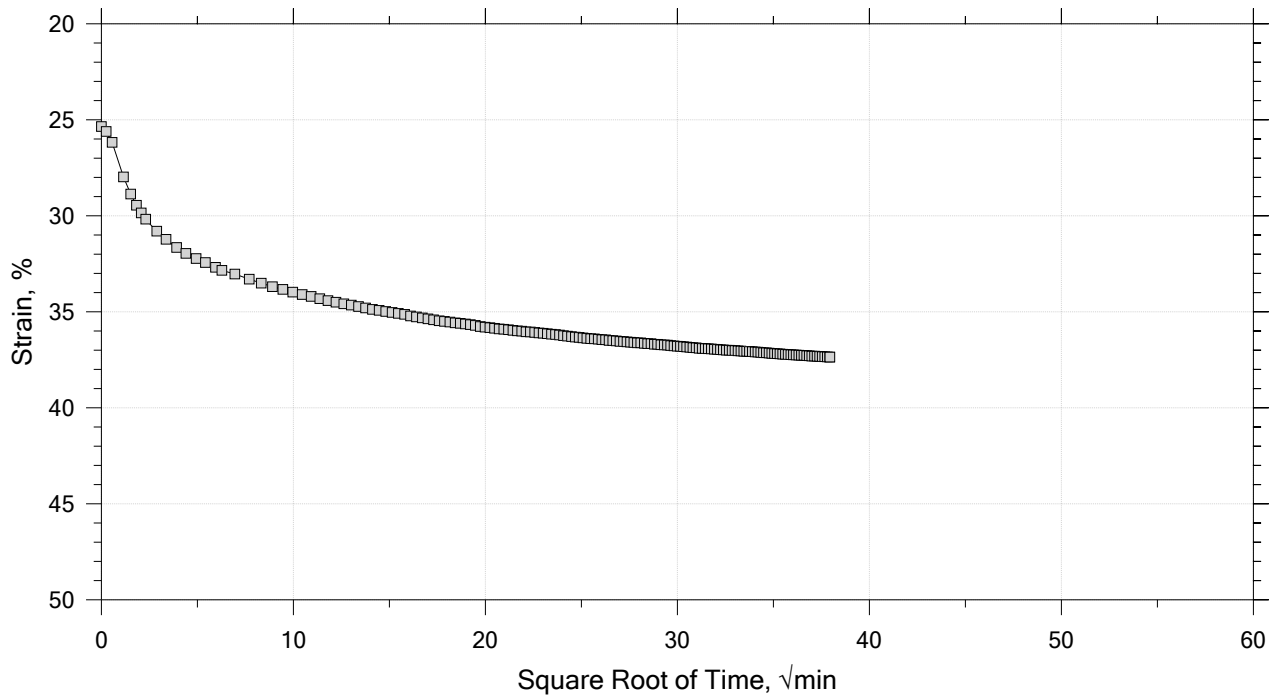
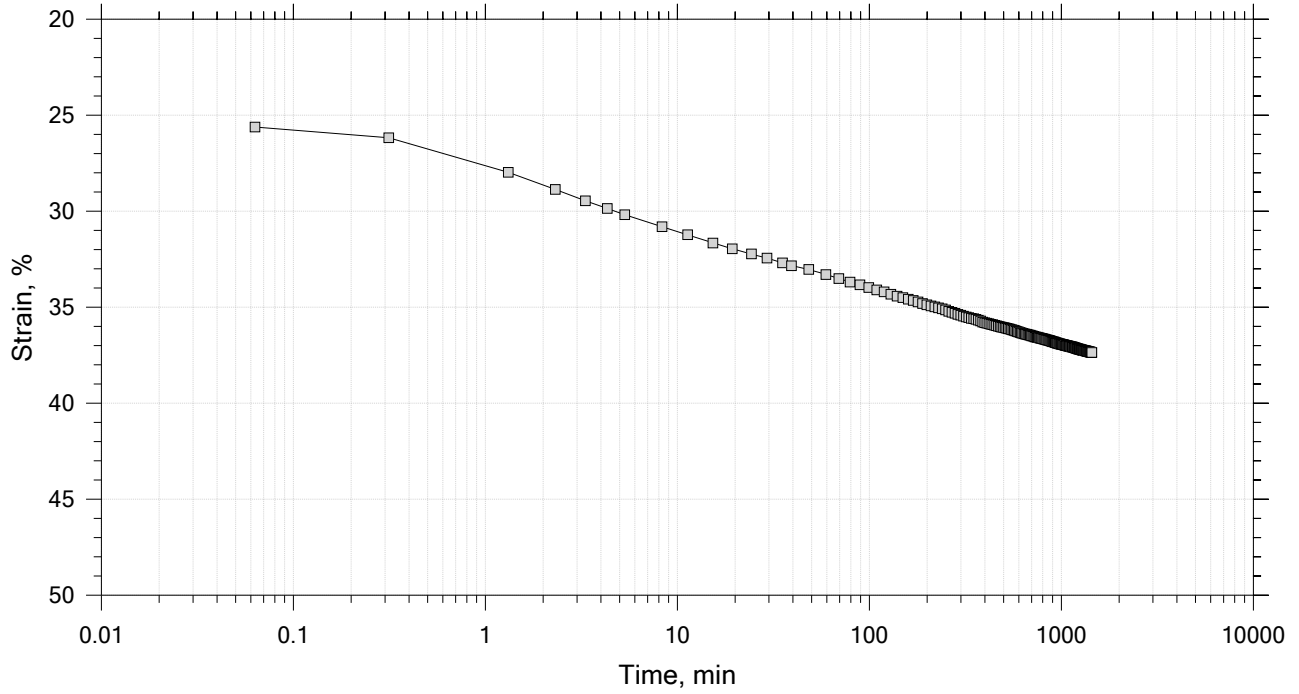
Stress: 250 psf




 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-1	Tested By: jm	Checked By: mcm
	Sample No.: 1	Test Date: 10/7/20	Depth: 0-2 ft
	Test No.: IP-1	Sample Type: intact	Elevation: ---
	Description: Moist, black peat (PT)		

# One-Dimensional Consolidation by ASTM D2435 - Method B

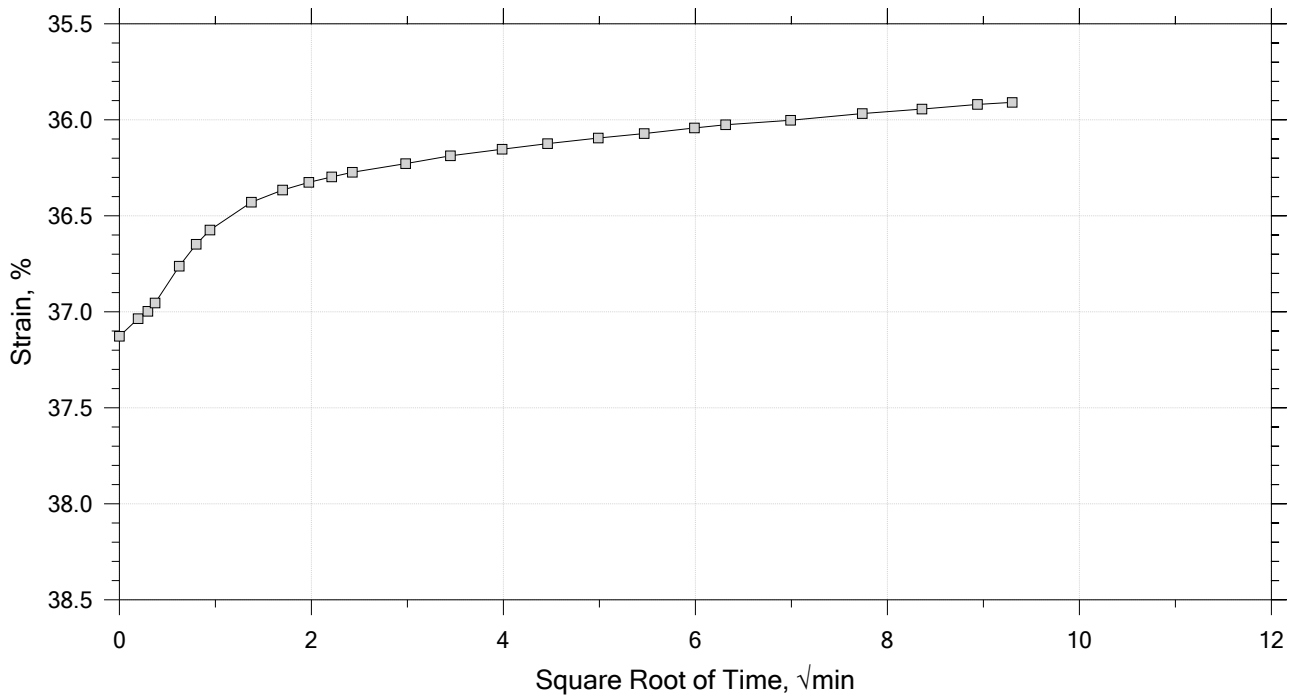
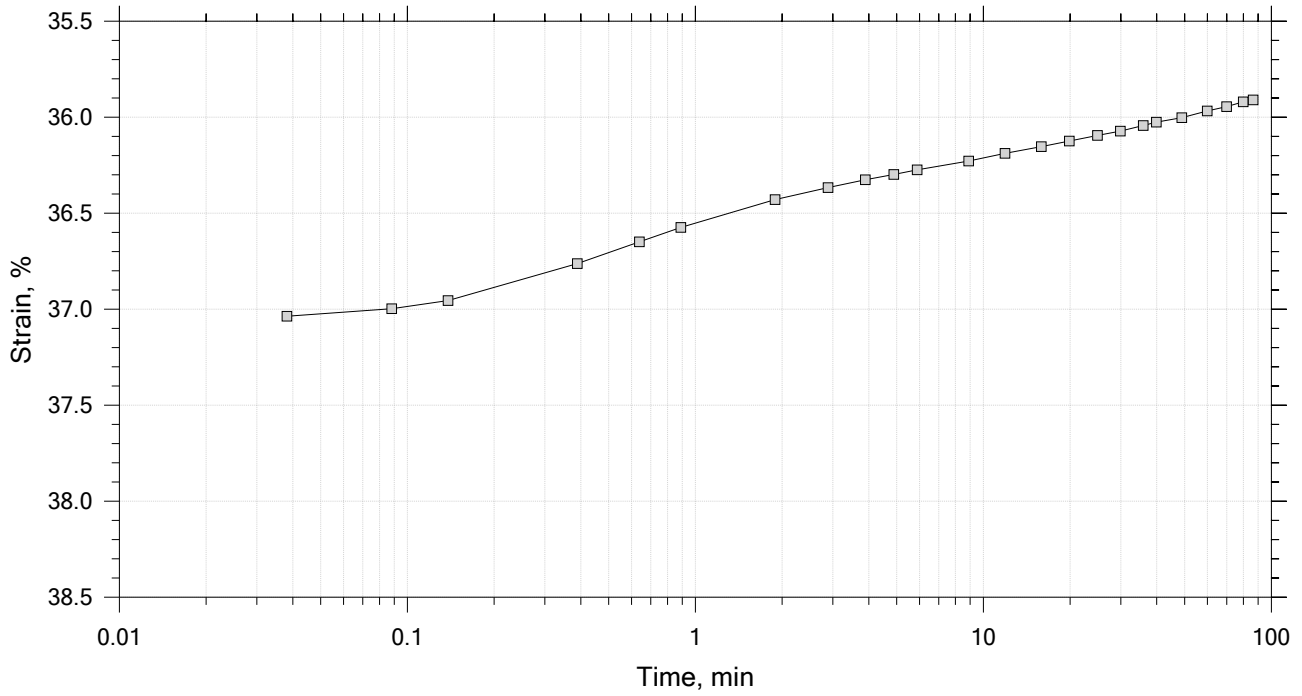
Time Curve 3 of 12  
 Constant Load Step  
 Stress: 500 psf




 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-1	Tested By: jm	Checked By: mcm
	Sample No.: 1	Test Date: 10/7/20	Depth: 0-2 ft
	Test No.: IP-1	Sample Type: intact	Elevation: ---
	Description: Moist, black peat (PT)		

# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 4 of 12  
 Constant Load Step  
 Stress: 250 psf



 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-1	Tested By: jm	Checked By: mcm
	Sample No.: 1	Test Date: 10/7/20	Depth: 0-2 ft
	Test No.: IP-1	Sample Type: intact	Elevation: ---
	Description: Moist, black peat (PT)		

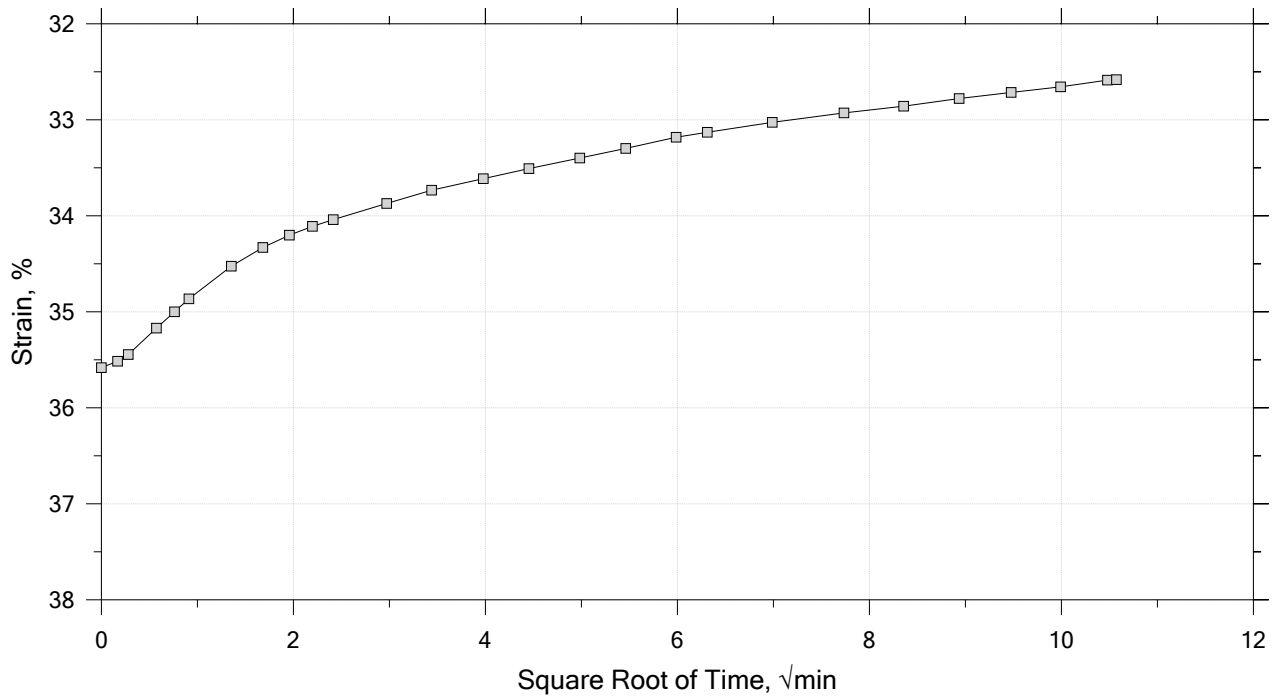
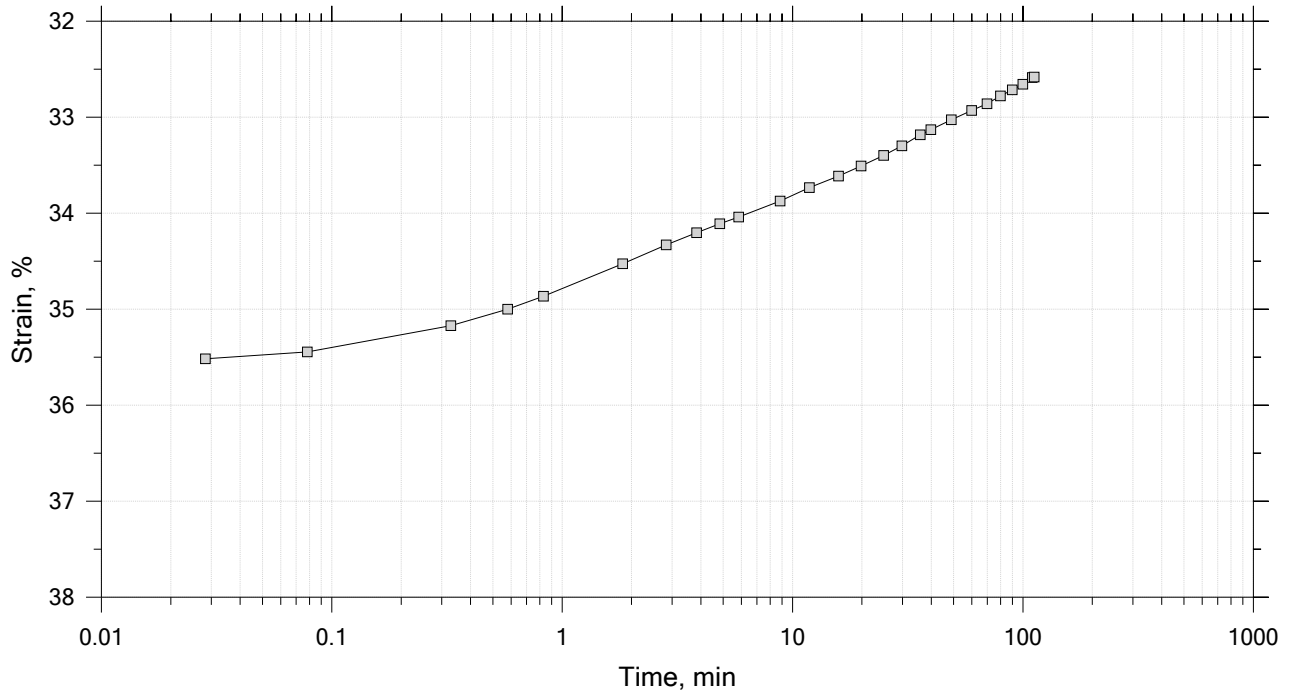



# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 5 of 12

Constant Load Step

Stress: 100 psf



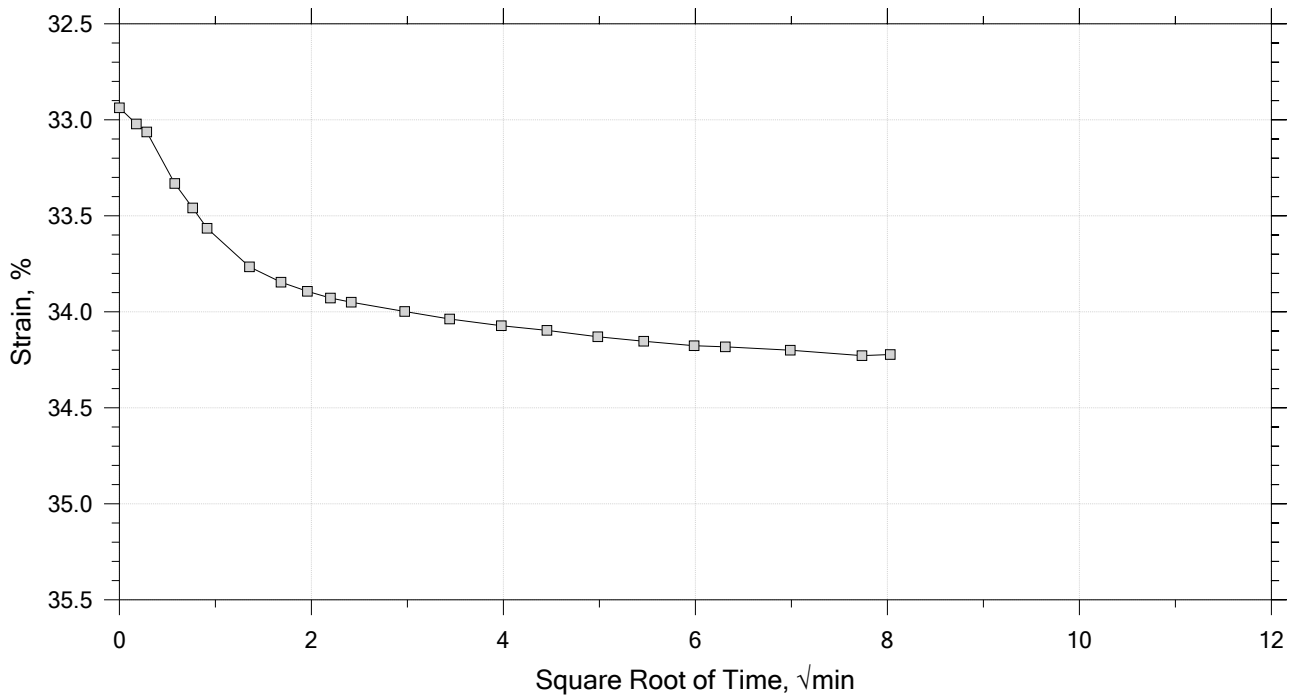
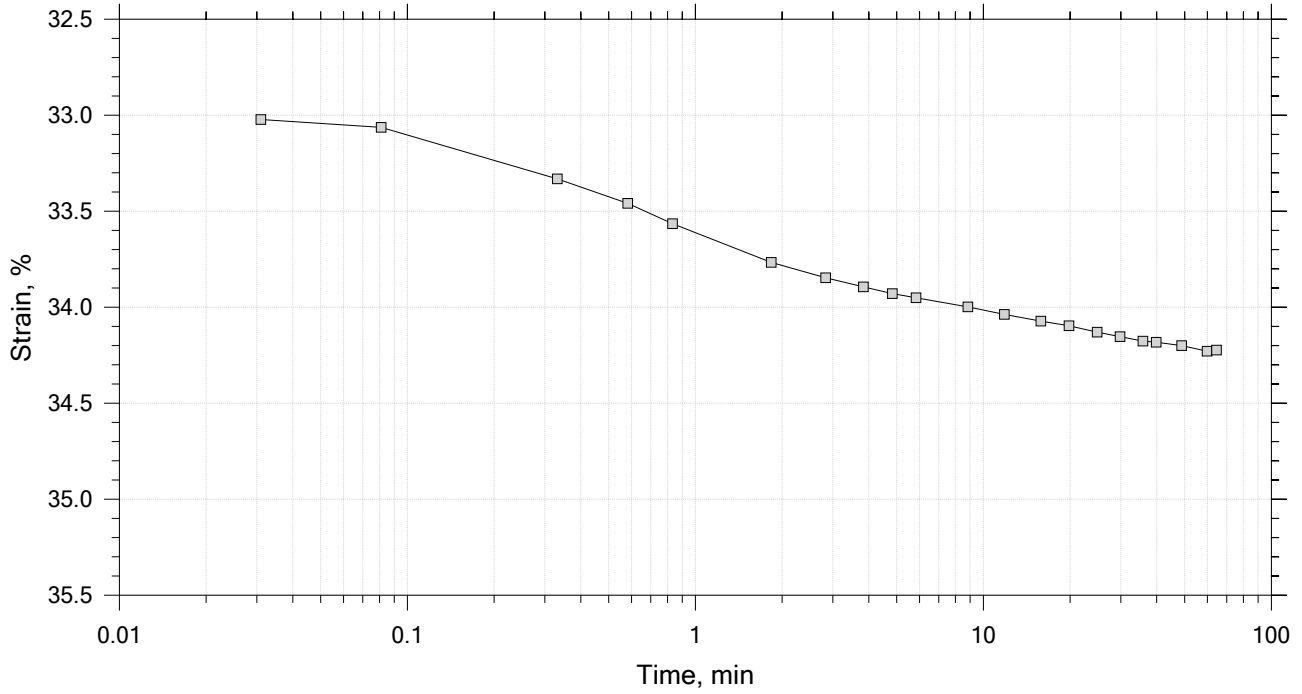
 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-1	Tested By: jm	Checked By: mcm
	Sample No.: 1	Test Date: 10/7/20	Depth: 0-2 ft
	Test No.: IP-1	Sample Type: intact	Elevation: ---
	Description: Moist, black peat (PT)		


# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 6 of 12

Constant Load Step

Stress: 250 psf



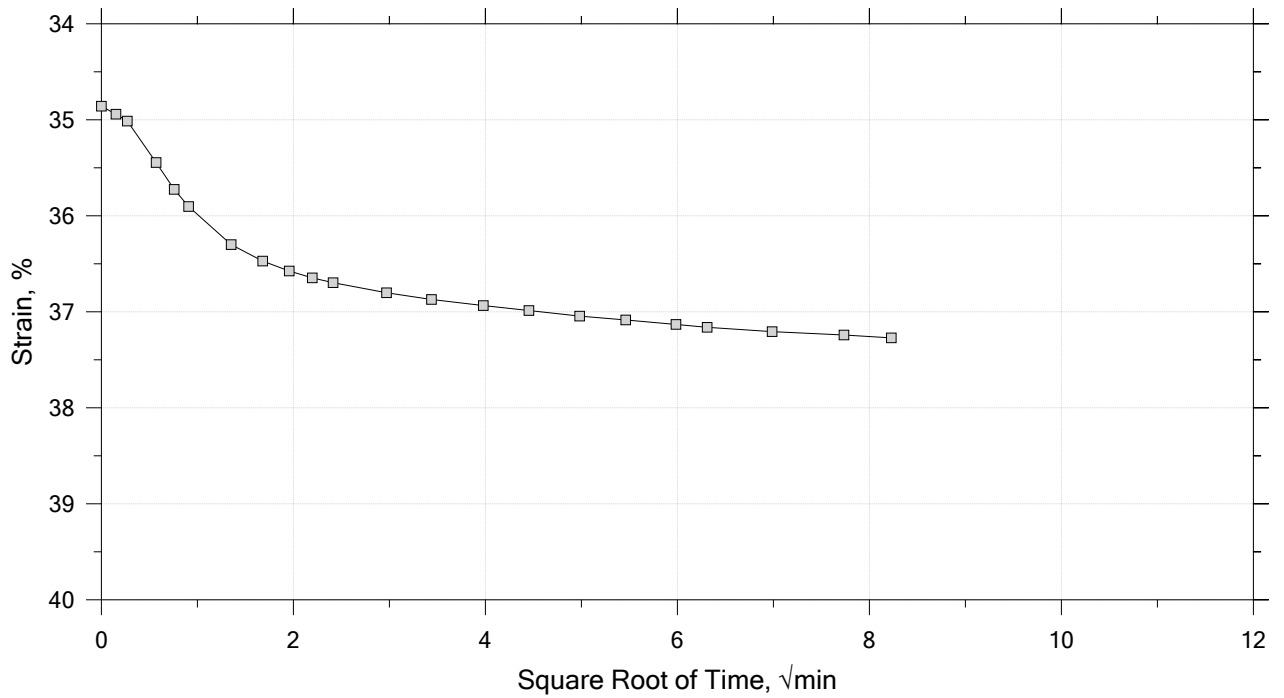
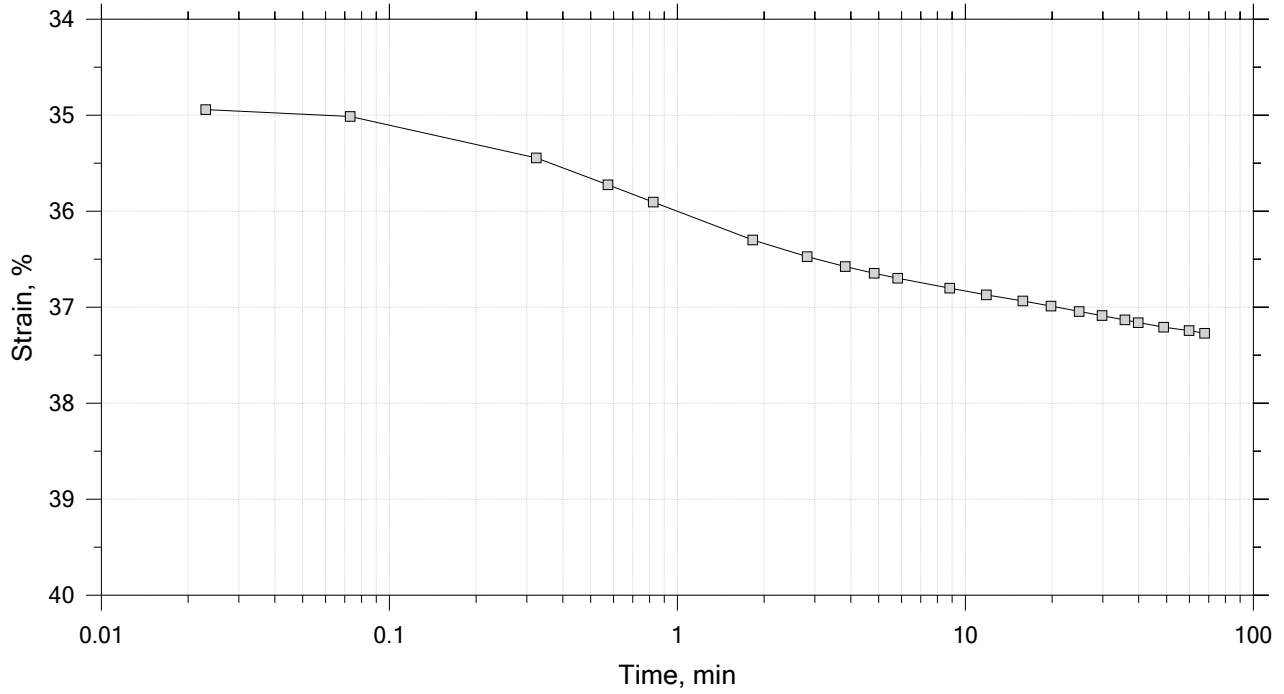
 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-1	Tested By: jm	Checked By: mcm
	Sample No.: 1	Test Date: 10/7/20	Depth: 0-2 ft
	Test No.: IP-1	Sample Type: intact	Elevation: ---
	Description: Moist, black peat (PT)		


# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 7 of 12

Constant Load Step

Stress: 500 psf



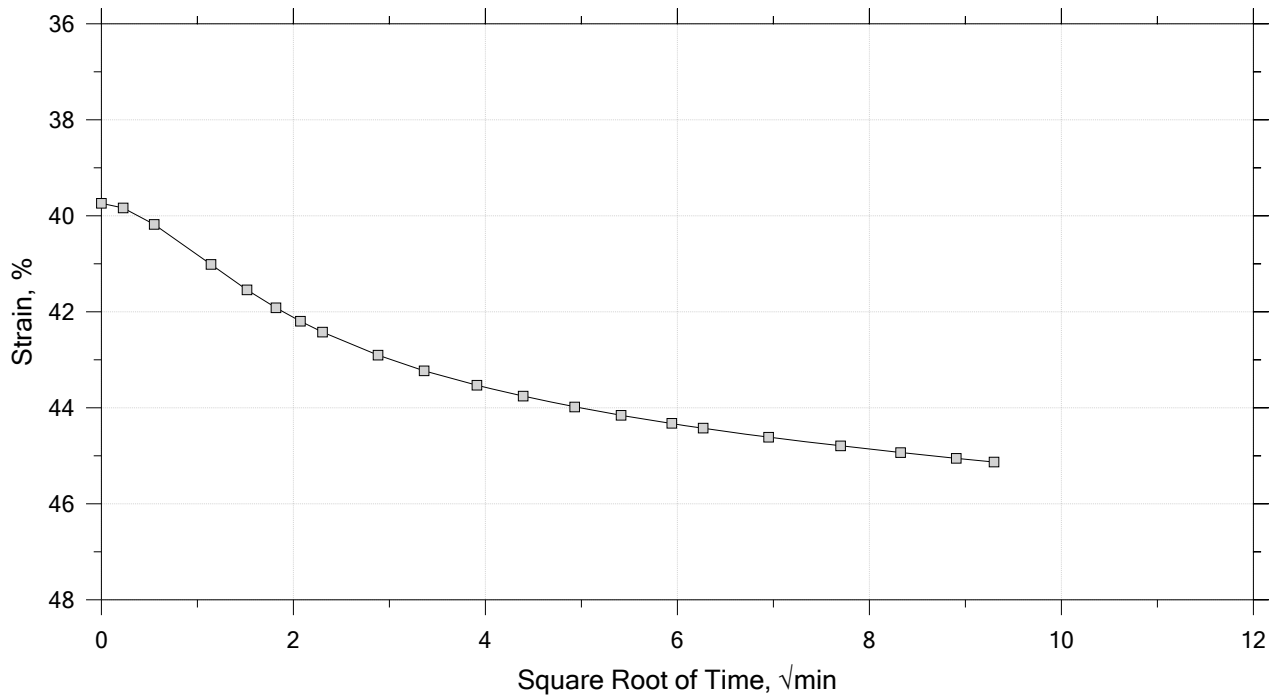
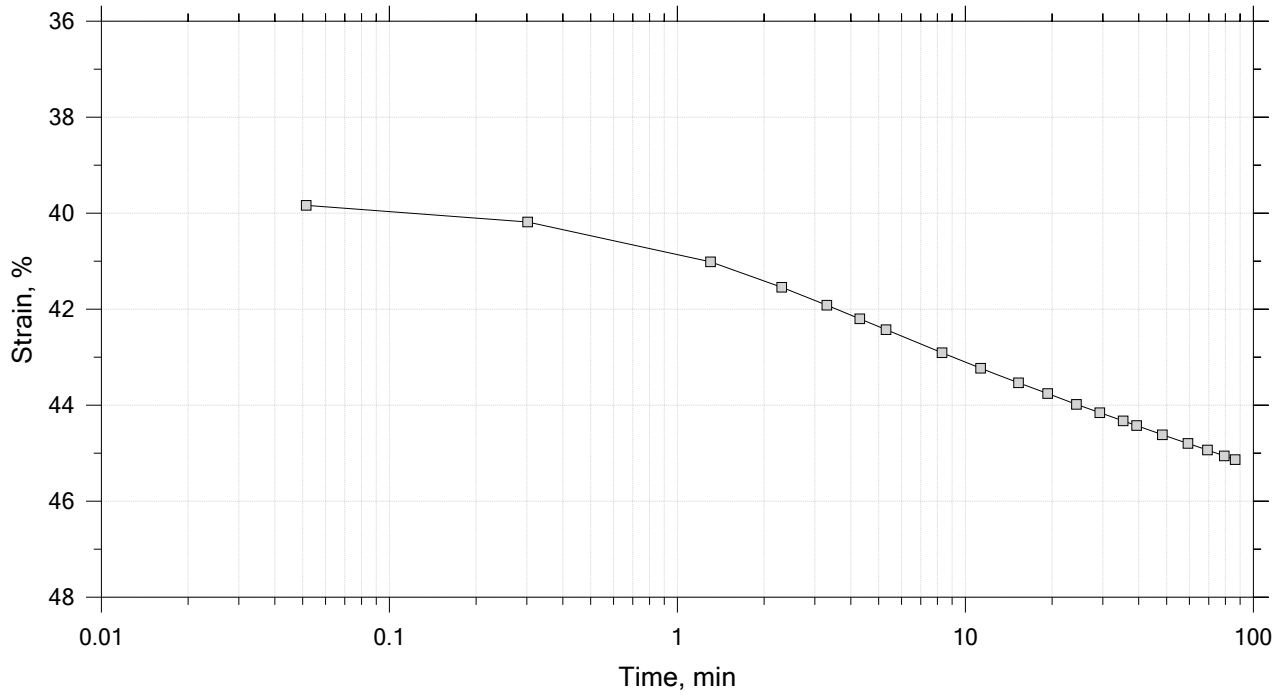
 <p>Engineering and Testing</p>	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-1	Tested By: jm	Checked By: mcm
	Sample No.: 1	Test Date: 10/7/20	Depth: 0-2 ft
	Test No.: IP-1	Sample Type: intact	Elevation: ---
	Description: Moist, black peat (PT)		


# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 8 of 12

Constant Load Step

Stress: 1e+03 psf



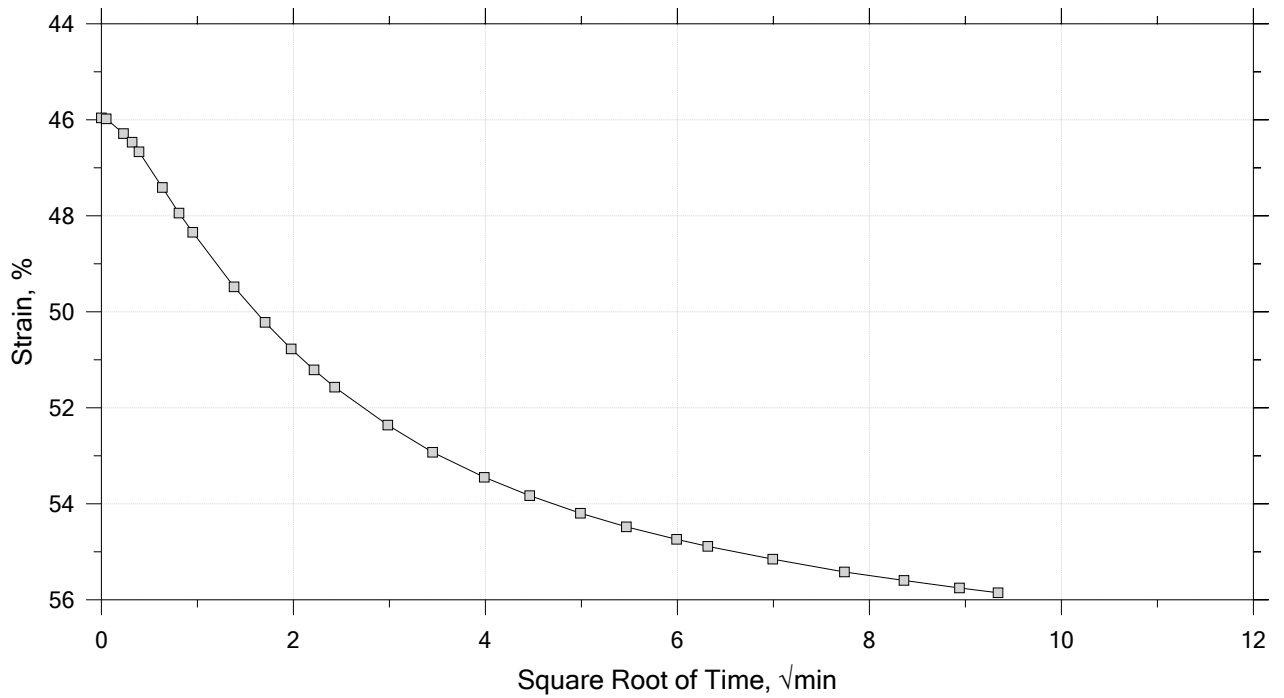
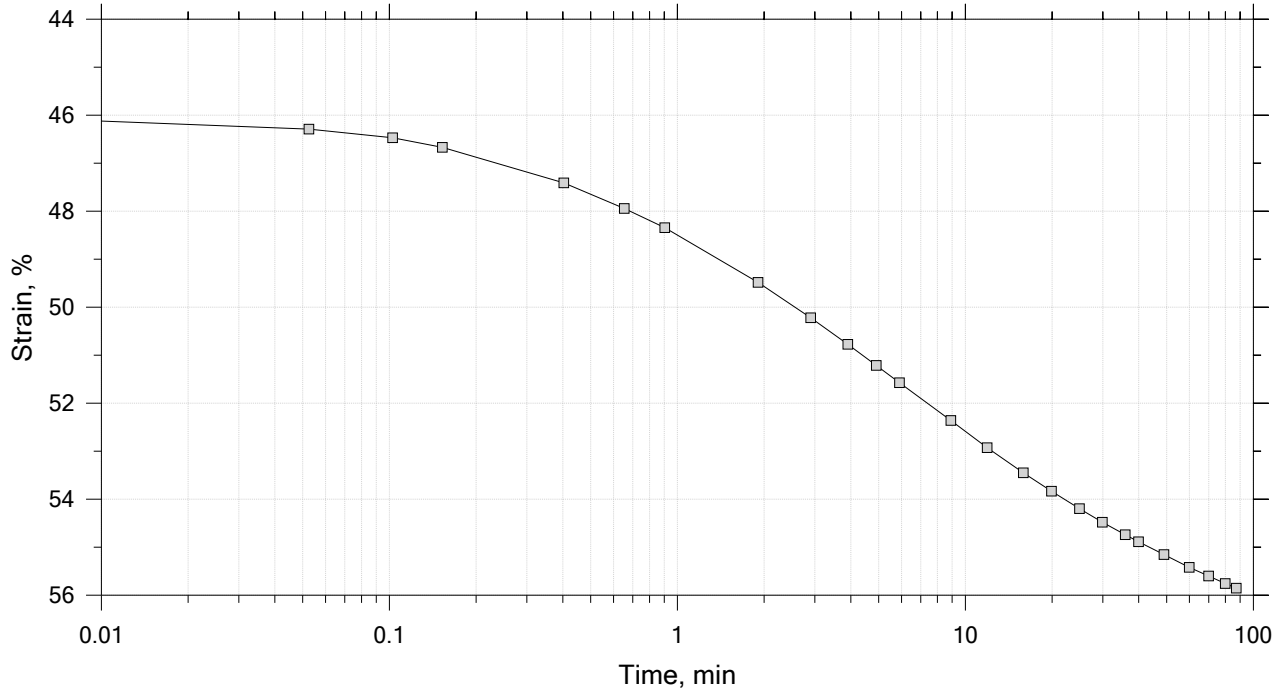
 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-1	Tested By: jm	Checked By: mcm
	Sample No.: 1	Test Date: 10/7/20	Depth: 0-2 ft
	Test No.: IP-1	Sample Type: intact	Elevation: ---
	Description: Moist, black peat (PT)		


# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 9 of 12

Constant Load Step

Stress: 2e+03 psf



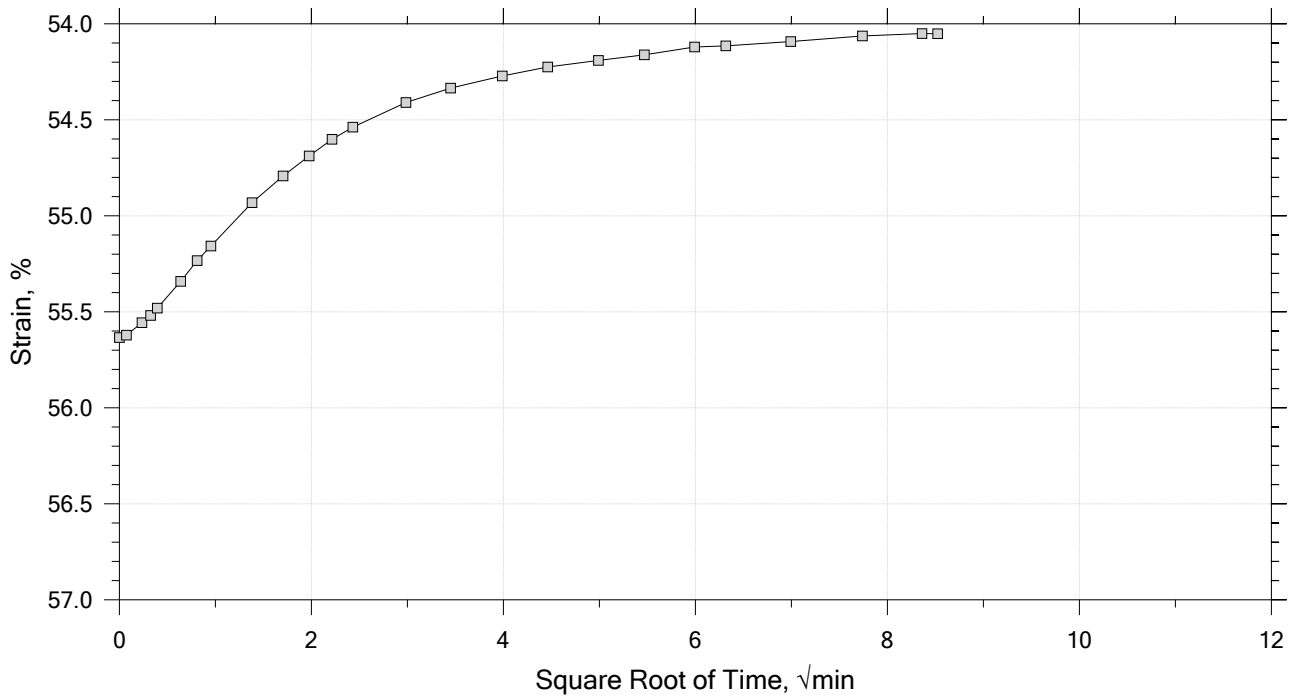
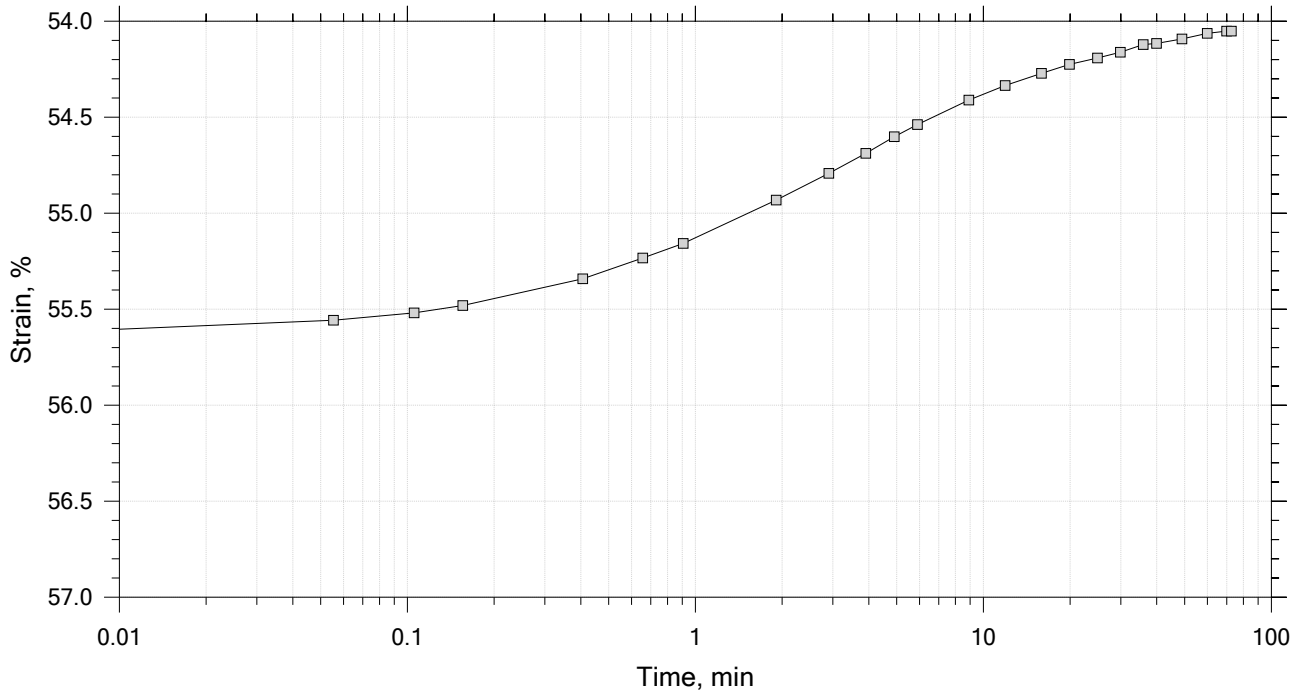
 <p>Engineering and Testing</p>	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-1	Tested By: jm	Checked By: mcm
	Sample No.: 1	Test Date: 10/7/20	Depth: 0-2 ft
	Test No.: IP-1	Sample Type: intact	Elevation: ---
	Description: Moist, black peat (PT)		


# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 10 of 12

Constant Load Step

Stress: 1e+03 psf



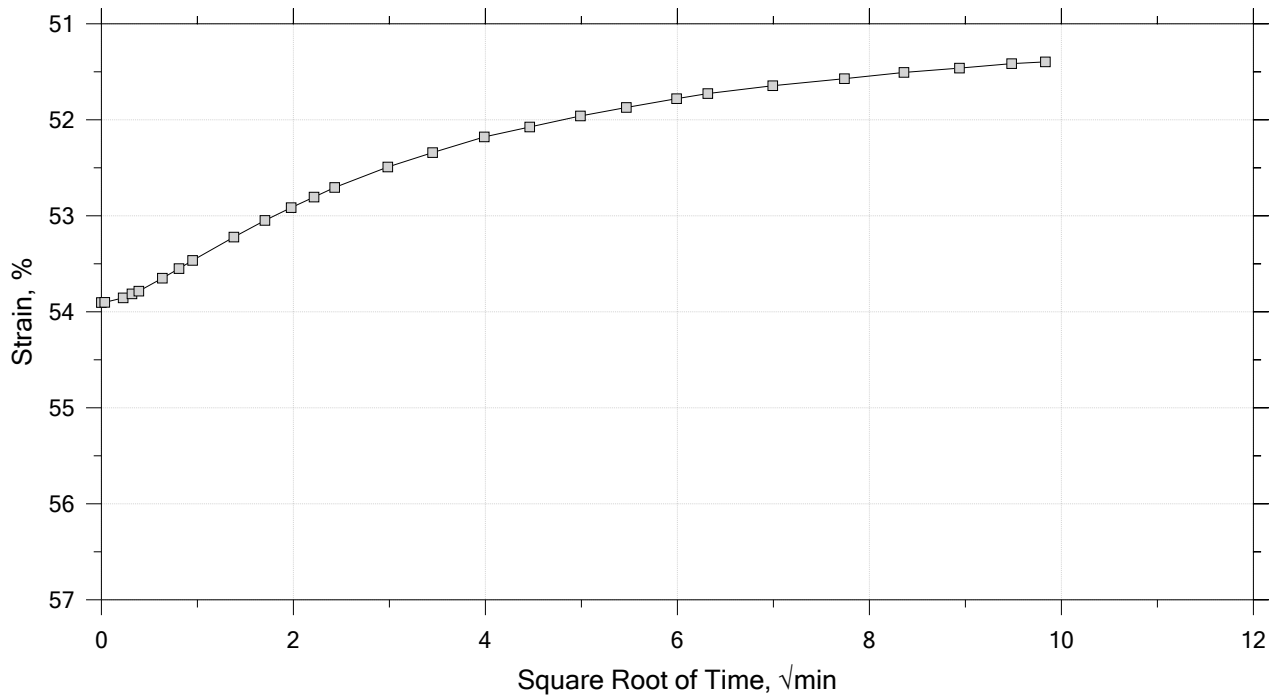
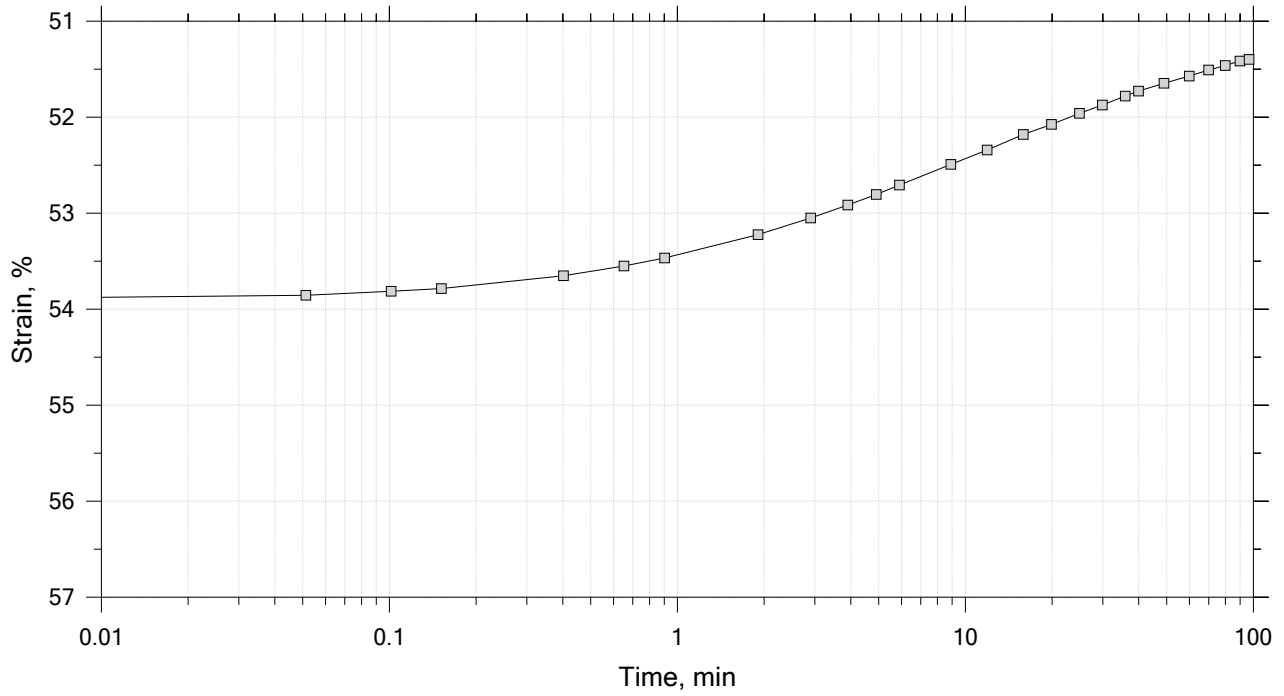
 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-1	Tested By: jm	Checked By: mcm
	Sample No.: 1	Test Date: 10/7/20	Depth: 0-2 ft
	Test No.: IP-1	Sample Type: intact	Elevation: ---
	Description: Moist, black peat (PT)		


# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 11 of 12

Constant Load Step

Stress: 500 psf



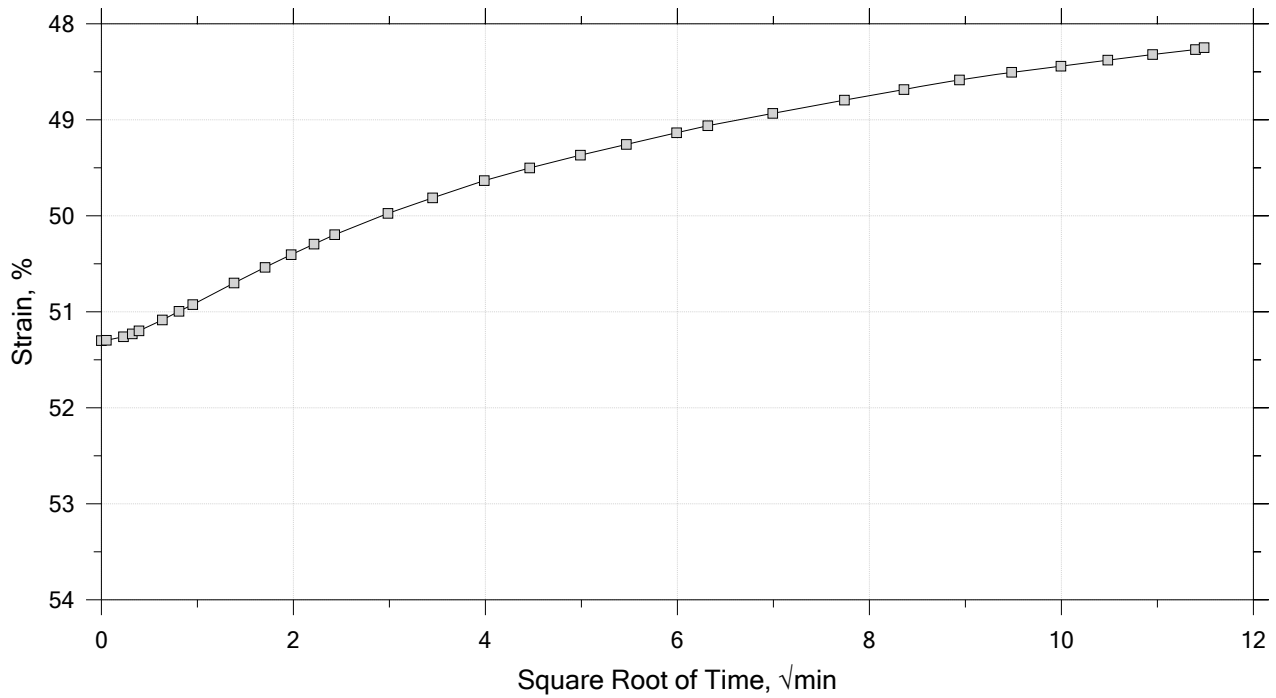
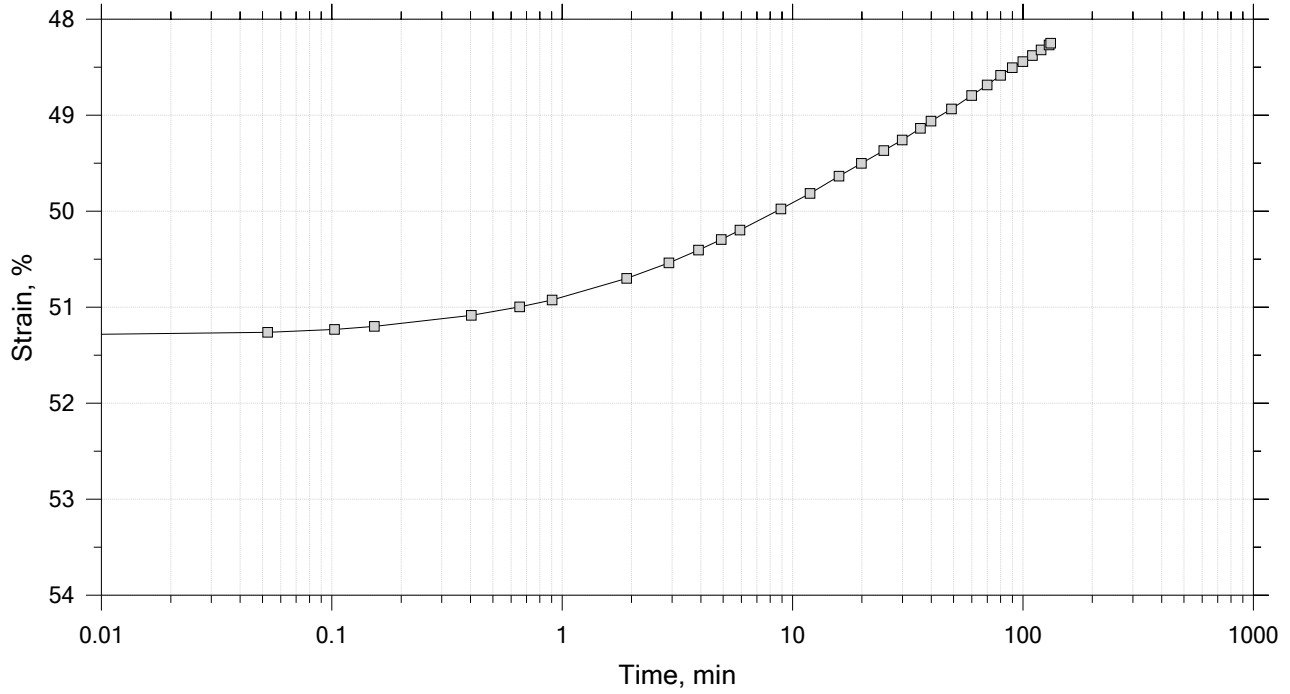
 <p>Engineering and Testing</p>	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-1	Tested By: jm	Checked By: mcm
	Sample No.: 1	Test Date: 10/7/20	Depth: 0-2 ft
	Test No.: IP-1	Sample Type: intact	Elevation: ---
	Description: Moist, black peat (PT)		


# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 12 of 12

Constant Load Step

Stress: 250 psf

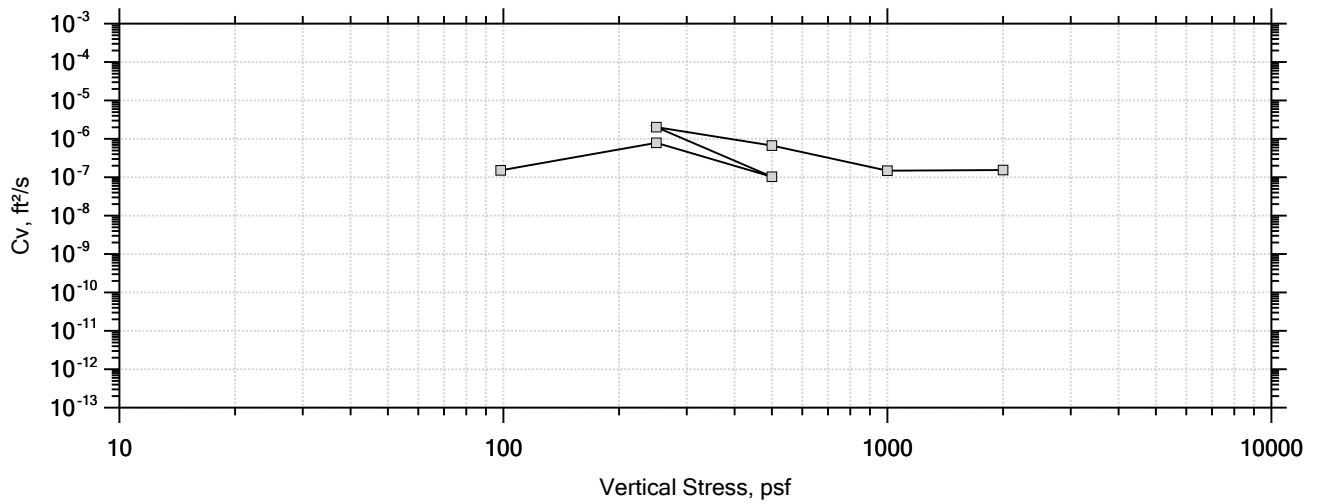
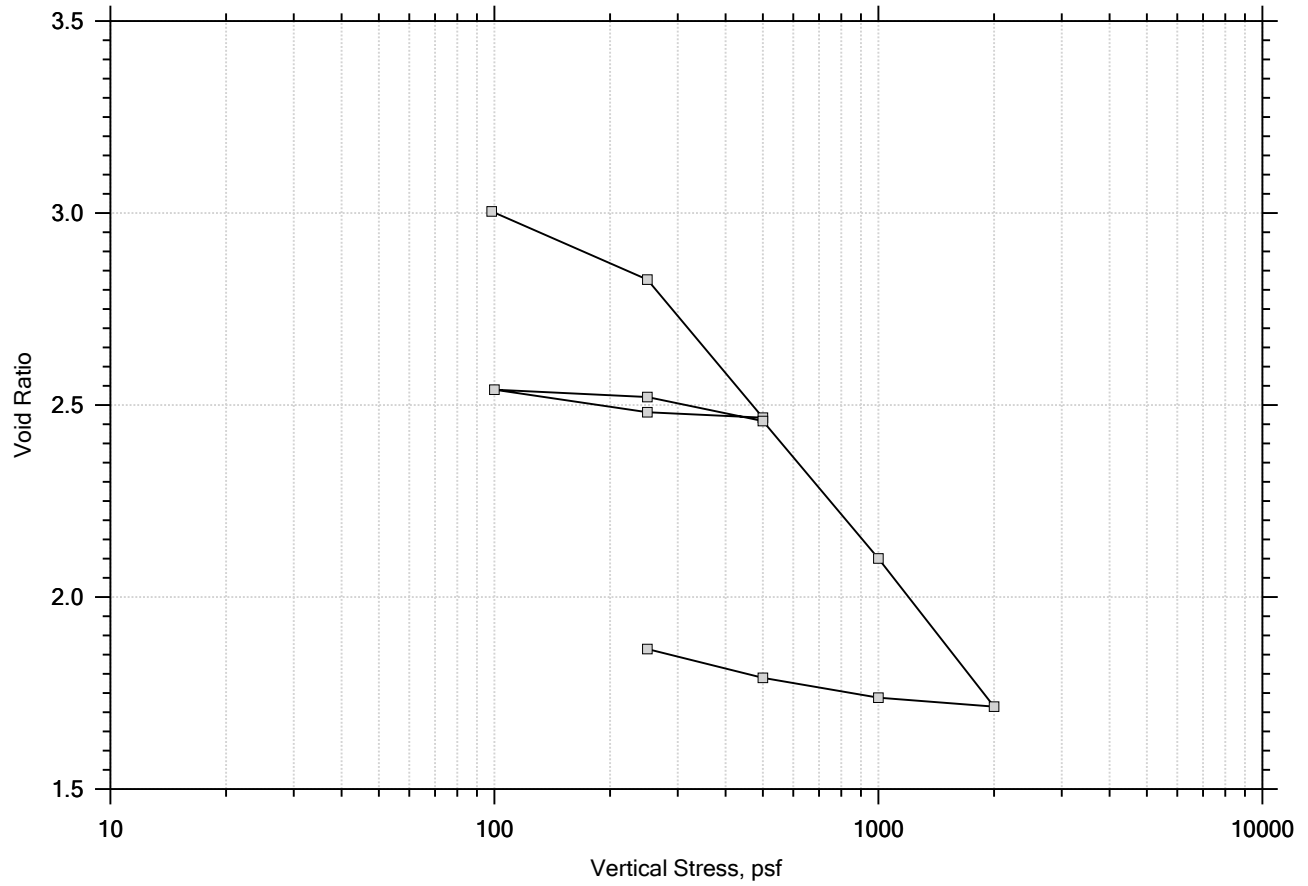



 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-1	Tested By: jm	Checked By: mcm
	Sample No.: 1	Test Date: 10/7/20	Depth: 0-2 ft
	Test No.: IP-1	Sample Type: intact	Elevation: ---
	Description: Moist, black peat (PT)		



# One-Dimensional Consolidation by ASTM D2435 - Method B

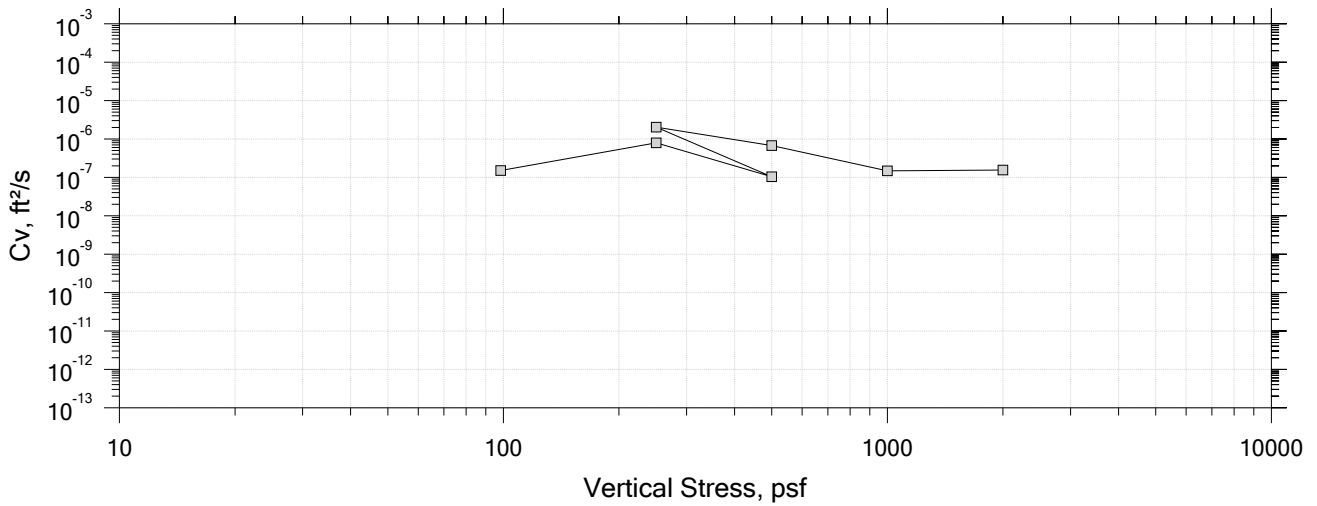
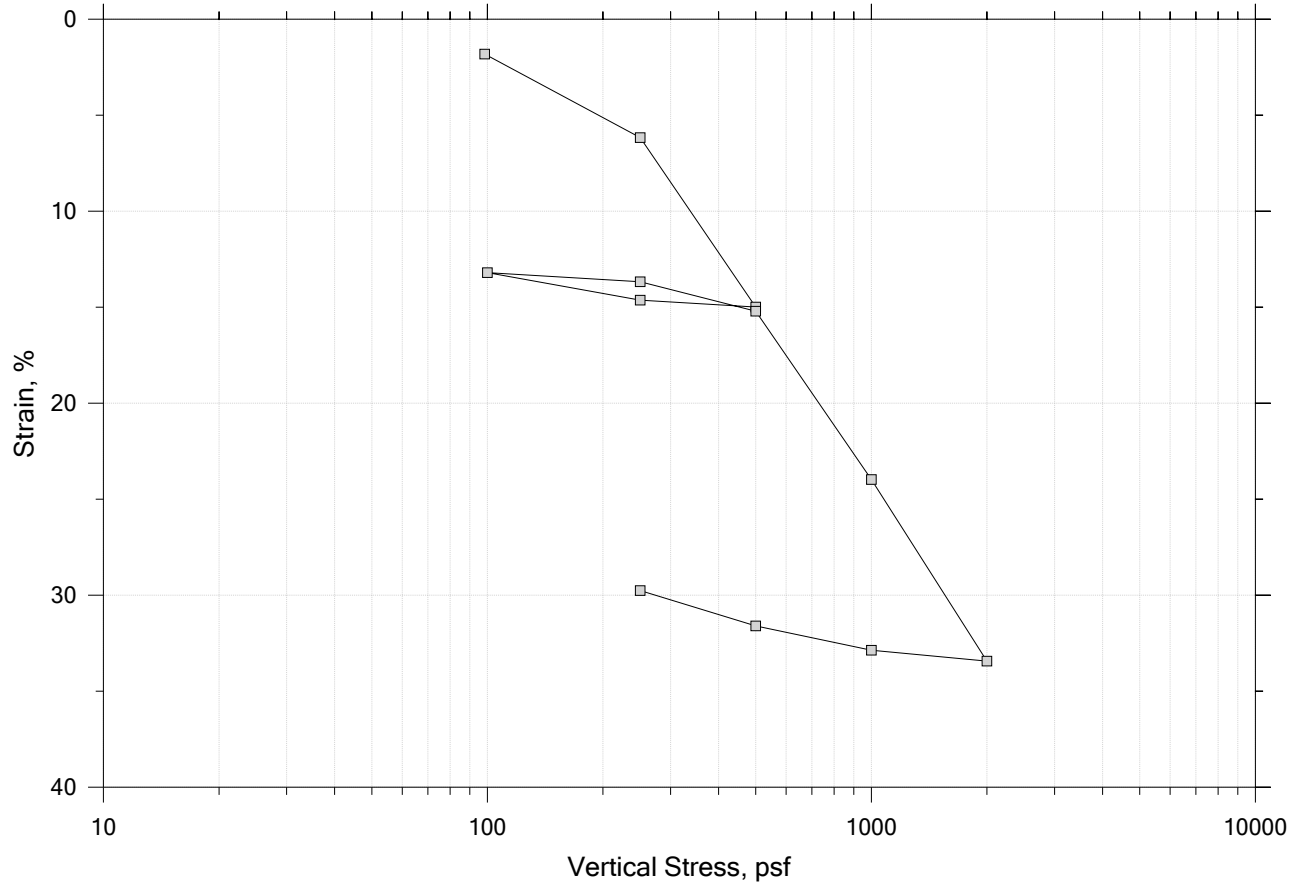
## Summary Report




 <b>APS</b> Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-1	Tested By: jm	Checked By: mcm
	Sample No.: 3	Test Date: 10/7/20	Depth: 4-6 ft
	Test No.: IP-2	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay(CH)	Measured specific gravity: 2.50	

# One-Dimensional Consolidation by ASTM D2435 - Method B

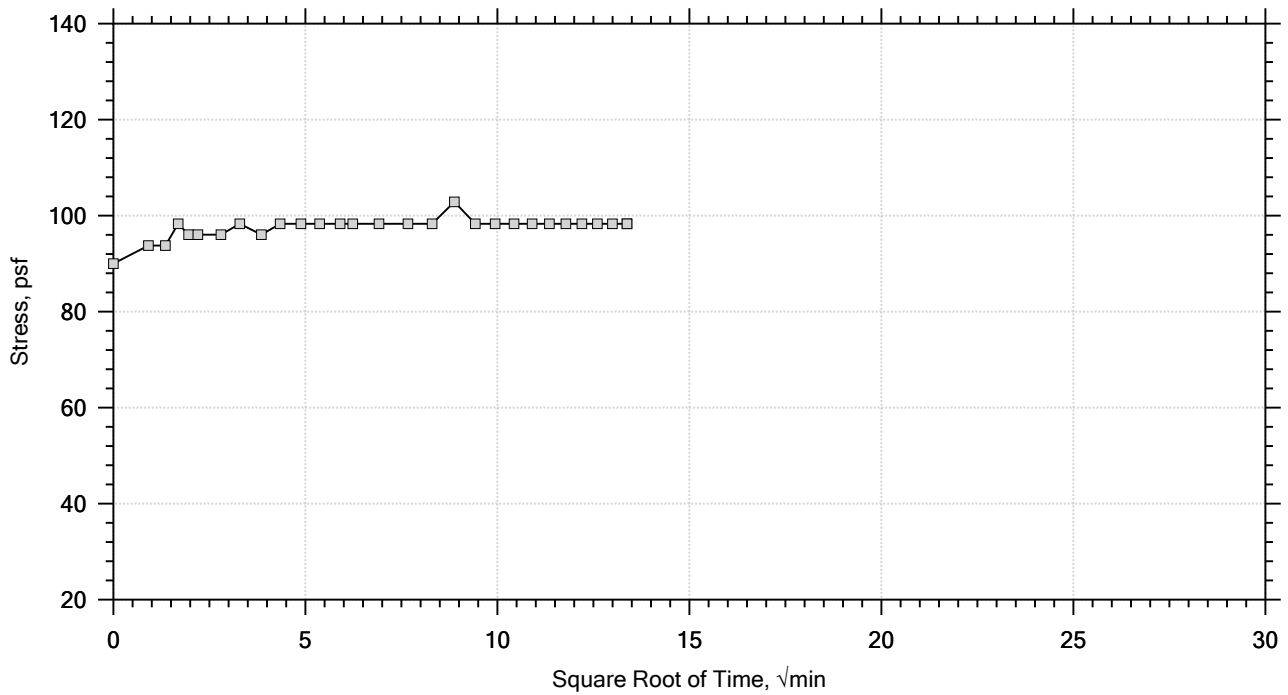
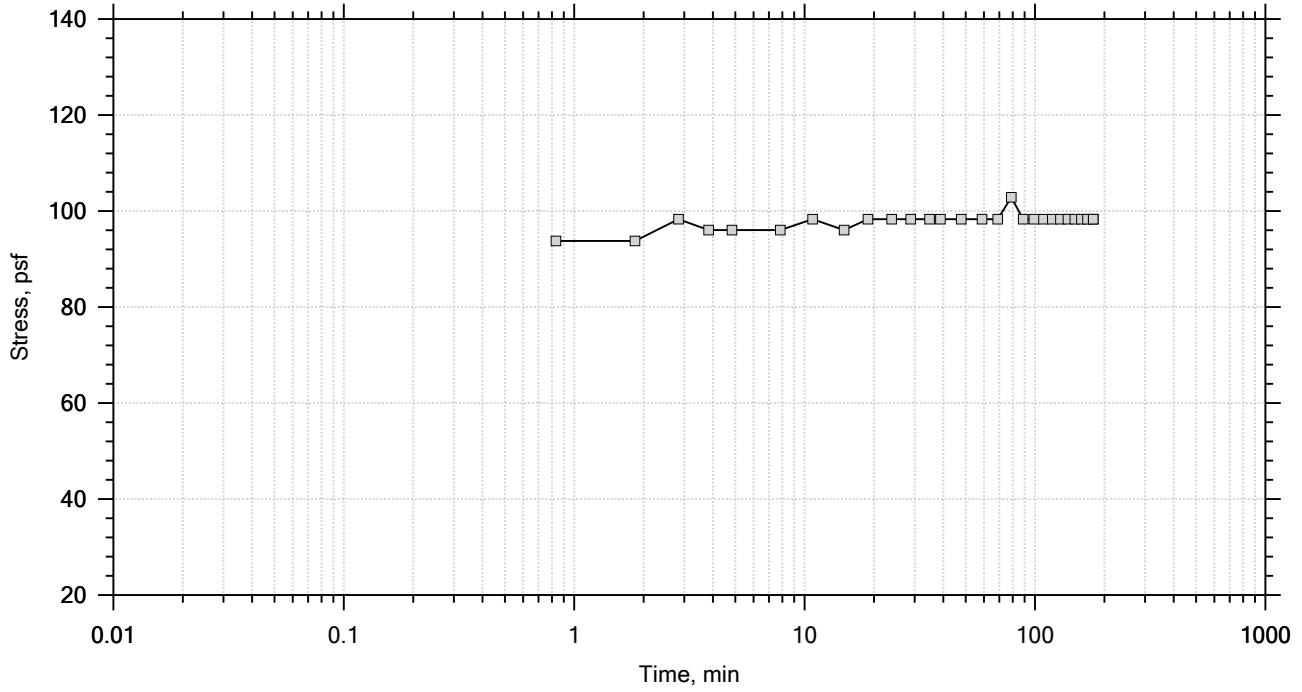
## Summary Report




 <p>Engineering and Testing</p>	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-1	Tested By: jm	Checked By: mcm
	Sample No.: 3	Test Date: 10/7/20	Depth: 4-6 ft
	Test No.: IP-2	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay (CH)		

# One-Dimensional Consolidation by ASTM D2435 - Method B

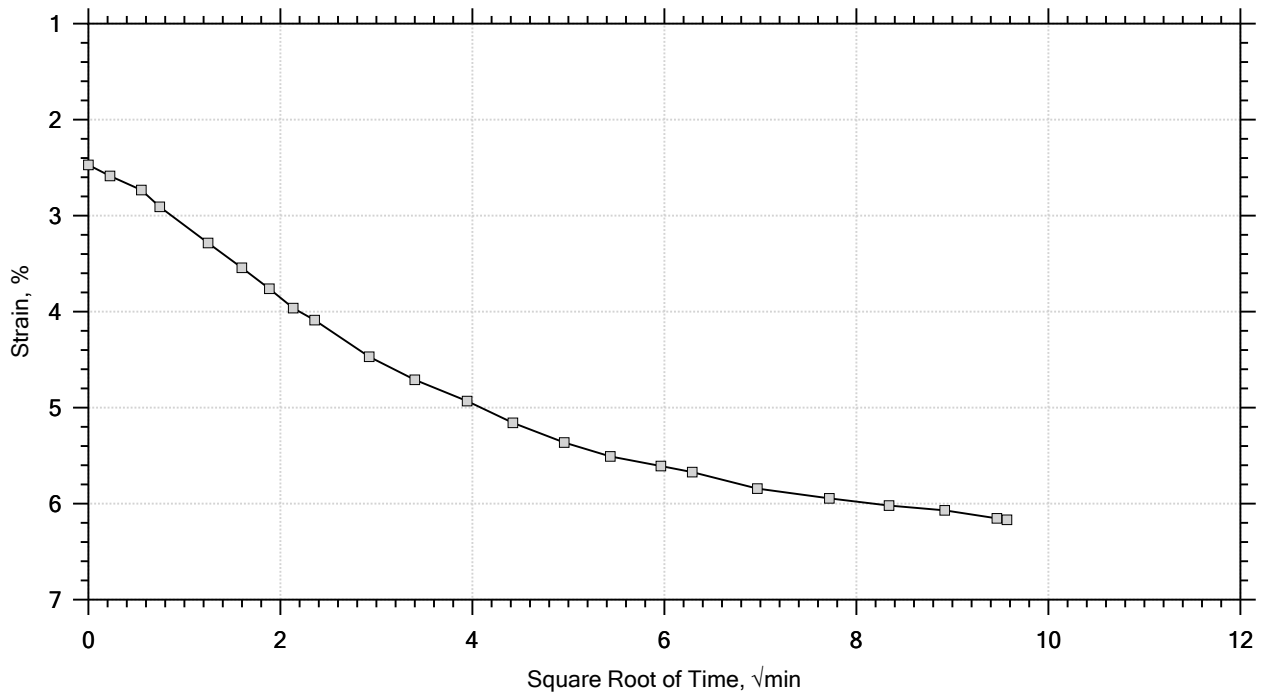
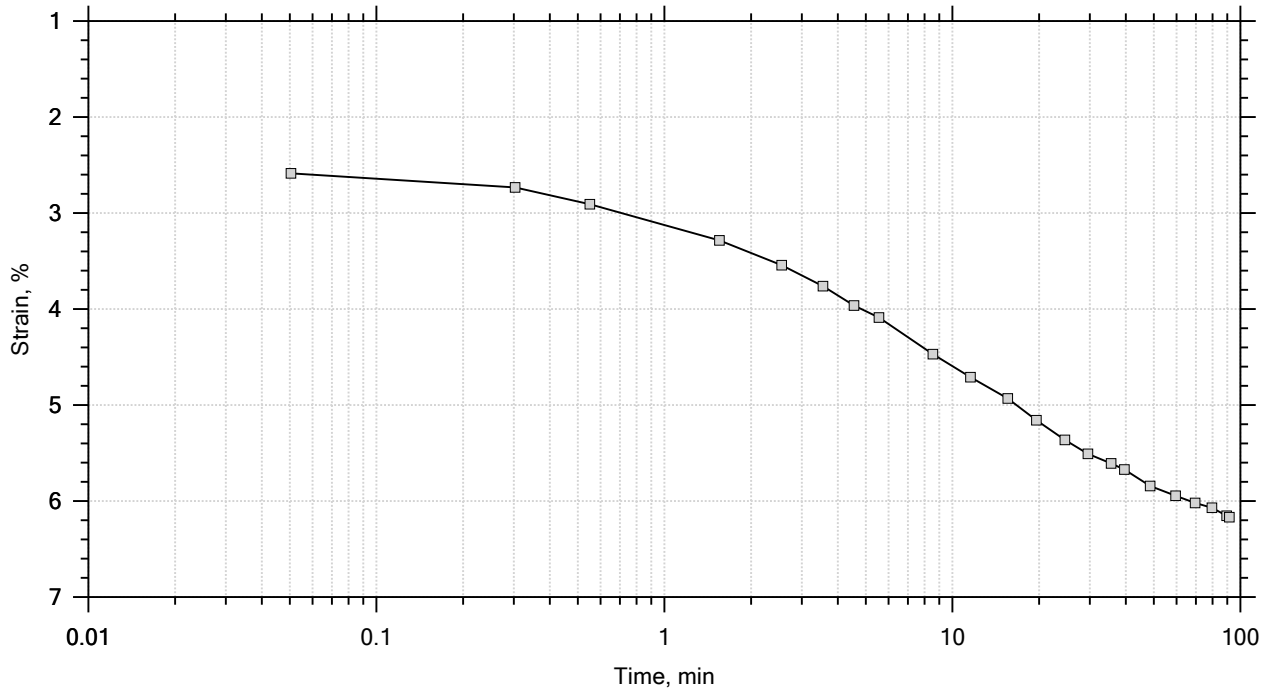
Time Curve 1 of 12  
 Constant Volume Step  
 Stress: 98.3 psf




 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-1	Tested By: jm	Checked By: mcm
	Sample No.: 3	Test Date: 10/7/20	Depth: 4-6 ft
	Test No.: IP-2	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay (CH)		

# One-Dimensional Consolidation by ASTM D2435 - Method B

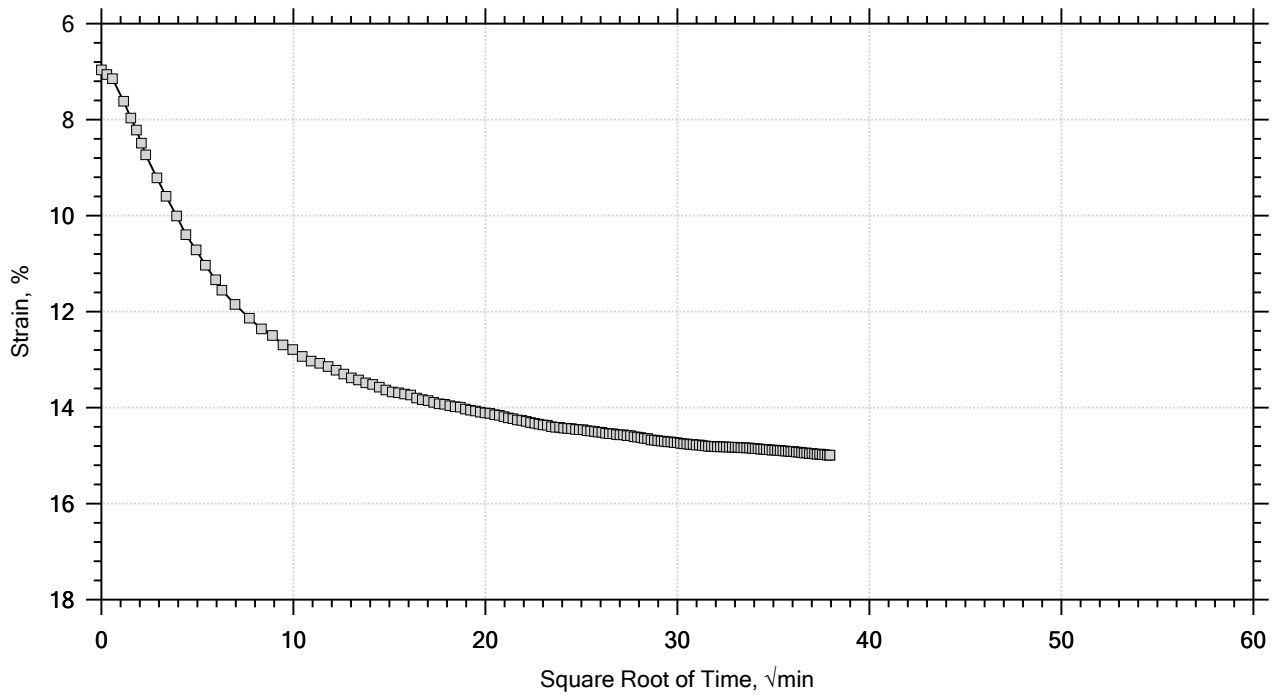
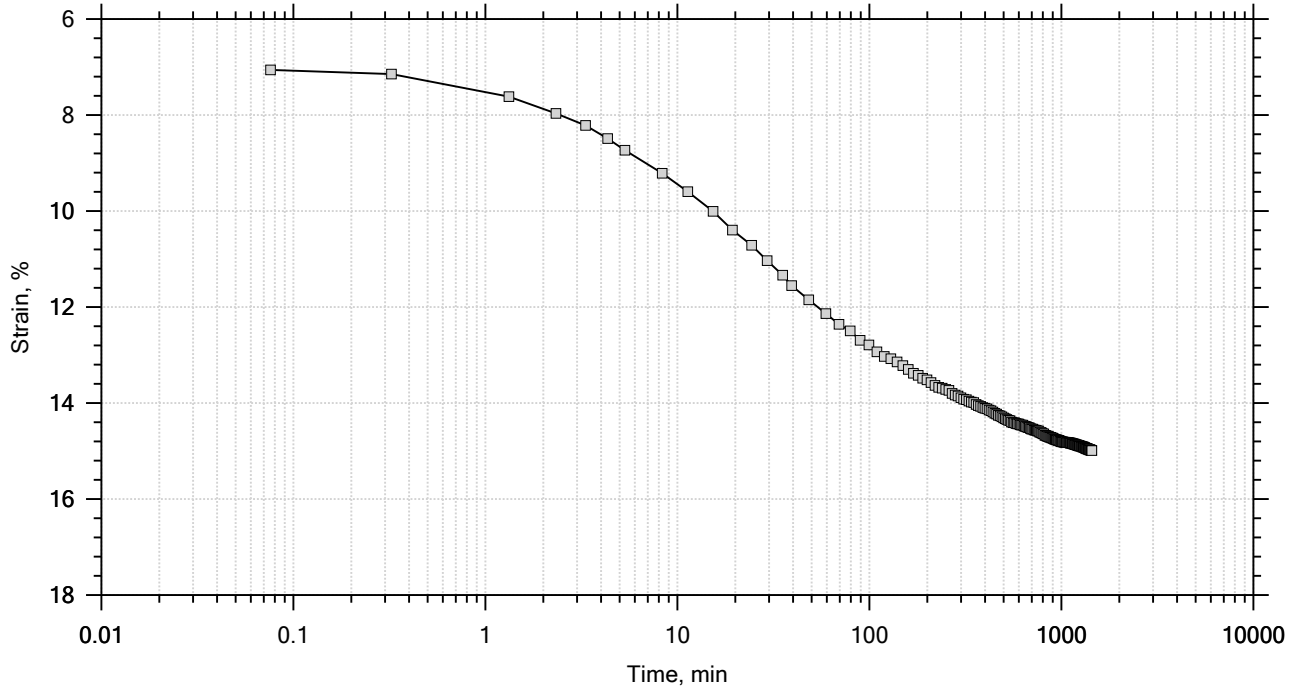
Time Curve 2 of 12  
 Constant Load Step  
 Stress: 250 psf




 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-1	Tested By: jm	Checked By: mcm
	Sample No.: 3	Test Date: 10/7/20	Depth: 4-6 ft
	Test No.: IP-2	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay (CH)		

# One-Dimensional Consolidation by ASTM D2435 - Method B

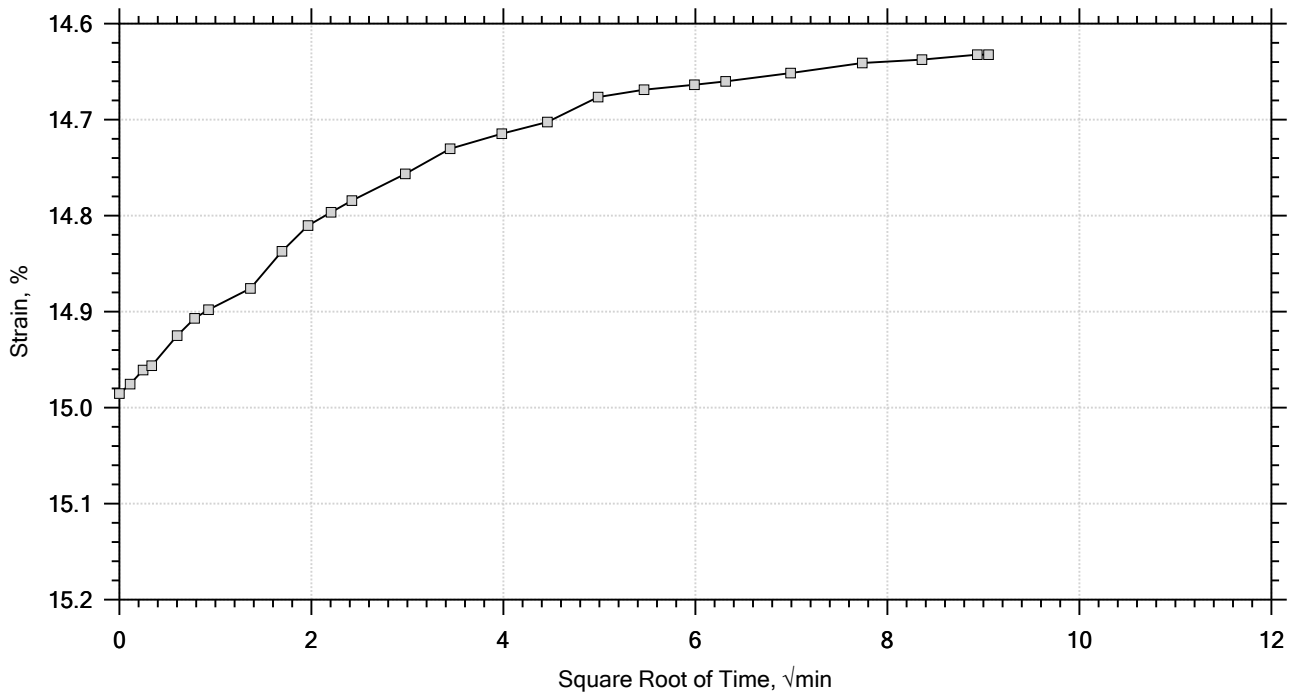
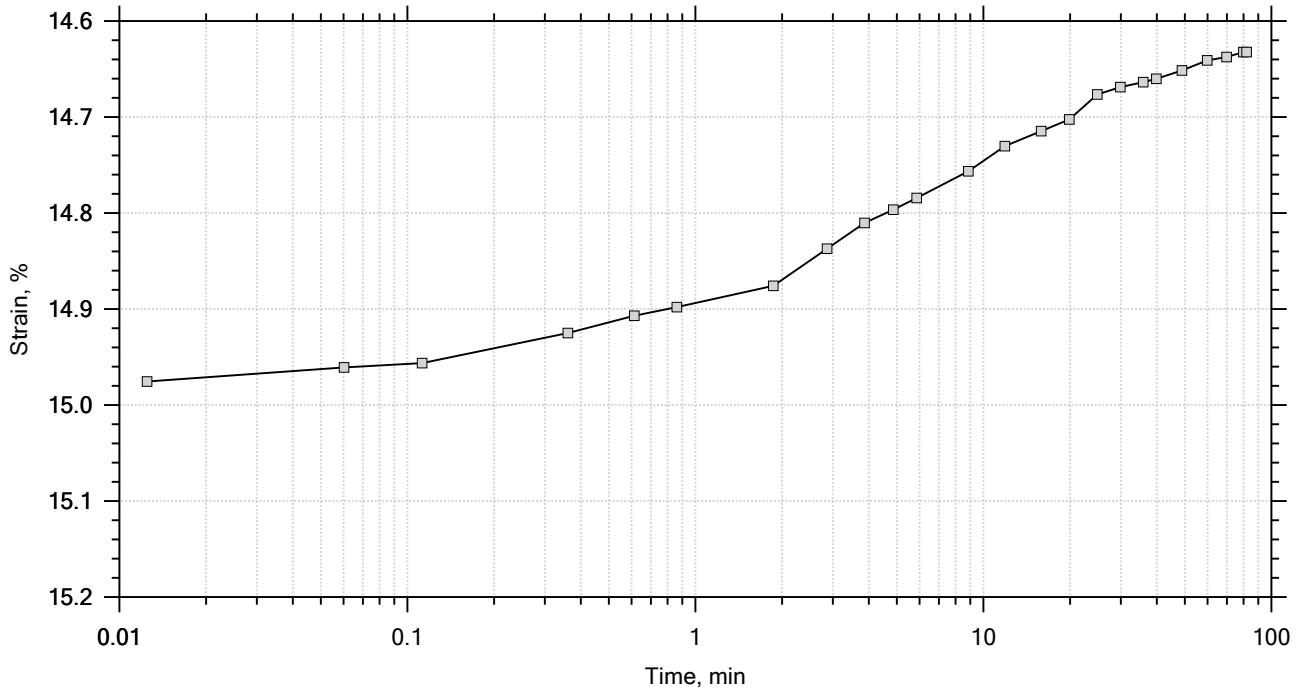
Time Curve 3 of 12  
 Constant Load Step  
 Stress: 500 psf




 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-1	Tested By: jm	Checked By: mcm
	Sample No.: 3	Test Date: 10/7/20	Depth: 4-6 ft
	Test No.: IP-2	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay (CH)		

# One-Dimensional Consolidation by ASTM D2435 - Method B

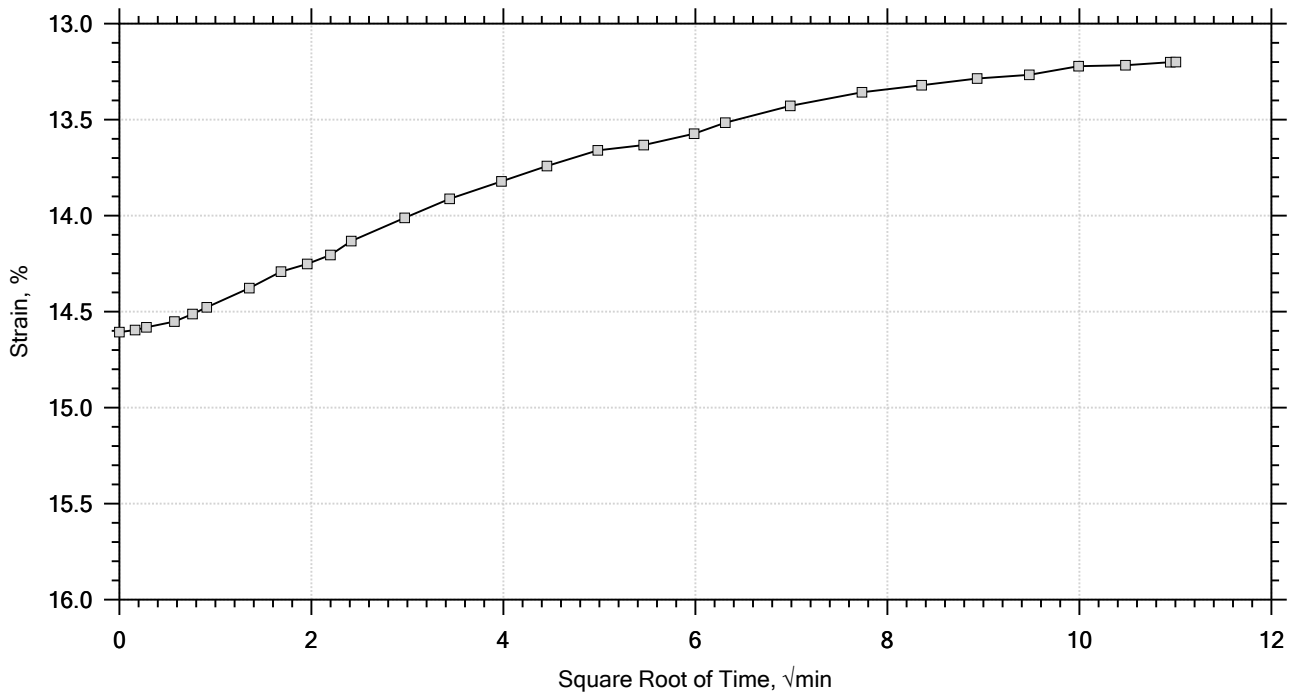
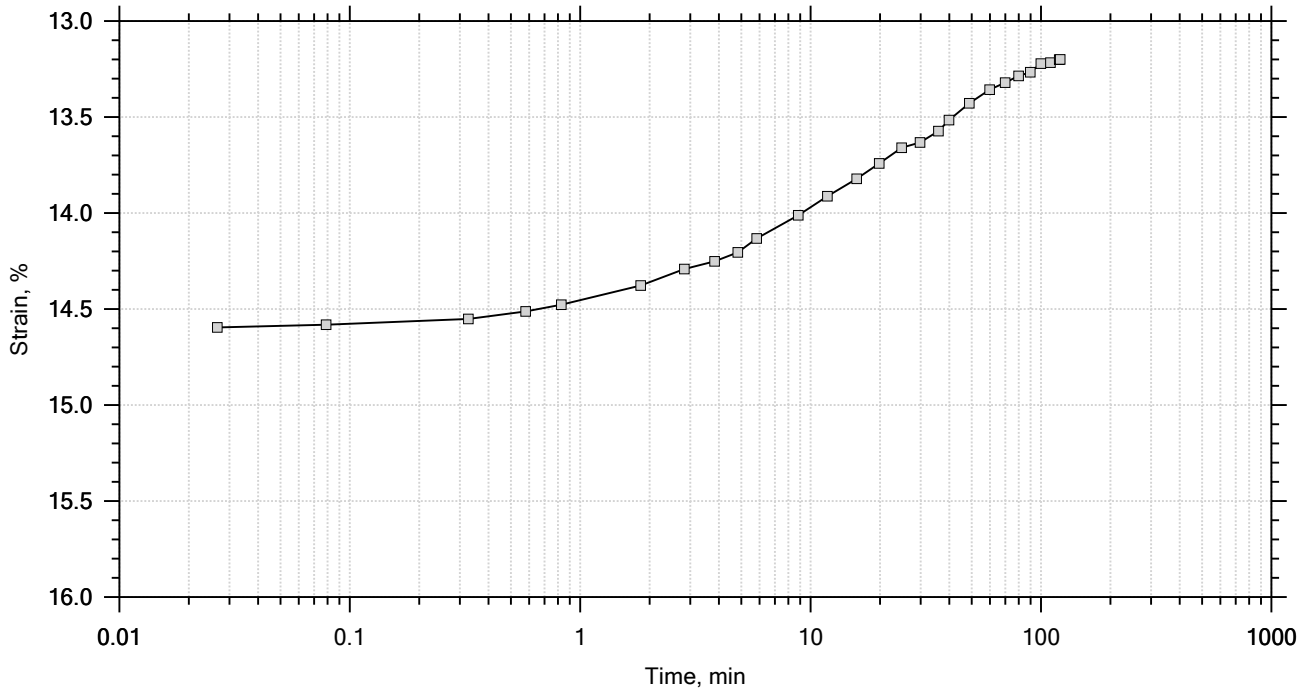
Time Curve 4 of 12  
 Constant Load Step  
 Stress: 250 psf




 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-1	Tested By: jm	Checked By: mcm
	Sample No.:3	Test Date: 10/7/20	Depth: 4-6 ft
	Test No.: IP-2	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay (CH)		

# One-Dimensional Consolidation by ASTM D2435 - Method B

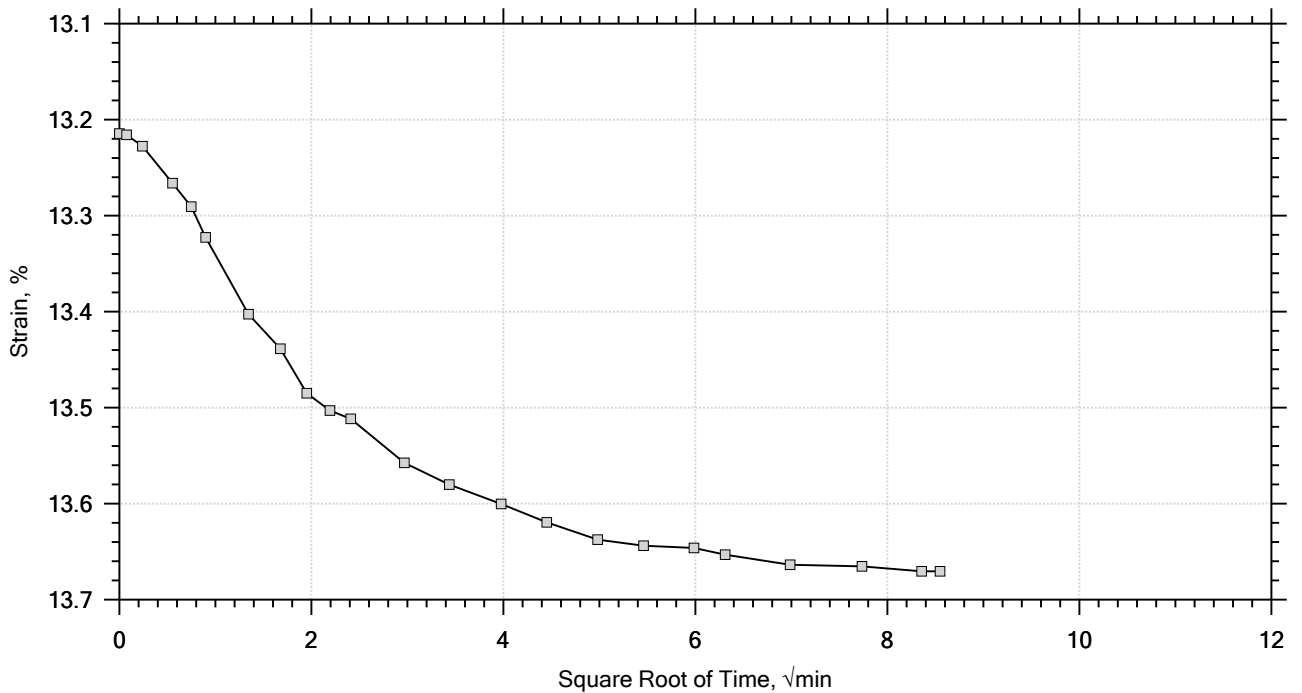
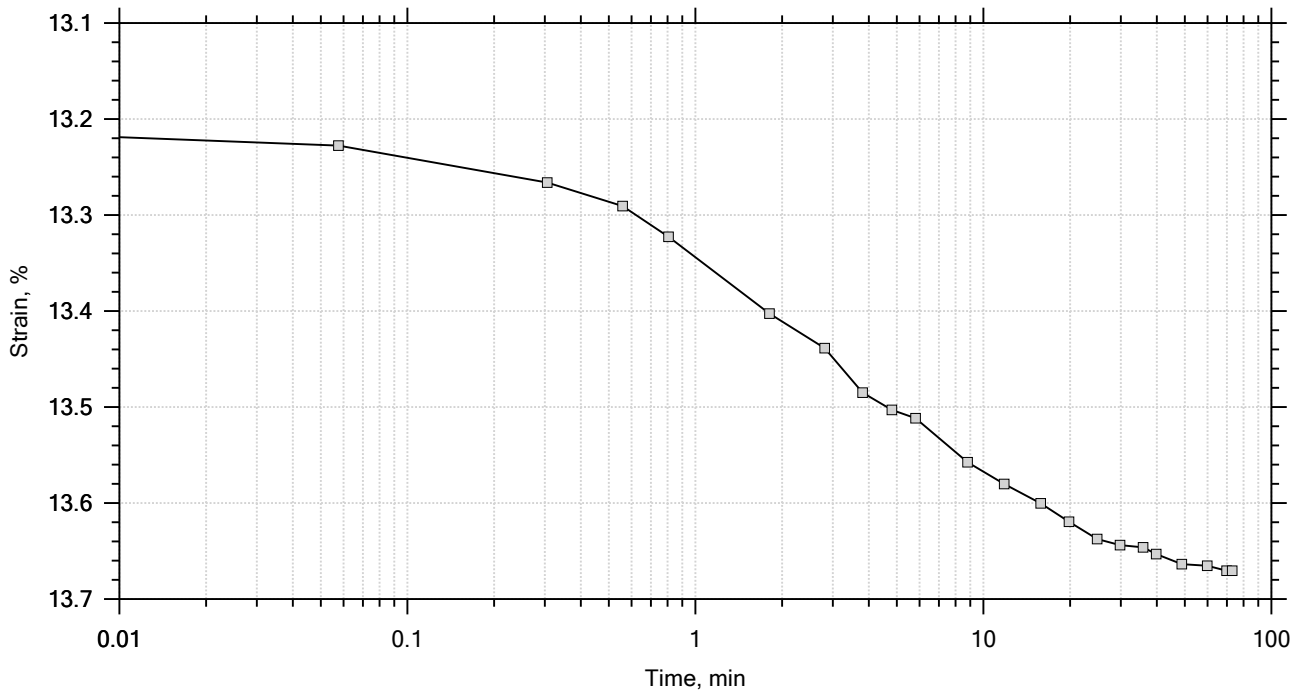
Time Curve 5 of 12  
 Constant Load Step  
 Stress: 100 psf




 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-1	Tested By: jm	Checked By: mcm
	Sample No.: 3	Test Date: 10/7/20	Depth: 4-6 ft
	Test No.: IP-2	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay (CH)		

# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 6 of 12  
 Constant Load Step  
 Stress: 250 psf

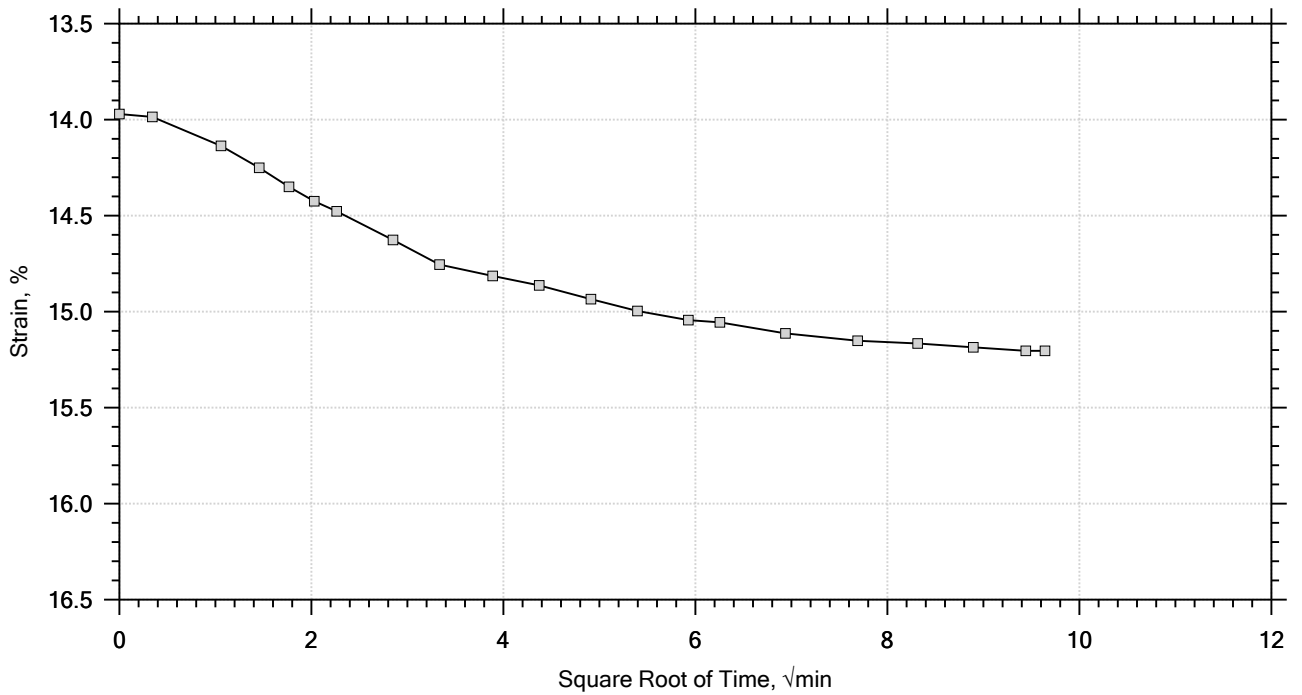
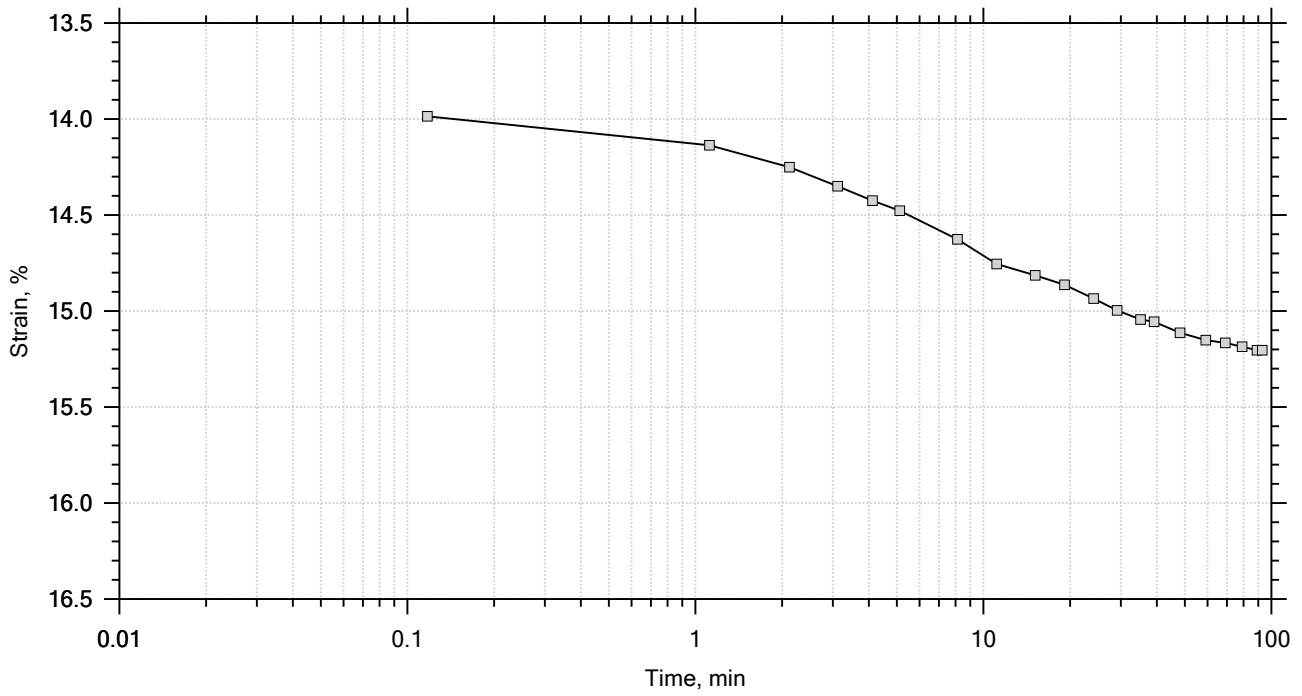



 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-1	Tested By: jm	Checked By: mcm
	Sample No.: 3	Test Date: 10/7/20	Depth: 4-6 ft
	Test No.: IP-2	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay (CH)		



# One-Dimensional Consolidation by ASTM D2435 - Method B

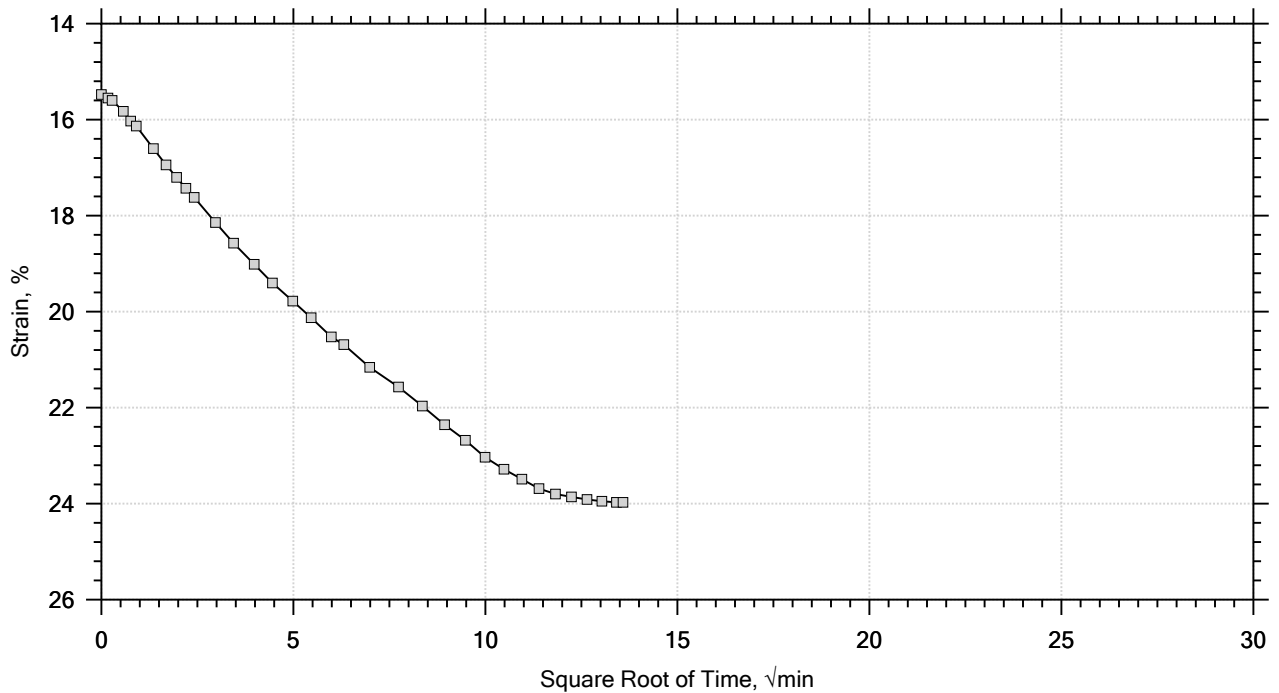
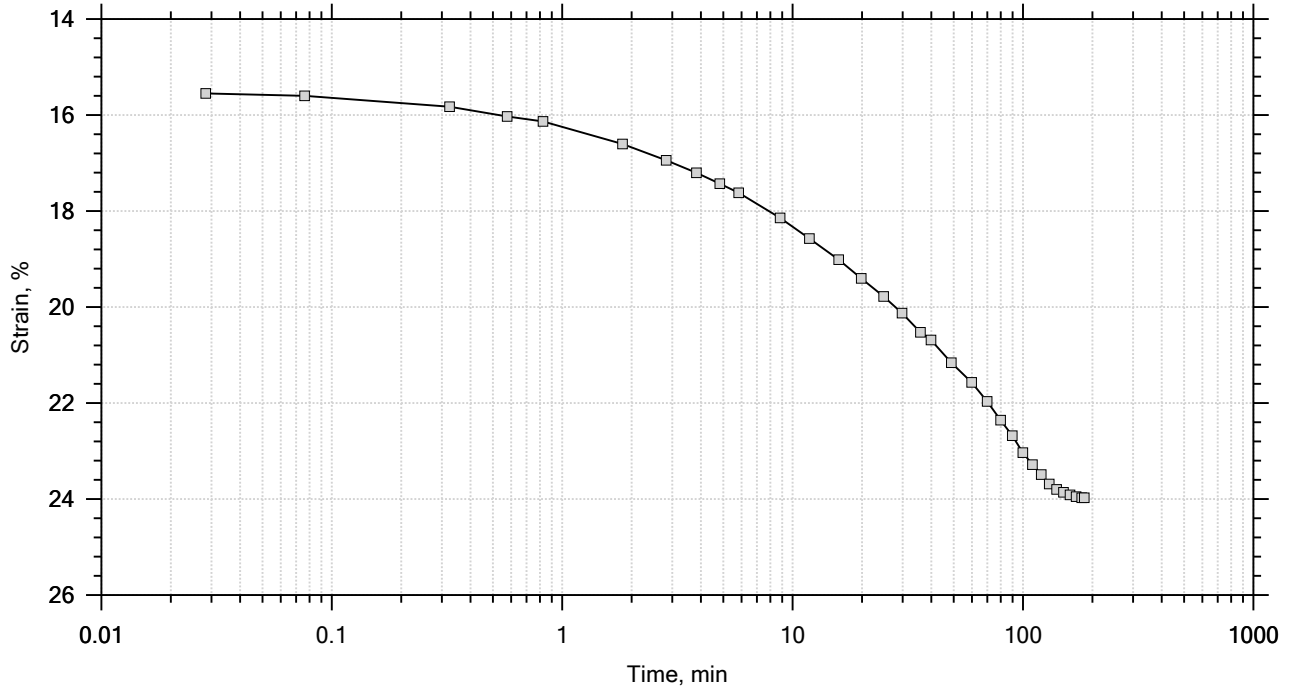
Time Curve 7 of 12  
 Constant Load Step  
 Stress: 500 psf




 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-1	Tested By: jm	Checked By: mcm
	Sample No.: 3	Test Date: 10/7/20	Depth: 4-6 ft
	Test No.: IP-2	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay (CH)		

# One-Dimensional Consolidation by ASTM D2435 - Method B

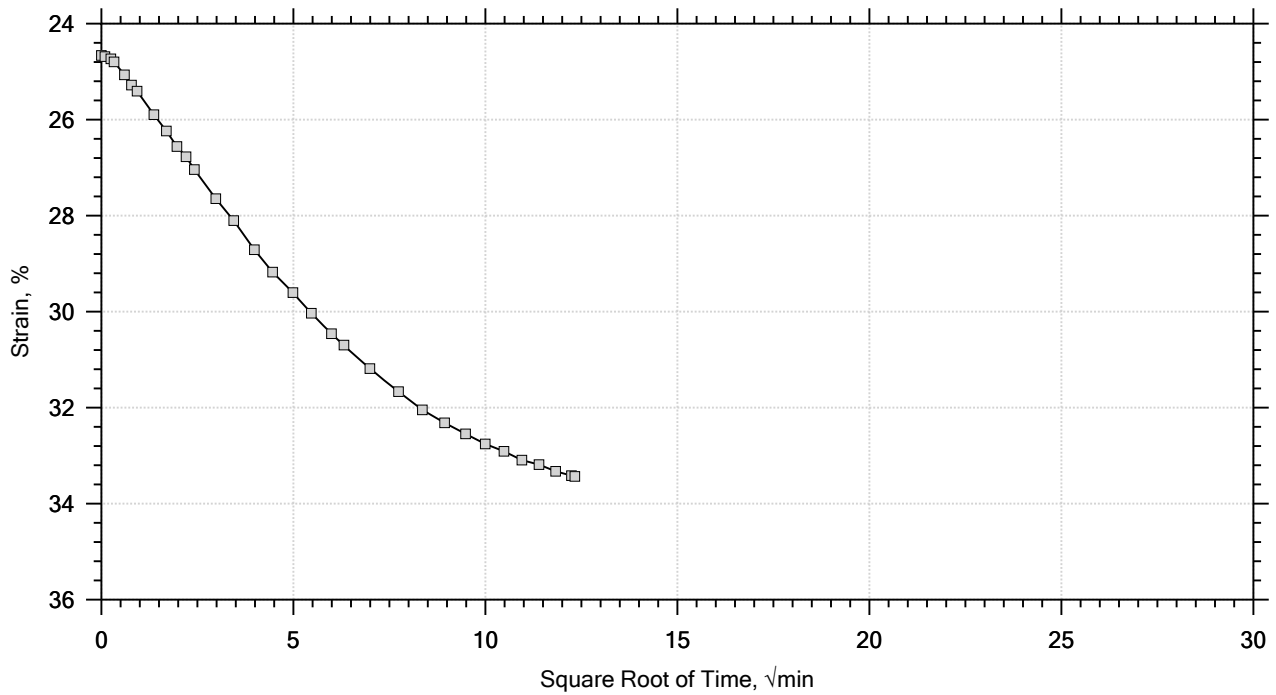
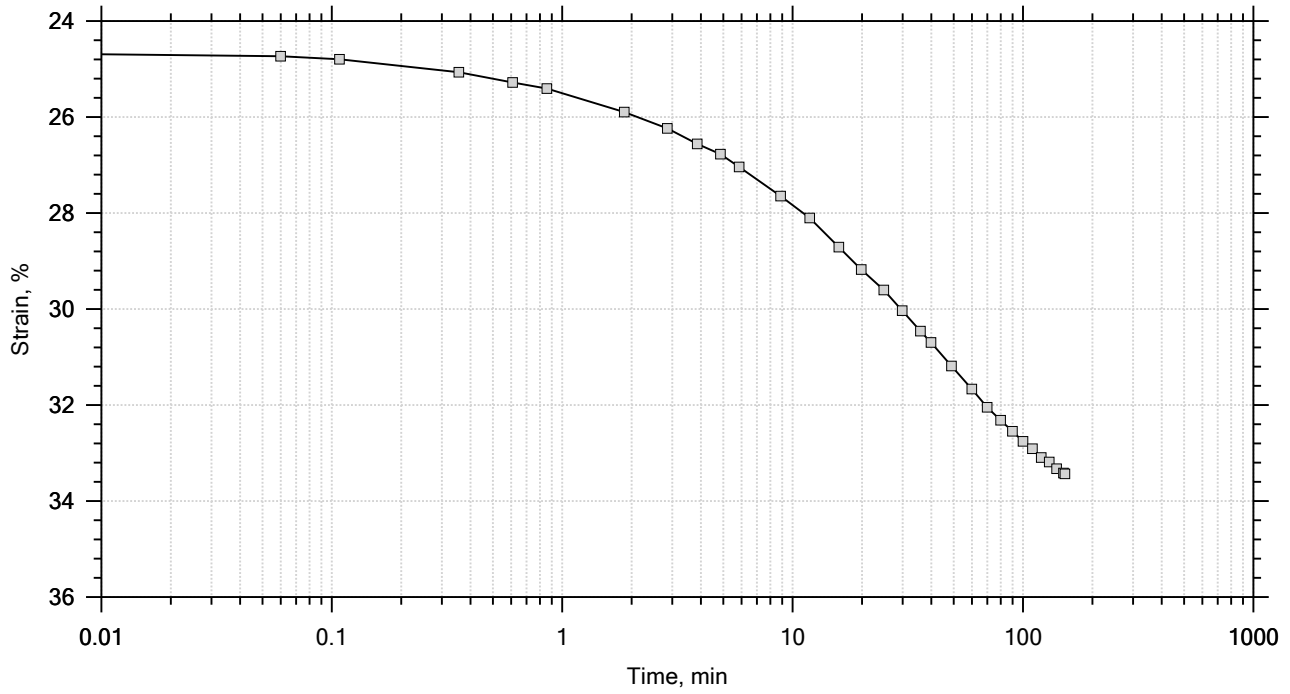
Time Curve 8 of 12  
 Constant Load Step  
 Stress: 1e+03 psf




 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-1	Tested By: jm	Checked By: mcm
	Sample No.: 3	Test Date: 10/7/20	Depth: 4-6 ft
	Test No.: IP-2	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay(CH)		

# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 9 of 12  
 Constant Load Step  
 Stress: 2e+03 psf



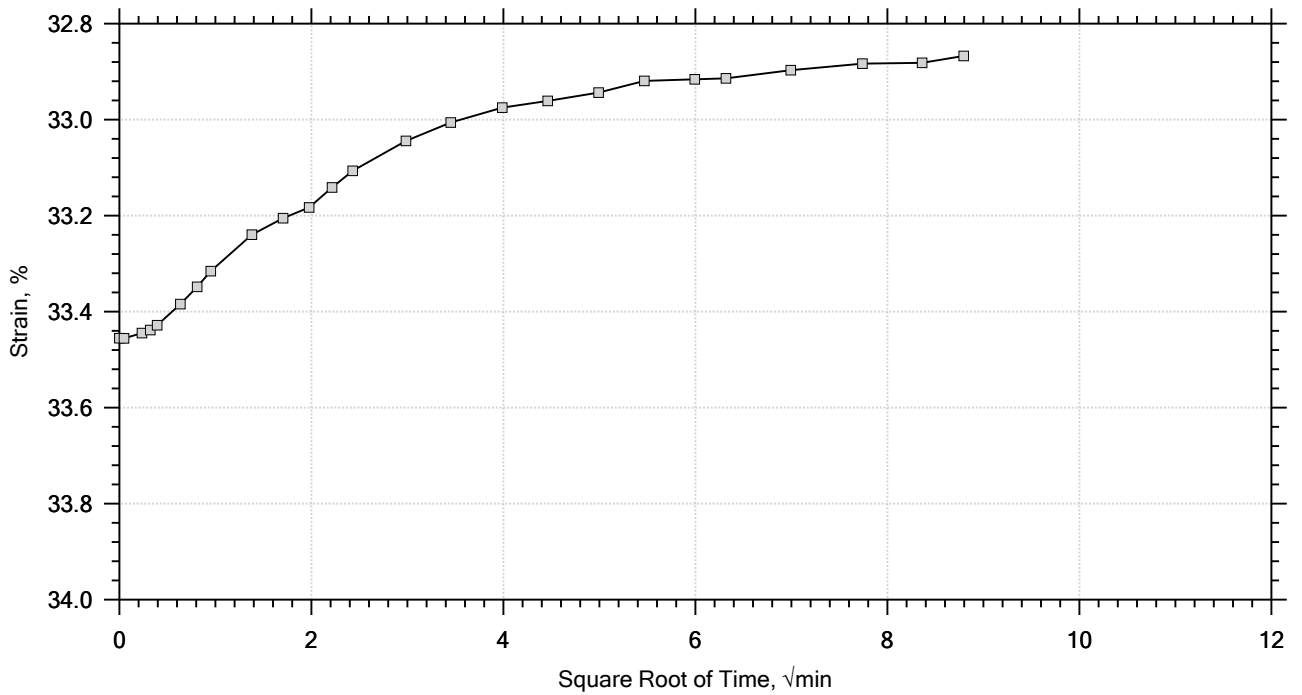
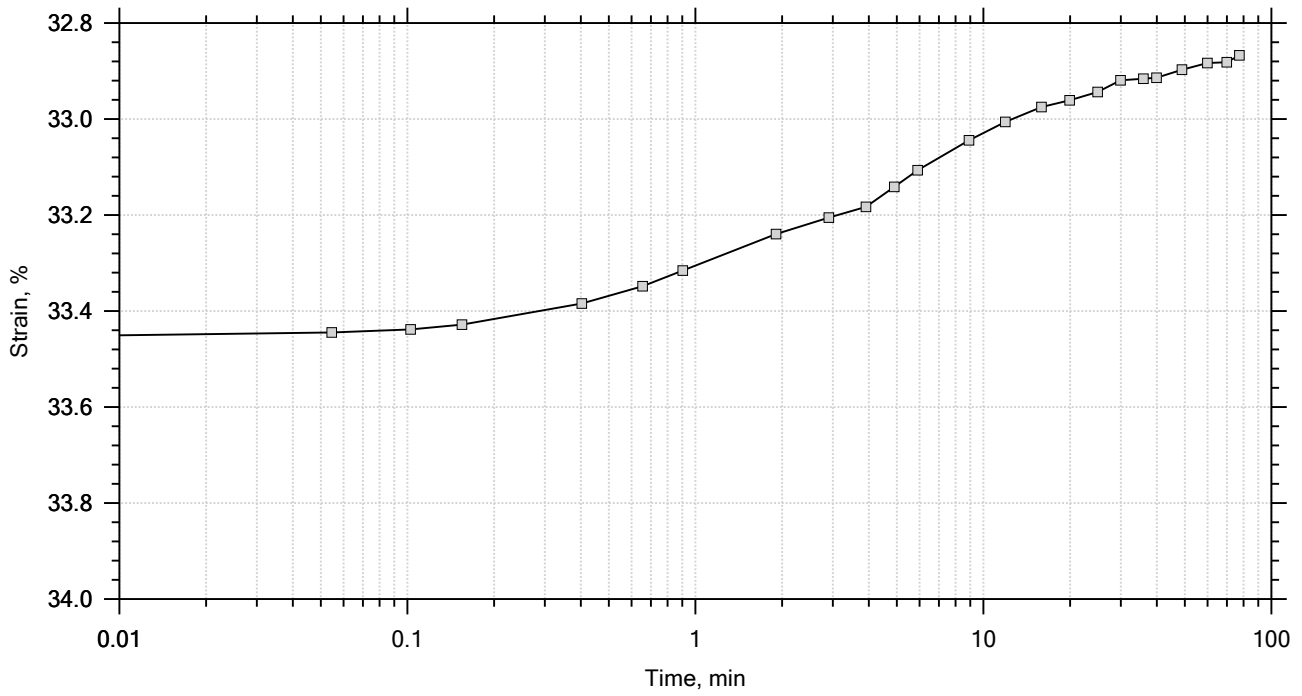
 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-1	Tested By: jm	Checked By: mcm
	Sample No.: 3	Test Date: 10/7/20	Depth: 4-6 ft
	Test No.: IP-2	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay (CH)		


# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 10 of 12

Constant Load Step

Stress: 1e+03 psf



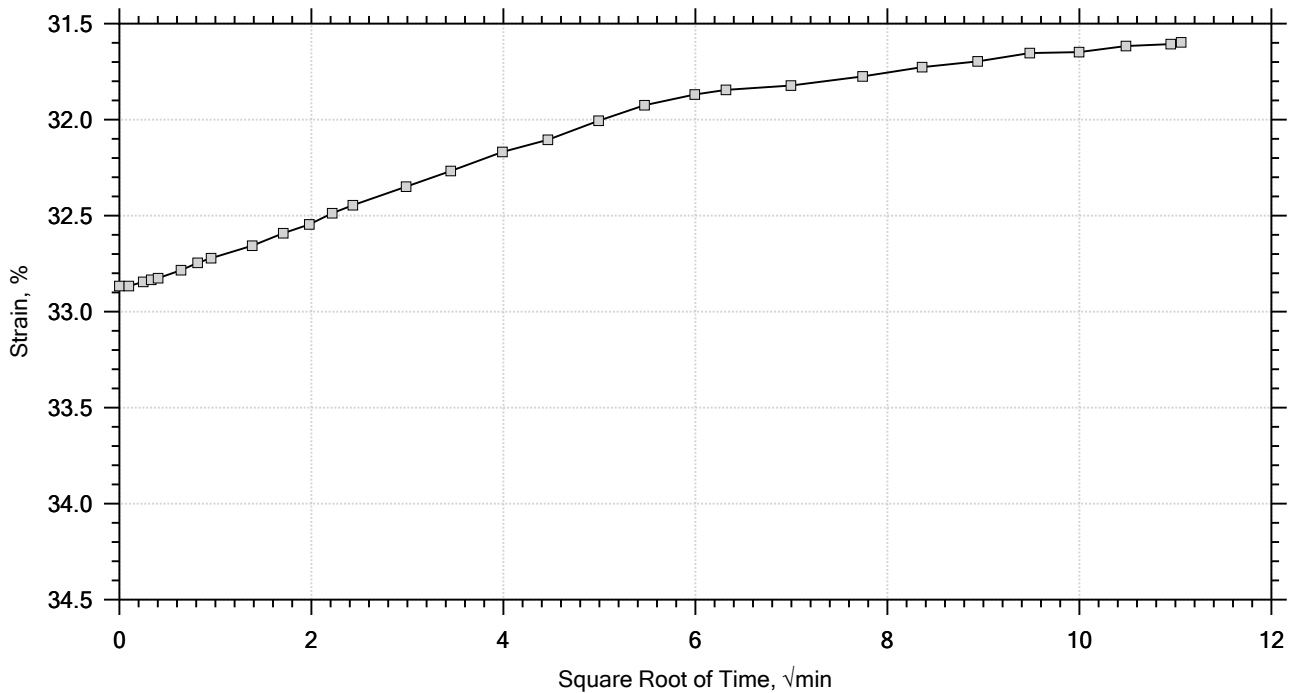
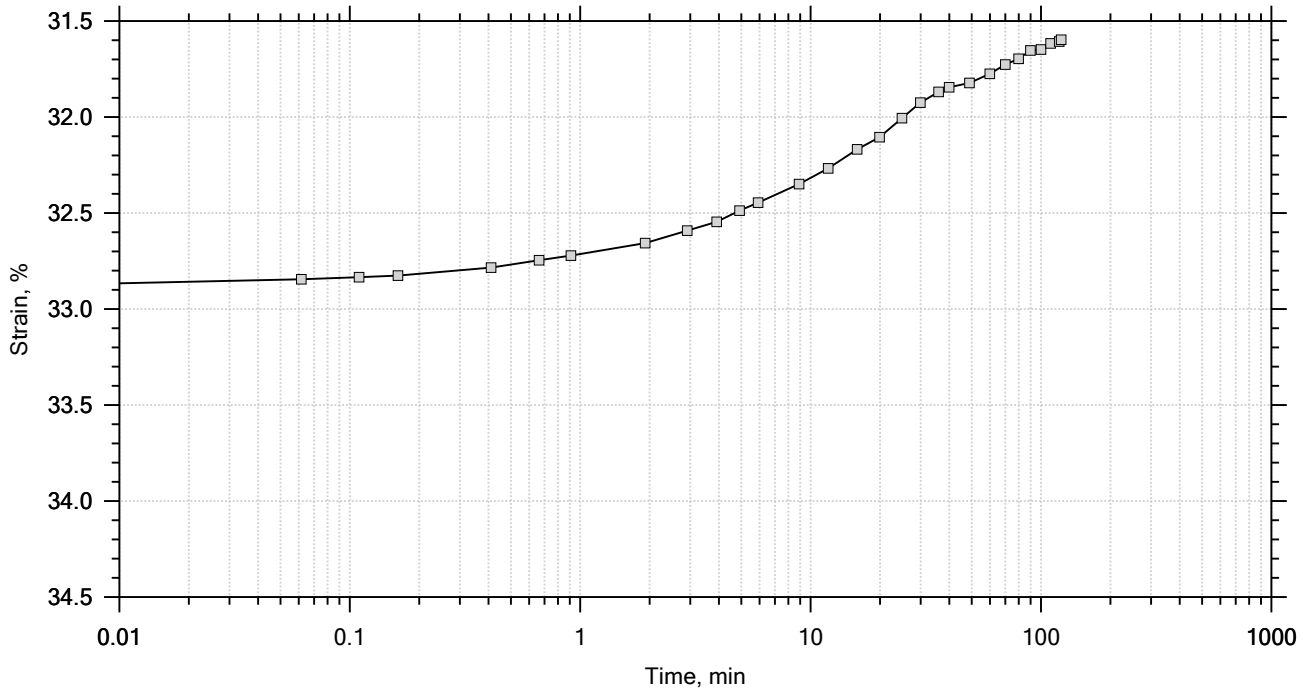
 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-1	Tested By: jm	Checked By: mcm
	Sample No.: 3	Test Date: 10/7/20	Depth: 4-6 ft
	Test No.: IP-2	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay (CH)		


# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 11 of 12

Constant Load Step

Stress: 500 psf



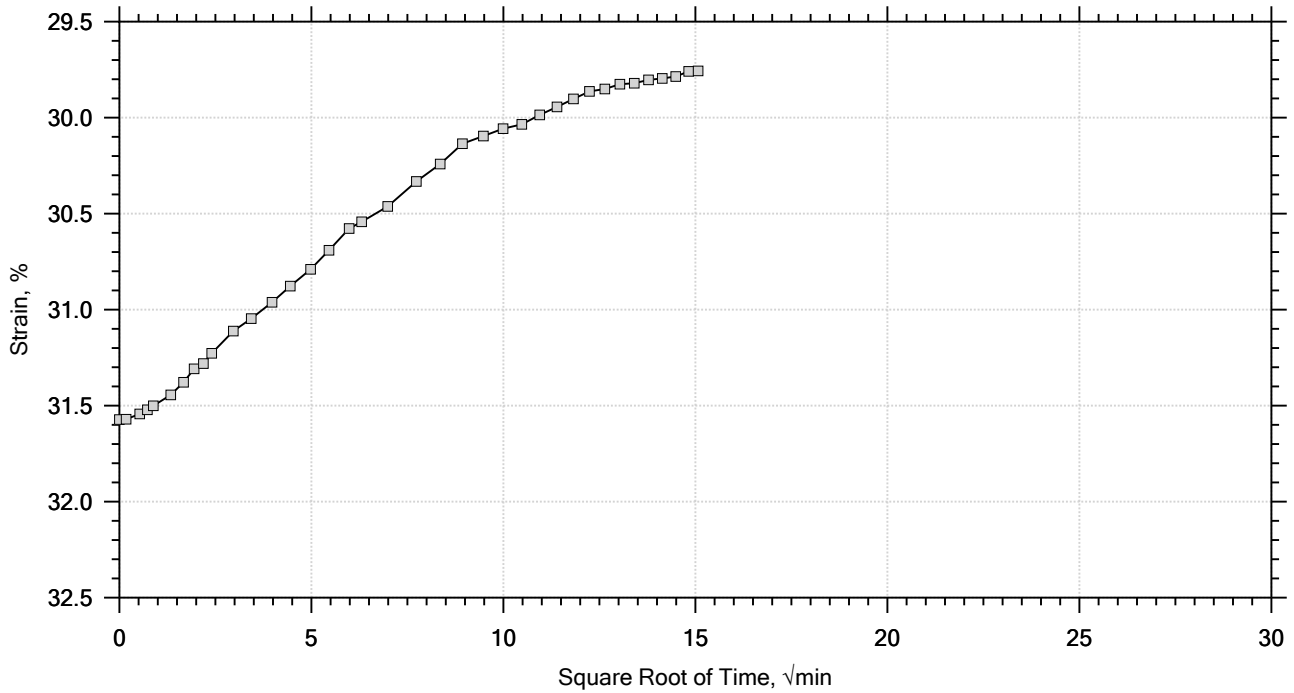
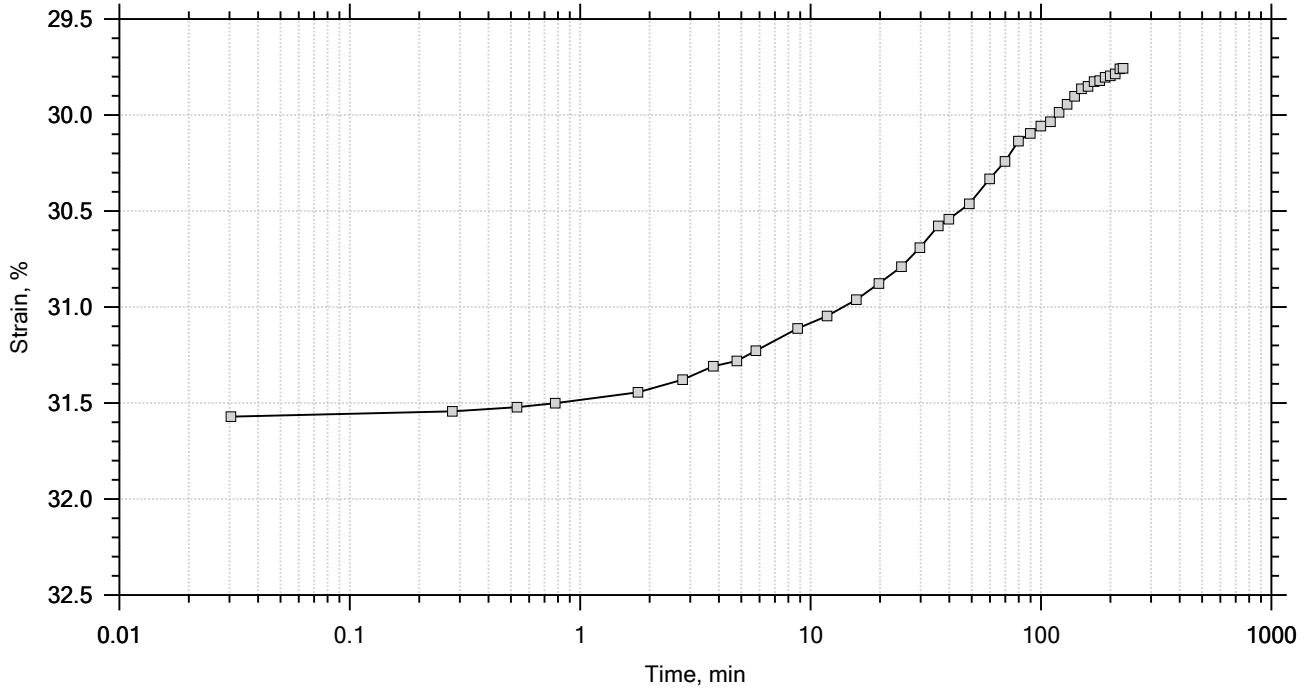
 <p>Engineering and Testing</p>	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-1	Tested By: jm	Checked By: mcm
	Sample No.: 3	Test Date: 10/7/20	Depth: 4-6 ft
	Test No.: IP-2	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay (CH)		


# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 12 of 12

Constant Load Step

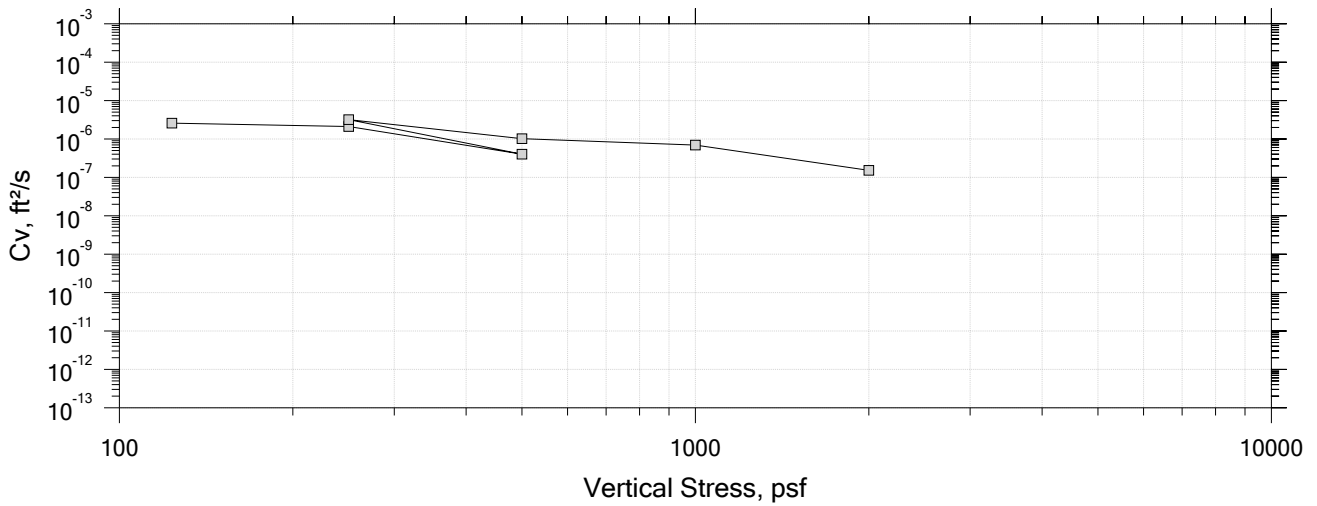
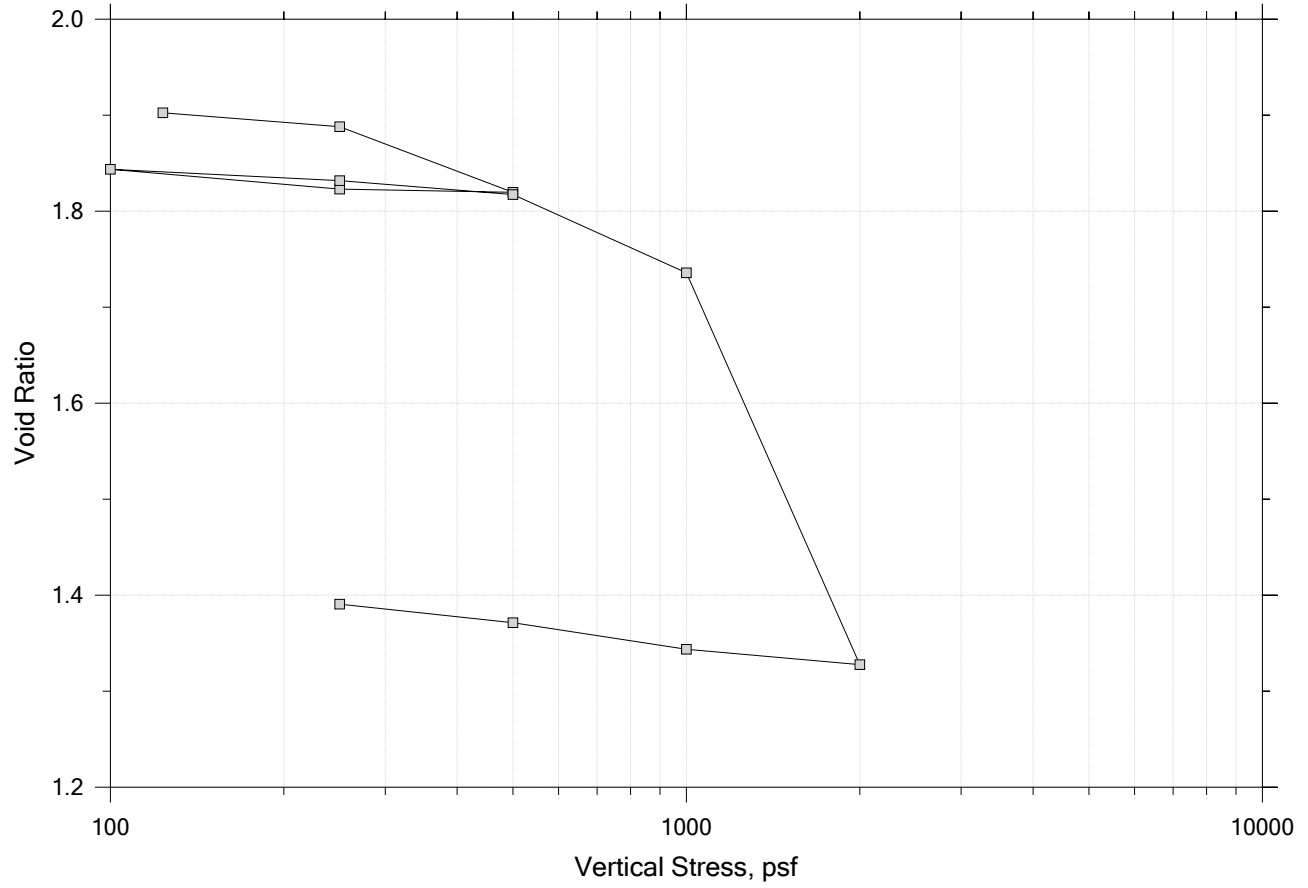
Stress: 250 psf




 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-1	Tested By: jm	Checked By: mcm
	Sample No.: 3	Test Date: 10/7/20	Depth: 4-6 ft
	Test No.: IP-2	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay (CH)		

# One-Dimensional Consolidation by ASTM D2435 - Method B

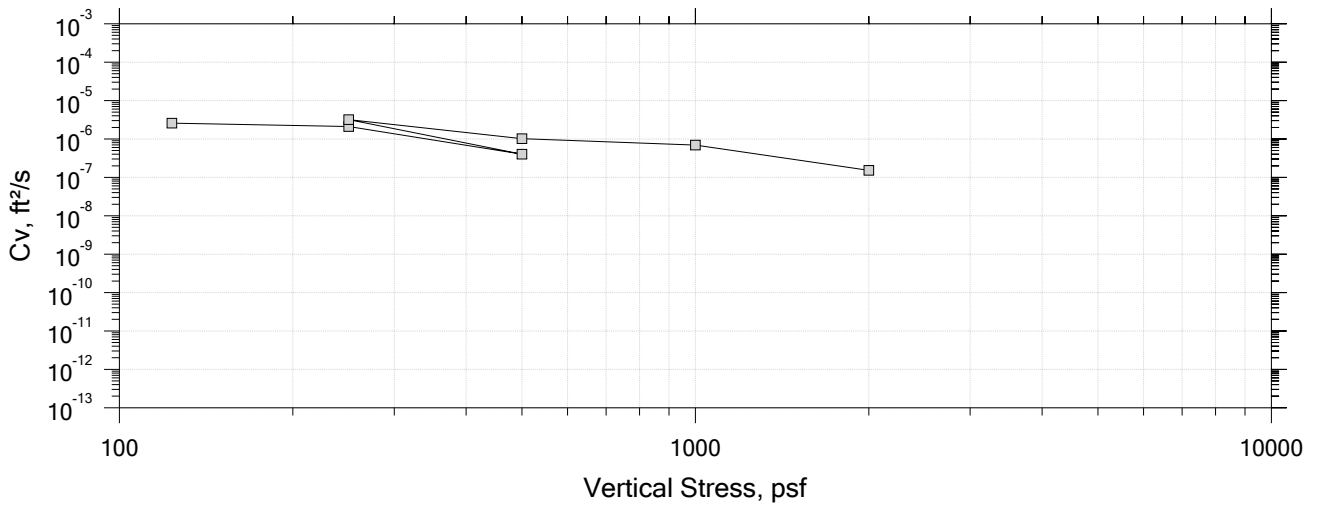
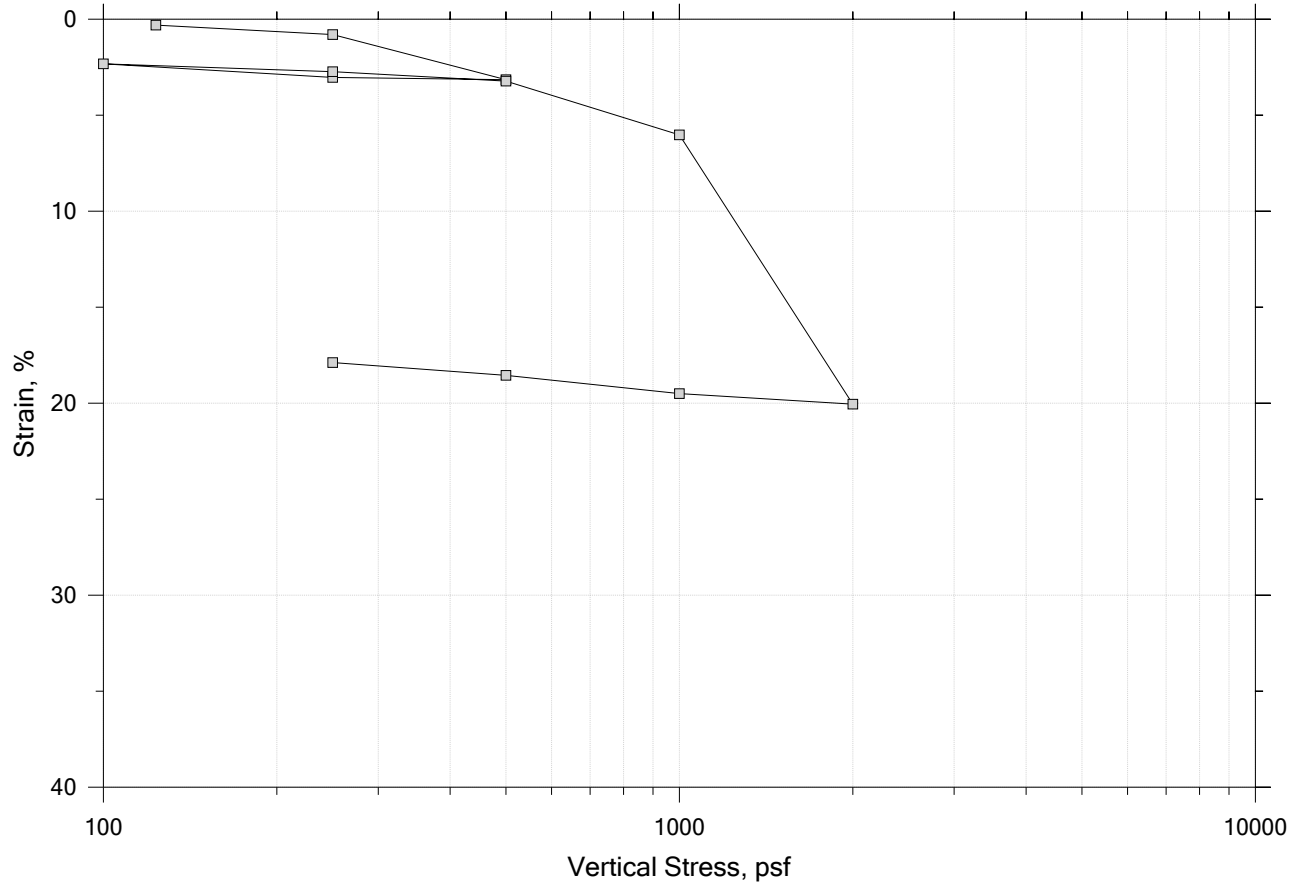
## Summary Report




 <p>Engineering and Testing</p>	Project: Breton Lakebridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-1	Tested By: jm	Checked By: mcm
	Sample No.: 9	Test Date: 10/7/20	Depth: 16-18 ft
	Test No.: IP-3	Sample Type: intact	Elevation: ---
	Description: Moist, greenish gray clay(CH)	Measured specific gravity: 2.62	

# One-Dimensional Consolidation by ASTM D2435 - Method B

## Summary Report

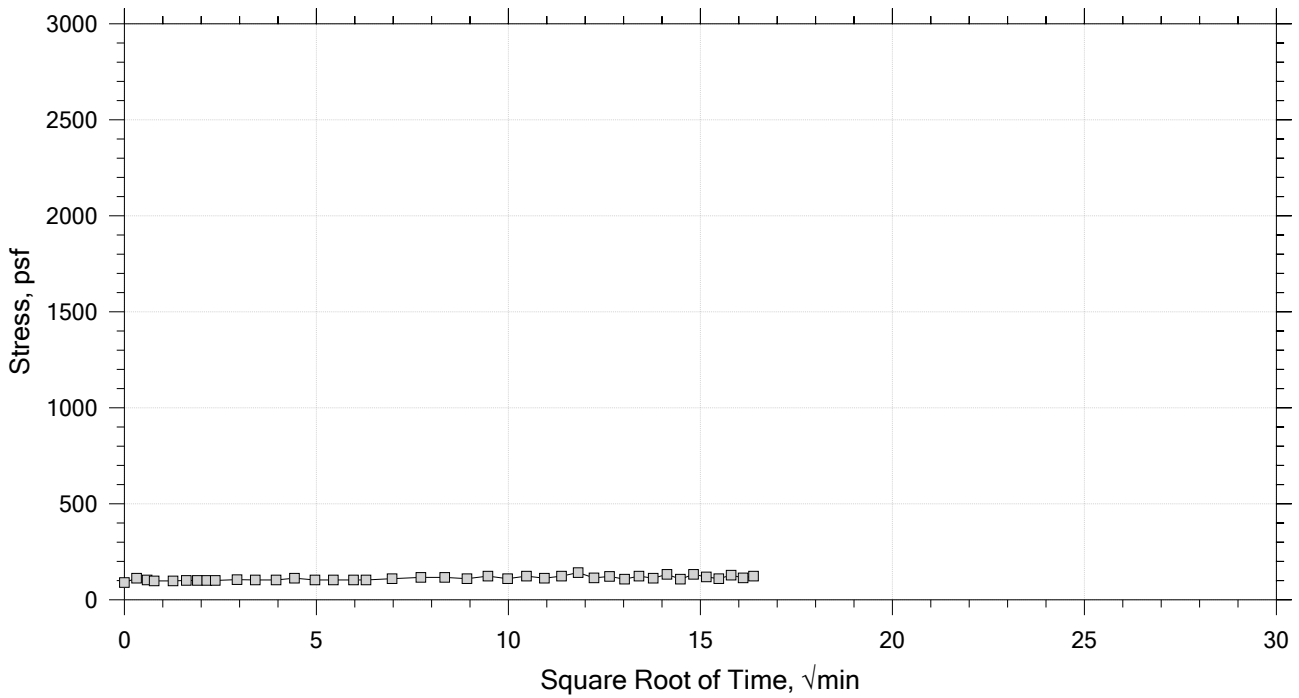
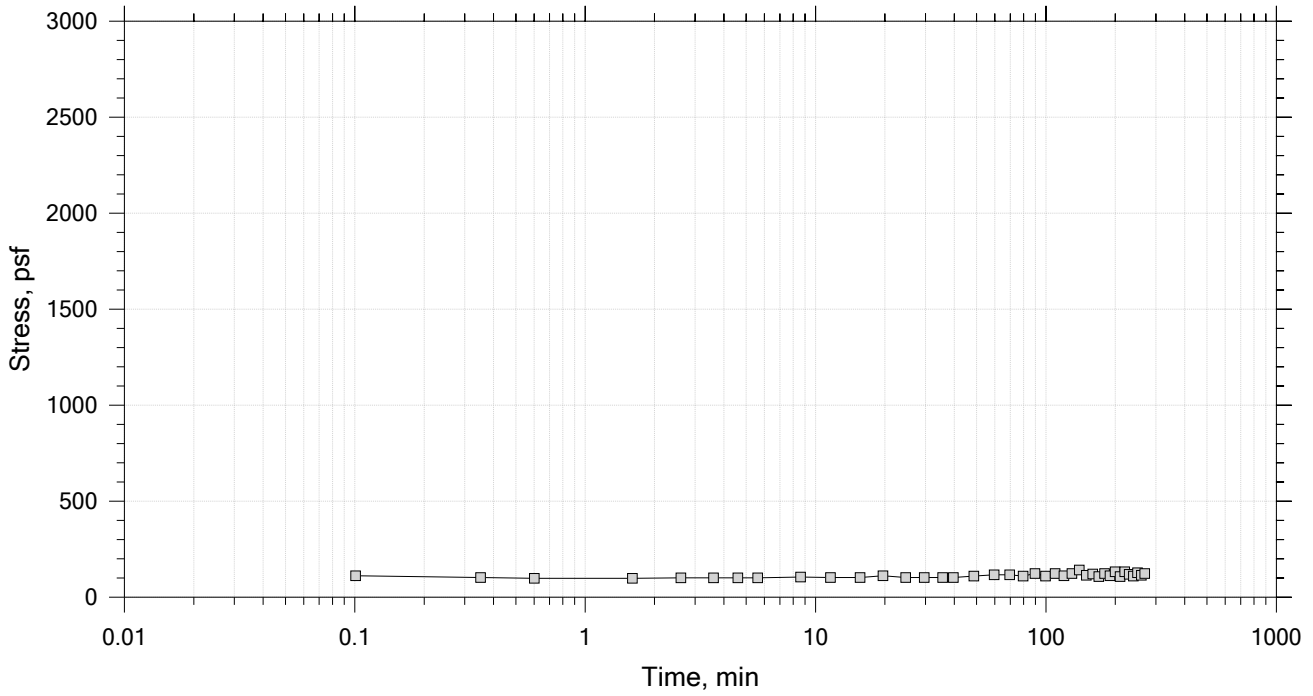



 <p>Engineering and Testing</p>	Project: Breton Lakebridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-1	Tested By: jm	Checked By: mcm
	Sample No.: 9	Test Date: 10/7/20	Depth: 16-18 ft
	Test No.: IP-3	Sample Type: intact	Elevation: ---
	Description: Moist, greenish gray clay (CH)		



# One-Dimensional Consolidation by ASTM D2435 - Method B

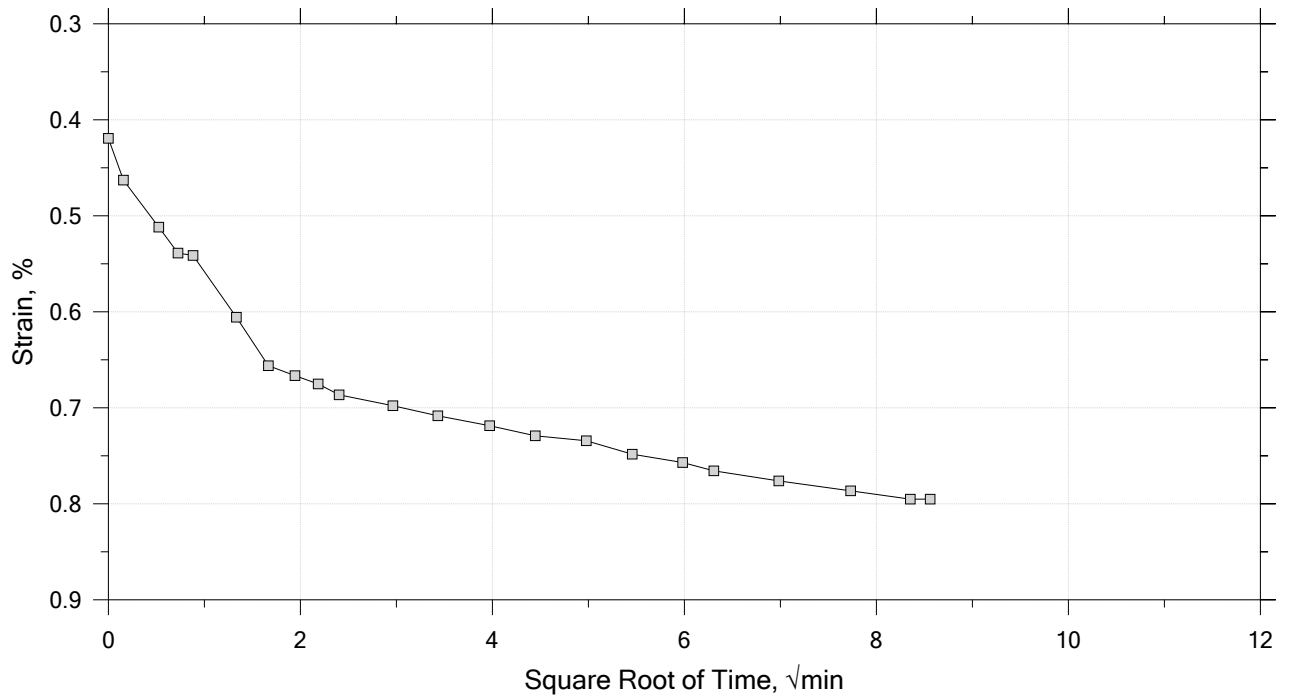
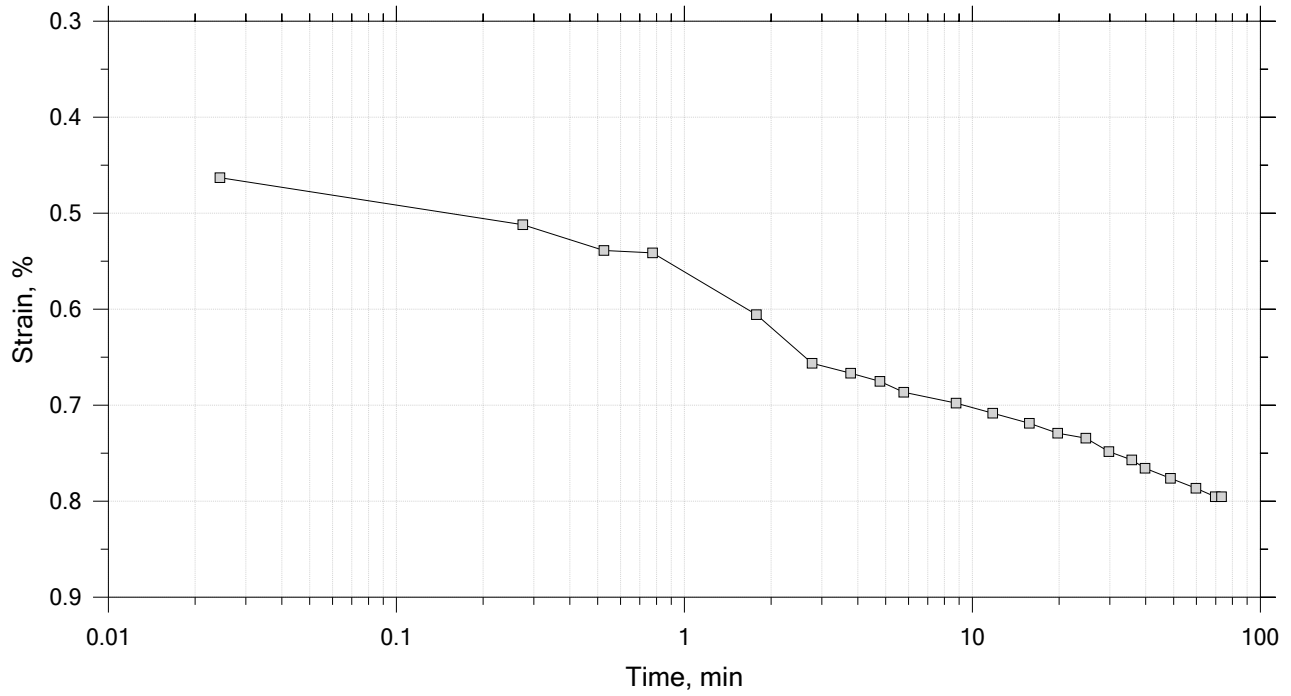
Time Curve 1 of 12  
 Constant Volume Step  
 Stress: 123 psf




 Engineering and Testing	Project: Breton Lakebridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-1	Tested By: jm	Checked By: mcm
	Sample No.: 9	Test Date: 10/7/20	Depth: 16-18 ft
	Test No.: IP-3	Sample Type: intact	Elevation: ---
	Description: Moist, greenish gray clay(CH)		

# One-Dimensional Consolidation by ASTM D2435 - Method B

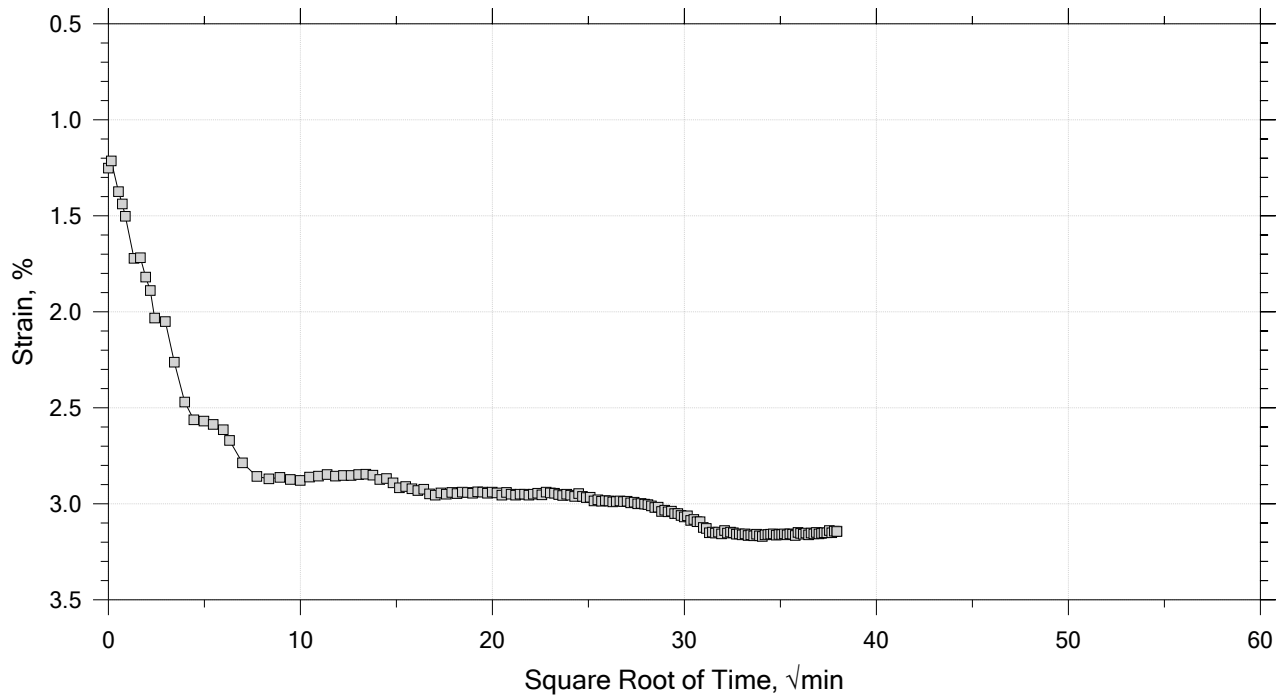
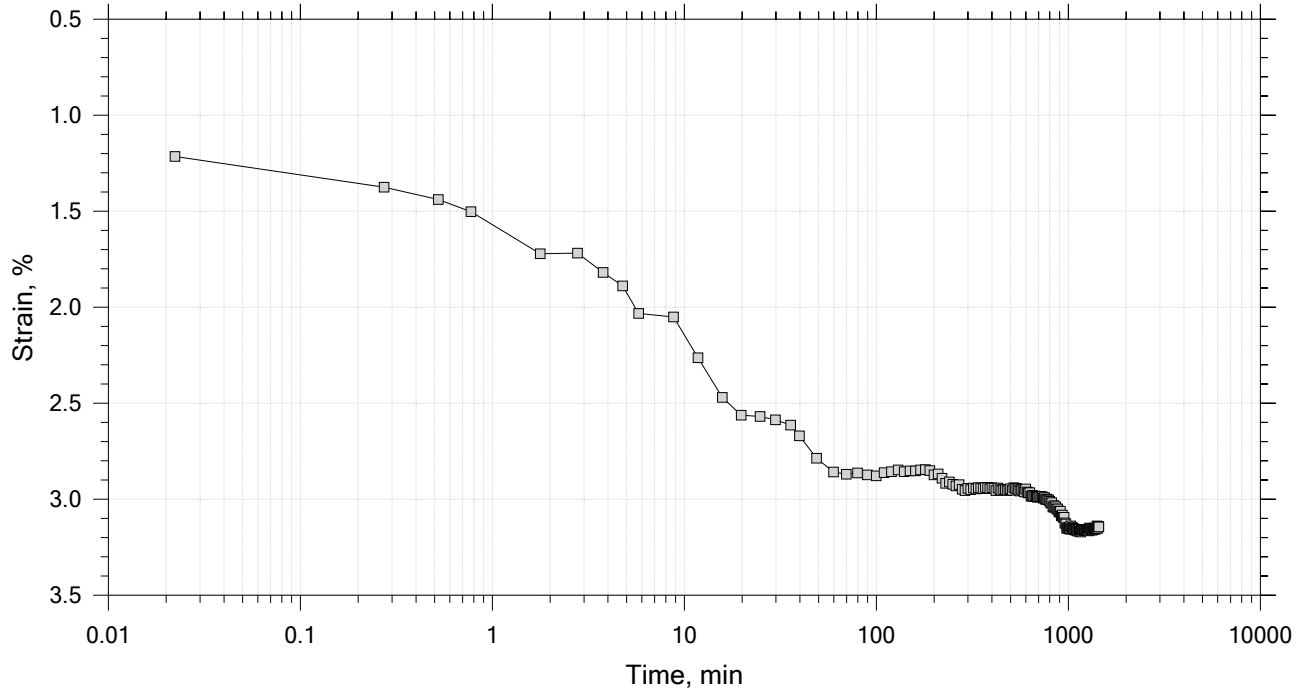
Time Curve 2 of 12  
 Constant Load Step  
 Stress: 250 psf




 Engineering and Testing	Project: Breton Lakebridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-1	Tested By: jm	Checked By: mcm
	Sample No.: 9	Test Date: 10/7/20	Depth: 16-18 ft
	Test No.: IP-3	Sample Type: intact	Elevation: ---
	Description: Moist, greenish gray clay(CH)		

# One-Dimensional Consolidation by ASTM D2435 - Method B

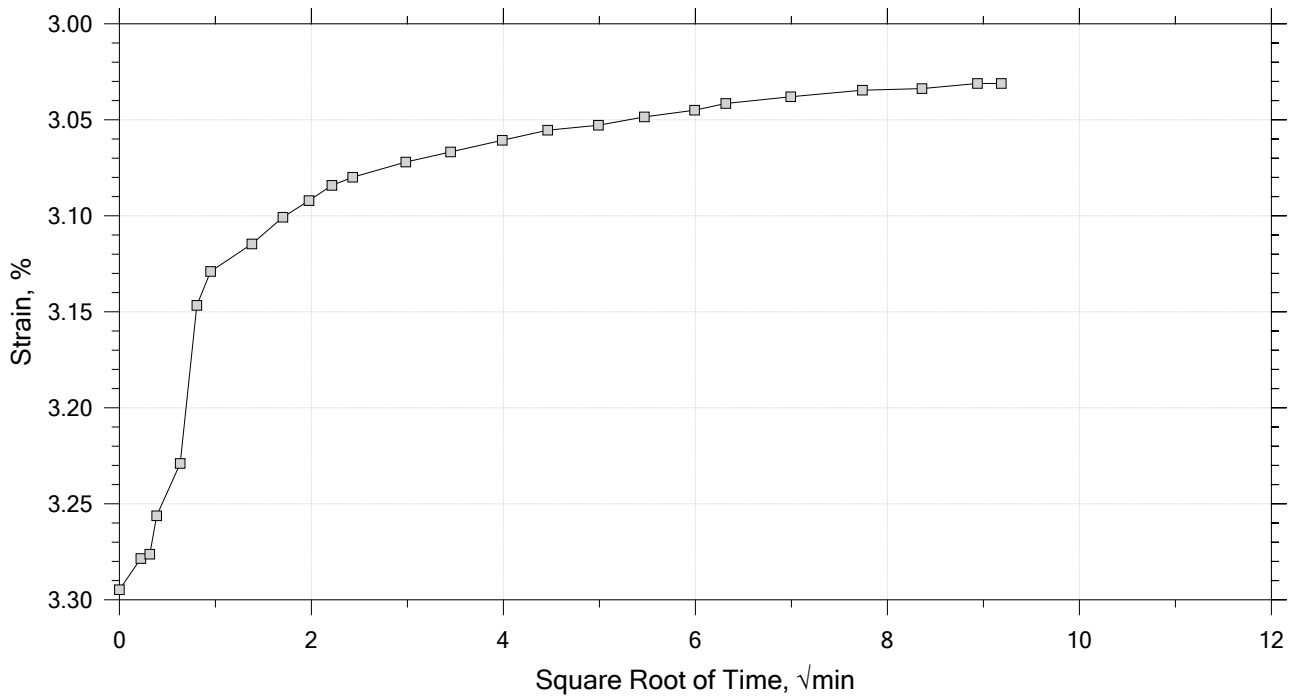
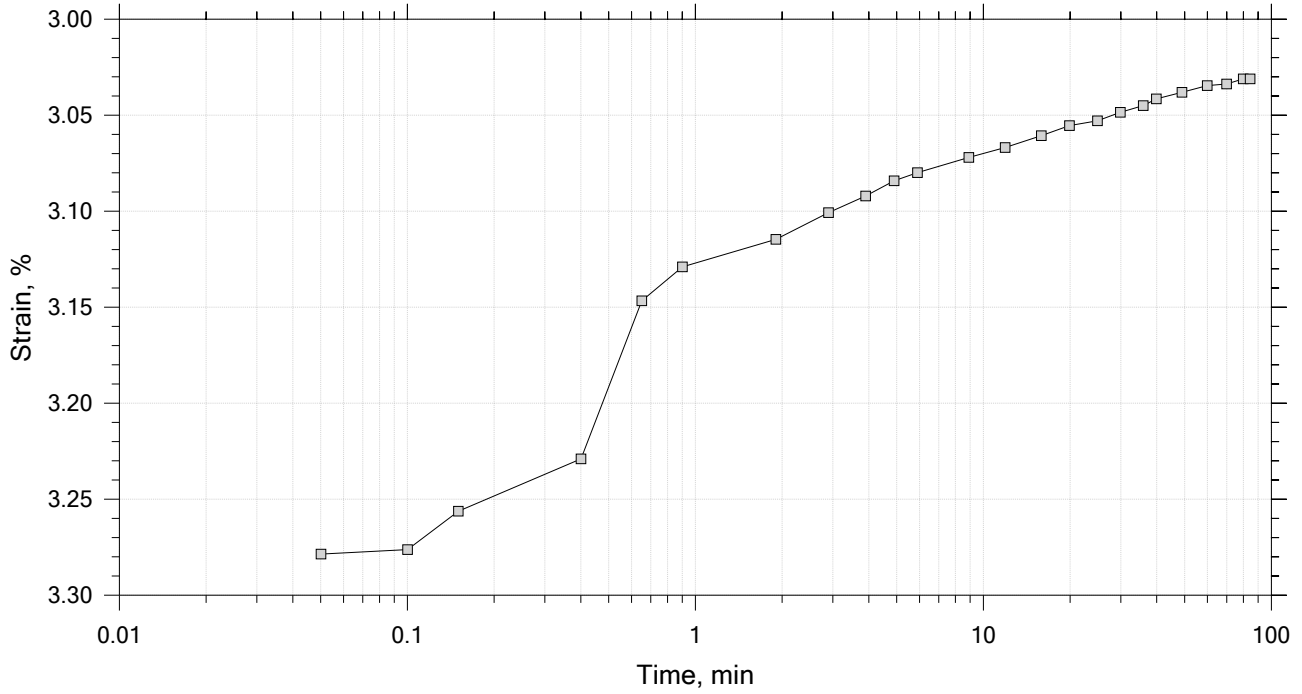
Time Curve 3 of 12  
 Constant Load Step  
 Stress: 500 psf




 Engineering and Testing	Project: Breton Lakebridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-1	Tested By: jm	Checked By: mcm
	Sample No.: 9	Test Date: 10/7/20	Depth: 16-18 ft
	Test No.: IP-3	Sample Type: intact	Elevation: ---
	Description: Moist, greenish gray clay(CH)		

# One-Dimensional Consolidation by ASTM D2435 - Method B

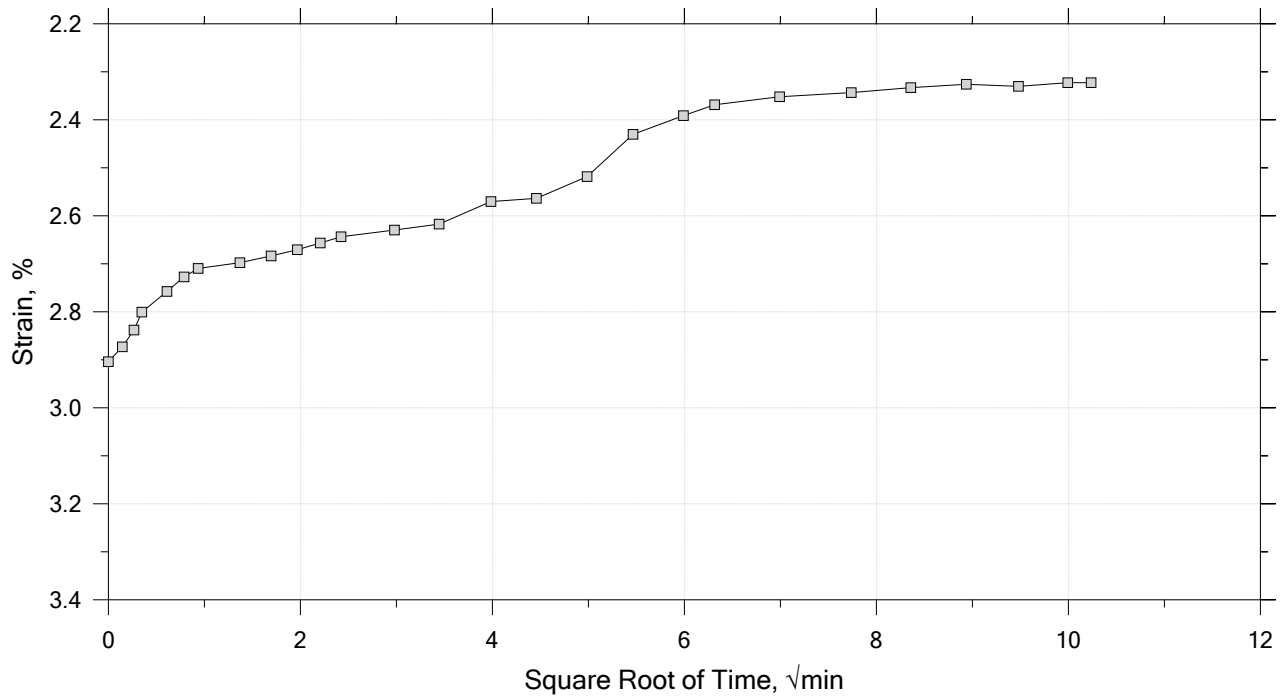
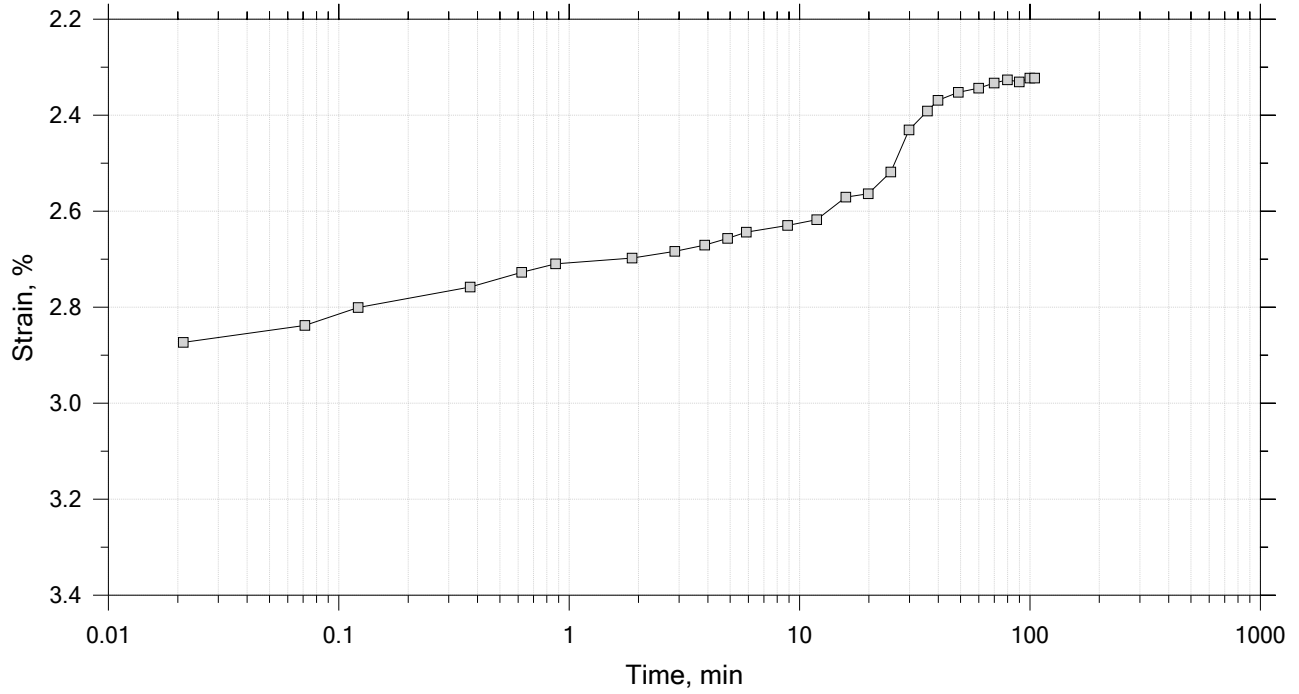
Time Curve 4 of 12  
 Constant Load Step  
 Stress: 250 psf




 Engineering and Testing	Project: Breton Lakebridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-1	Tested By: jm	Checked By: mcm
	Sample No.: 9	Test Date: 10/7/20	Depth: 16-18 ft
	Test No.: IP-3	Sample Type: intact	Elevation: ---
	Description: Moist, greenish gray clay(CH)		

# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 5 of 12  
 Constant Load Step  
 Stress: 100 psf



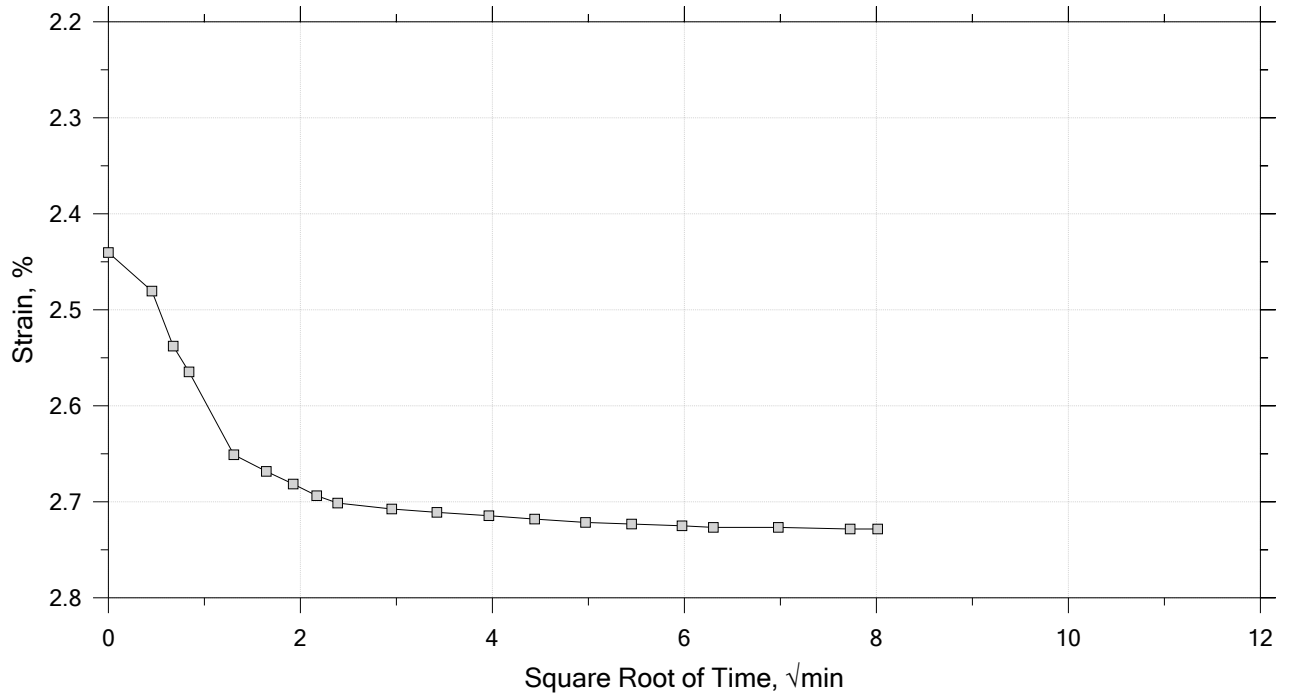
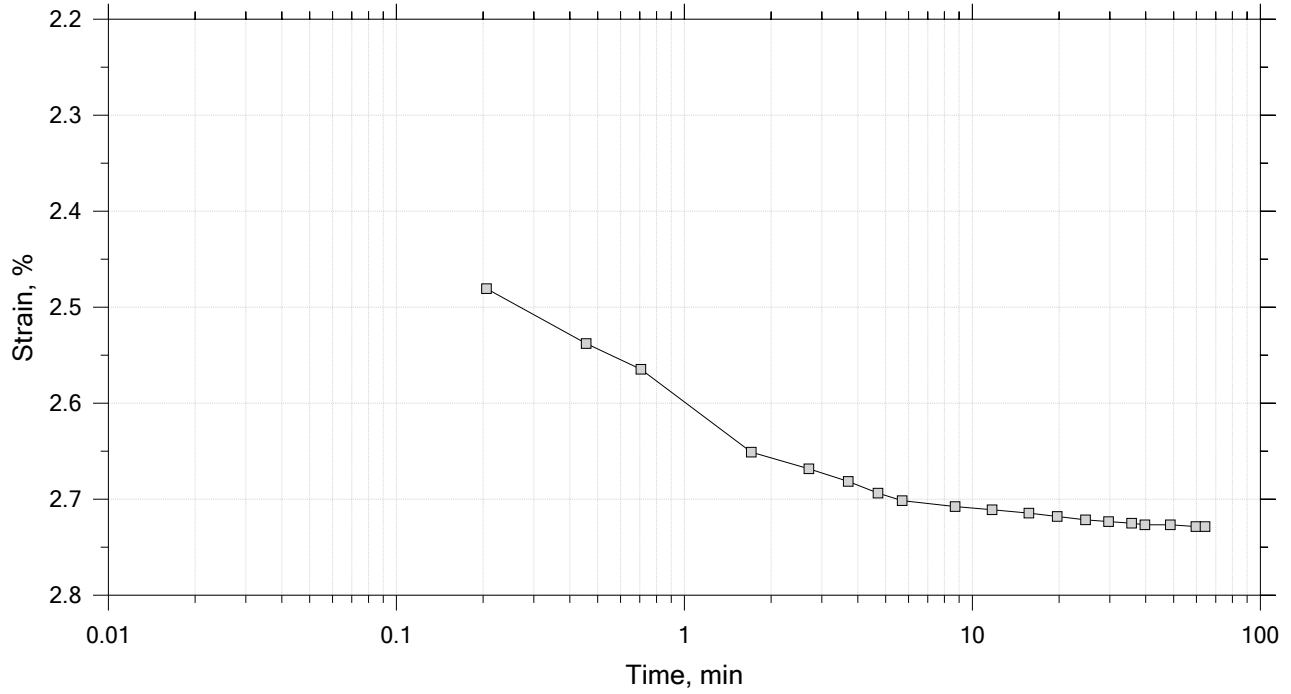
 Engineering and Testing	Project: Breton Lakebridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-1	Tested By: jm	Checked By: mcm
	Sample No.: 9	Test Date: 10/7/20	Depth: 16-18 ft
	Test No.: IP-3	Sample Type: intact	Elevation: ---
	Description: Moist, greenish gray clay(CH)		


# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 6 of 12

Constant Load Step

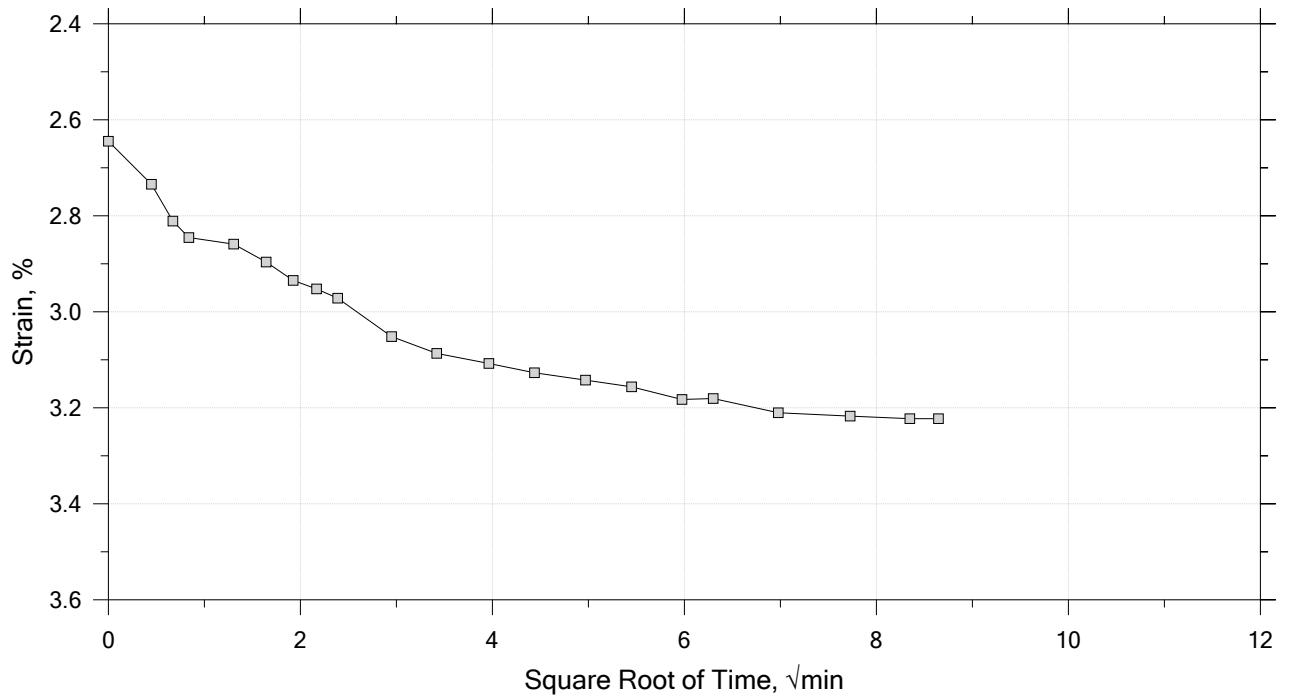
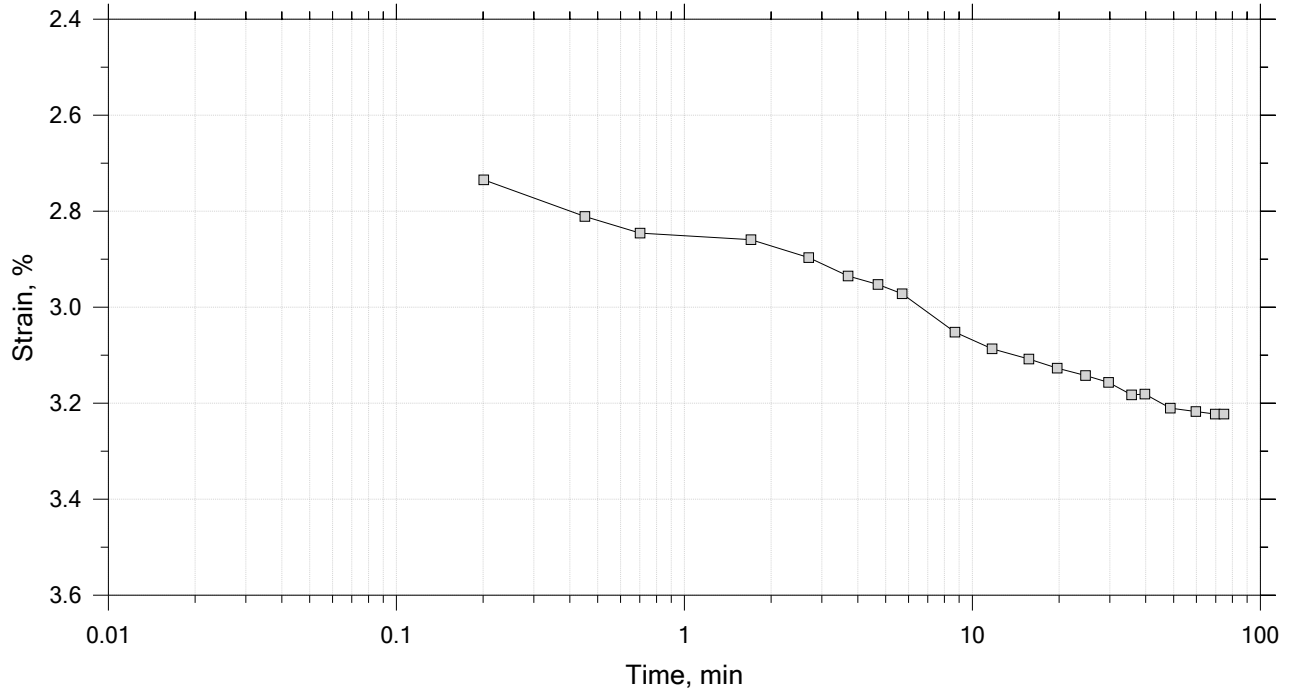
Stress: 250 psf




 Engineering and Testing	Project: Breton Lakebridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-1	Tested By: jm	Checked By: mcm
	Sample No.: 9	Test Date: 10/7/20	Depth: 16-18 ft
	Test No.: IP-3	Sample Type: intact	Elevation: ---
	Description: Moist, greenish gray clay(CH)		

# One-Dimensional Consolidation by ASTM D2435 - Method B

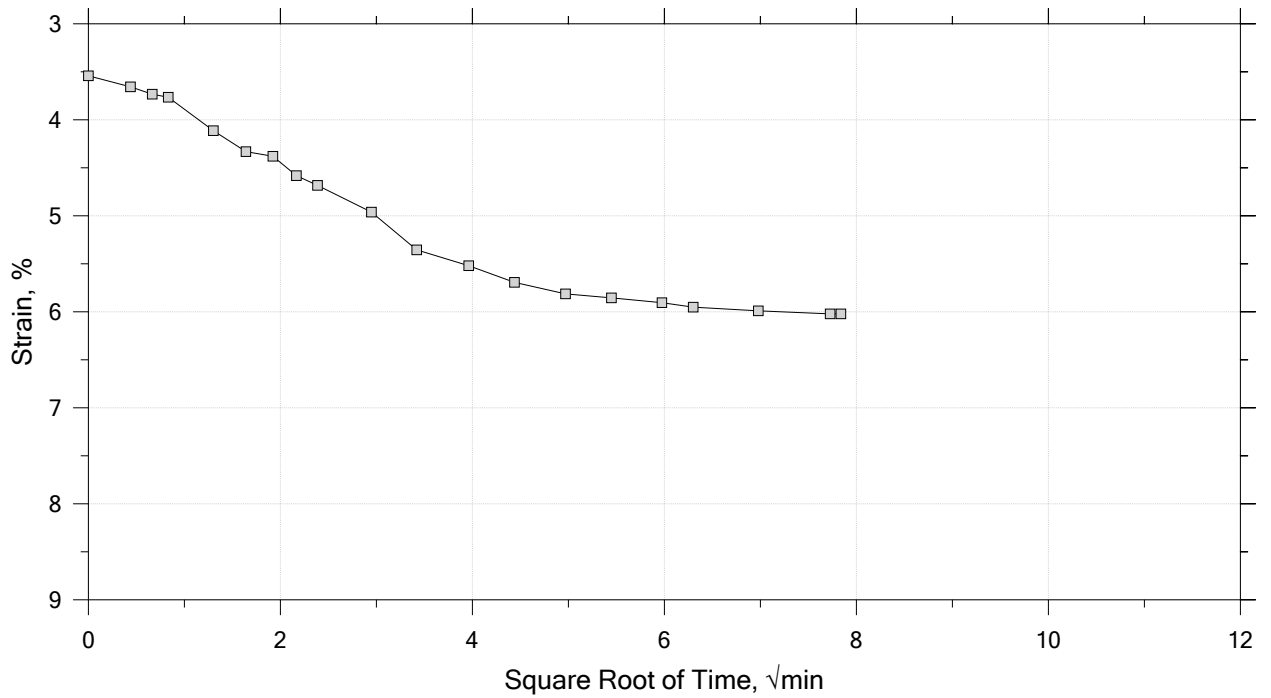
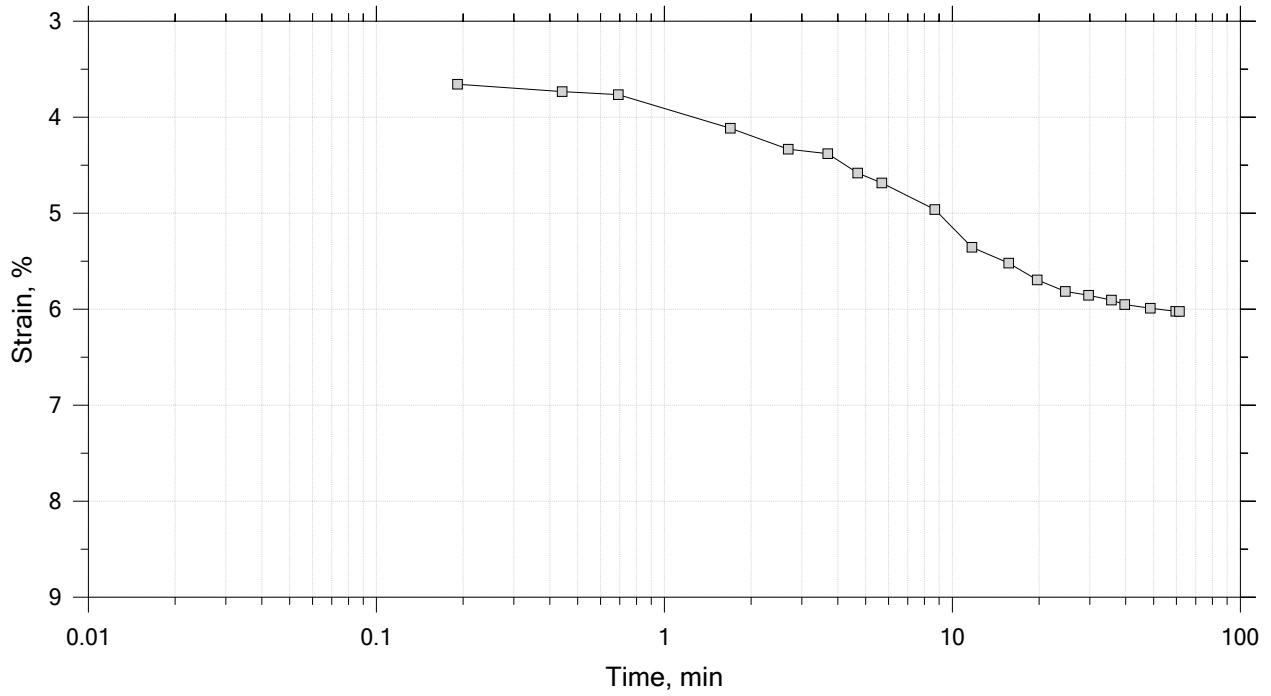
Time Curve 7 of 12  
 Constant Load Step  
 Stress: 500 psf




 Engineering and Testing	Project: Breton Lakebridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-1	Tested By: jm	Checked By: mcm
	Sample No.: 9	Test Date: 10/7/20	Depth: 16-18 ft
	Test No.: IP-3	Sample Type: intact	Elevation: ---
	Description: Moist, greenish gray clay(CH)		

# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 8 of 12  
 Constant Load Step  
 Stress: 1e+03 psf

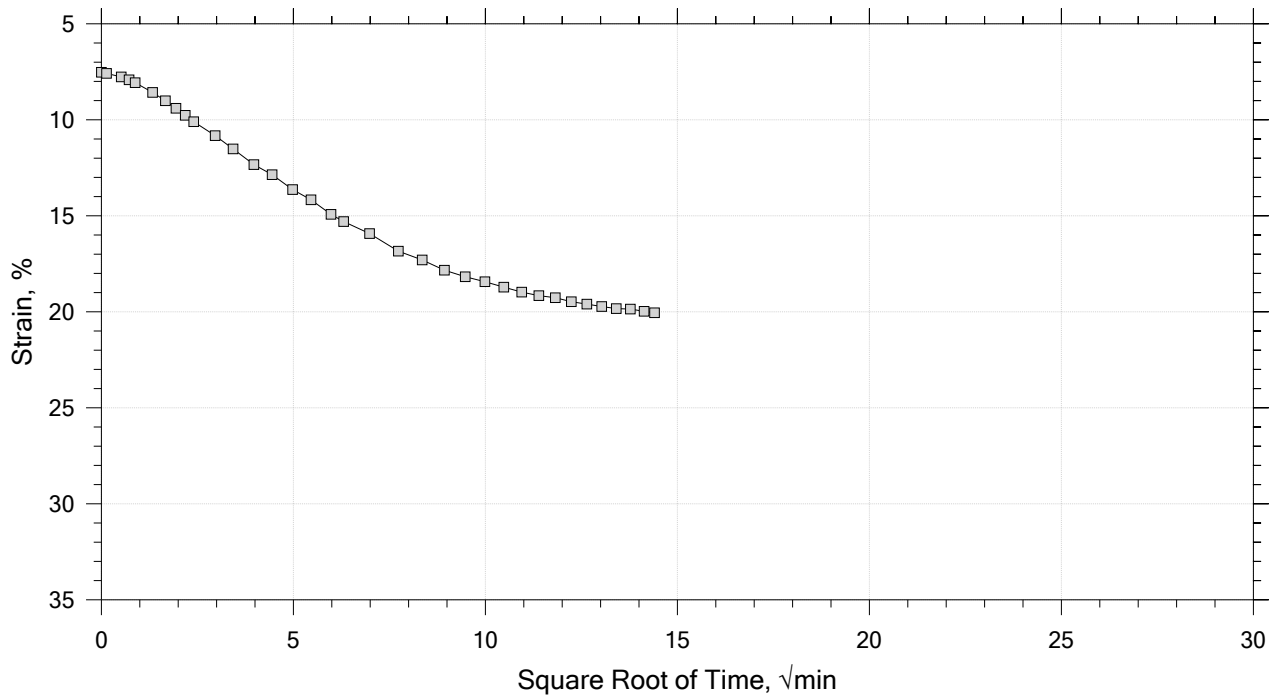
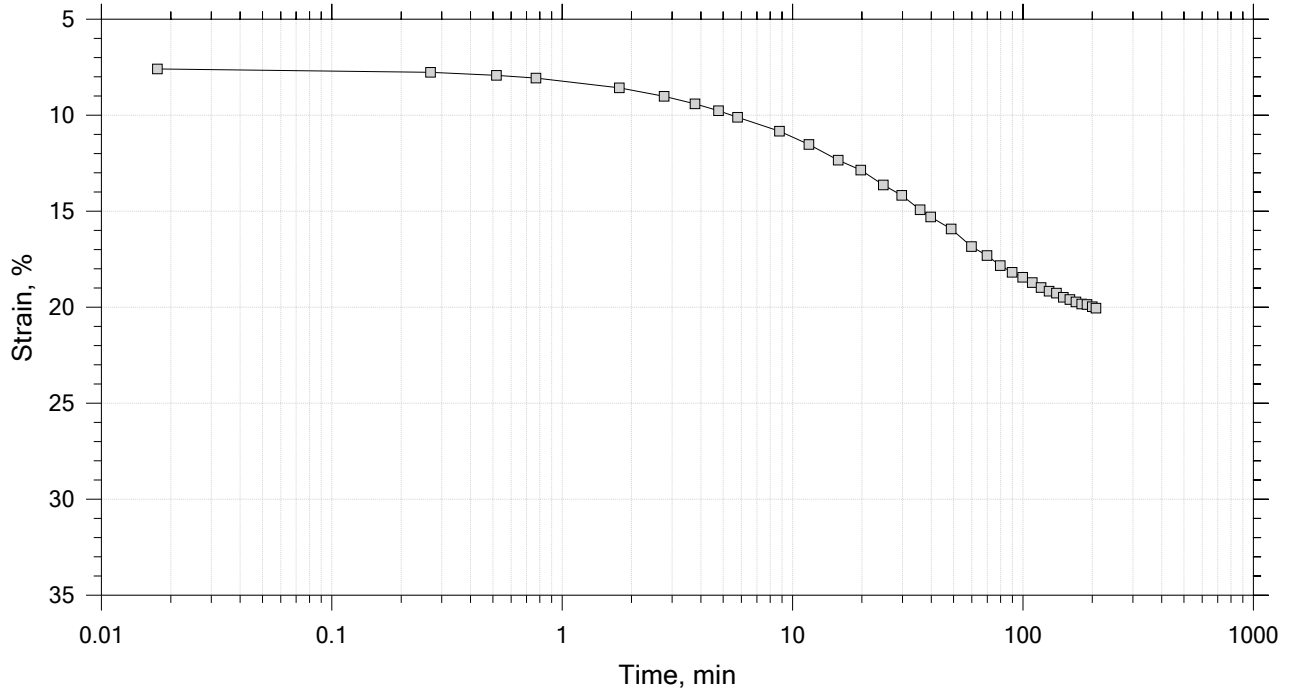



 Engineering and Testing	Project: Breton Lakebridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-1	Tested By: jm	Checked By: mcm
	Sample No.:9	Test Date: 10/7/20	Depth: 16-18 ft
	Test No.: IP-3	Sample Type: intact	Elevation: ---
	Description: Moist, greenish gray clay (CH)		



# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 9 of 12  
 Constant Load Step  
 Stress: 2e+03 psf



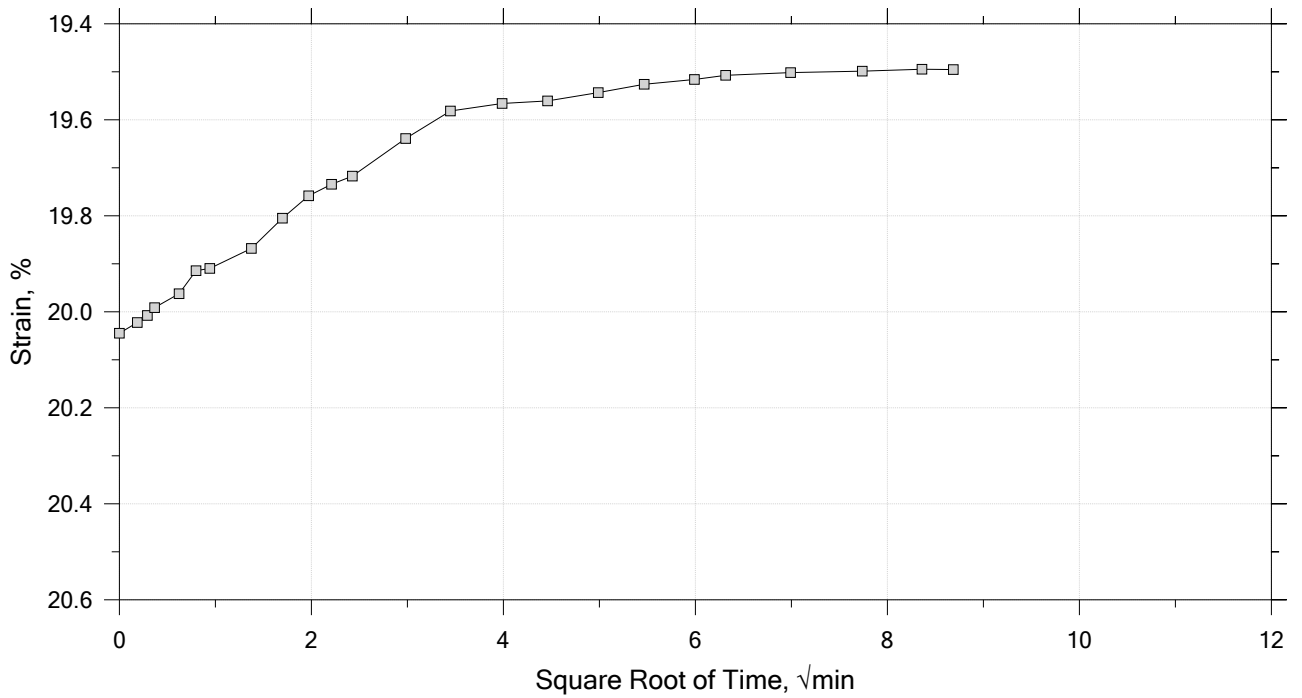
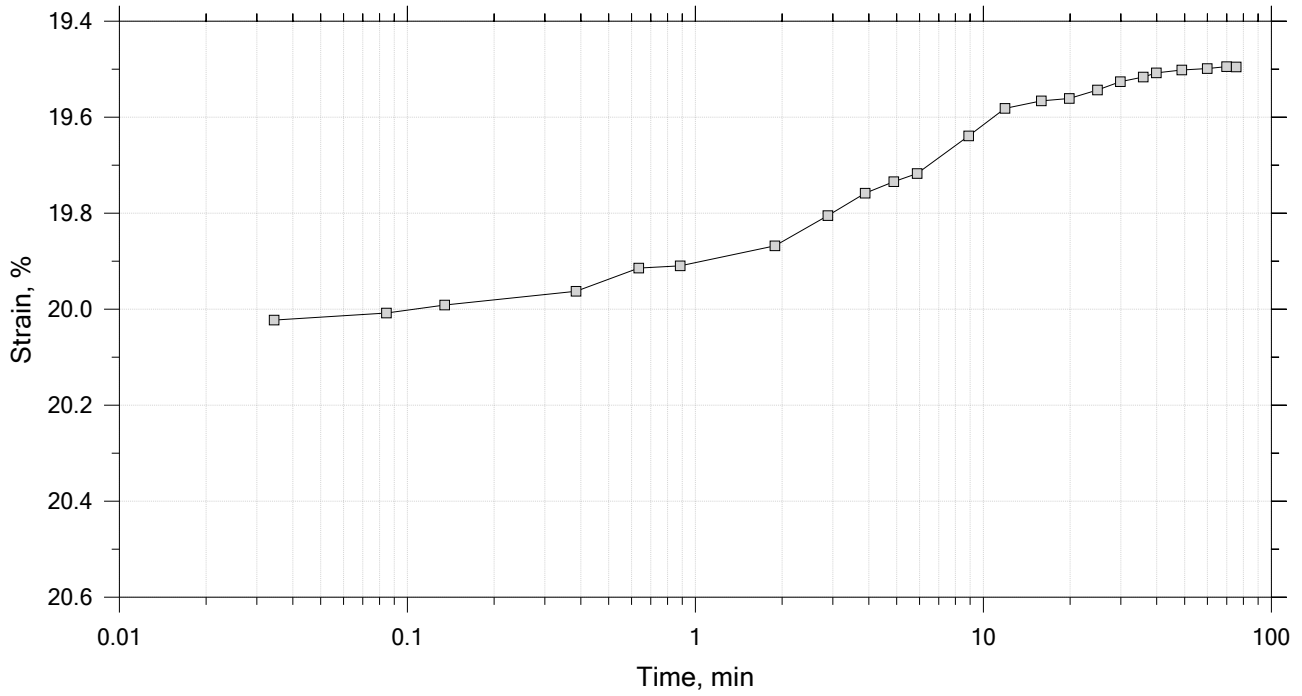
 Engineering and Testing	Project: Breton Lakebridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-1	Tested By: jm	Checked By: mcm
	Sample No.: 9	Test Date: 10/7/20	Depth: 16-18 ft
	Test No.: IP-3	Sample Type: intact	Elevation: ---
	Description: Moist, greenish gray clay(CH)		


# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 10 of 12

Constant Load Step

Stress: 1e+03 psf



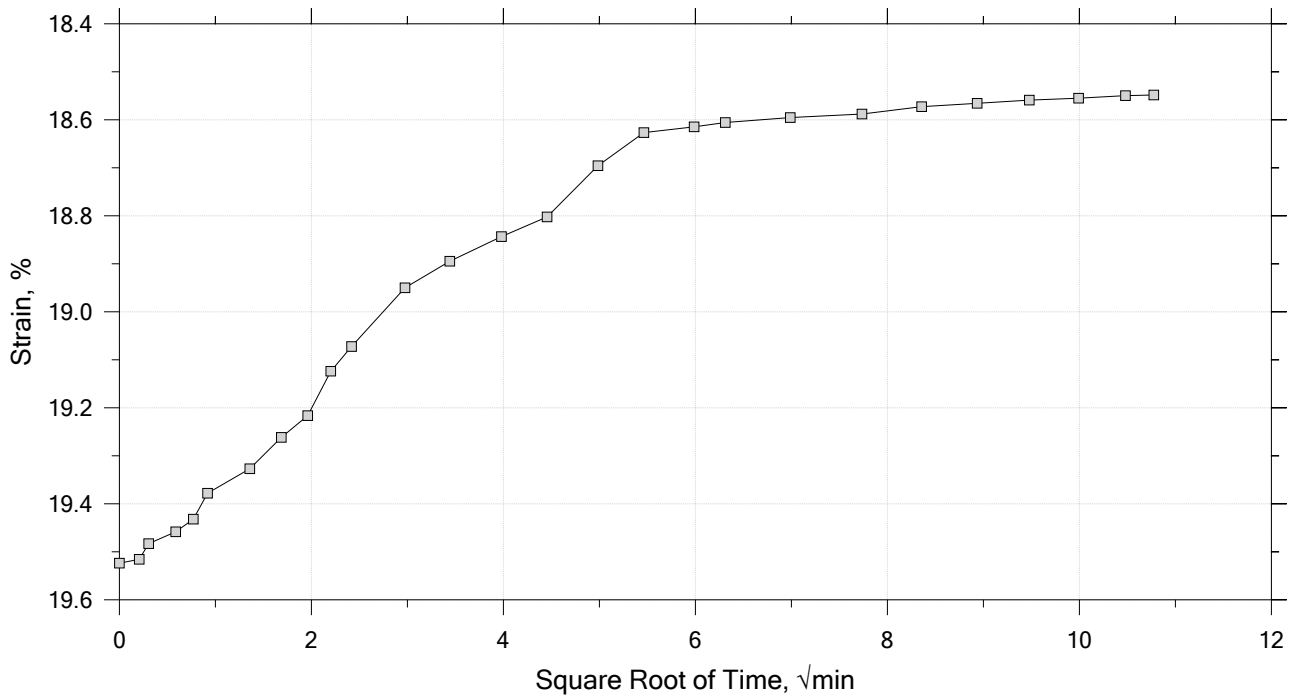
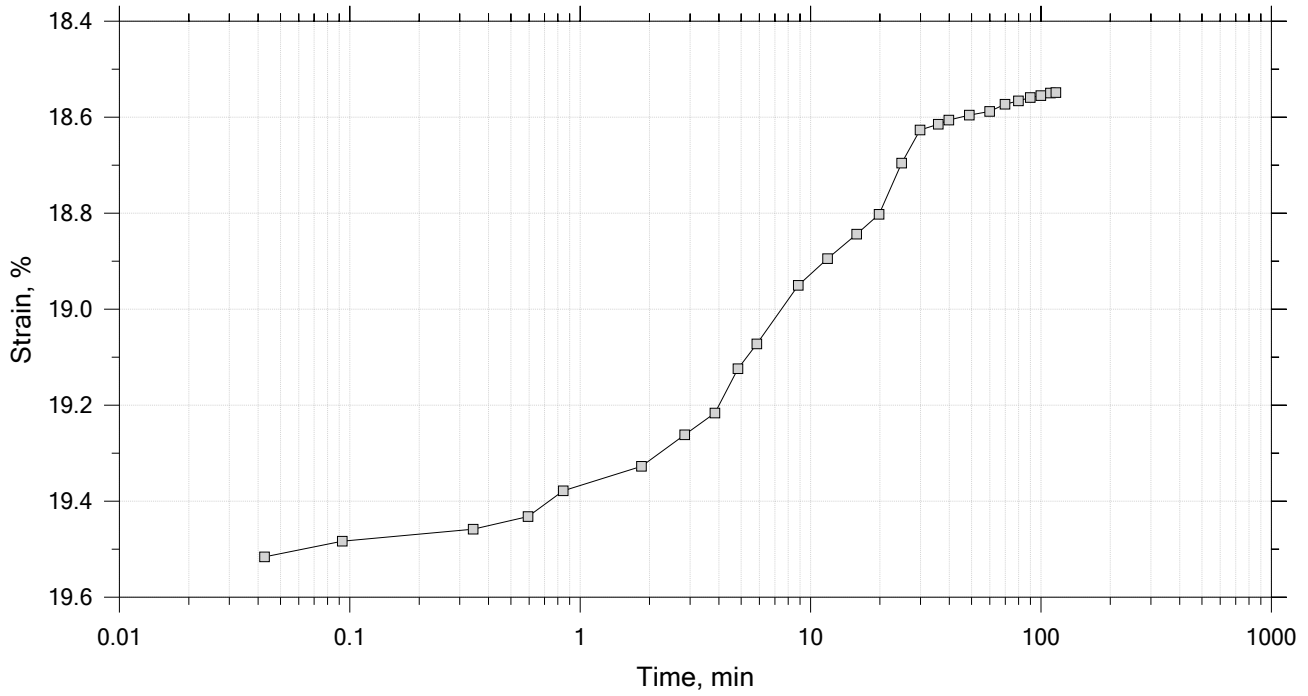
 <p>Engineering and Testing</p>	Project: Breton Lakebridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-1	Tested By: jm	Checked By: mcm
	Sample No.: 9	Test Date: 10/7/20	Depth: 16-18 ft
	Test No.: IP-3	Sample Type: intact	Elevation: ---
	Description: Moist, greenish gray clay(CH)		


# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 11 of 12

Constant Load Step

Stress: 500 psf



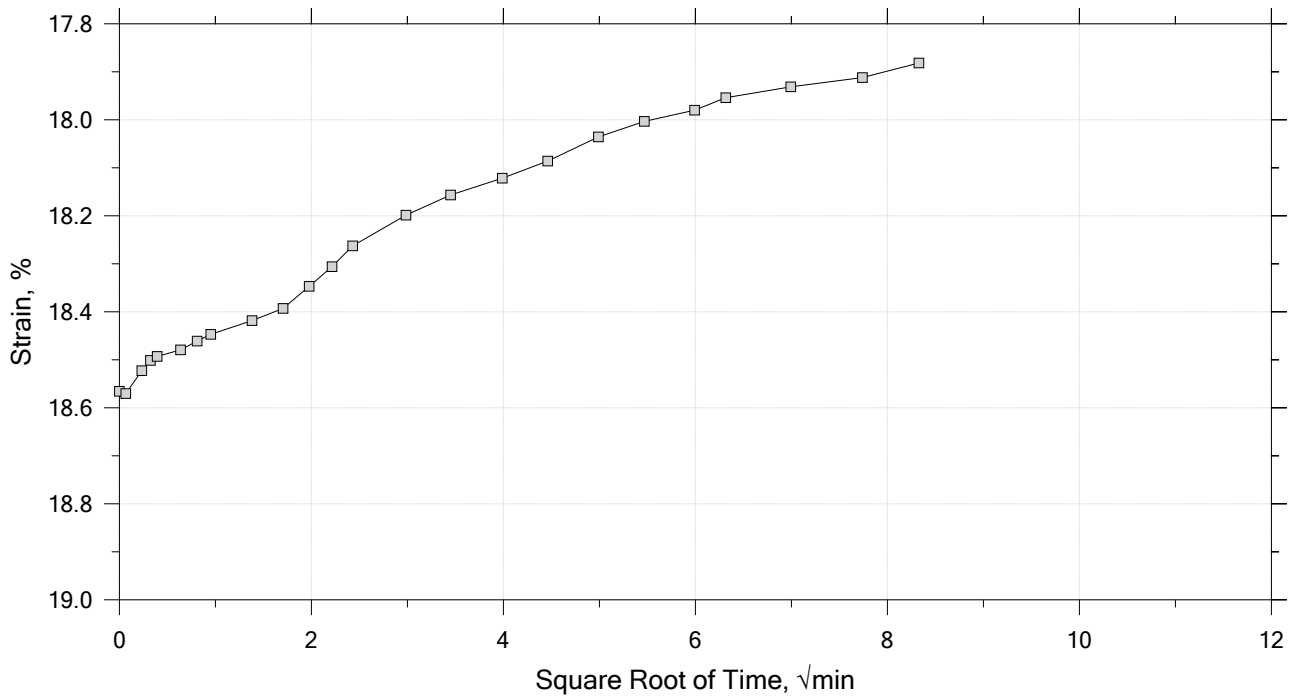
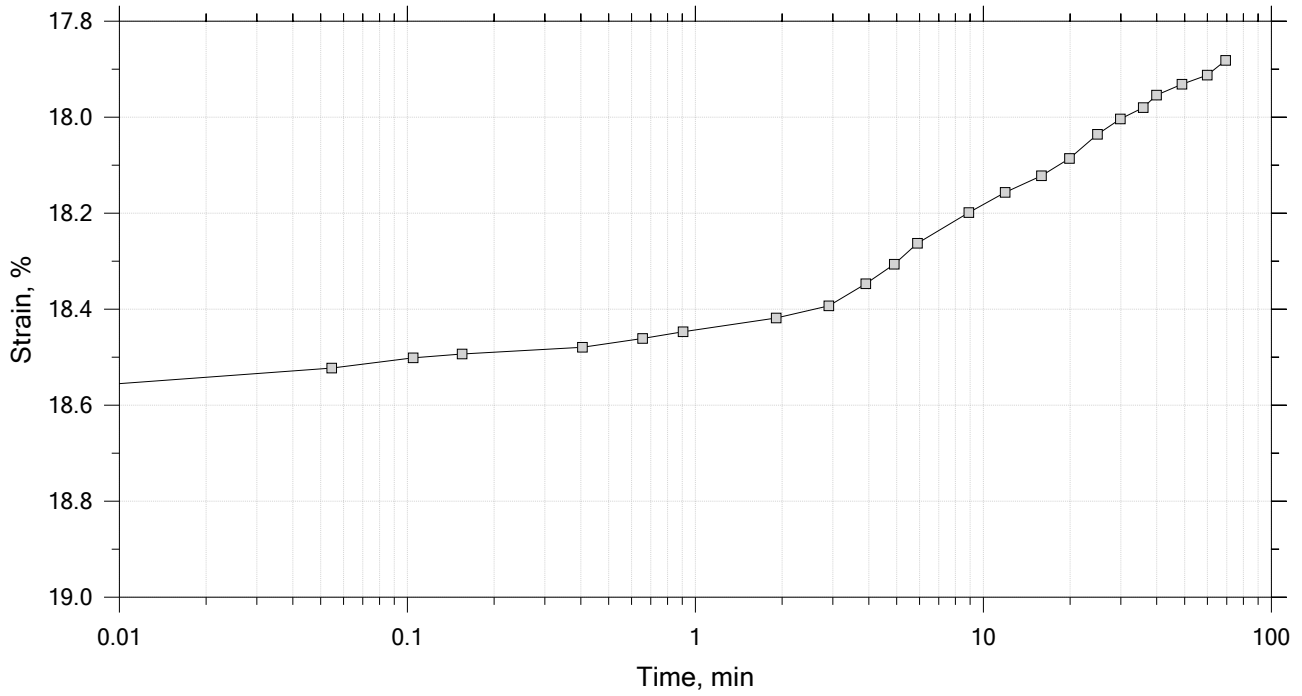
 Engineering and Testing	Project: Breton Lakebridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-1	Tested By: jm	Checked By: mcm
	Sample No.: 9	Test Date: 10/7/20	Depth: 16-18 ft
	Test No.: IP-3	Sample Type: intact	Elevation: ---
	Description: Moist, greenish gray clay (CH)		


# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 12 of 12

Constant Load Step

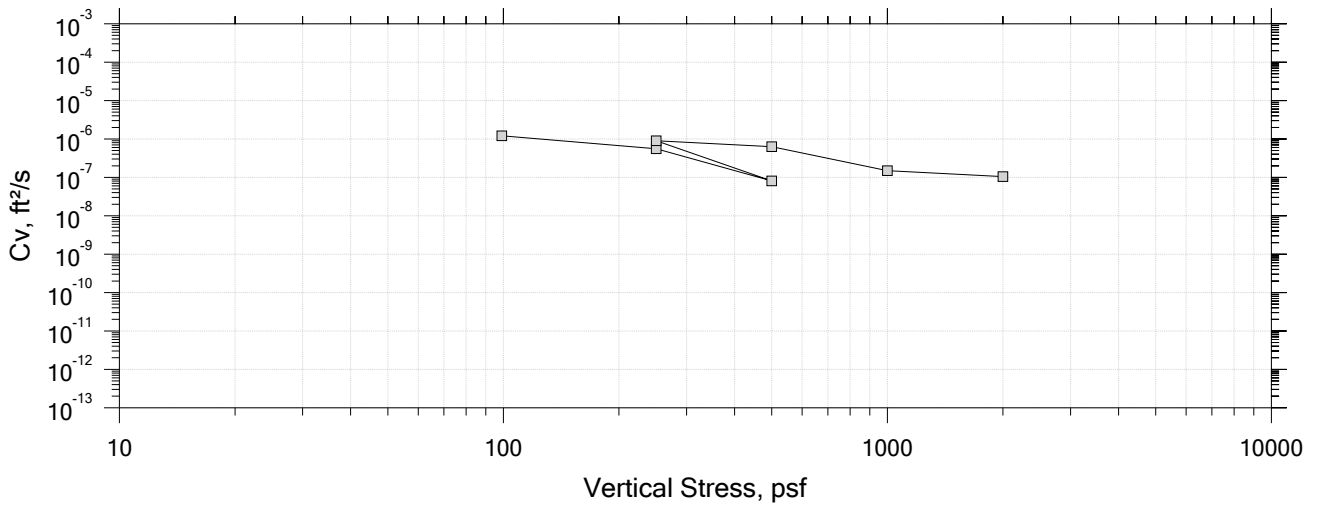
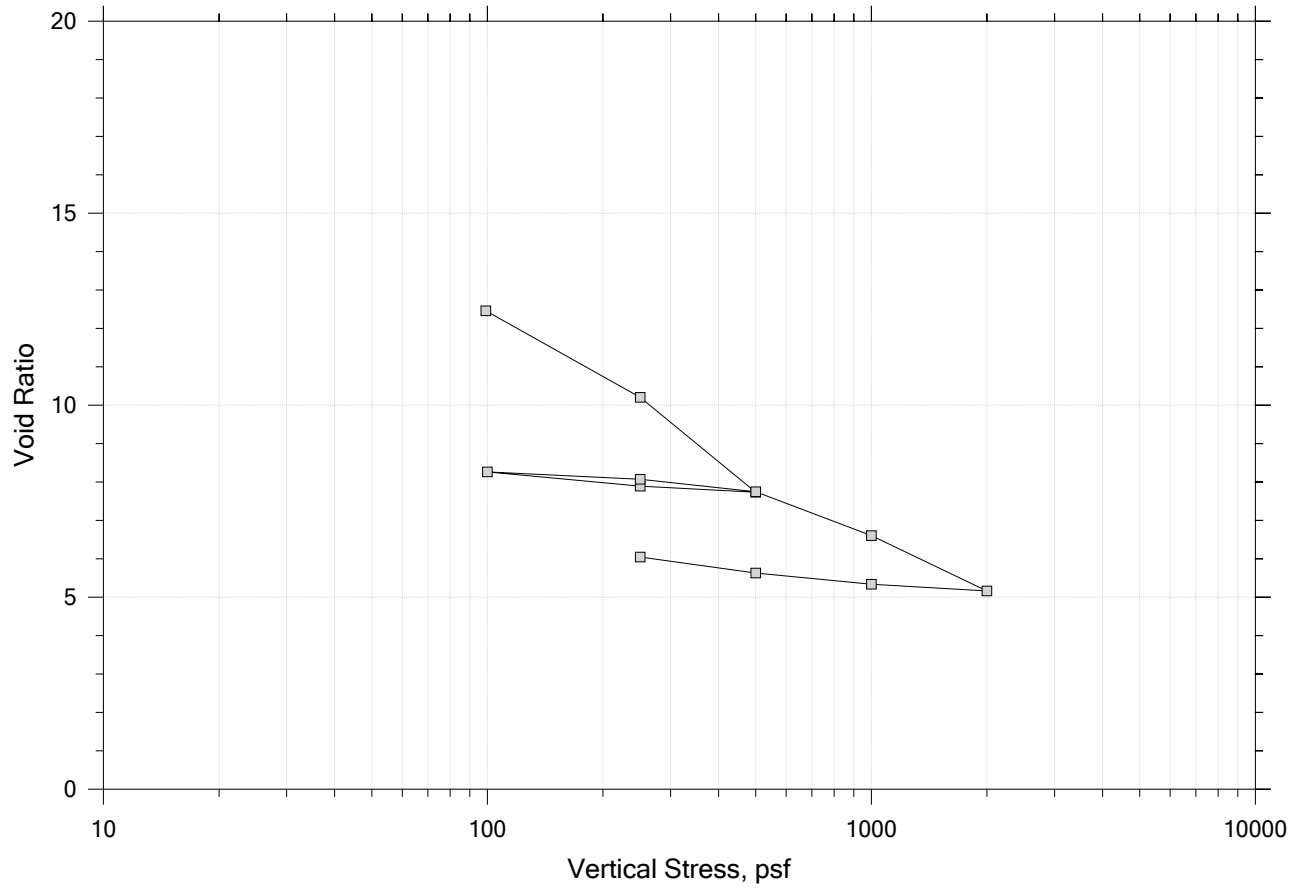
Stress: 250 psf




 Engineering and Testing	Project: Breton Lakebridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-1	Tested By: jm	Checked By: mcm
	Sample No.: 9	Test Date: 10/7/20	Depth: 16-18 ft
	Test No.: IP-3	Sample Type: intact	Elevation: ---
	Description: Moist, greenish gray clay(CH)		

# One-Dimensional Consolidation by ASTM D2435 - Method B

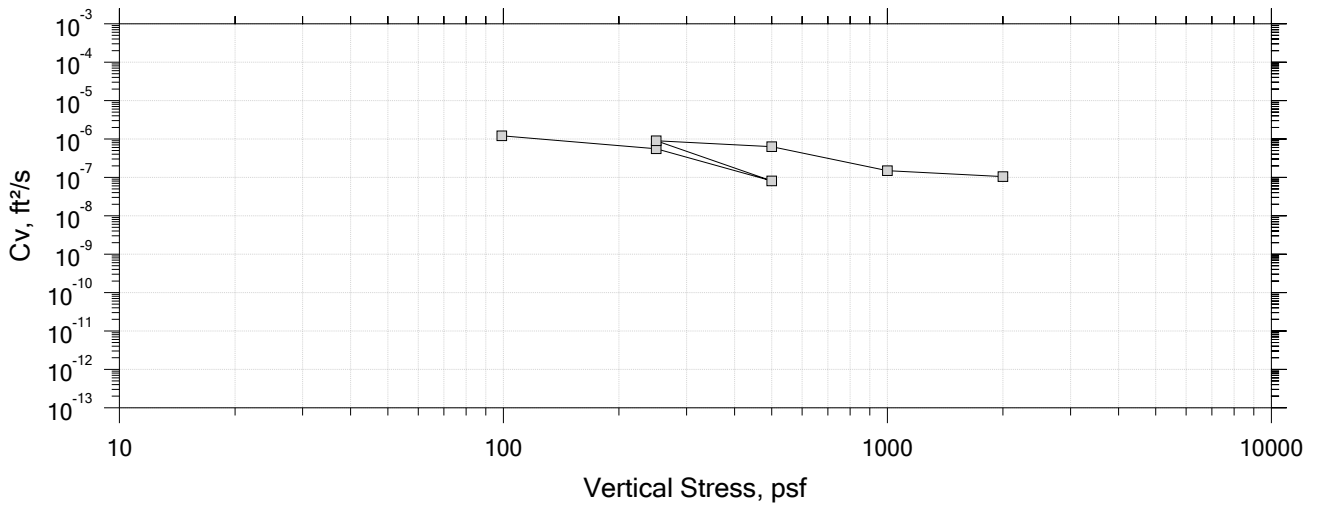
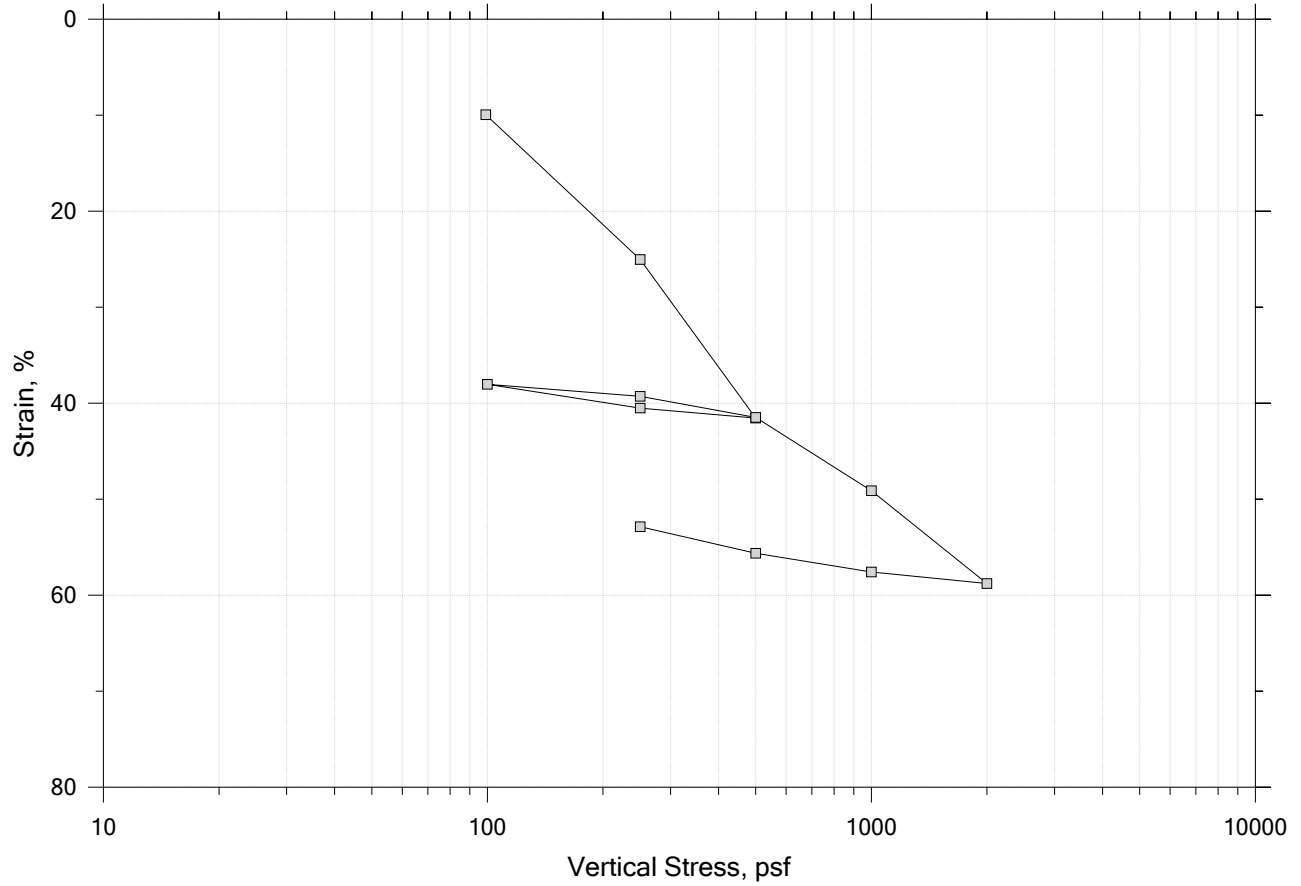
## Summary Report




	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-3	Tested By: jm	Checked By: mcm
	Sample No.: 1	Test Date: 10/10/20	Depth: 0-2 ft
	Test No.: IP-4	Sample Type: intact	Elevation: ---
	Description: Moist, very dark brown peat(PT)	Measured specific gravity: 1.84	

# One-Dimensional Consolidation by ASTM D2435 - Method B

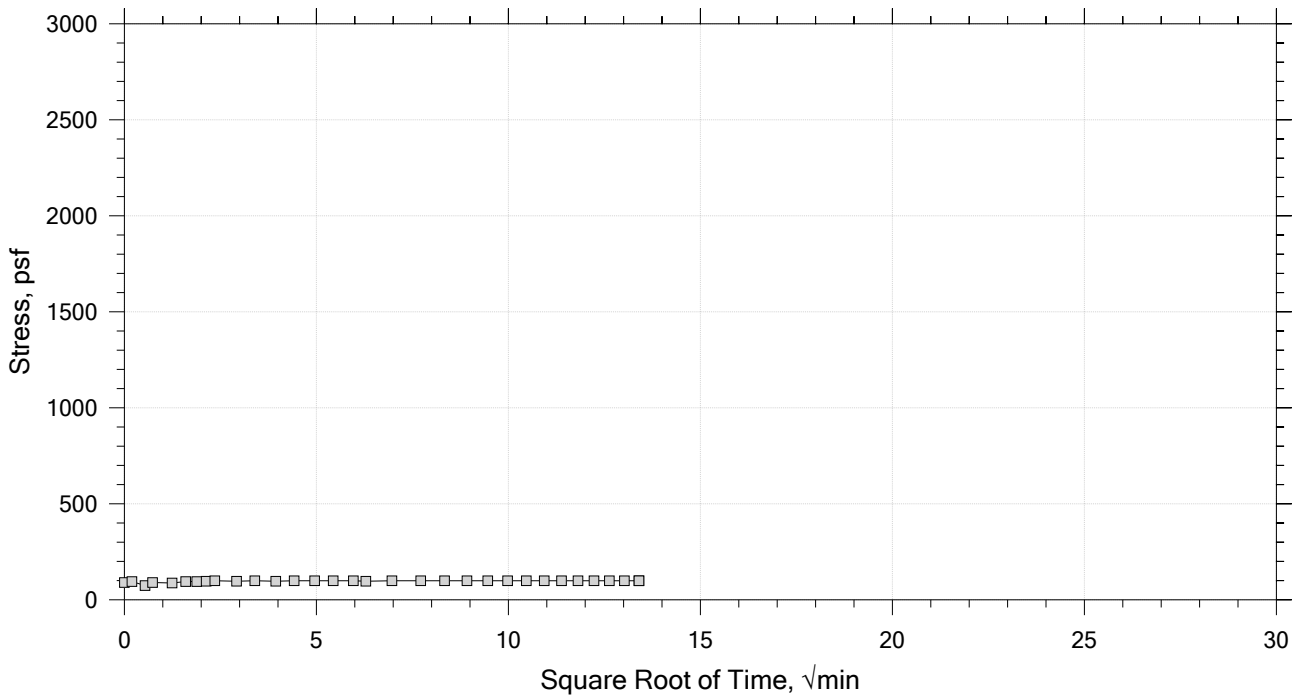
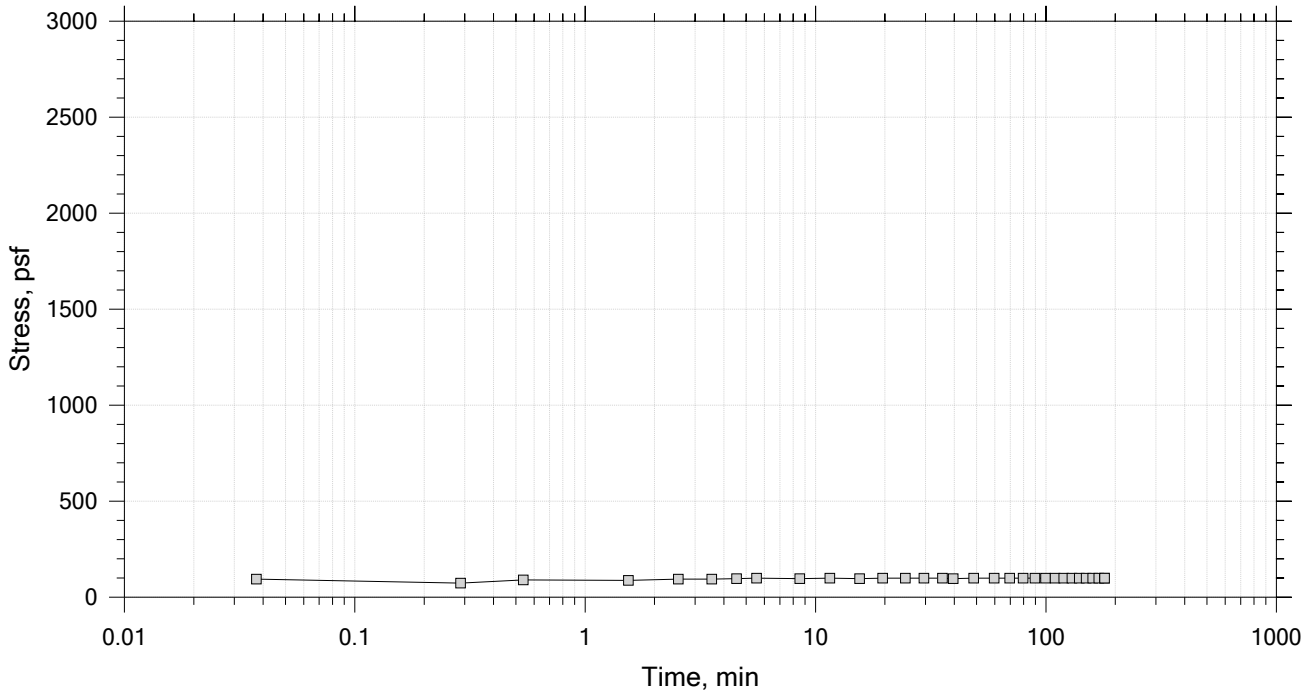
## Summary Report




 <p>APS Engineering and Testing</p>	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-3	Tested By: jm	Checked By: mcm
	Sample No.: 1	Test Date: 10/10/20	Depth: 0-2 ft
	Test No.: IP-4	Sample Type: intact	Elevation: ---
	Description: Moist, very dark brown peat (PT)		

# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 1 of 12  
 Constant Volume Step  
 Stress: 99 psf



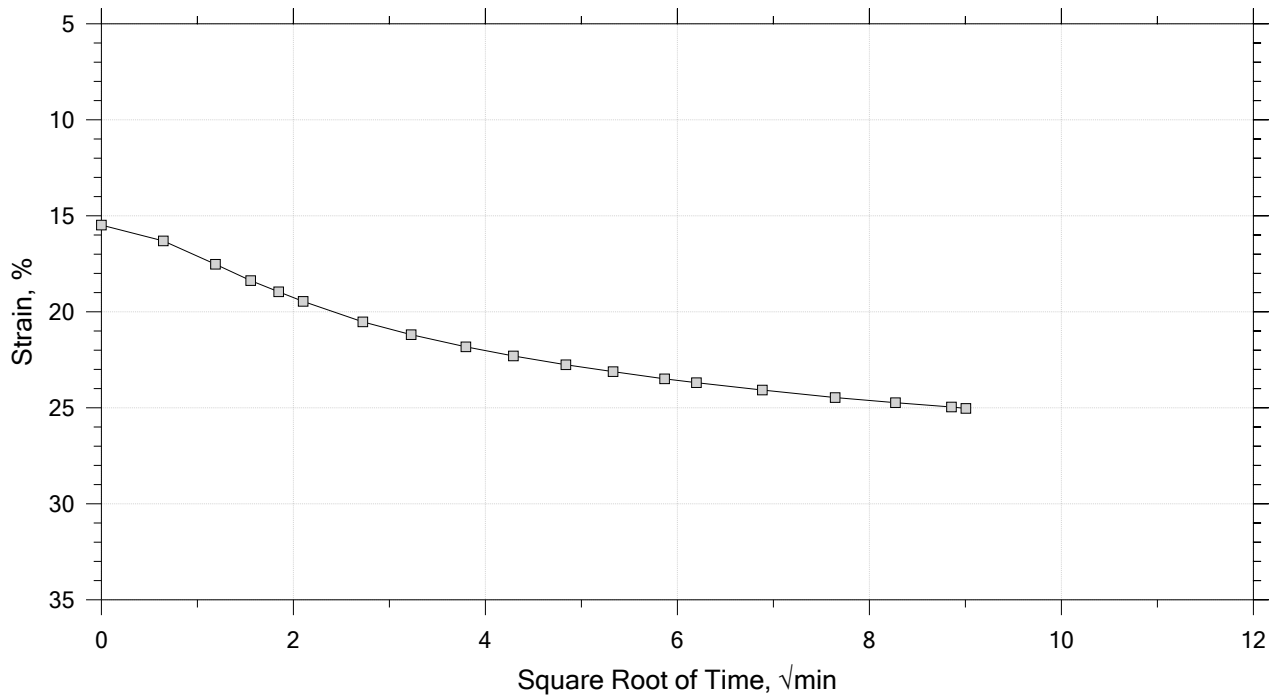
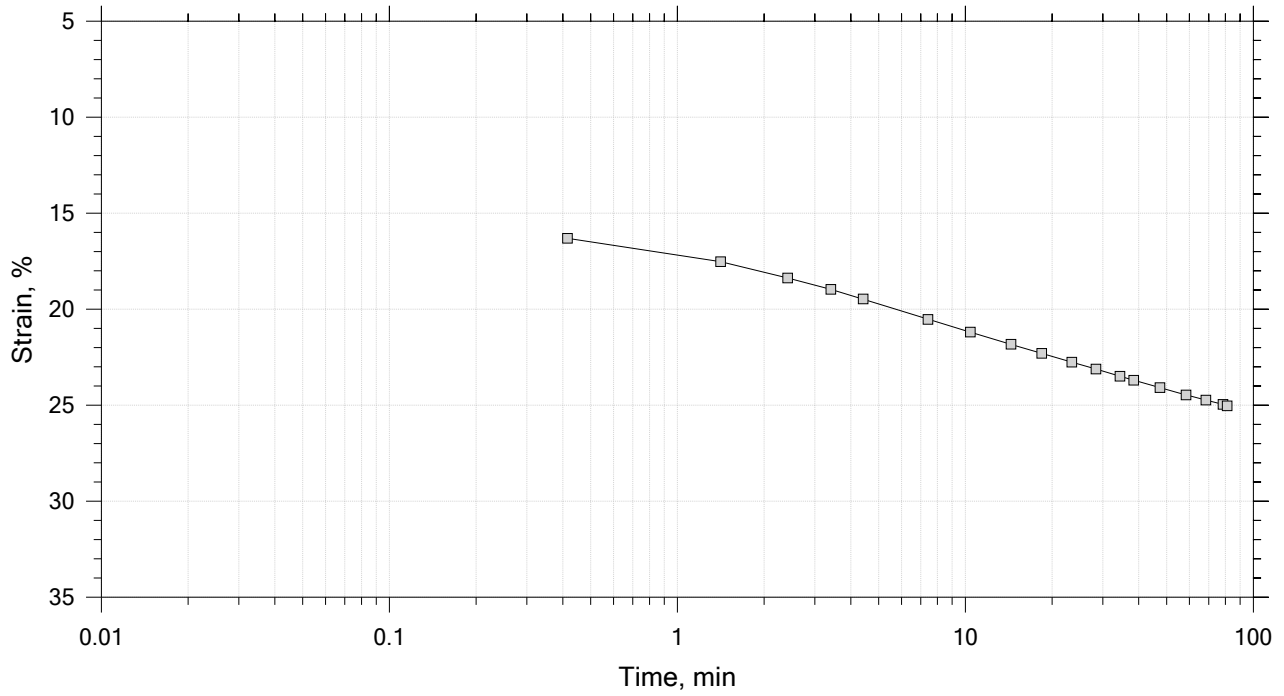
 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-3	Tested By: jm	Checked By: mcm
	Sample No.: 1	Test Date: 10/10/20	Depth: 0-2 ft
	Test No.: IP-4	Sample Type: intact	Elevation: ---


# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 2 of 12

Constant Load Step

Stress: 250 psf

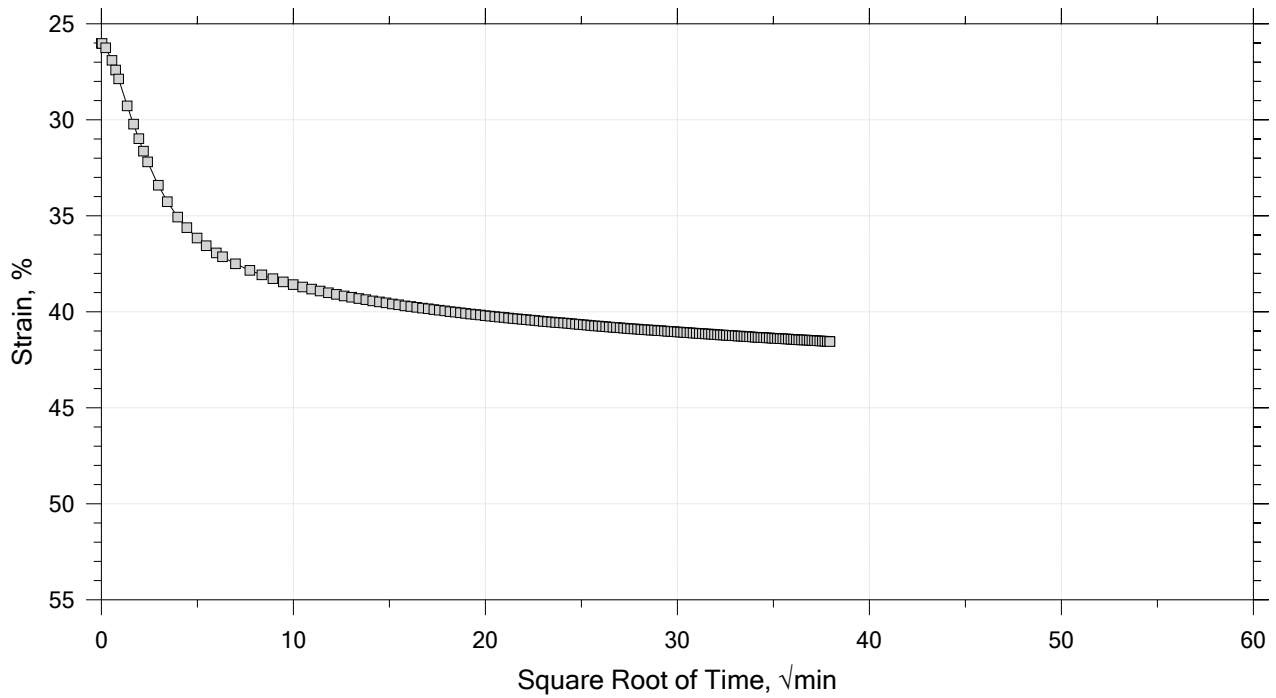
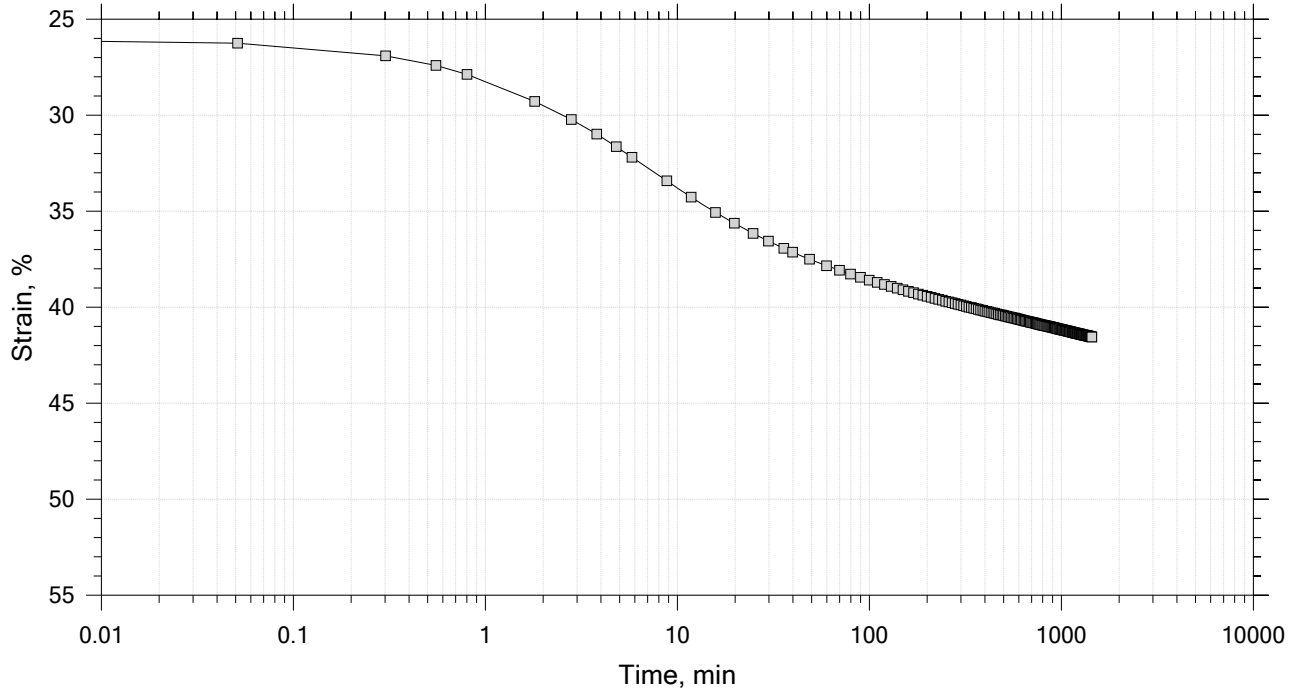



 <p>Engineering and Testing</p>	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-3	Tested By: jm	Checked By: mcm
	Sample No.: 1	Test Date: 10/10/20	Depth: 0-2 ft
	Test No.: IP-4	Sample Type: intact	Elevation: ---



# One-Dimensional Consolidation by ASTM D2435 - Method B

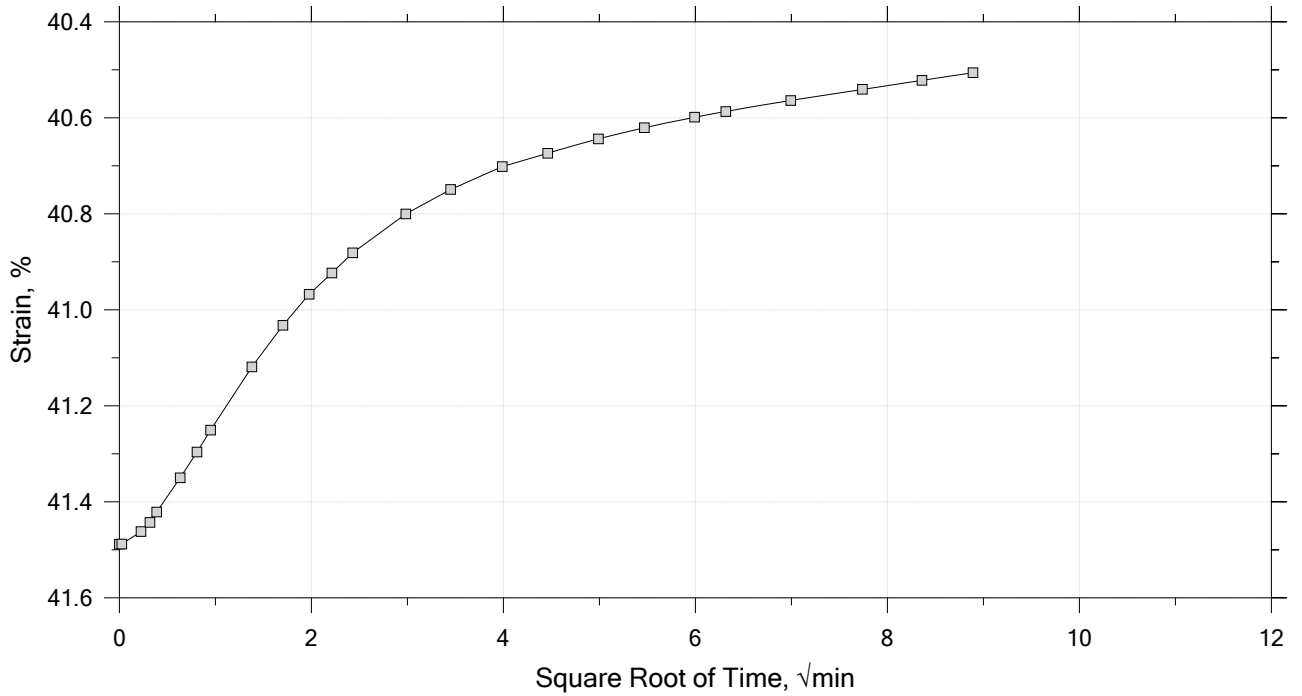
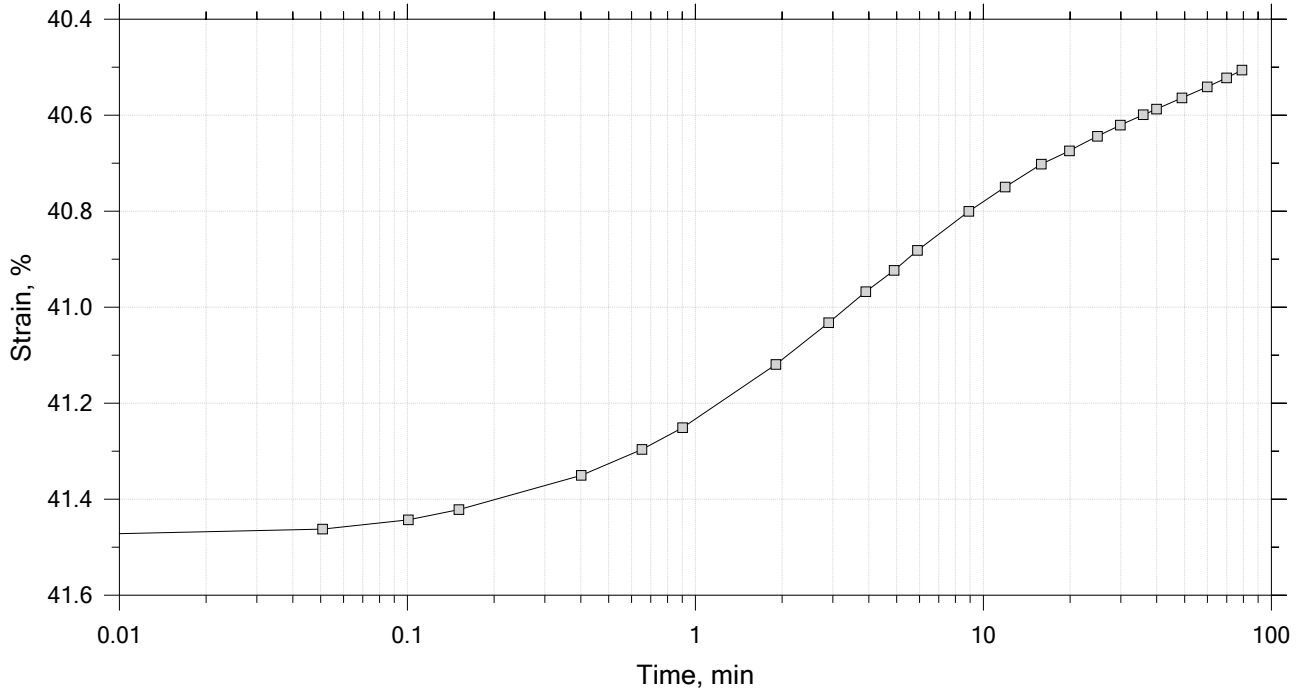
Time Curve 3 of 12  
 Constant Load Step  
 Stress: 500 psf




 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-3	Tested By: jm	Checked By: mcm
	Sample No.:1	Test Date: 10/10/20	Depth: 0-2 ft
	Test No.: IP-4	Sample Type: intact	Elevation: ---
	Description: Moist, very dark brown peat(PT)		

# One-Dimensional Consolidation by ASTM D2435 - Method B

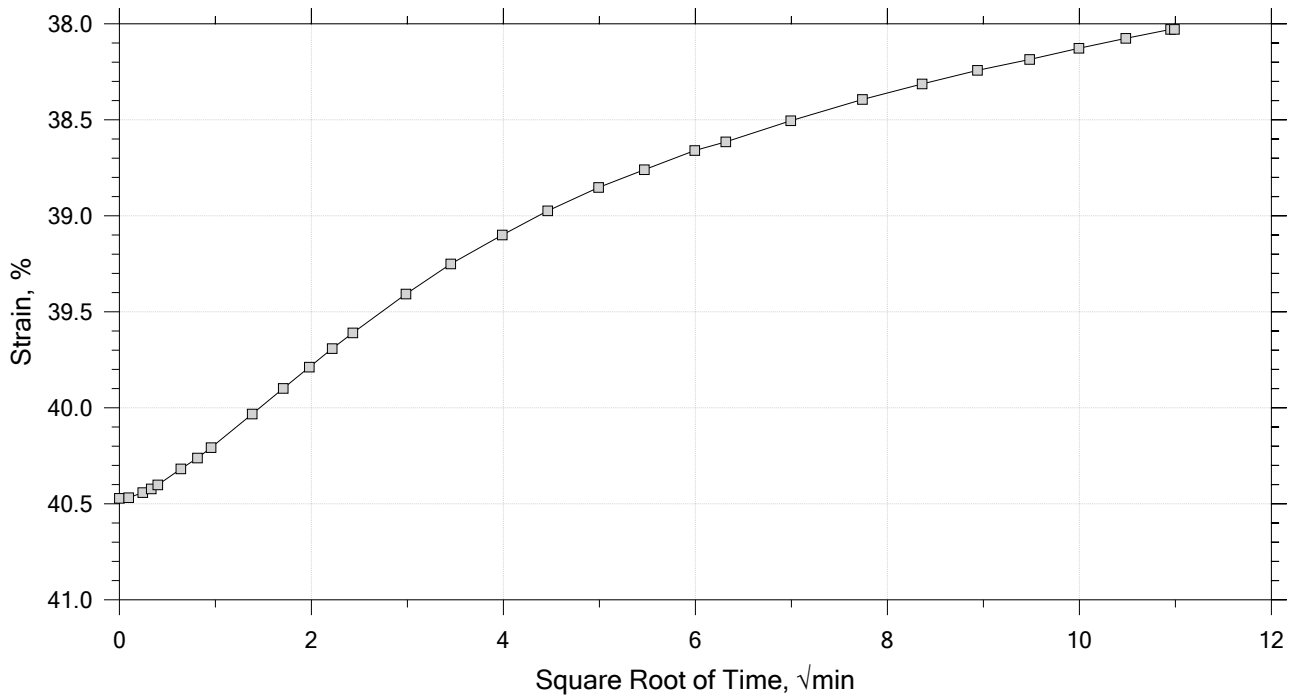
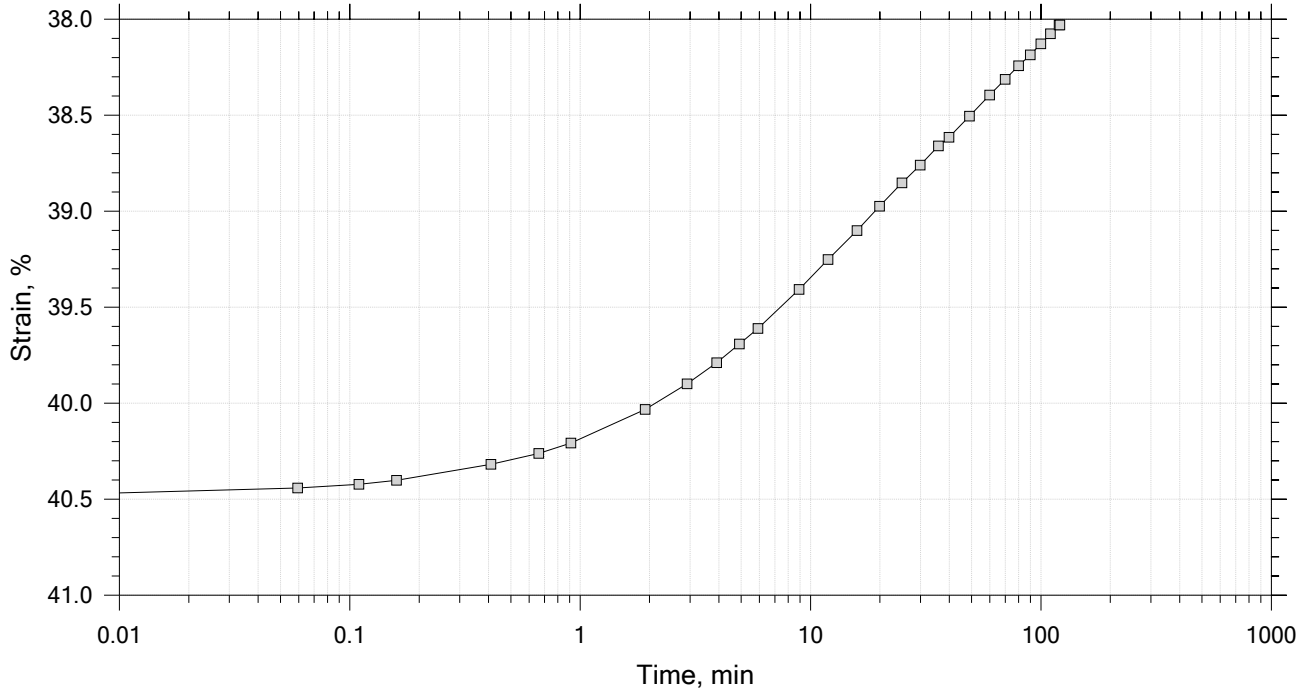
Time Curve 4 of 12  
 Constant Load Step  
 Stress: 250 psf




 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-3	Tested By: jm	Checked By: mcm
	Sample No.:1	Test Date: 10/10/20	Depth: 0-2 ft
	Test No.: IP-4	Sample Type: intact	Elevation: ---

# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 5 of 12  
 Constant Load Step  
 Stress: 100 psf



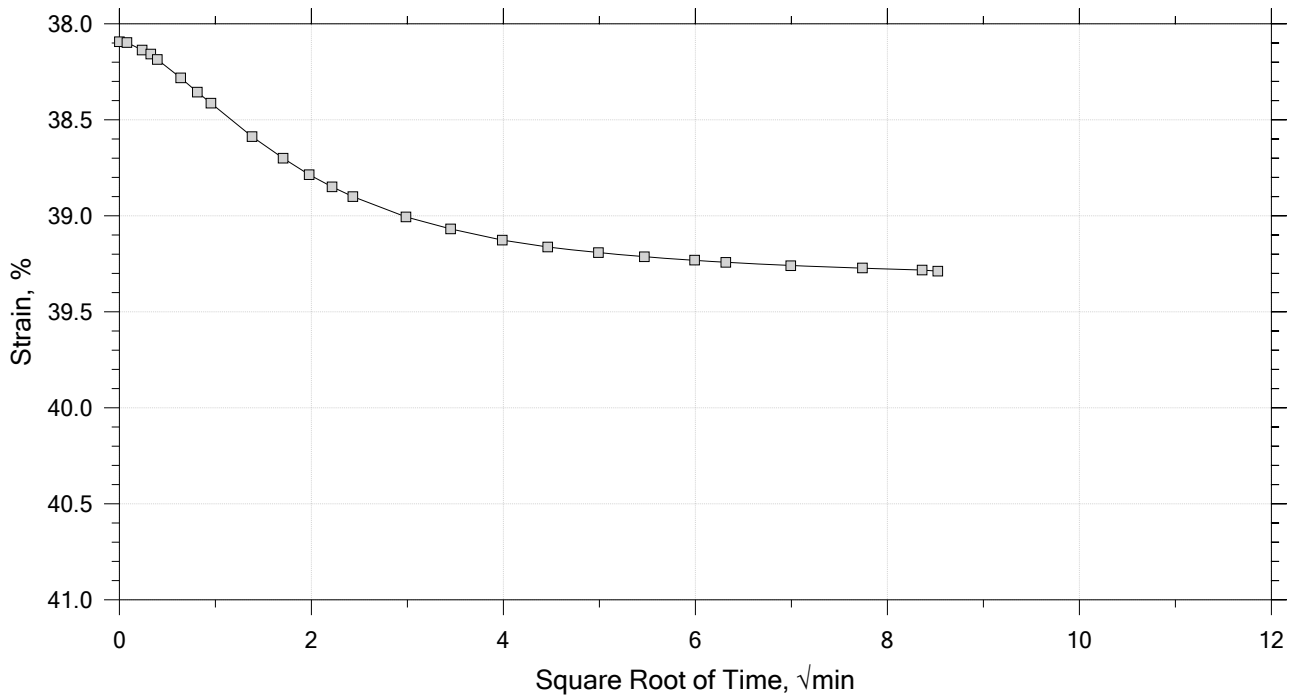
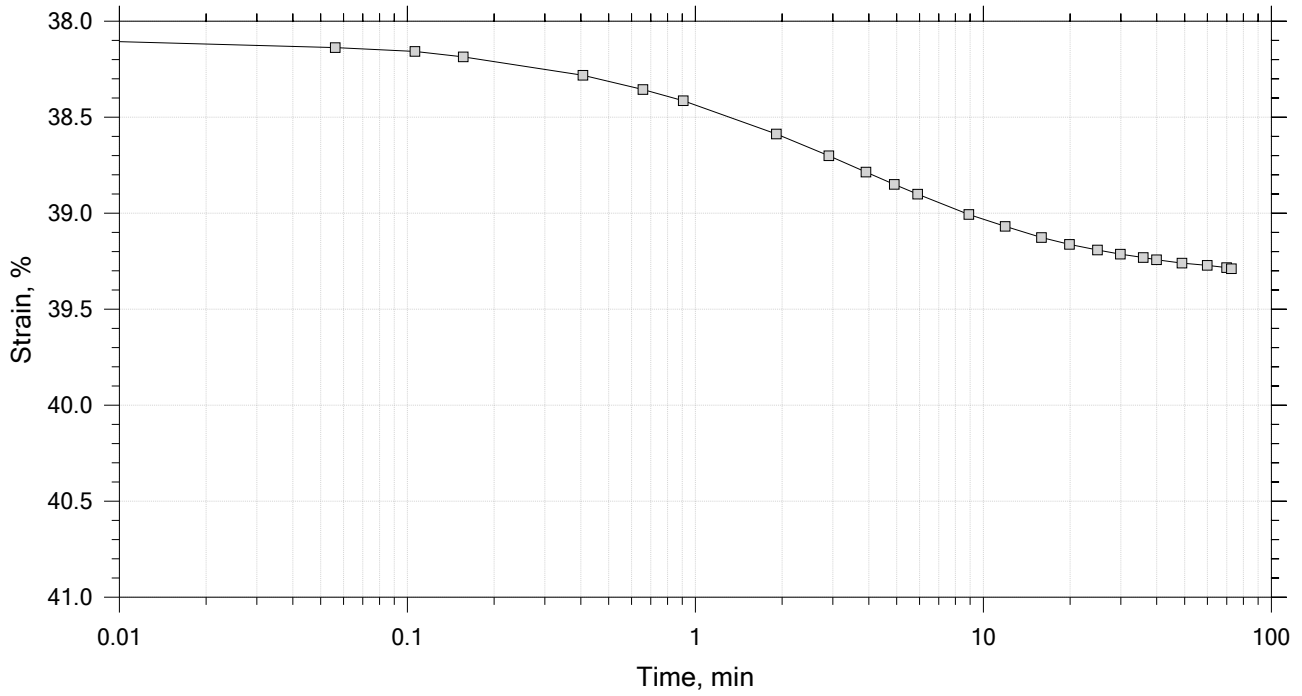
 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-3	Tested By: jm	Checked By: mcm
	Sample No.: 1	Test Date: 10/10/20	Depth: 0-2 ft
	Test No.: IP-4	Sample Type: intact	Elevation: ---
	Description: Moist, very dark brown peat(PT)		


# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 6 of 12

Constant Load Step

Stress: 250 psf



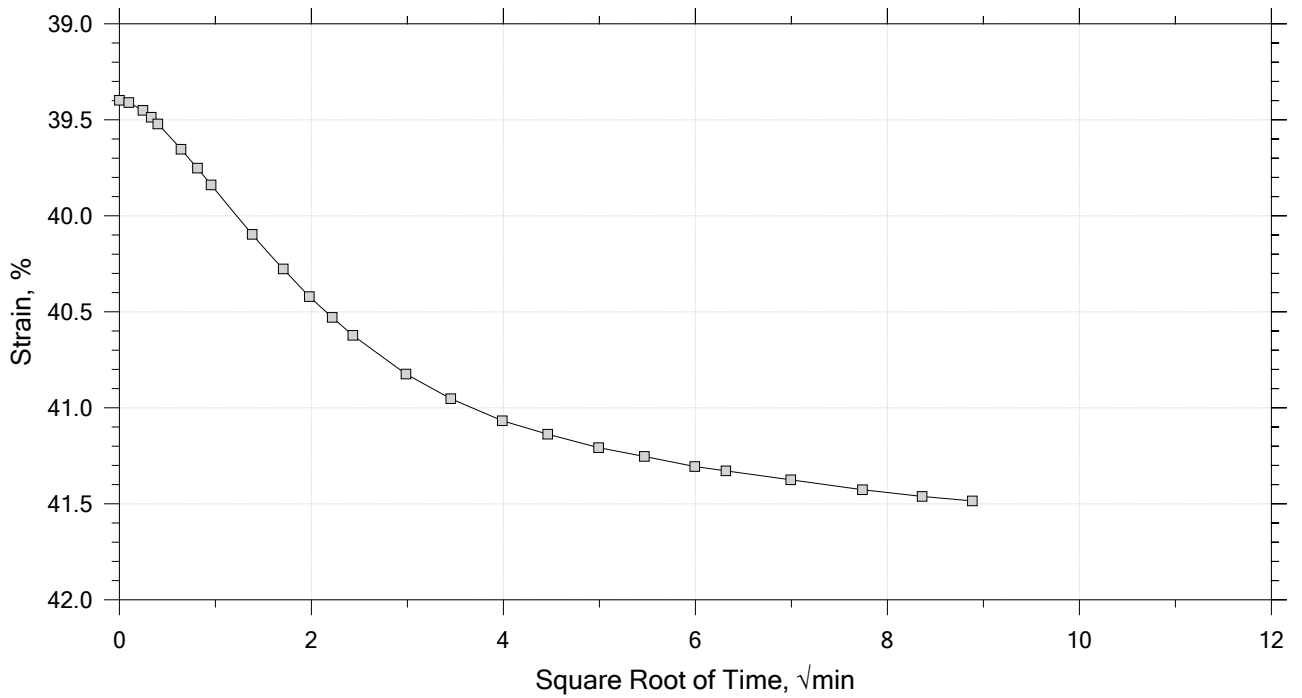
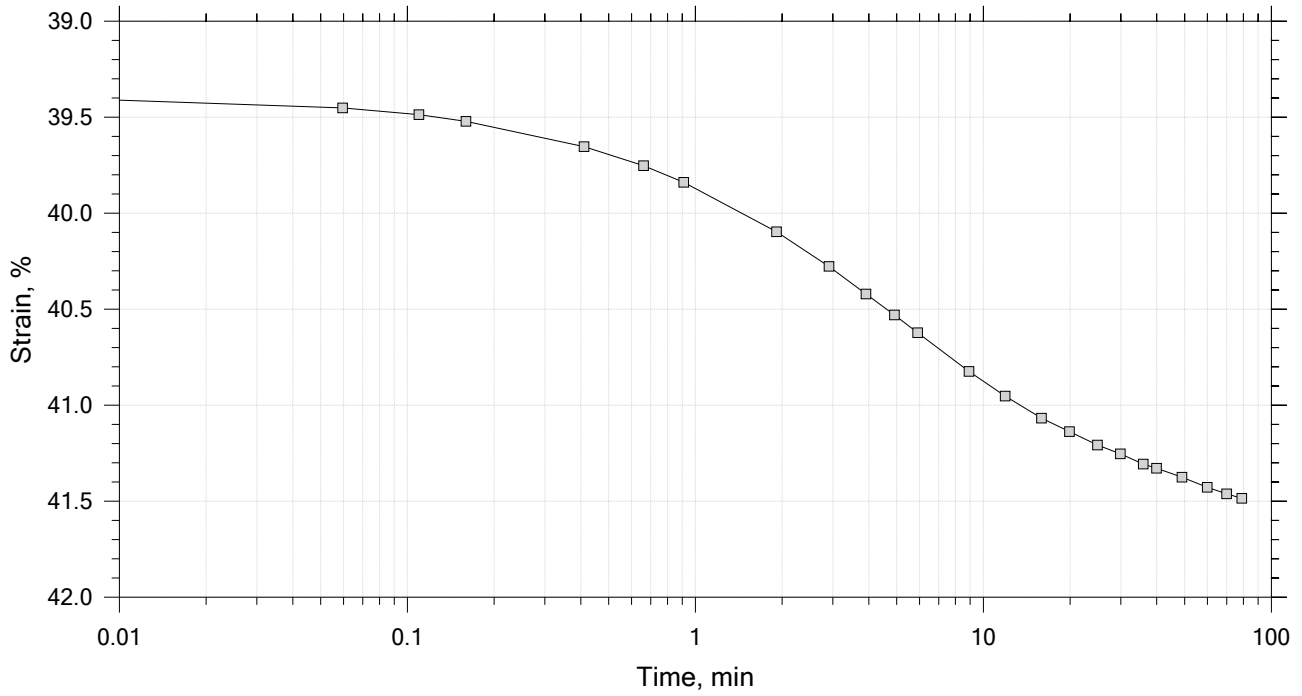
 <p>Engineering and Testing</p>	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-3	Tested By: jm	Checked By: mcm
	Sample No.:1	Test Date: 10/10/20	Depth: 0-2 ft
	Test No.: IP-4	Sample Type: intact	Elevation: ---
	Description: Moist, very dark brown peat(PT)		


# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 7 of 12

Constant Load Step

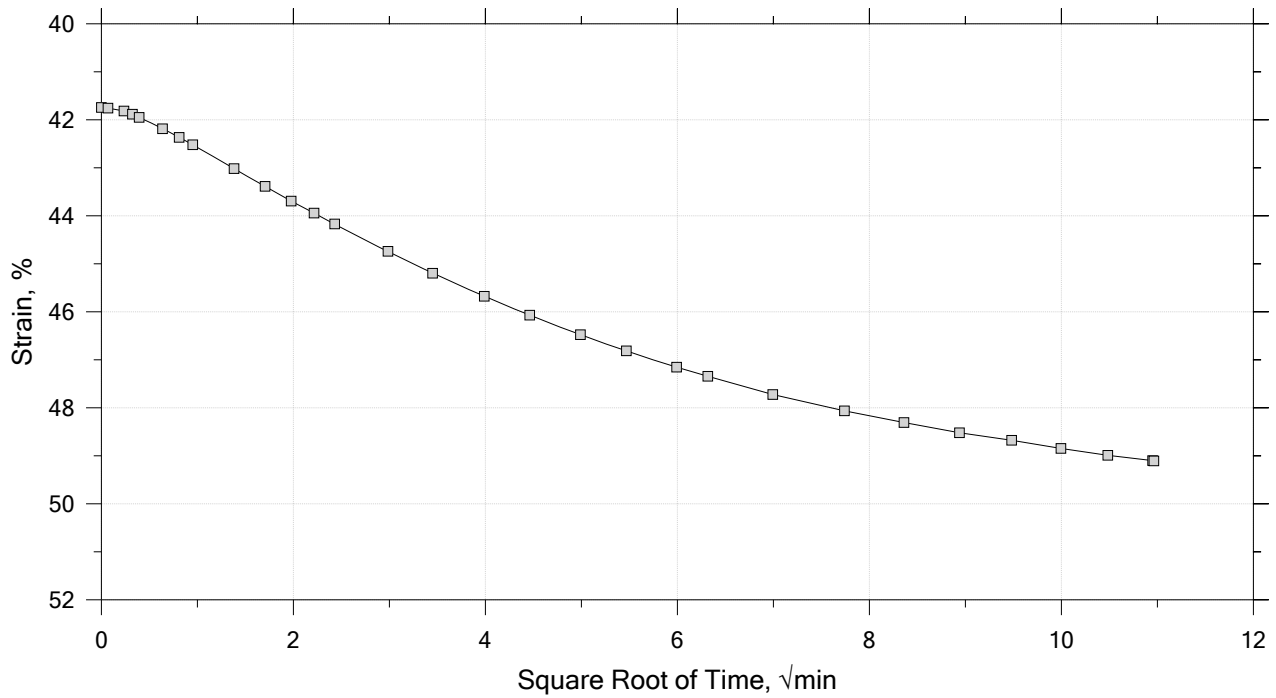
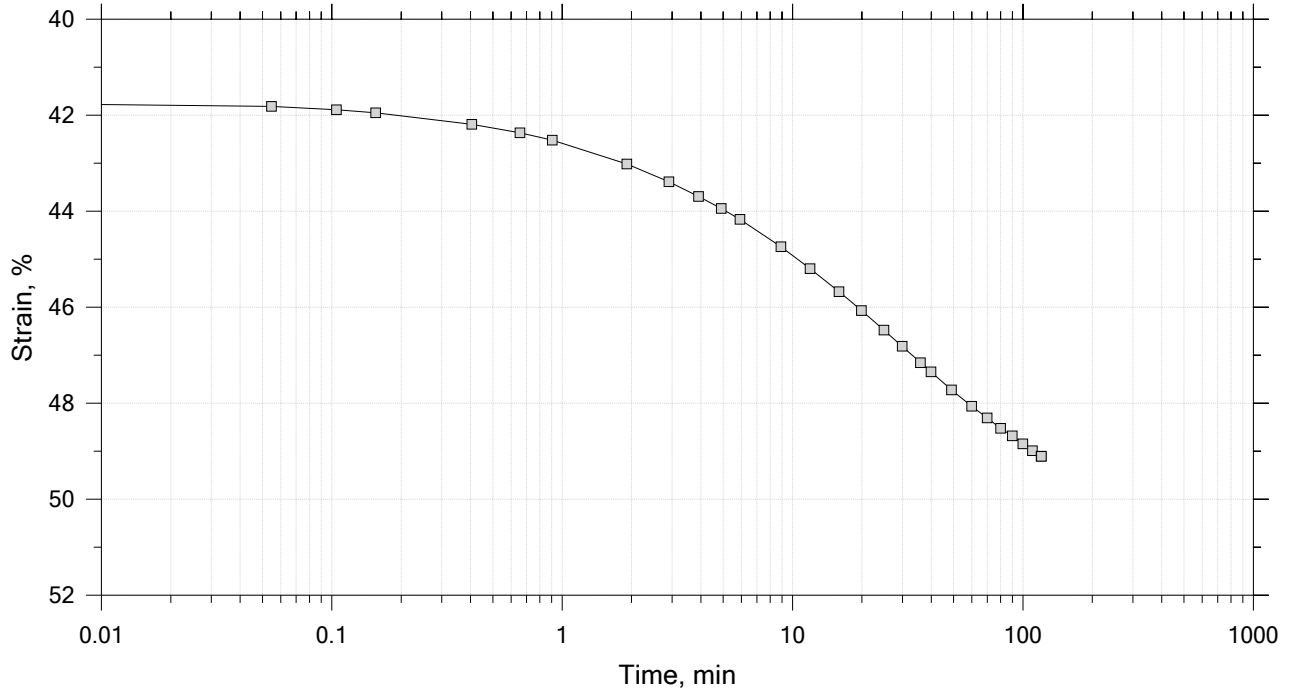
Stress: 500 psf




 <p>Engineering and Testing</p>	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-3	Tested By: jm	Checked By: mcm
	Sample No.:1	Test Date: 10/10/20	Depth: 0-2 ft
	Test No.: IP-4	Sample Type: intact	Elevation: ---
	Description: Moist, very dark brown peat(PT)		

# One-Dimensional Consolidation by ASTM D2435 - Method B

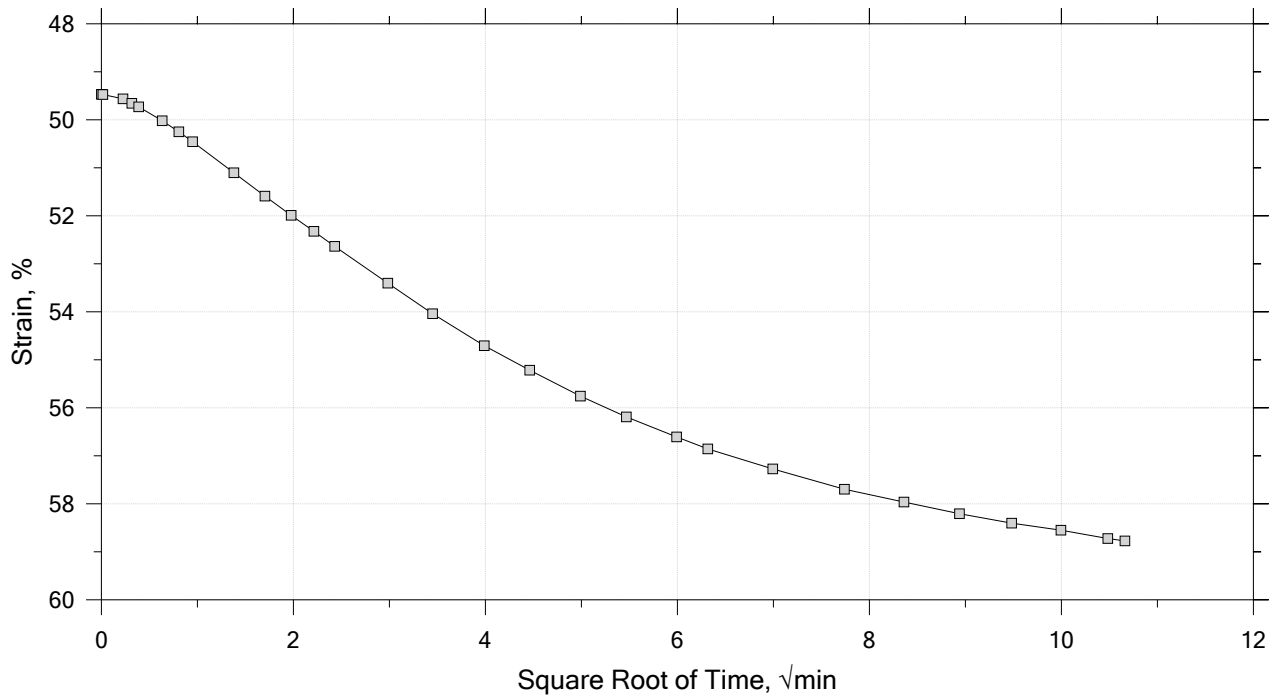
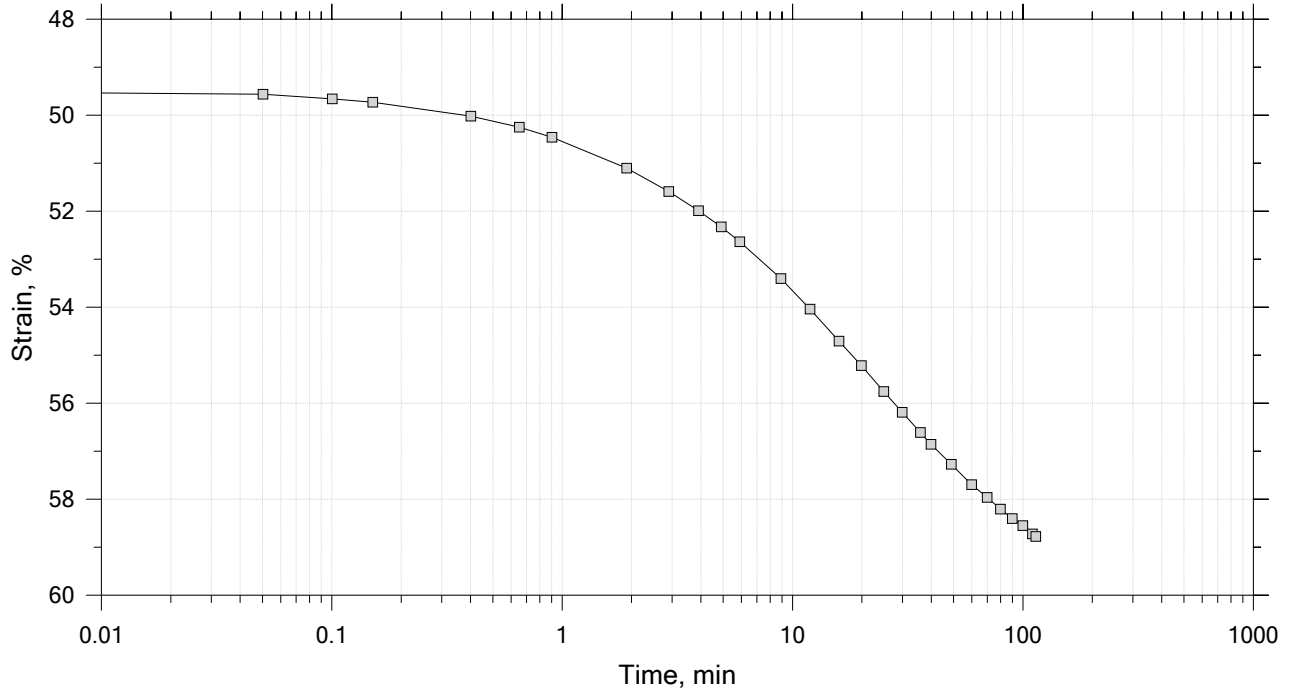
Time Curve 8 of 12  
 Constant Load Step  
 Stress: 1e+03 psf




 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-3	Tested By: jm	Checked By: mcm
	Sample No.:1	Test Date: 10/10/20	Depth: 0-2 ft
	Test No.: IP-4	Sample Type: intact	Elevation: ---
	Description: Moist, very dark brown peat(PT)		

# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 9 of 12  
 Constant Load Step  
 Stress: 2e+03 psf



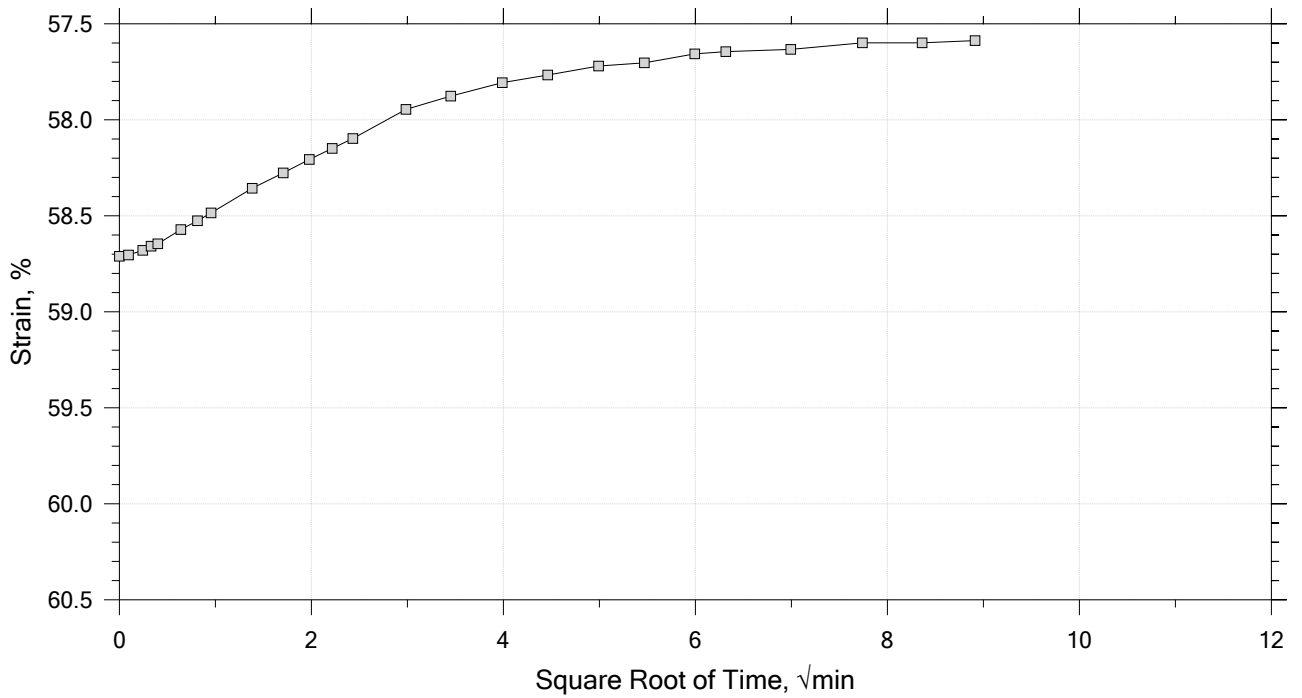
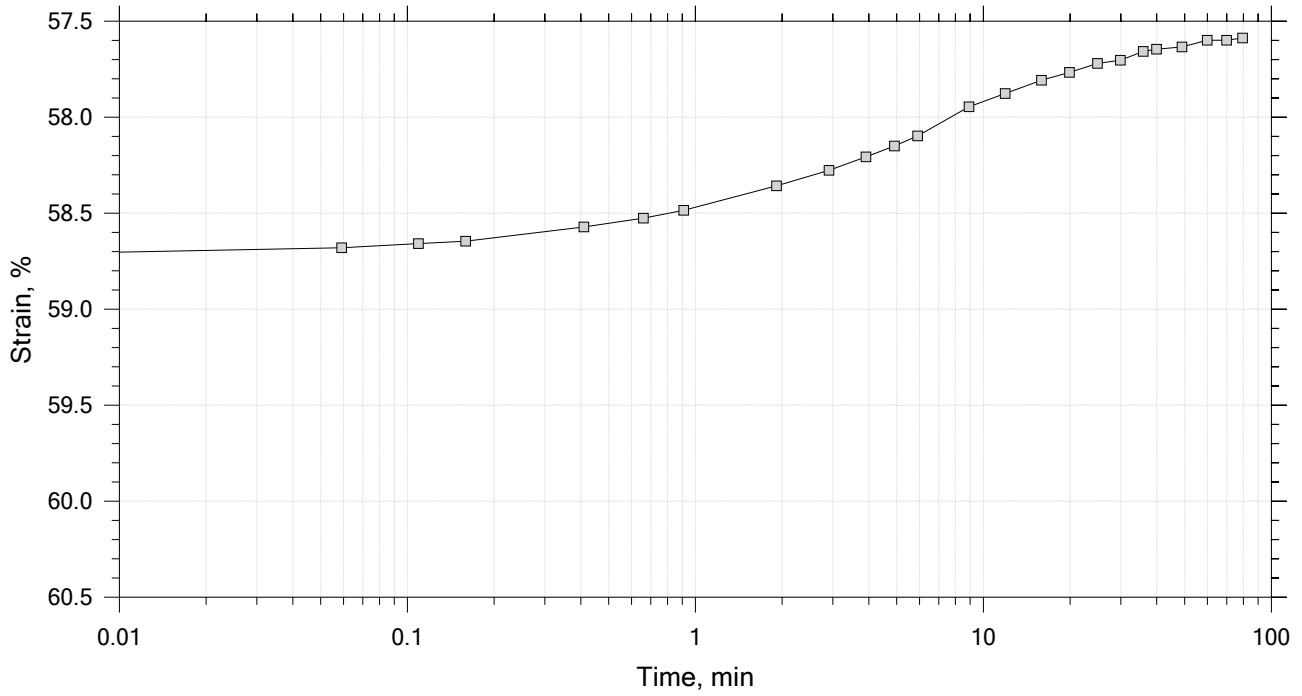
 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-3	Tested By: jm	Checked By: mcm
	Sample No.: 1	Test Date: 10/10/20	Depth: 0-2 ft
	Test No.: IP-4	Sample Type: intact	Elevation: ---
	Description: Moist, very dark brown peat(PT)		


# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 10 of 12

Constant Load Step

Stress: 1e+03 psf



 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-3	Tested By: jm	Checked By: mcm
	Sample No.:1	Test Date: 10/10/20	Depth: 0-2 ft
	Test No.: IP-4	Sample Type: intact	Elevation: ---
	Description: Moist, very dark brown peat(PT)		

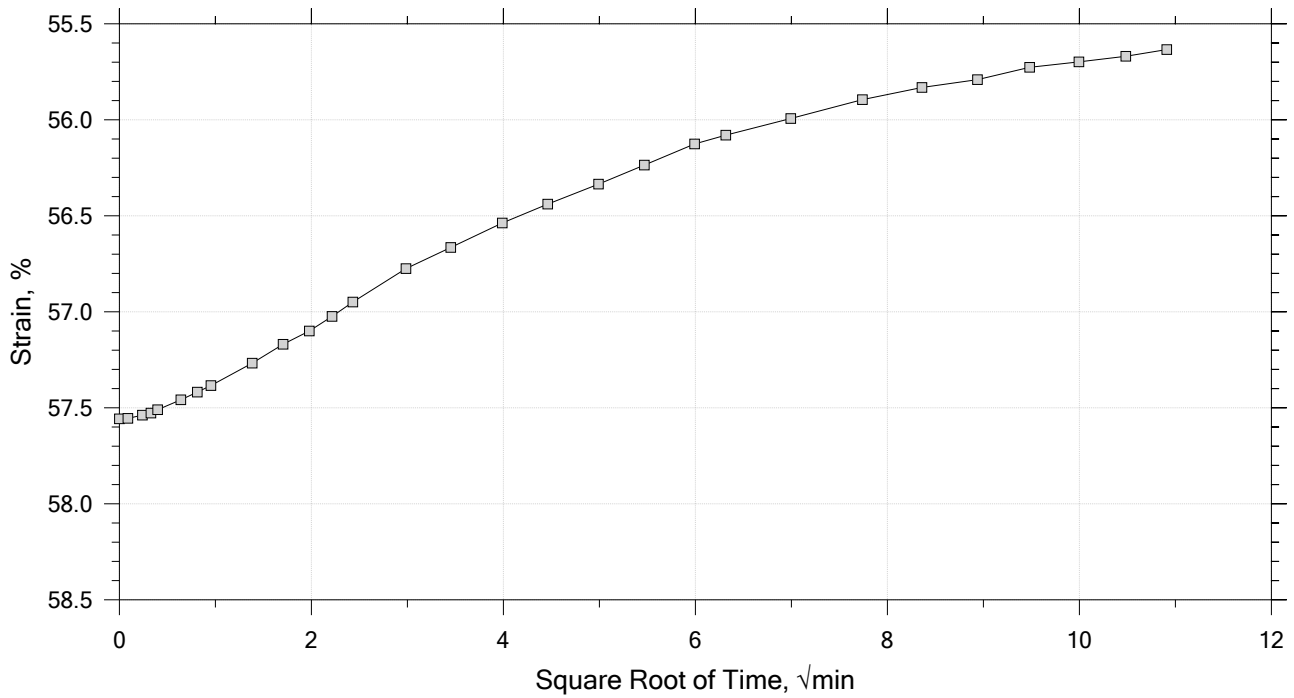
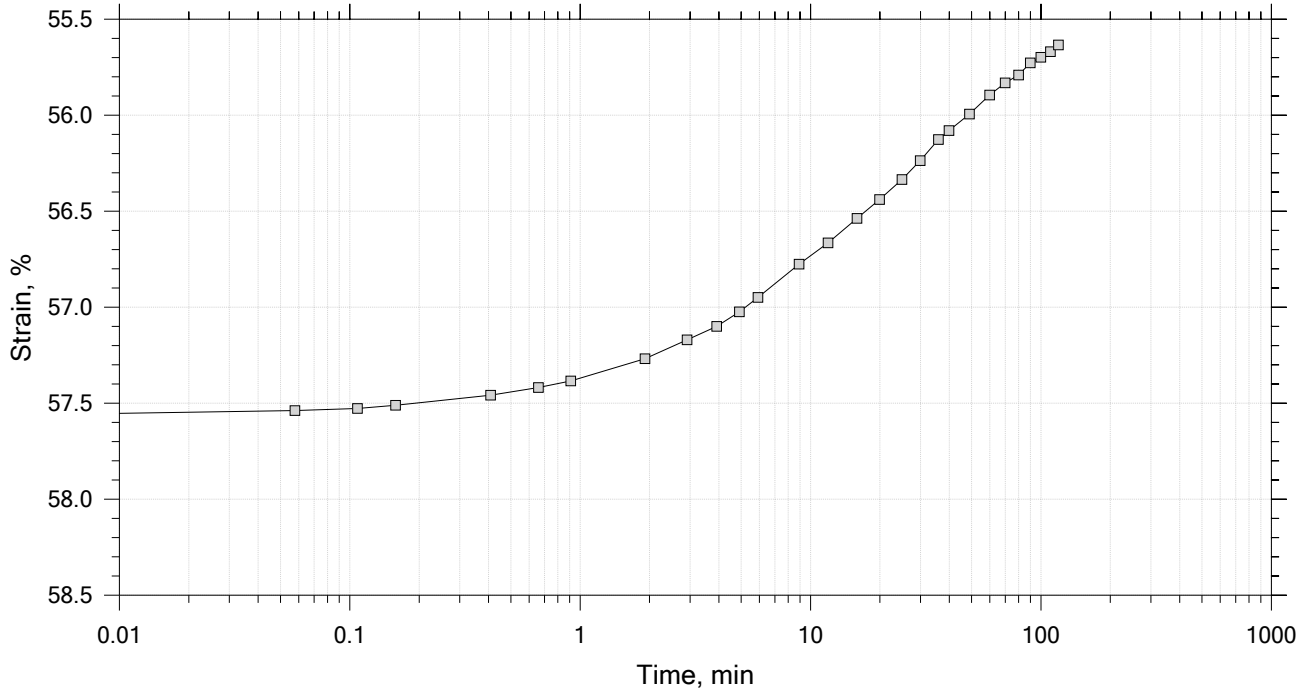



# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 11 of 12

Constant Load Step

Stress: 500 psf



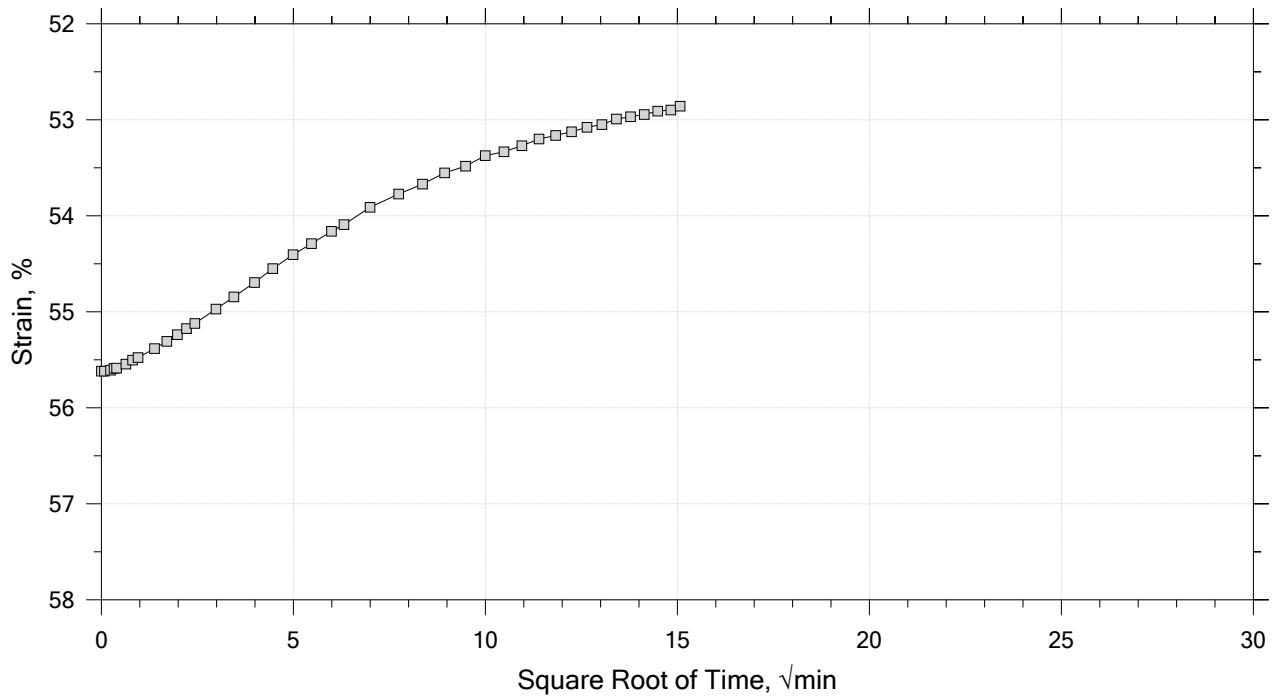
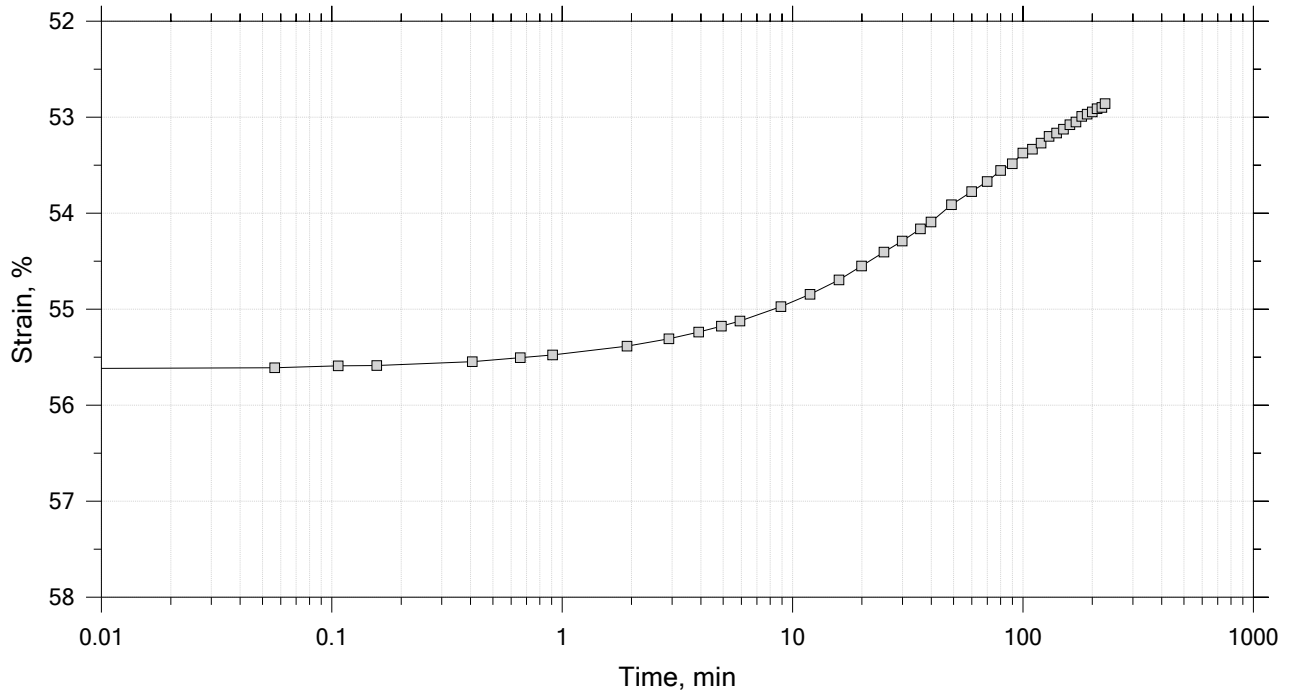
 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-3	Tested By: jm	Checked By: mcm
	Sample No.: 1	Test Date: 10/10/20	Depth: 0-2 ft
	Test No.: IP-4	Sample Type: intact	Elevation: ---
	Description: Moist, very dark brown peat(PT)		


# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 12 of 12

Constant Load Step

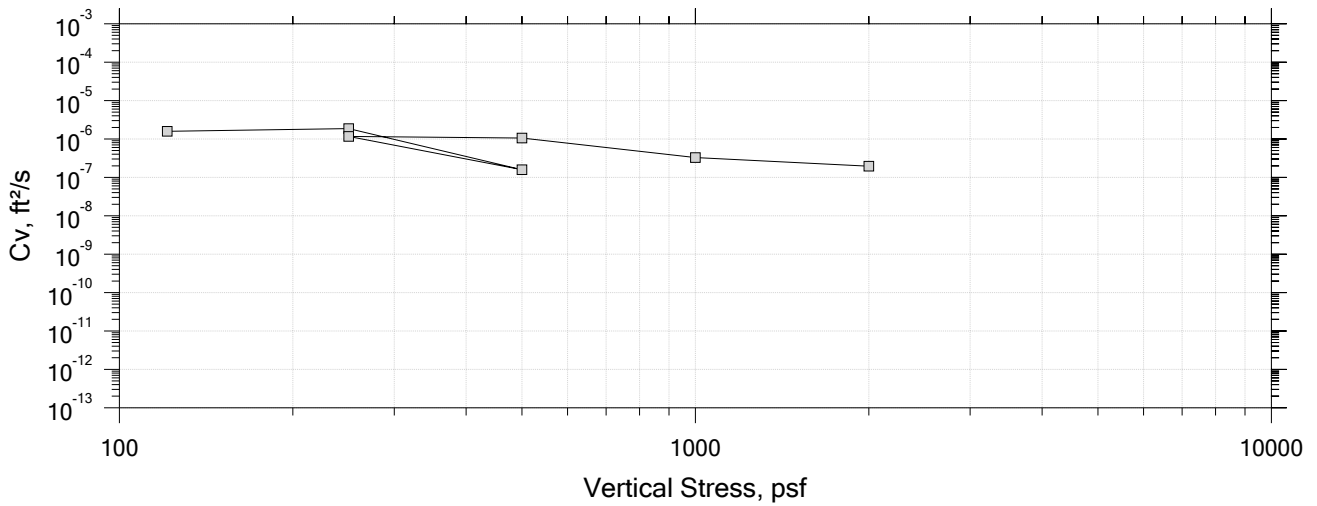
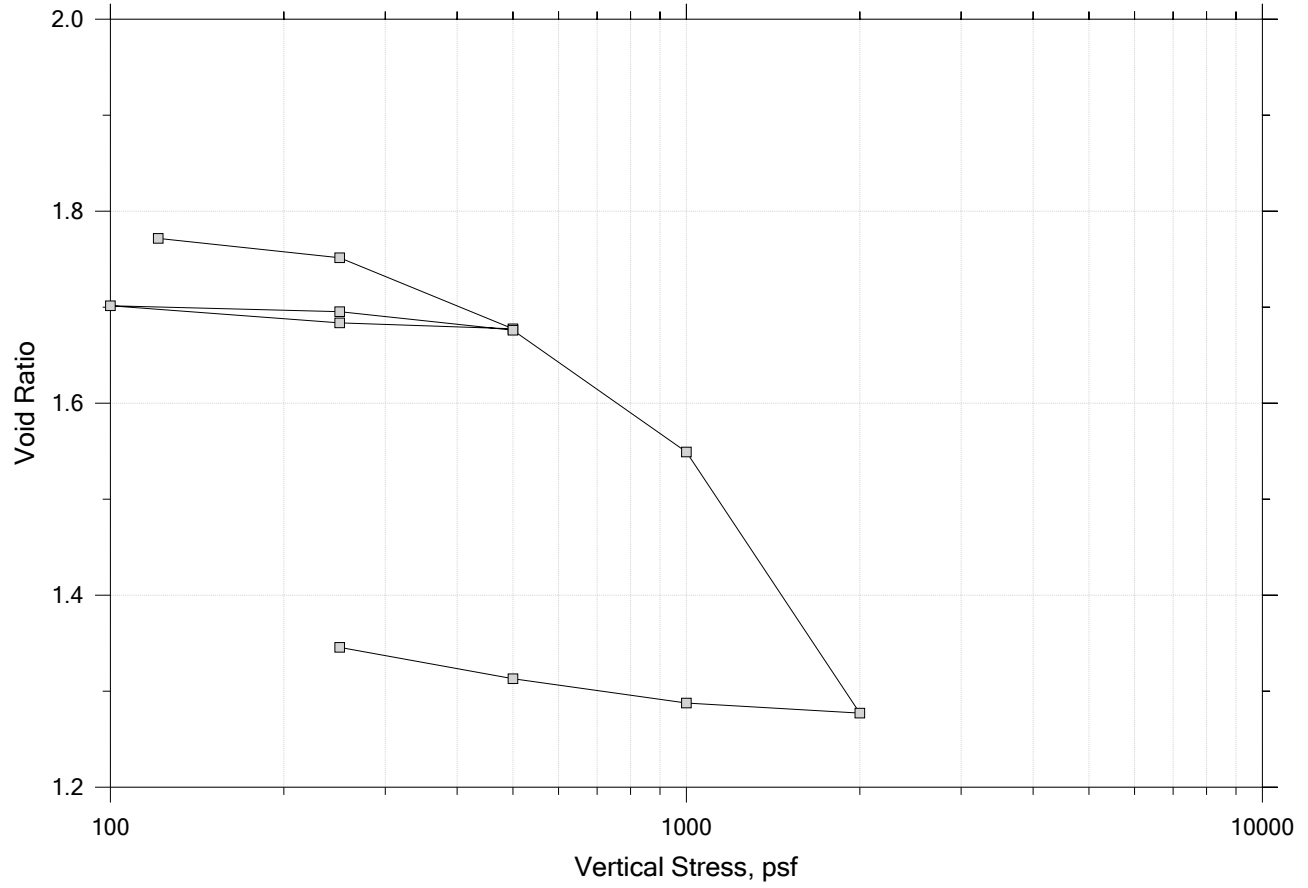
Stress: 250 psf




 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-3	Tested By: jm	Checked By: mcm
	Sample No.: 1	Test Date: 10/10/20	Depth: 0-2 ft
	Test No.: IP-4	Sample Type: intact	Elevation: ---
	Description: Moist, very dark brown peat(PT)		

# One-Dimensional Consolidation by ASTM D2435 - Method B

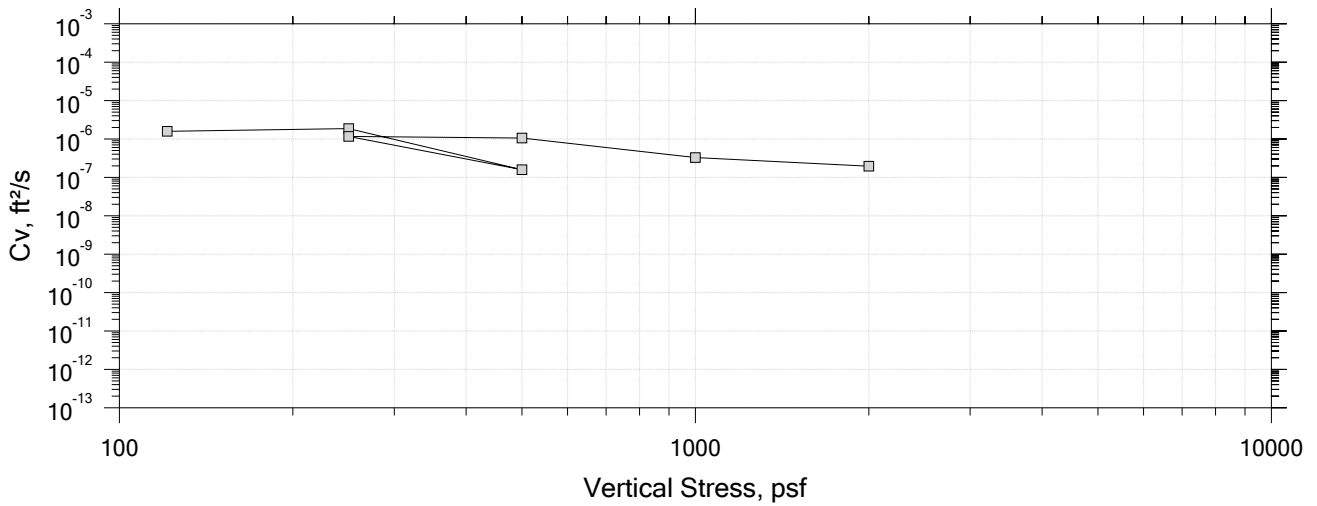
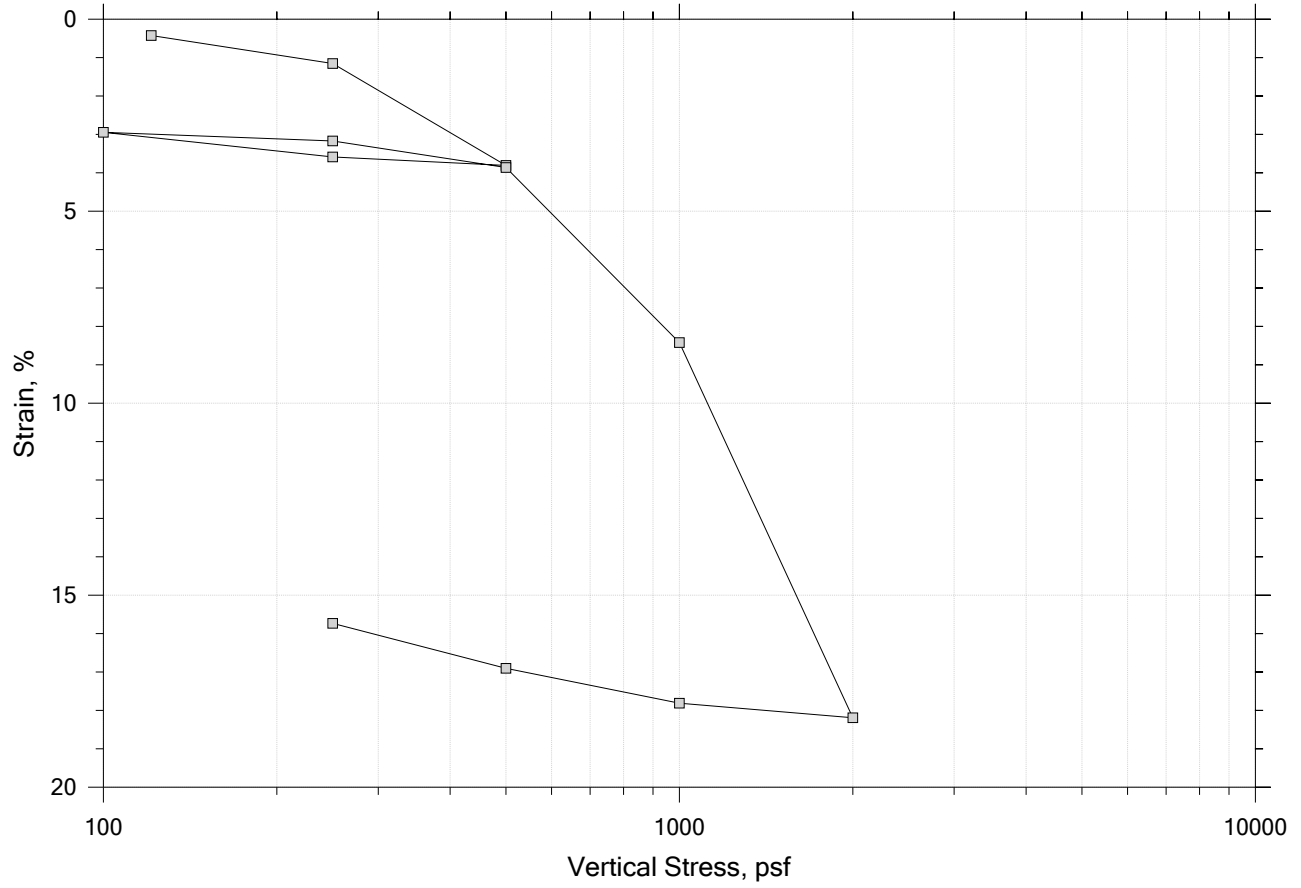
## Summary Report




	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-3	Tested By: jm	Checked By: mcm
	Sample No.: 6	Test Date: 10/8/20	Depth: 10-12 ft
	Test No.: IP-5	Sample Type: intact	Elevation: ---
	Description: Moist, greenish gray clay(CH)	Measured specific gravity: 2.62	

# One-Dimensional Consolidation by ASTM D2435 - Method B

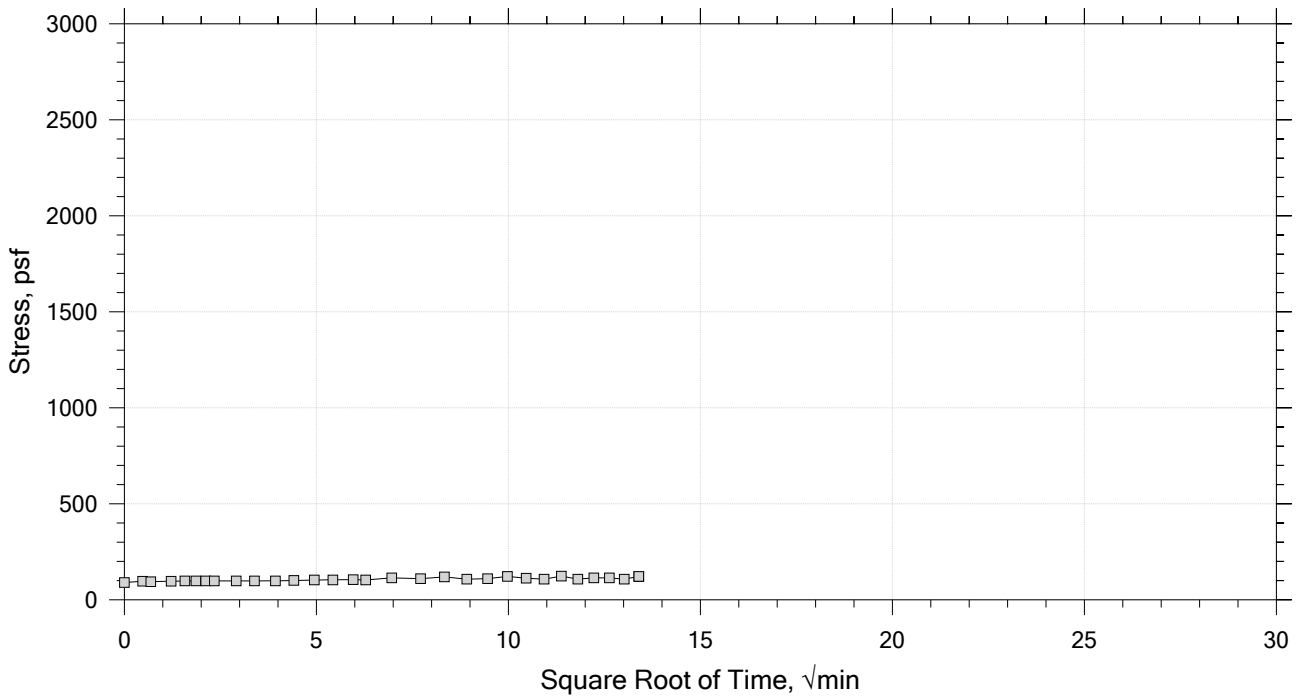
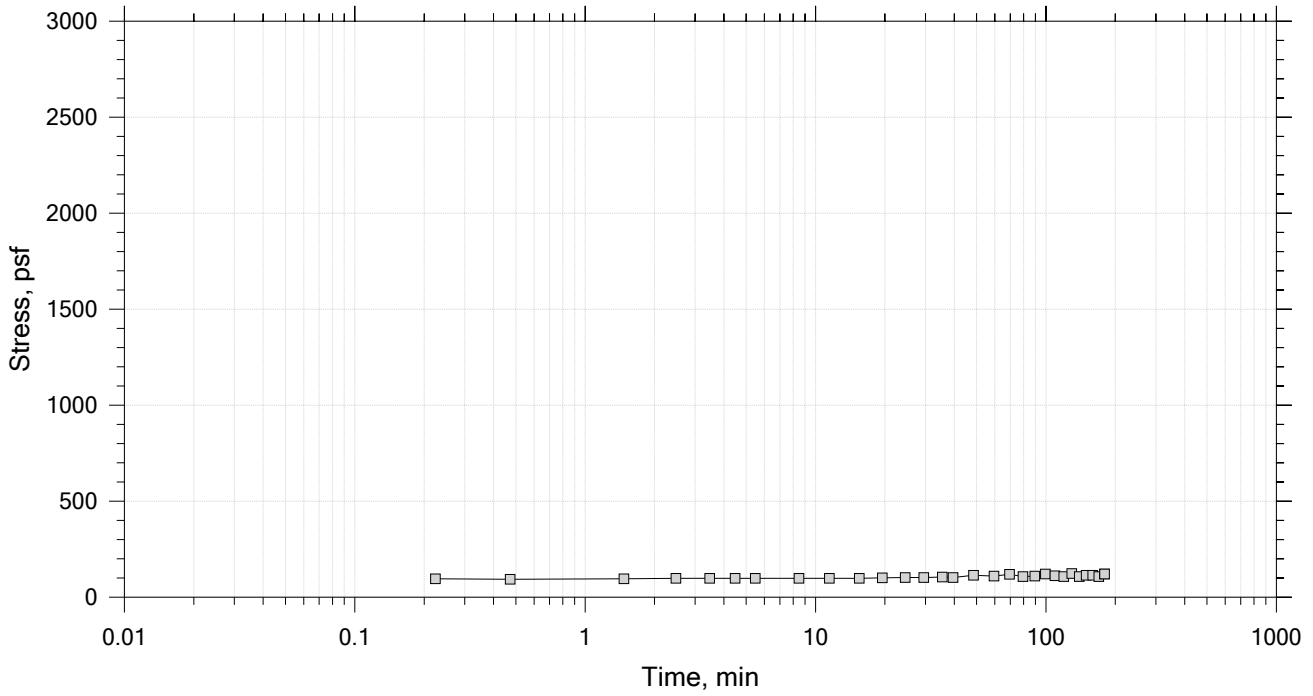
## Summary Report




 <p>APS Engineering and Testing</p>	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-3	Tested By: jm	Checked By: mcm
	Sample No.: 6	Test Date: 10/8/20	Depth: 10-12 ft
	Test No.: IP-5	Sample Type: intact	Elevation: ---
	Description: Moist, greenish gray clay (CH)		

# One-Dimensional Consolidation by ASTM D2435 - Method B

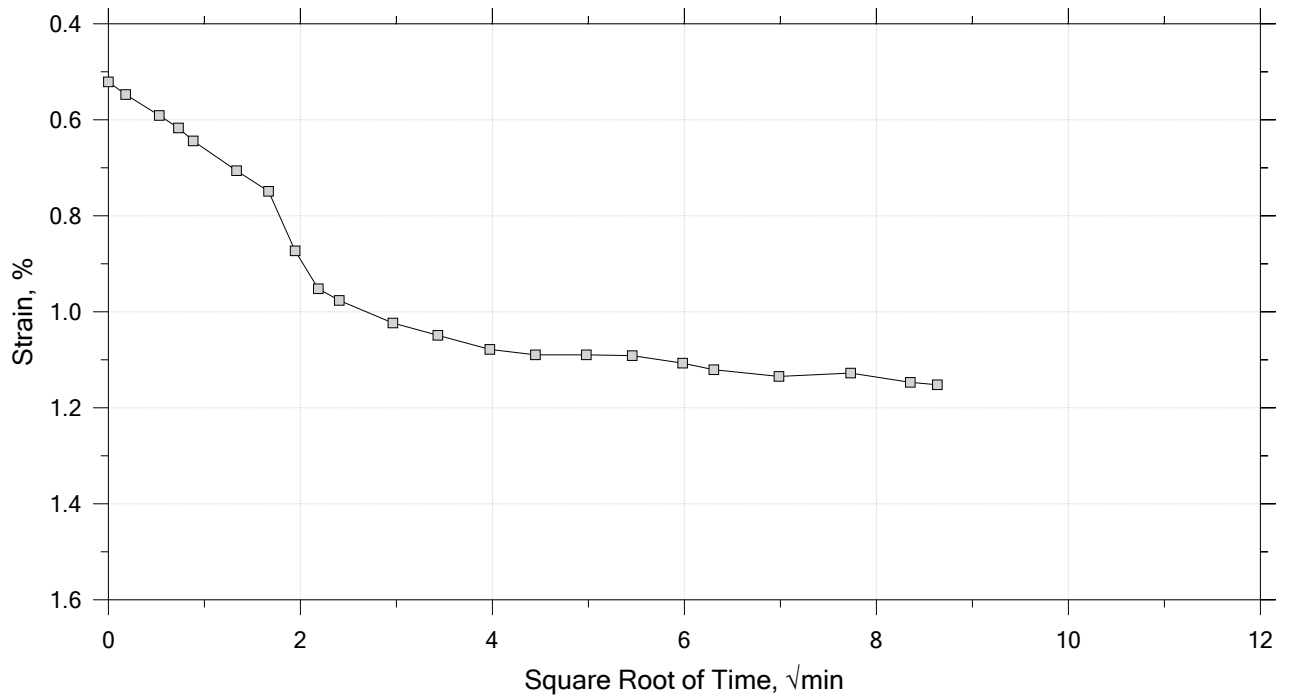
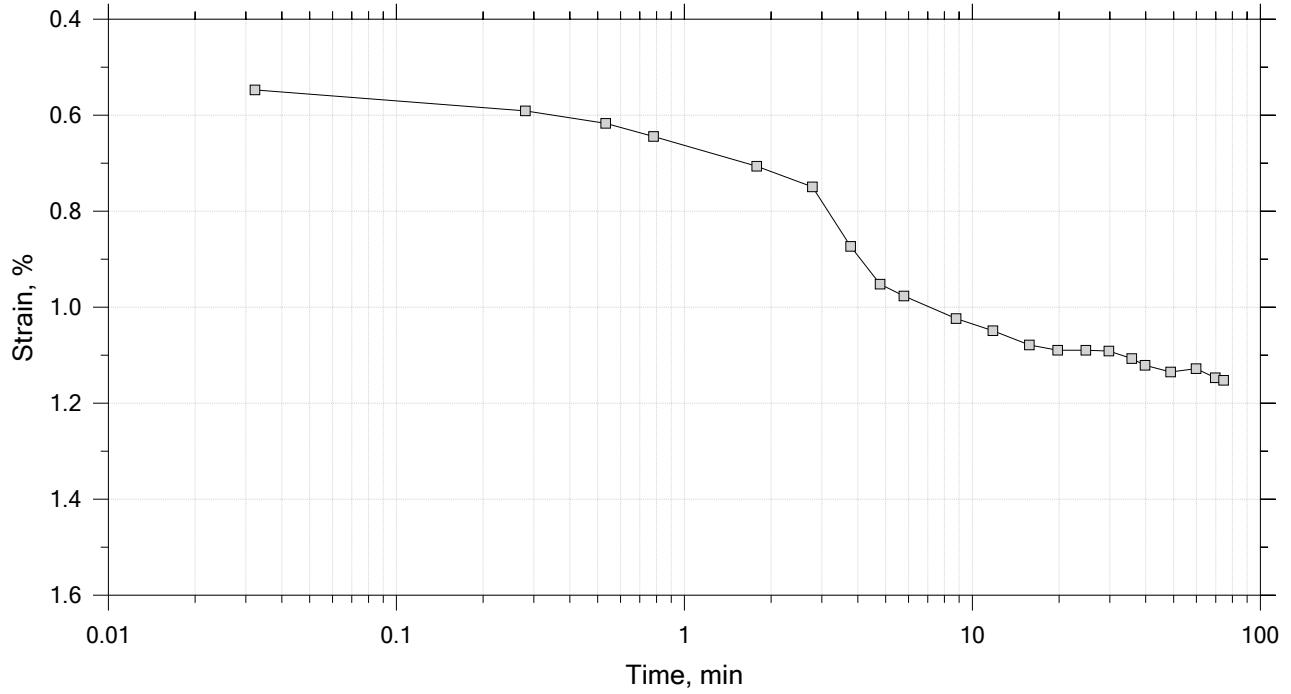
Time Curve 1 of 12  
 Constant Volume Step  
 Stress: 121 psf




 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-3	Tested By: jm	Checked By: mcm
	Sample No.: 6	Test Date: 10/8/20	Depth: 10-12 ft
	Test No.: IP-5	Sample Type: intact	Elevation: ---
	Description: Moist, greenish gray clay(CH)		

# One-Dimensional Consolidation by ASTM D2435 - Method B

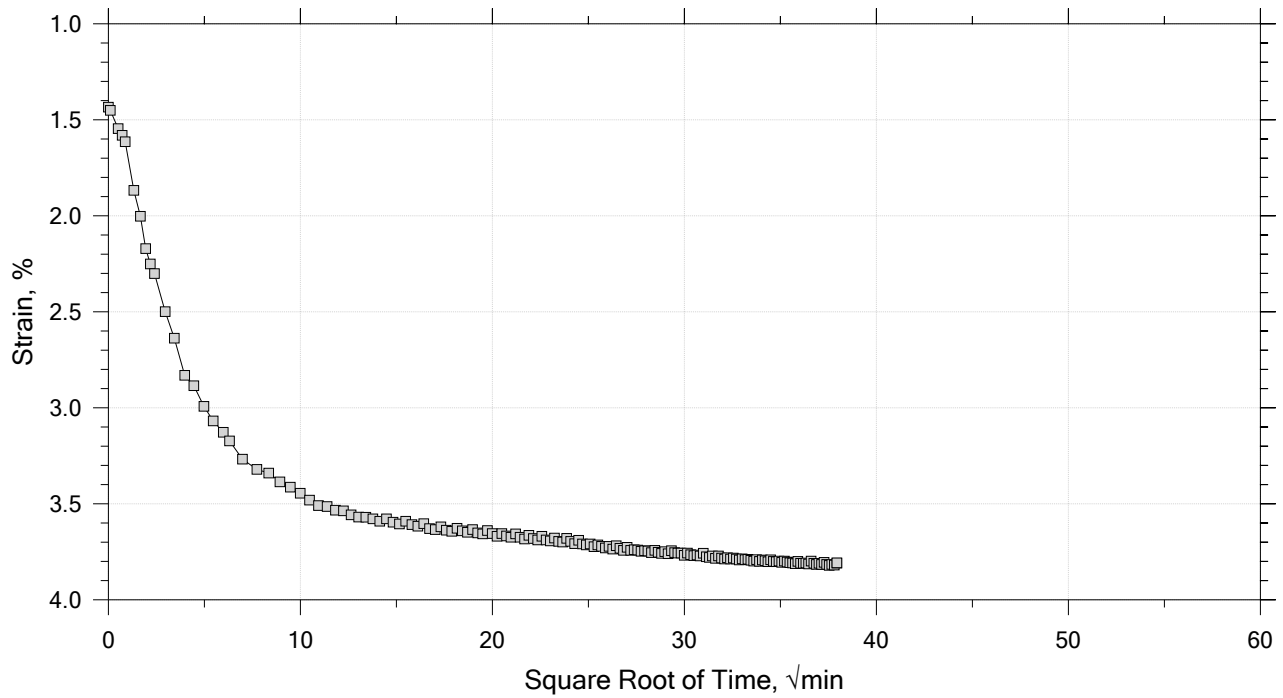
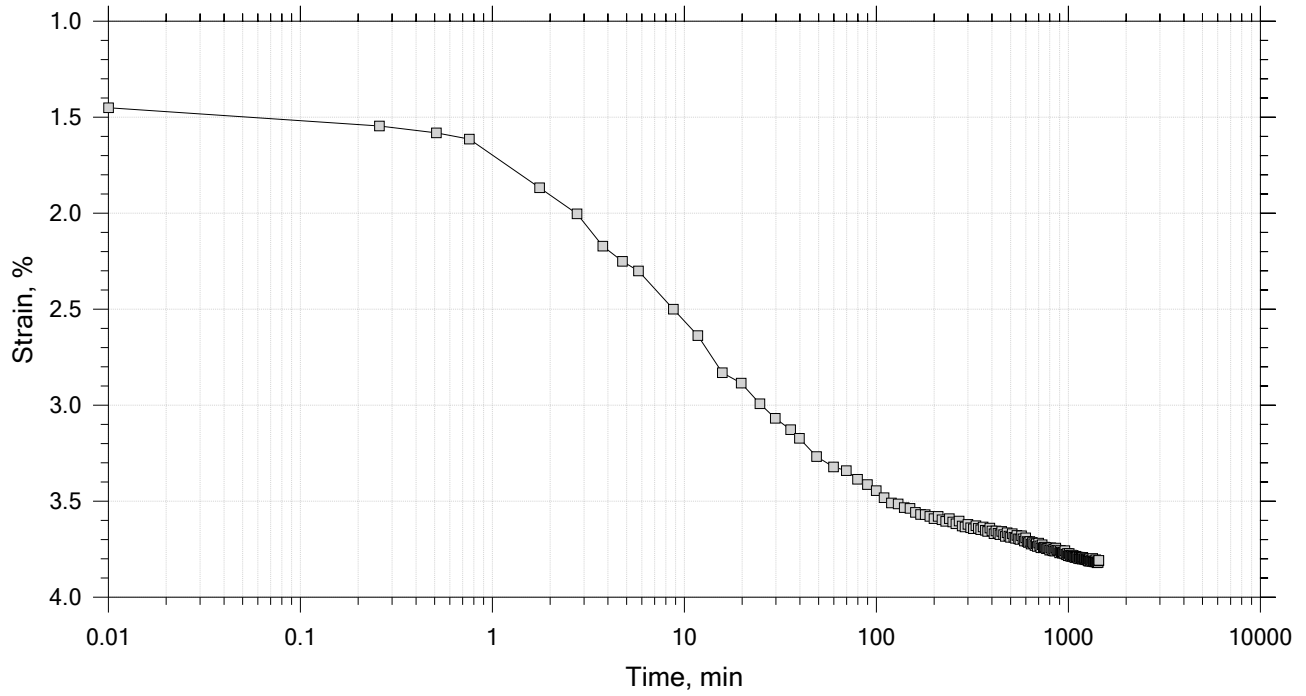
Time Curve 2 of 12  
 Constant Load Step  
 Stress: 250 psf




 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-3	Tested By: jm	Checked By: mcm
	Sample No.: 6	Test Date: 10/8/20	Depth: 10-12 ft
	Test No.: IP-5	Sample Type: intact	Elevation: ---
	Description: Moist, greenish gray clay(CH)		

# One-Dimensional Consolidation by ASTM D2435 - Method B

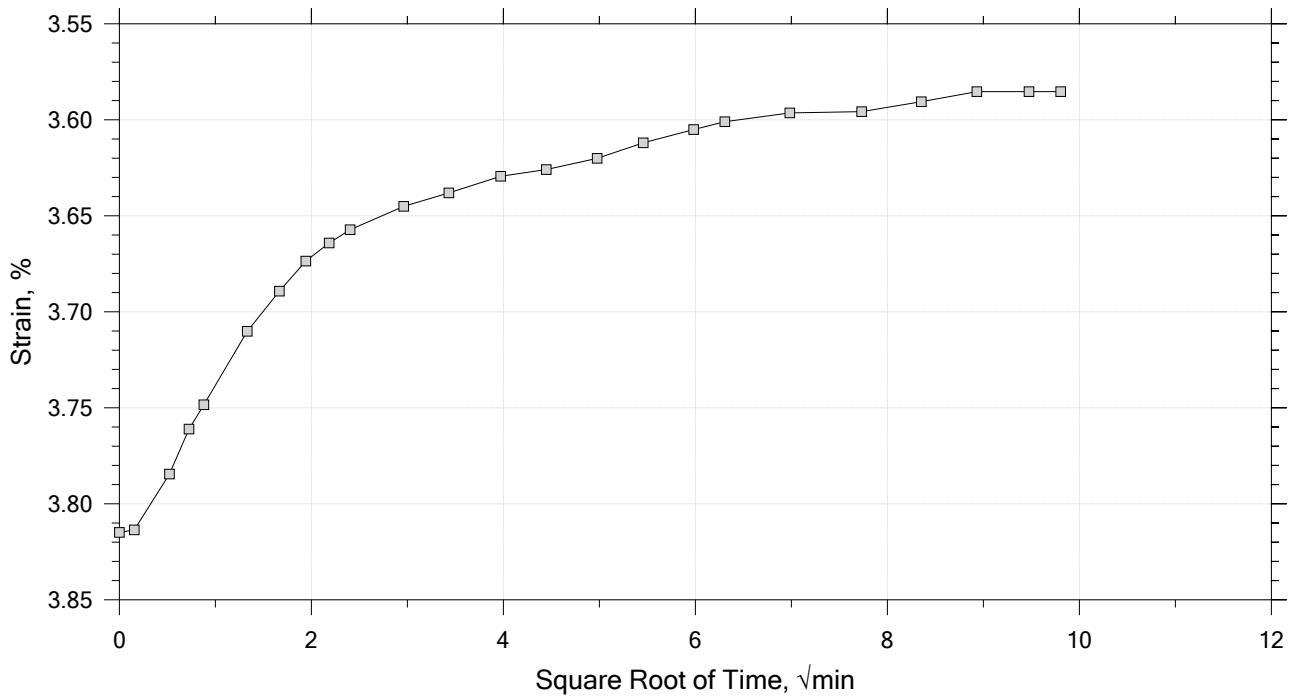
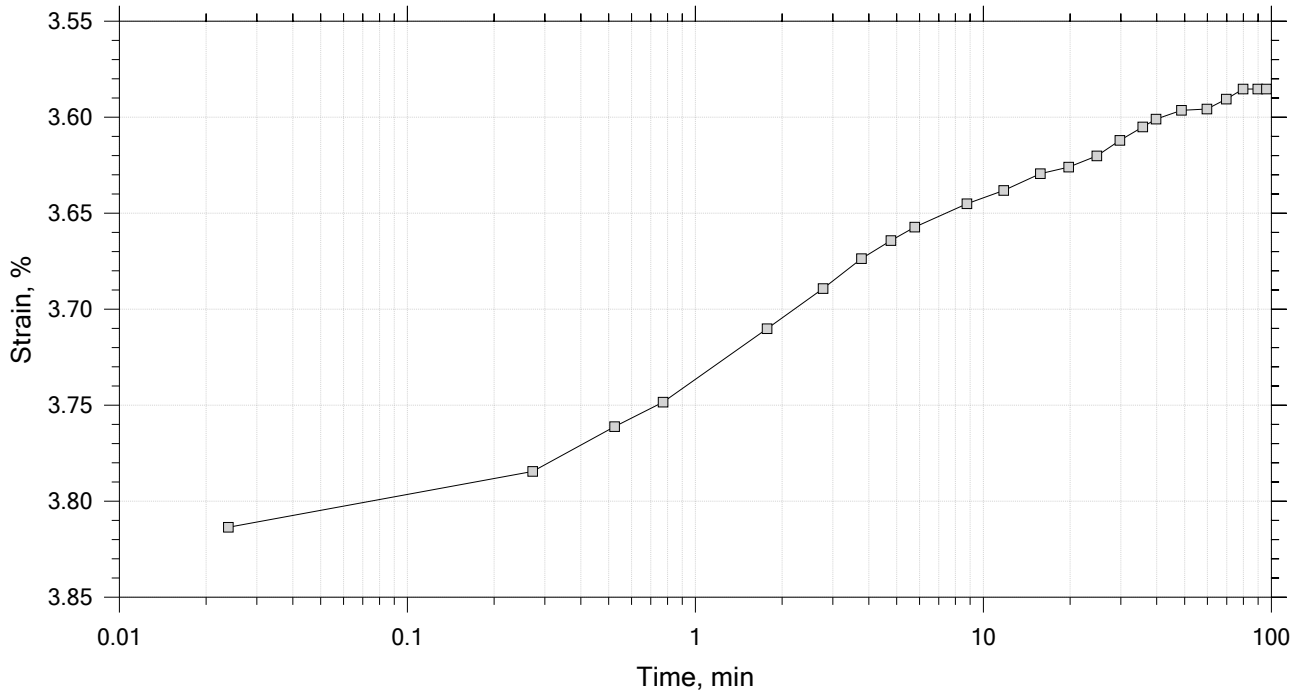
Time Curve 3 of 12  
 Constant Load Step  
 Stress: 500 psf




 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-3	Tested By: jm	Checked By: mcm
	Sample No.: 6	Test Date: 10/8/20	Depth: 10-12 ft
	Test No.: IP-5	Sample Type: intact	Elevation: ---
	Description: Moist, greenish gray clay(CH)		

# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 4 of 12  
 Constant Load Step  
 Stress: 250 psf

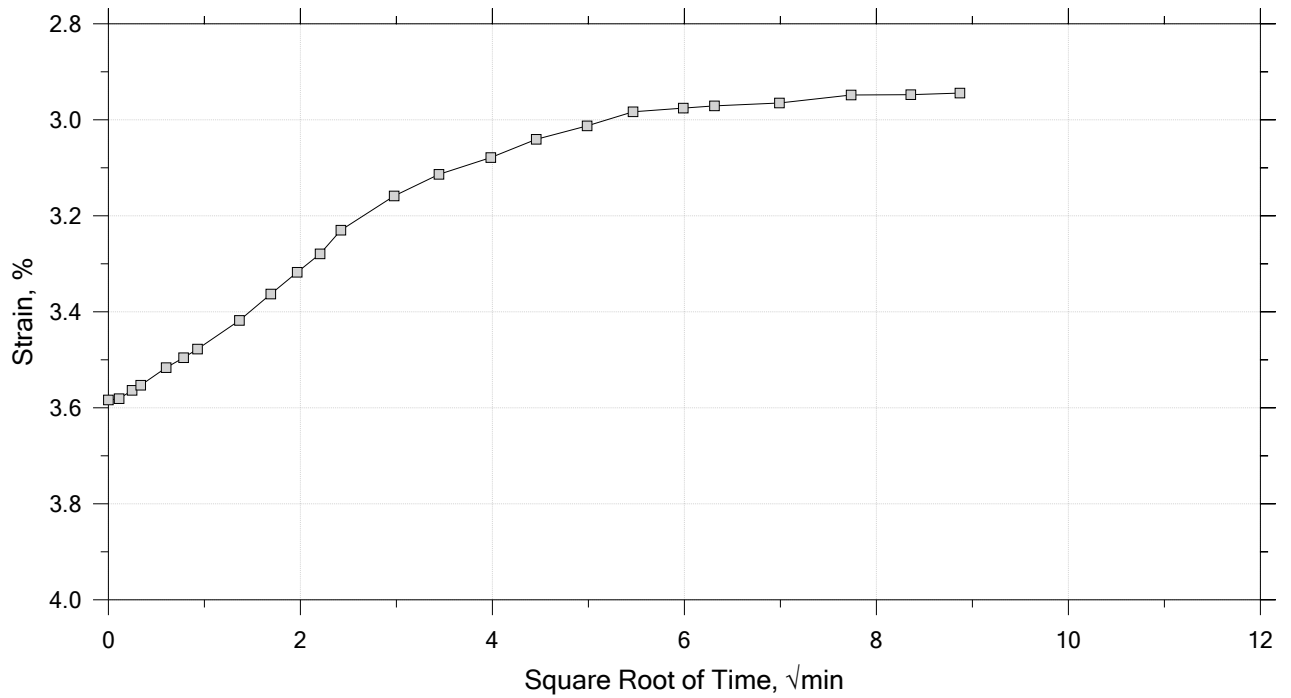
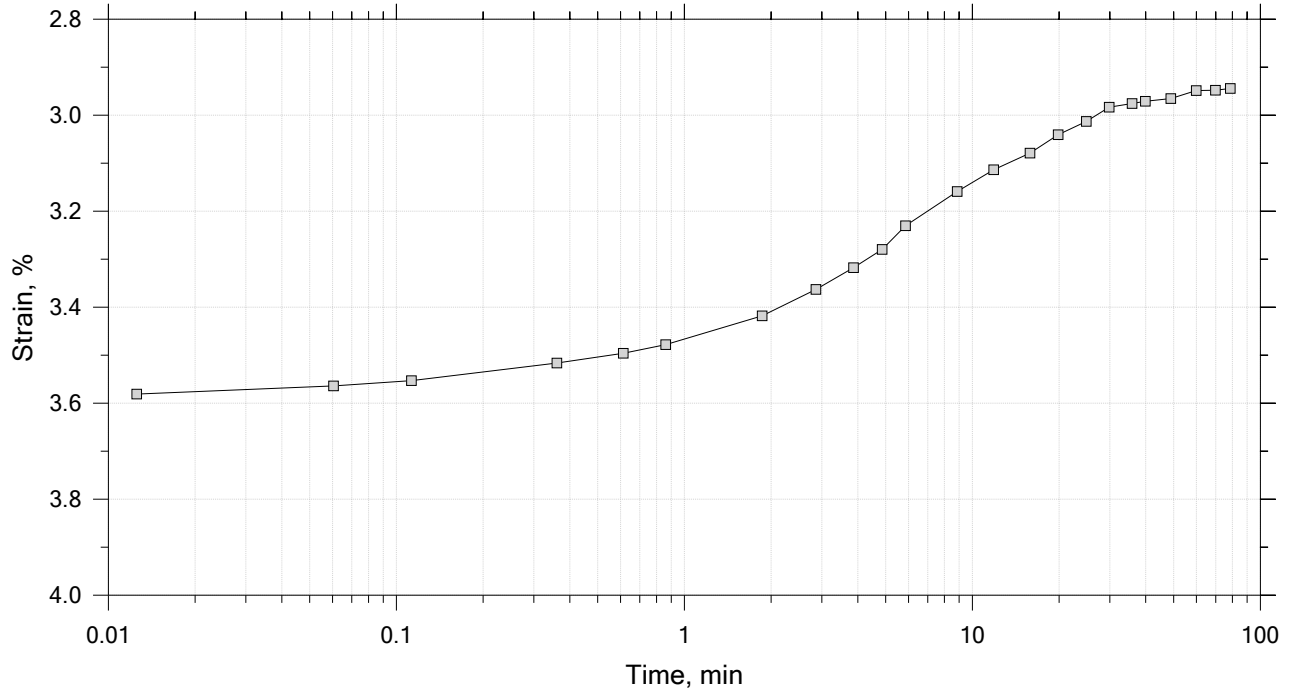



 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-3	Tested By: jm	Checked By: mcm
	Sample No.: 6	Test Date: 10/8/20	Depth: 10-12 ft
	Test No.: IP-5	Sample Type: intact	Elevation: ---
	Description: Moist, greenish gray clay(CH)		



# One-Dimensional Consolidation by ASTM D2435 - Method B

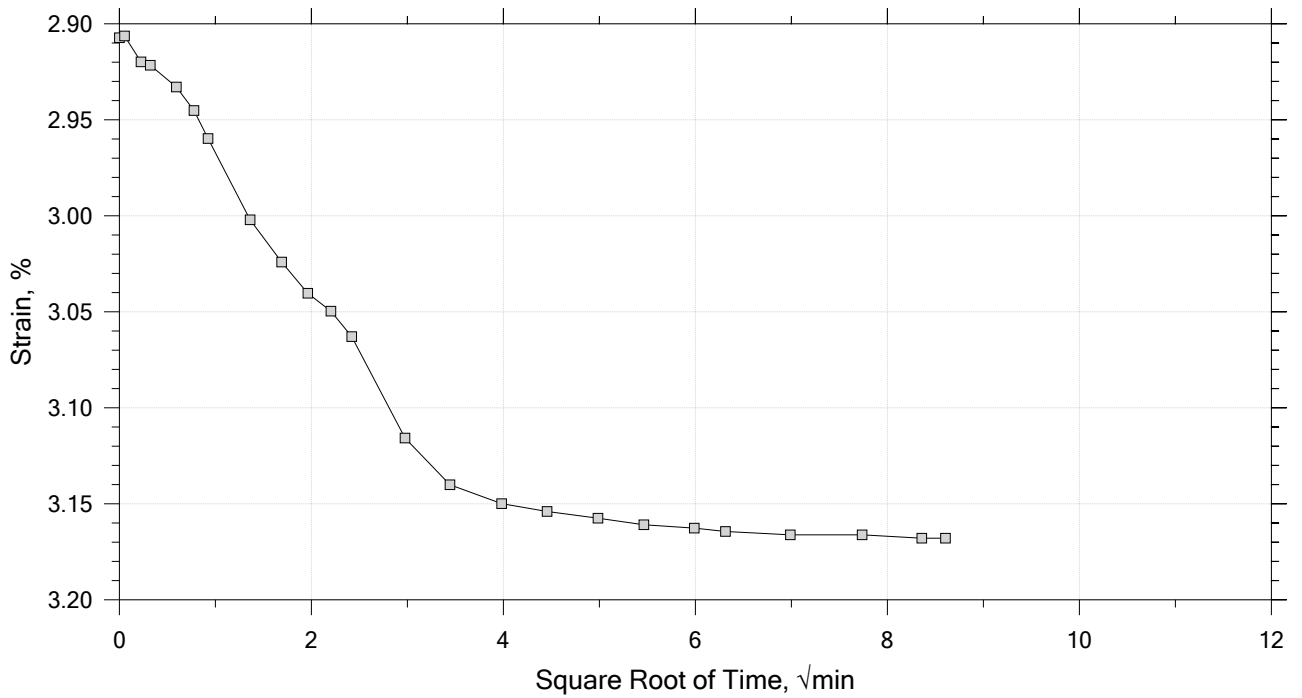
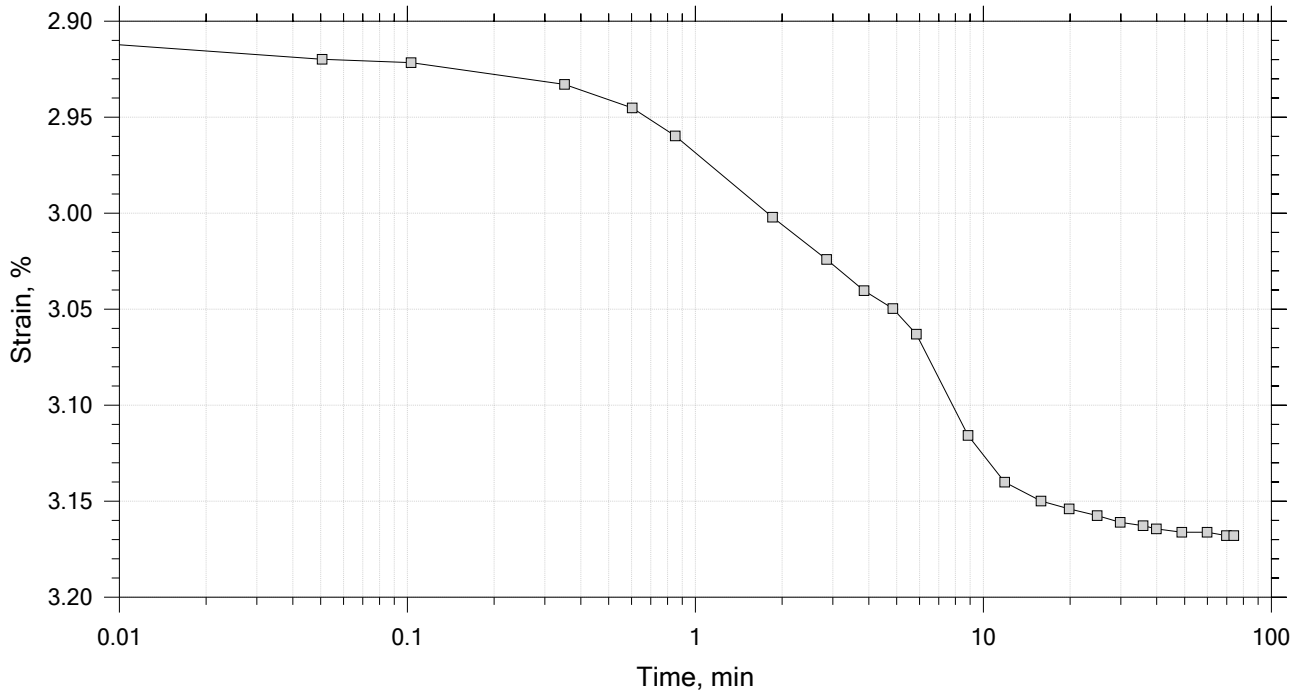
Time Curve 5 of 12  
 Constant Load Step  
 Stress: 100 psf




 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-3	Tested By: jm	Checked By: mcm
	Sample No.: 6	Test Date: 10/8/20	Depth: 10-12 ft
	Test No.: IP-5	Sample Type: intact	Elevation: ---
	Description: Moist, greenish gray clay(CH)		

# One-Dimensional Consolidation by ASTM D2435 - Method B

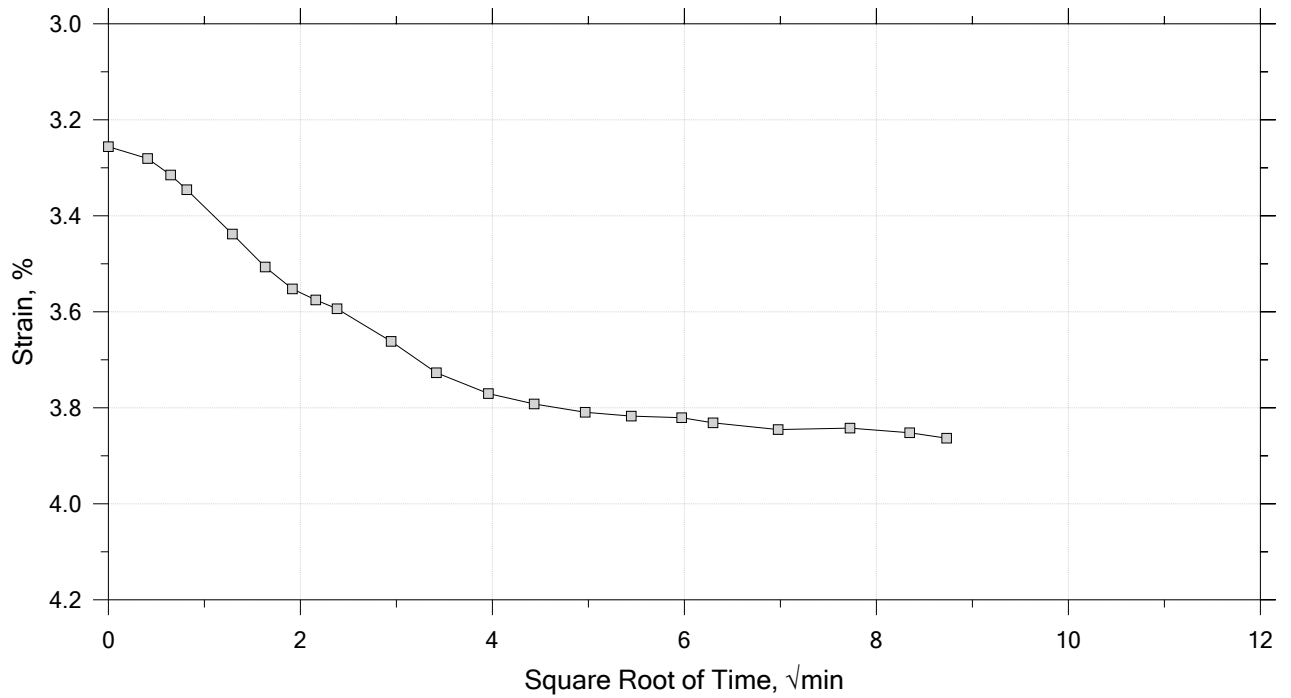
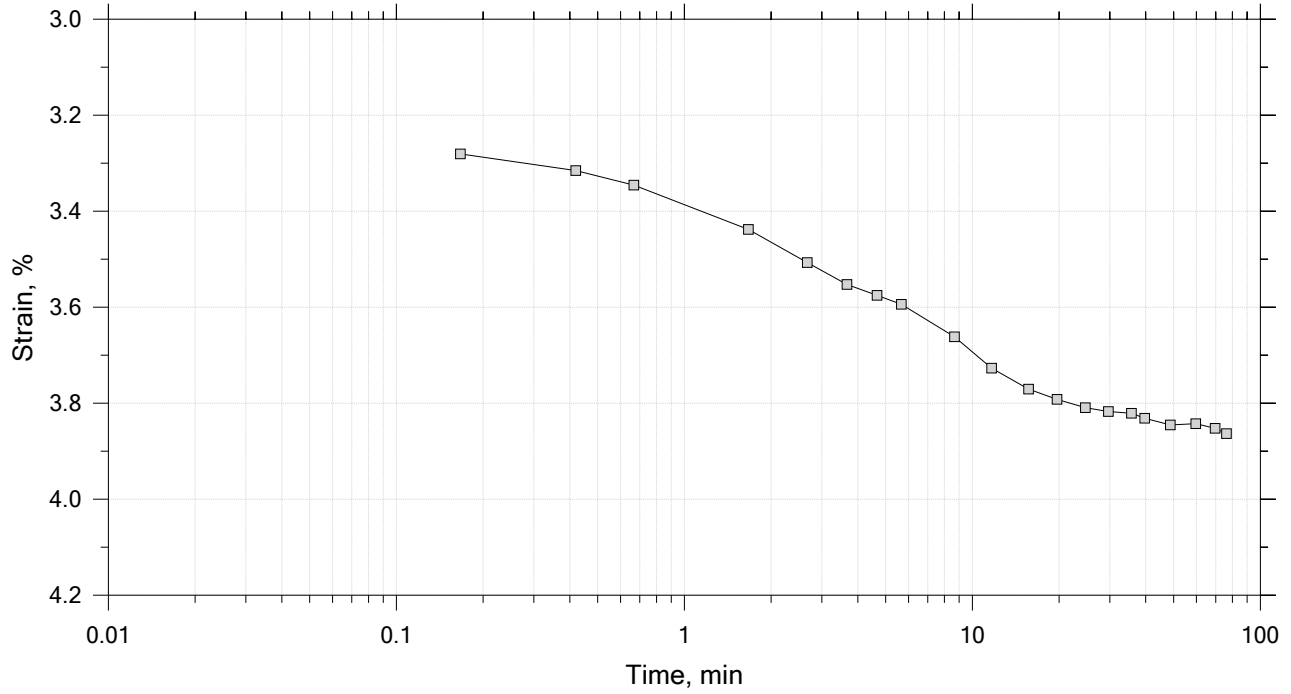
Time Curve 6 of 12  
 Constant Load Step  
 Stress: 250 psf




 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-3	Tested By: jm	Checked By: mcm
	Sample No.: 6	Test Date: 10/8/20	Depth: 10-12 ft
	Test No.: IP-5	Sample Type: intact	Elevation: ---
	Description: Moist, greenish gray clay(CH)		

# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 7 of 12  
 Constant Load Step  
 Stress: 500 psf



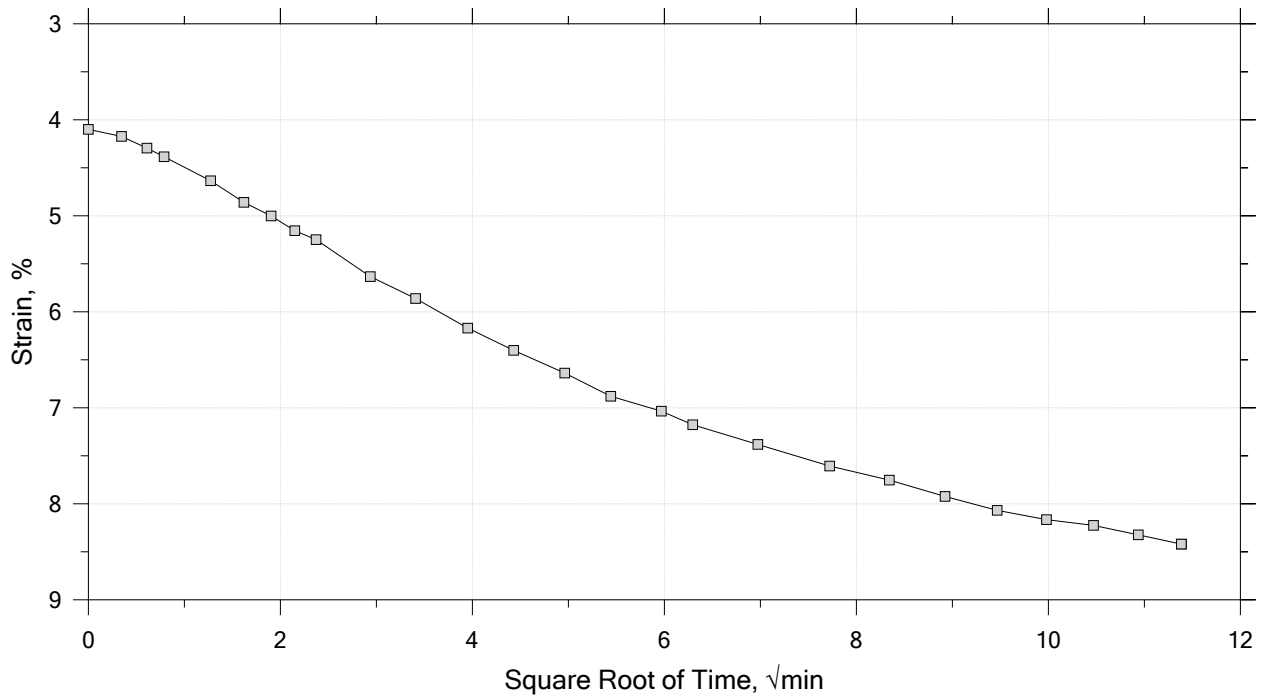
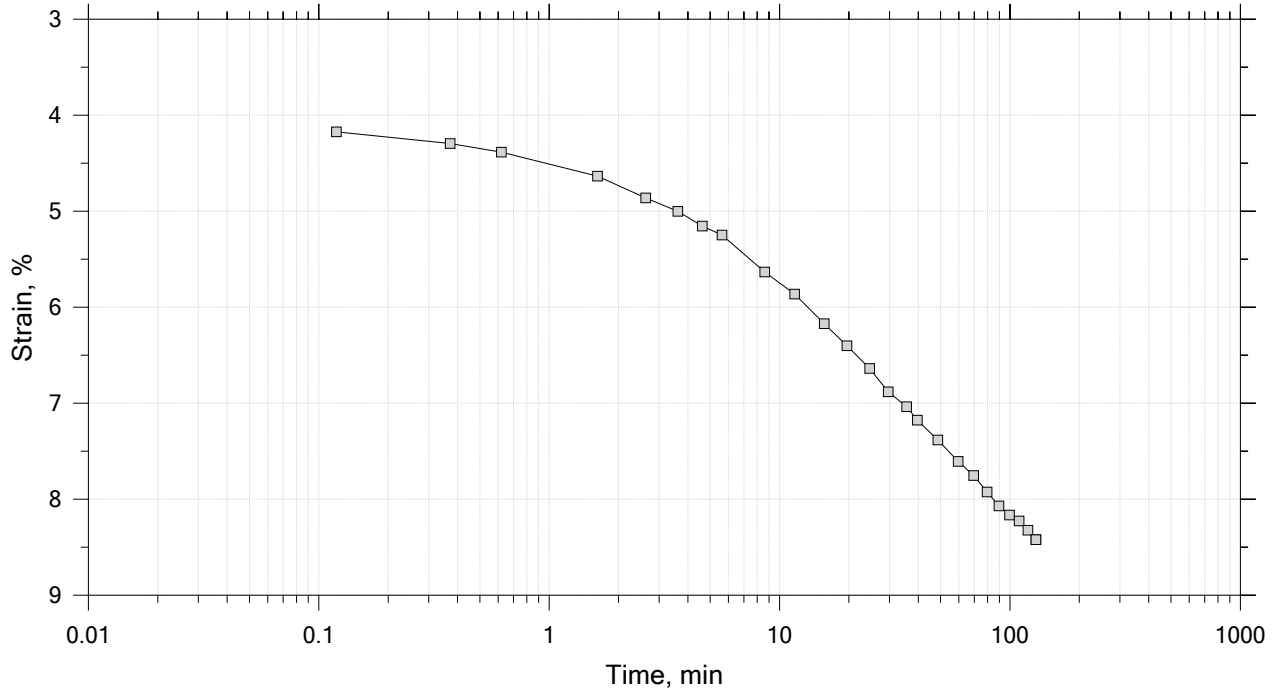
 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-3	Tested By: jm	Checked By: mcm
	Sample No.: 6	Test Date: 10/8/20	Depth: 10-12 ft
	Test No.: IP-5	Sample Type: intact	Elevation: ---
	Description: Moist, greenish gray clay(CH)		


# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 8 of 12

Constant Load Step

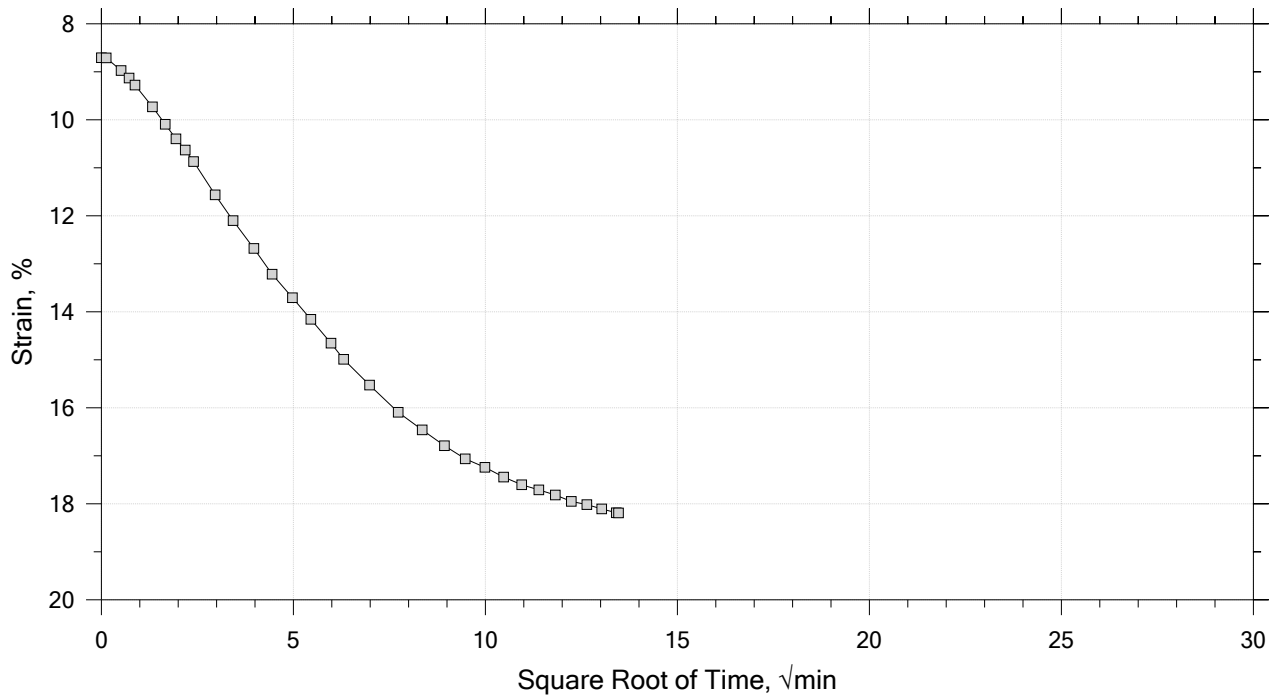
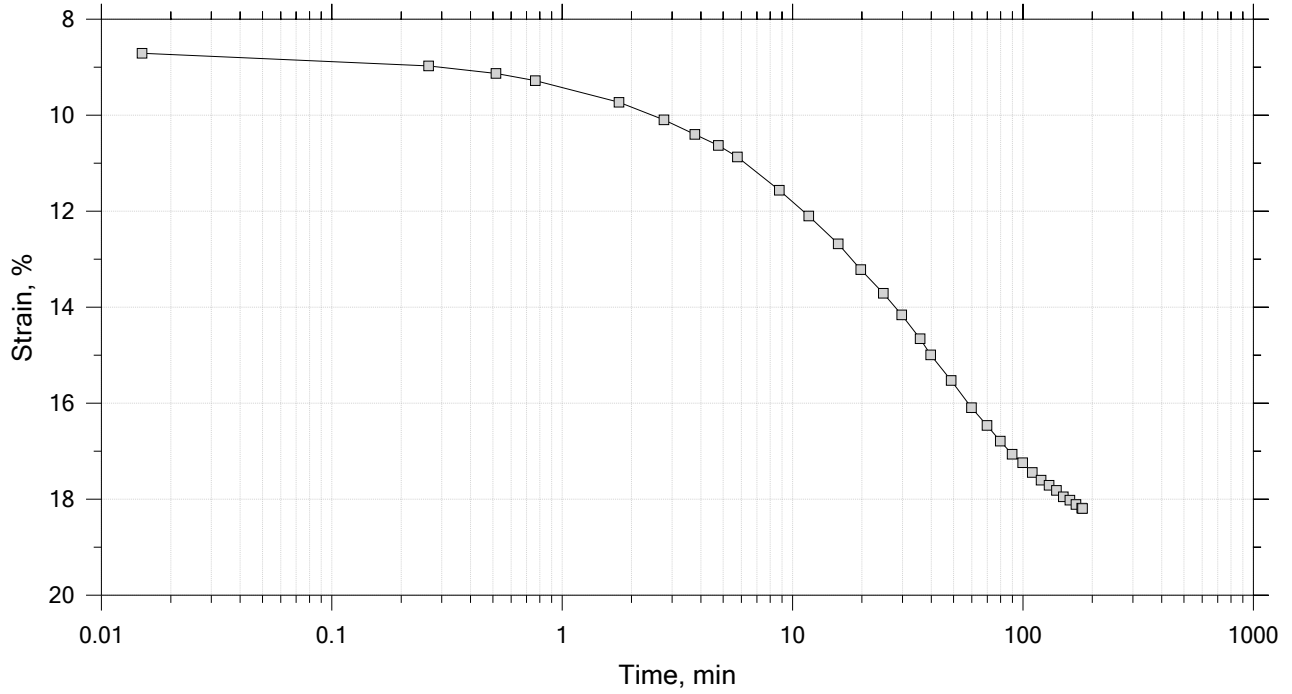
Stress: 1e+03 psf




 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-3	Tested By: jm	Checked By: mcm
	Sample No.: 6	Test Date: 10/8/20	Depth: 10-12 ft
	Test No.: IP-5	Sample Type: intact	Elevation: ---
	Description: Moist, greenish gray clay(CH)		

# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 9 of 12  
 Constant Load Step  
 Stress: 2e+03 psf



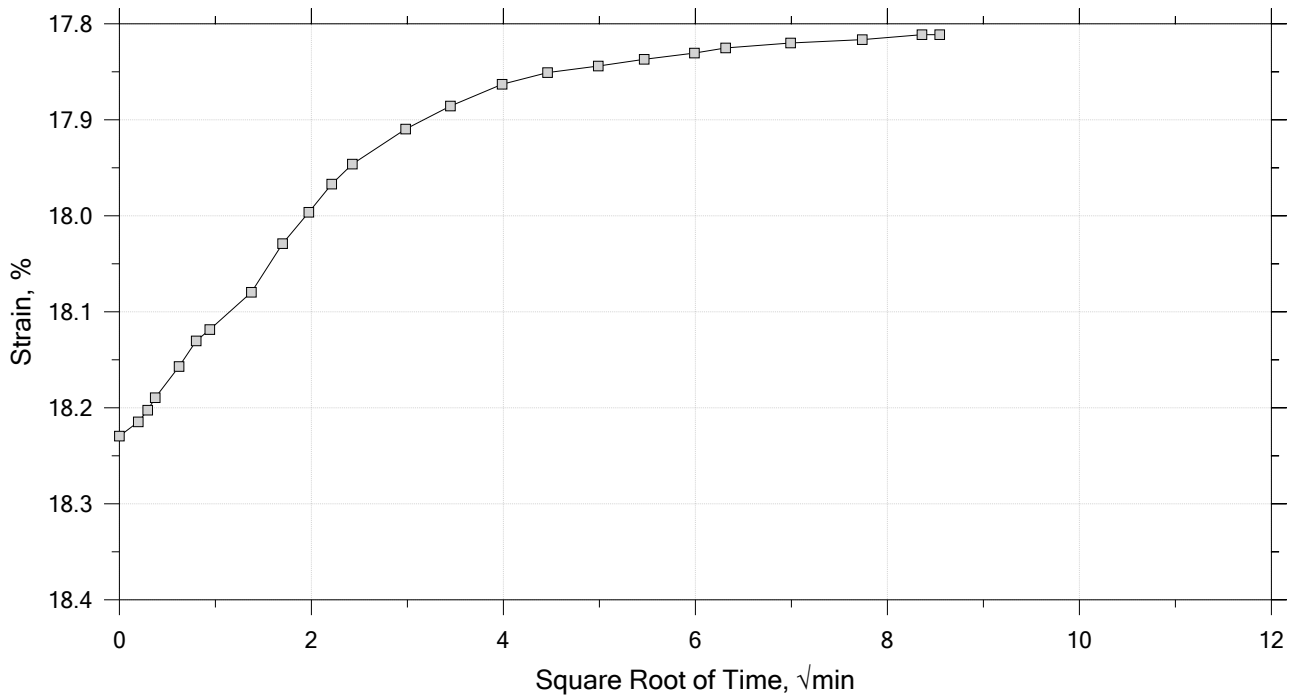
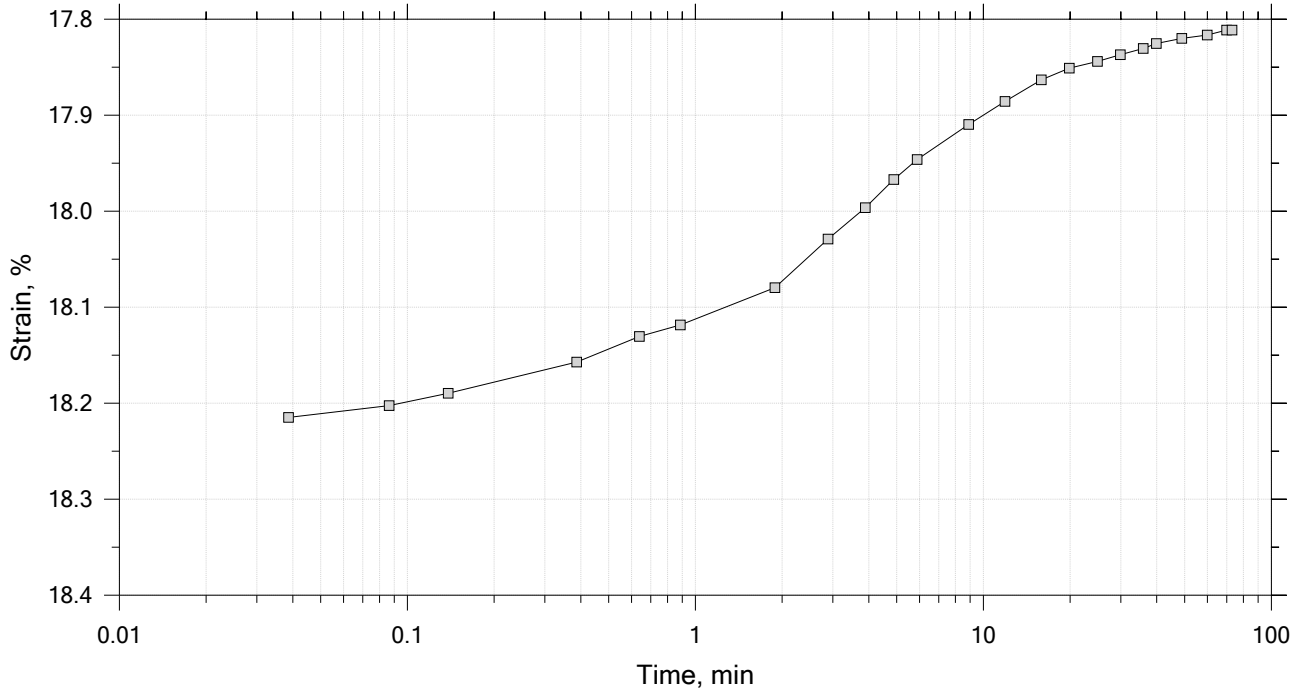
 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-3	Tested By: jm	Checked By: mcm
	Sample No.:6	Test Date: 10/8/20	Depth: 10-12 ft
	Test No.: IP-5	Sample Type: intact	Elevation: ---
	Description: Moist, greenish gray clay(CH)		


# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 10 of 12

Constant Load Step

Stress: 1e+03 psf



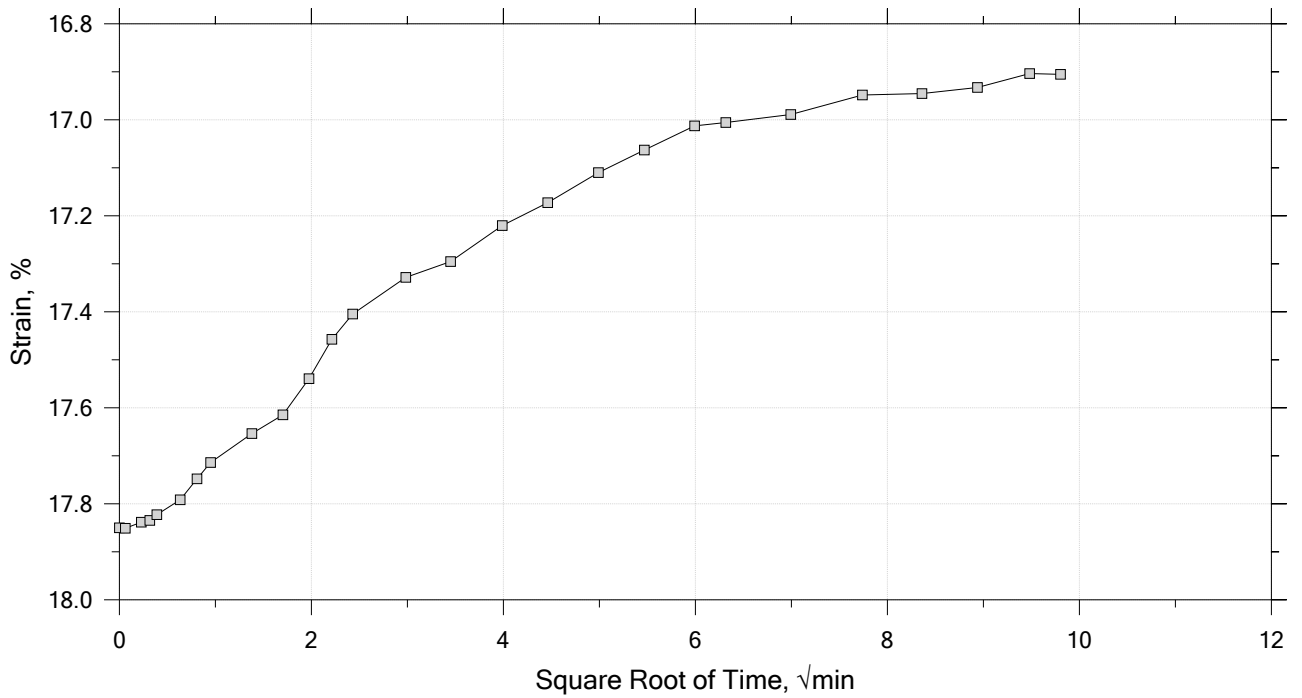
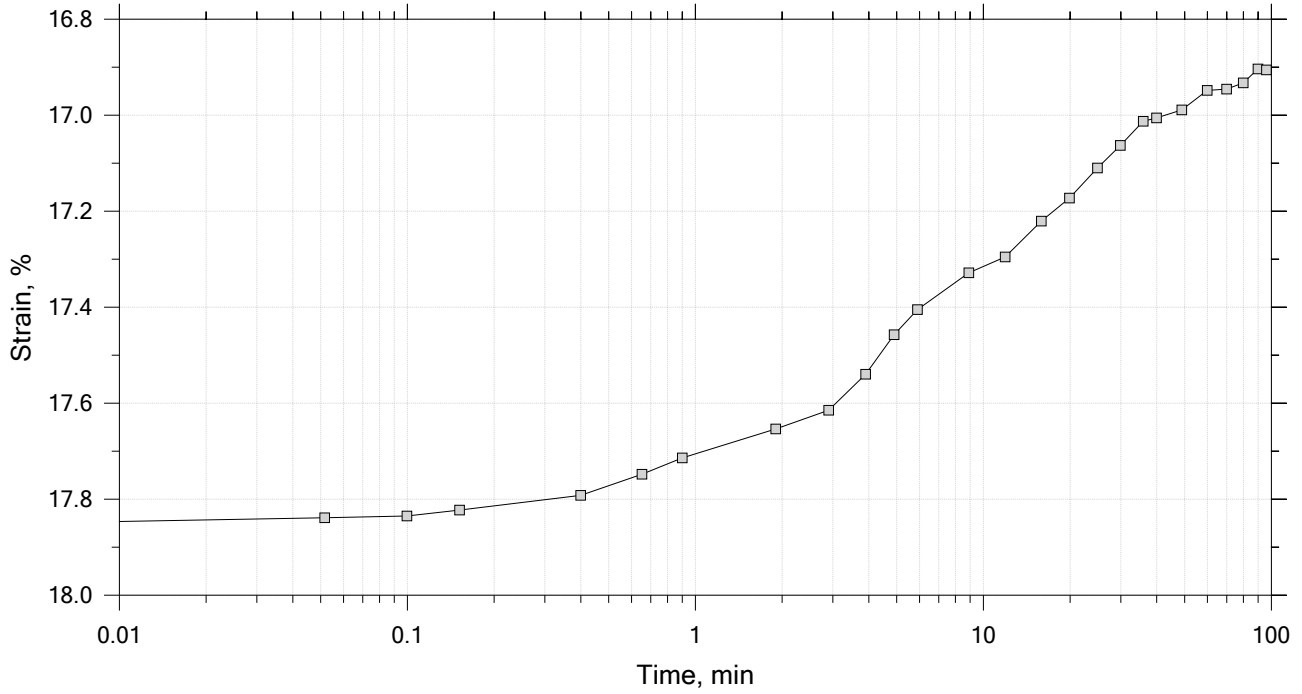
 <p>Engineering and Testing</p>	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-3	Tested By: jm	Checked By: mcm
	Sample No.: 6	Test Date: 10/8/20	Depth: 10-12 ft
	Test No.: IP-5	Sample Type: intact	Elevation: ---
	Description: Moist, greenish gray clay(CH)		


# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 11 of 12

Constant Load Step

Stress: 500 psf



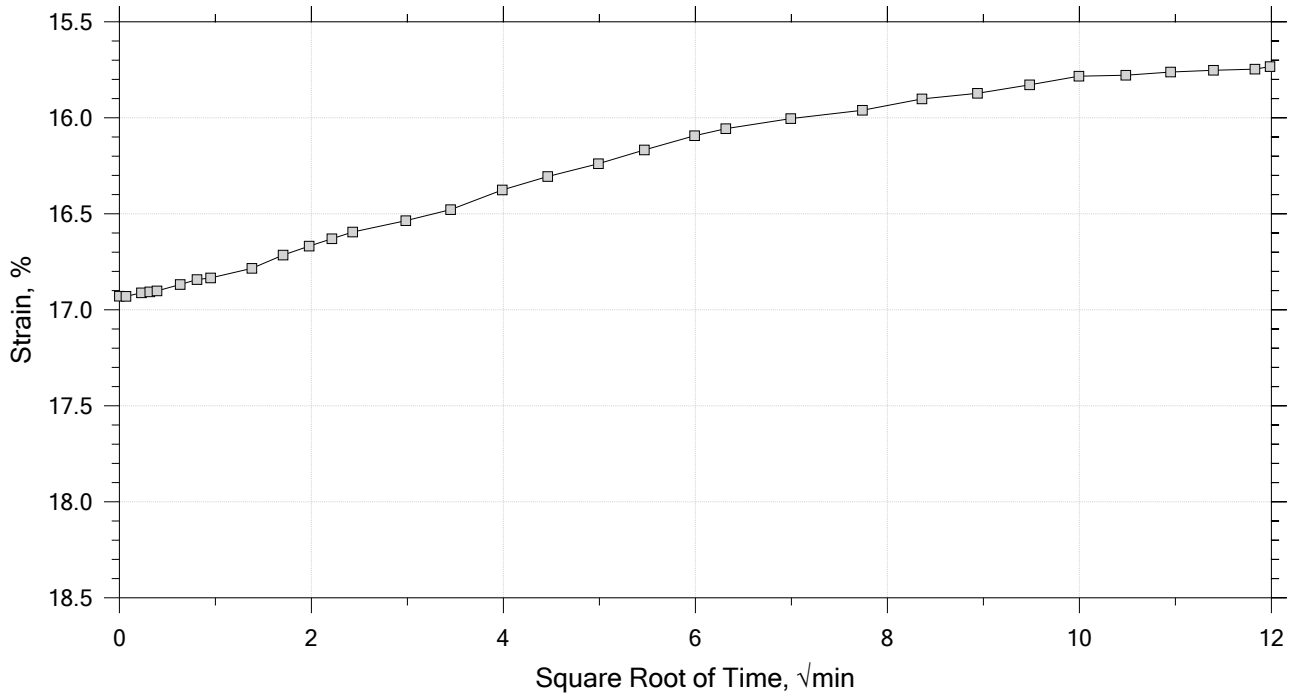
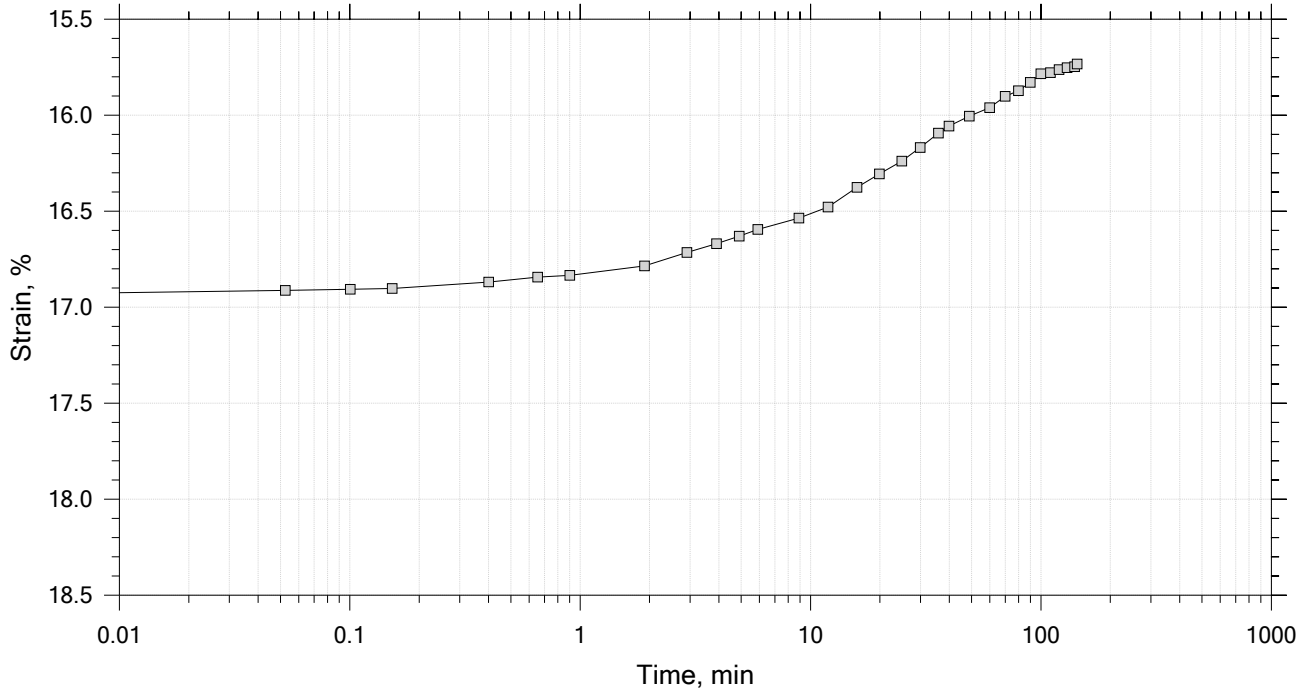
 <p>Engineering and Testing</p>	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-3	Tested By: jm	Checked By: mcm
	Sample No.: 6	Test Date: 10/8/20	Depth: 10-12 ft
	Test No.: IP-5	Sample Type: intact	Elevation: ---
	Description: Moist, greenish gray clay(CH)		


# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 12 of 12

Constant Load Step

Stress: 250 psf

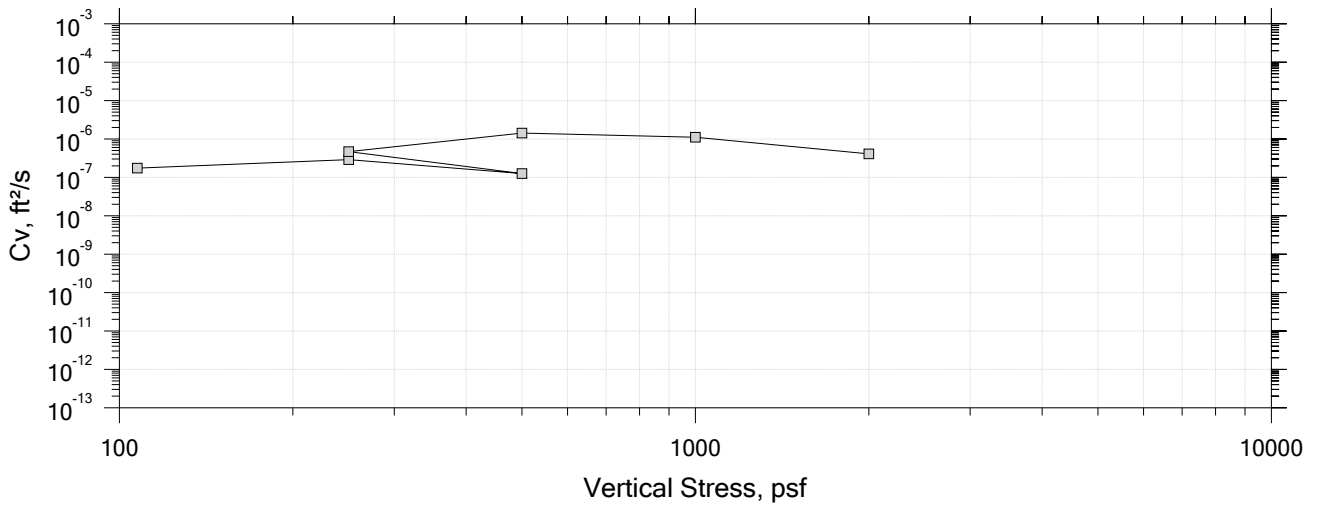
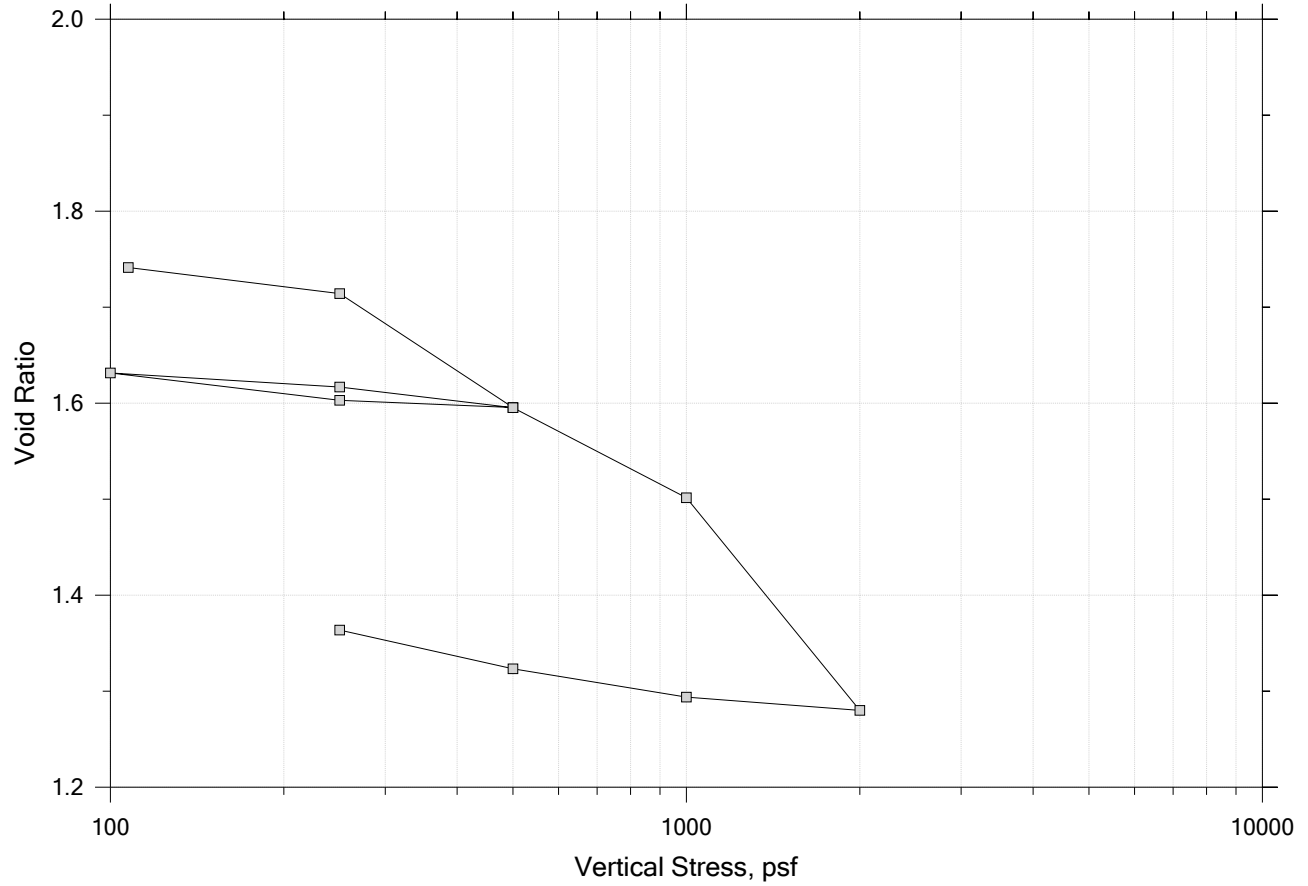



 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-3	Tested By: jm	Checked By: mcm
	Sample No.: 6	Test Date: 10/8/20	Depth: 10-12 ft
	Test No.: IP-5	Sample Type: intact	Elevation: ---
	Description: Moist, greenish gray clay(CH)		



# One-Dimensional Consolidation by ASTM D2435 - Method B

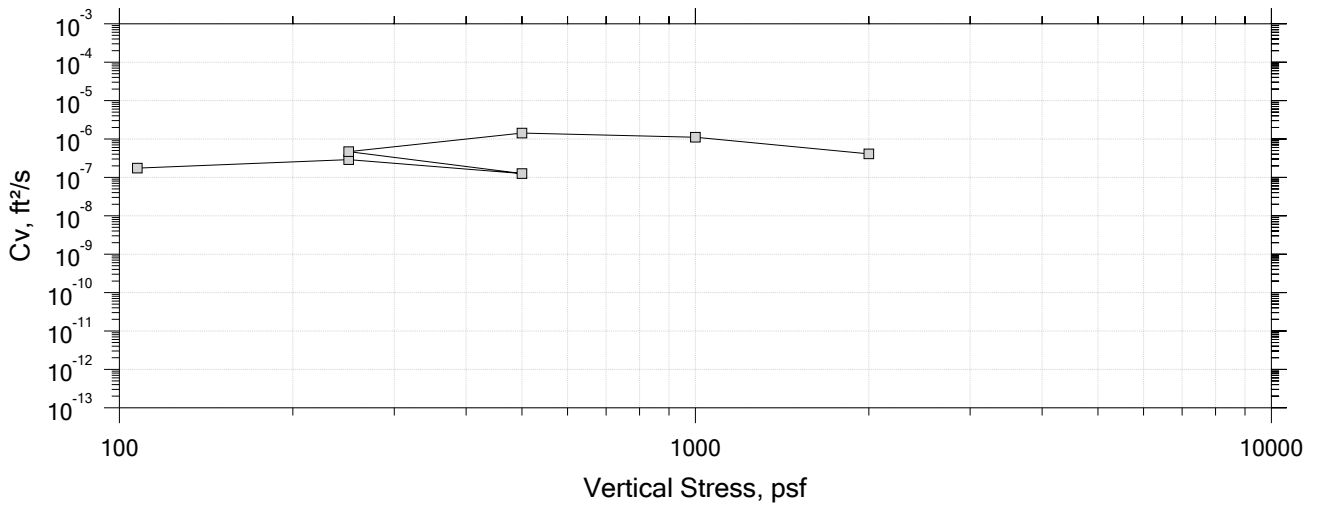
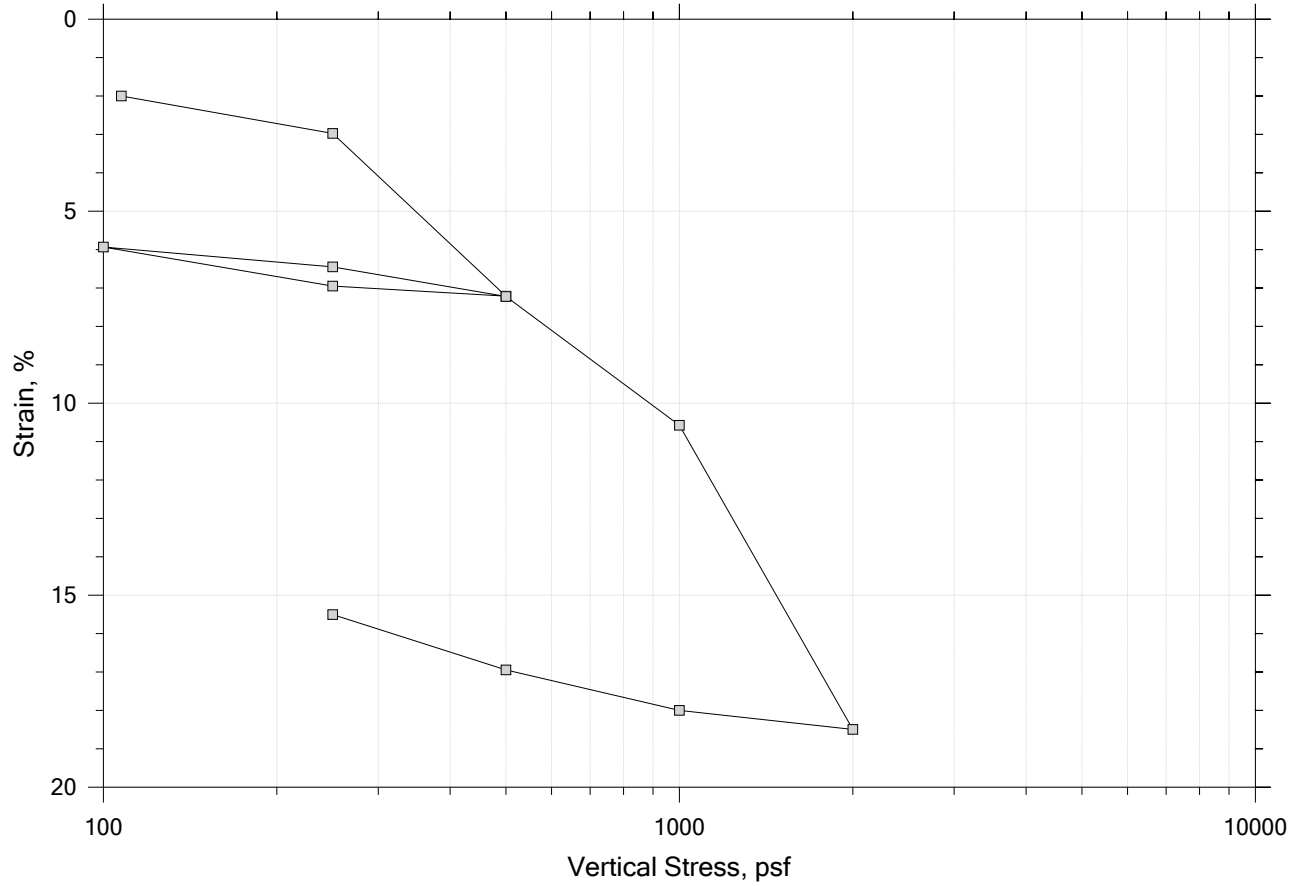
## Summary Report




 <p>APS Engineering and Testing</p>	Project: Breton Lakebridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-3	Tested By: jm	Checked By: mcm
	Sample No.: 8	Test Date: 10/10/20	Depth: 14-16 ft
	Test No.: IP-6	Sample Type: intact	Elevation: ---
	Description: Moist, greenish gray clay(CH)	Measured specific gravity: 2.58	

# One-Dimensional Consolidation by ASTM D2435 - Method B

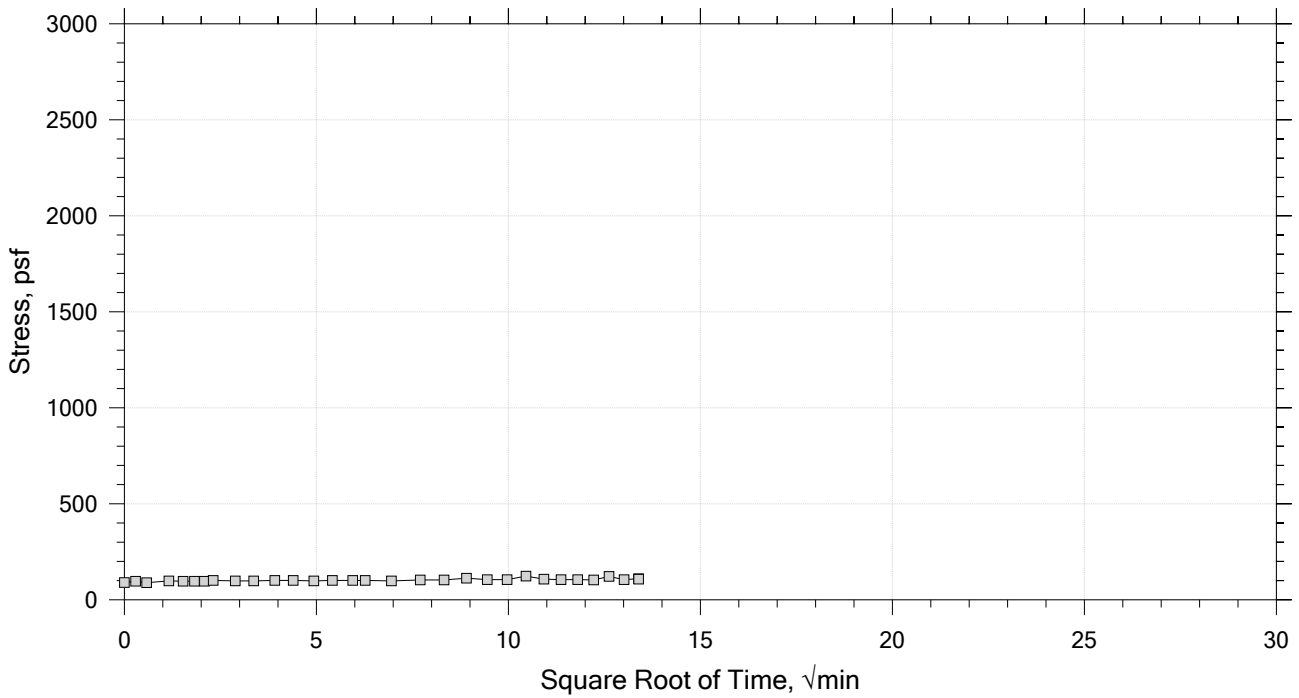
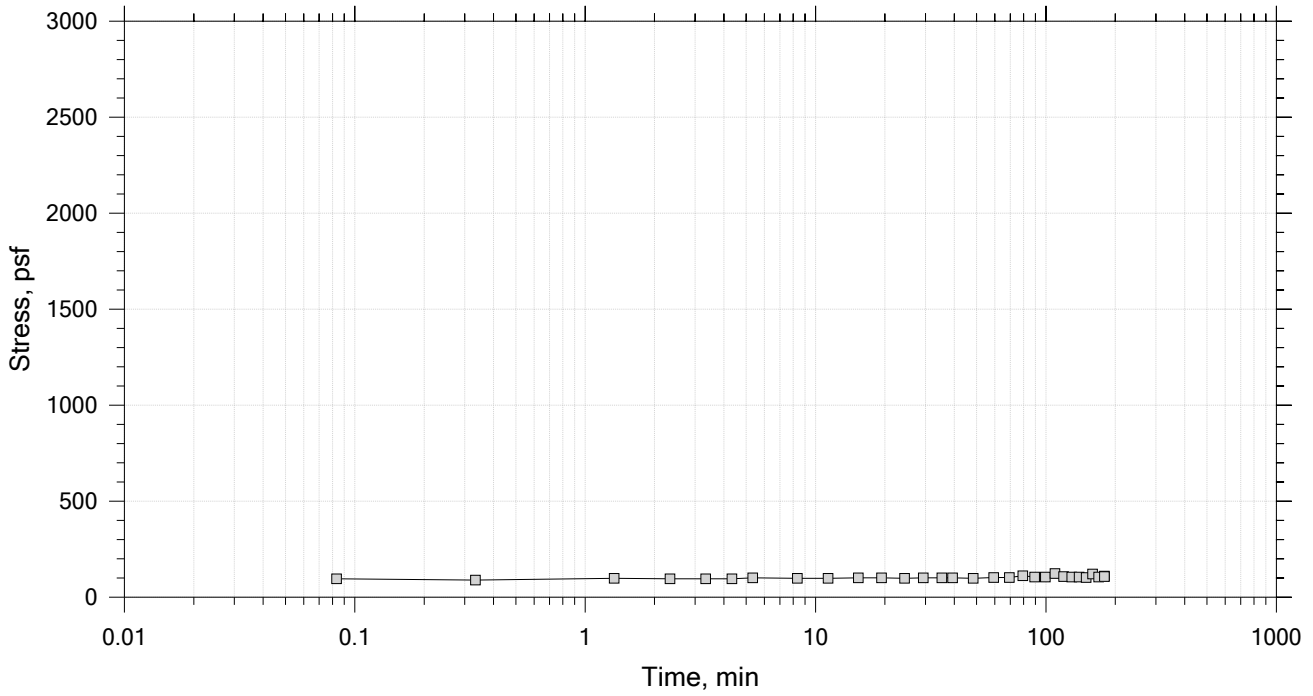
## Summary Report




 <p>APS Engineering and Testing</p>	Project: Breton Lakebridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-3	Tested By: jm	Checked By: mcm
	Sample No.: 8	Test Date: 10/10/20	Depth: 14-16 ft
	Test No.: IP-6	Sample Type: intact	Elevation: ---
	Description: Moist, greenish gray clay (CH)		

# One-Dimensional Consolidation by ASTM D2435 - Method B

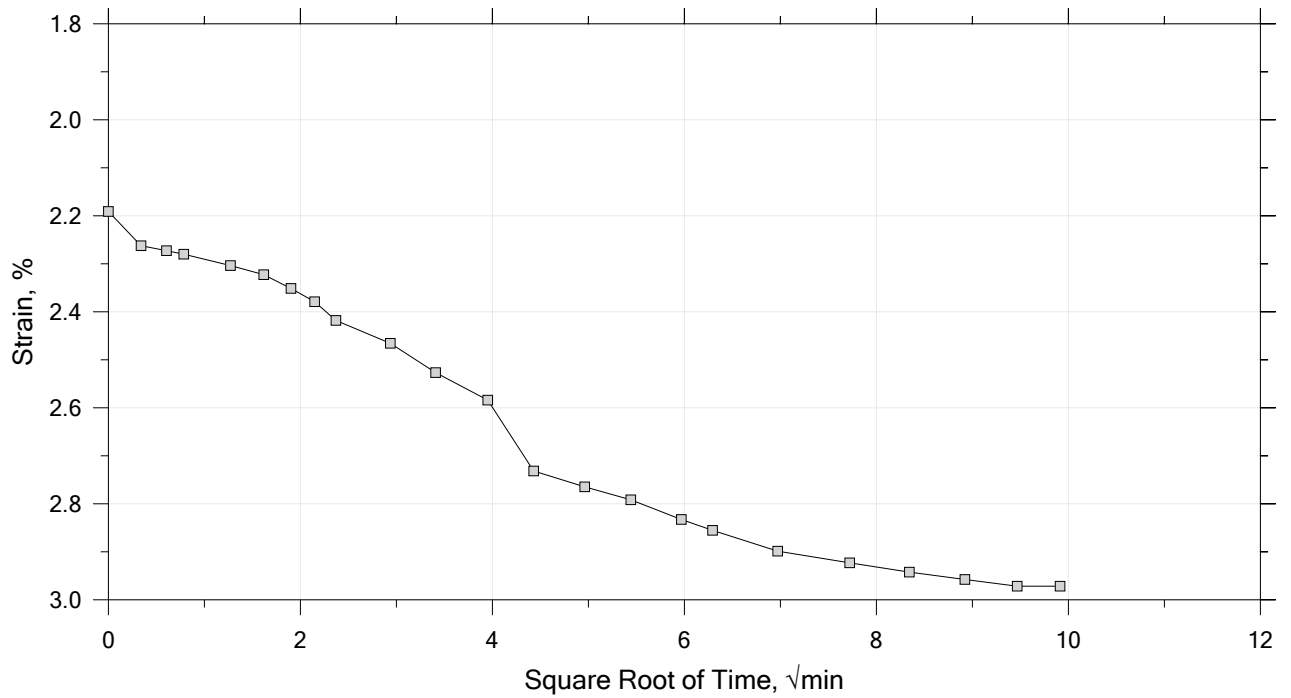
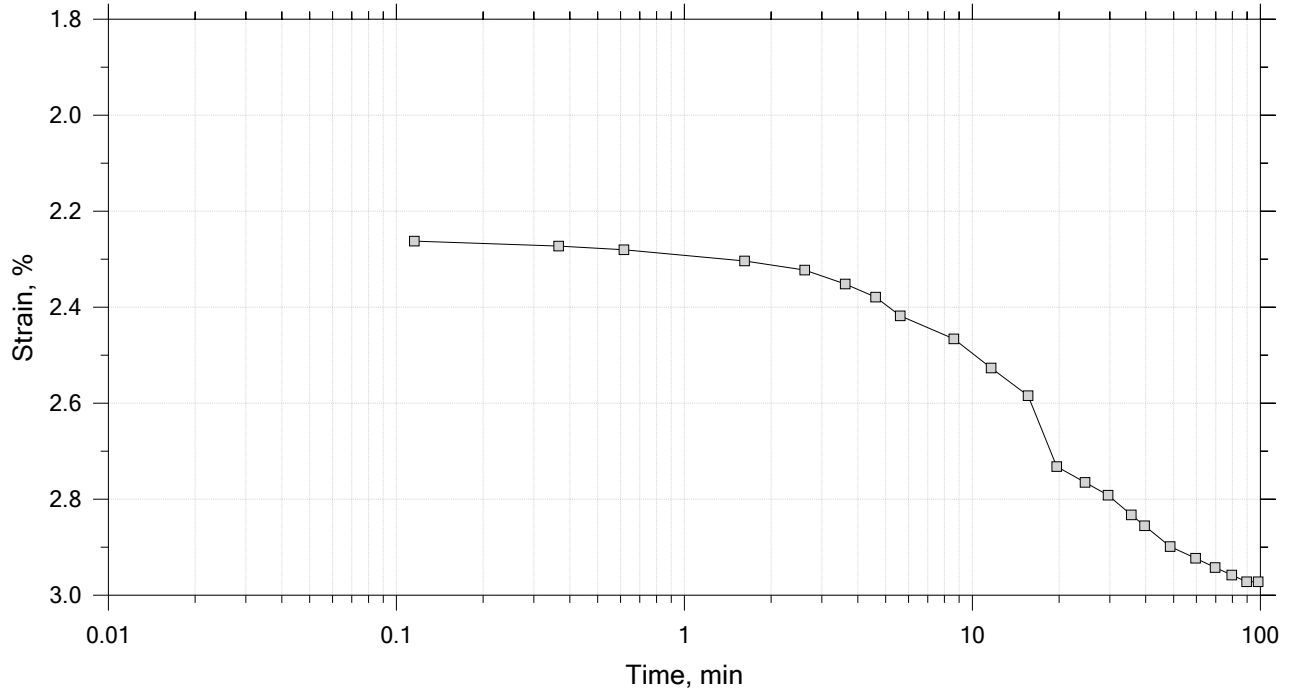
Time Curve 1 of 12  
 Constant Volume Step  
 Stress: 107 psf




 Engineering and Testing	Project: Breton Lakebridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-3	Tested By: jm	Checked By: mcm
	Sample No.: 8	Test Date: 10/10/20	Depth: 14-16 ft
	Test No.: IP-6	Sample Type: intact	Elevation: ---
	Description: Moist, greenish gray clay(CH)		

# One-Dimensional Consolidation by ASTM D2435 - Method B

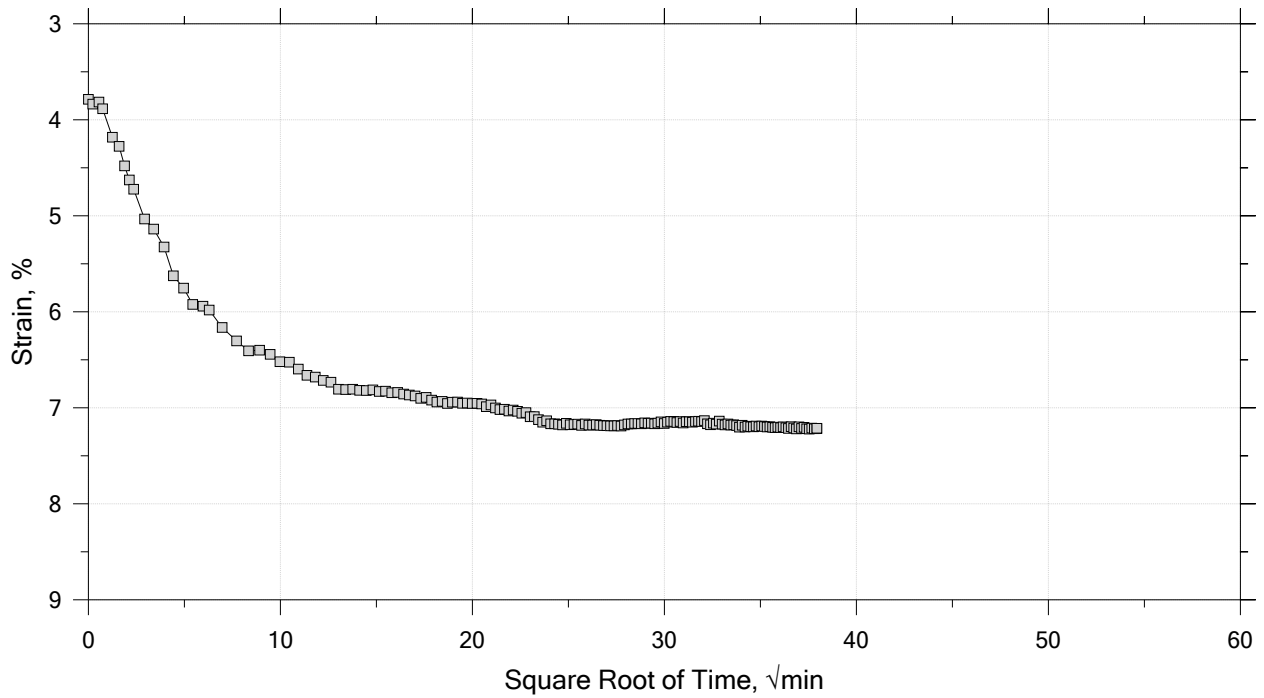
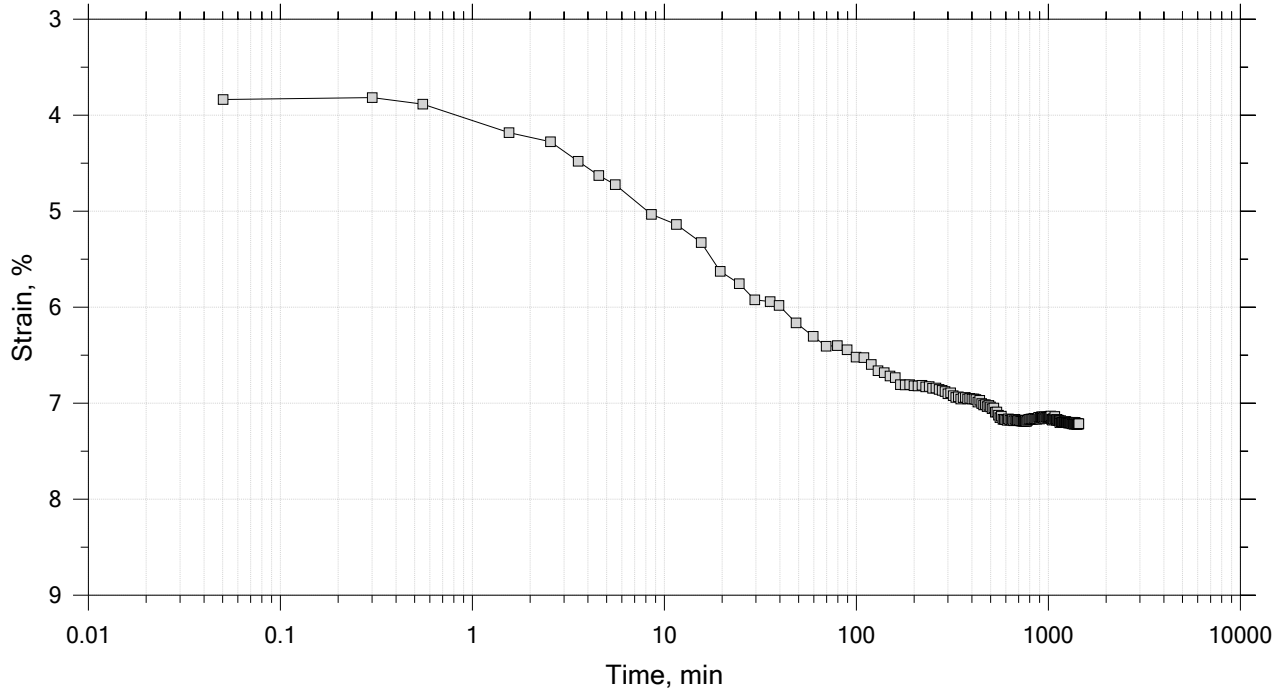
Time Curve 2 of 12  
 Constant Load Step  
 Stress: 250 psf




 Engineering and Testing	Project: Breton Lakebridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-3	Tested By: jm	Checked By: mcm
	Sample No.: 8	Test Date: 10/10/20	Depth: 14-16 ft
	Test No.: IP-6	Sample Type: intact	Elevation: ---
	Description: Moist, greenish gray clay(CH)		

# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 3 of 12  
 Constant Load Step  
 Stress: 500 psf



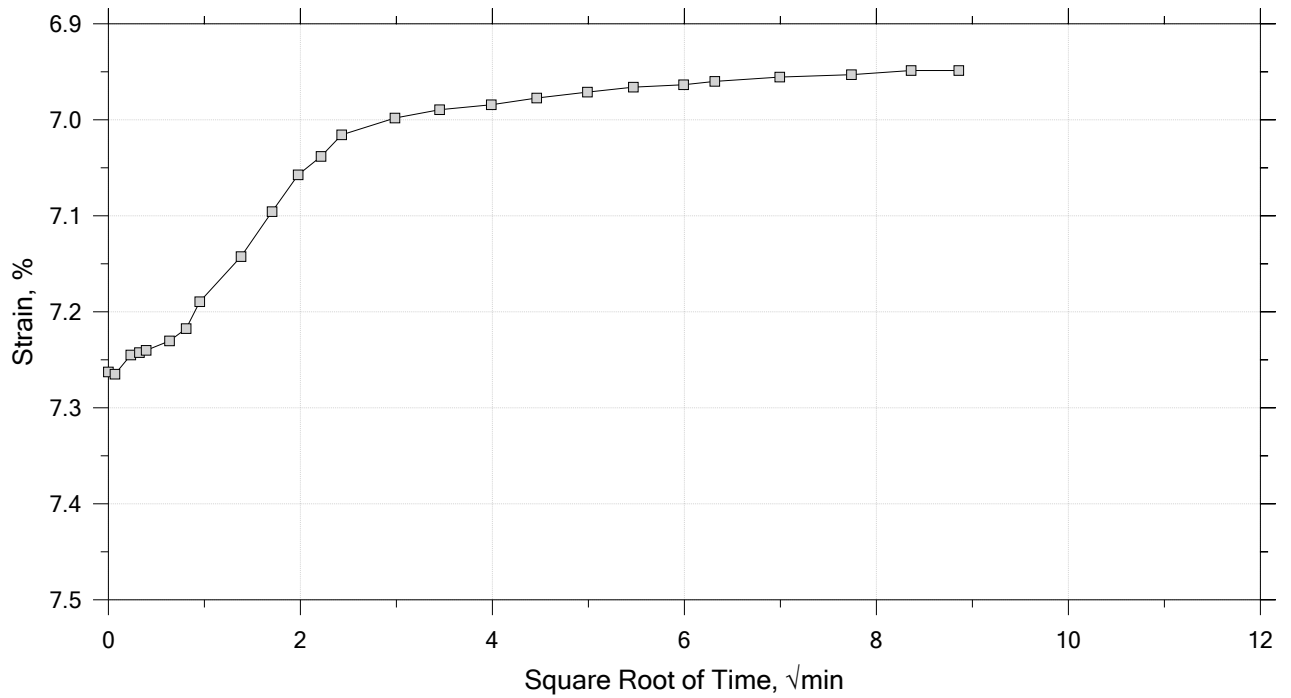
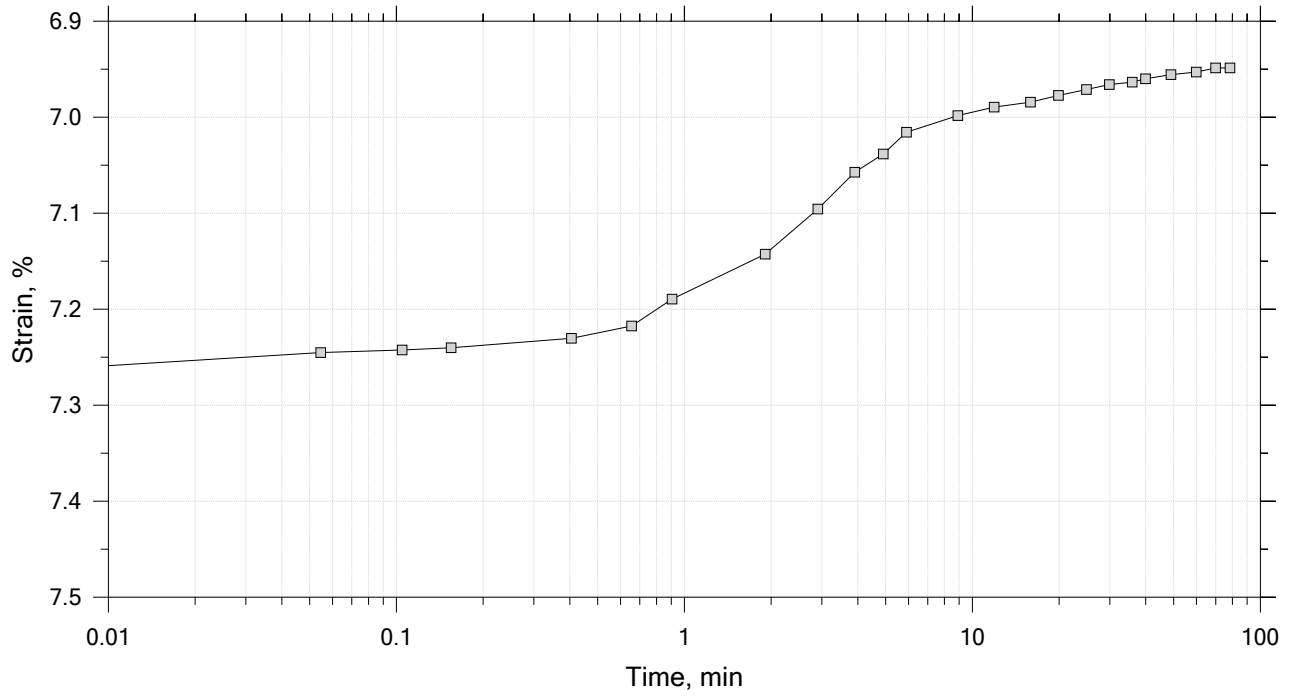
 Engineering and Testing	Project: Breton Lakebridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-3	Tested By: jm	Checked By: mcm
	Sample No.: 8	Test Date: 10/10/20	Depth: 14-16 ft
	Test No.: IP-6	Sample Type: intact	Elevation: ---
	Description: Moist, greenish gray clay(CH)		


# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 4 of 12

Constant Load Step

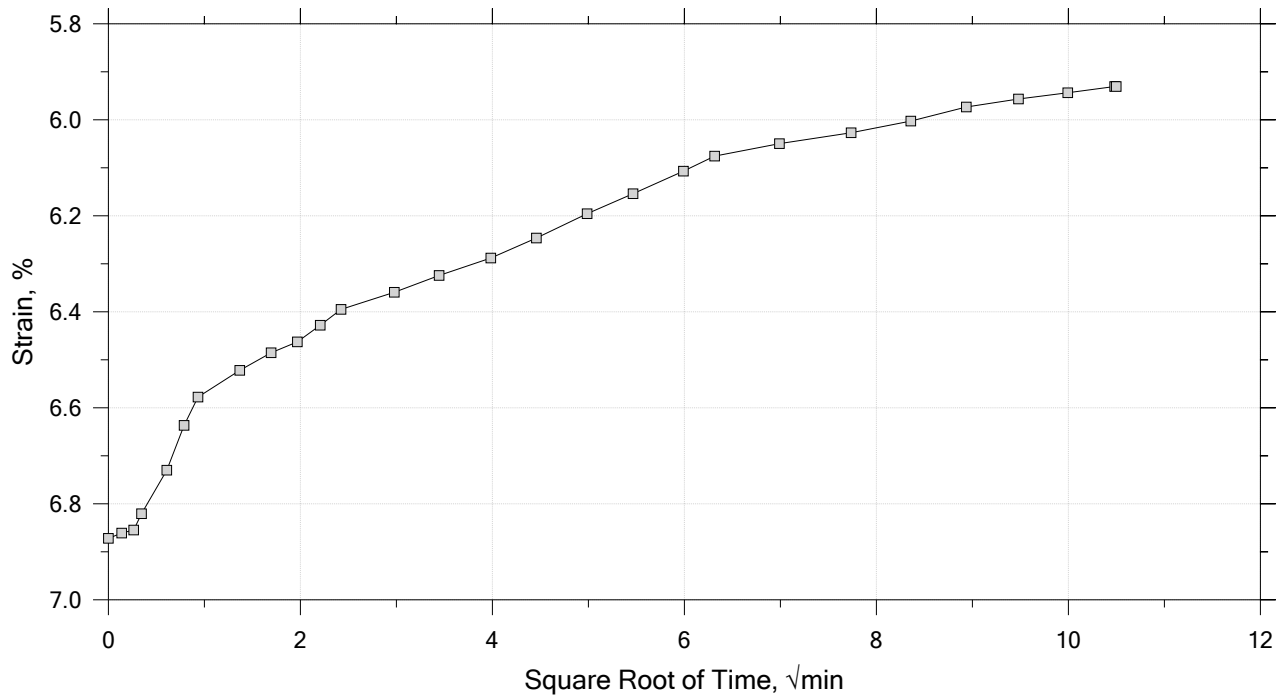
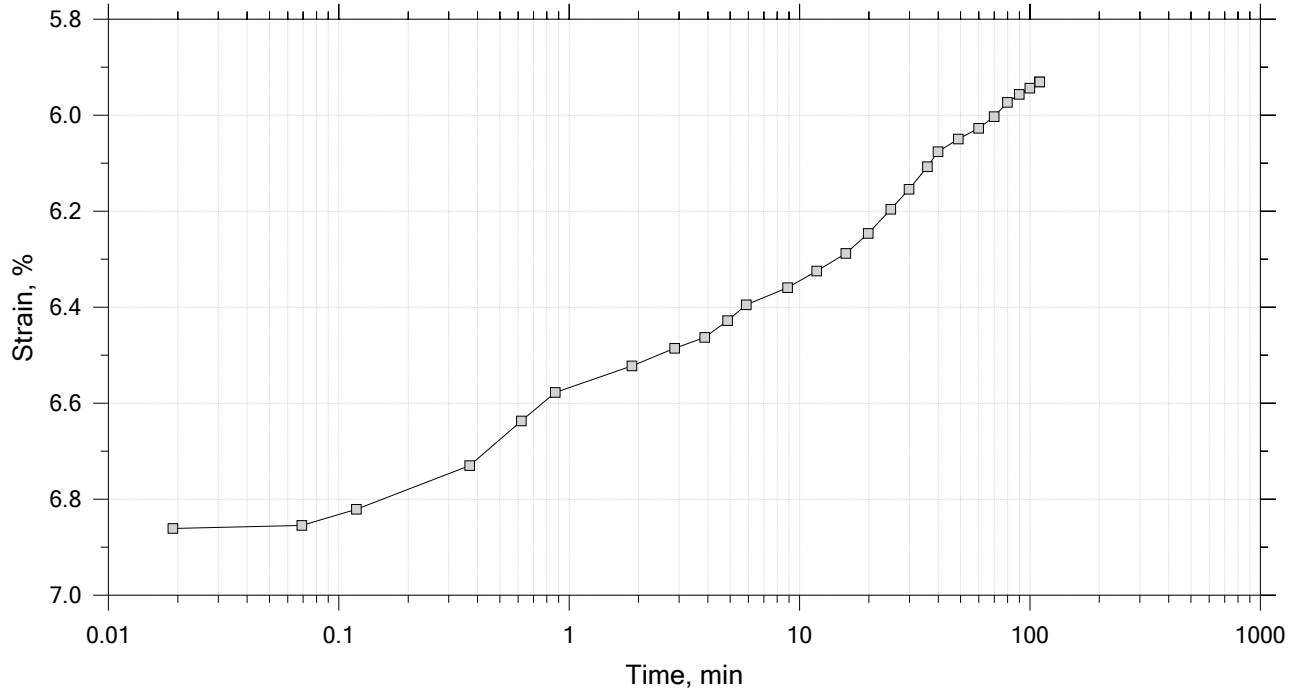
Stress: 250 psf




 <p>Engineering and Testing</p>	Project: Breton Lakebridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-3	Tested By: jm	Checked By: mcm
	Sample No.: 8	Test Date: 10/10/20	Depth: 14-16 ft
	Test No.: IP-6	Sample Type: intact	Elevation: ---
	Description: Moist, greenish gray clay(CH)		

# One-Dimensional Consolidation by ASTM D2435 - Method B

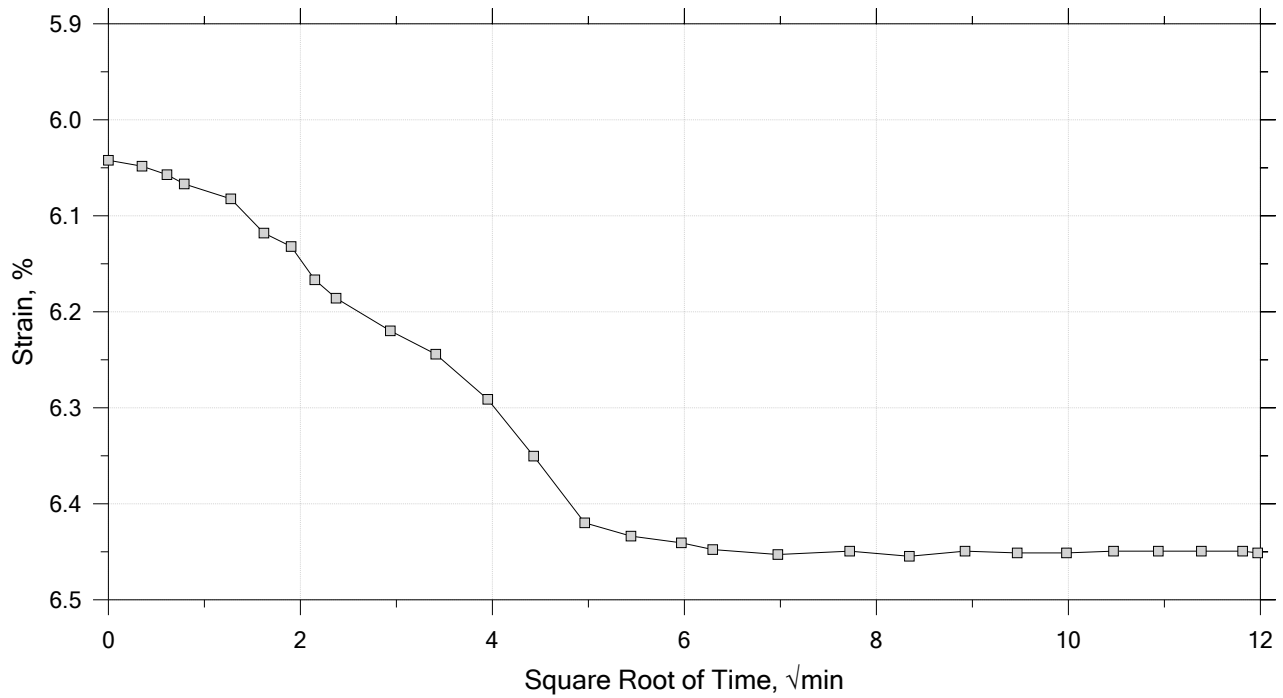
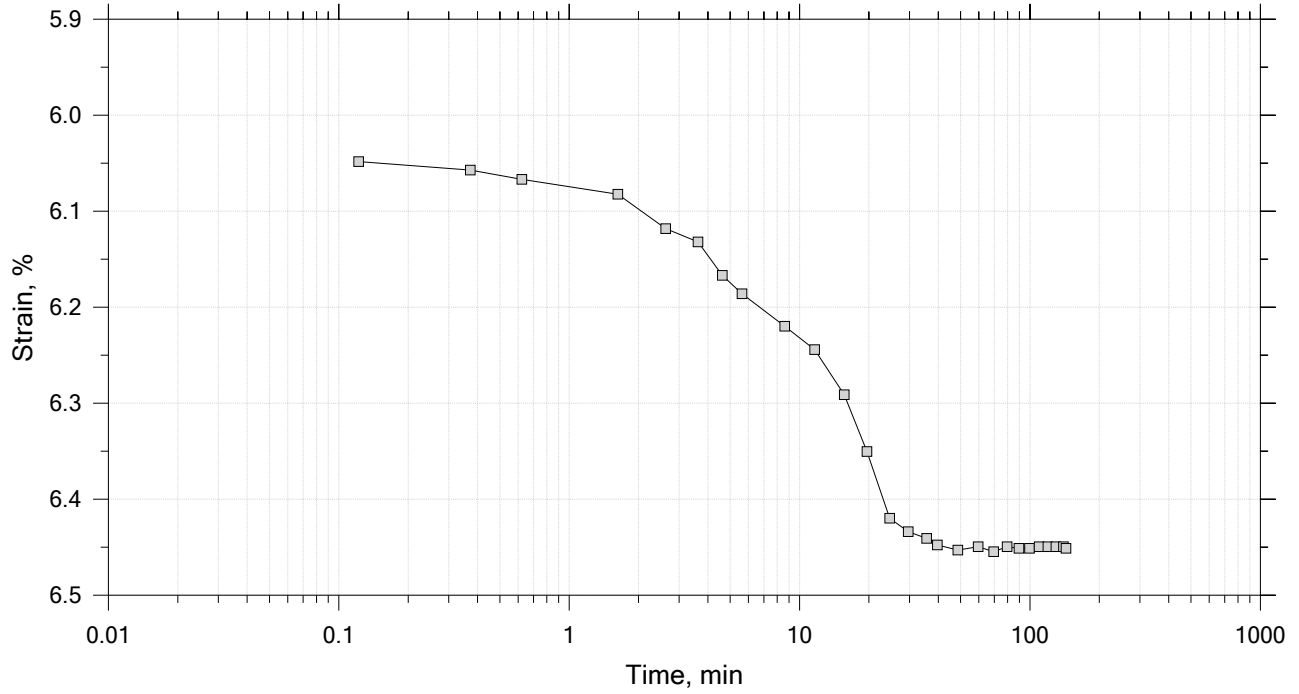
Time Curve 5 of 12  
 Constant Load Step  
 Stress: 100 psf




 Engineering and Testing	Project: Breton Lakebridge Project	Location: see map	Project No.: GTX-312518
	Boring No.: B-3	Tested By: jm	Checked By: mcm
	Sample No.: 8	Test Date: 10/10/20	Depth: 14-16 ft
	Test No.: IP-6	Sample Type: intact	Elevation: ---
	Description: Moist, greenish gray clay(CH)		

# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 6 of 12  
 Constant Load Step  
 Stress: 250 psf

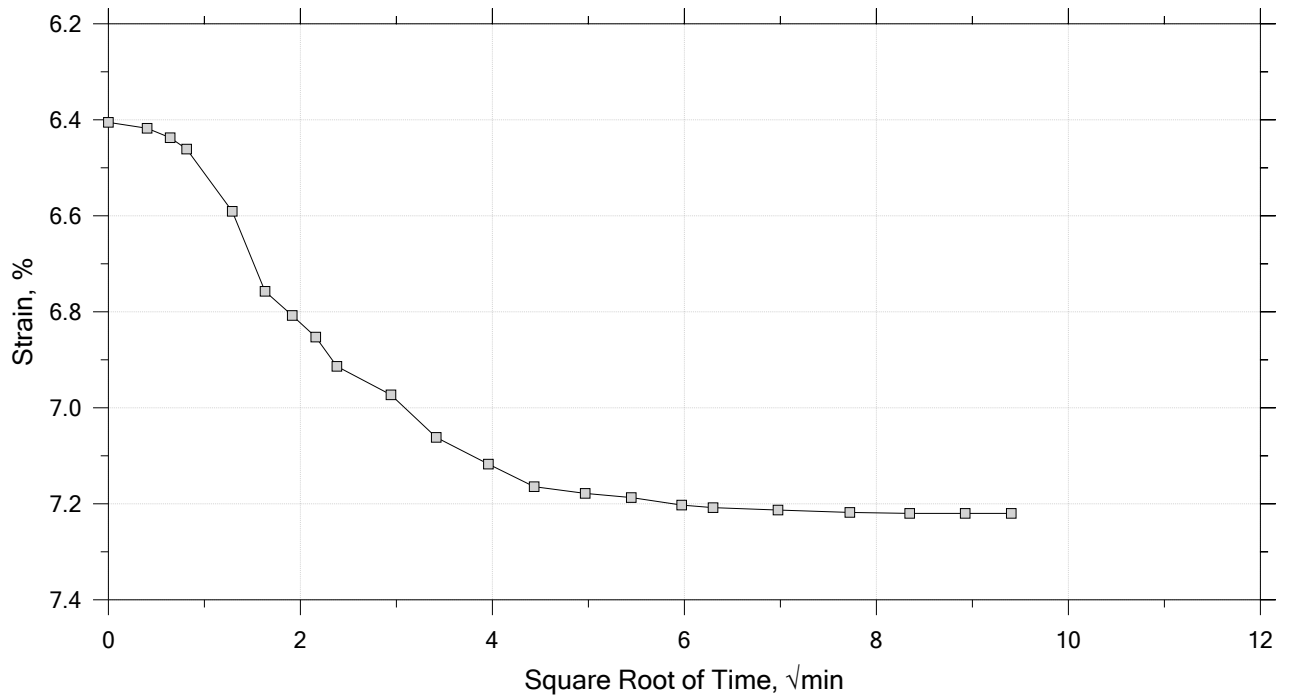
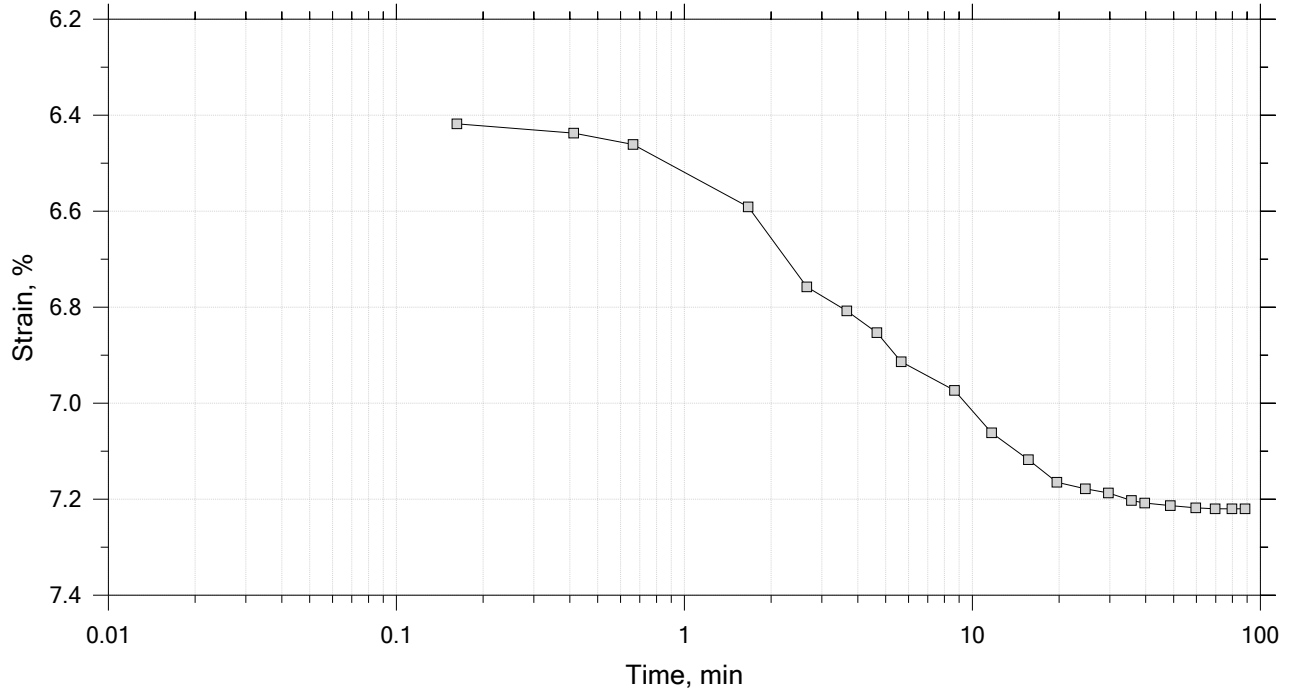



	Project: Breton Lakebridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-3	Tested By: jm	Checked By: mcm
	Sample No.: 8	Test Date: 10/10/20	Depth: 14-16 ft
	Test No.: IP-6	Sample Type: intact	Elevation: ---
	Description: Moist, greenish gray clay(CH)		



# One-Dimensional Consolidation by ASTM D2435 - Method B

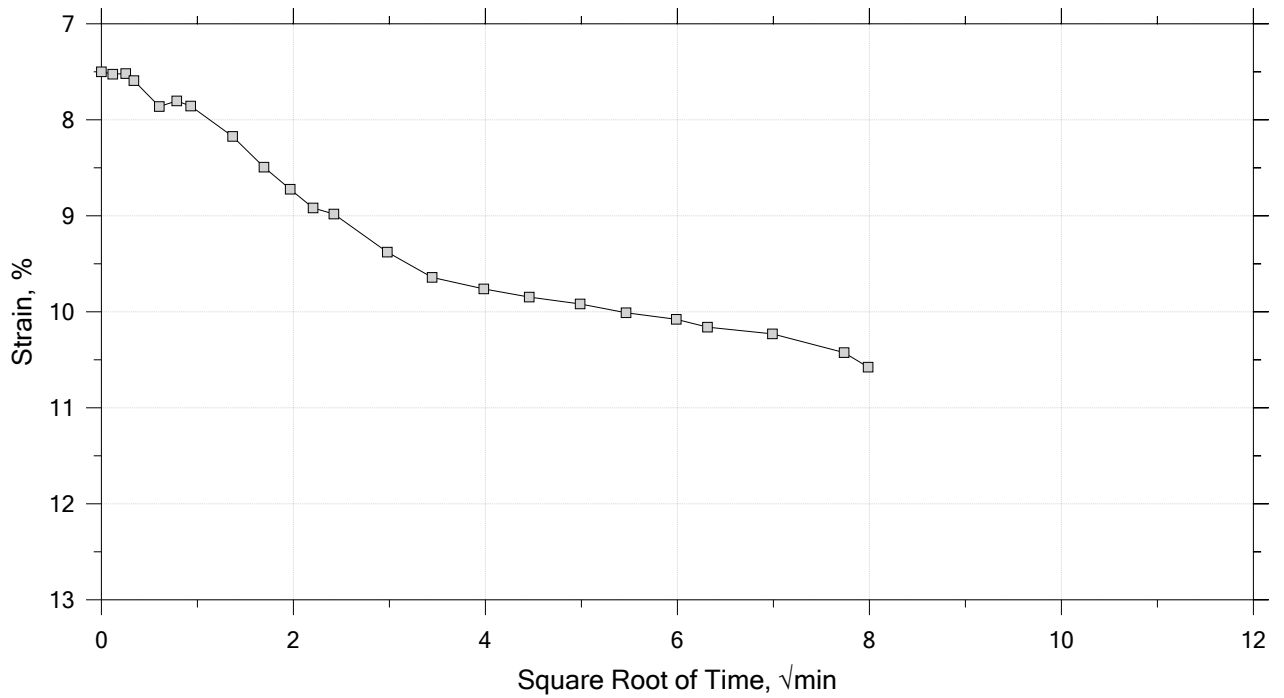
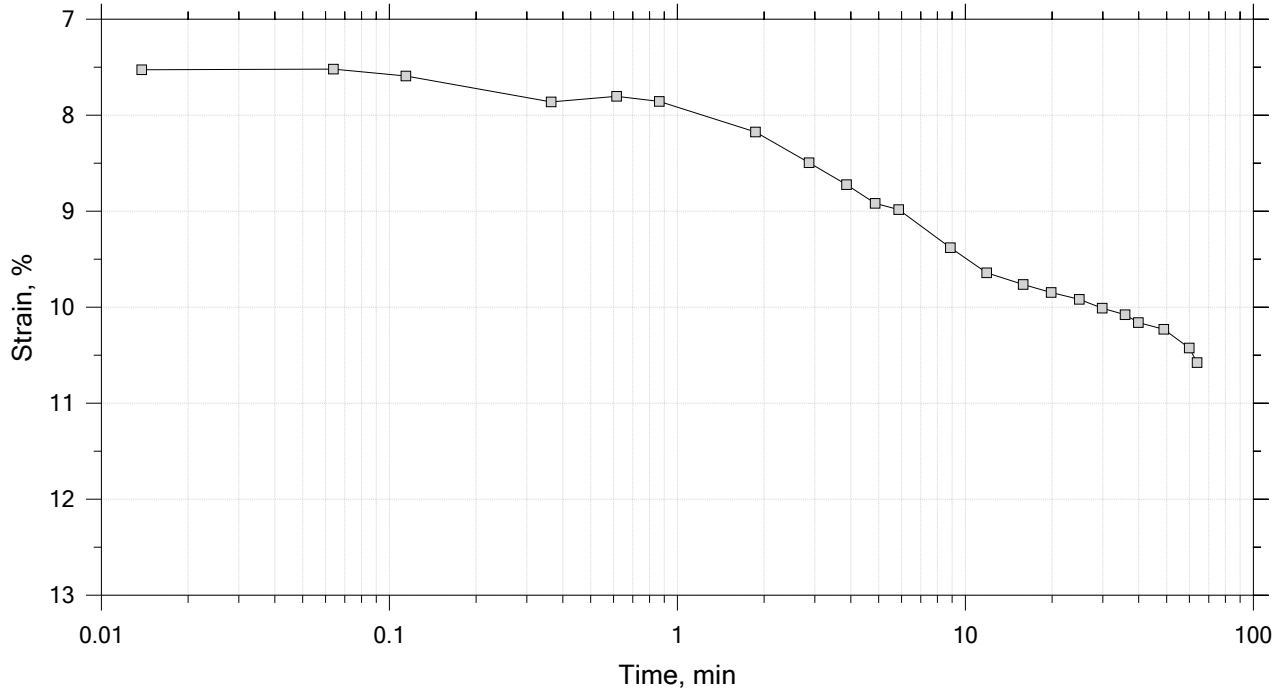
Time Curve 7 of 12  
 Constant Load Step  
 Stress: 500 psf




 Engineering and Testing	Project: Breton Lakebridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-3	Tested By: jm	Checked By: mcm
	Sample No.: 8	Test Date: 10/10/20	Depth: 14-16 ft
	Test No.: IP-6	Sample Type: intact	Elevation: ---
	Description: Moist, greenish gray clay(CH)		

# One-Dimensional Consolidation by ASTM D2435 - Method B

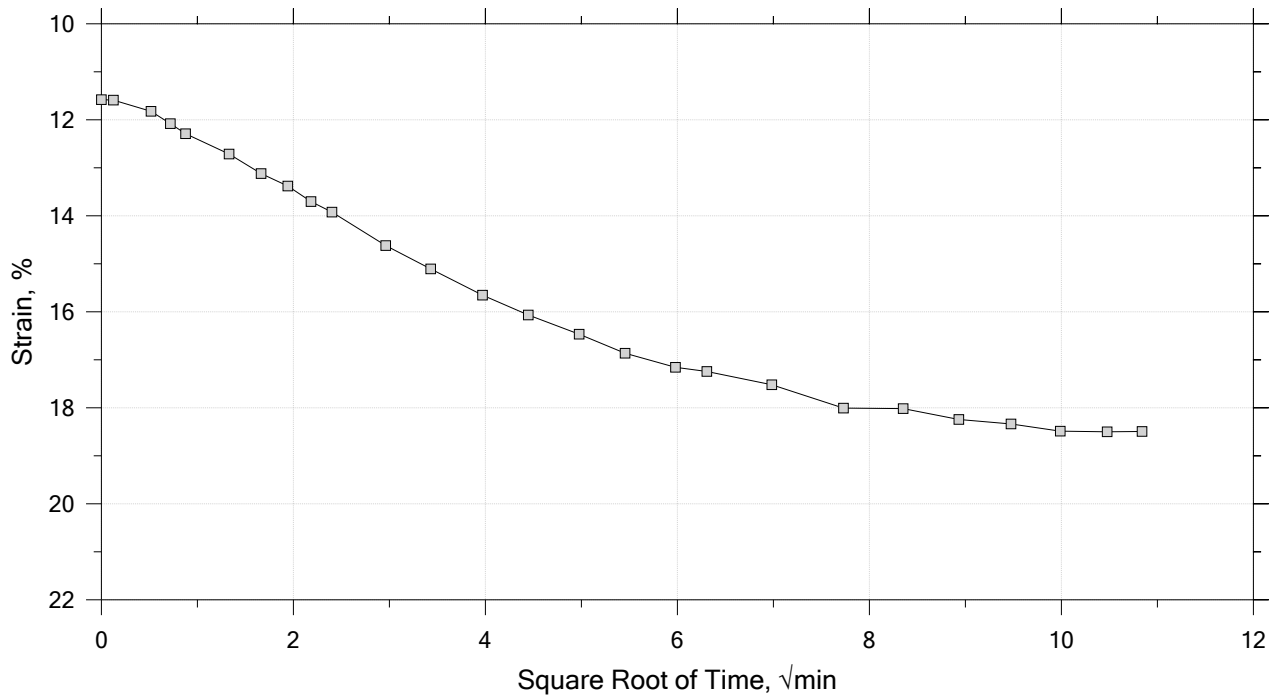
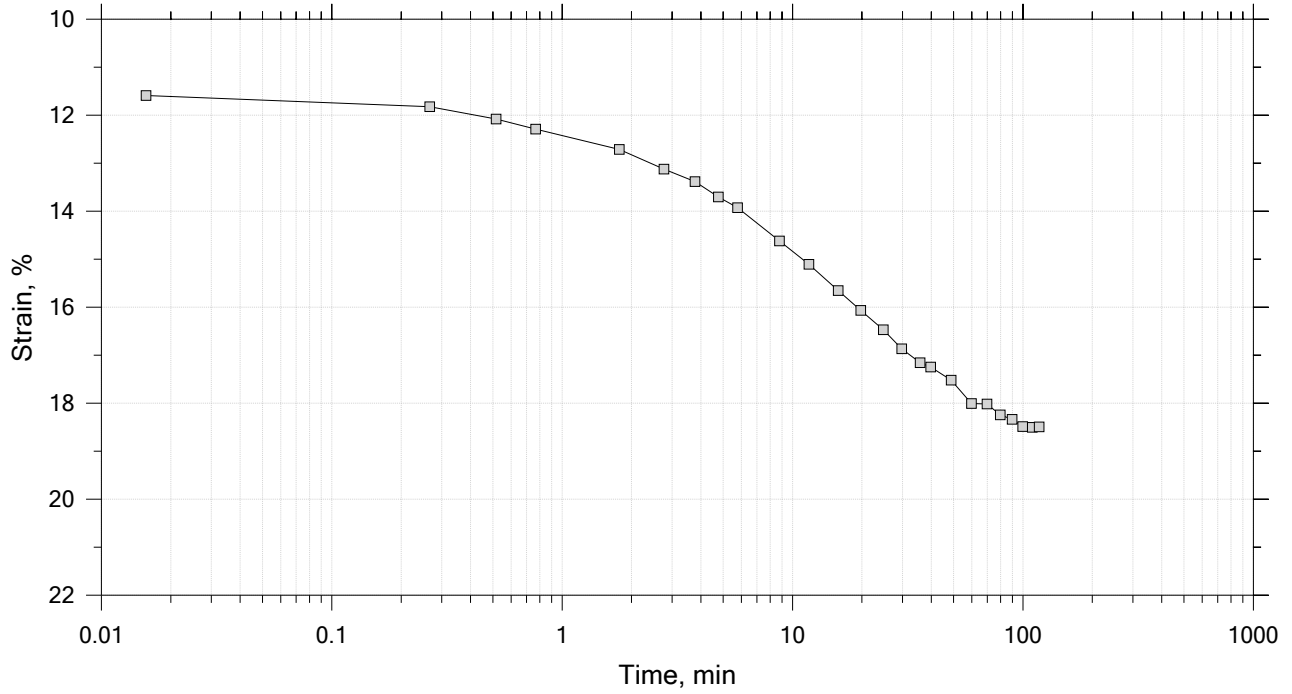
Time Curve 8 of 12  
 Constant Load Step  
 Stress: 1e+03 psf




 Engineering and Testing	Project: Breton Lakebridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-3	Tested By: jm	Checked By: mcm
	Sample No.:8	Test Date: 10/10/20	Depth: 14-16 ft
	Test No.: IP-6	Sample Type: intact	Elevation: ---
	Description: Moist, greenish gray clay(CH)		

# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 9 of 12  
 Constant Load Step  
 Stress: 2e+03 psf



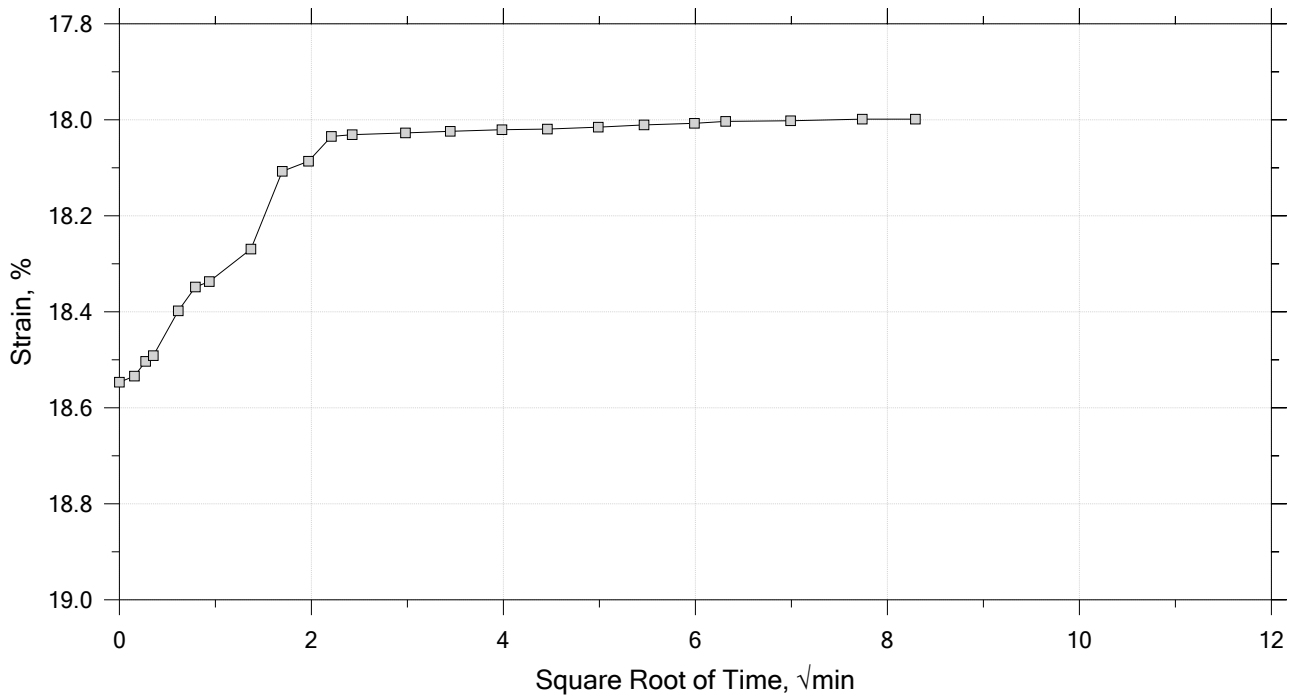
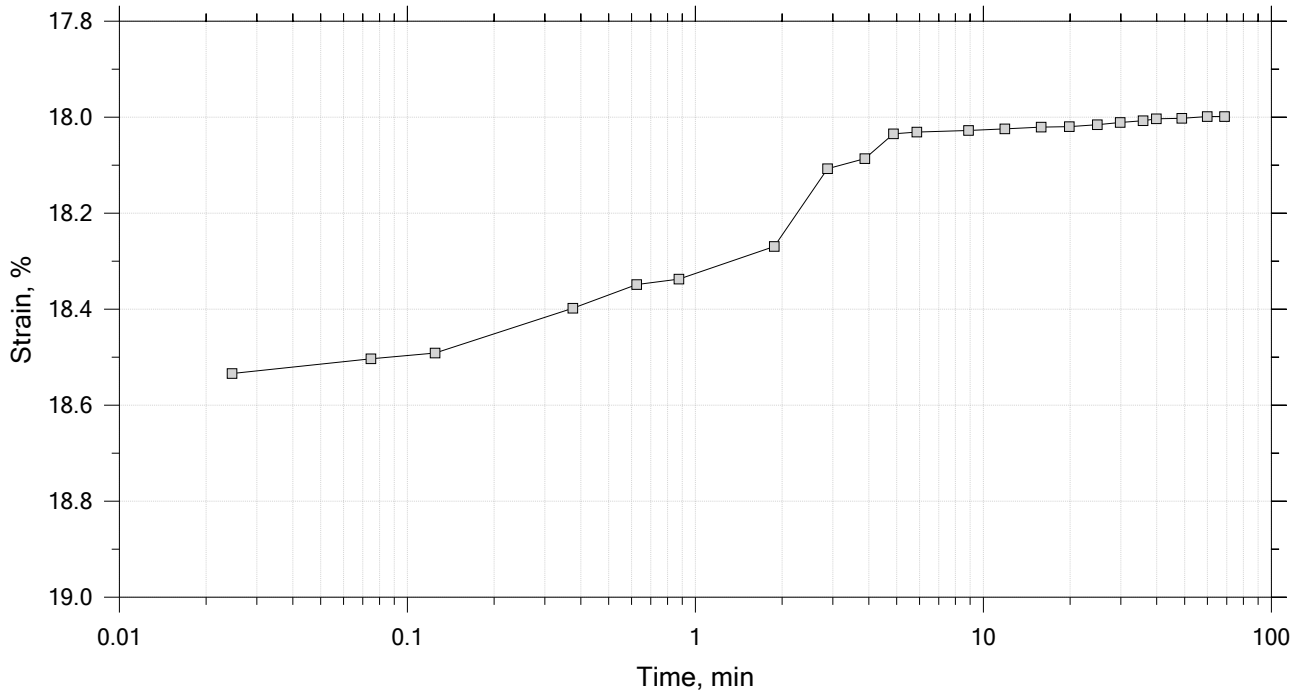
 Engineering and Testing	Project: Breton Lakebridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-3	Tested By: jm	Checked By: mcm
	Sample No.: 8	Test Date: 10/10/20	Depth: 14-16 ft
	Test No.: IP-6	Sample Type: intact	Elevation: ---
	Description: Moist, greenish gray clay(CH)		


# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 10 of 12

Constant Load Step

Stress: 1e+03 psf



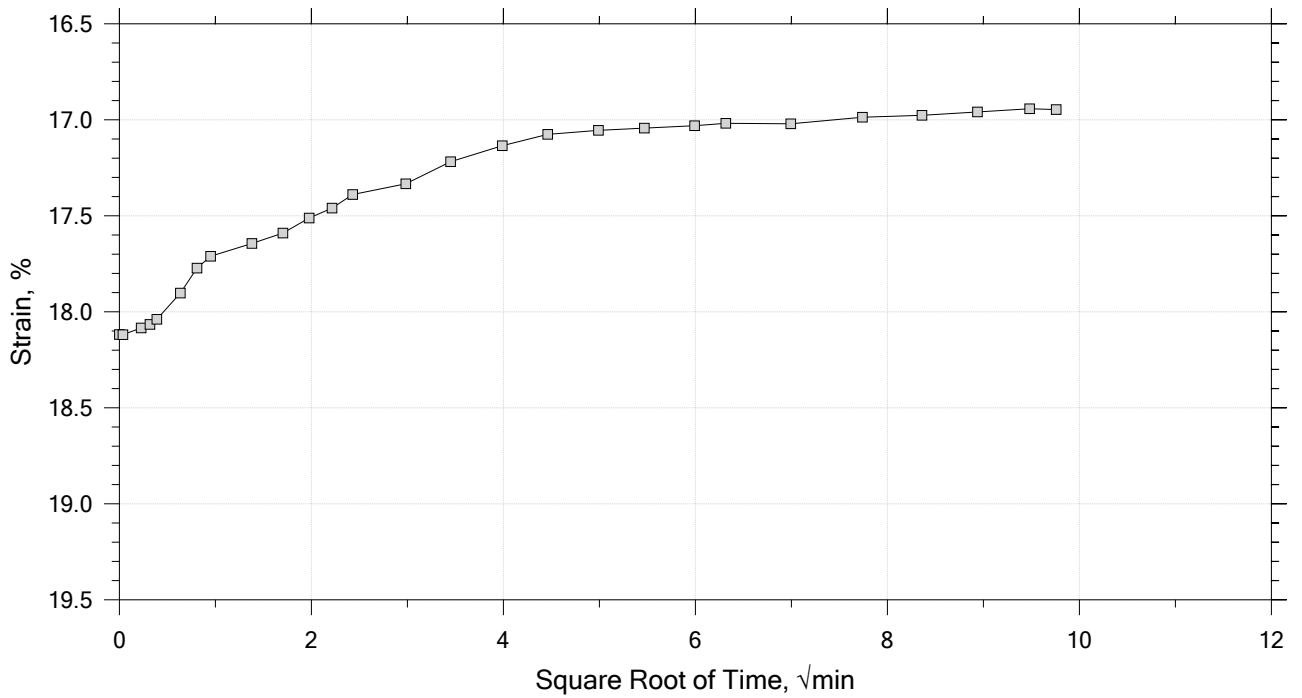
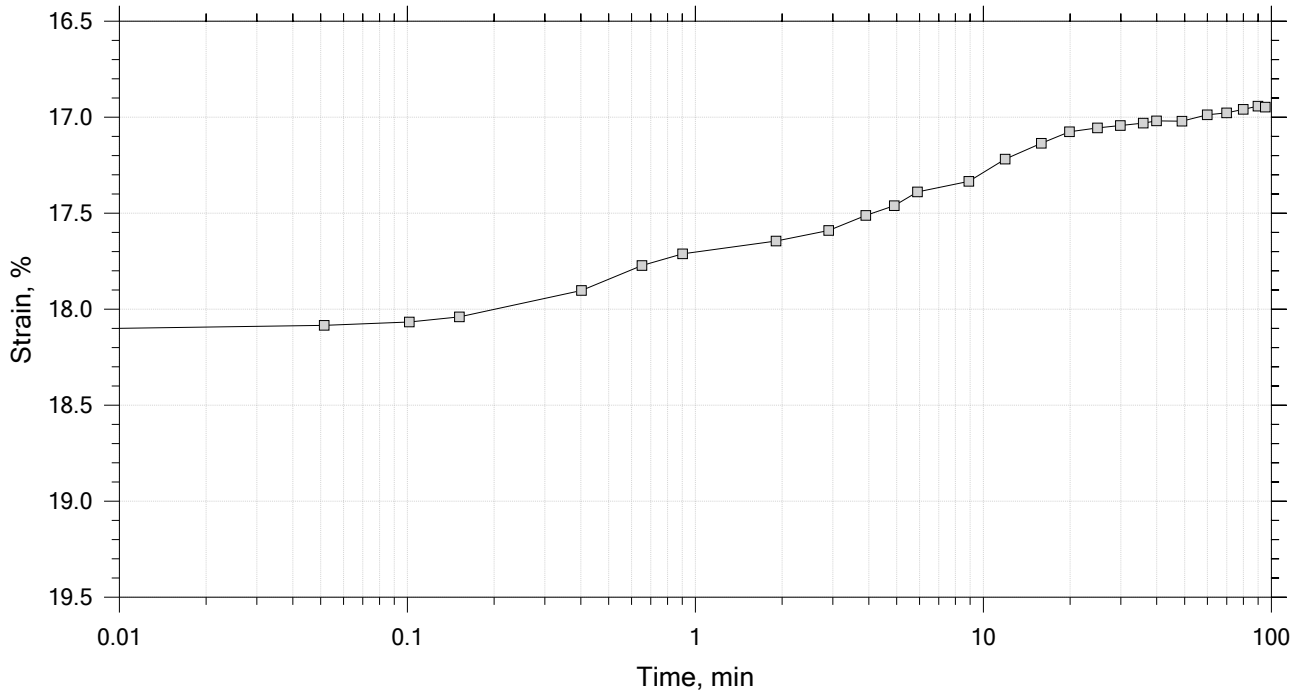
 Engineering and Testing	Project: Breton Lakebridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-3	Tested By: jm	Checked By: mcm
	Sample No.: 8	Test Date: 10/10/20	Depth: 14-16 ft
	Test No.: IP-6	Sample Type: intact	Elevation: ---
	Description: Moist, greenish gray clay(CH)		


# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 11 of 12

Constant Load Step

Stress: 500 psf



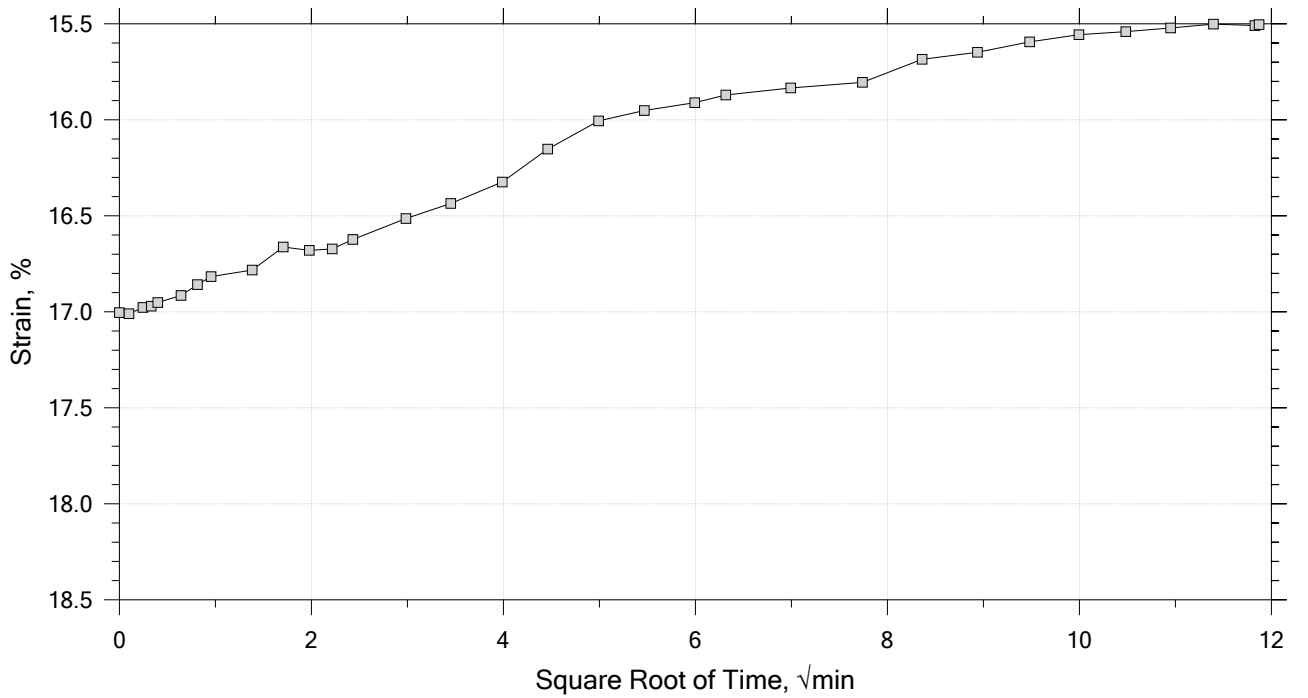
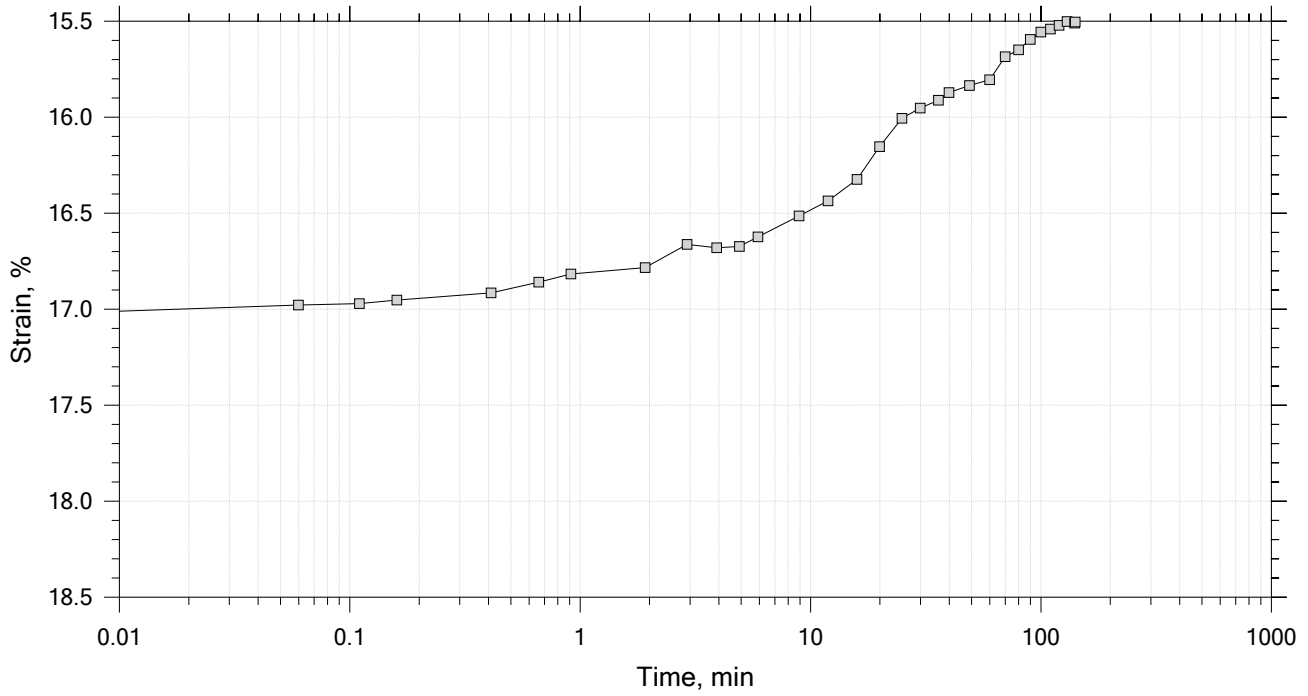
 Engineering and Testing	Project: Breton Lakebridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-3	Tested By: jm	Checked By: mcm
	Sample No.: ---	Test Date: 10/10/20	Depth: 14-16 ft
	Test No.: IP-6	Sample Type: intact	Elevation: ---
	Description: Moist, greenish gray clay(CH)		


# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 12 of 12

Constant Load Step

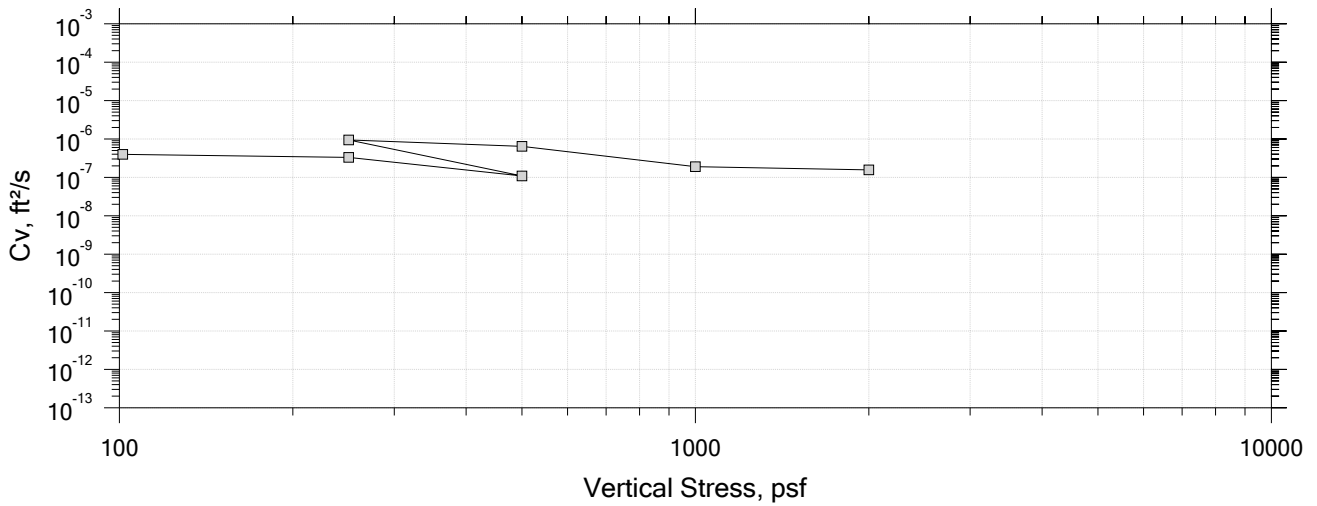
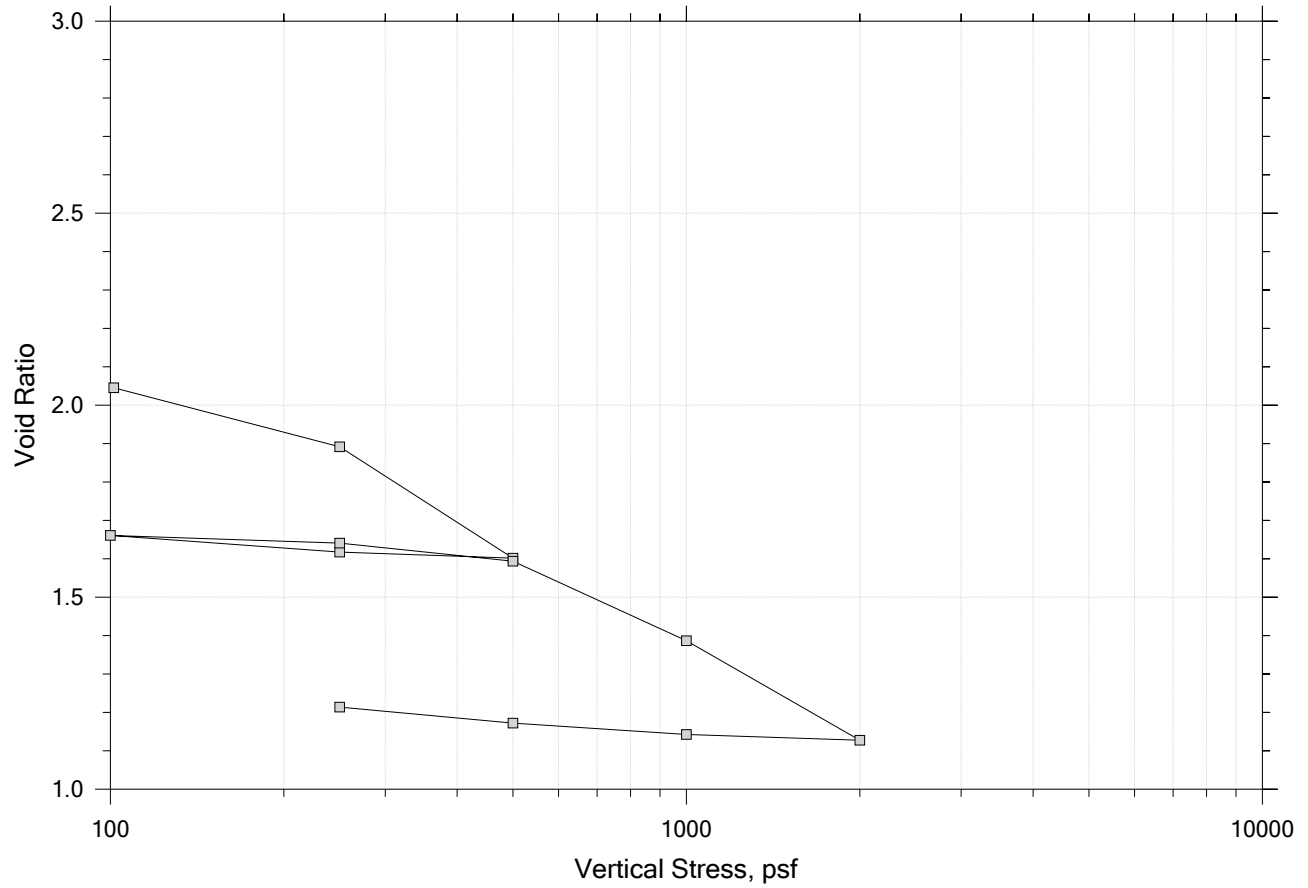
Stress: 250 psf




 <p>Engineering and Testing</p>	Project: Breton Lakebridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-3	Tested By: jm	Checked By: mcm
	Sample No.: 8	Test Date: 10/10/20	Depth: 14-16 ft
	Test No.: IP-6	Sample Type: intact	Elevation: ---
	Description: Moist, greenish gray clay(CH)		

# One-Dimensional Consolidation by ASTM D2435 - Method B

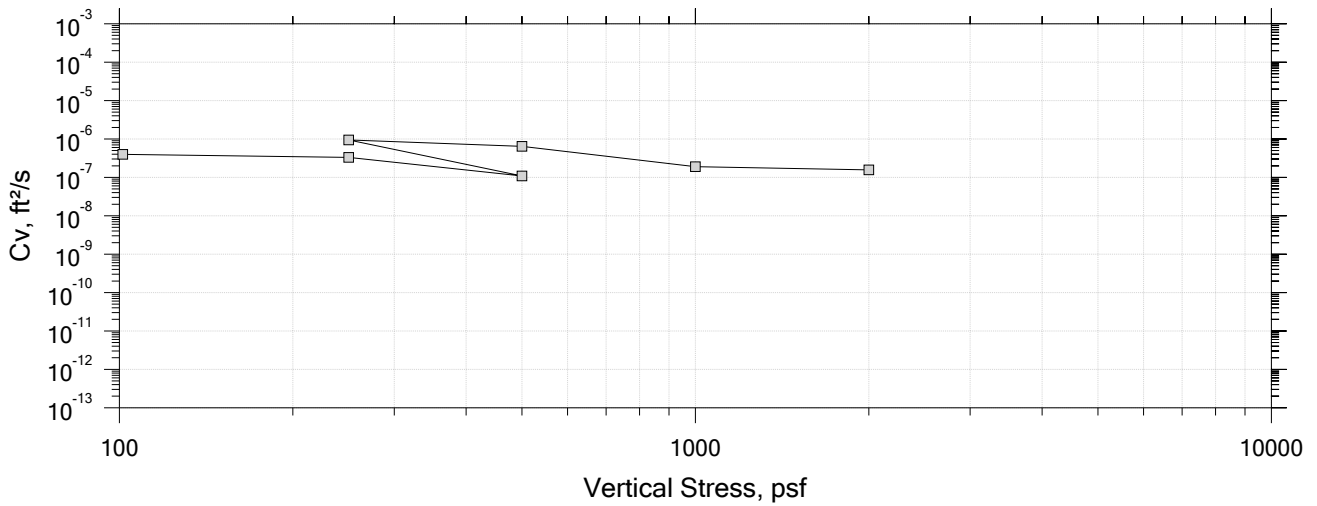
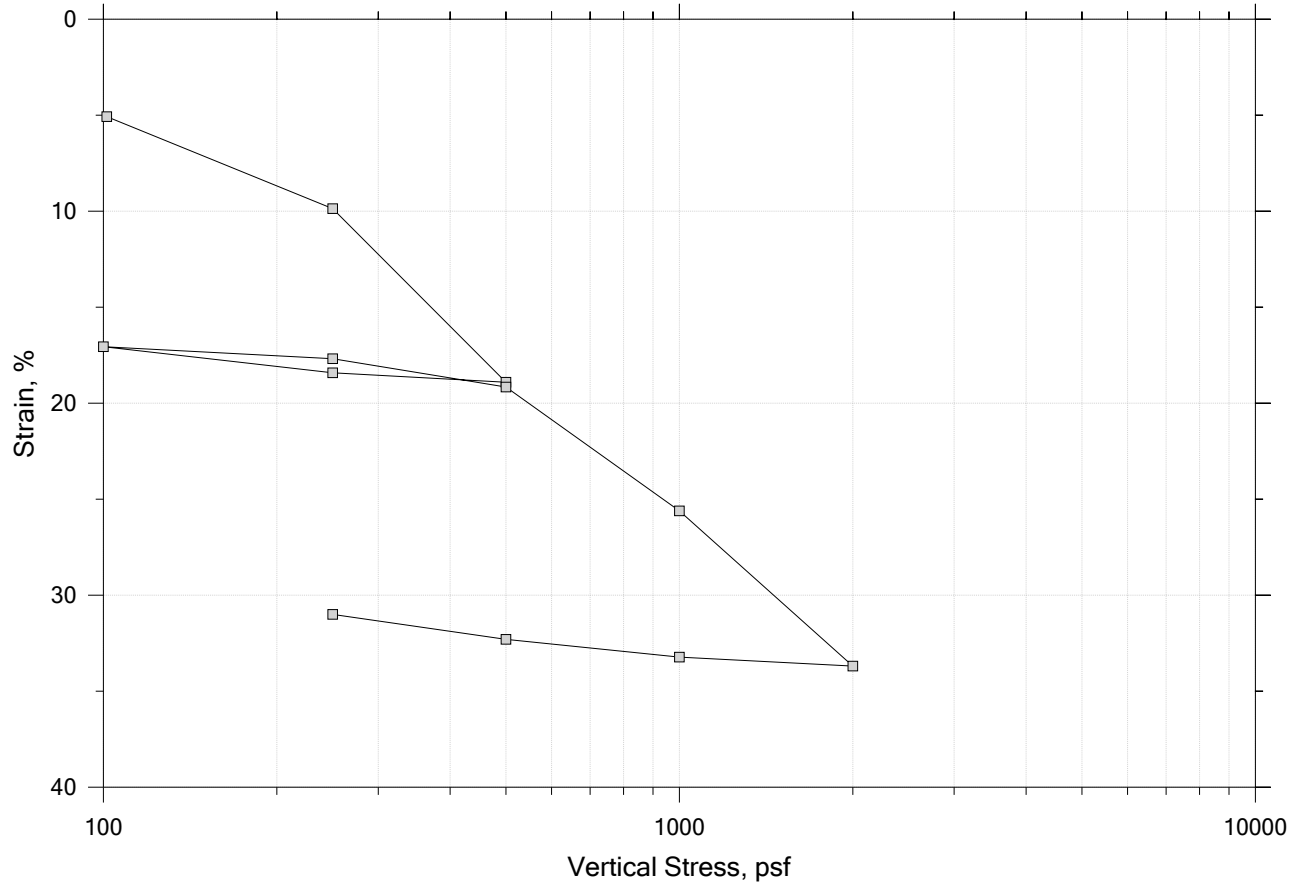
## Summary Report




 <p>APS Engineering and Testing</p>	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-5	Tested By: jm	Checked By: mcm
	Sample No.: 1	Test Date: 10/16/20	Depth: 0-2 ft
	Test No.: IP-7	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay(CL)	Measured specific gravity: 2.48	

# One-Dimensional Consolidation by ASTM D2435 - Method B

## Summary Report

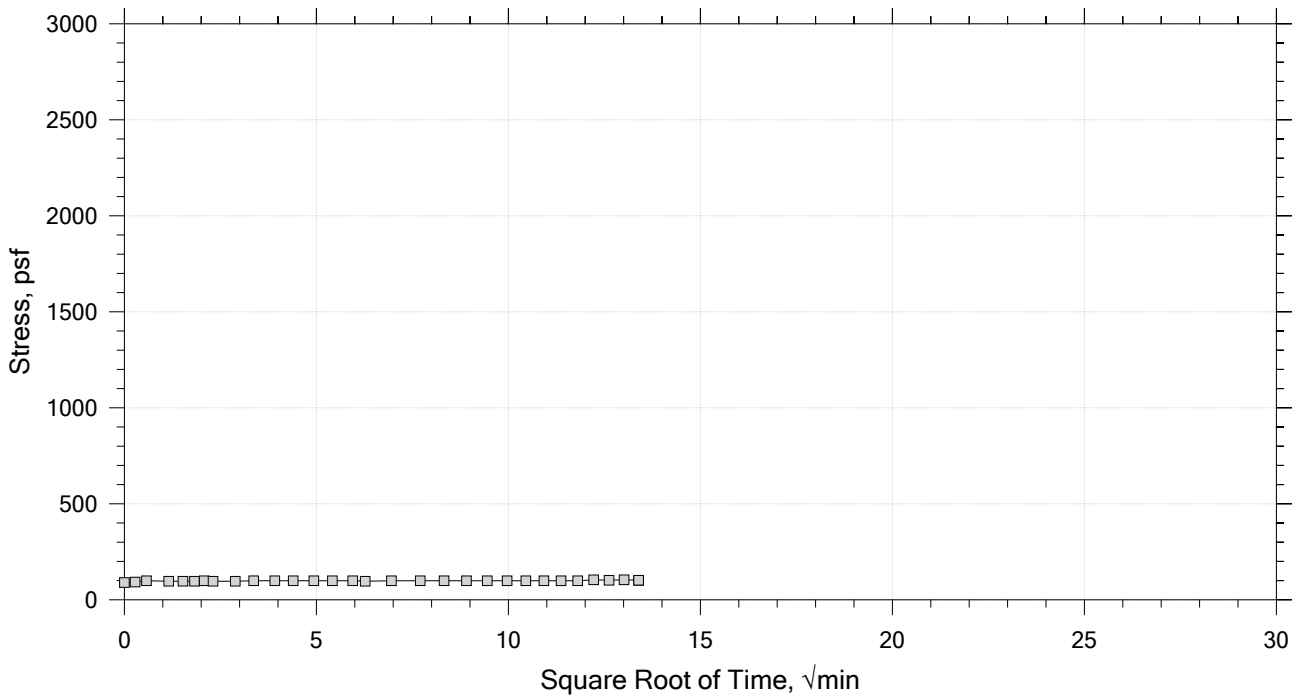
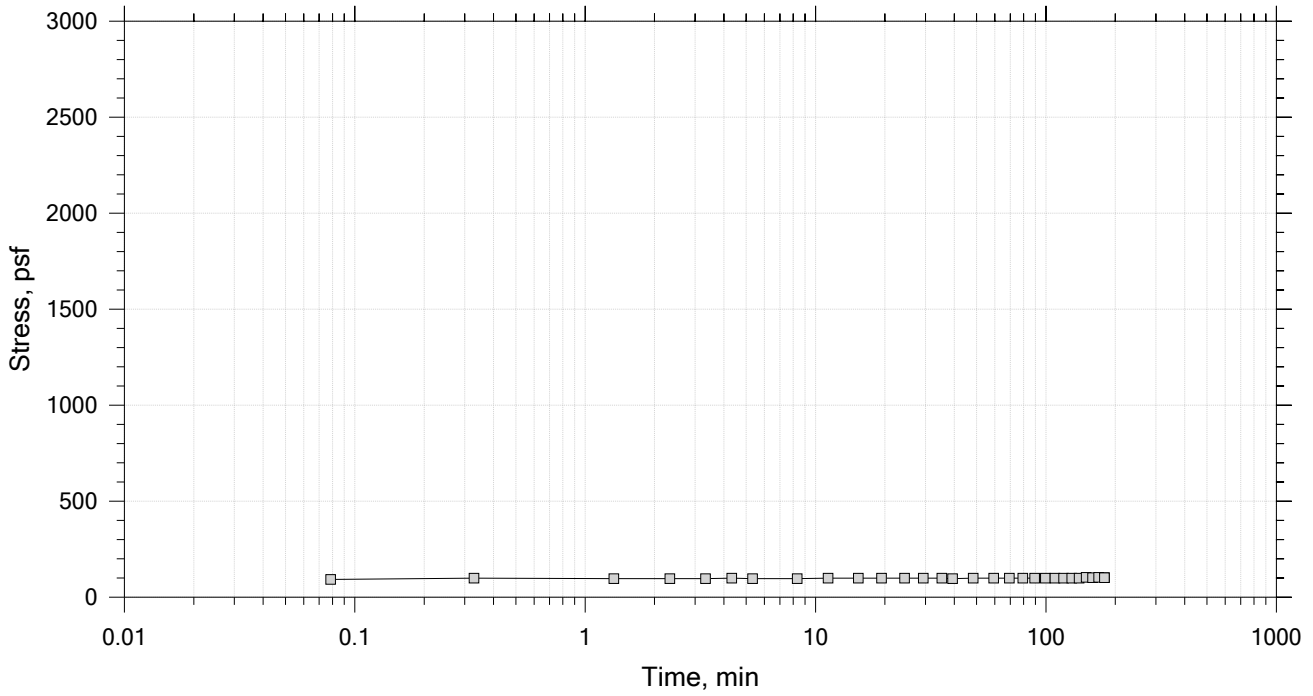



 <p>Engineering and Testing</p>	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-5	Tested By: jm	Checked By: mcm
	Sample No.: 1	Test Date: 10/16/20	Depth: 0-2 ft
	Test No.: IP-7	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay (CL)		



# One-Dimensional Consolidation by ASTM D2435 - Method B

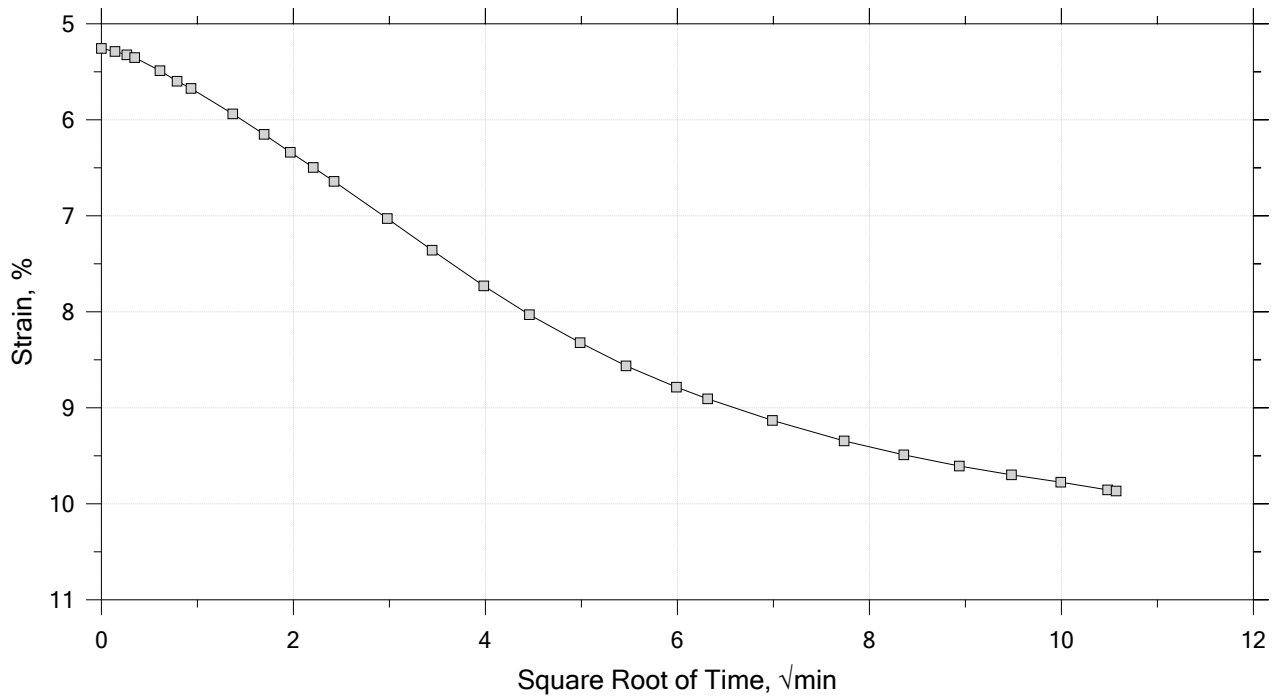
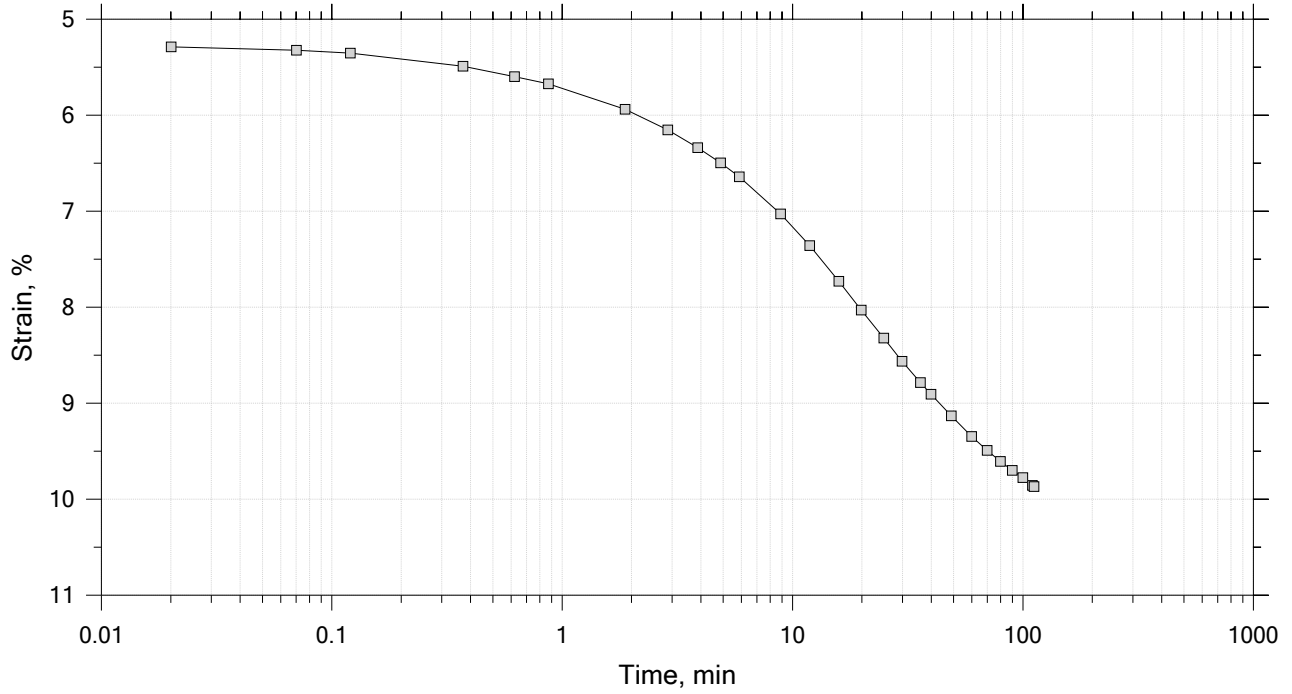
Time Curve 1 of 12  
 Constant Volume Step  
 Stress: 101 psf




 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-5	Tested By: jm	Checked By: mcm
	Sample No.:1	Test Date: 10/16/20	Depth: 0-2 ft
	Test No.: IP-7	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay(CL)		

# One-Dimensional Consolidation by ASTM D2435 - Method B

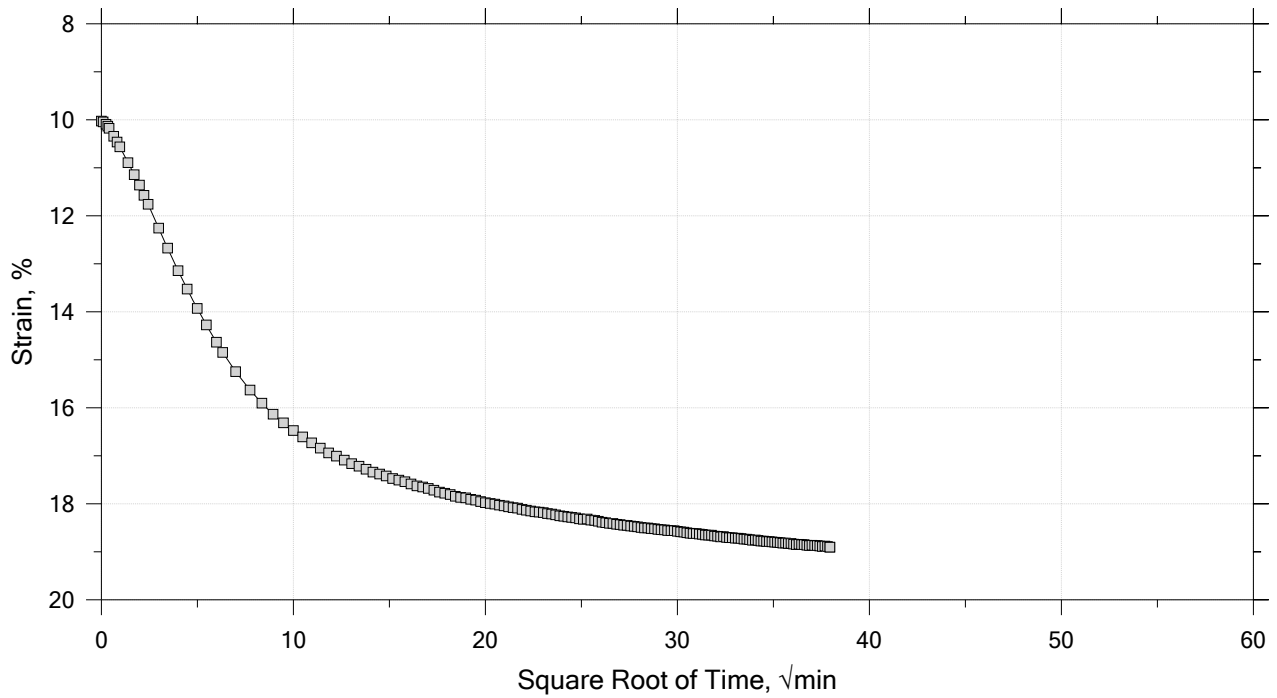
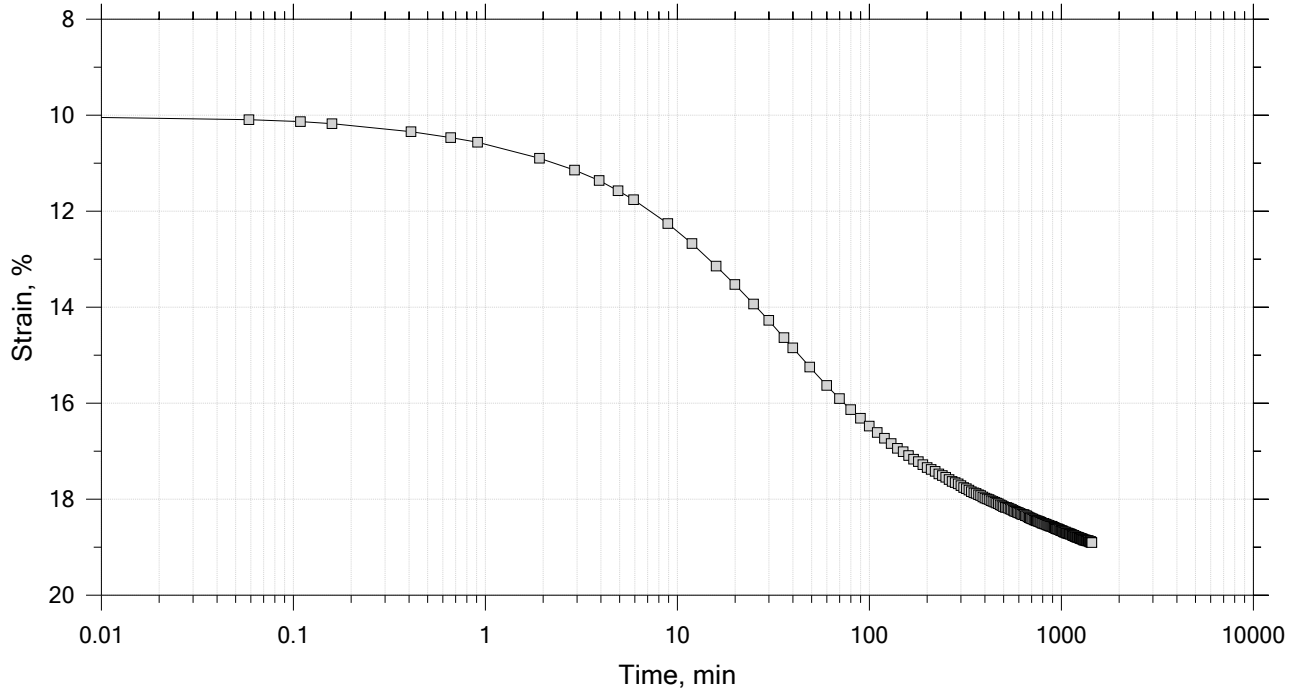
Time Curve 2 of 12  
 Constant Load Step  
 Stress: 250 psf




 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-5	Tested By: jm	Checked By: mcm
	Sample No.: 1	Test Date: 10/16/20	Depth: 0-2 ft
	Test No.: IP-7	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay(CL)		

# One-Dimensional Consolidation by ASTM D2435 - Method B

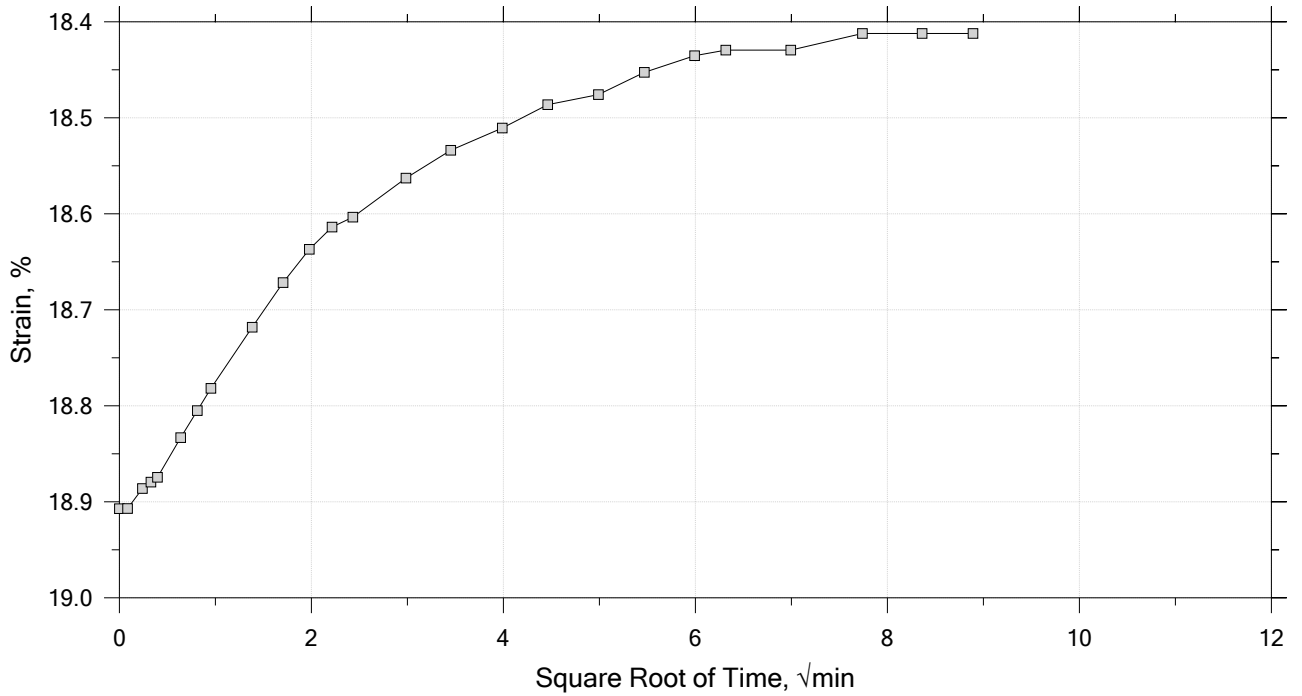
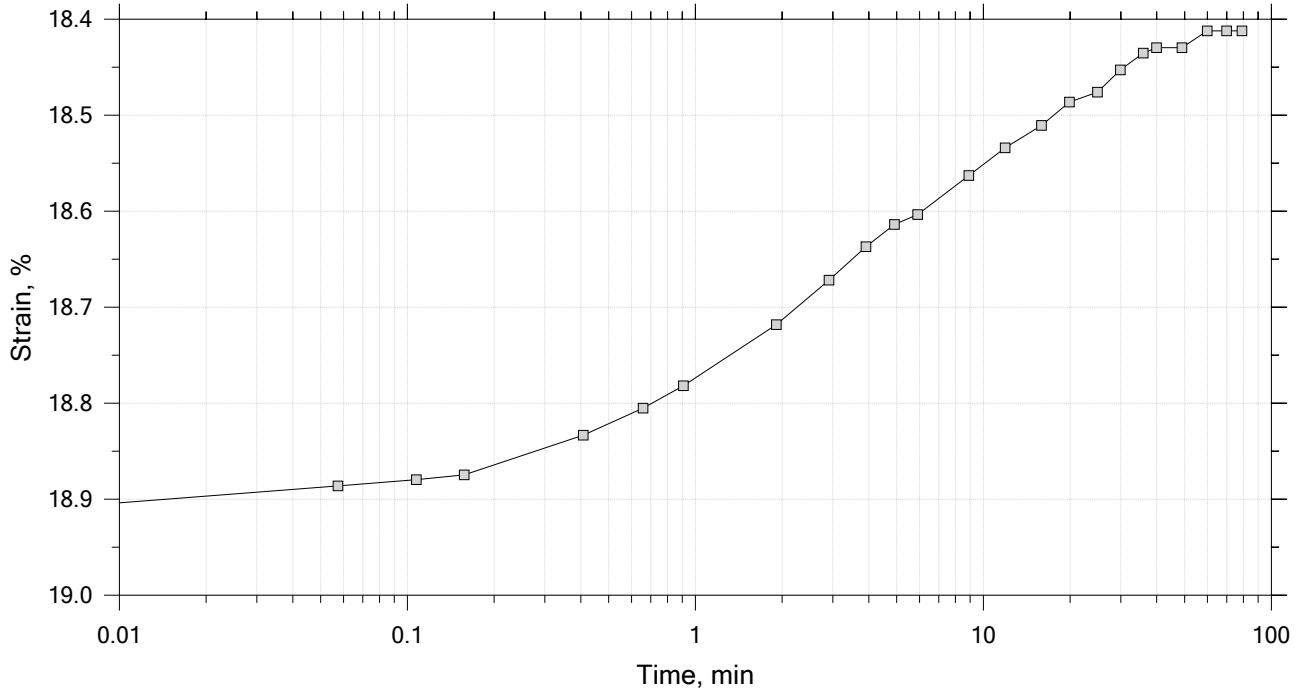
Time Curve 3 of 12  
 Constant Load Step  
 Stress: 500 psf




 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-5	Tested By: jm	Checked By: mcm
	Sample No.: 1	Test Date: 10/16/20	Depth: 0-2 ft
	Test No.: IP-7	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay(CL)		

# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 4 of 12  
 Constant Load Step  
 Stress: 250 psf



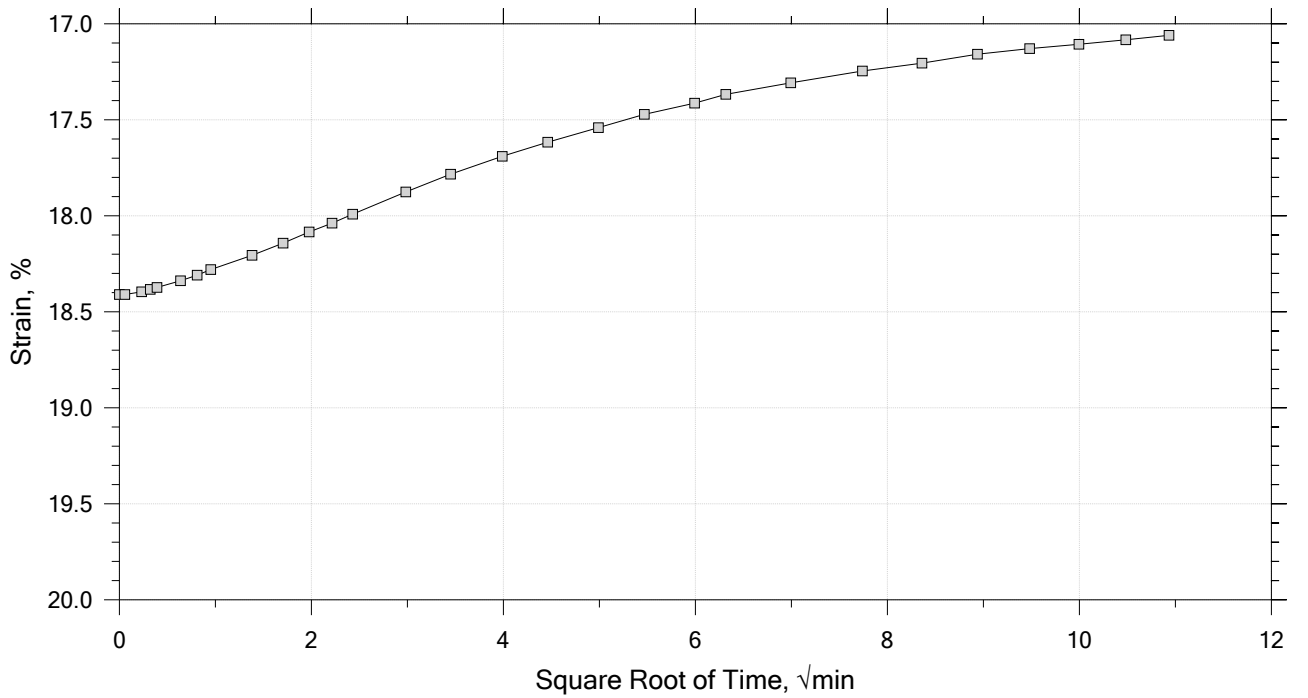
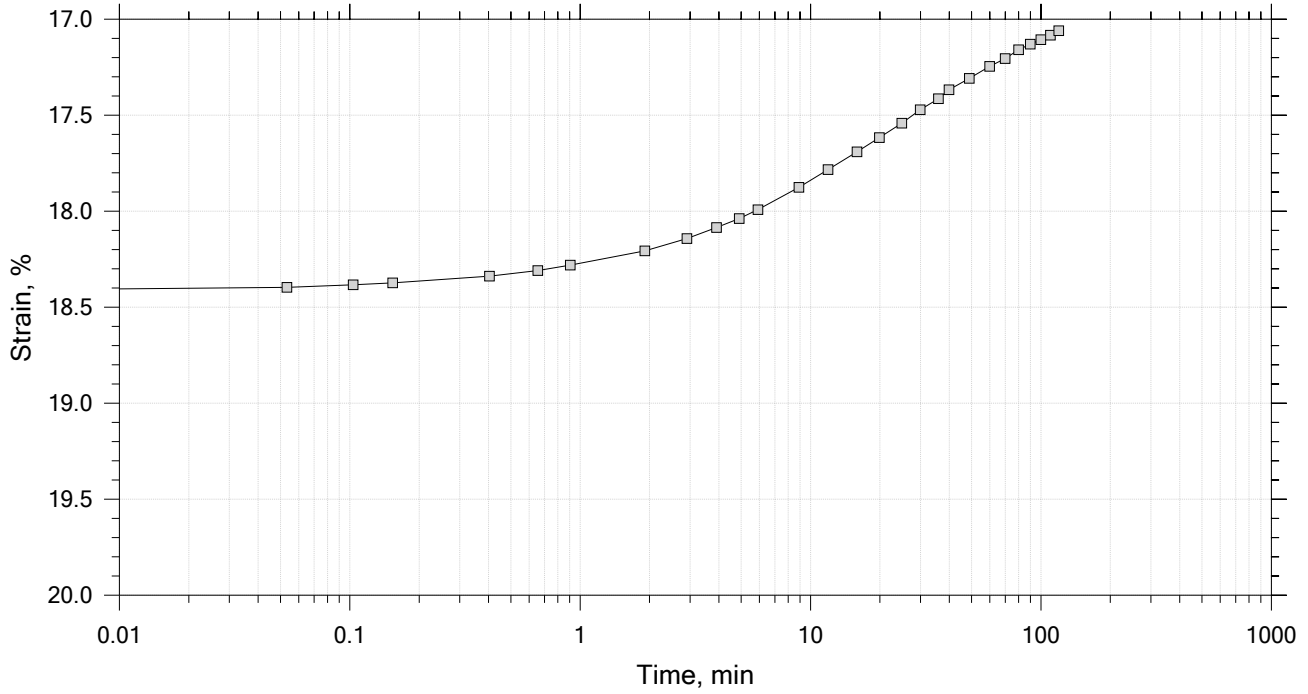
 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-5	Tested By: jm	Checked By: mcm
	Sample No.: 1	Test Date: 10/16/20	Depth: 0-2 ft
	Test No.: IP-7	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay(CL)		


# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 5 of 12

Constant Load Step

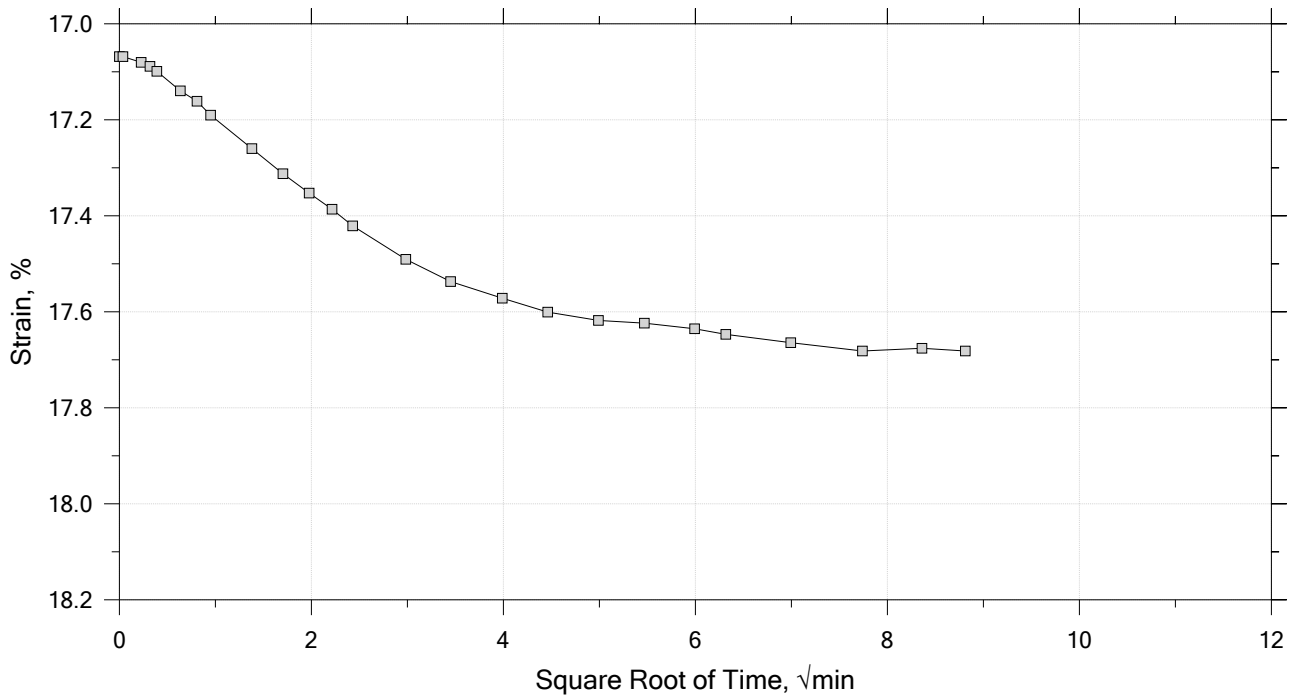
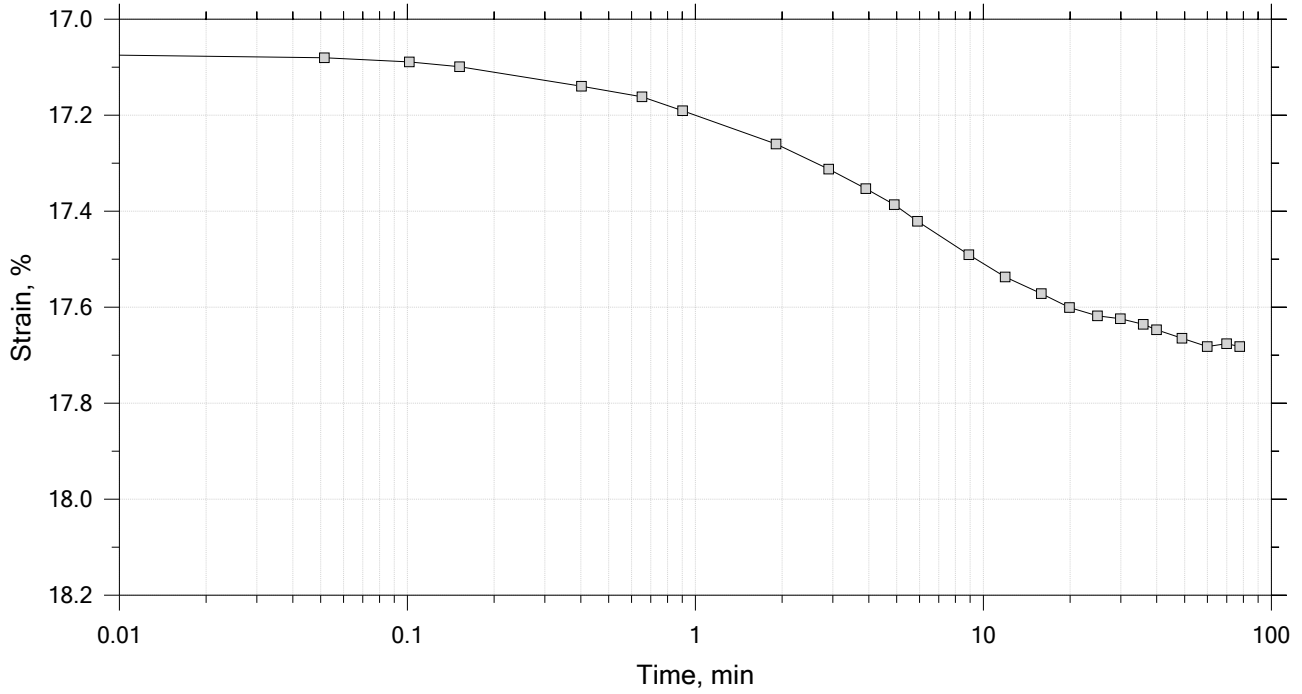
Stress: 100 psf




 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-5	Tested By: jm	Checked By: mcm
	Sample No.: 1	Test Date: 10/16/20	Depth: 0-2 ft
	Test No.: IP-7	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay(CL)		

# One-Dimensional Consolidation by ASTM D2435 - Method B

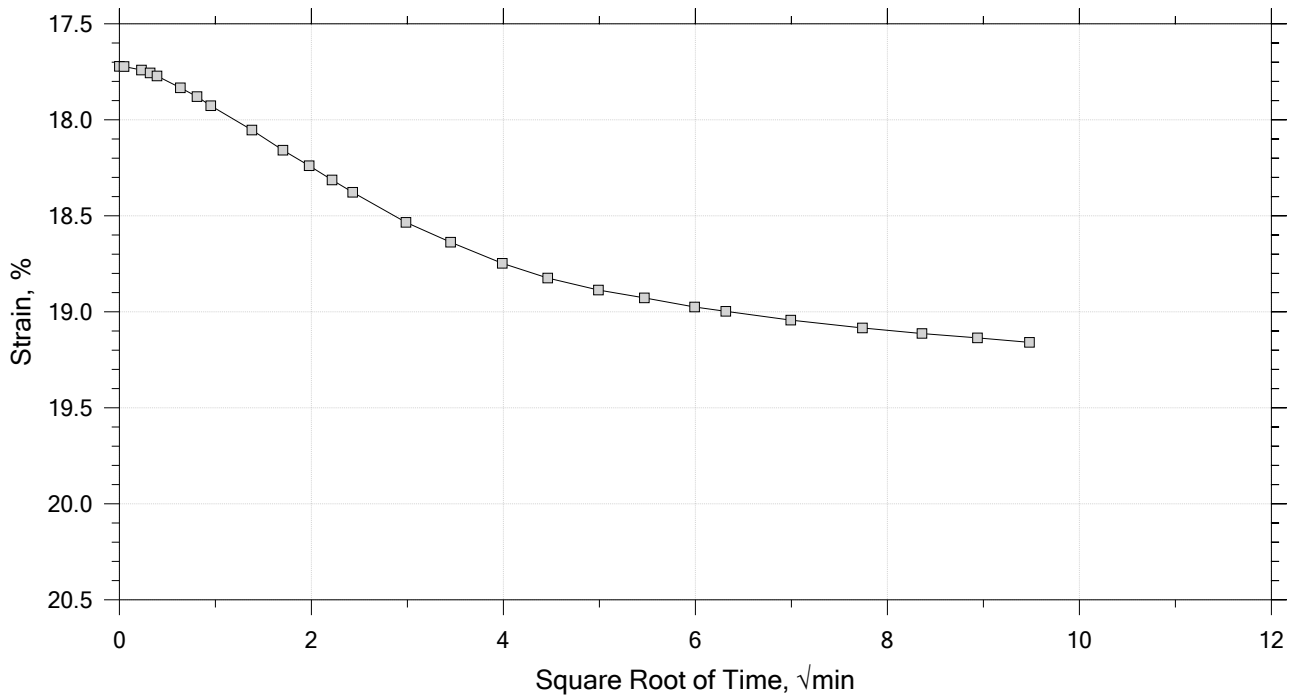
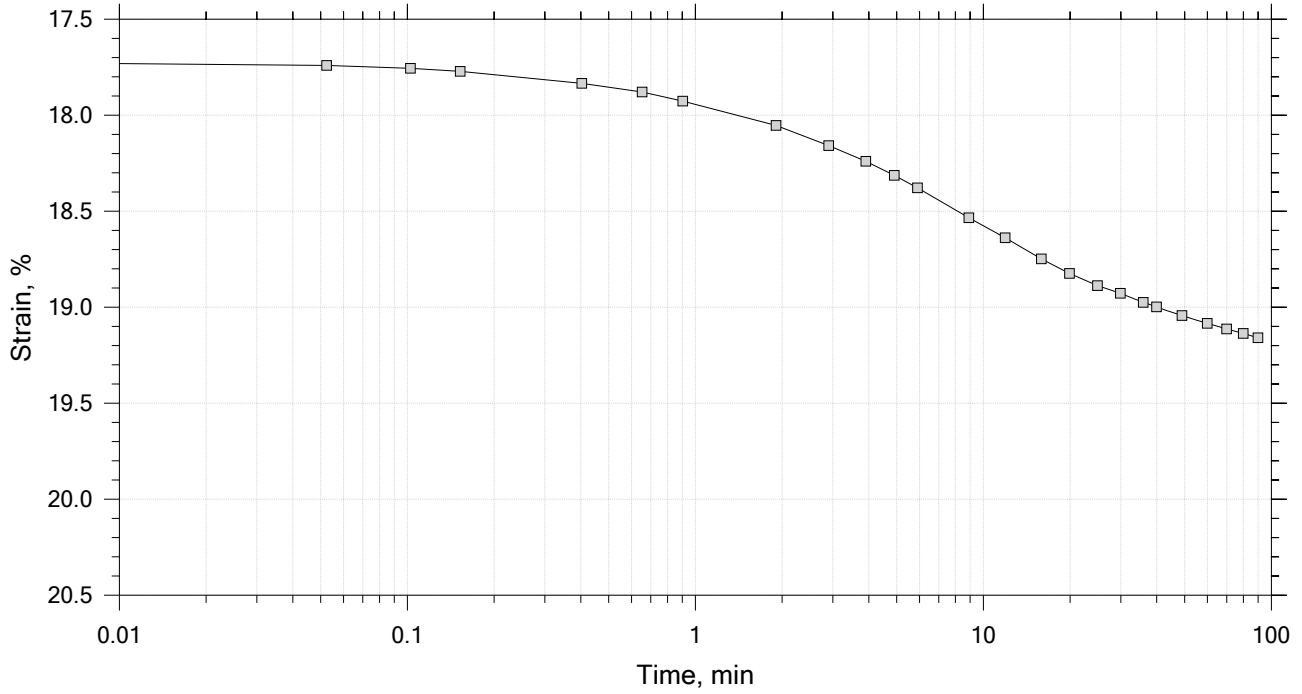
Time Curve 6 of 12  
 Constant Load Step  
 Stress: 250 psf




 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-5	Tested By: jm	Checked By: mcm
	Sample No.: 1	Test Date: 10/16/20	Depth: 0-2 ft
	Test No.: IP-7	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay(CL)		

# One-Dimensional Consolidation by ASTM D2435 - Method B

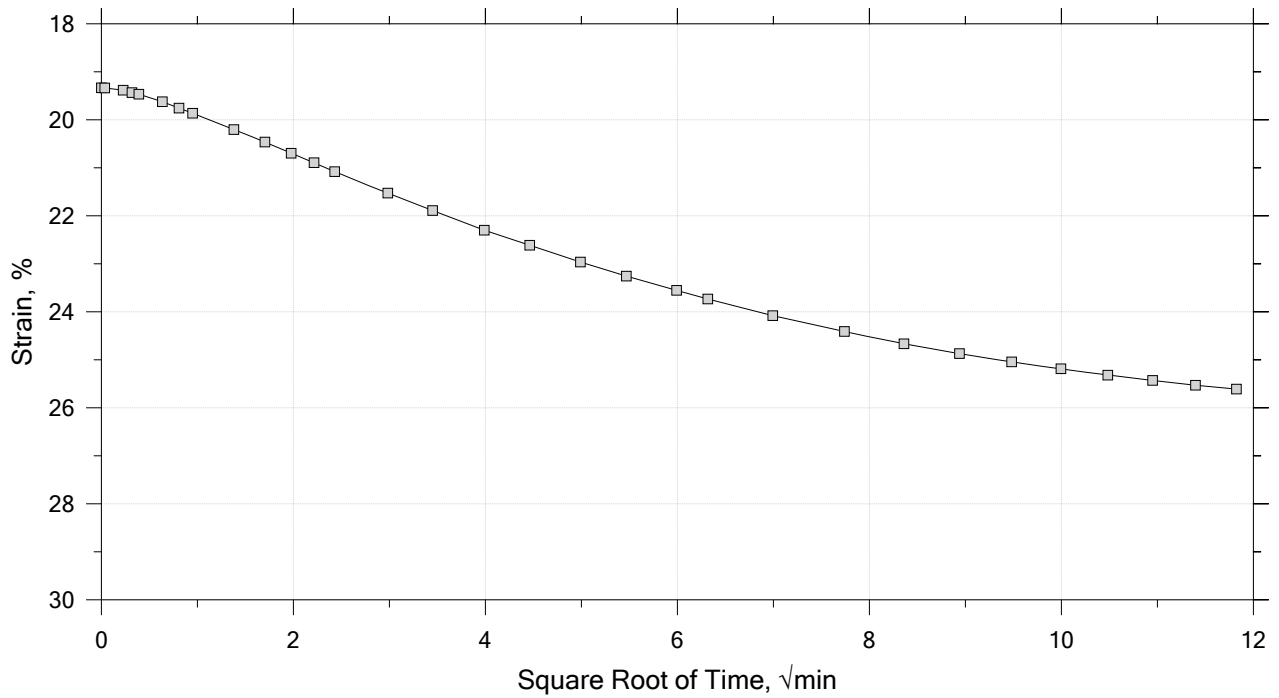
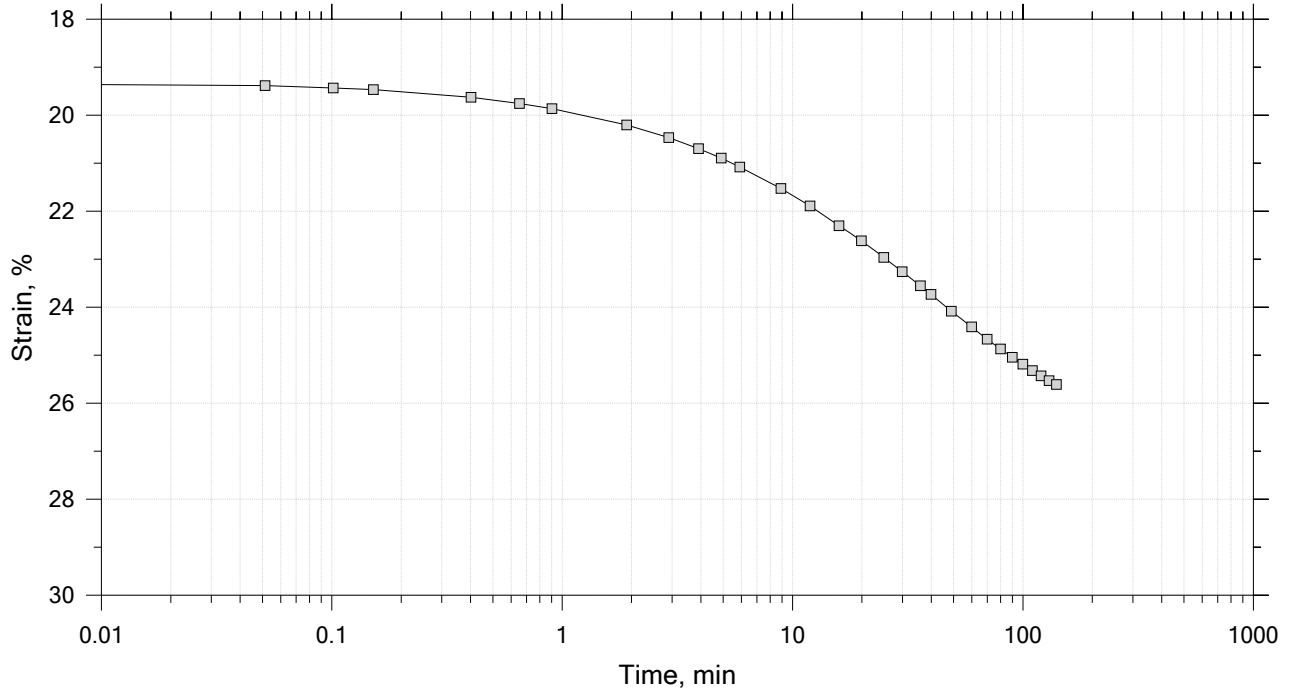
Time Curve 7 of 12  
 Constant Load Step  
 Stress: 500 psf




 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-5	Tested By: jm	Checked By: mcm
	Sample No.: 1	Test Date: 10/16/20	Depth: 0-2 ft
	Test No.: IP-7	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay(CL)		

# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 8 of 12  
 Constant Load Step  
 Stress: 1e+03 psf

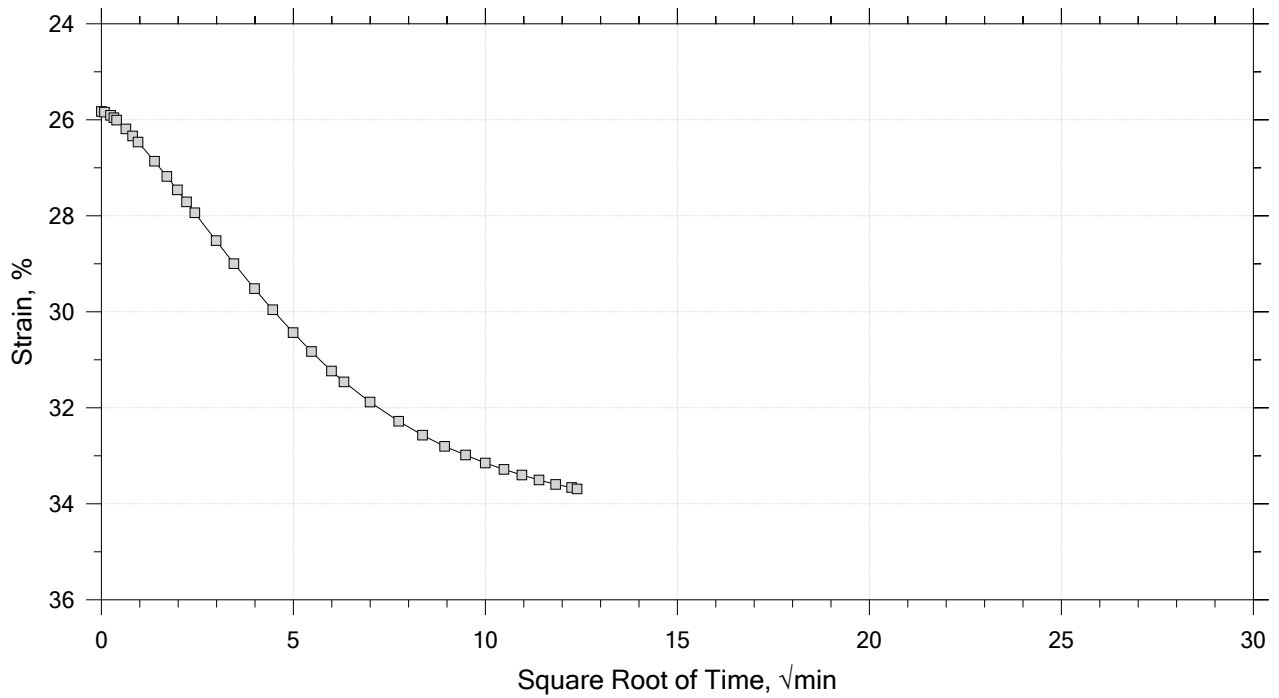
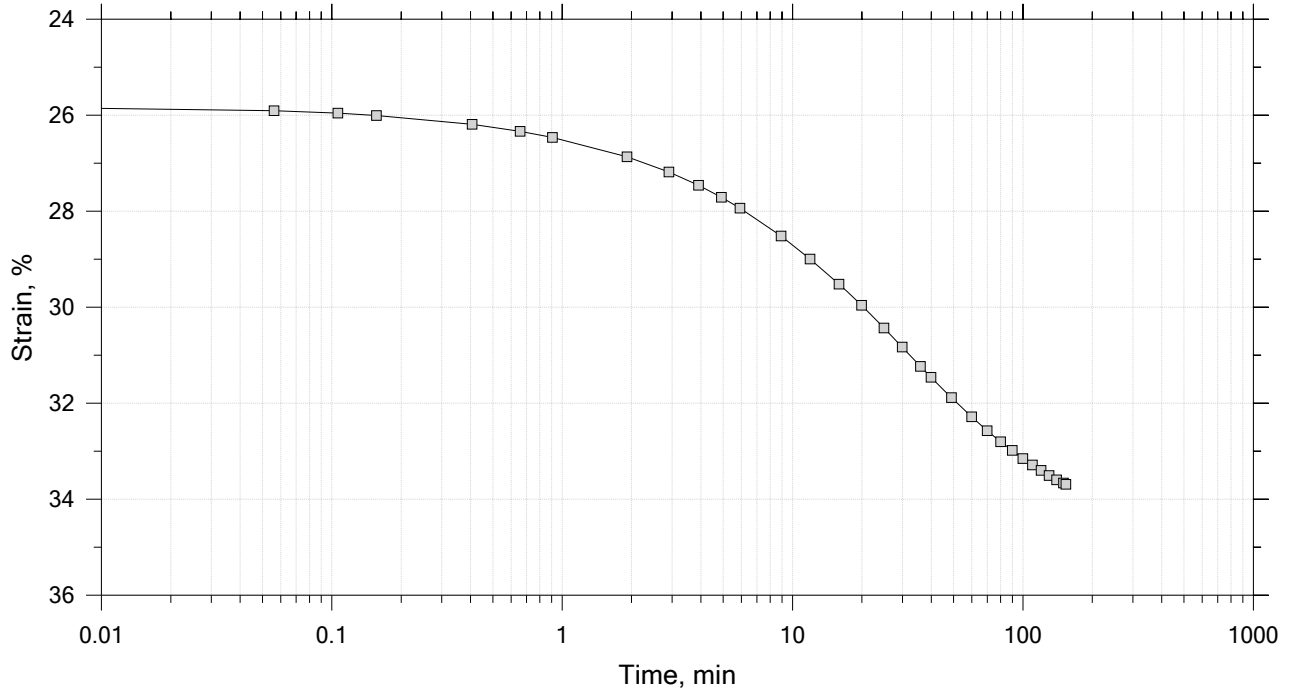



 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-5	Tested By: jm	Checked By: mcm
	Sample No.: 1	Test Date: 10/16/20	Depth: 0-2 ft
	Test No.: IP-7	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay(CL)		



# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 9 of 12  
 Constant Load Step  
 Stress: 2e+03 psf



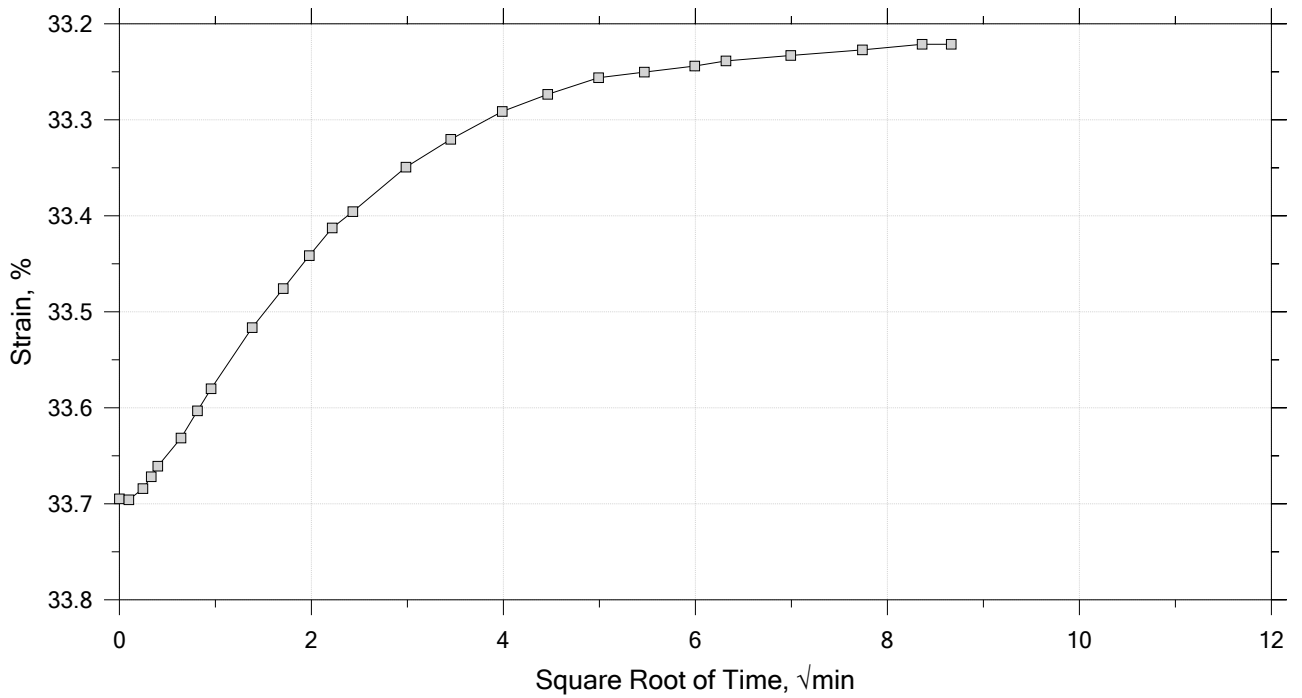
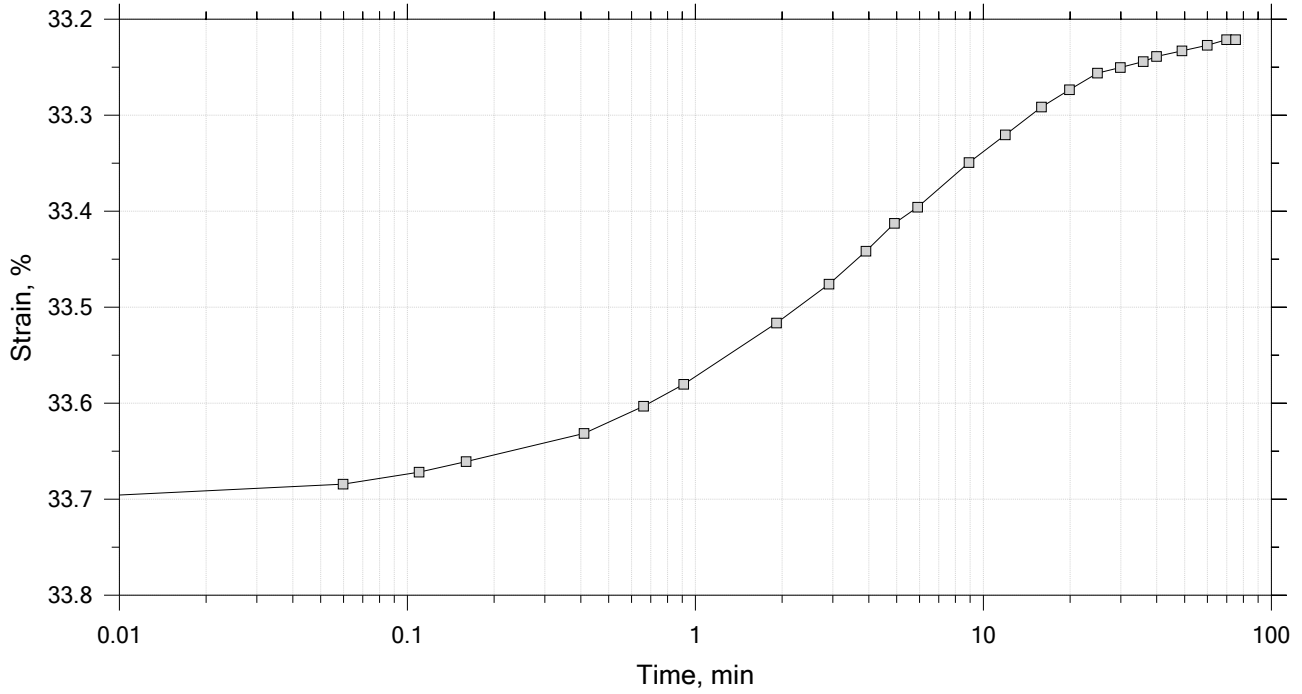
 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-5	Tested By: jm	Checked By: mcm
	Sample No.: 1	Test Date: 10/16/20	Depth: 0-2 ft
	Test No.: IP-7	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay(CL)		


# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 10 of 12

Constant Load Step

Stress: 1e+03 psf



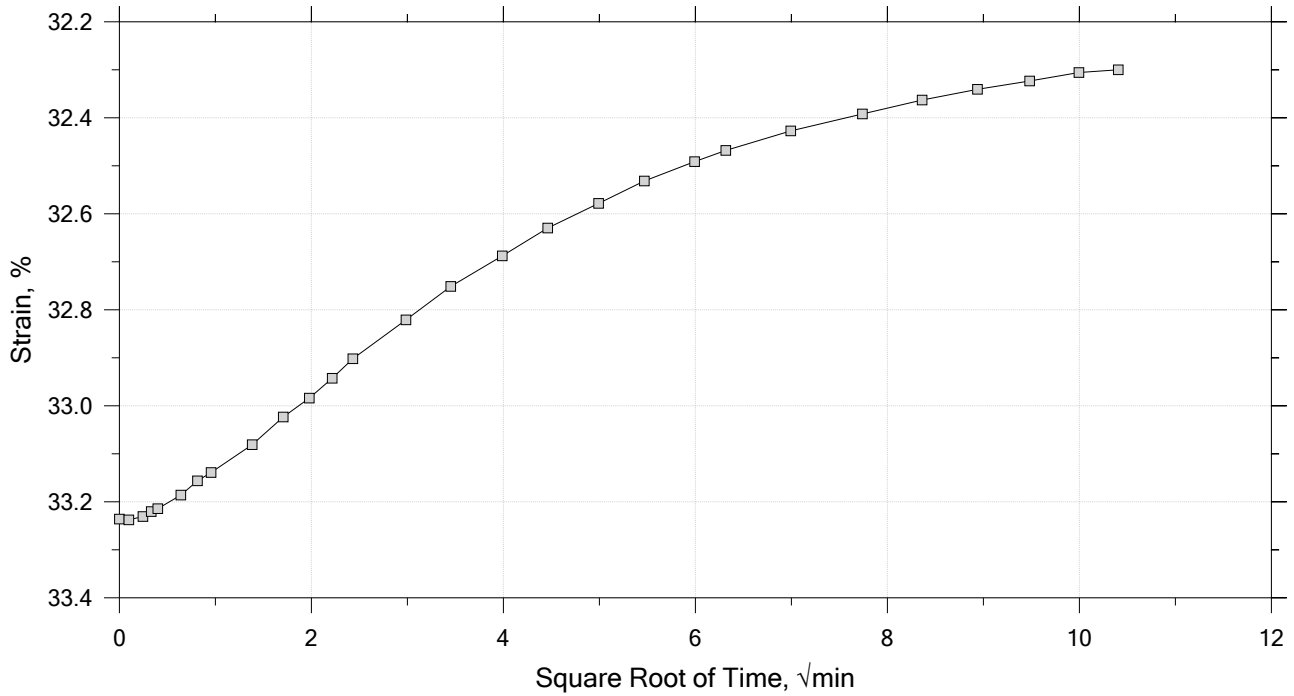
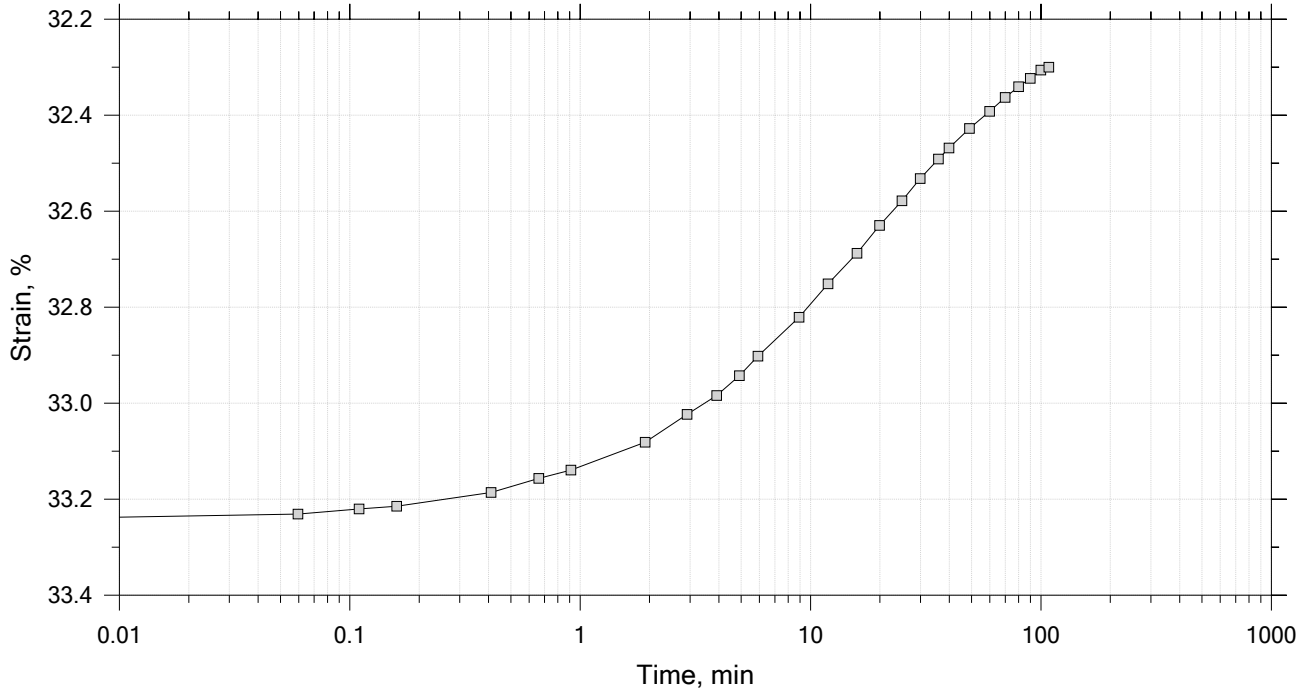
 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-5	Tested By: jm	Checked By: mcm
	Sample No.: 1	Test Date: 10/16/20	Depth: 0-2 ft
	Test No.: IP-7	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay(CL)		


# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 11 of 12

Constant Load Step

Stress: 500 psf



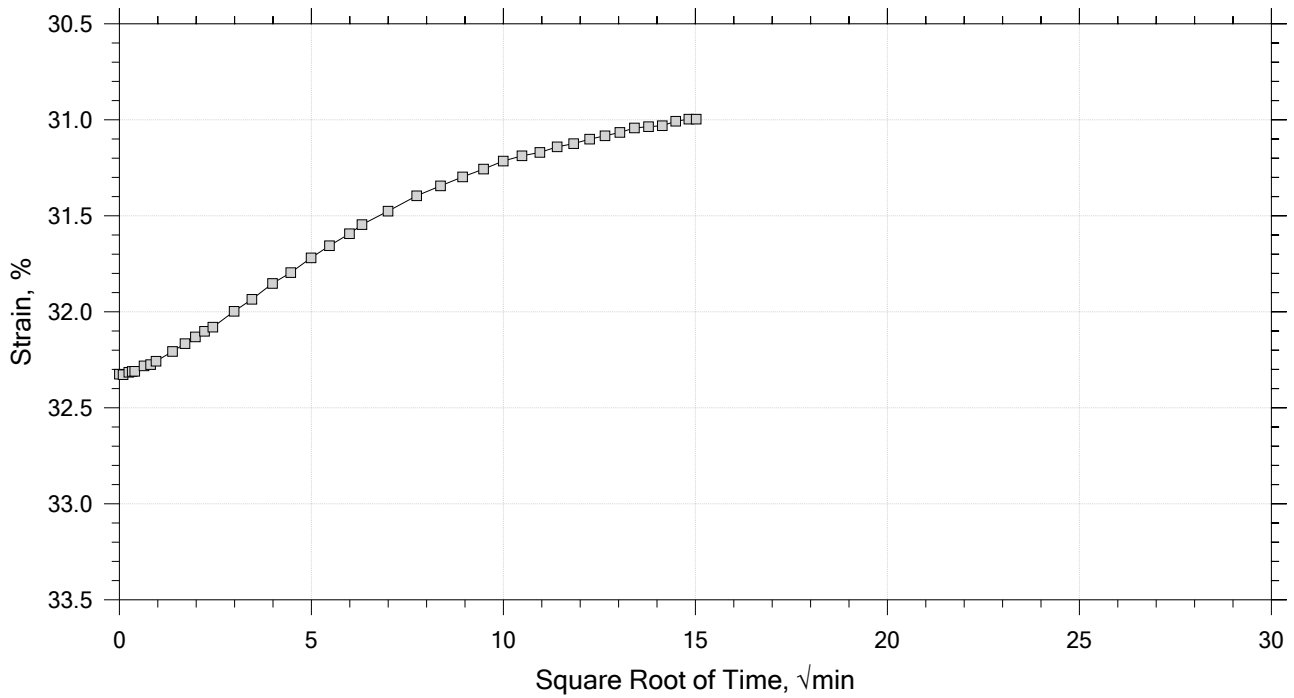
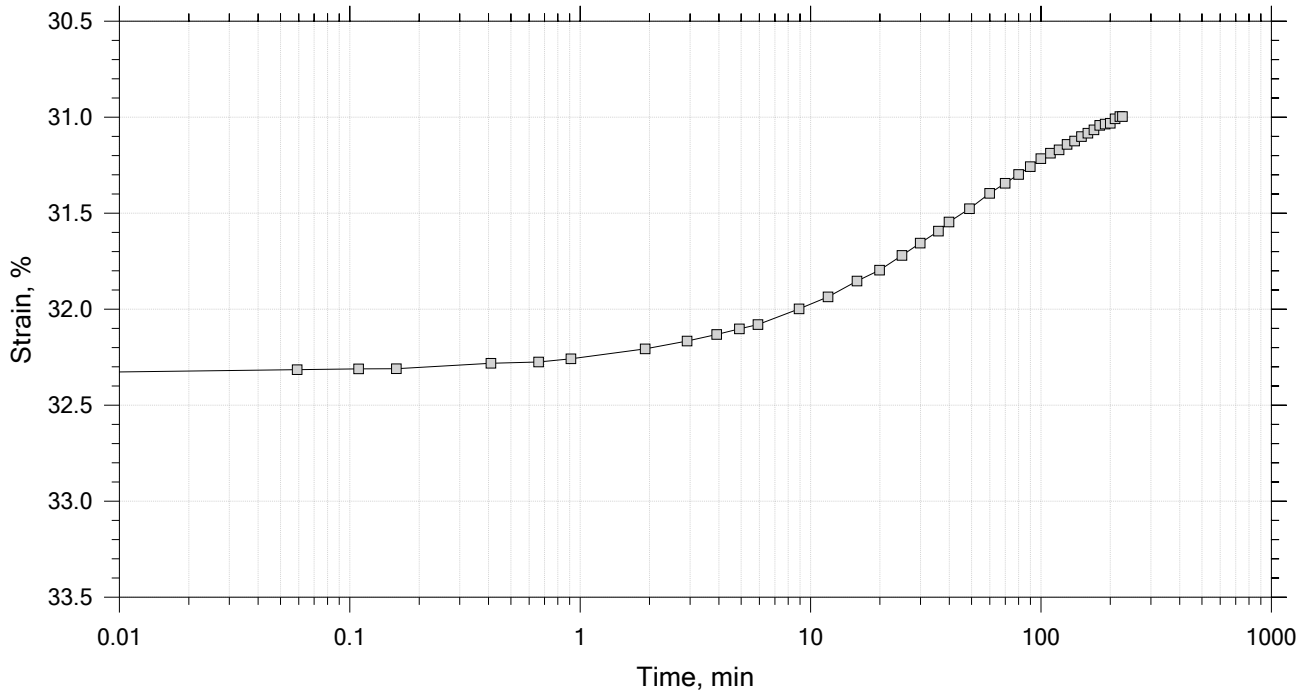
 <p>Engineering and Testing</p>	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-5	Tested By: jm	Checked By: mcm
	Sample No.:1	Test Date: 10/16/20	Depth: 0-2 ft
	Test No.: IP-7	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay(CL)		


# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 12 of 12

Constant Load Step

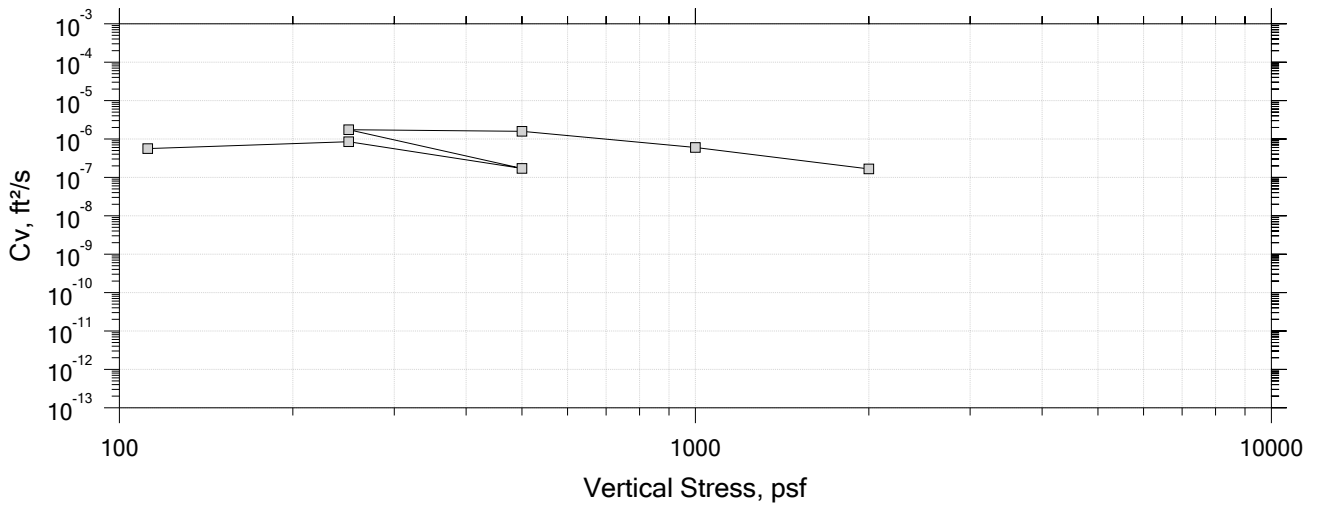
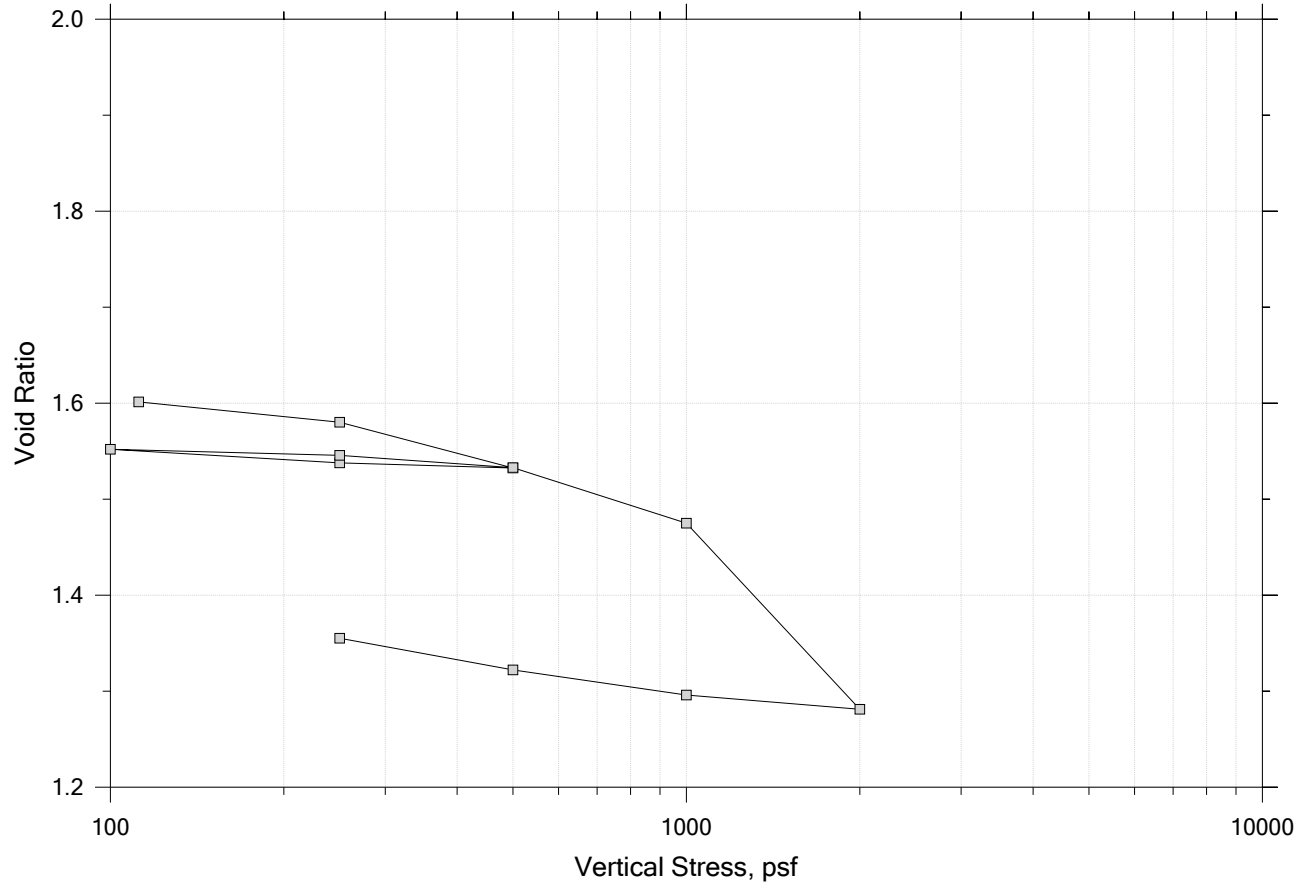
Stress: 250 psf




 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-5	Tested By: jm	Checked By: mcm
	Sample No.: 1	Test Date: 10/16/20	Depth: 0-2 ft
	Test No.: IP-7	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay(CL)		

# One-Dimensional Consolidation by ASTM D2435 - Method B

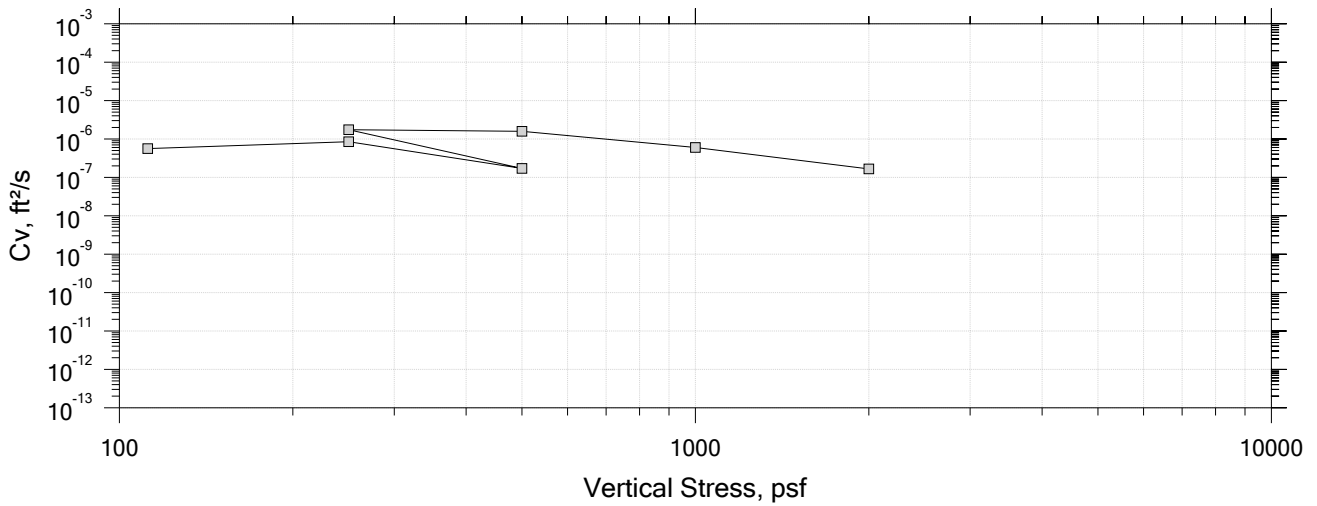
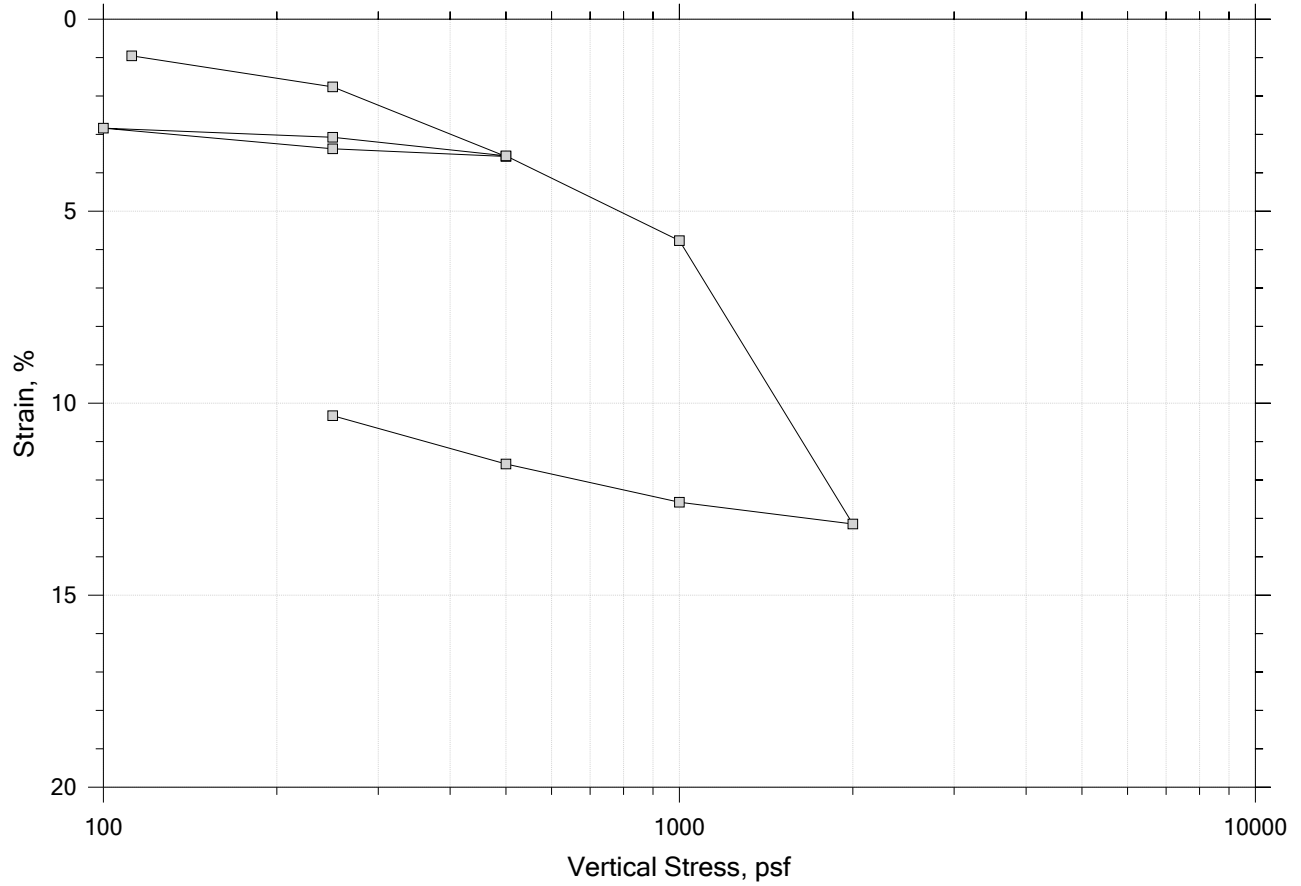
## Summary Report




	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-5	Tested By: jm	Checked By: mcm
	Sample No.: 8	Test Date: 10/12/20	Depth: 14-16 ft
	Test No.: IP-8	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay(CH)	Measured specific gravity: 2.57	

# One-Dimensional Consolidation by ASTM D2435 - Method B

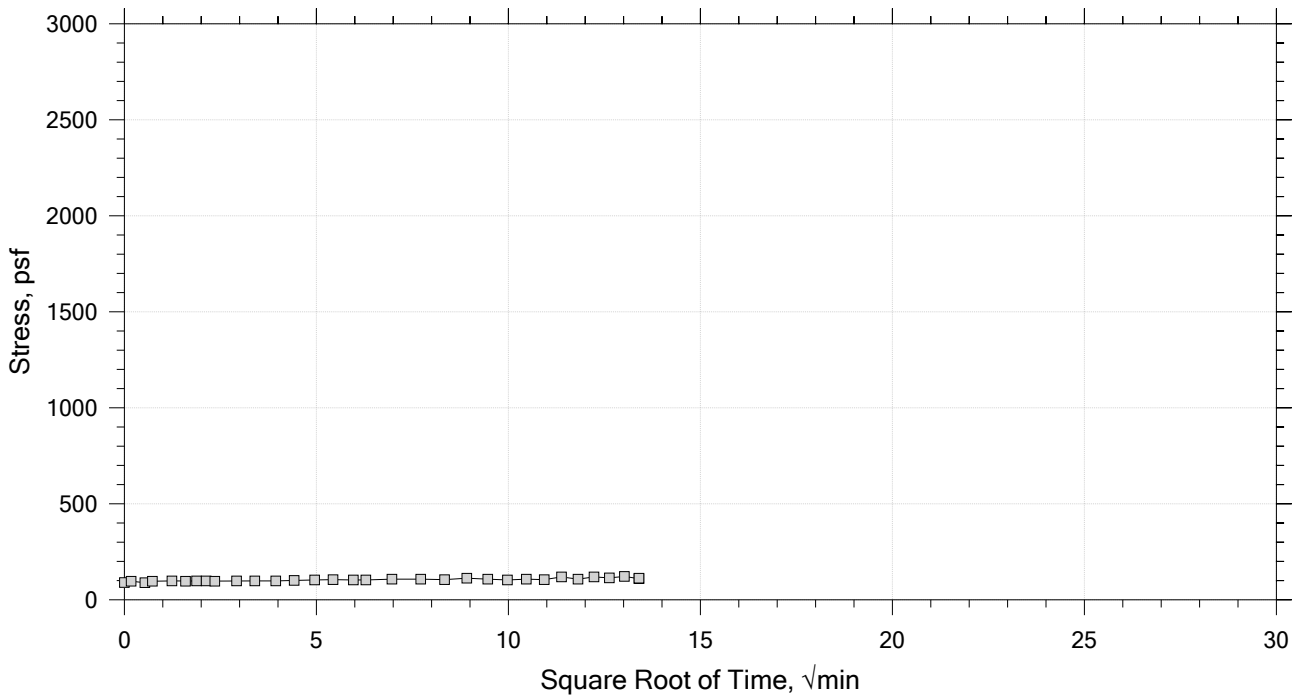
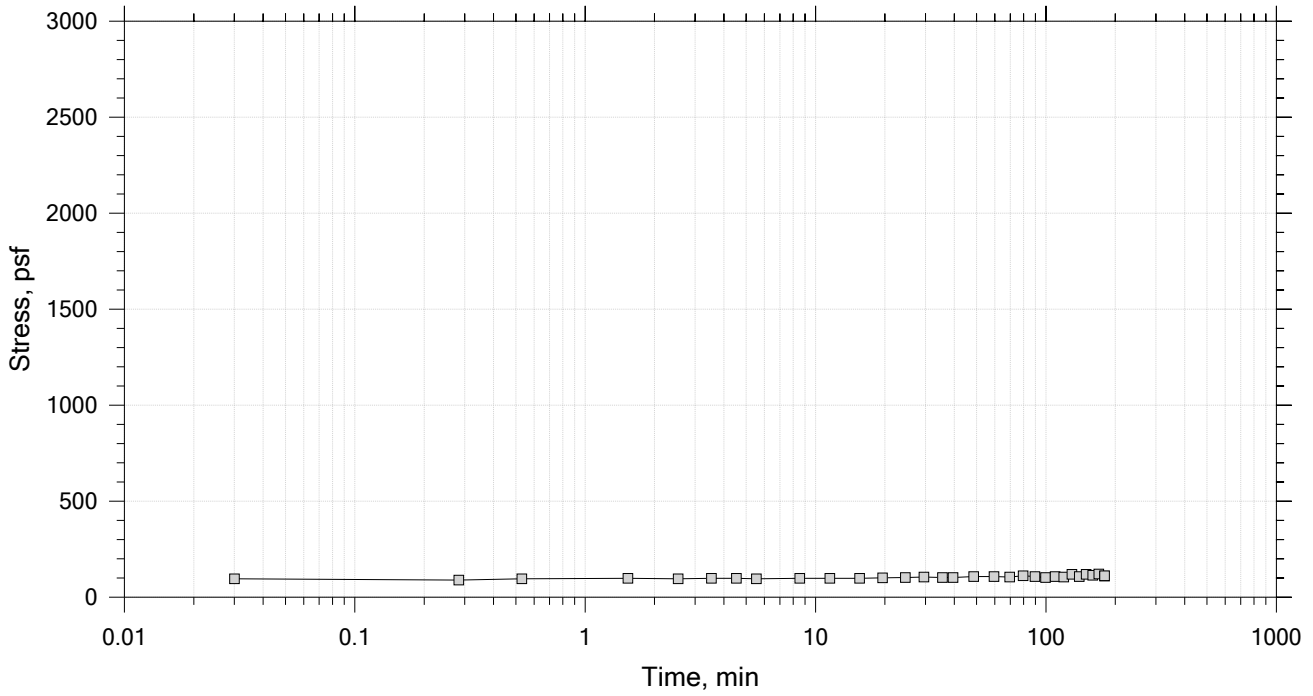
## Summary Report




 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-5	Tested By: jm	Checked By: mcm
	Sample No.: 8	Test Date: 10/12/20	Depth: 14-16 ft
	Test No.: IP-8	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay (CH)		

# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 1 of 12  
 Constant Volume Step  
 Stress: 112 psf



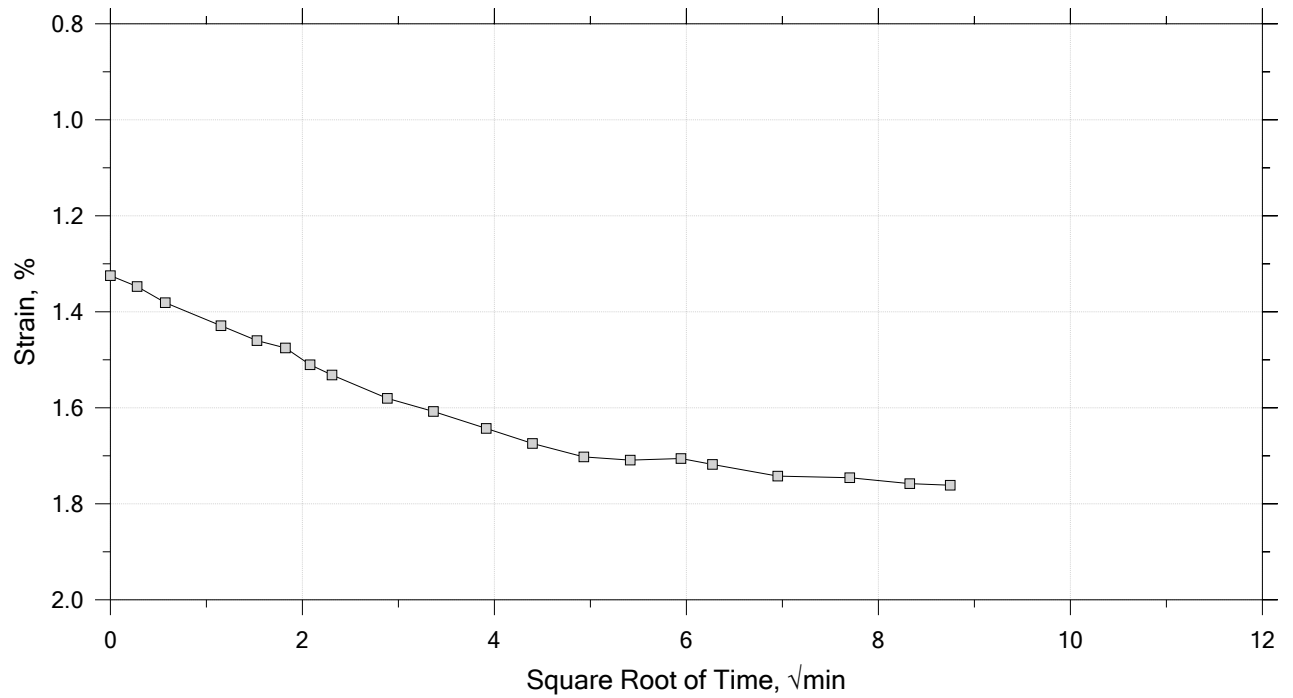
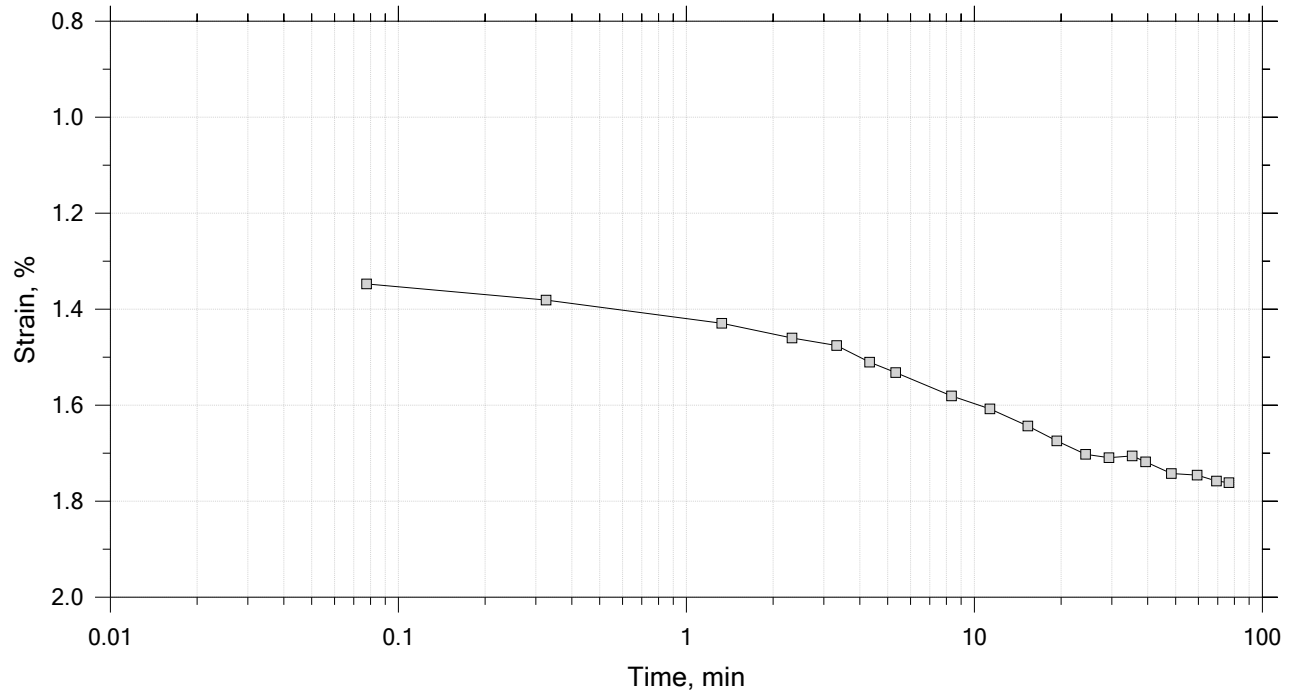
 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-5	Tested By: jm	Checked By: mcm
	Sample No.: 8	Test Date: 10/12/20	Depth: 14-16 ft
	Test No.: IP-8	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay(CH)		


# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 2 of 12

Constant Load Step

Stress: 250 psf

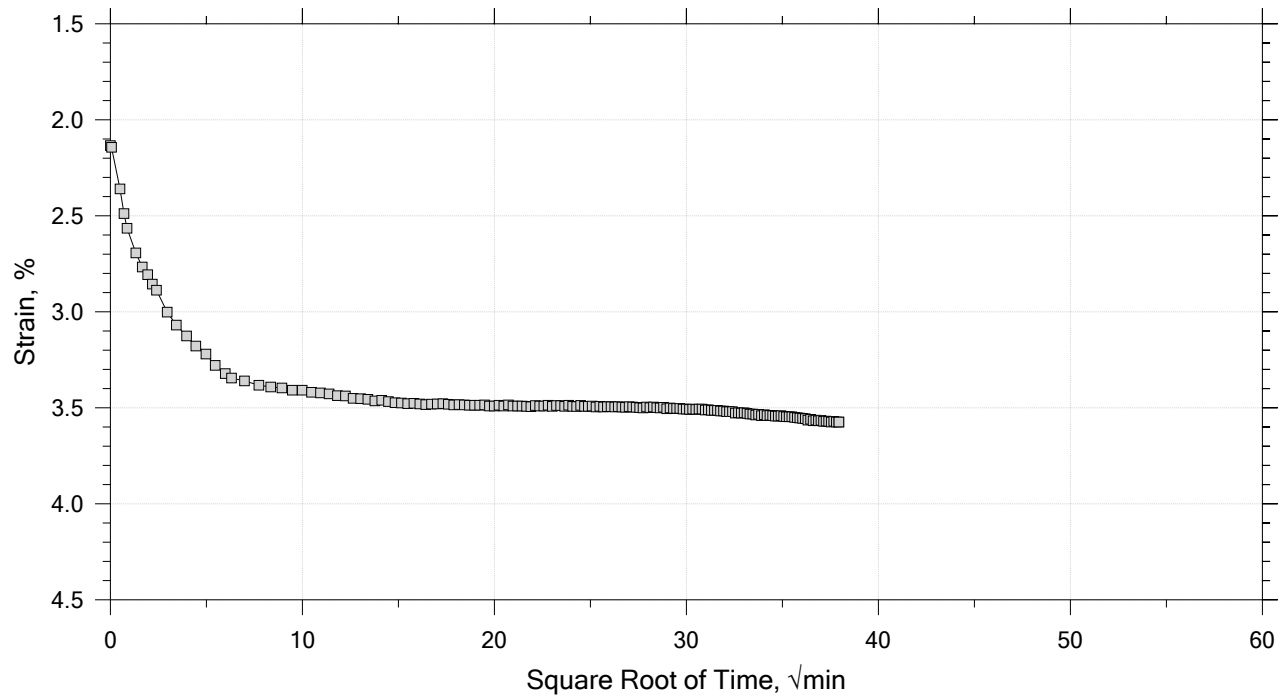
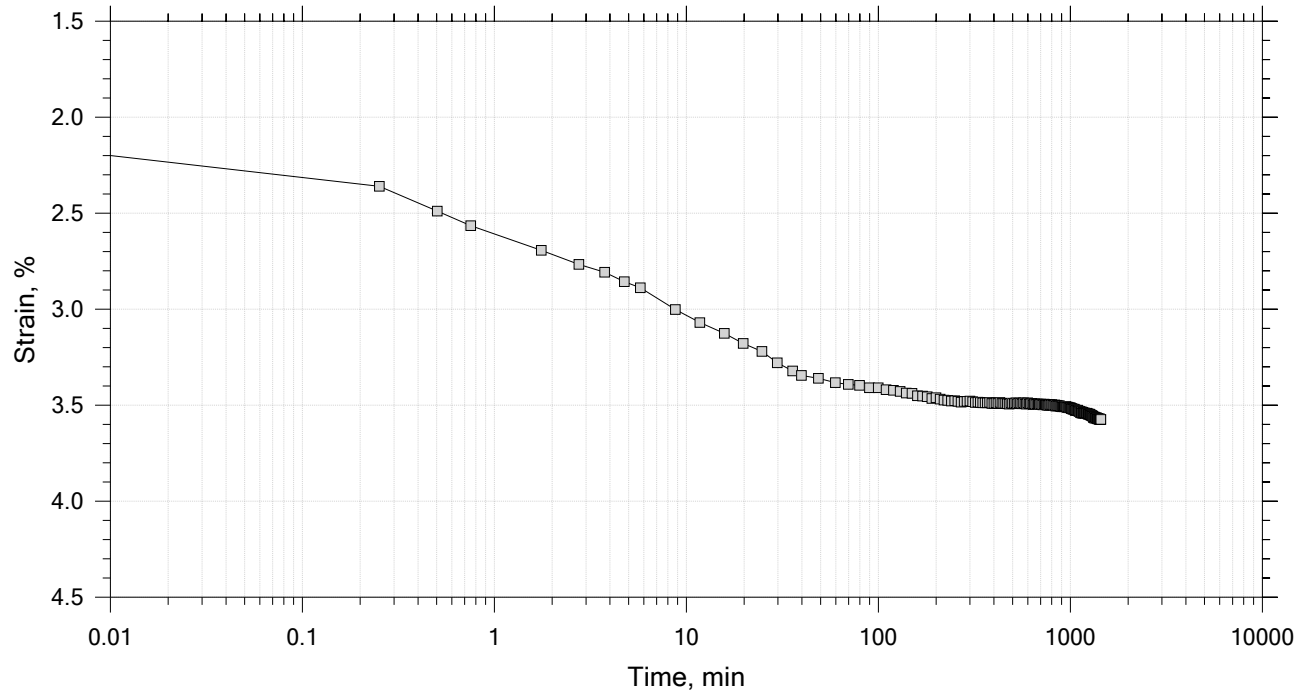



 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-5	Tested By: jm	Checked By: mcm
	Sample No.: 8	Test Date: 10/12/20	Depth: 14-16 ft
	Test No.: IP-8	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay(CH)		



# One-Dimensional Consolidation by ASTM D2435 - Method B

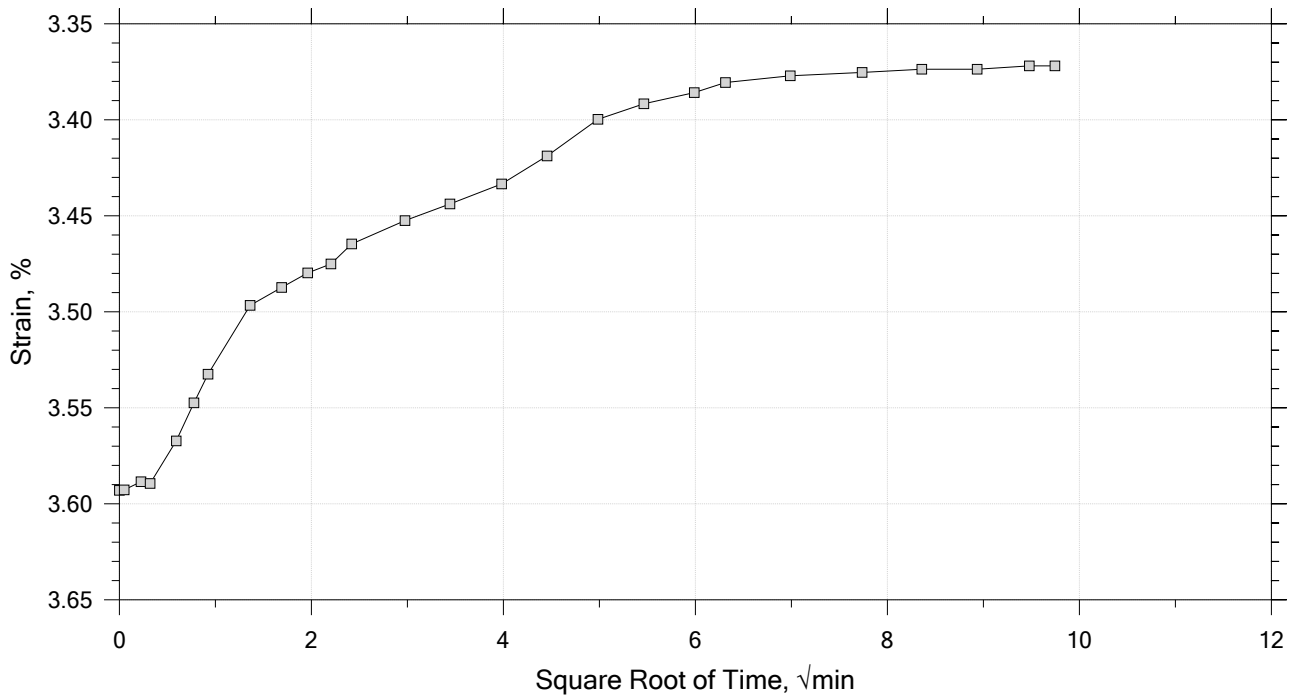
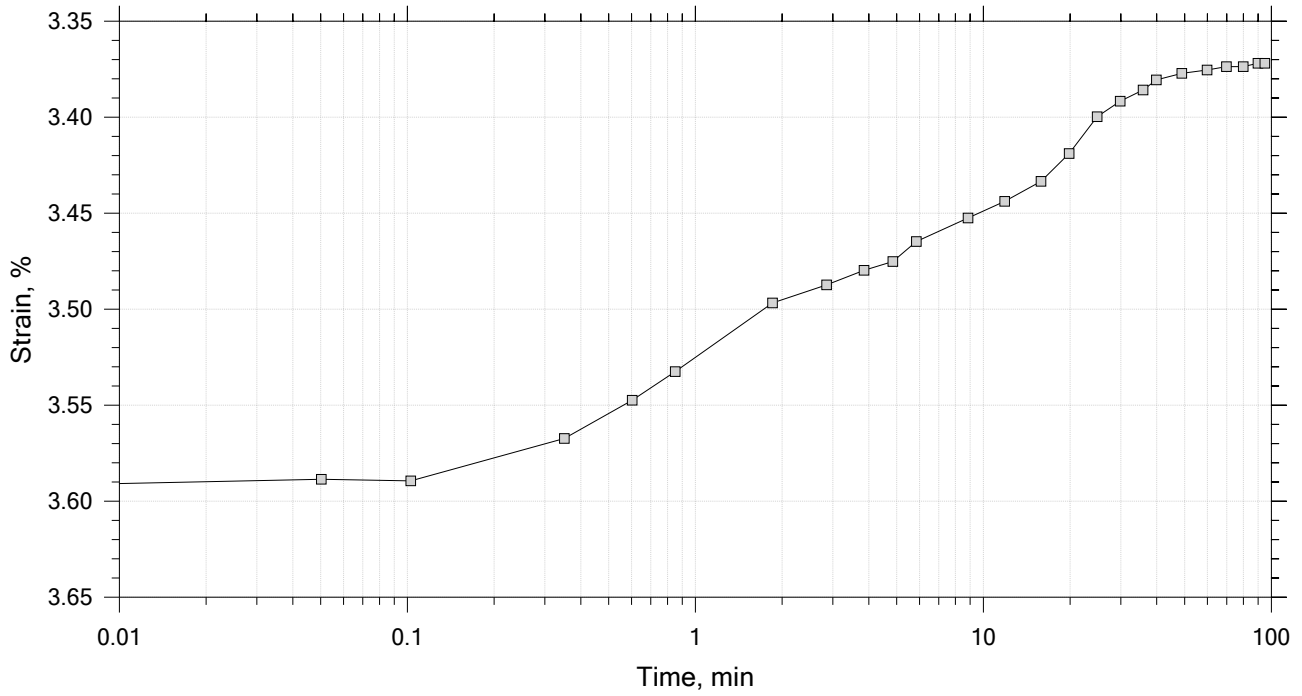
Time Curve 3 of 12  
 Constant Load Step  
 Stress: 500 psf




 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-5	Tested By: jm	Checked By: mcm
	Sample No.: 8	Test Date: 10/12/20	Depth: 14-16 ft
	Test No.: IP-8	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay(CH)		

# One-Dimensional Consolidation by ASTM D2435 - Method B

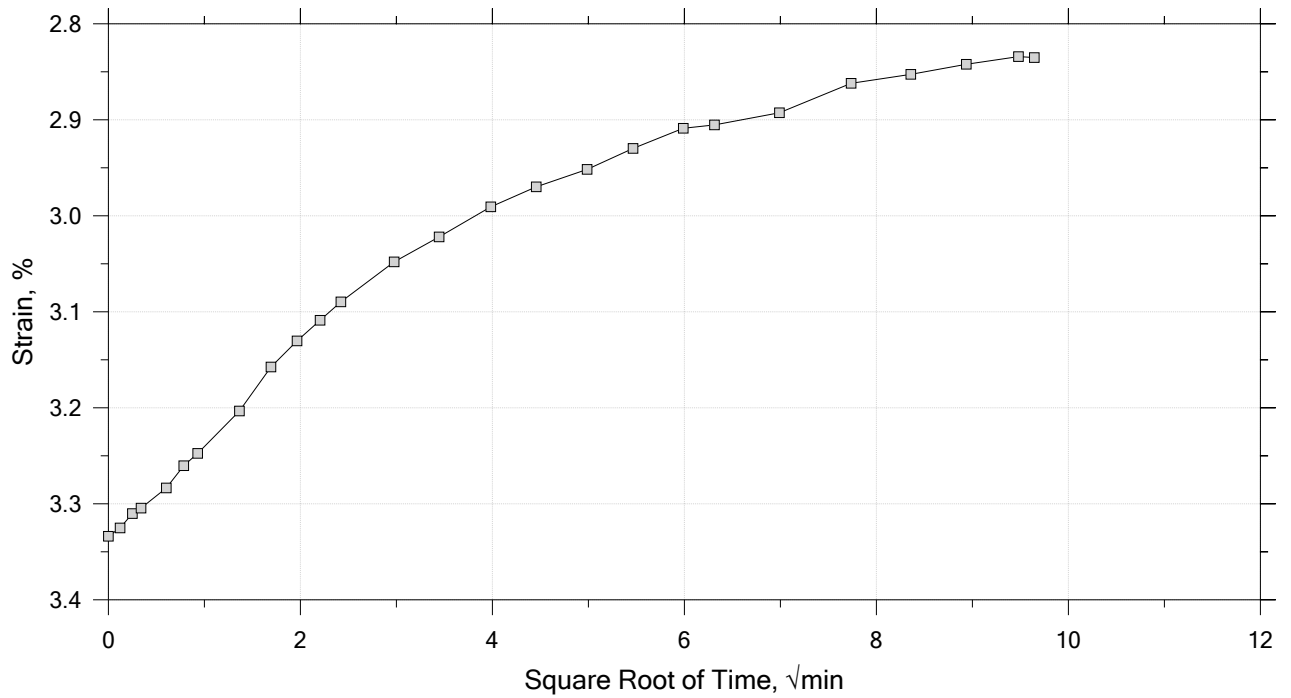
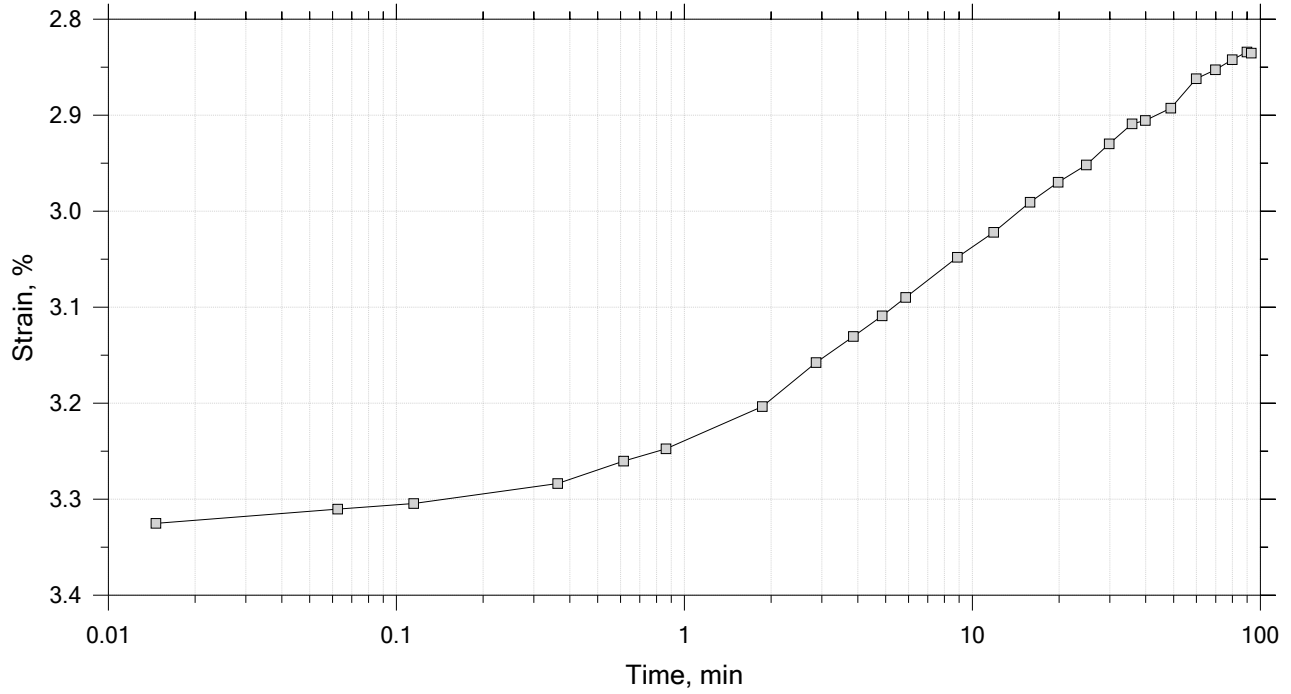
Time Curve 4 of 12  
 Constant Load Step  
 Stress: 250 psf




 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-5	Tested By: jm	Checked By: mcm
	Sample No.: 8	Test Date: 10/12/20	Depth: 14-16 ft
	Test No.: IP-8	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay(CH)		

# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 5 of 12  
 Constant Load Step  
 Stress: 100 psf



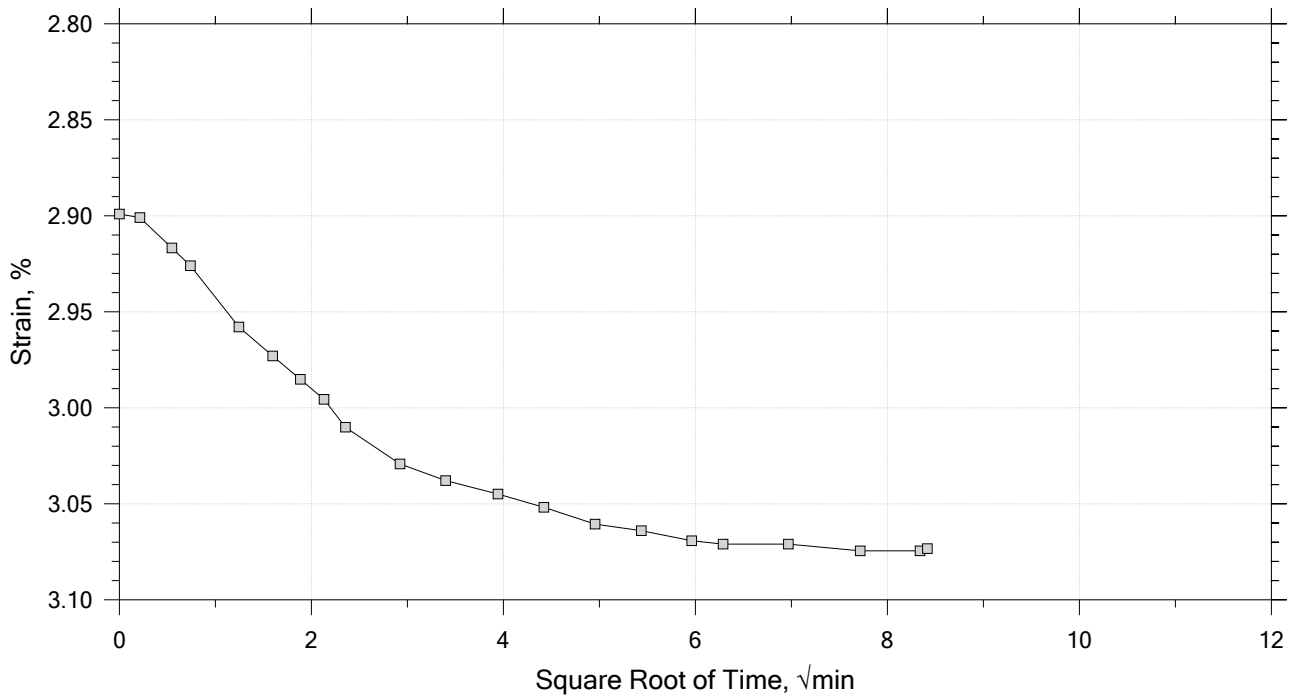
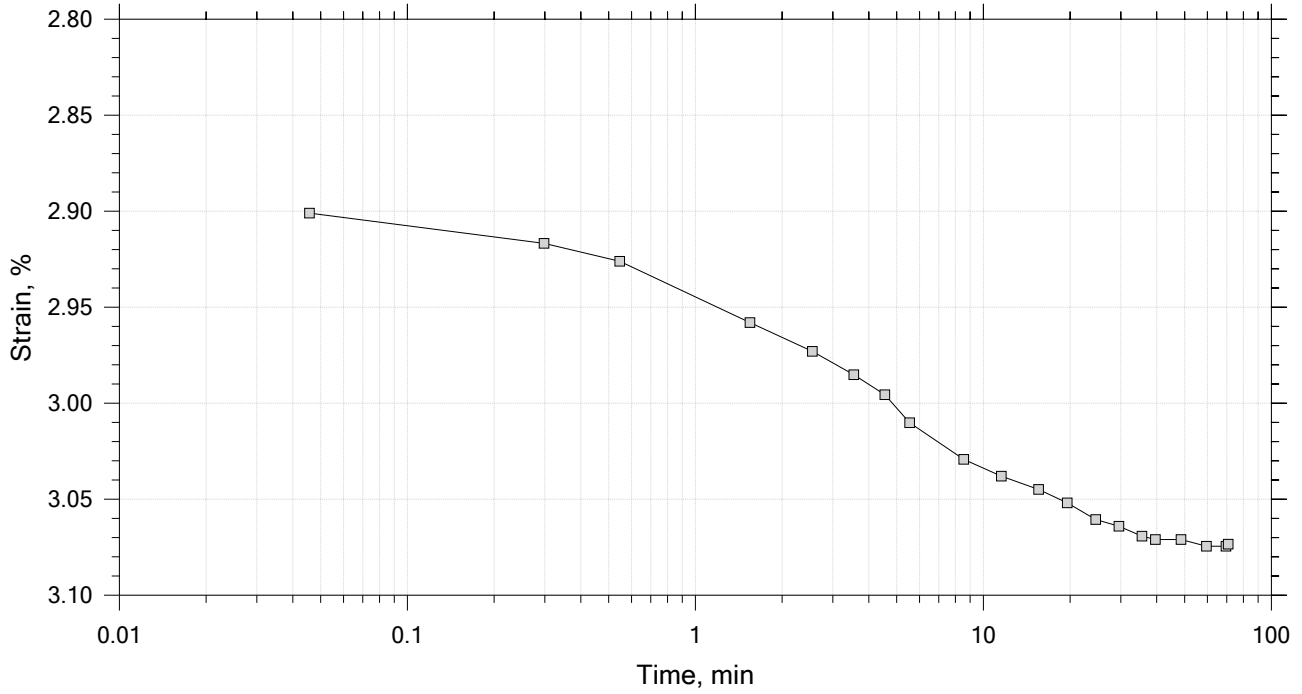
 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-5	Tested By: jm	Checked By: mcm
	Sample No.: 8	Test Date: 10/12/20	Depth: 14-16 ft
	Test No.: IP-8	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay(CH)		


# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 6 of 12

Constant Load Step

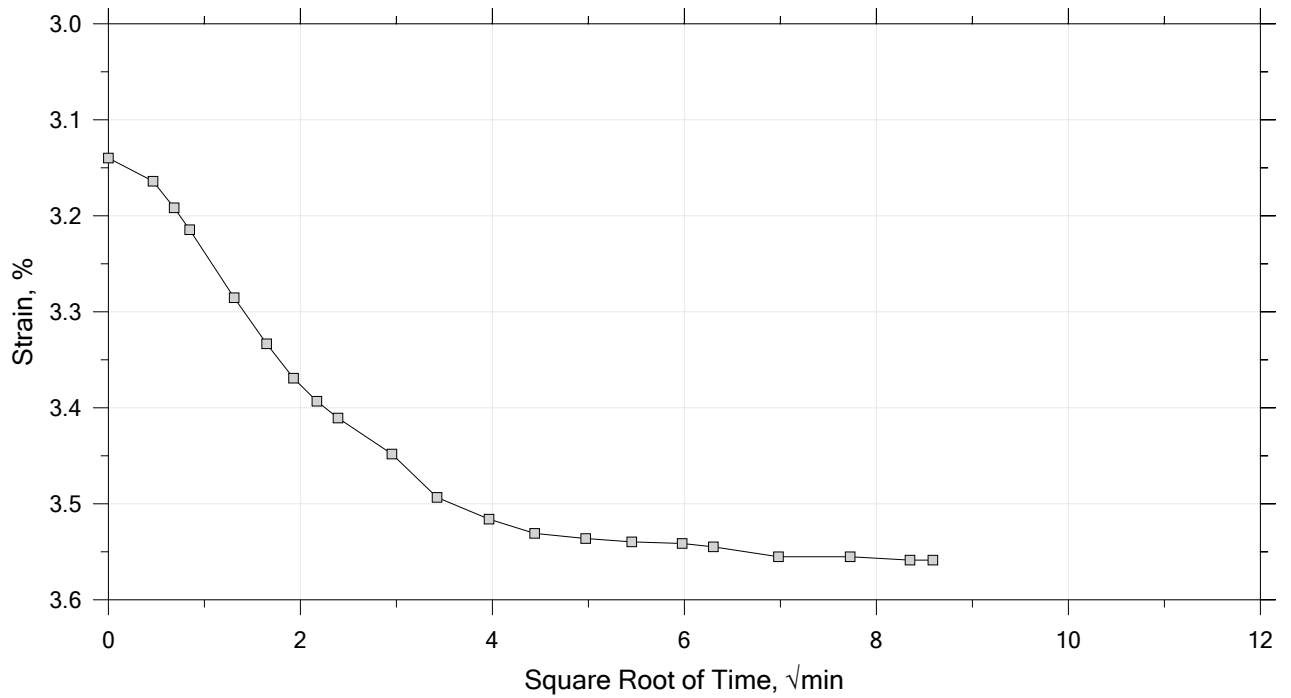
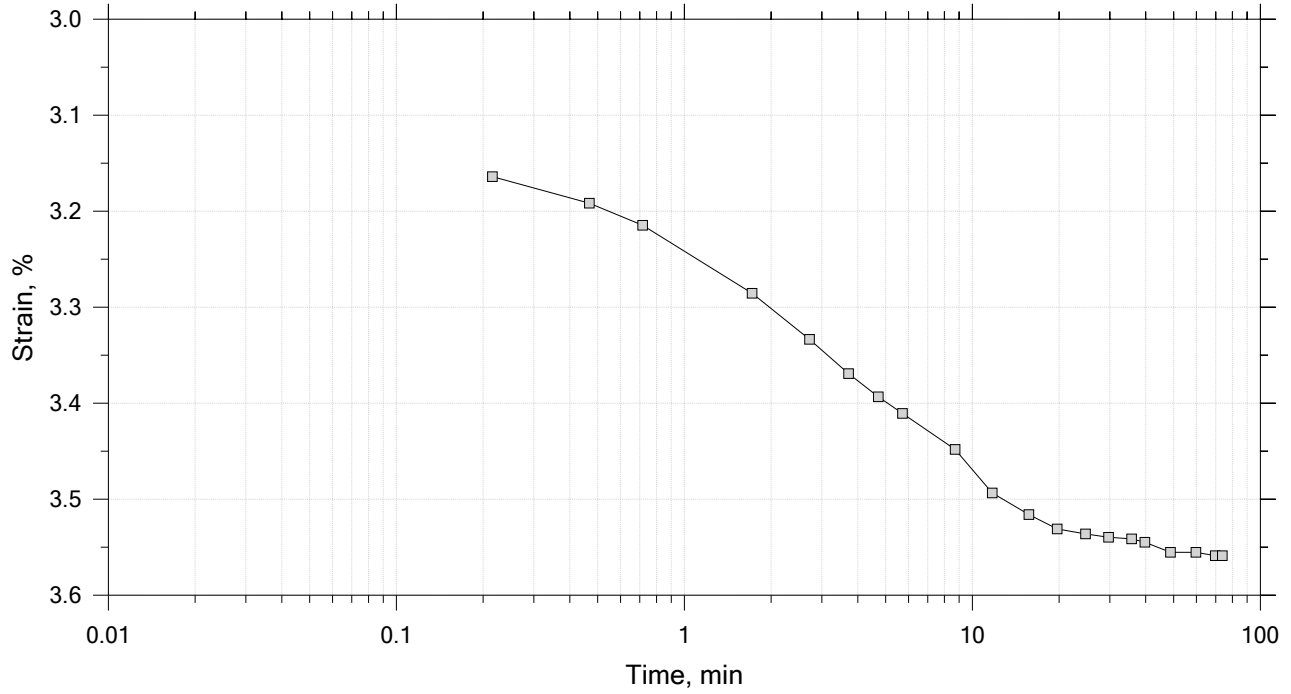
Stress: 250 psf




 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-5	Tested By: jm	Checked By: mcm
	Sample No.: 8	Test Date: 10/12/20	Depth: 14-16 ft
	Test No.: IP-8	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay		

# One-Dimensional Consolidation by ASTM D2435 - Method B

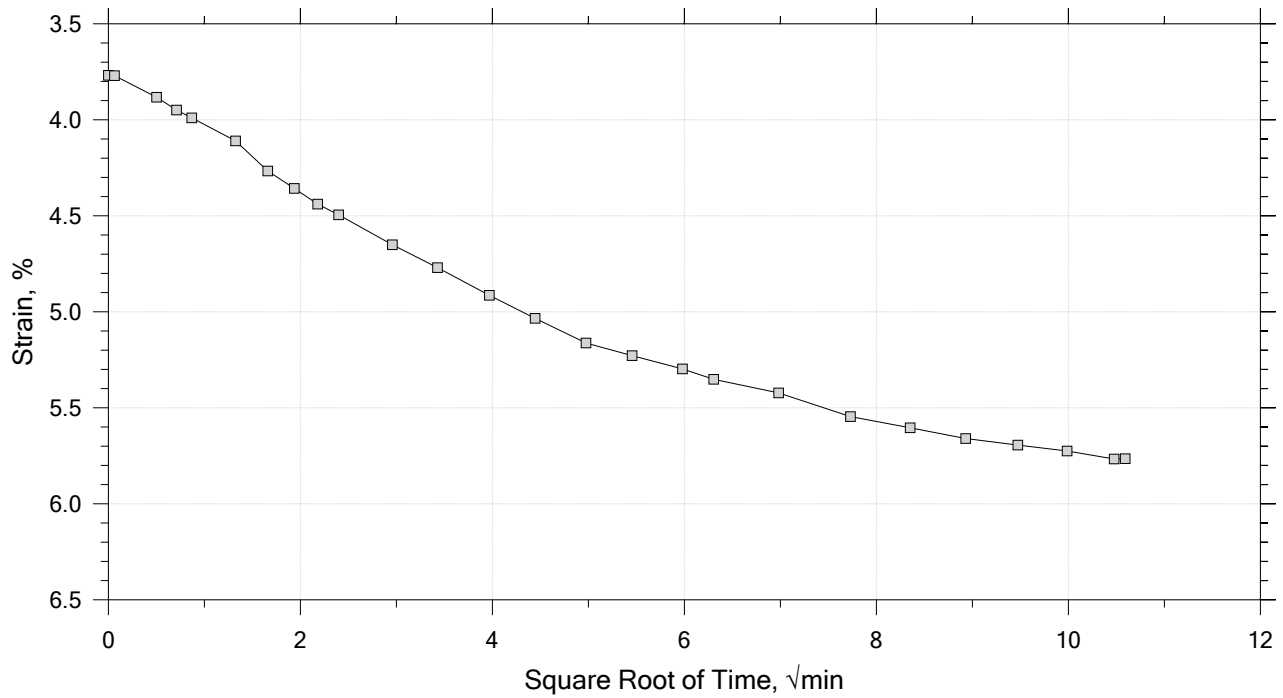
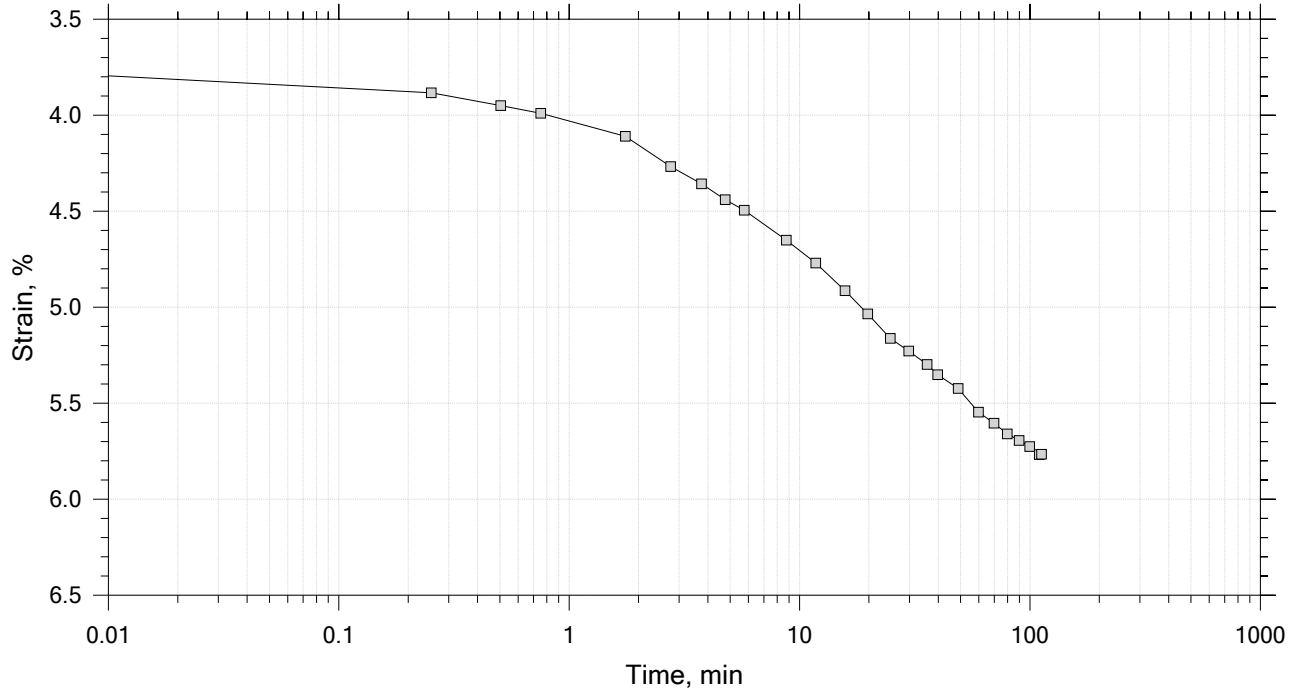
Time Curve 7 of 12  
 Constant Load Step  
 Stress: 500 psf




 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-5	Tested By: jm	Checked By: mcm
	Sample No.: 8	Test Date: 10/12/20	Depth: 14-16 ft
	Test No.: IP-8	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay(CH)		

# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 8 of 12  
 Constant Load Step  
 Stress: 1e+03 psf



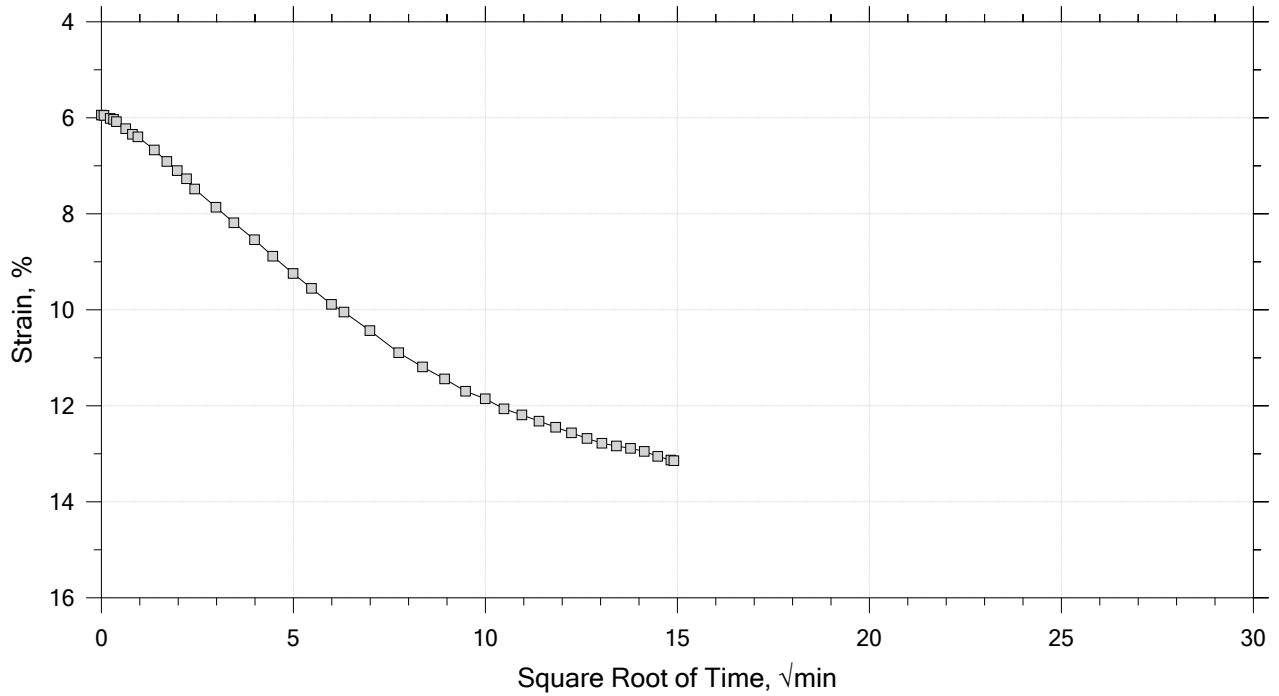
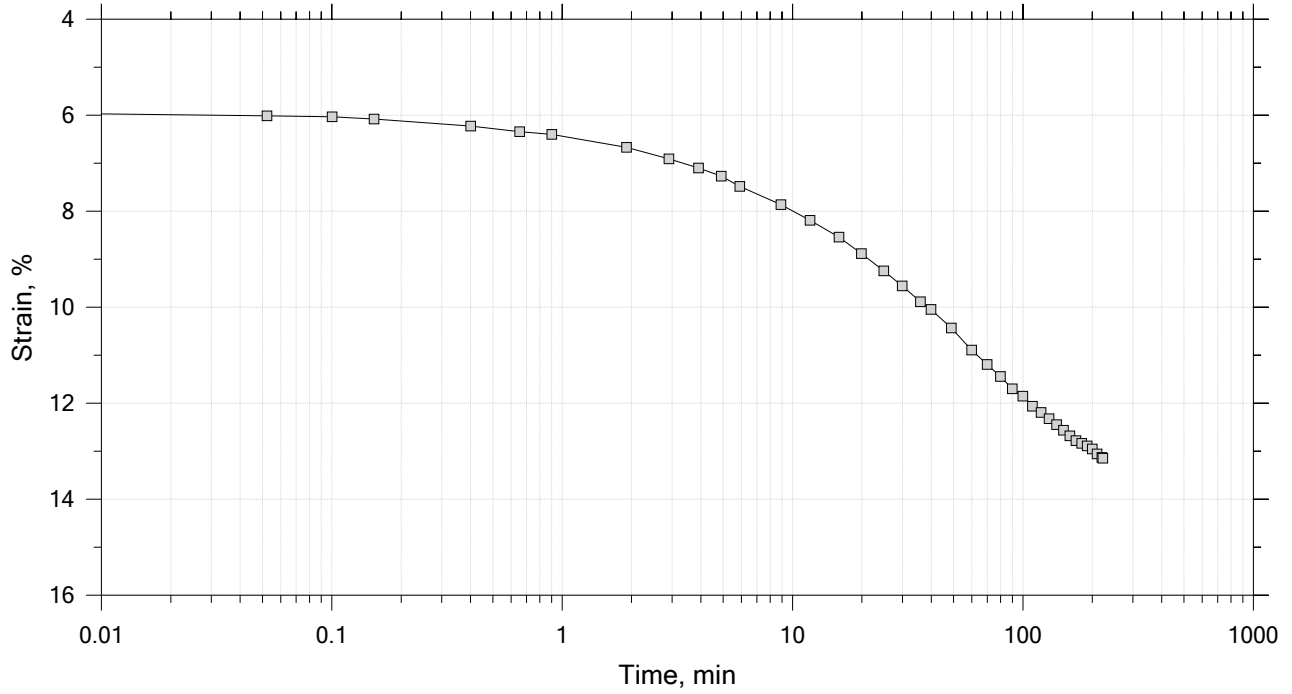
 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-5	Tested By: jm	Checked By: mcm
	Sample No.: 8	Test Date: 10/12/20	Depth: 14-16 ft
	Test No.: IP-8	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay(CH)		


# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 9 of 12

Constant Load Step

Stress: 2e+03 psf



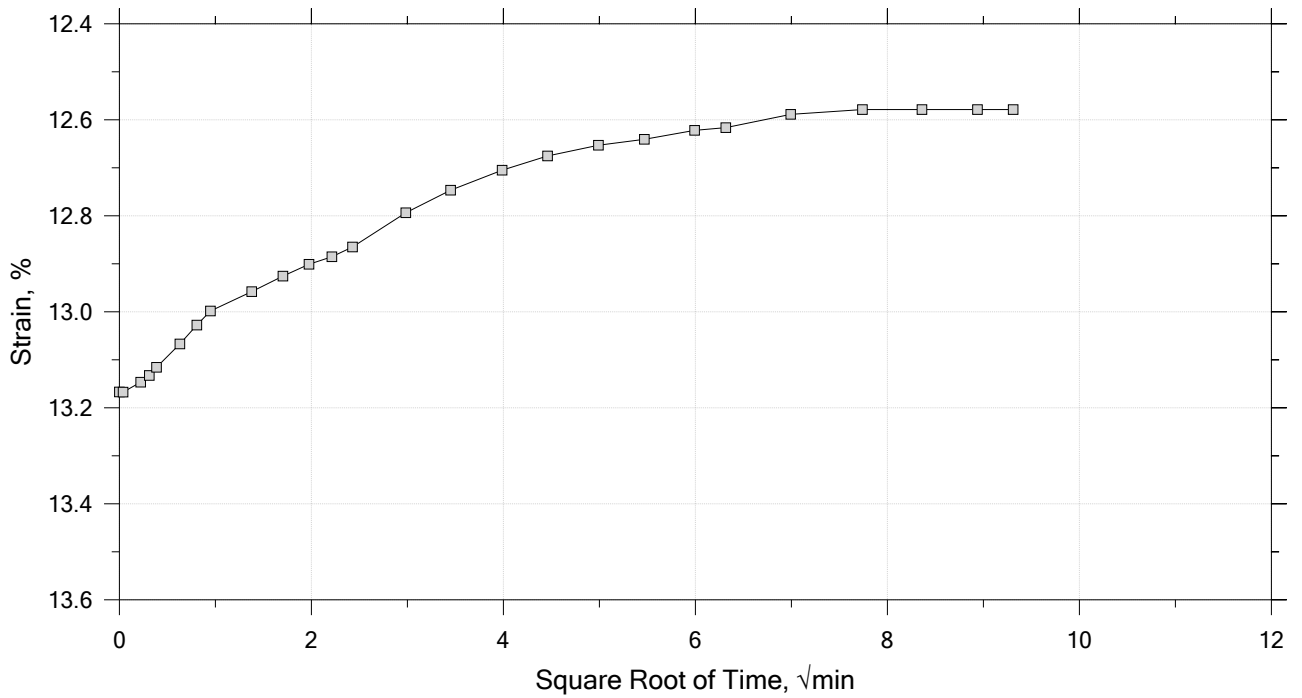
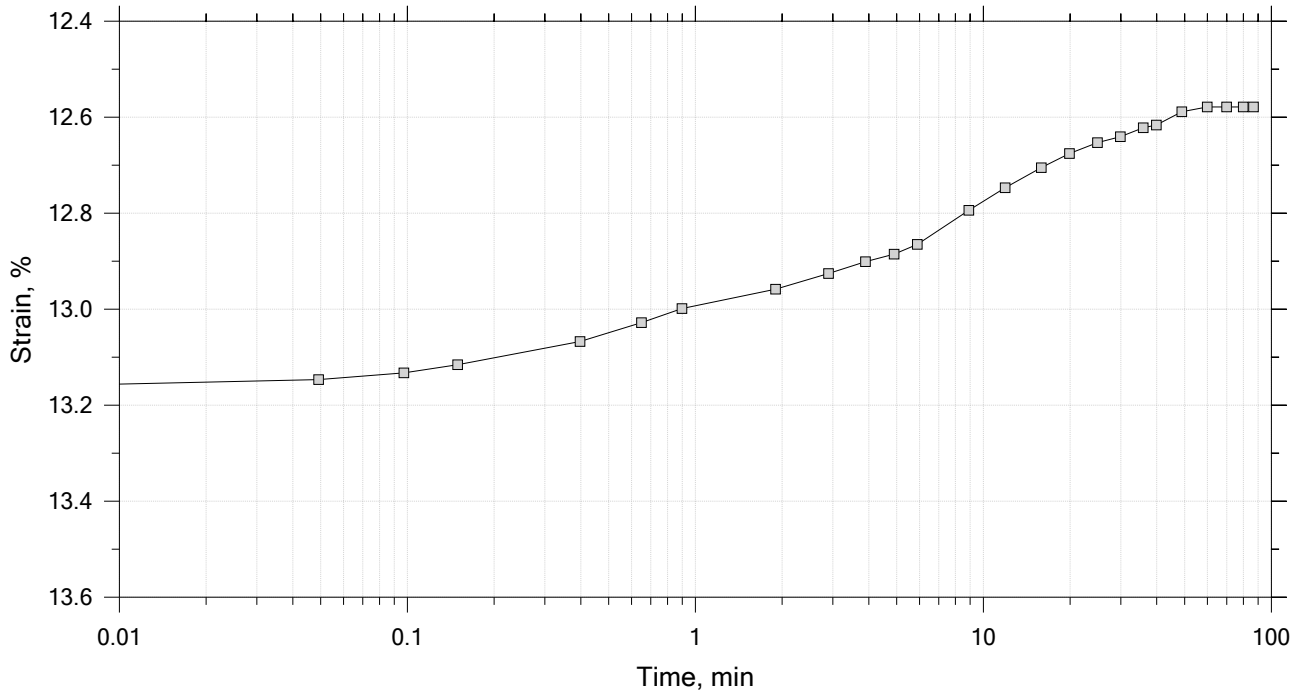
 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-5	Tested By: jm	Checked By: mcm
	Sample No.: 8	Test Date: 10/12/20	Depth: 14-16 ft
	Test No.: IP-8	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay(CH)		


# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 10 of 12

Constant Load Step

Stress: 1e+03 psf



 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-5	Tested By: jm	Checked By: mcm
	Sample No.: 8	Test Date: 10/12/20	Depth: 14-16 ft
	Test No.: IP-8	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay(CH)		

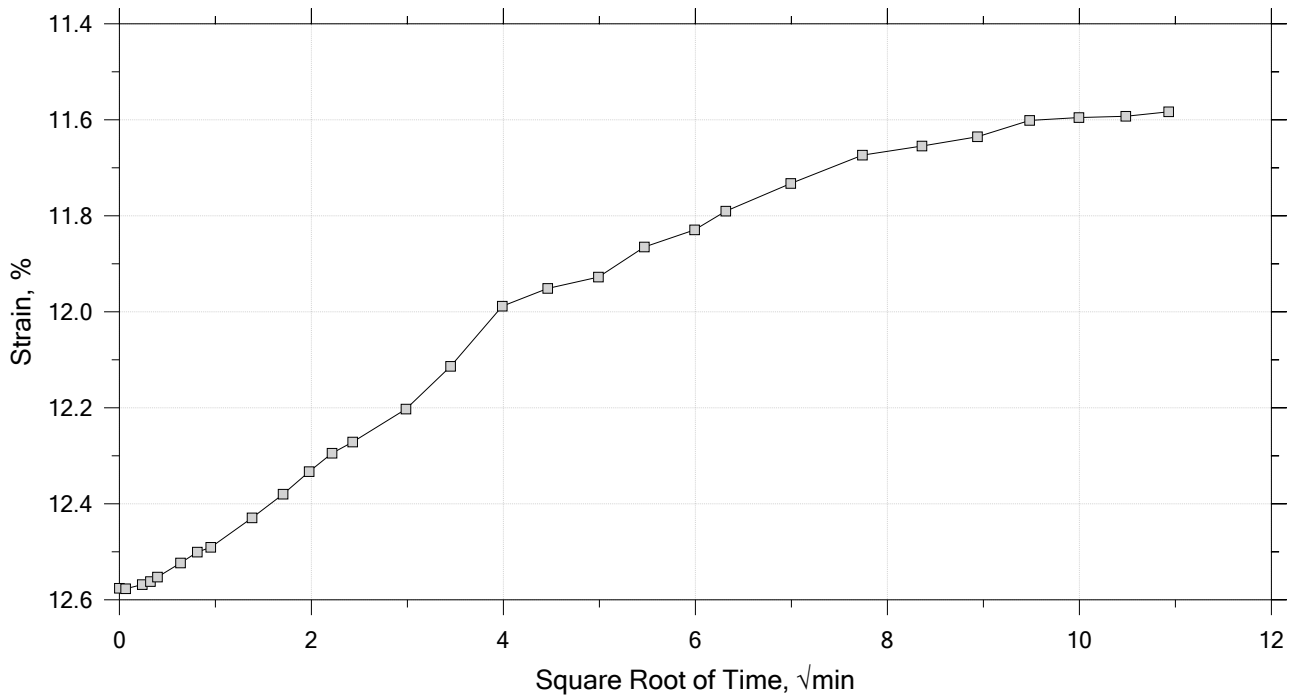
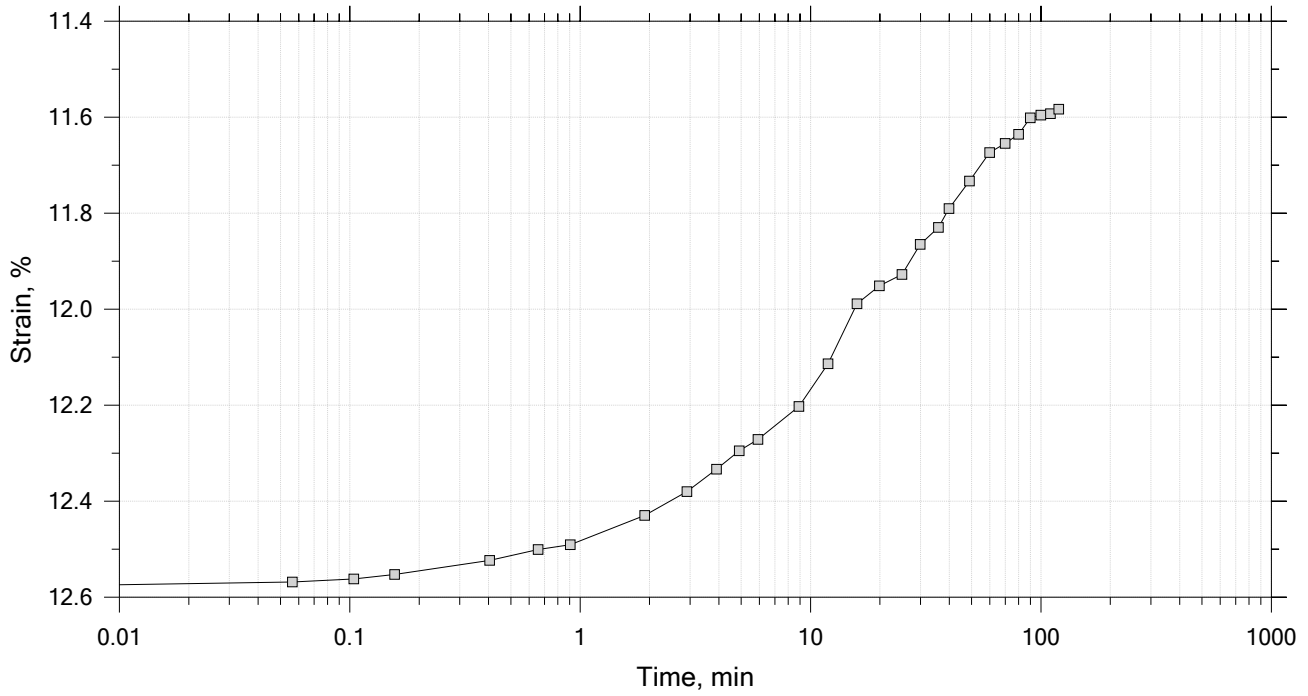



# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 11 of 12

Constant Load Step

Stress: 500 psf



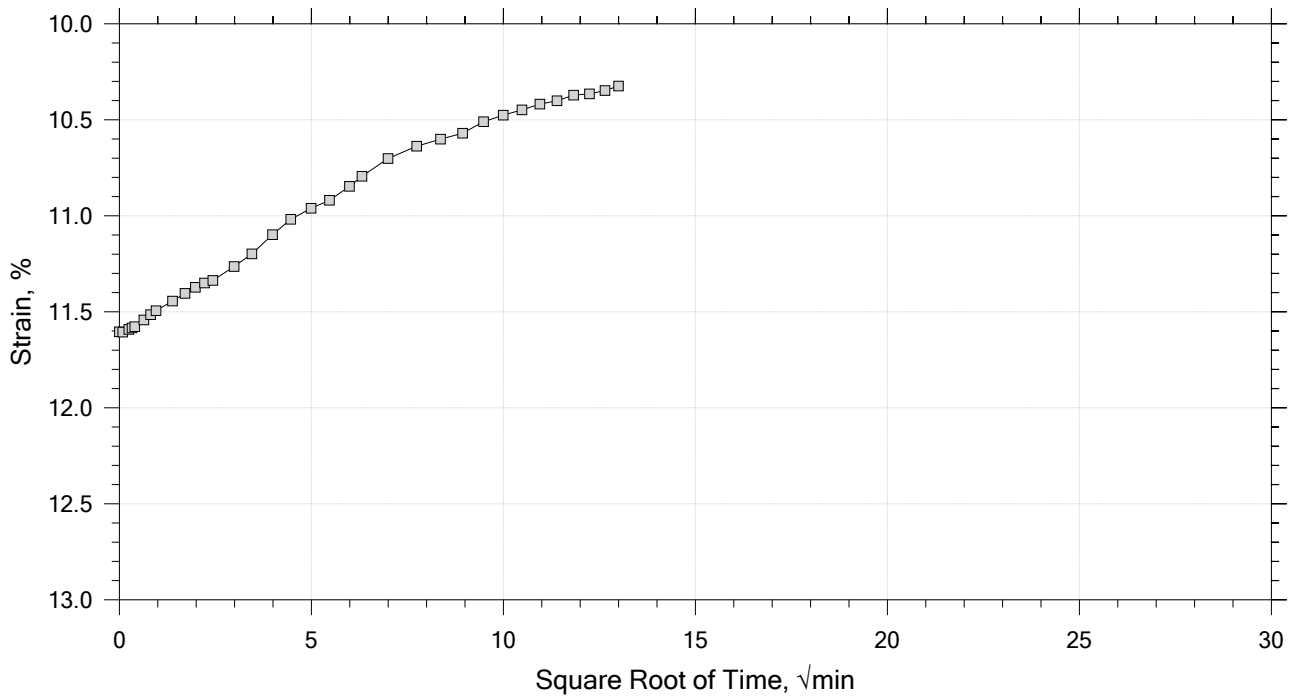
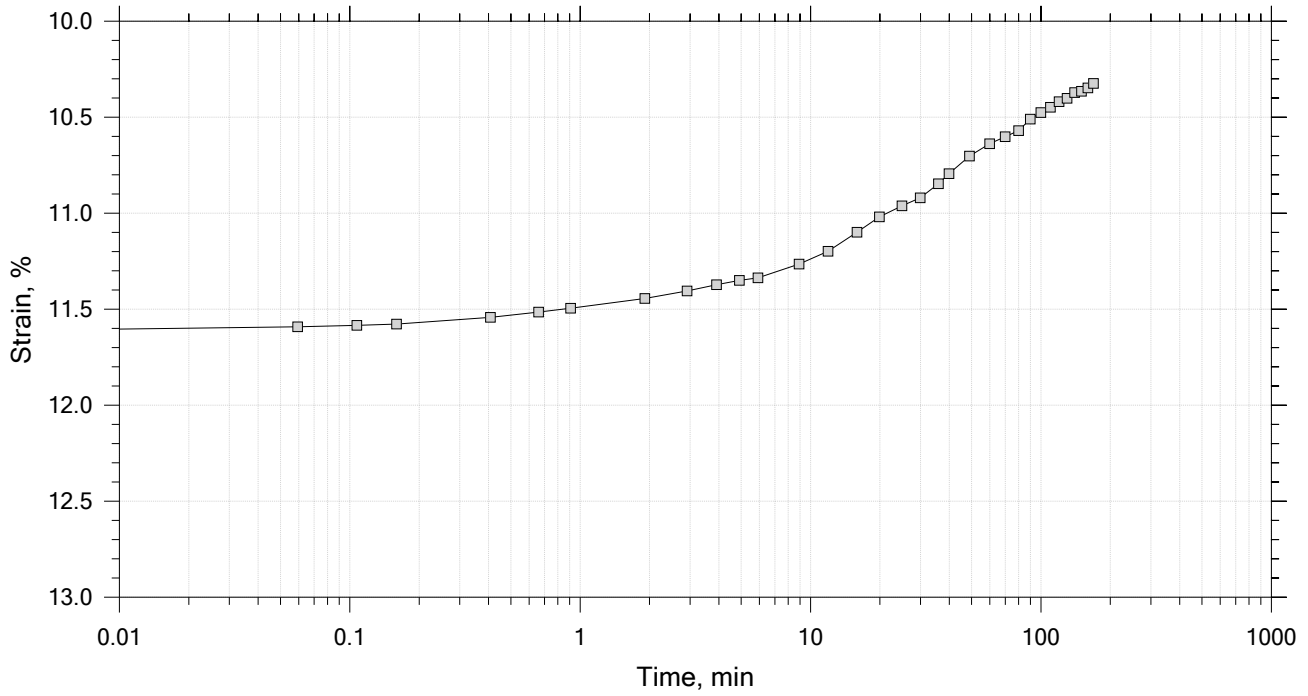
 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-5	Tested By: jm	Checked By: mcm
	Sample No.: 8	Test Date: 10/12/20	Depth: 14-16 ft
	Test No.: IP-8	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay(CH)		


# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 12 of 12

Constant Load Step

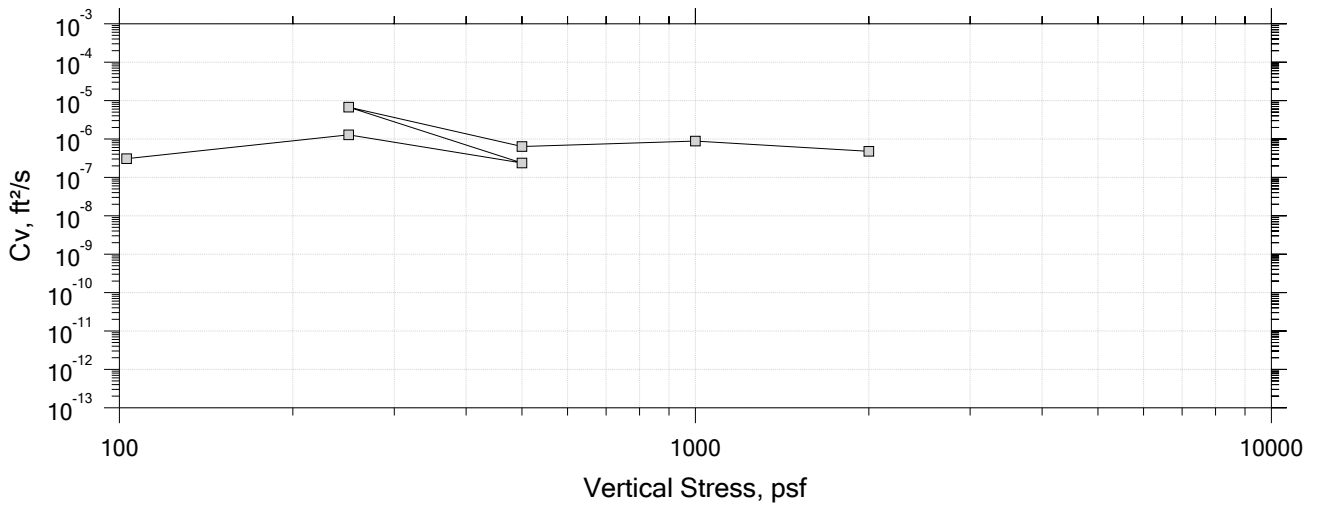
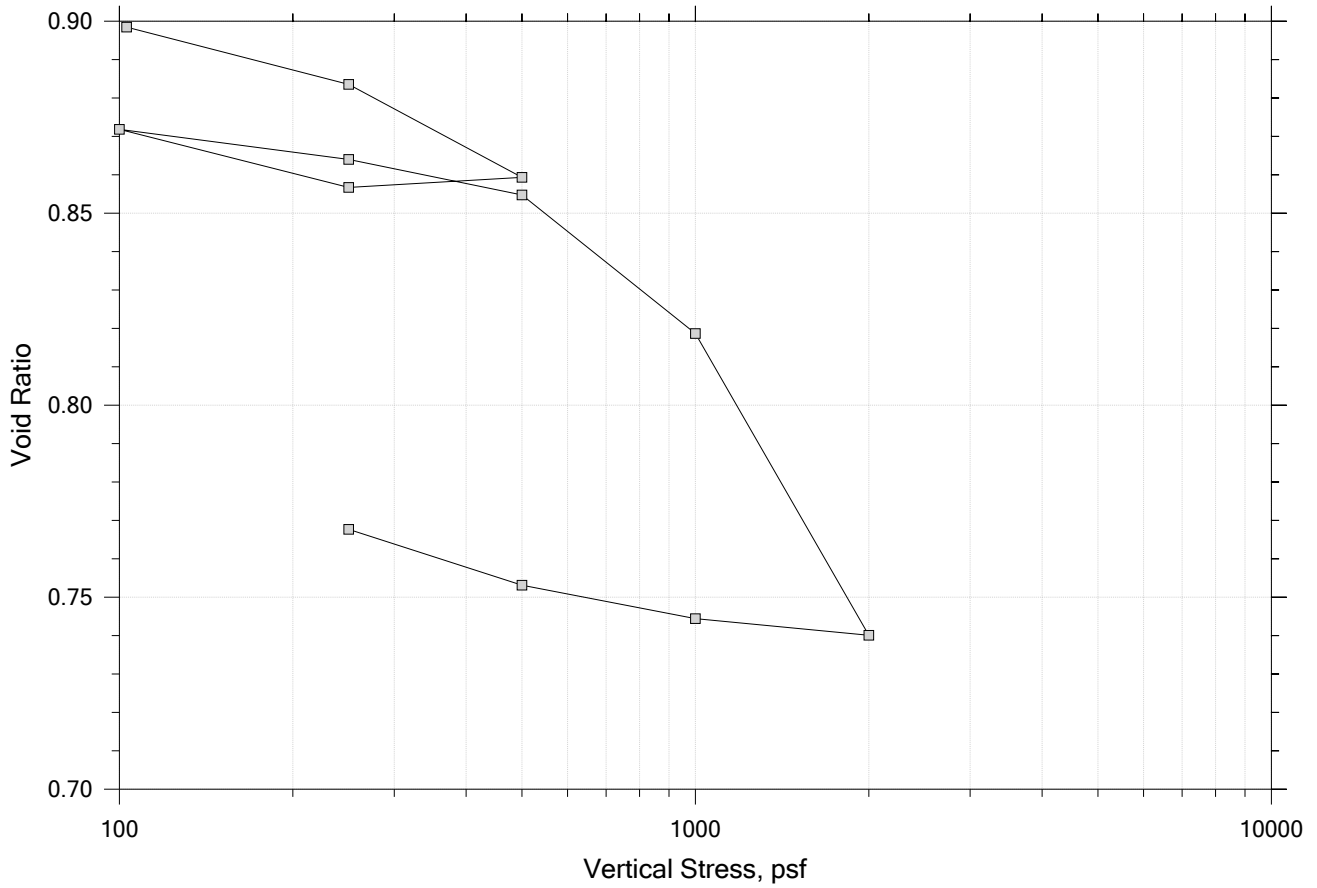
Stress: 250 psf




 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-5	Tested By: jm	Checked By: mcm
	Sample No.: 8	Test Date: 10/12/20	Depth: 14-16 ft
	Test No.: IP-8	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay(CH)		

# One-Dimensional Consolidation by ASTM D2435 - Method B

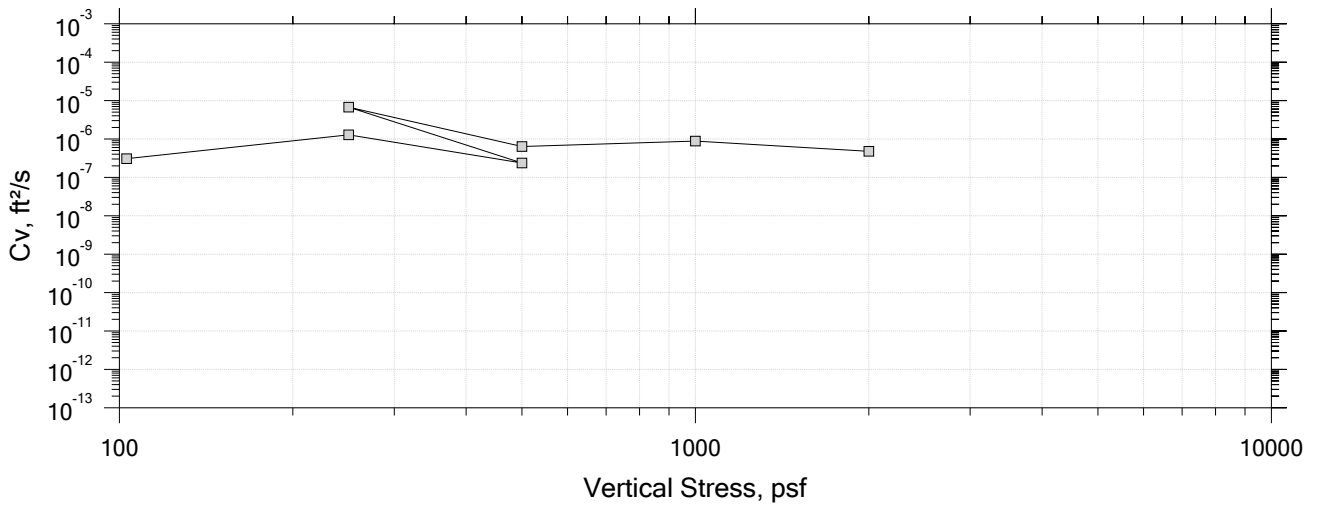
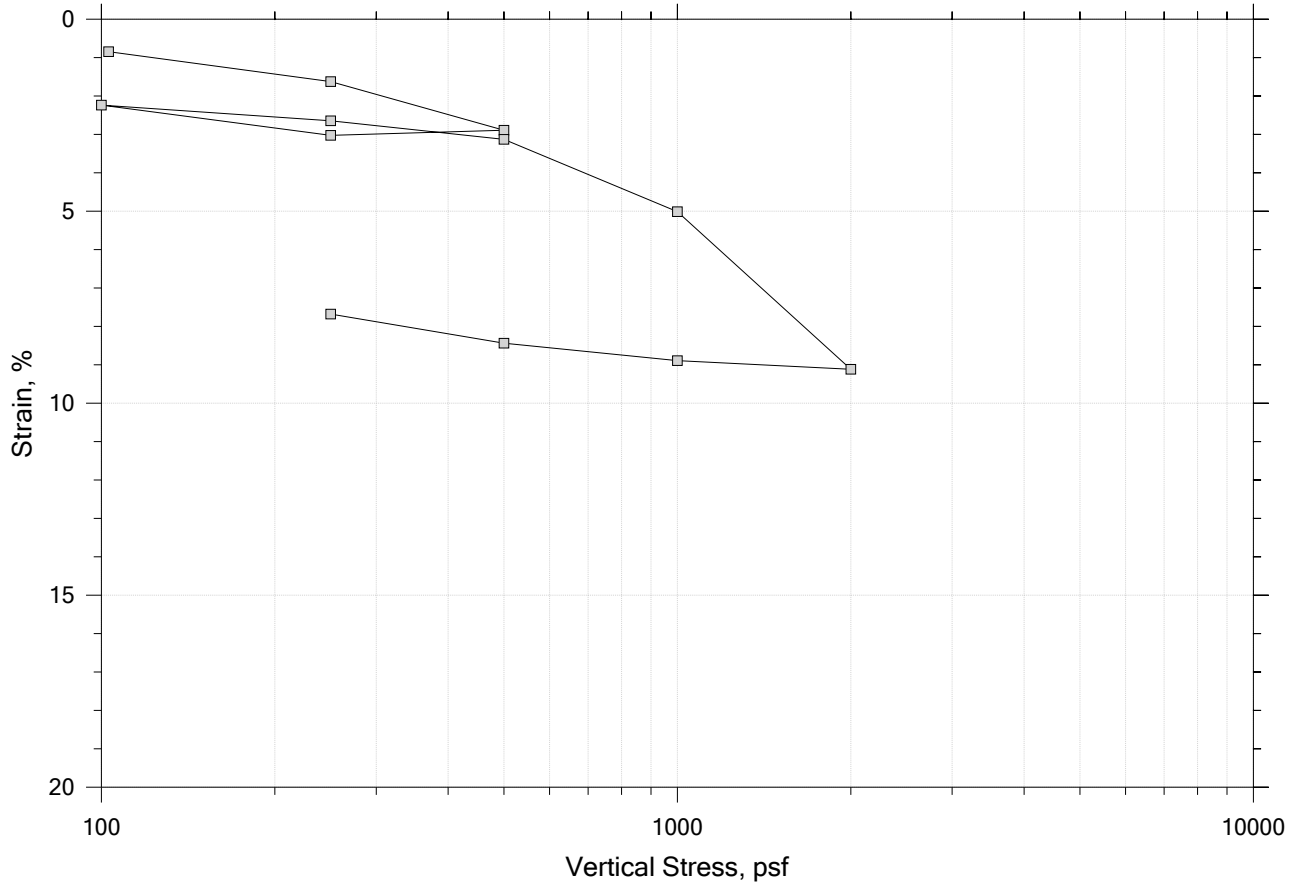
## Summary Report




 <b>APS</b> Engineering and Testing	Project: Breton Lakebridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-5	Tested By: jm	Checked By: mcm
	Sample No.: 10	Test Date: 10/10/20	Depth: 18-20 ft
	Test No.: IP-9	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay(CH)	Measured specific gravity: 2.56	

# One-Dimensional Consolidation by ASTM D2435 - Method B

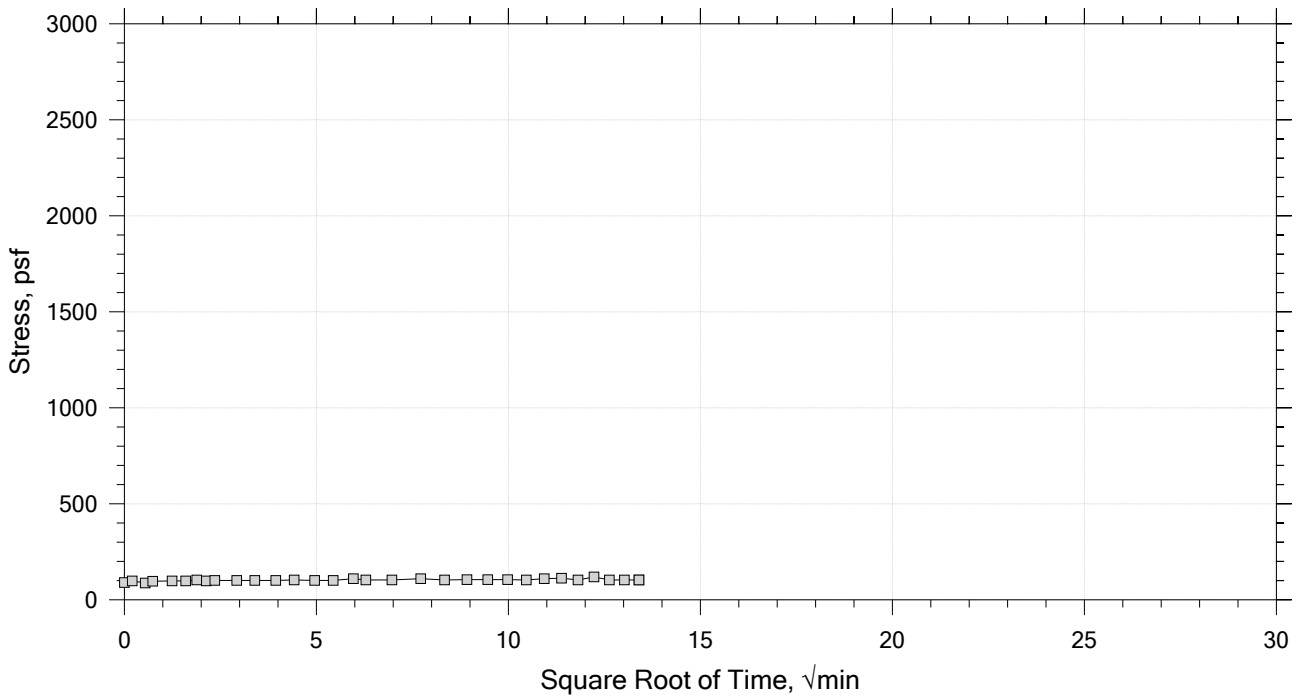
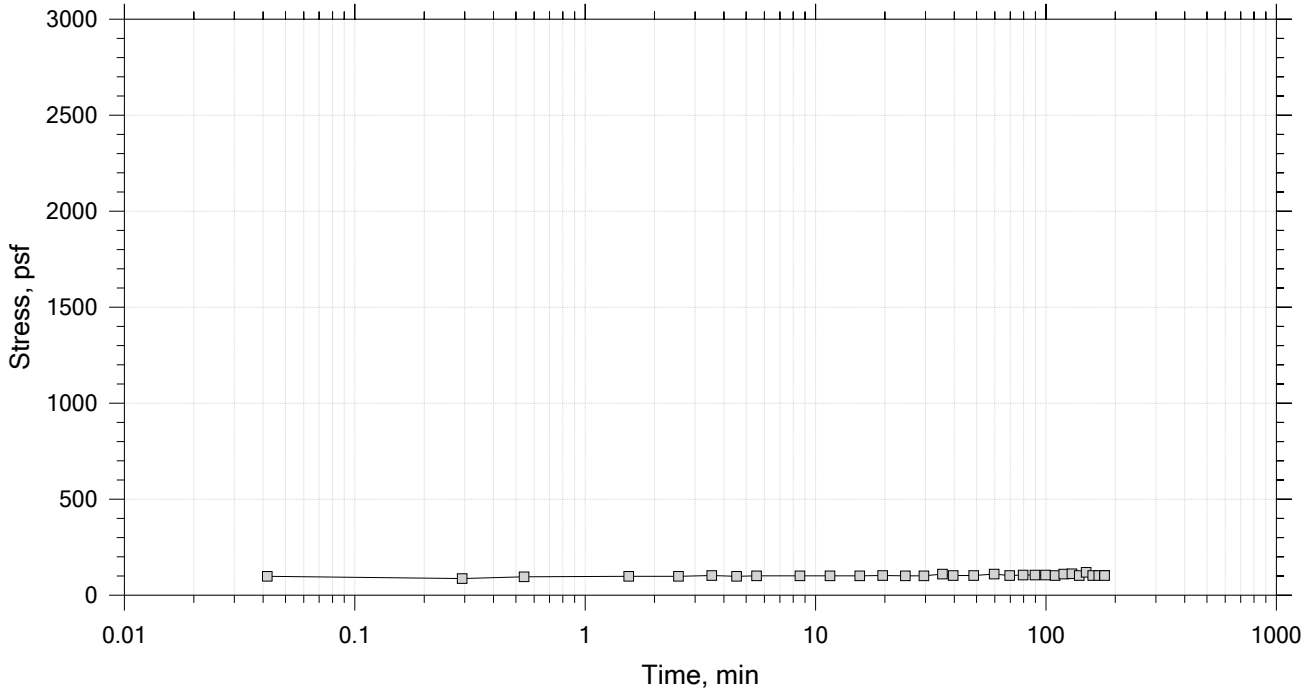
## Summary Report




 <p>APS Engineering and Testing</p>	Project: Breton Lakebridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-5	Tested By: jm	Checked By: mcm
	Sample No.: 10	Test Date: 10/10/20	Depth: 18-20 ft
	Test No.: IP-9	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay (CH)		

# One-Dimensional Consolidation by ASTM D2435 - Method B

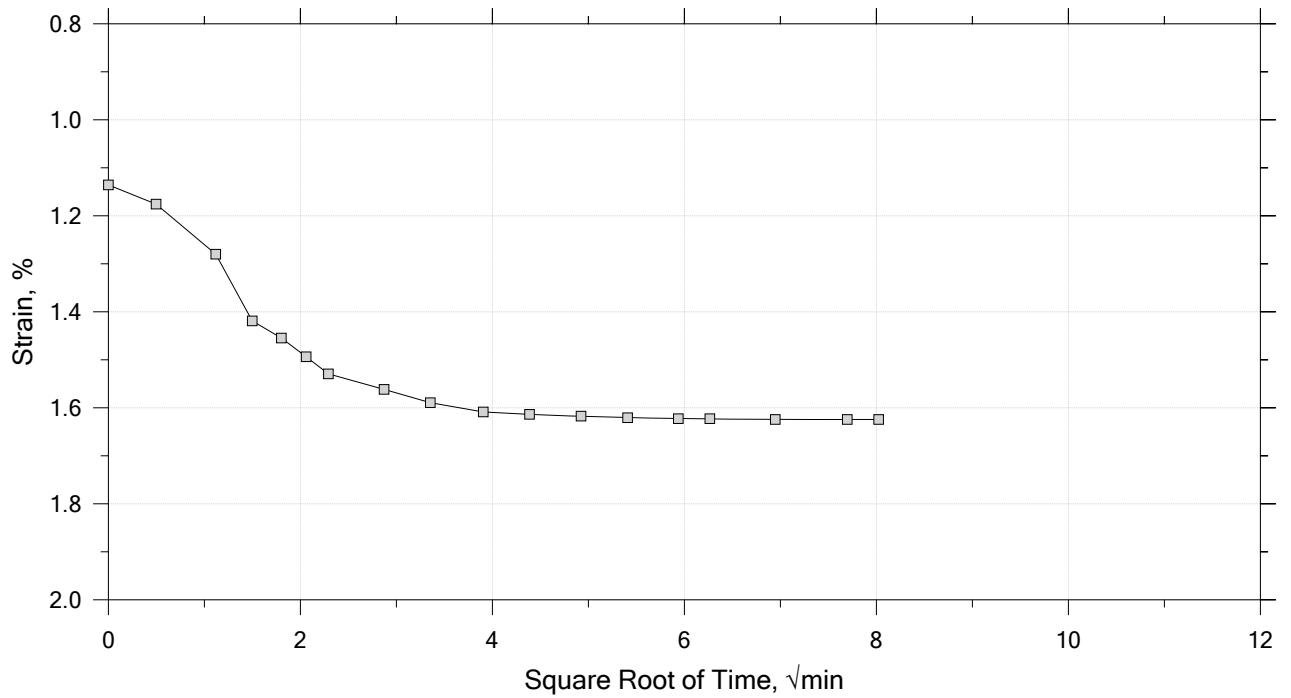
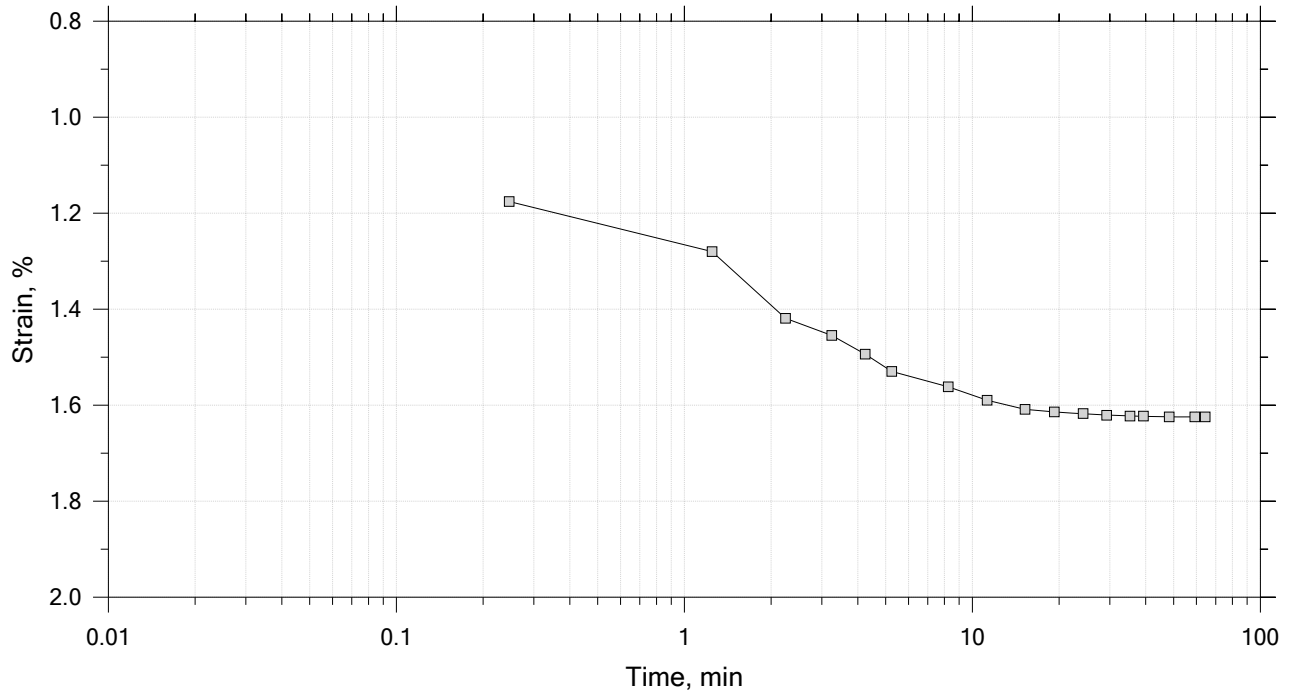
Time Curve 1 of 12  
 Constant Volume Step  
 Stress: 103 psf




 Engineering and Testing	Project: Breton Lakebridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-5	Tested By: jm	Checked By: mcm
	Sample No.: 10	Test Date: 10/10/20	Depth: 18-20 ft
	Test No.: IP-9	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay(CH)		

# One-Dimensional Consolidation by ASTM D2435 - Method B

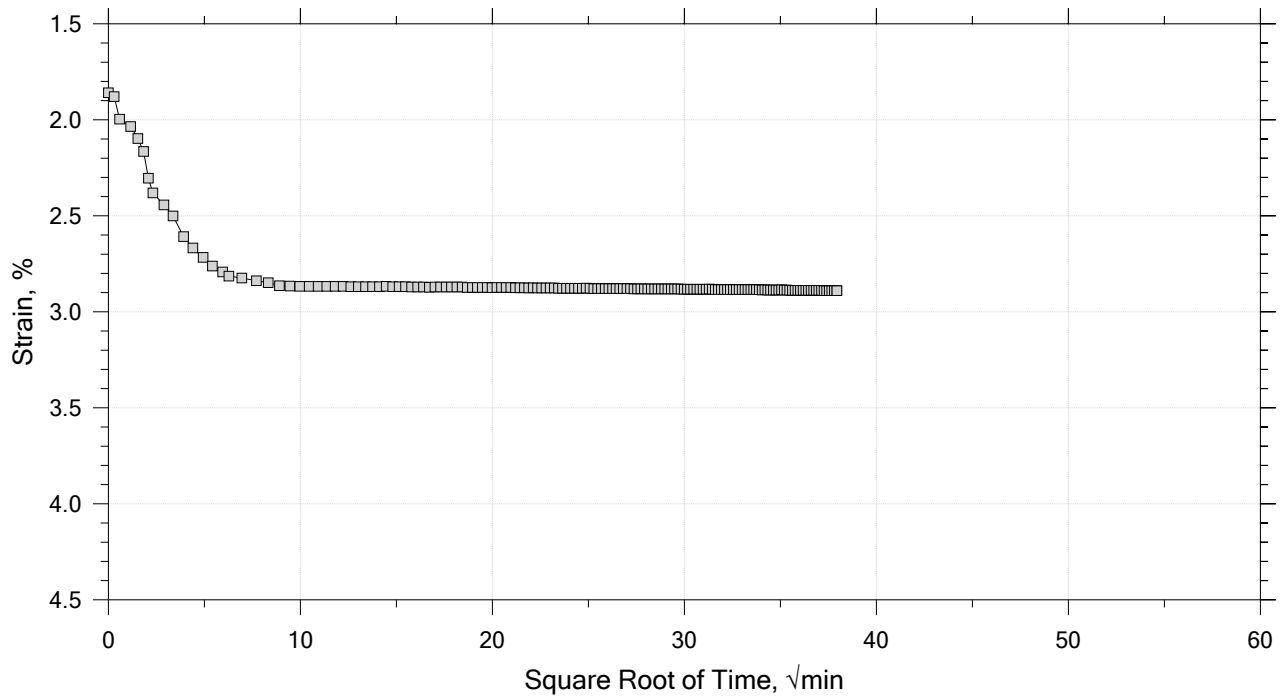
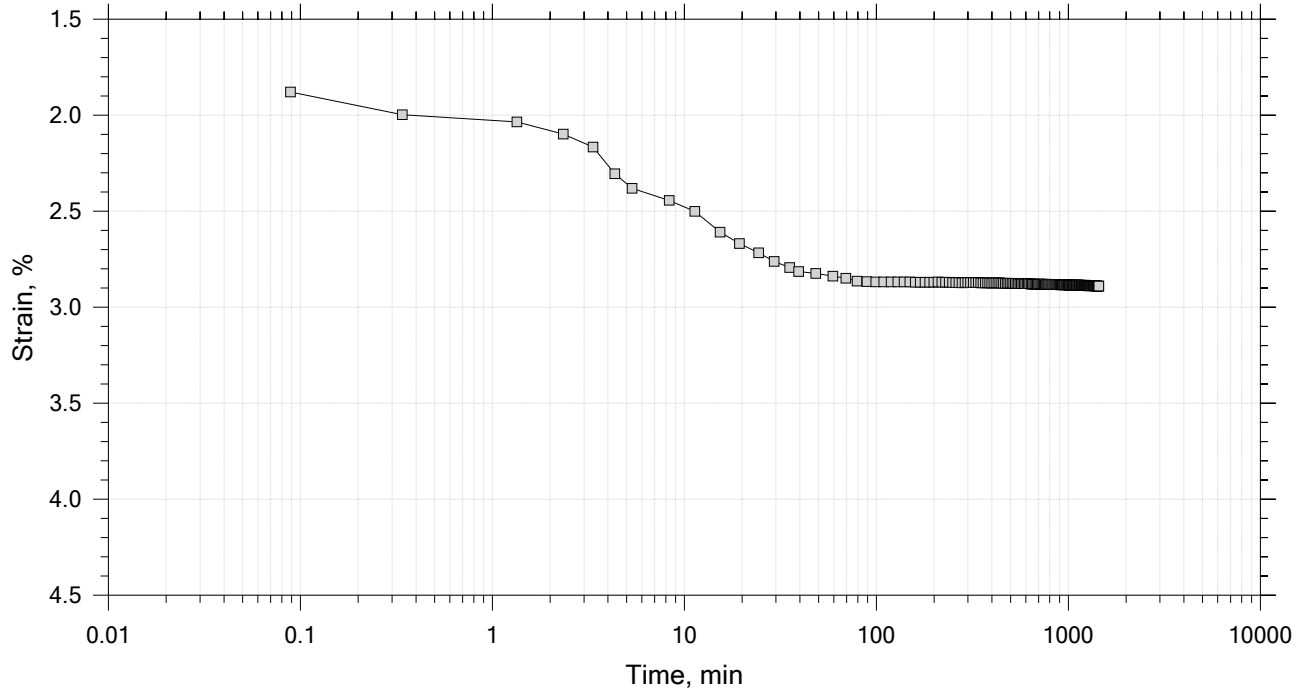
Time Curve 2 of 12  
 Constant Load Step  
 Stress: 250 psf




 Engineering and Testing	Project: Breton Lakebridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-5	Tested By: jm	Checked By: mcm
	Sample No.: 10	Test Date: 10/10/20	Depth: 18-20 ft
	Test No.: IP-9	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay(CH)		

# One-Dimensional Consolidation by ASTM D2435 - Method B

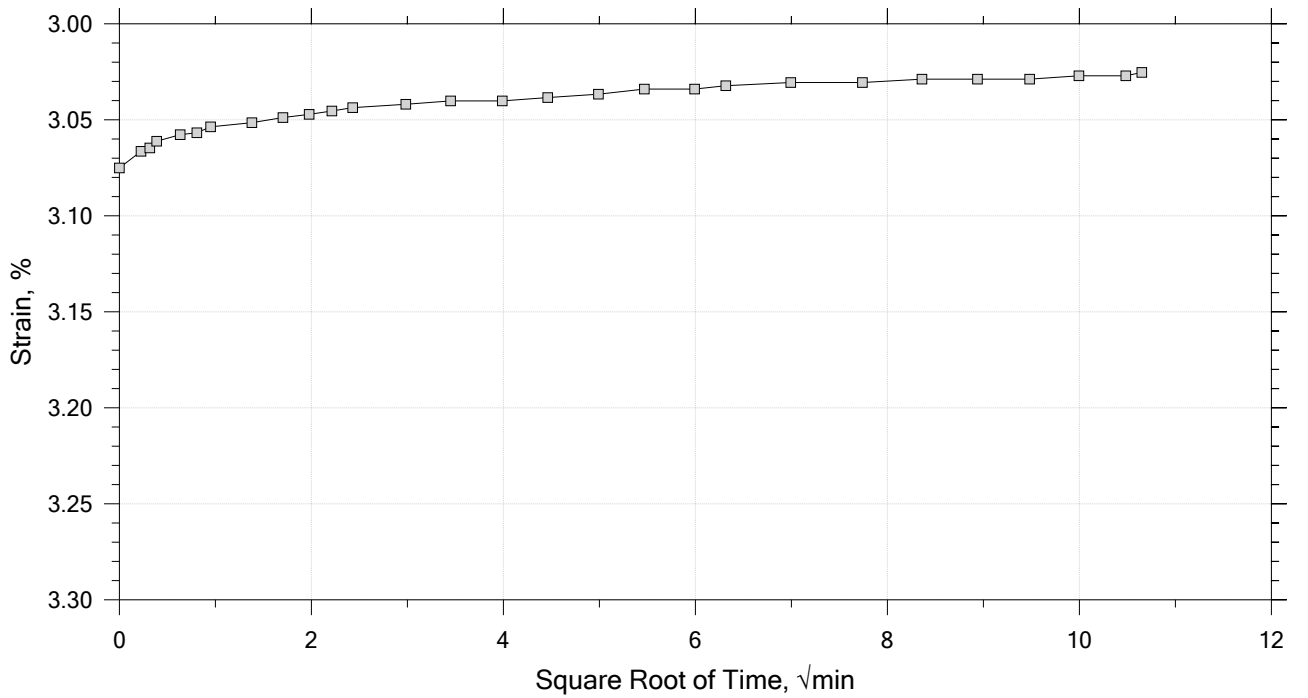
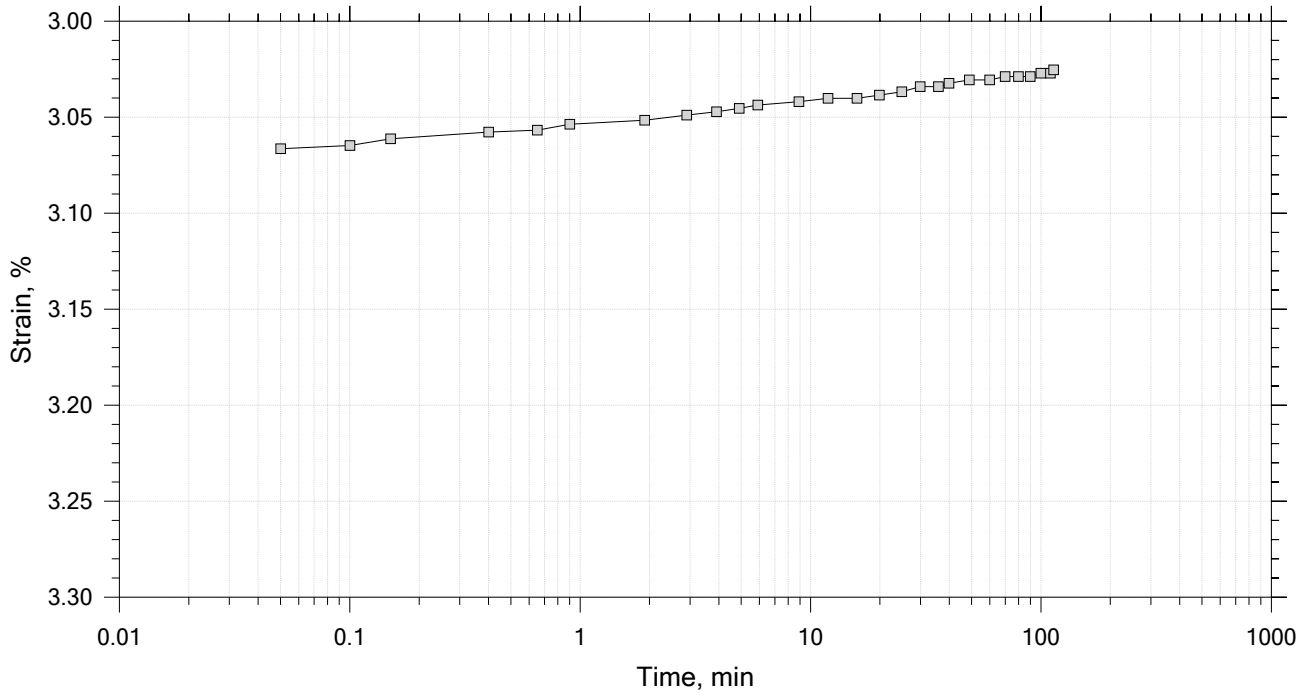
Time Curve 3 of 12  
 Constant Load Step  
 Stress: 500 psf




 Engineering and Testing	Project: Breton Lakebridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-5	Tested By: jm	Checked By: mcm
	Sample No.: 10	Test Date: 10/10/20	Depth: 18-20 ft
	Test No.: IP-9	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay(CH)		

# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 4 of 12  
 Constant Load Step  
 Stress: 250 psf

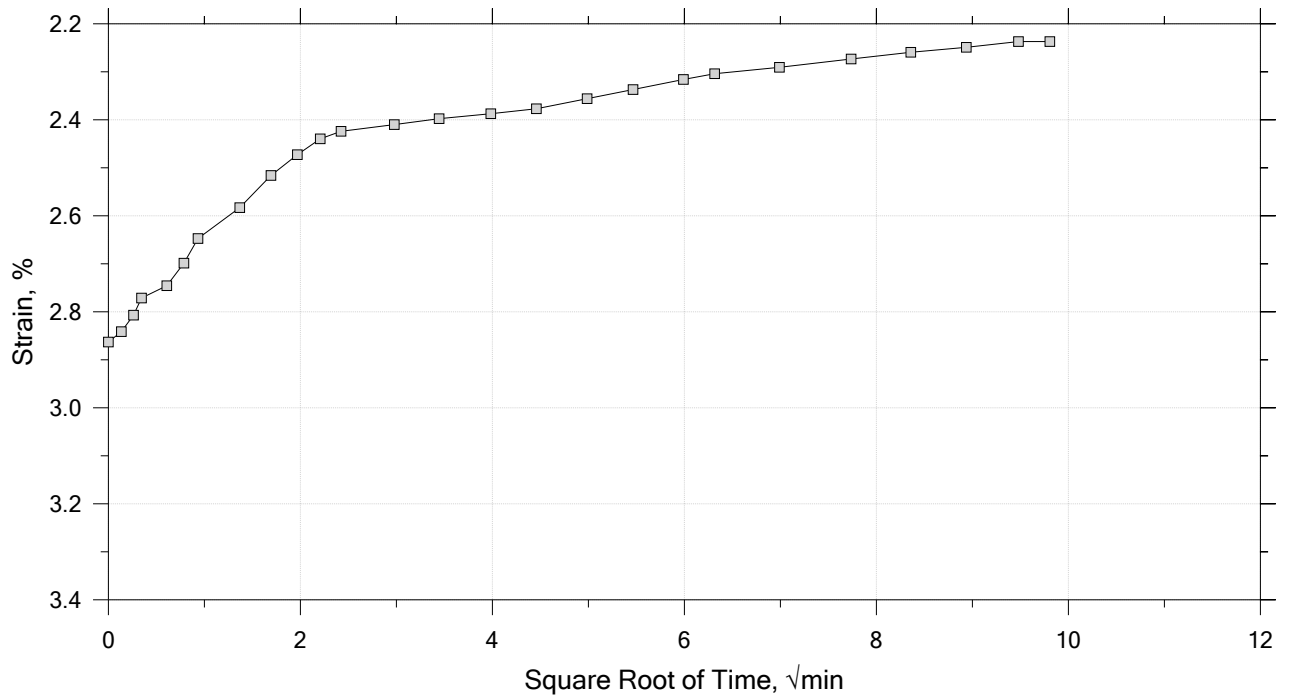
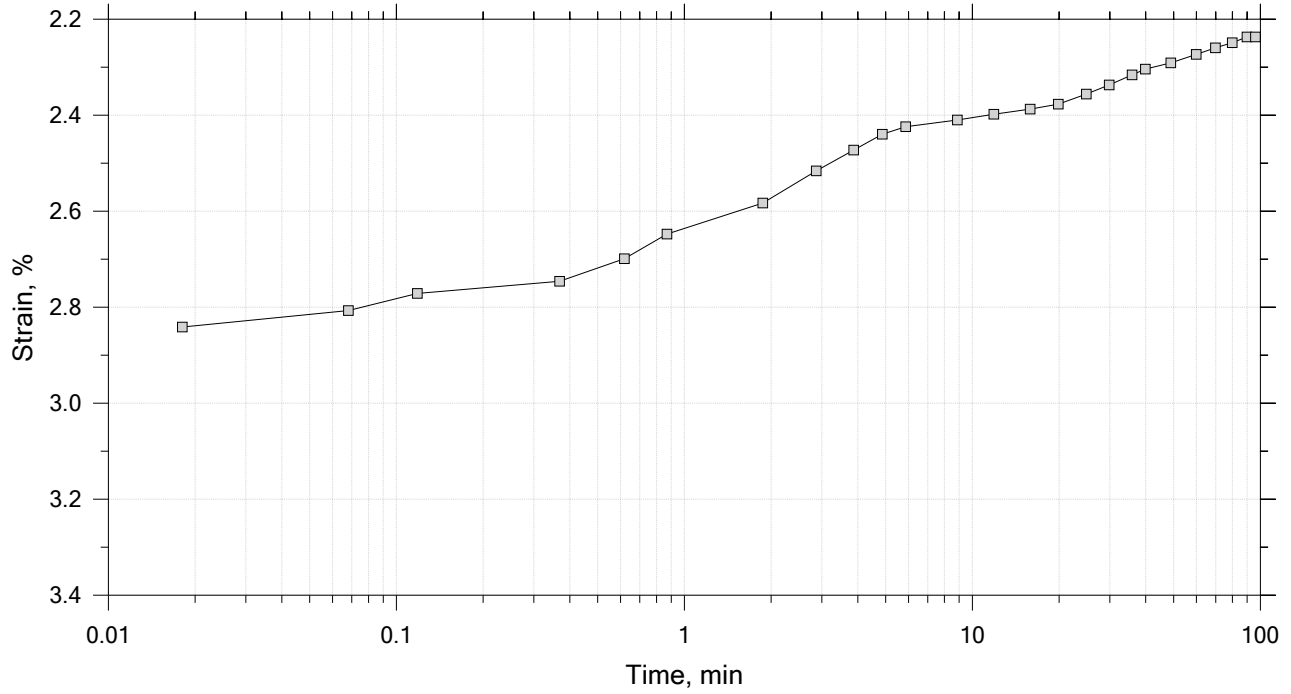



 Engineering and Testing	Project: Breton Lakebridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-5	Tested By: jm	Checked By: mcm
	Sample No.: 10	Test Date: 10/10/20	Depth: 18-20 ft
	Test No.: IP-9	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay(CH)		



# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 5 of 12  
 Constant Load Step  
 Stress: 100 psf



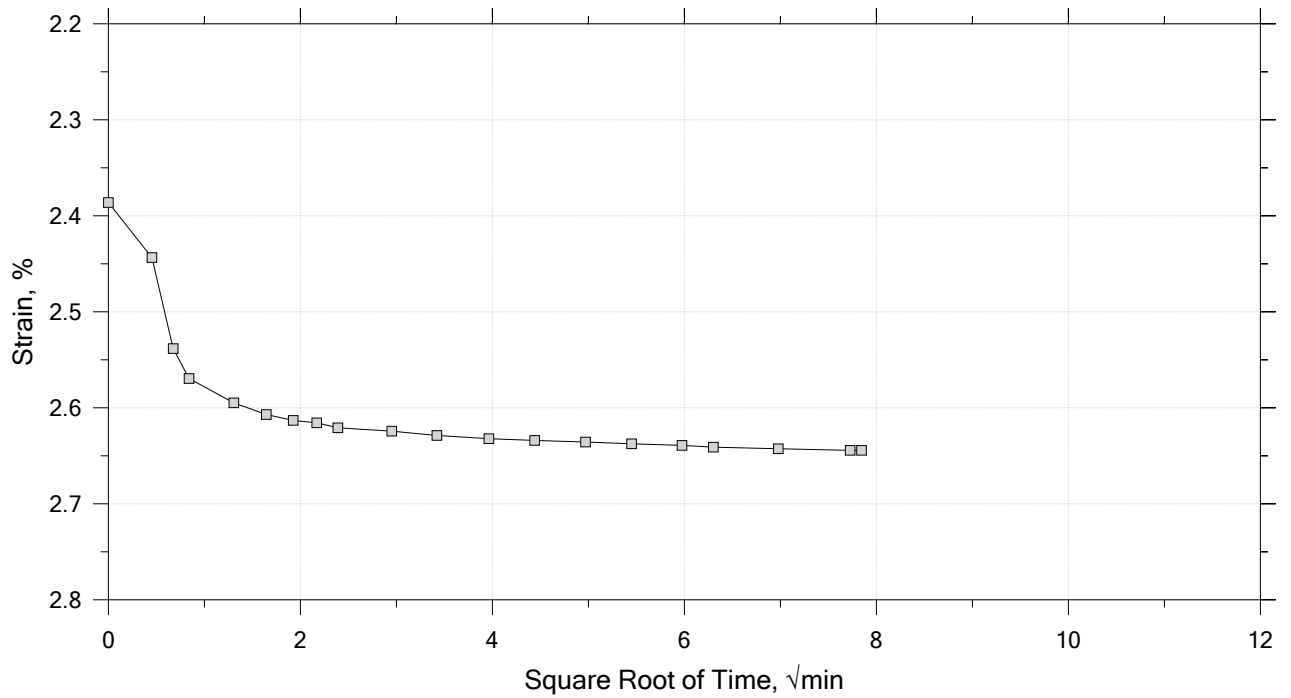
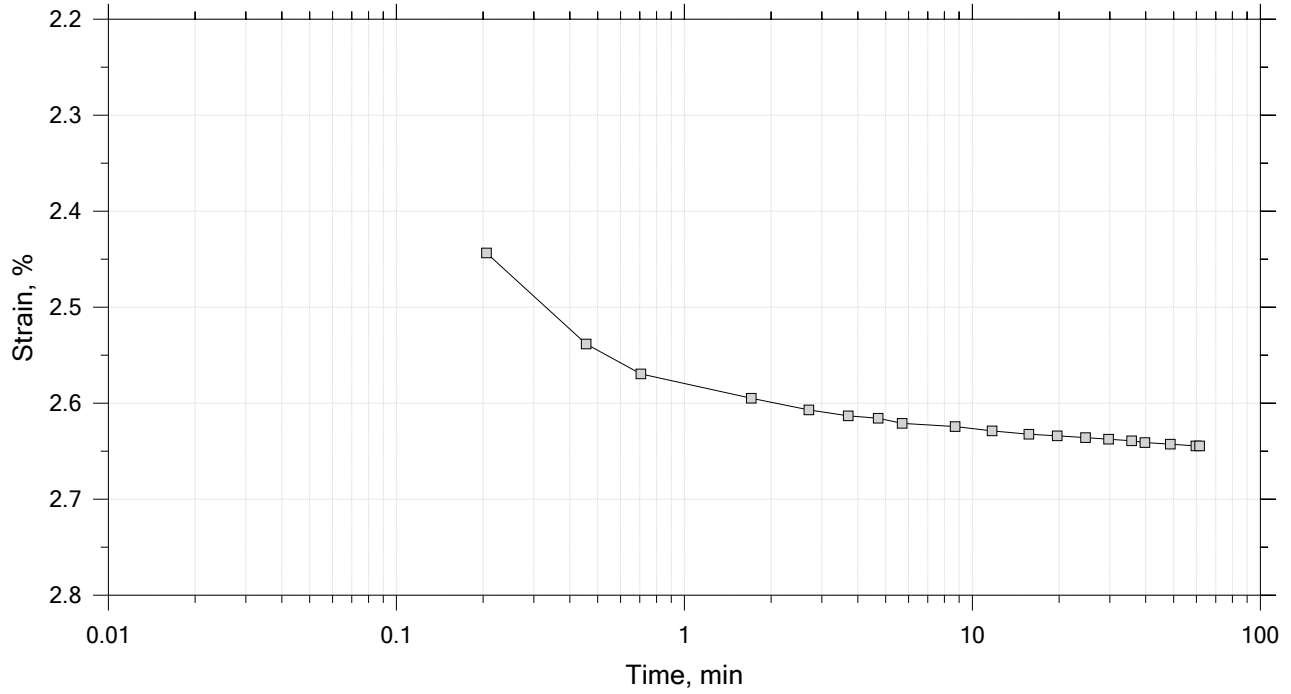
 Engineering and Testing	Project: Breton Lakebridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-5	Tested By: jm	Checked By: mcm
	Sample No.: 10	Test Date: 10/10/20	Depth: 18-20 ft
	Test No.: IP-9	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay(CH)		


# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 6 of 12

Constant Load Step

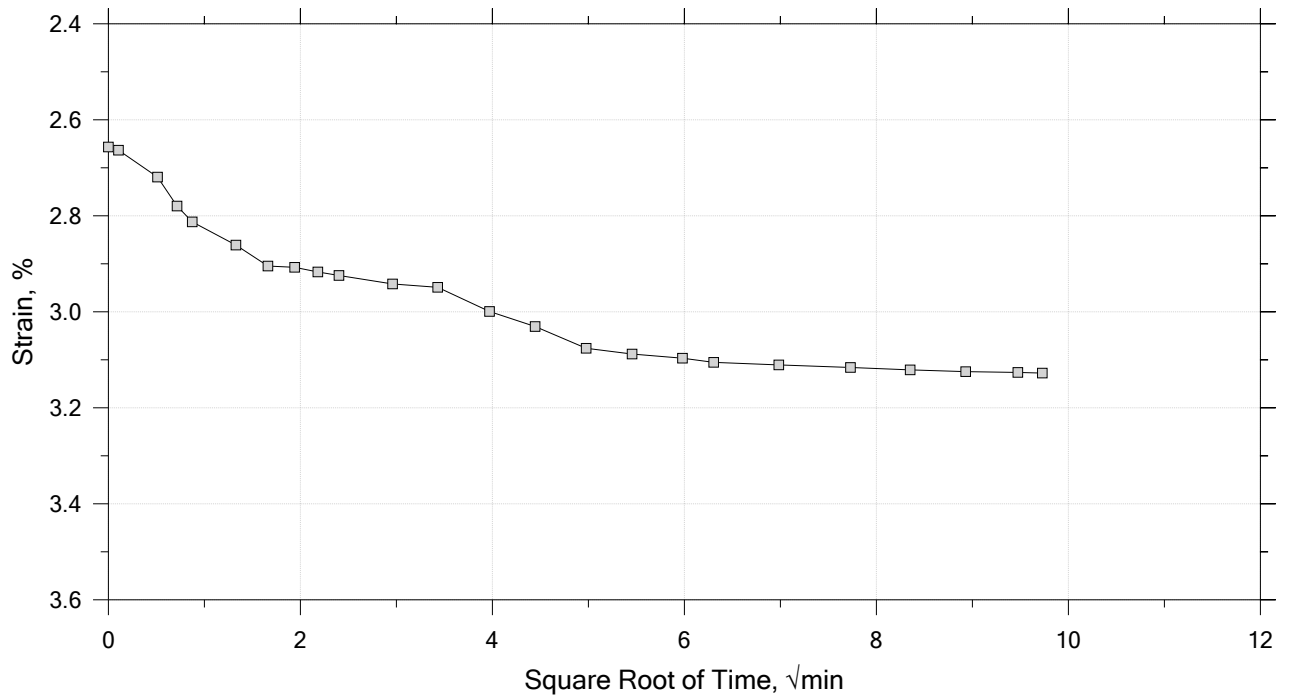
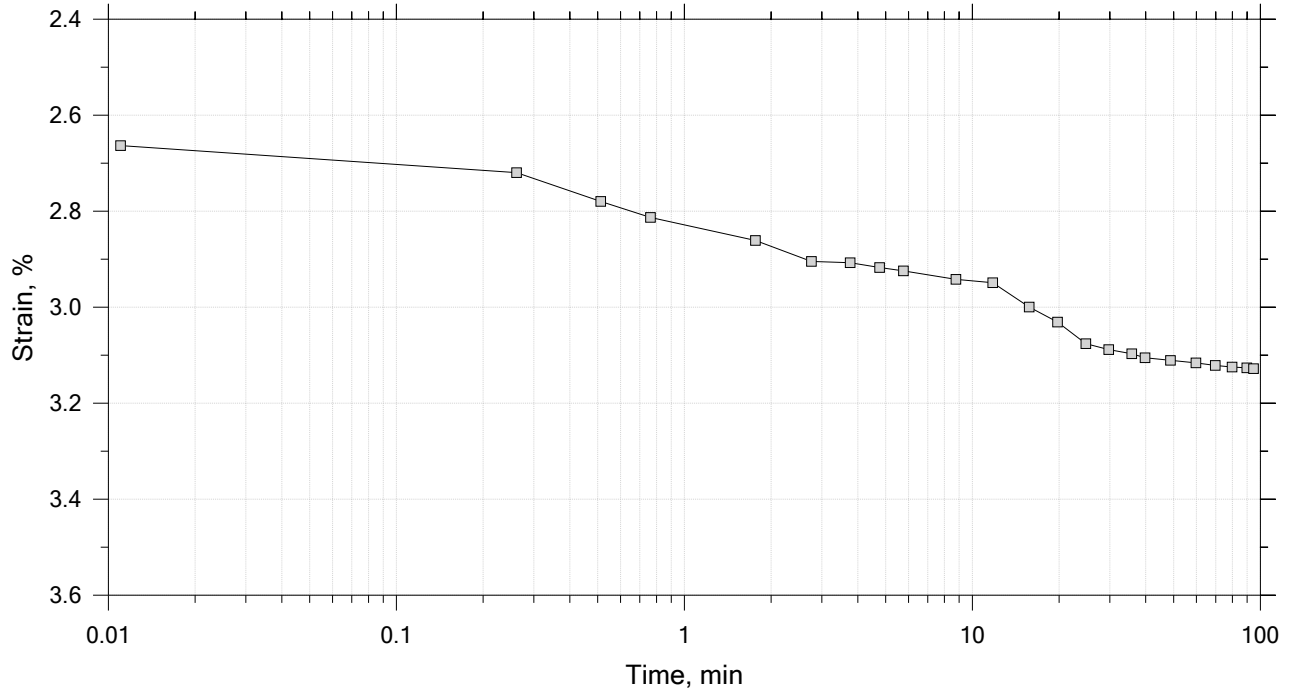
Stress: 250 psf




 Engineering and Testing	Project: Breton Lakebridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-5	Tested By: jm	Checked By: mcm
	Sample No.: 10	Test Date: 10/10/20	Depth: 18-20 ft
	Test No.: IP-9	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay(CH)		

# One-Dimensional Consolidation by ASTM D2435 - Method B

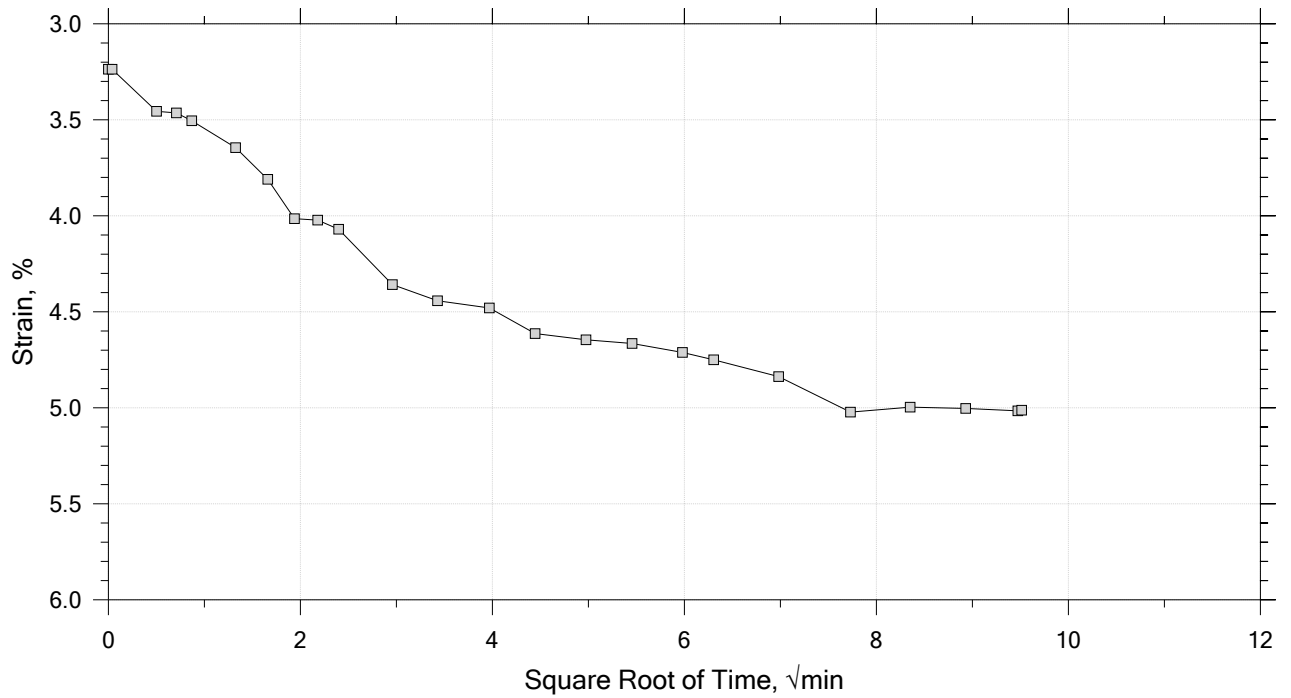
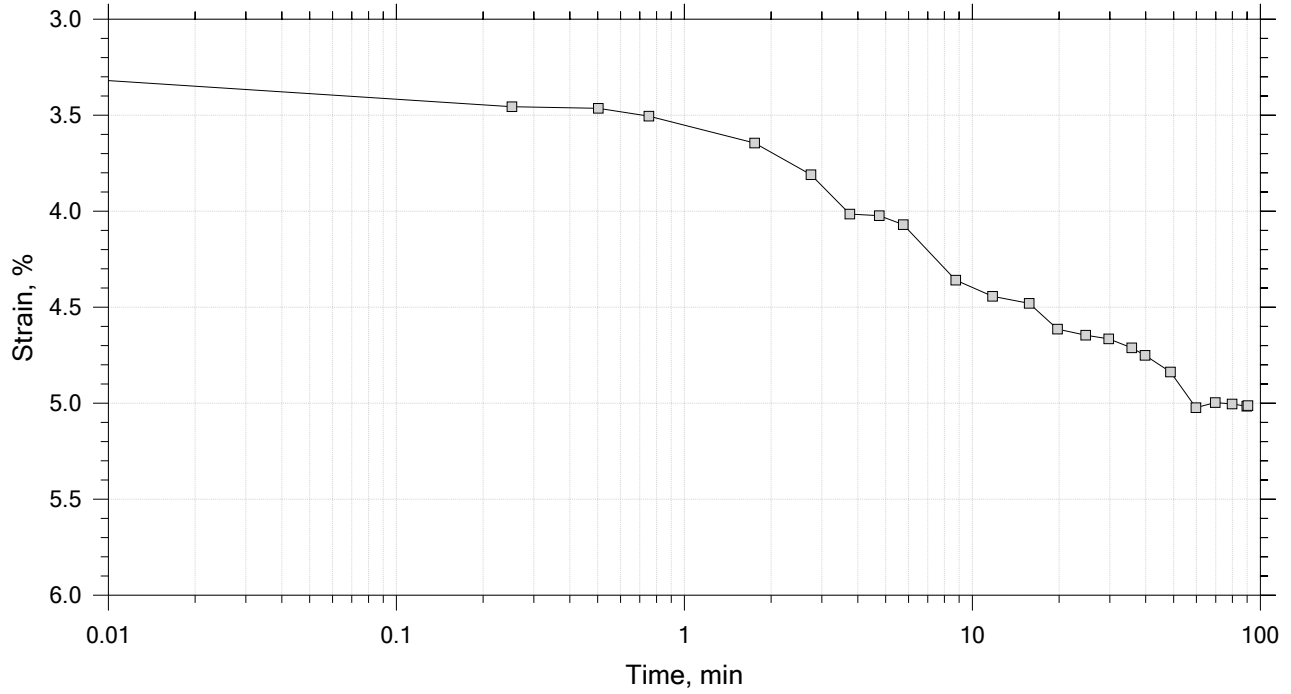
Time Curve 7 of 12  
 Constant Load Step  
 Stress: 500 psf




 Engineering and Testing	Project: Breton Lakebridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-5	Tested By: jm	Checked By: mcm
	Sample No.: 10	Test Date: 10/10/20	Depth: 18-20 ft
	Test No.: IP-9	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay(CH)		

# One-Dimensional Consolidation by ASTM D2435 - Method B

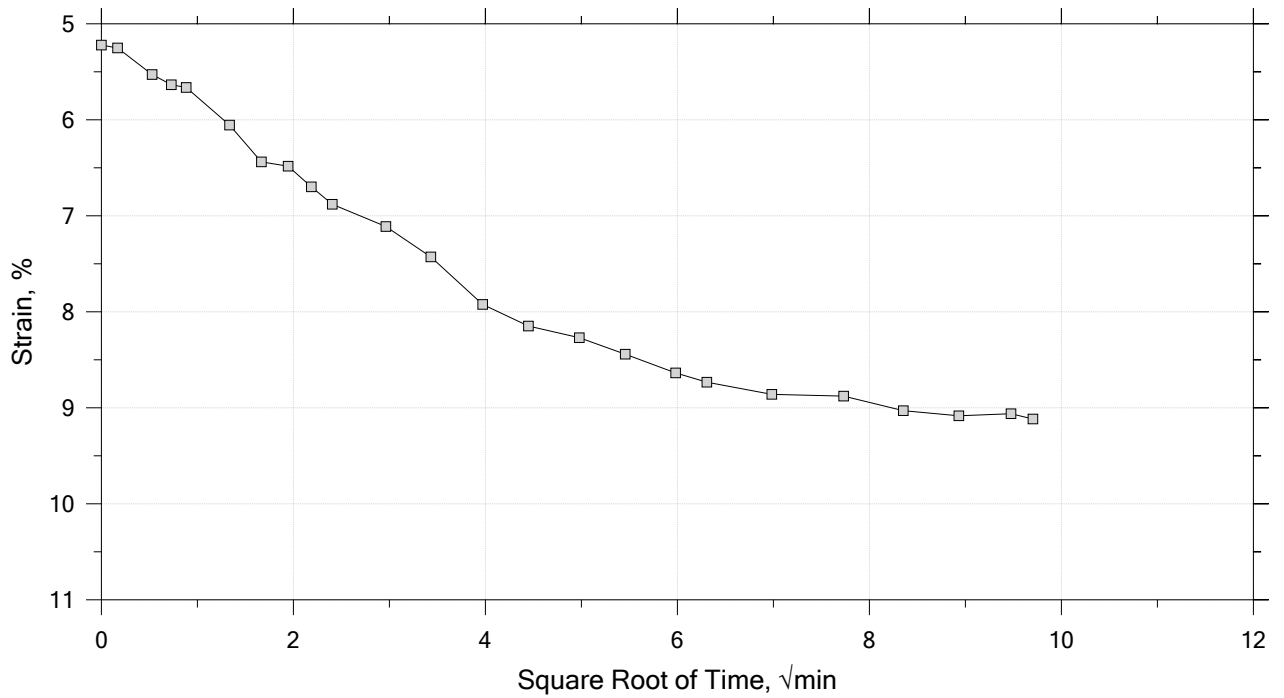
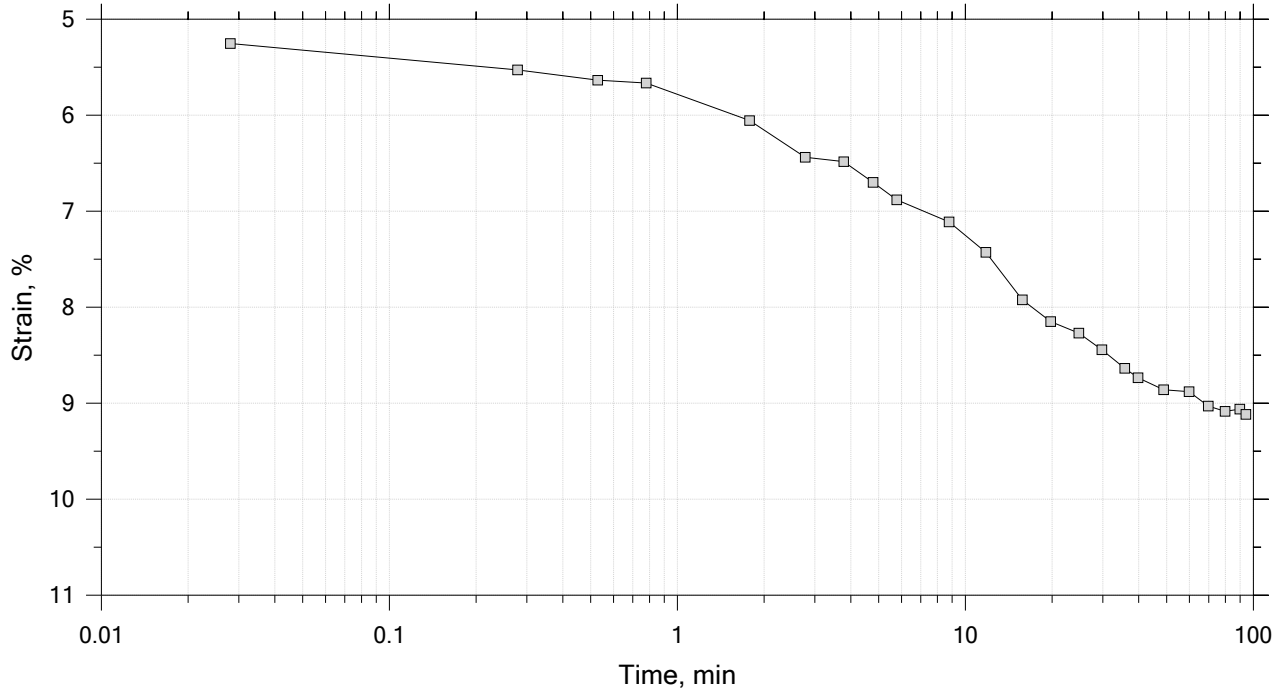
Time Curve 8 of 12  
 Constant Load Step  
 Stress: 1e+03 psf




 Engineering and Testing	Project: Breton Lakebridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-5	Tested By: jm	Checked By: mcm
	Sample No.: 10	Test Date: 10/10/20	Depth: 18-20 ft
	Test No.: IP-9	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay(CH)		

# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 9 of 12  
 Constant Load Step  
 Stress: 2e+03 psf



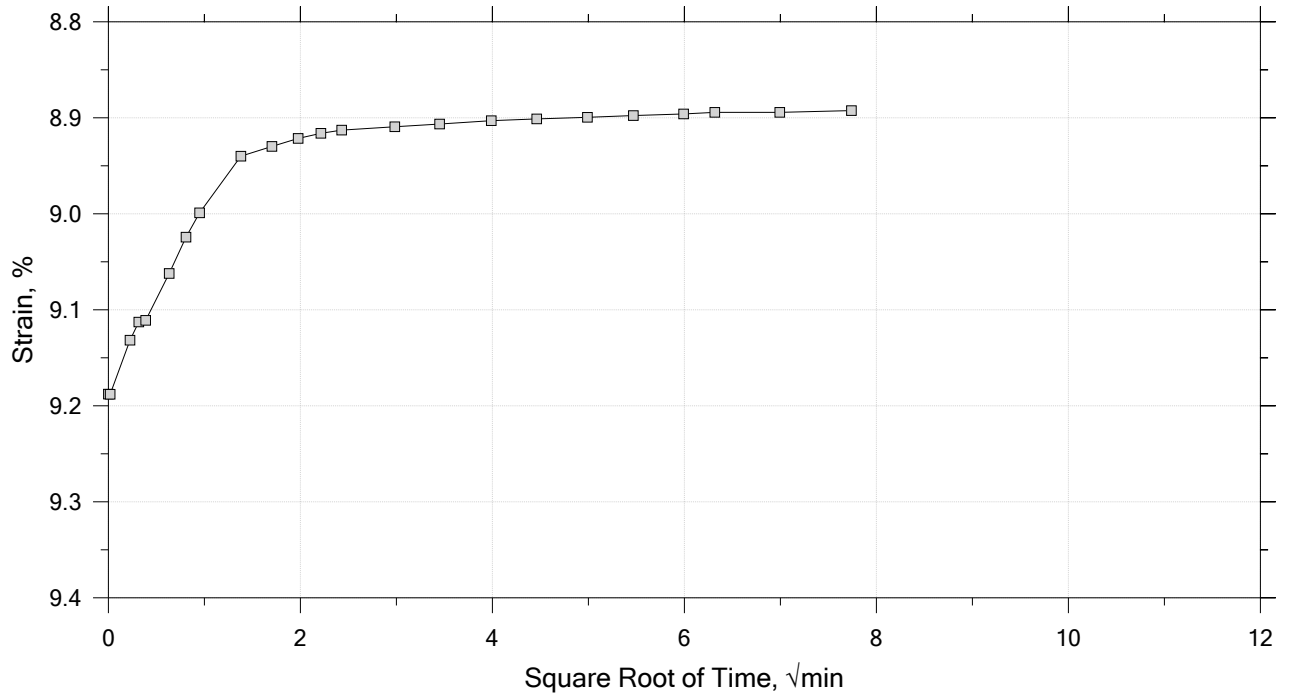
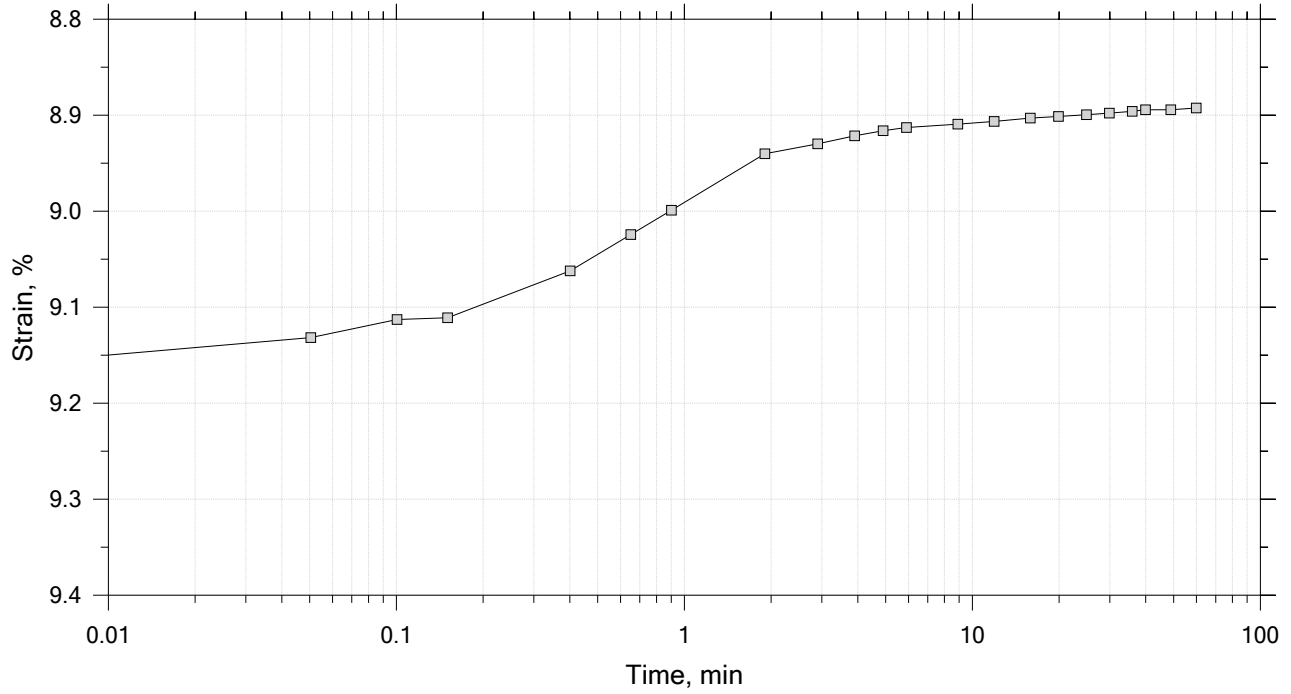
 Engineering and Testing	Project: Breton Lakebridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-5	Tested By: jm	Checked By: mcm
	Sample No.: 10	Test Date: 10/10/20	Depth: 18-20 ft
	Test No.: IP-9	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay(CH)		


# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 10 of 12

Constant Load Step

Stress: 1e+03 psf



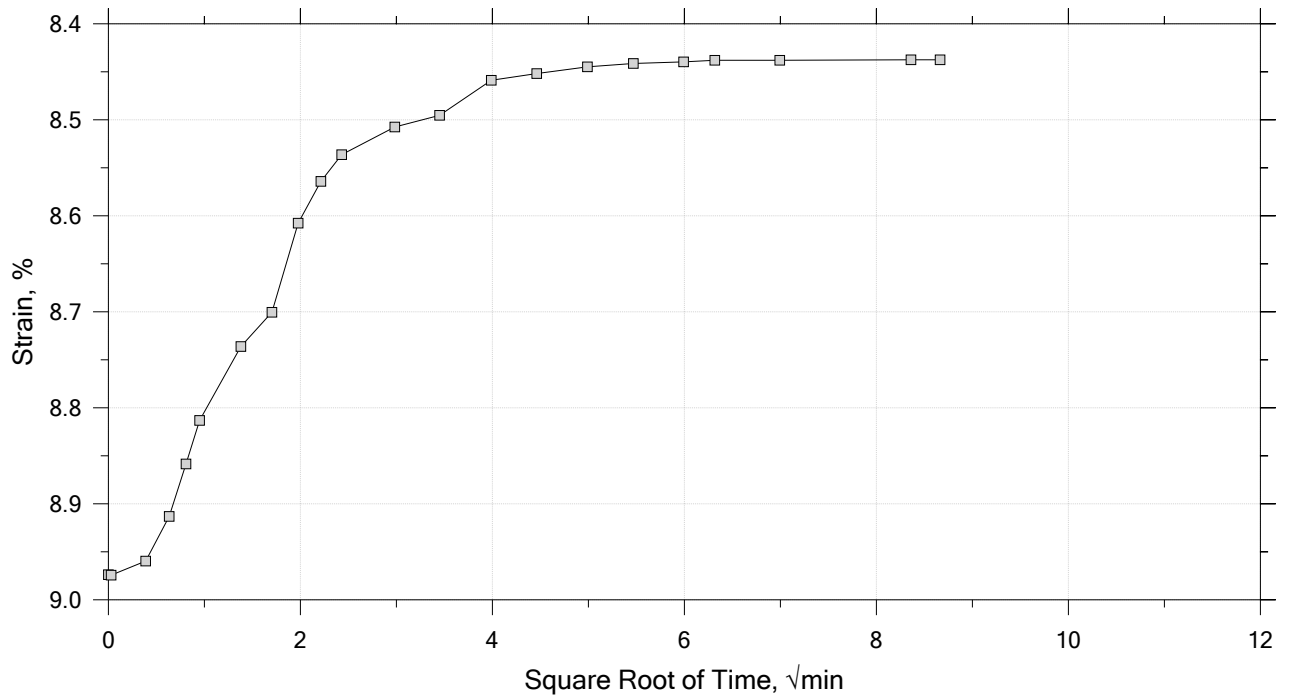
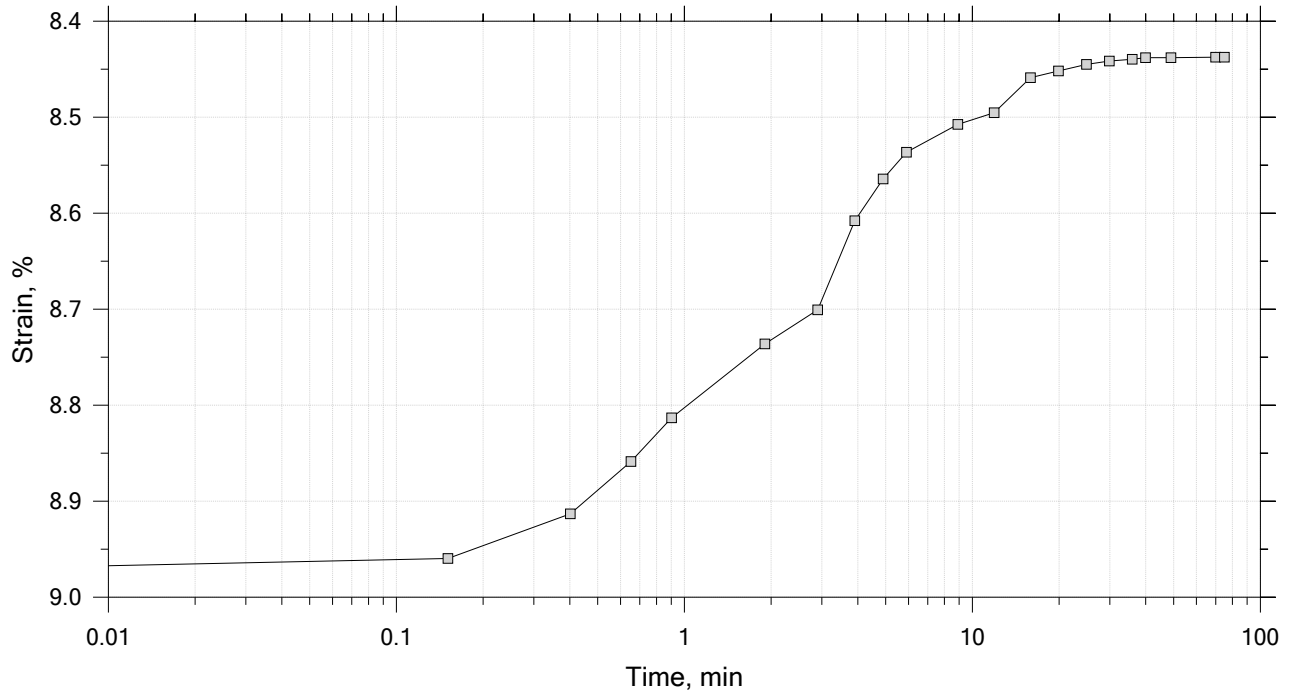
 Engineering and Testing	Project: Breton Lakebridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-5	Tested By: jm	Checked By: mcm
	Sample No.: 10	Test Date: 10/10/20	Depth: 18-20 ft
	Test No.: IP-9	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay(CH)		


# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 11 of 12

Constant Load Step

Stress: 500 psf



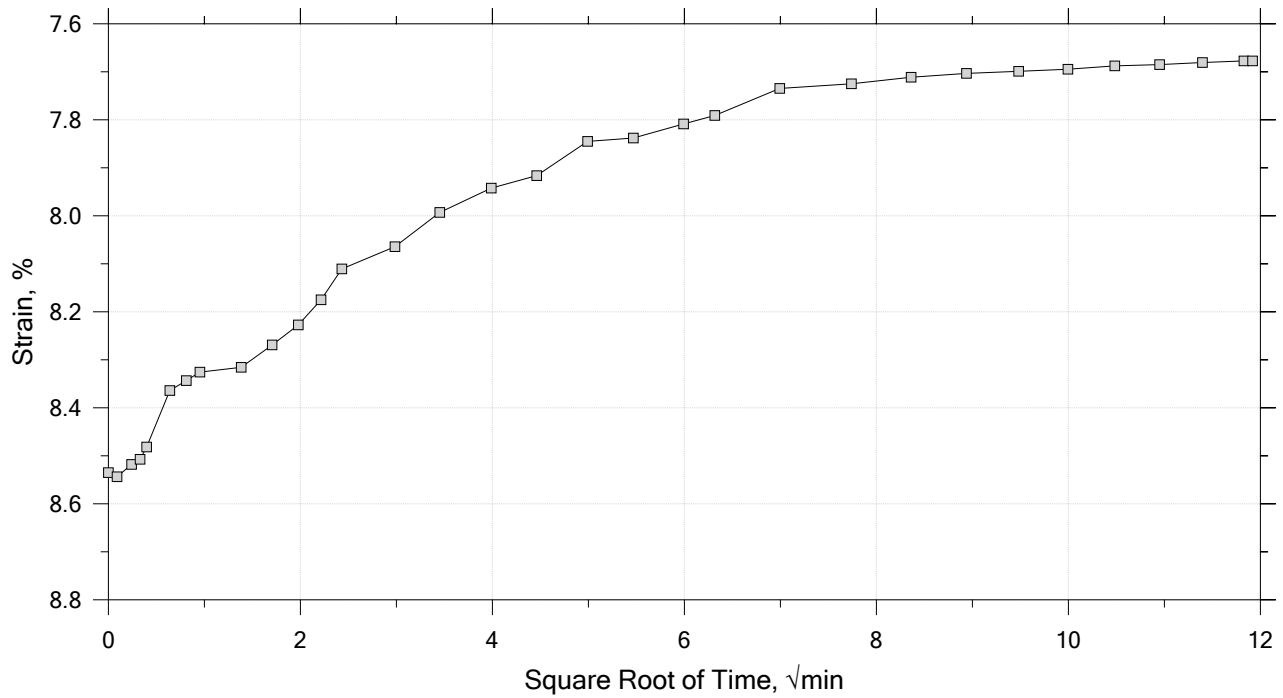
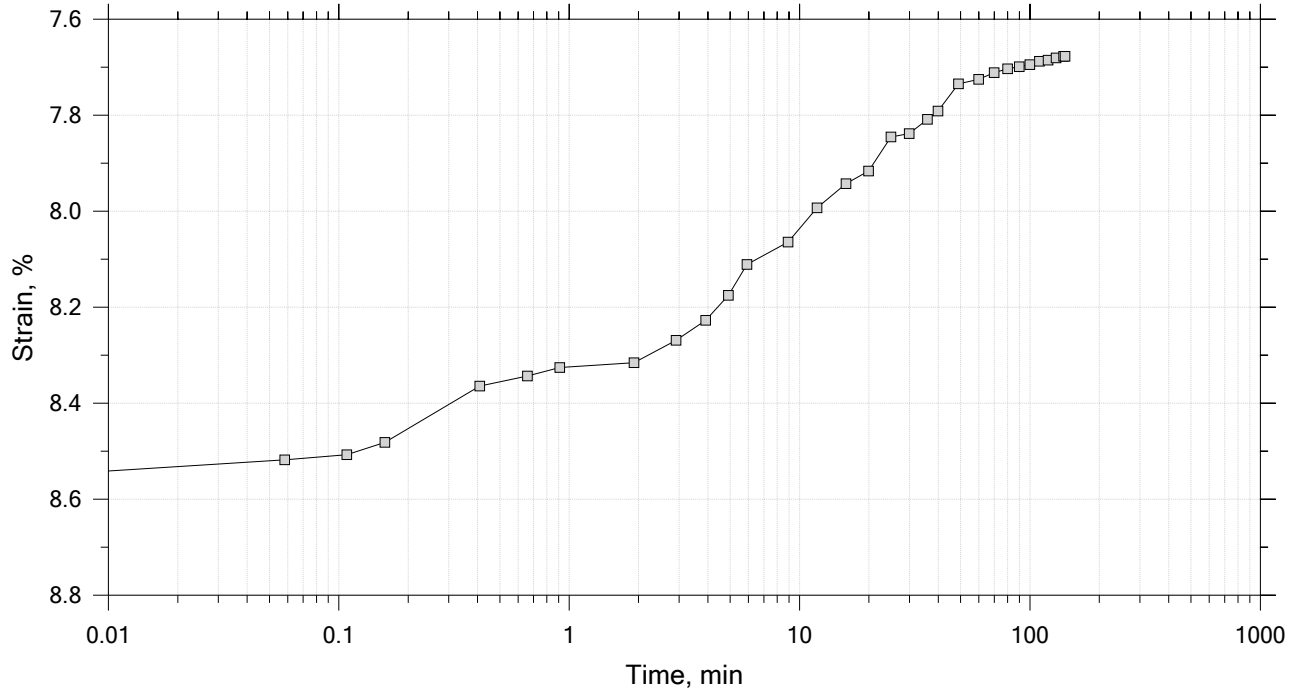
 Engineering and Testing	Project: Breton Lakebridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-5	Tested By: jm	Checked By: mcm
	Sample No.: ---	Test Date: 10/10/20	Depth: 18-20 ft
	Test No.: IP-9	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay		


# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 12 of 12

Constant Load Step

Stress: 250 psf

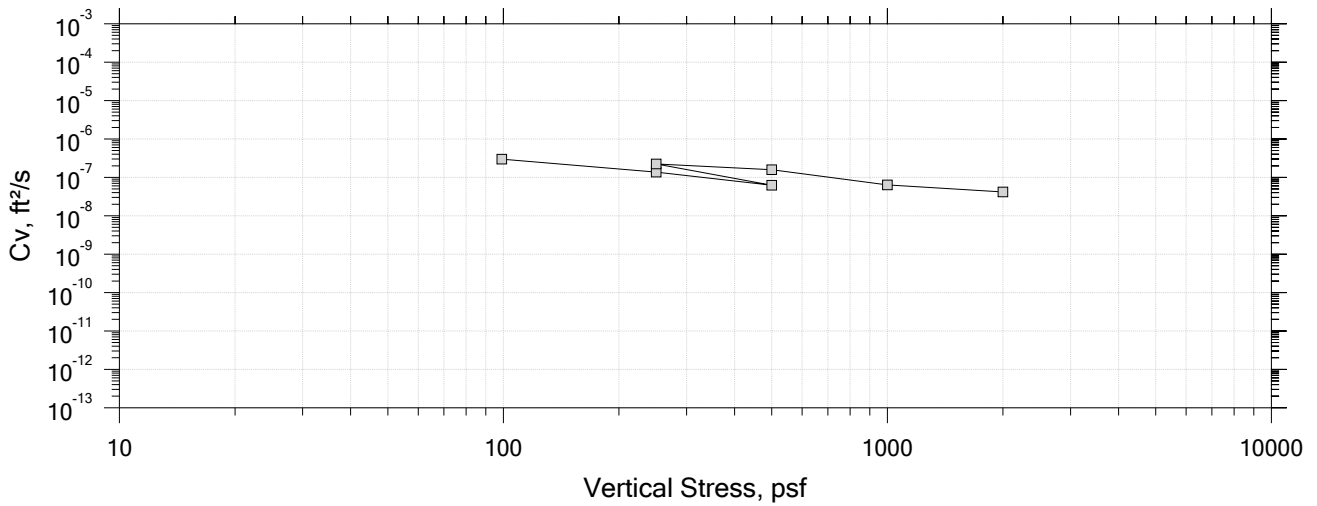
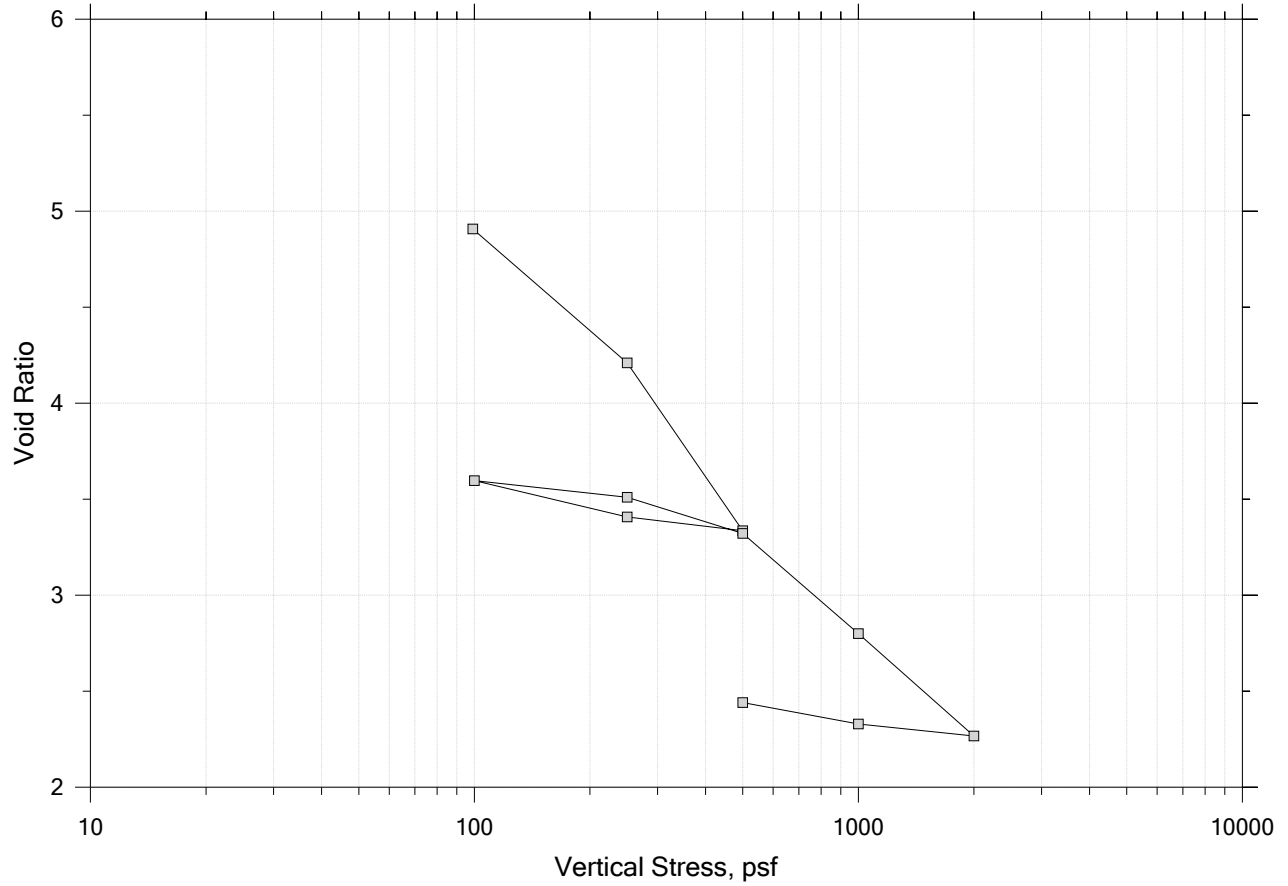



 Engineering and Testing	Project: Breton Lakebridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-5	Tested By: jm	Checked By: mcm
	Sample No.: 10	Test Date: 10/10/20	Depth: 18-20 ft
	Test No.: IP-9	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay(CH)		



# One-Dimensional Consolidation by ASTM D2435 - Method B

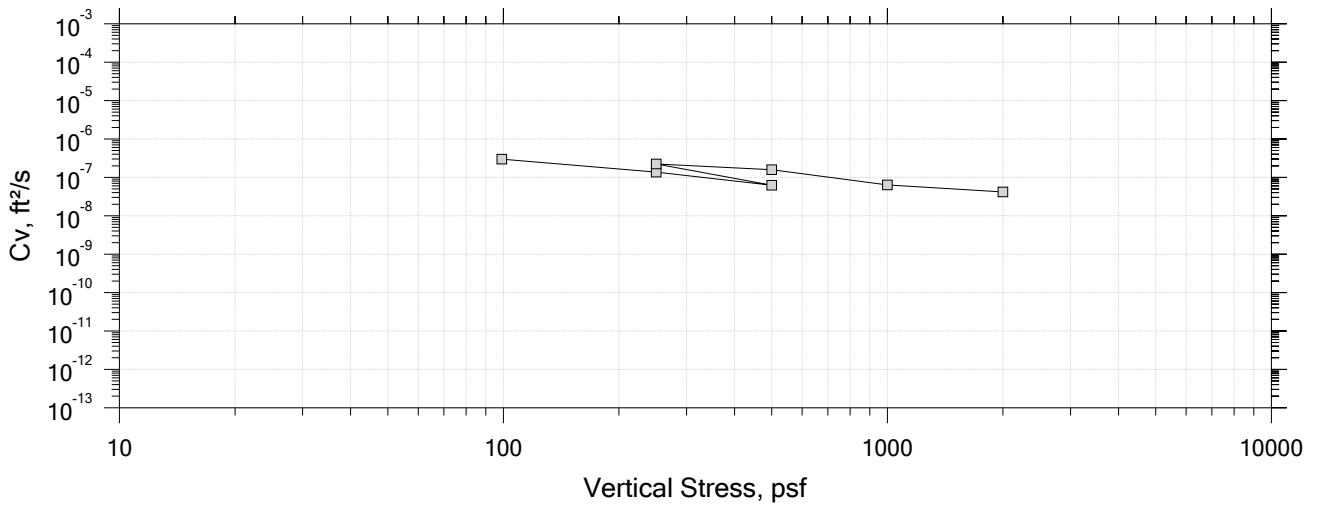
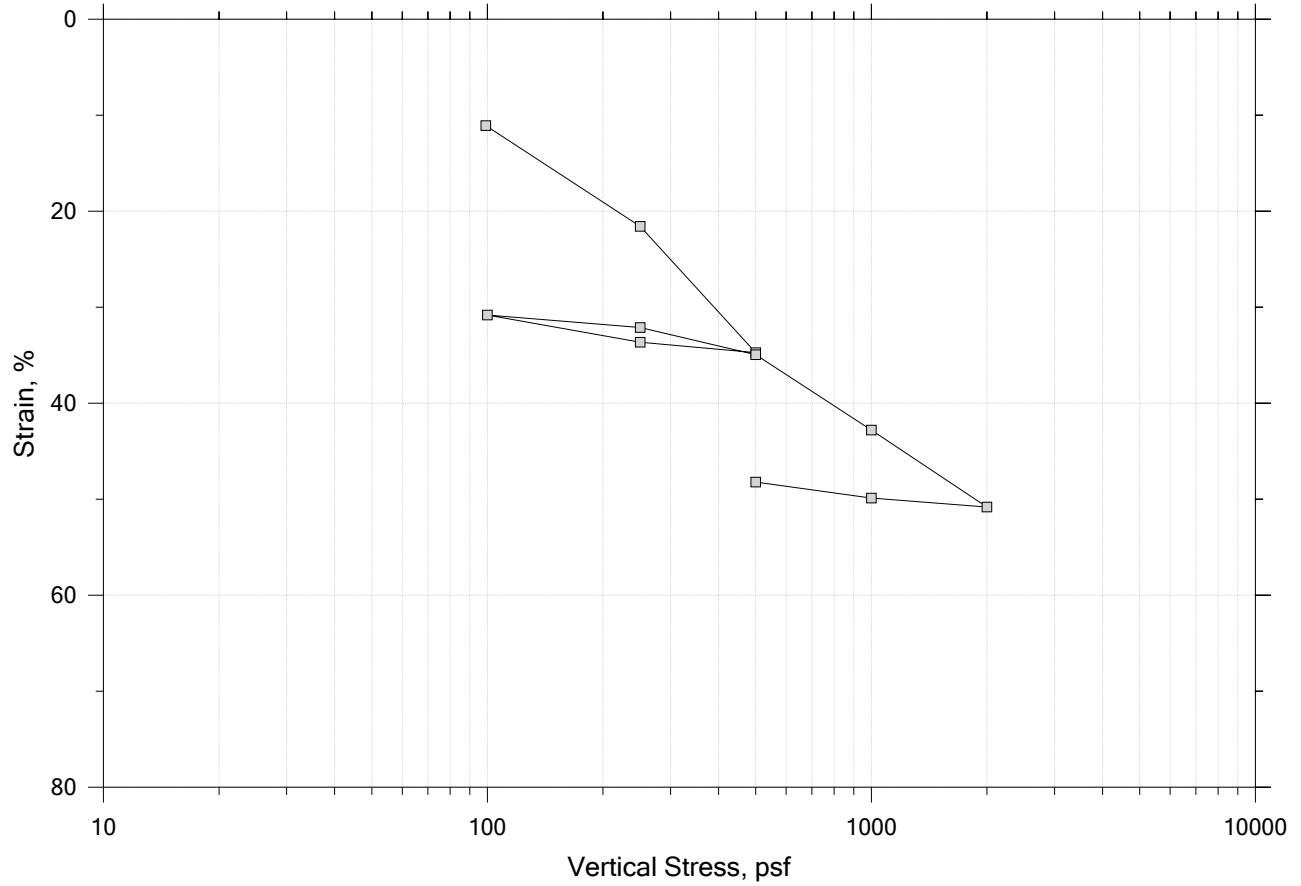
## Summary Report




 <b>APS</b> Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-6	Tested By: jm	Checked By: mcm
	Sample No.: 1	Test Date: 10/19/20	Depth: 0-2 ft
	Test No.: IP-10	Sample Type: intact	Elevation: ---
	Description: Moist, dark grayish brown clay(OH)	Measured specific gravity: 2.40	

# One-Dimensional Consolidation by ASTM D2435 - Method B

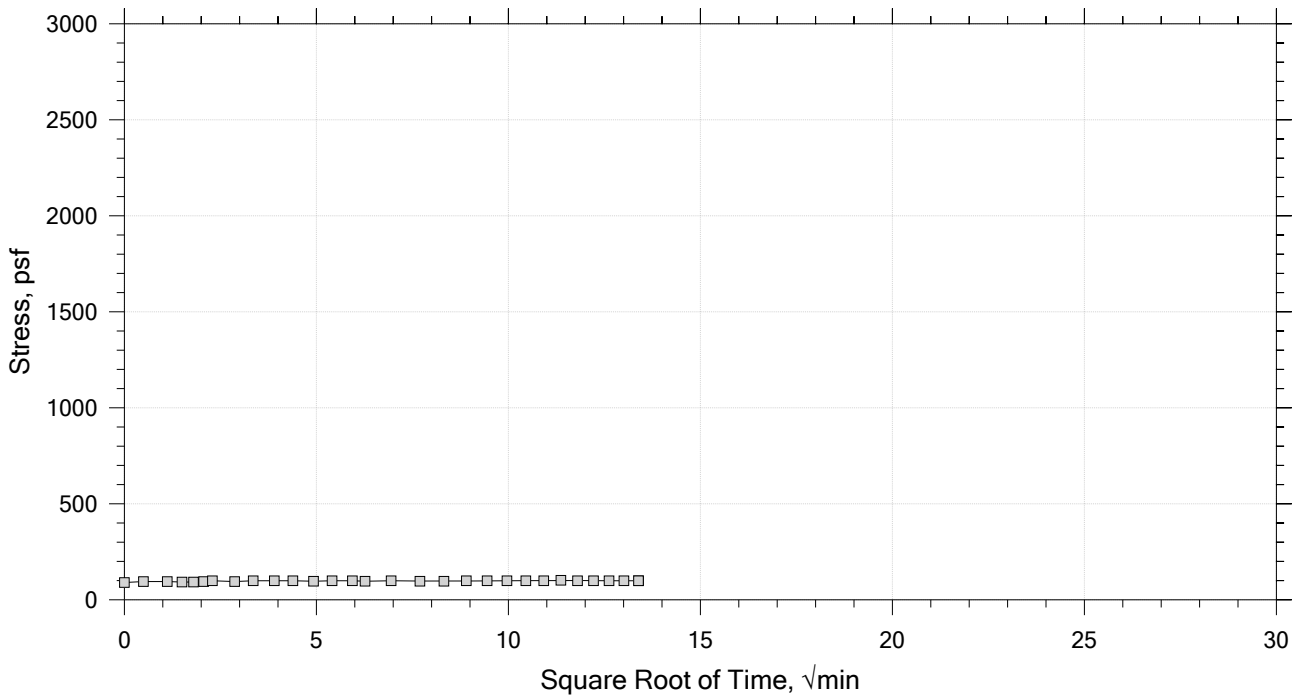
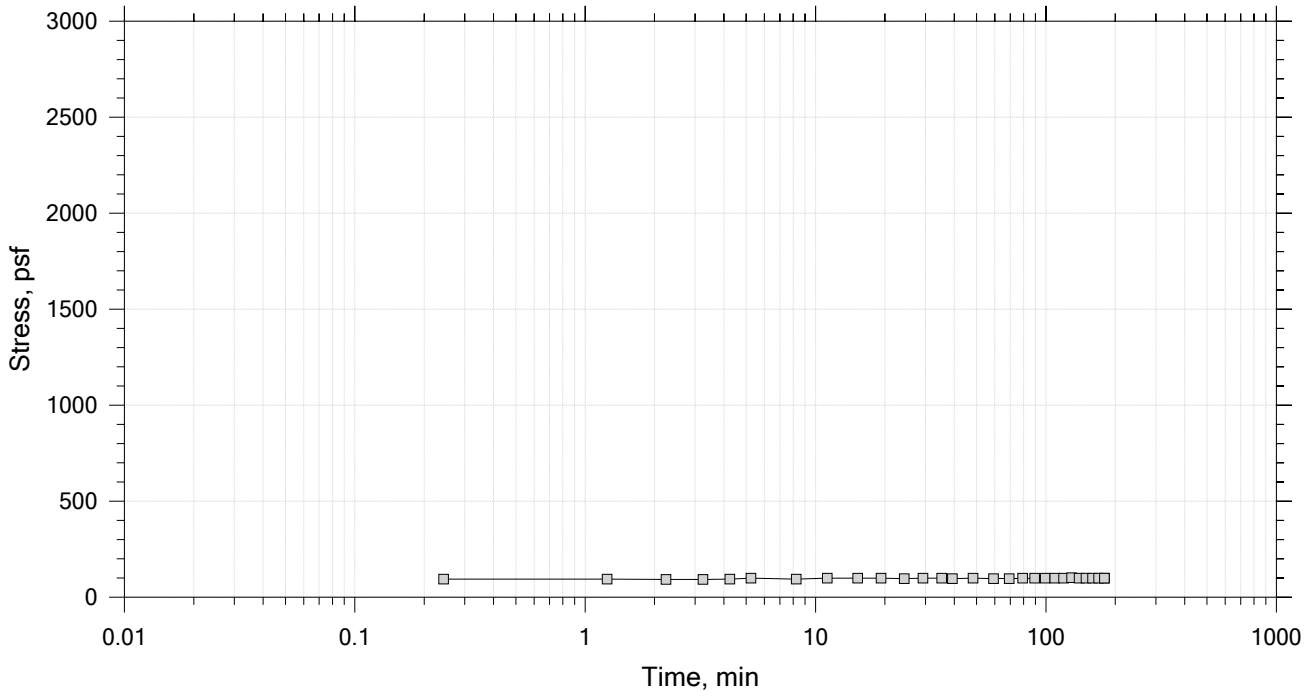
## Summary Report




 <p>APS Engineering and Testing</p>	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-6	Tested By: jm	Checked By: mcm
	Sample No.: 1	Test Date: 10/19/20	Depth: 0-2 ft
	Test No.: IP-10	Sample Type: intact	Elevation: ---
	Description: Moist, dark grayish brown clay (OH)		

# One-Dimensional Consolidation by ASTM D2435 - Method B

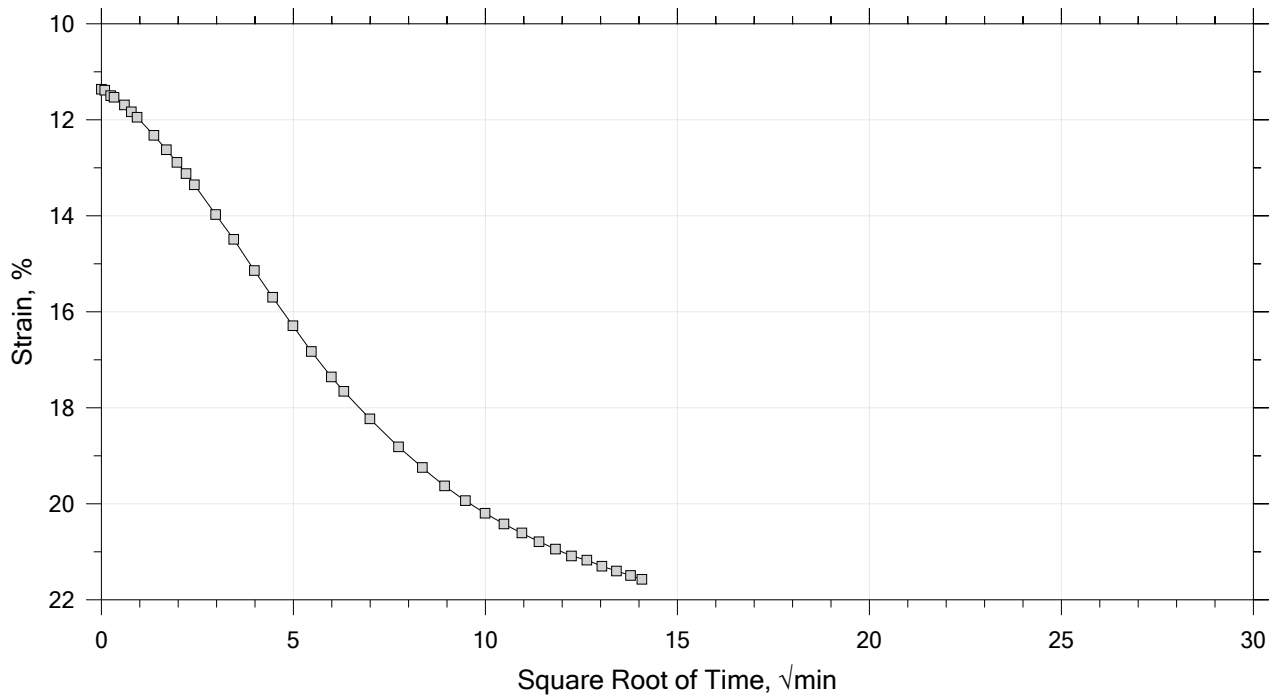
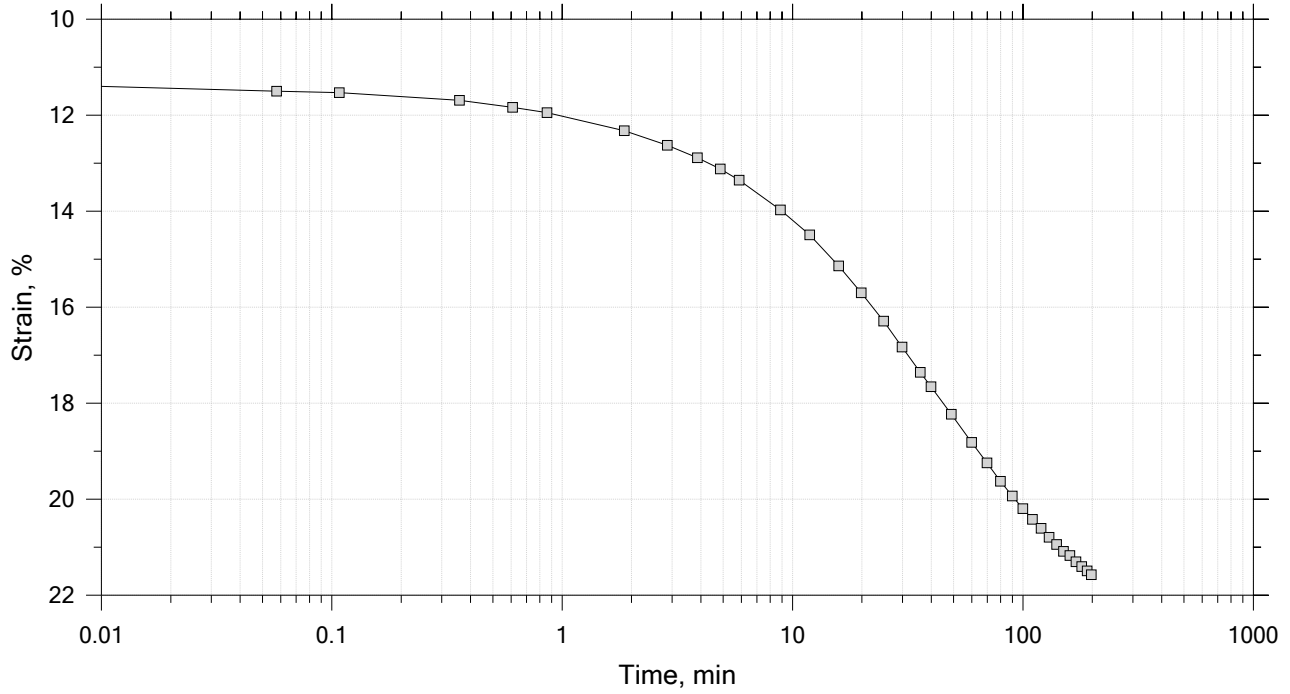
Time Curve 1 of 11  
 Constant Volume Step  
 Stress: 99 psf




 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-6	Tested By: jm	Checked By: mcm
	Sample No.: 1	Test Date: 10/19/20	Depth: 0-2 ft
	Test No.: IP-10	Sample Type: intact	Elevation: ---
	Description: Moist, dark grayish brown clay(OH)		

# One-Dimensional Consolidation by ASTM D2435 - Method B

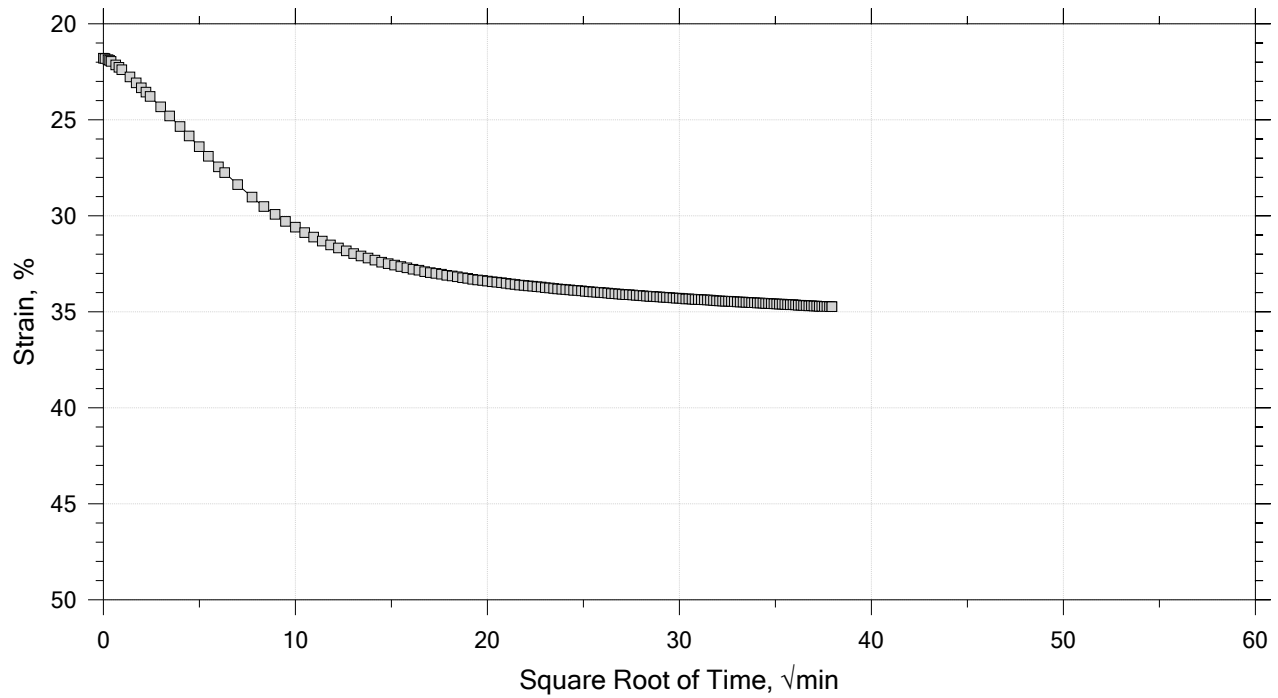
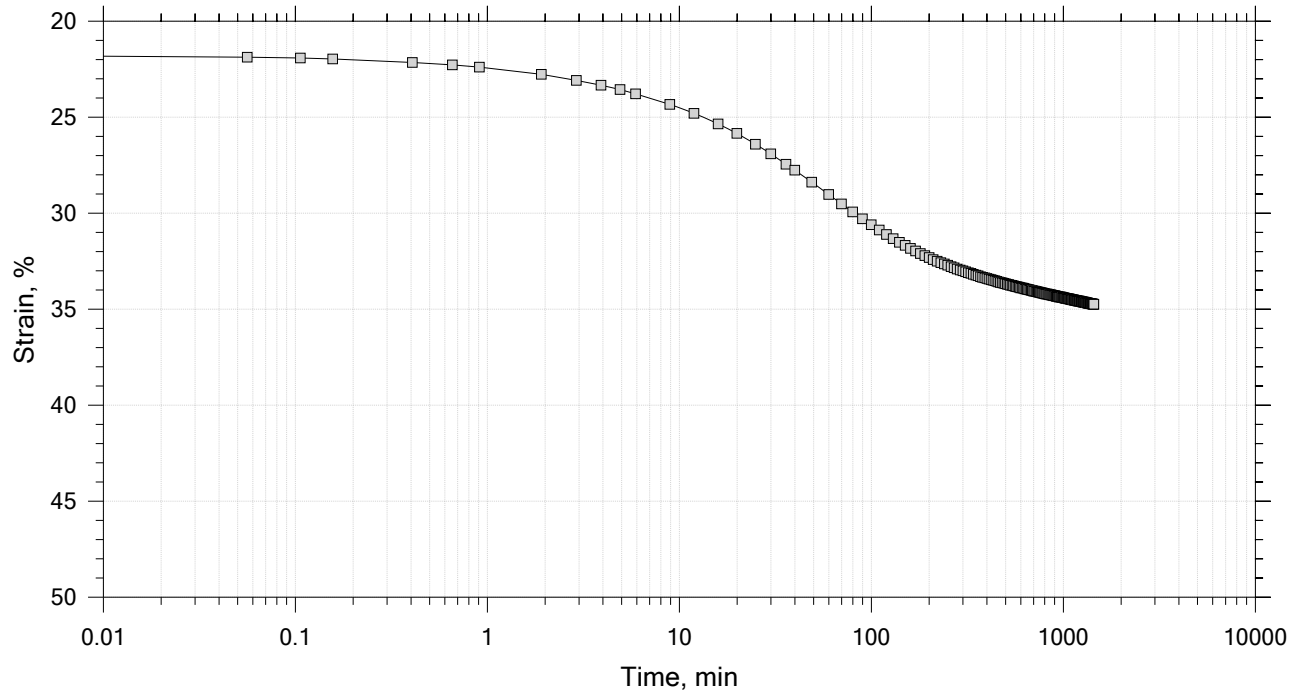
Time Curve 2 of 11  
 Constant Load Step  
 Stress: 250 psf




 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-6	Tested By: jm	Checked By: mcm
	Sample No.: 1	Test Date: 10/19/20	Depth: 0-2 ft
	Test No.: IP-10	Sample Type: intact	Elevation: ---
	Description: Moist, dark grayish brown clay(OH)		

# One-Dimensional Consolidation by ASTM D2435 - Method B

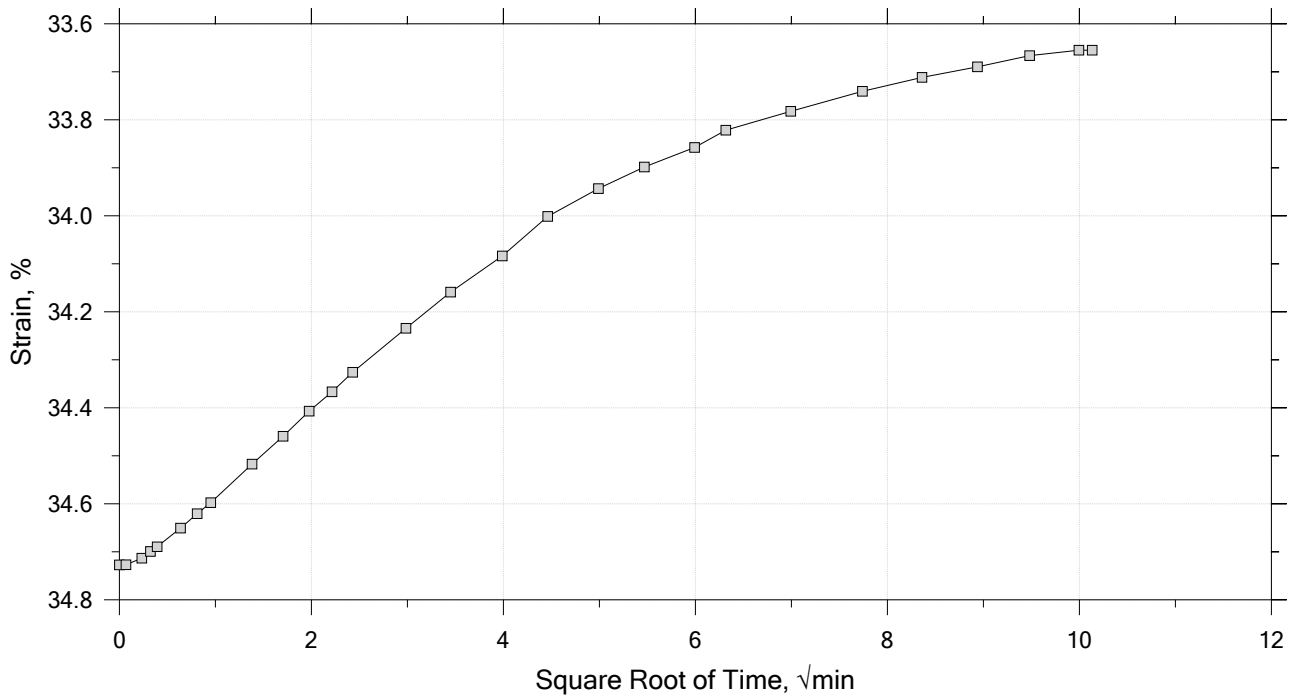
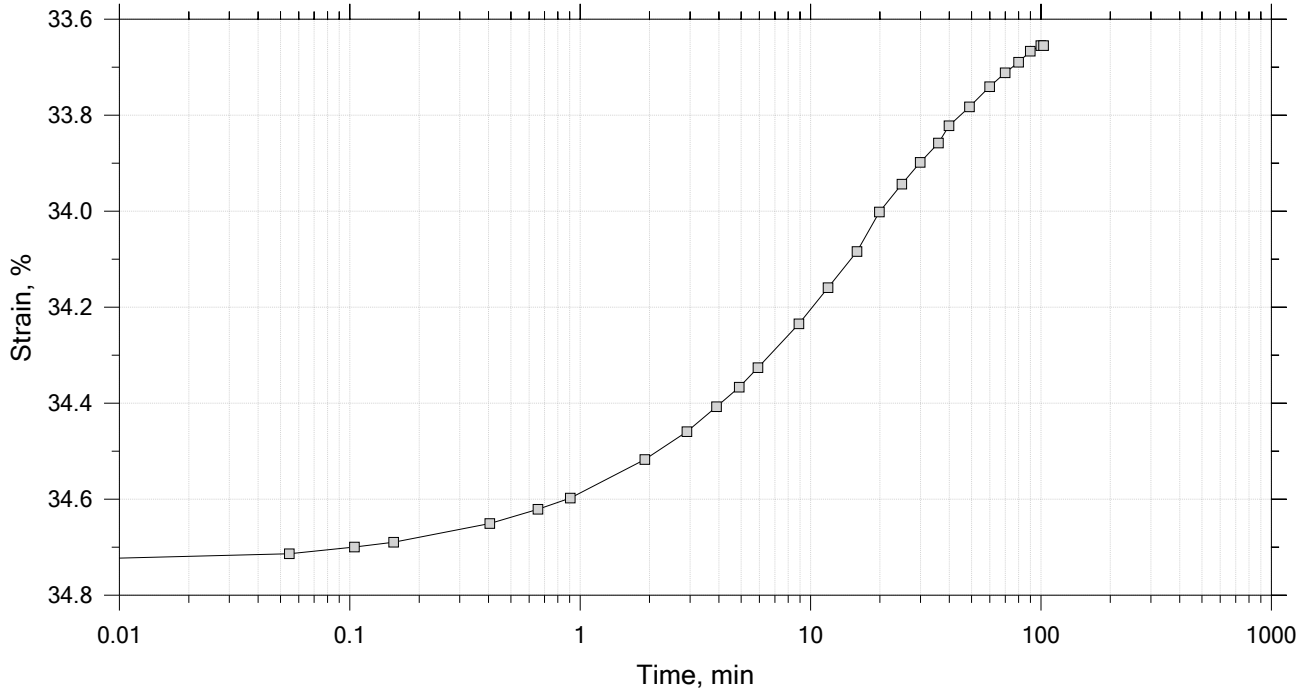
Time Curve 3 of 11  
 Constant Load Step  
 Stress: 500 psf




 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-6	Tested By: jm	Checked By: mcm
	Sample No.: 1	Test Date: 10/19/20	Depth: 0-2 ft
	Test No.: IP-10	Sample Type: intact	Elevation: ---
	Description: Moist, dark grayish brown clay(OH)		

# One-Dimensional Consolidation by ASTM D2435 - Method B

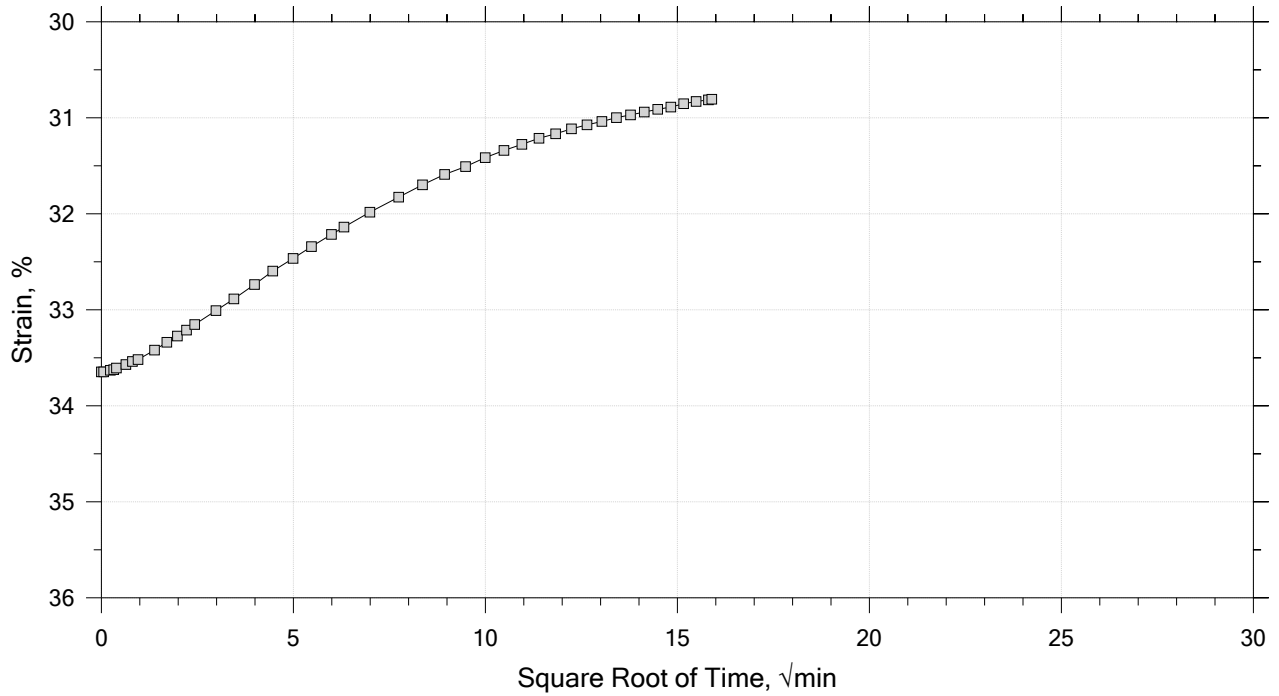
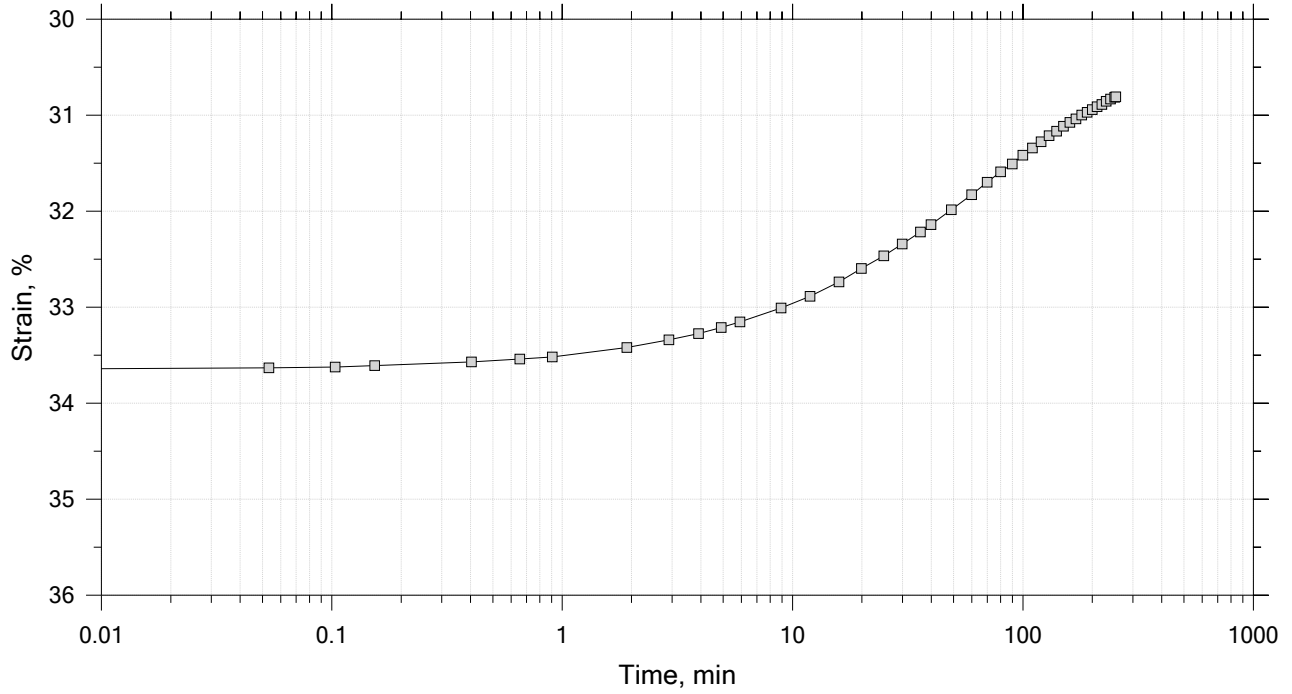
Time Curve 4 of 11  
 Constant Load Step  
 Stress: 250 psf




 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-6	Tested By: jm	Checked By: mcm
	Sample No.: 1	Test Date: 10/19/20	Depth: 0-2 ft
	Test No.: IP-10	Sample Type: intact	Elevation: ---
	Description: Moist, dark grayish brown clay(OH)		

# One-Dimensional Consolidation by ASTM D2435 - Method B

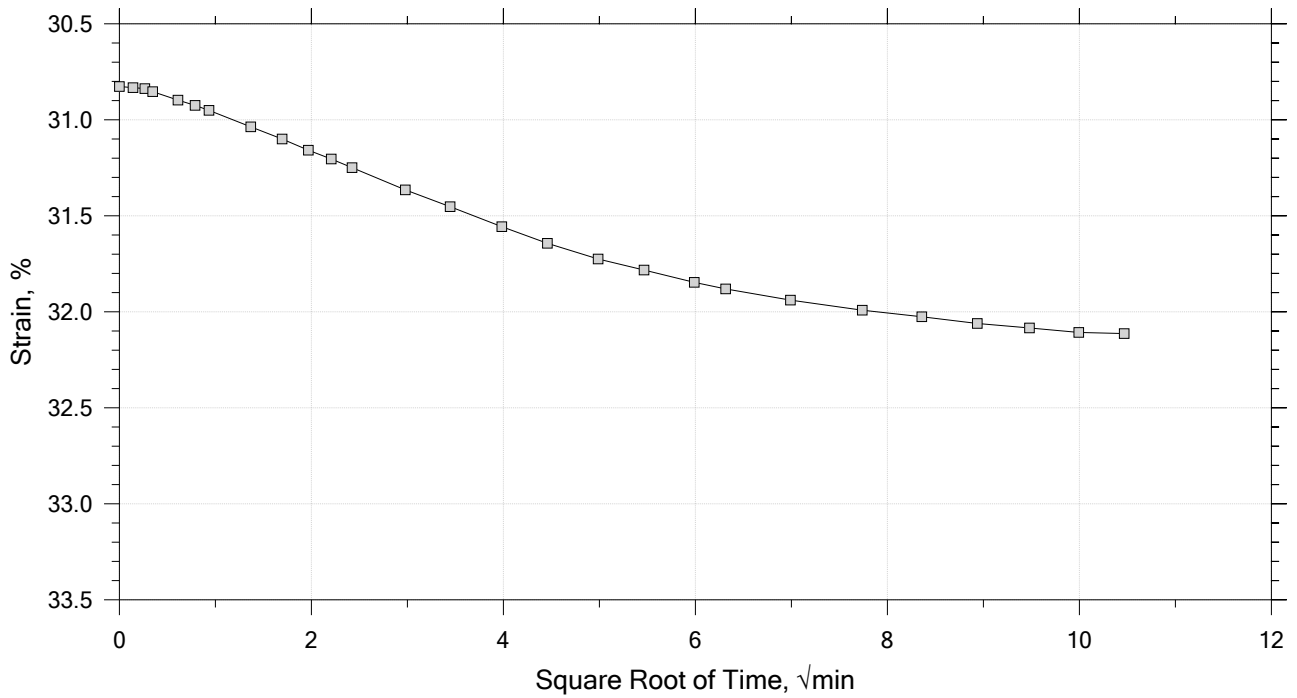
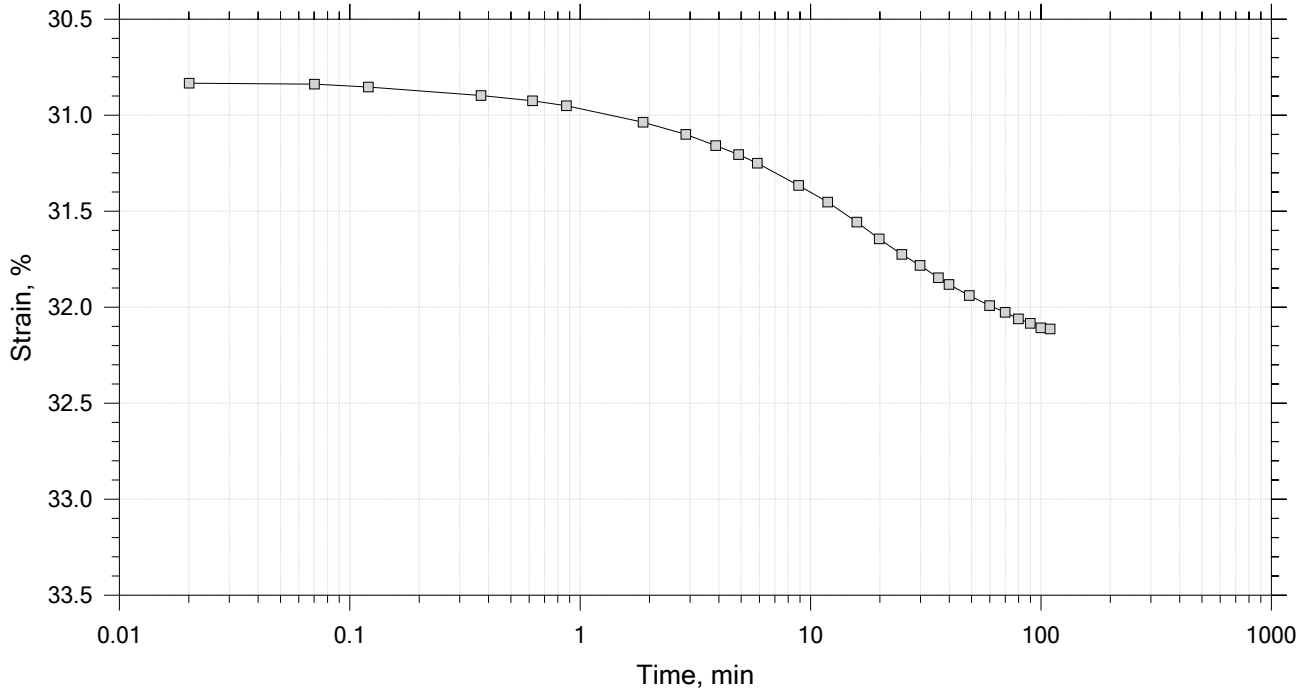
Time Curve 5 of 11  
 Constant Load Step  
 Stress: 100 psf




 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-6	Tested By: jm	Checked By: mcm
	Sample No.:1	Test Date: 10/19/20	Depth: 0-2 ft
	Test No.: IP-10	Sample Type: intact	Elevation: ---
	Description: Moist, dark grayish brown clay(OH)		

# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 6 of 11  
 Constant Load Step  
 Stress: 250 psf

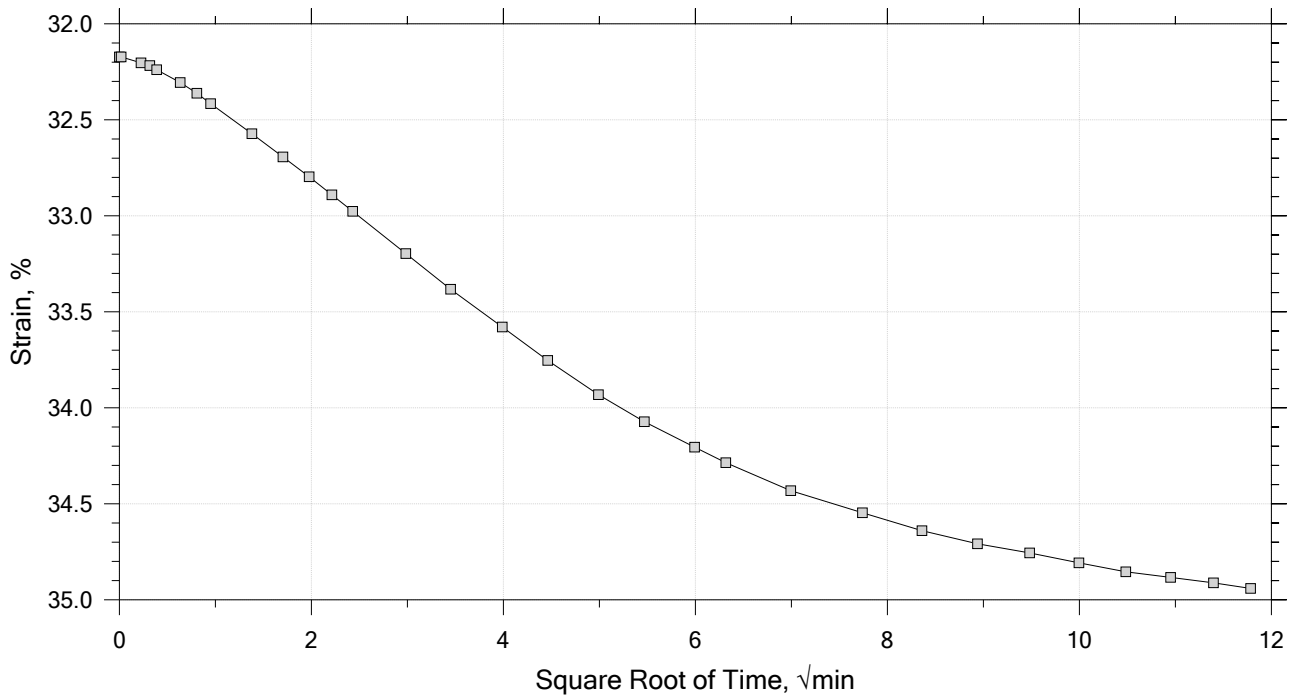
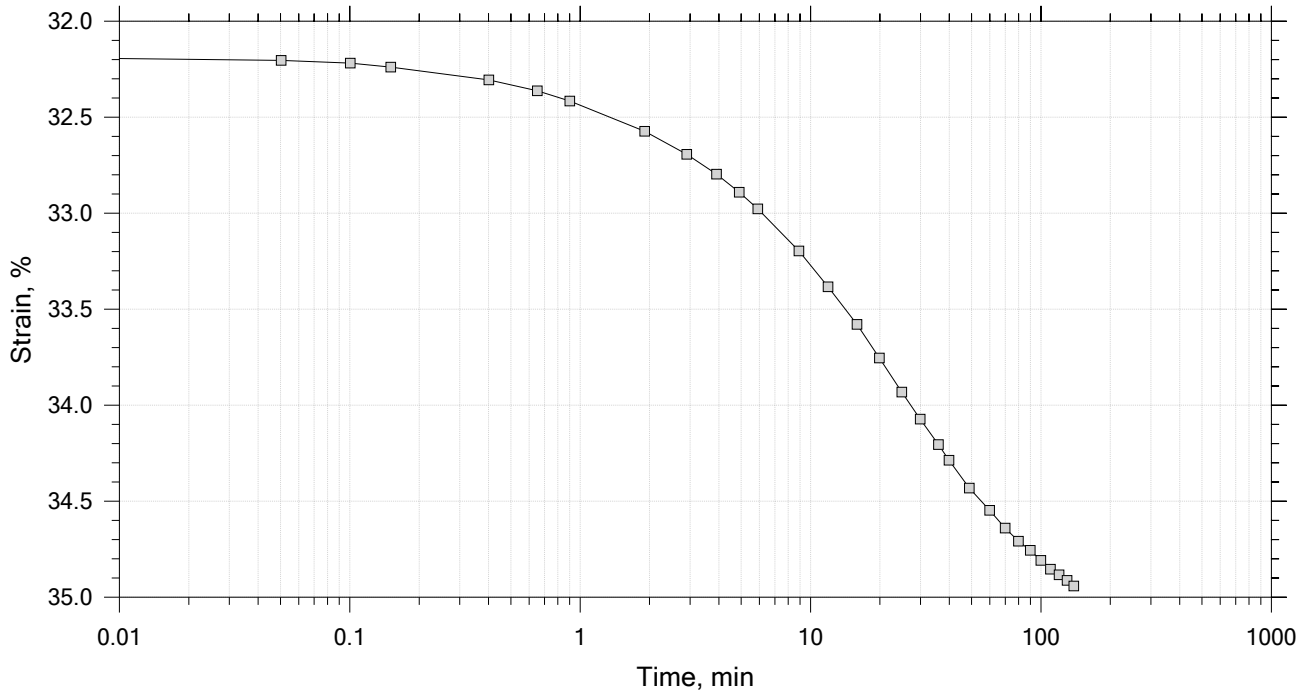



 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-6	Tested By: jm	Checked By: mcm
	Sample No.: 1	Test Date: 10/19/20	Depth: 0-2 ft
	Test No.: IP-10	Sample Type: intact	Elevation: ---
	Description: Moist, dark grayish brown clay(OH)		



# One-Dimensional Consolidation by ASTM D2435 - Method B

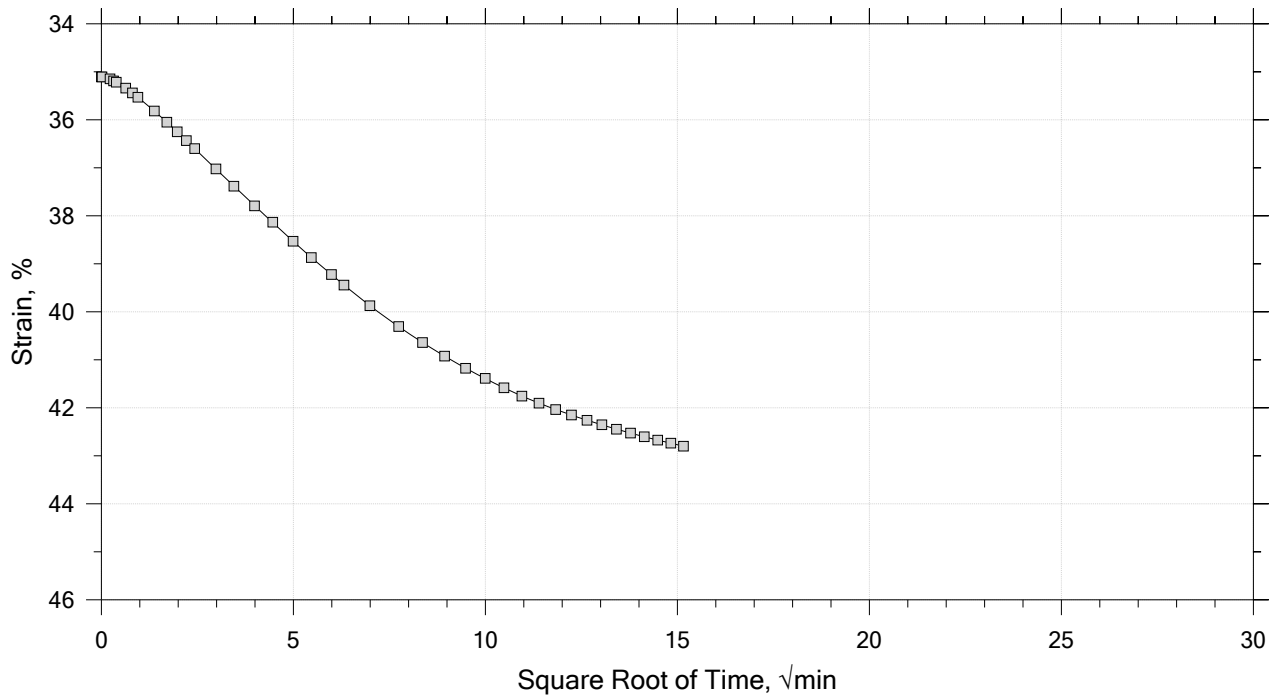
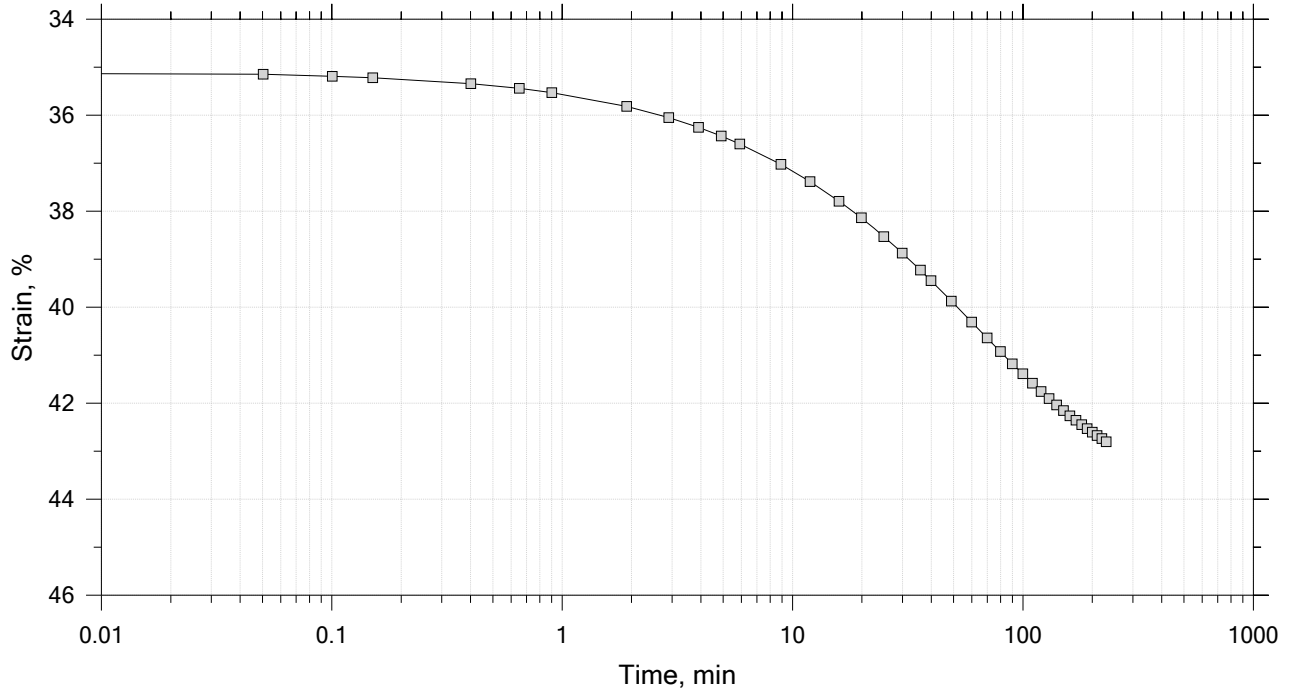
Time Curve 7 of 11  
 Constant Load Step  
 Stress: 500 psf




 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-6	Tested By: jm	Checked By: mcm
	Sample No.: 1	Test Date: 10/19/20	Depth: 0-2 ft
	Test No.: IP-10	Sample Type: intact	Elevation: ---
	Description: Moist, dark grayish brown clay(OH)		

# One-Dimensional Consolidation by ASTM D2435 - Method B

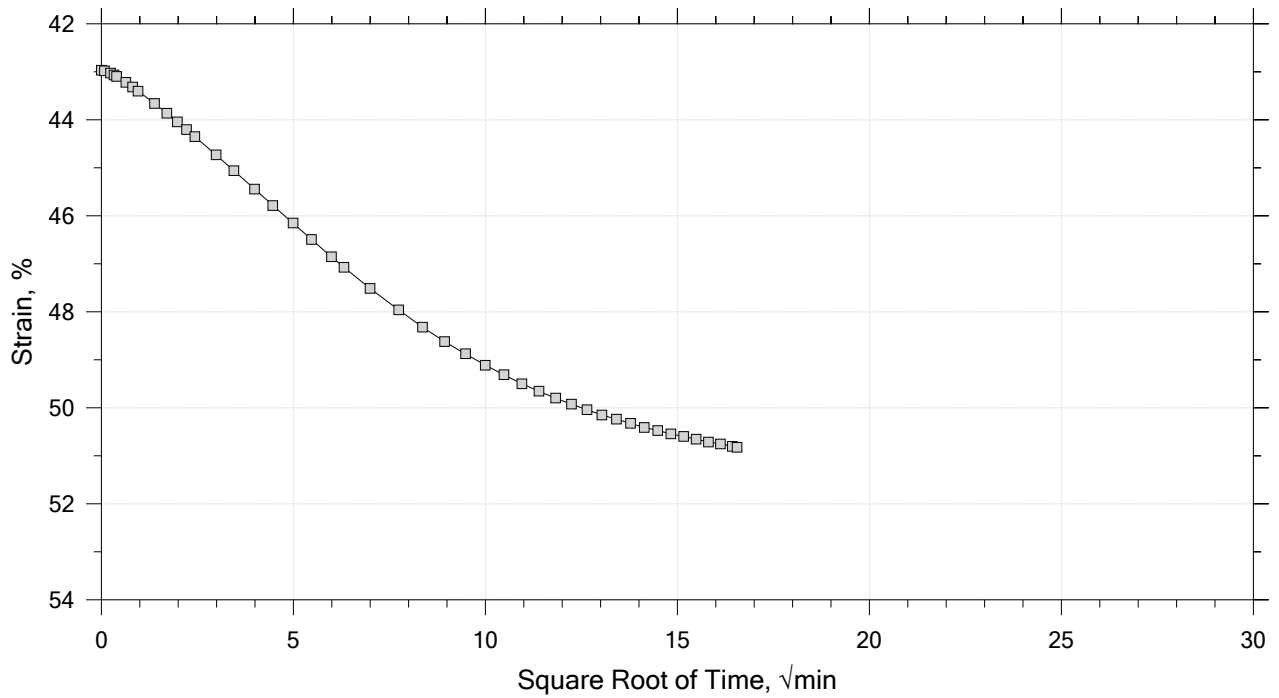
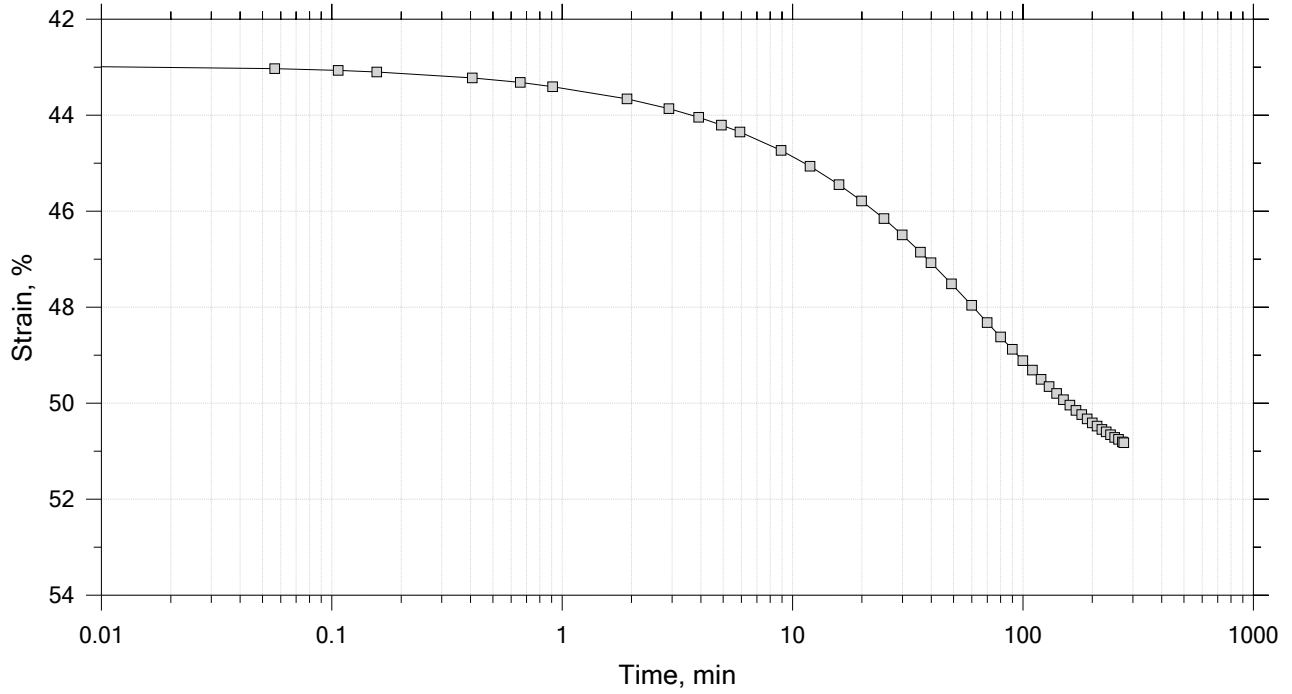
Time Curve 8 of 11  
 Constant Load Step  
 Stress: 1e+03 psf




 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-6	Tested By: jm	Checked By: mcm
	Sample No.: 1	Test Date: 10/19/20	Depth: 0-2 ft
	Test No.: IP-10	Sample Type: intact	Elevation: ---
	Description: Moist, dark grayish brown clay(OH)		

# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 9 of 11  
 Constant Load Step  
 Stress: 2e+03 psf



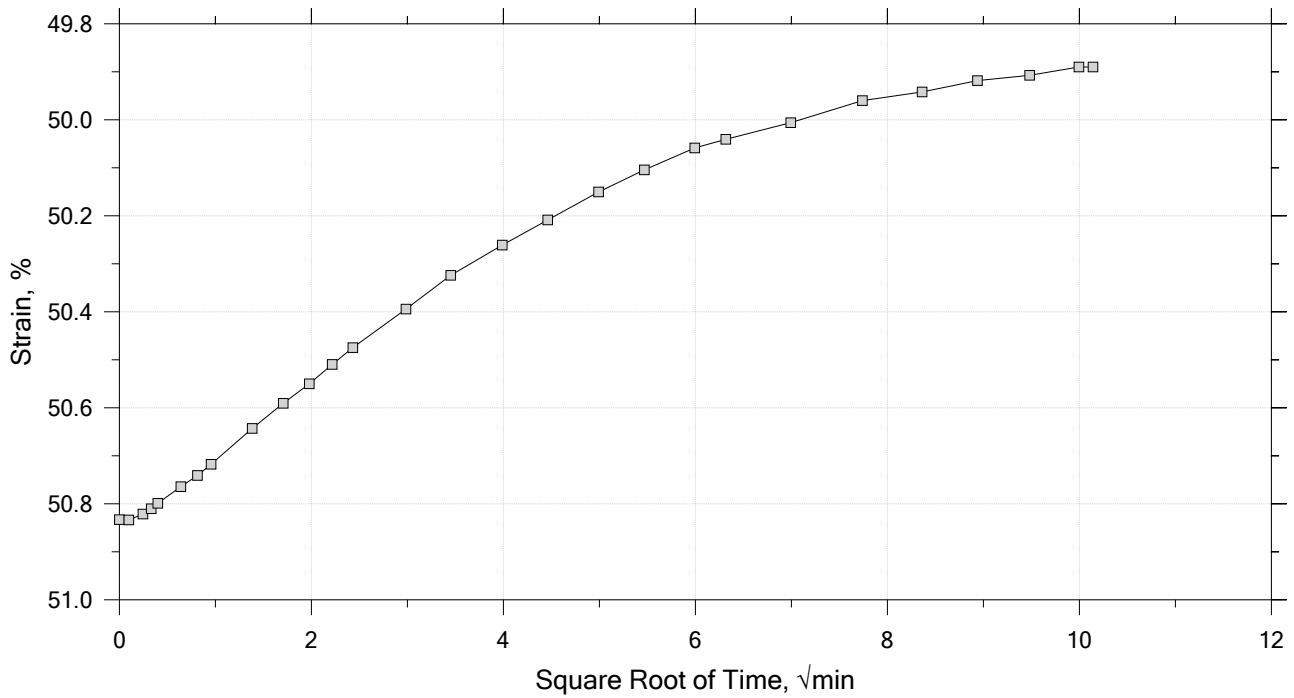
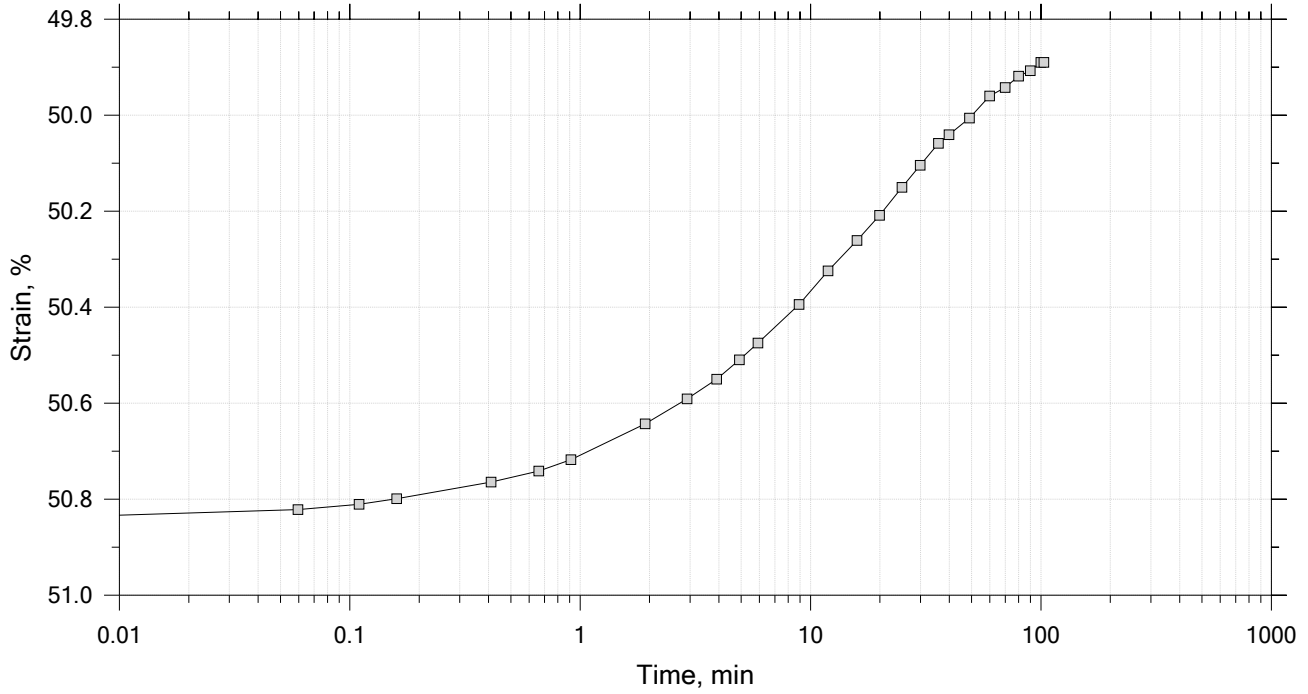
 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-6	Tested By: jm	Checked By: mcm
	Sample No.: 1	Test Date: 10/19/20	Depth: 0-2 ft
	Test No.: IP-10	Sample Type: intact	Elevation: ---
	Description: Moist, dark grayish brown clay(OH)		


# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 10 of 11

Constant Load Step

Stress: 1e+03 psf



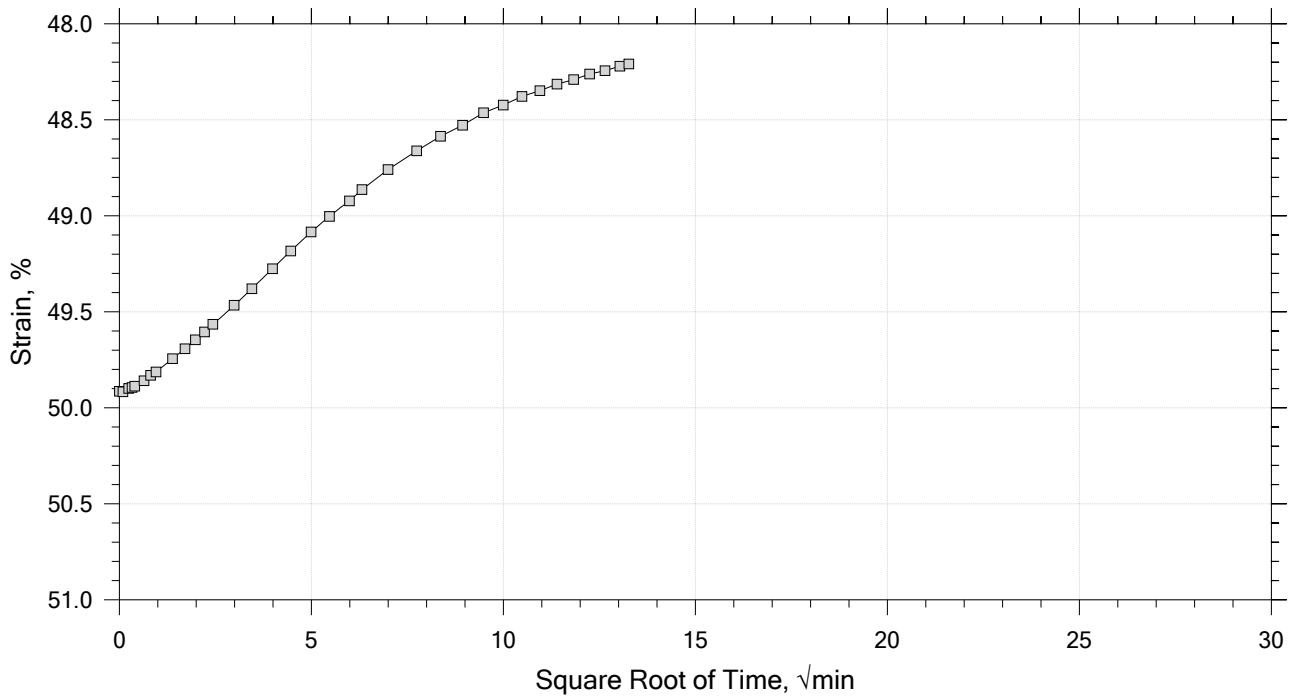
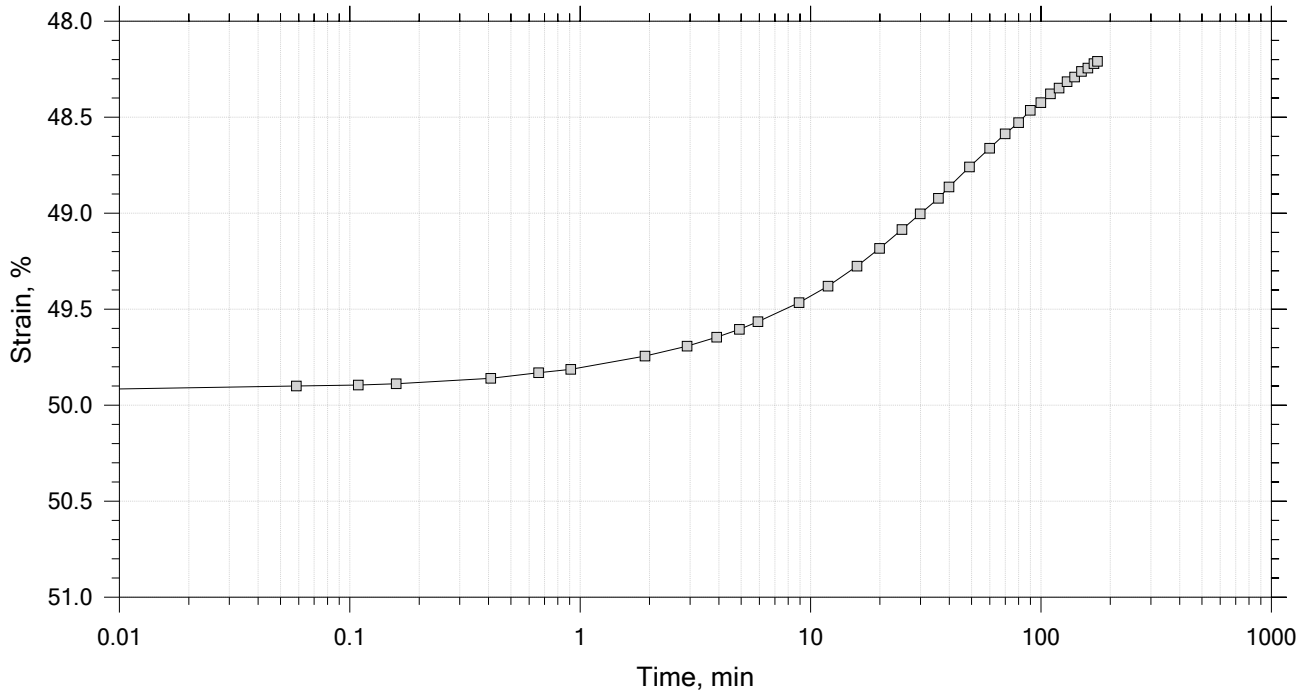
 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-6	Tested By: jm	Checked By: mcm
	Sample No.: 1	Test Date: 10/19/20	Depth: 0-2 ft
	Test No.: IP-10	Sample Type: intact	Elevation: ---
	Description: Moist, dark grayish brown clay(OH)		


# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 11 of 11

Constant Load Step

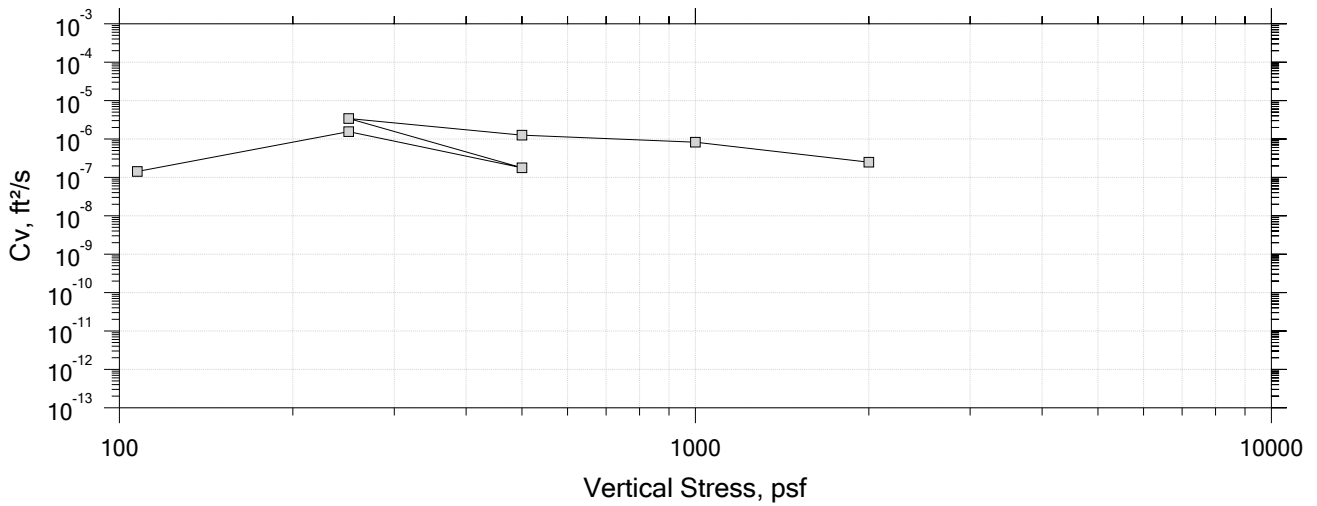
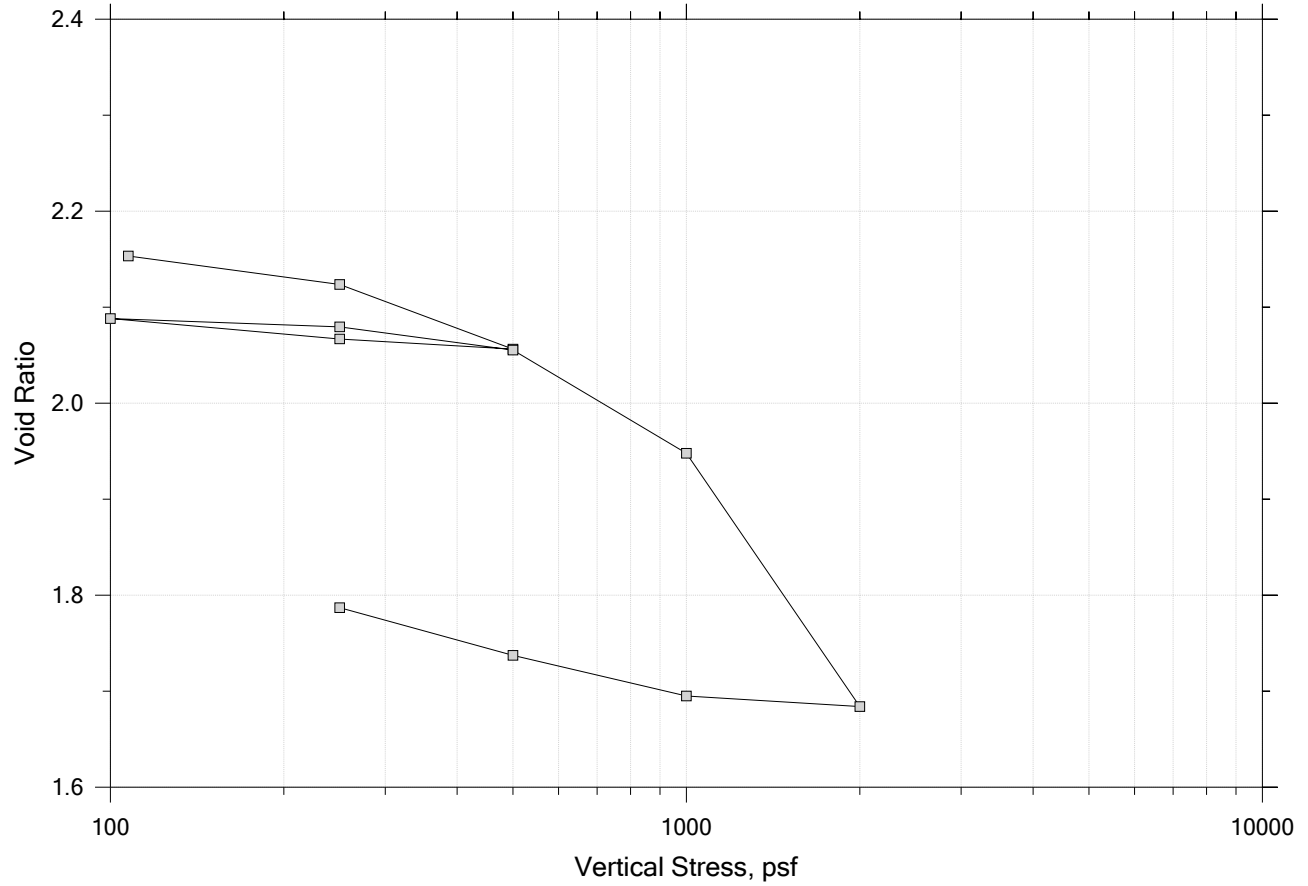
Stress: 500 psf




 <p>Engineering and Testing</p>	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-6	Tested By: jm	Checked By: mcm
	Sample No.: 1	Test Date: 10/19/20	Depth: 0-2 ft
	Test No.: IP-10	Sample Type: intact	Elevation: ---
	Description: Moist, dark grayish brown clay(OH)		

# One-Dimensional Consolidation by ASTM D2435 - Method B

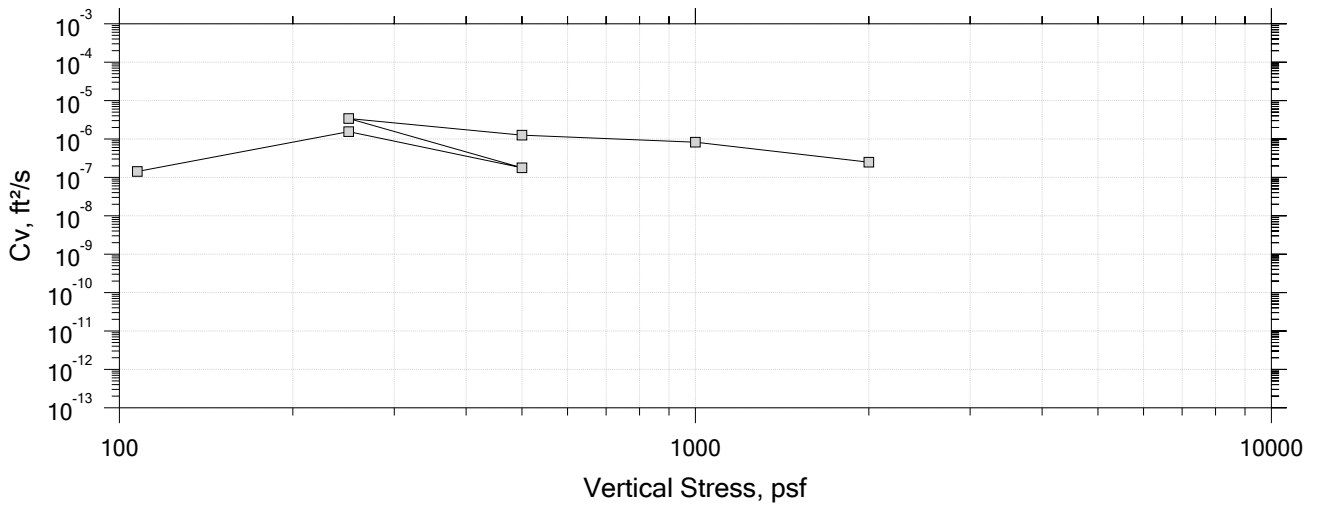
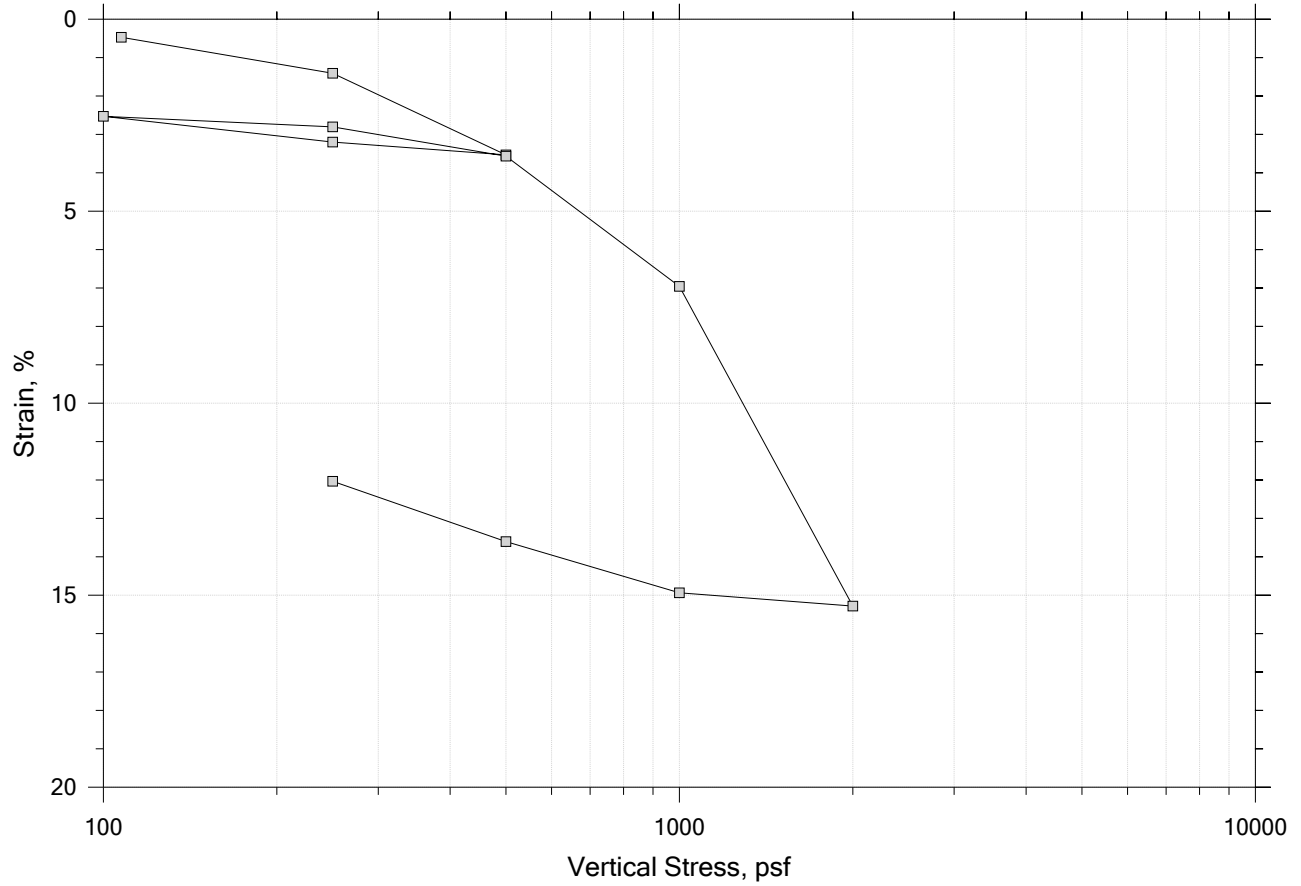
## Summary Report




 <p>APS Engineering and Testing</p>	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-6	Tested By: jm	Checked By: mcm
	Sample No.: 7	Test Date: 10/16/20	Depth: 12-14 ft
	Test No.: IP-11	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay(CH)	Measured specific gravity: 2.59	

# One-Dimensional Consolidation by ASTM D2435 - Method B

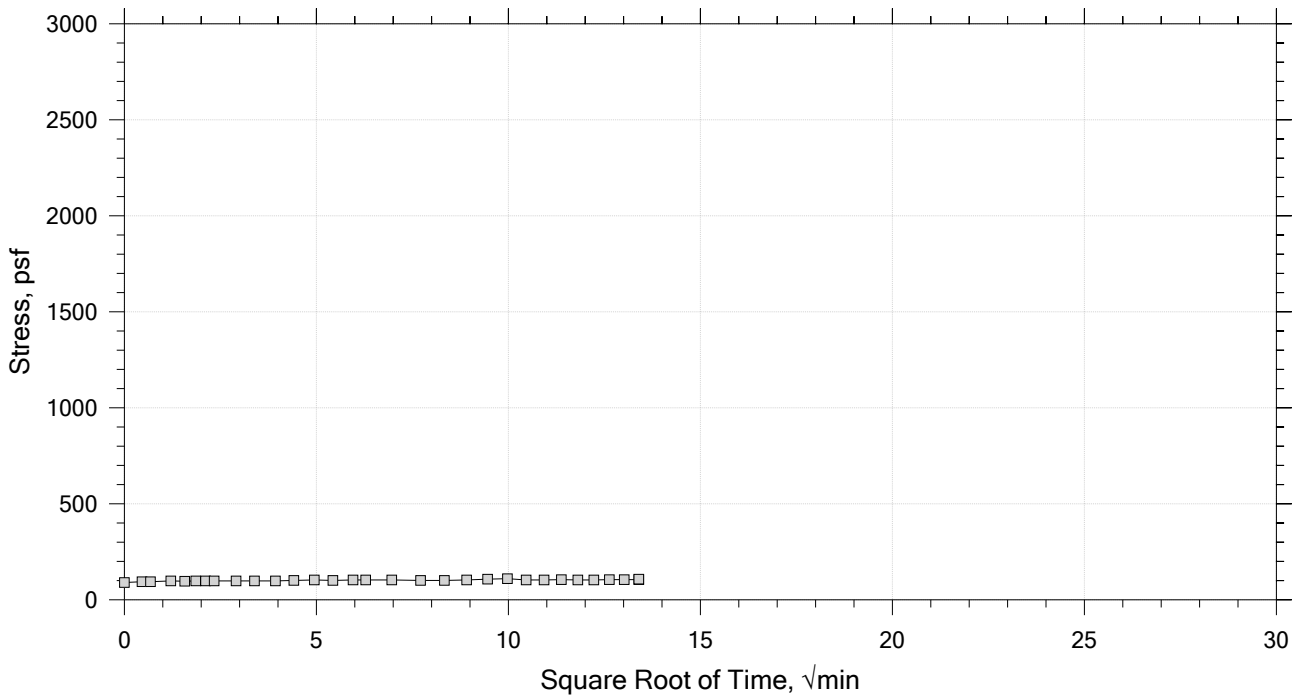
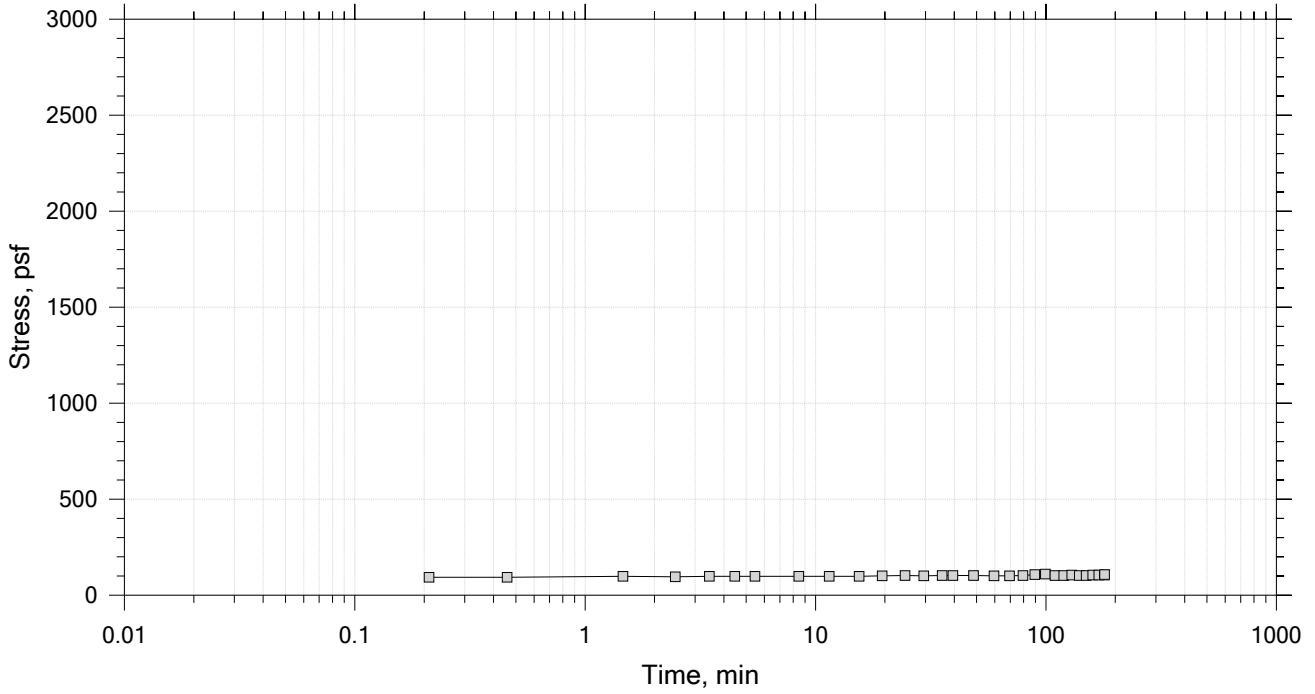
## Summary Report




 <p>Engineering and Testing</p>	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-6	Tested By: jm	Checked By: mcm
	Sample No.: 7	Test Date: 10/16/20	Depth: 12-14 ft
	Test No.: IP-11	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay (CH)		

# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 1 of 12  
 Constant Volume Step  
 Stress: 107 psf

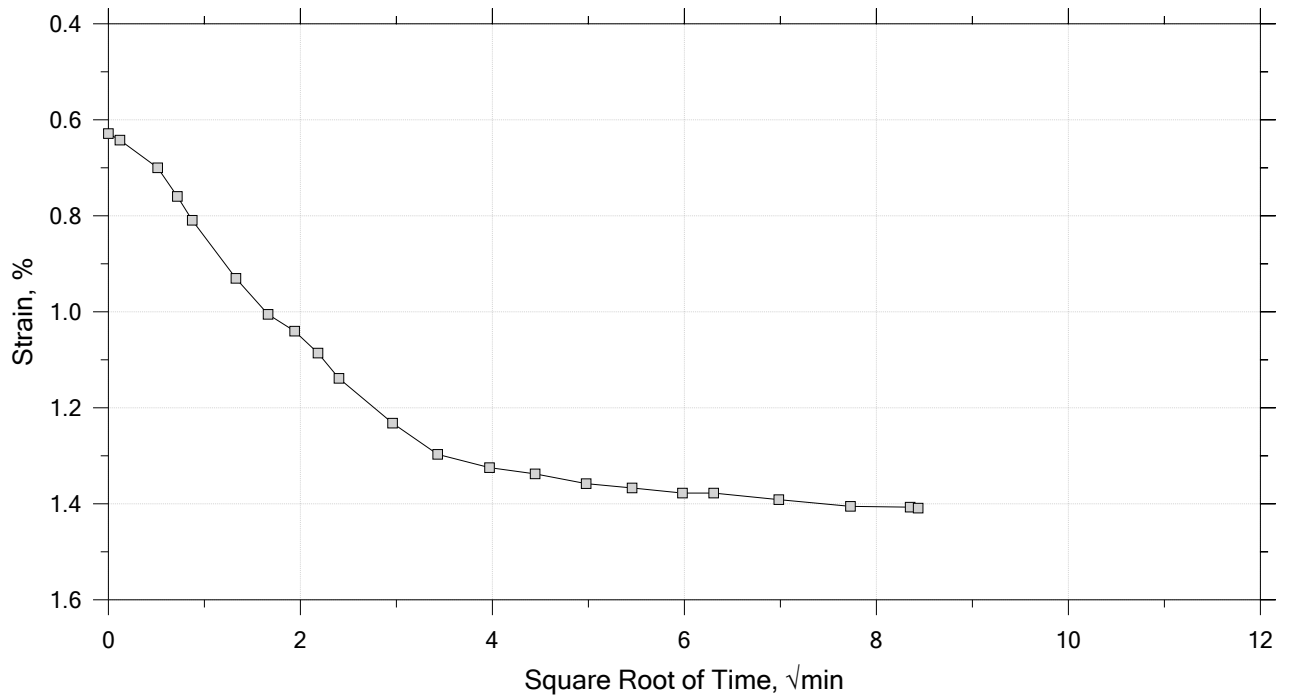
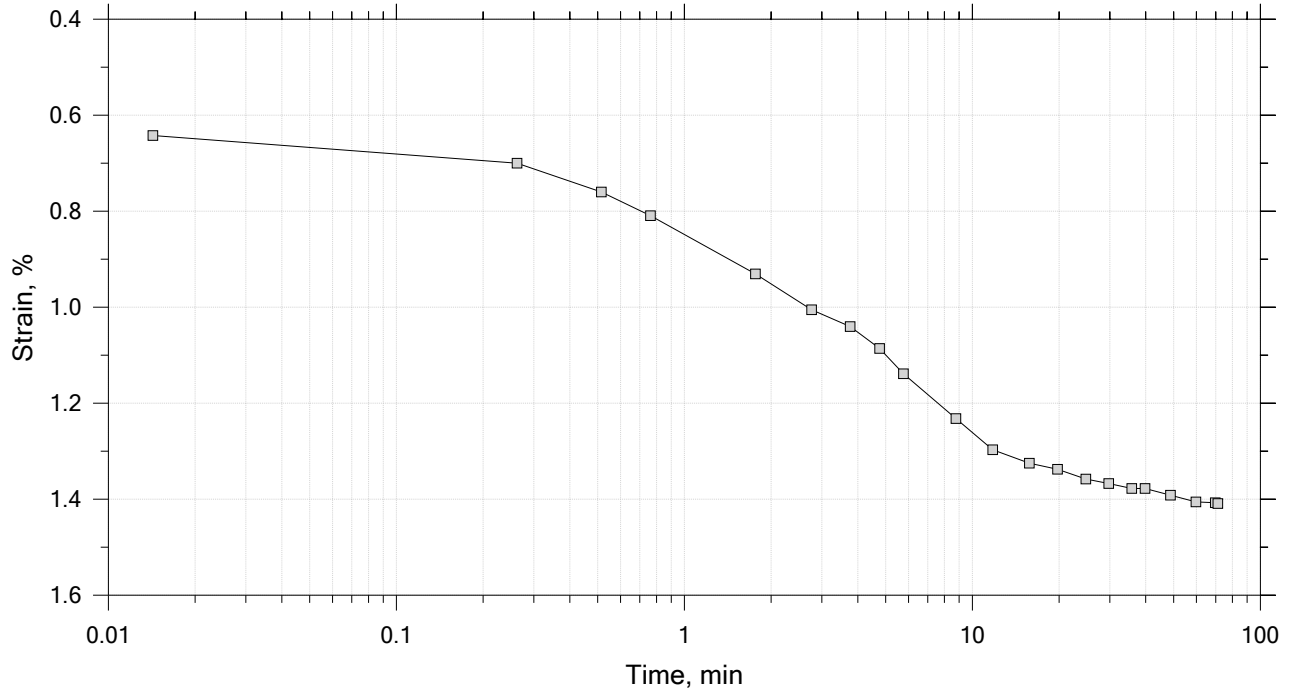



 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-6	Tested By: jm	Checked By: mcm
	Sample No.: 7	Test Date: 10/16/20	Depth: 12-14 ft
	Test No.: IP-11	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay(CH)		



# One-Dimensional Consolidation by ASTM D2435 - Method B

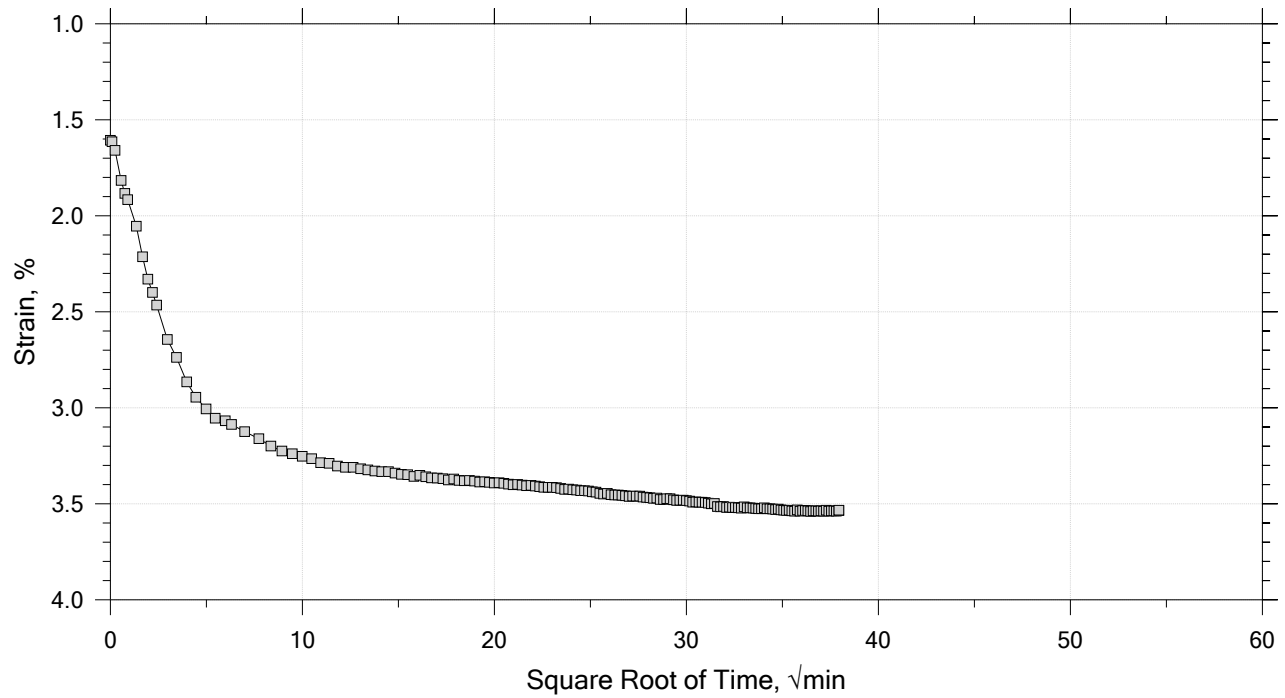
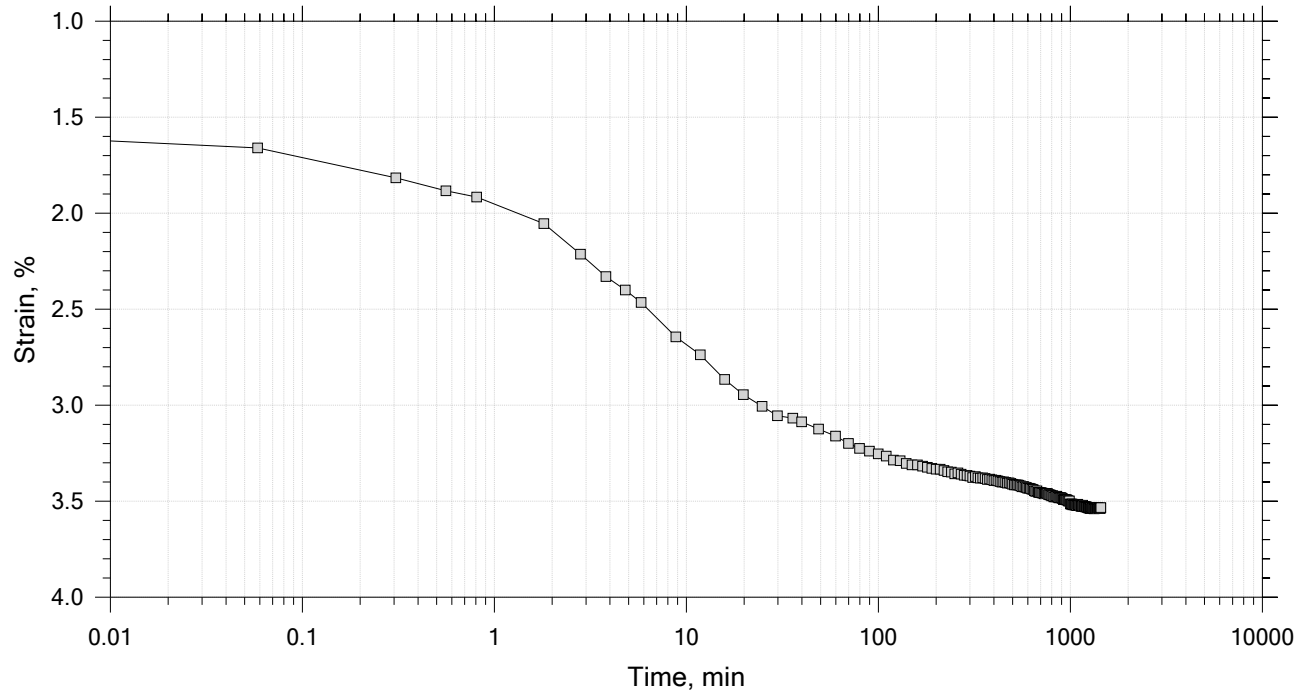
Time Curve 2 of 12  
 Constant Load Step  
 Stress: 250 psf




 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-6	Tested By: jm	Checked By: mcm
	Sample No.: 7	Test Date: 10/16/20	Depth: 12-14 ft
	Test No.: IP-11	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay(CH)		

# One-Dimensional Consolidation by ASTM D2435 - Method B

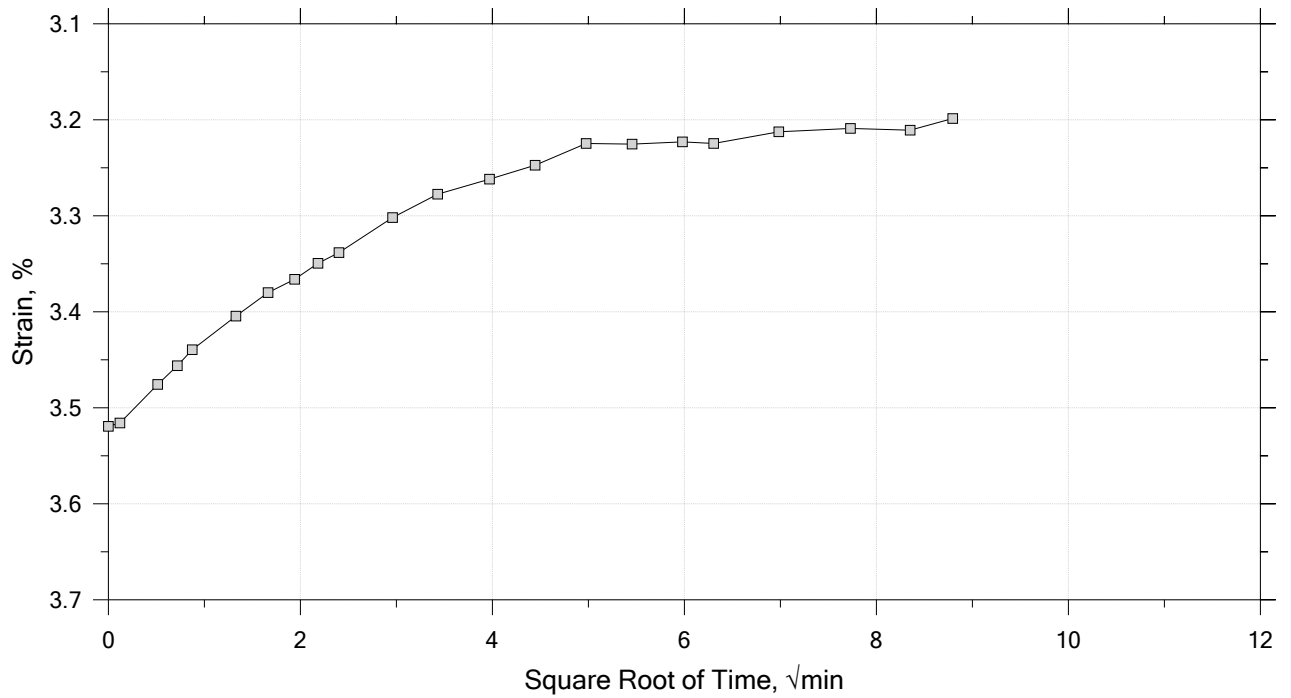
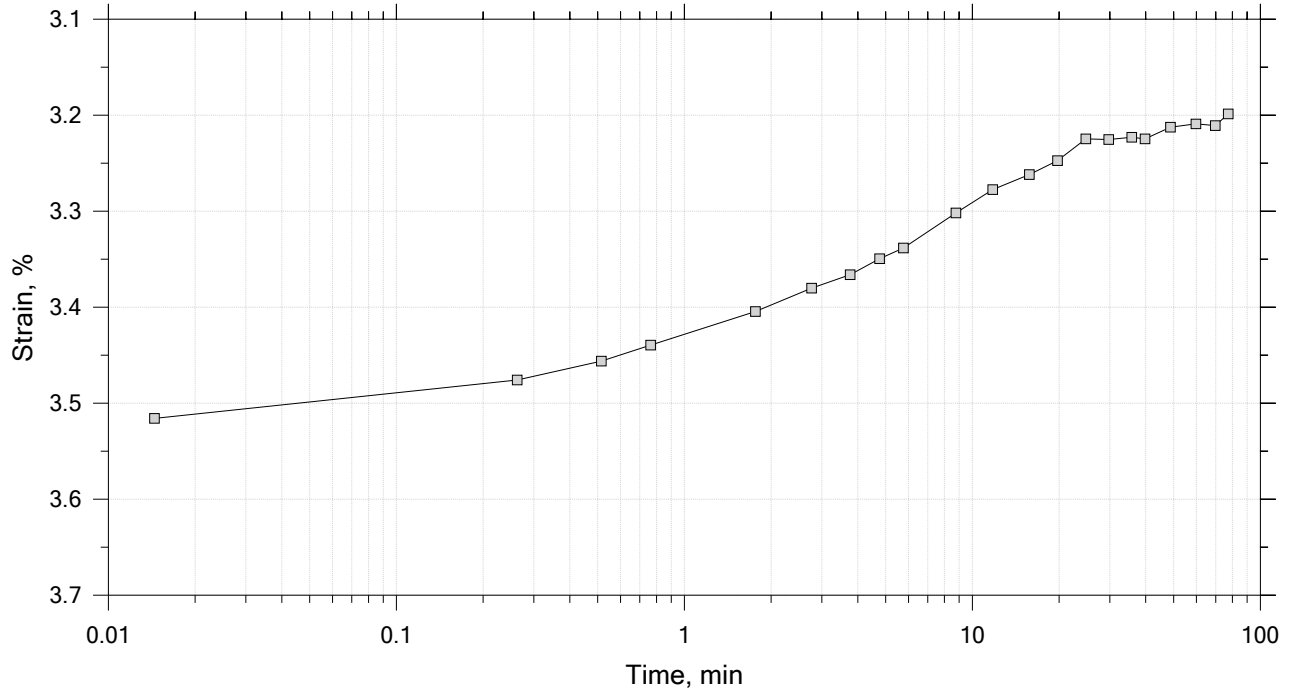
Time Curve 3 of 12  
 Constant Load Step  
 Stress: 500 psf




 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-6	Tested By: jm	Checked By: mcm
	Sample No.: 7	Test Date: 10/16/20	Depth: 12-14 ft
	Test No.: IP-11	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay(CH)		

# One-Dimensional Consolidation by ASTM D2435 - Method B

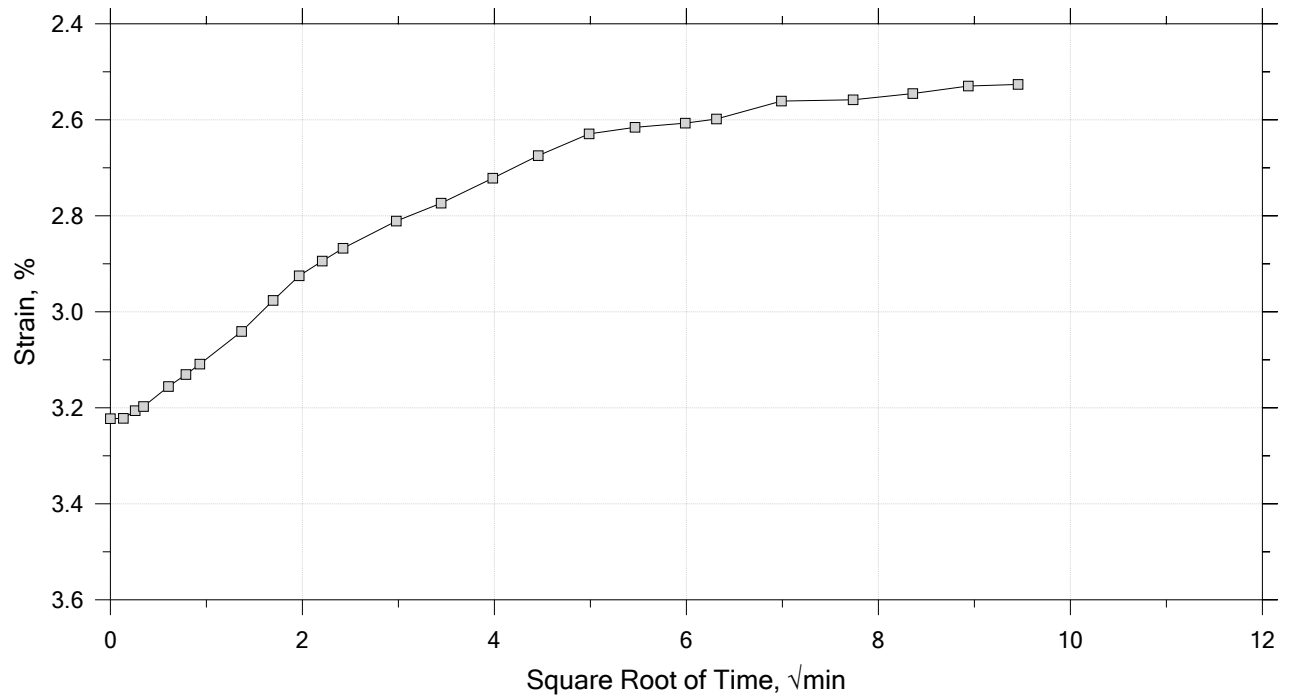
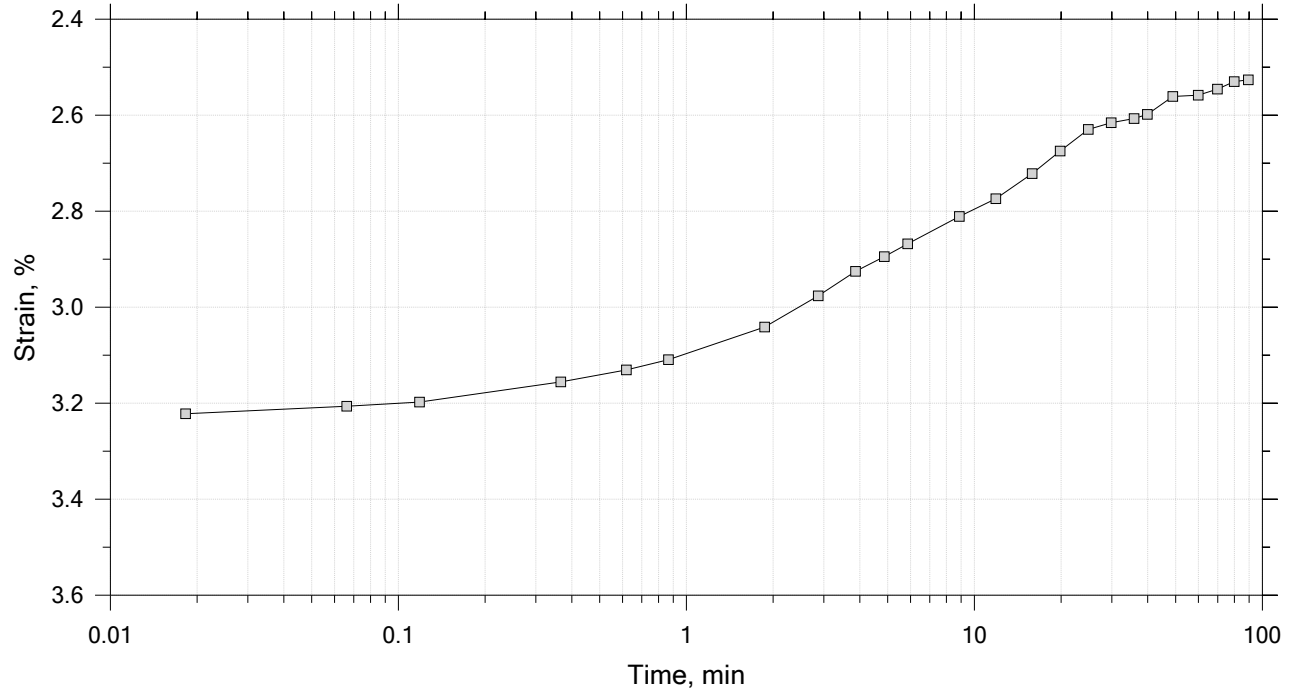
Time Curve 4 of 12  
 Constant Load Step  
 Stress: 250 psf




 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-6	Tested By: jm	Checked By: mcm
	Sample No.: 7	Test Date: 10/16/20	Depth: 12-14 ft
	Test No.: IP-11	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay(CH)		

# One-Dimensional Consolidation by ASTM D2435 - Method B

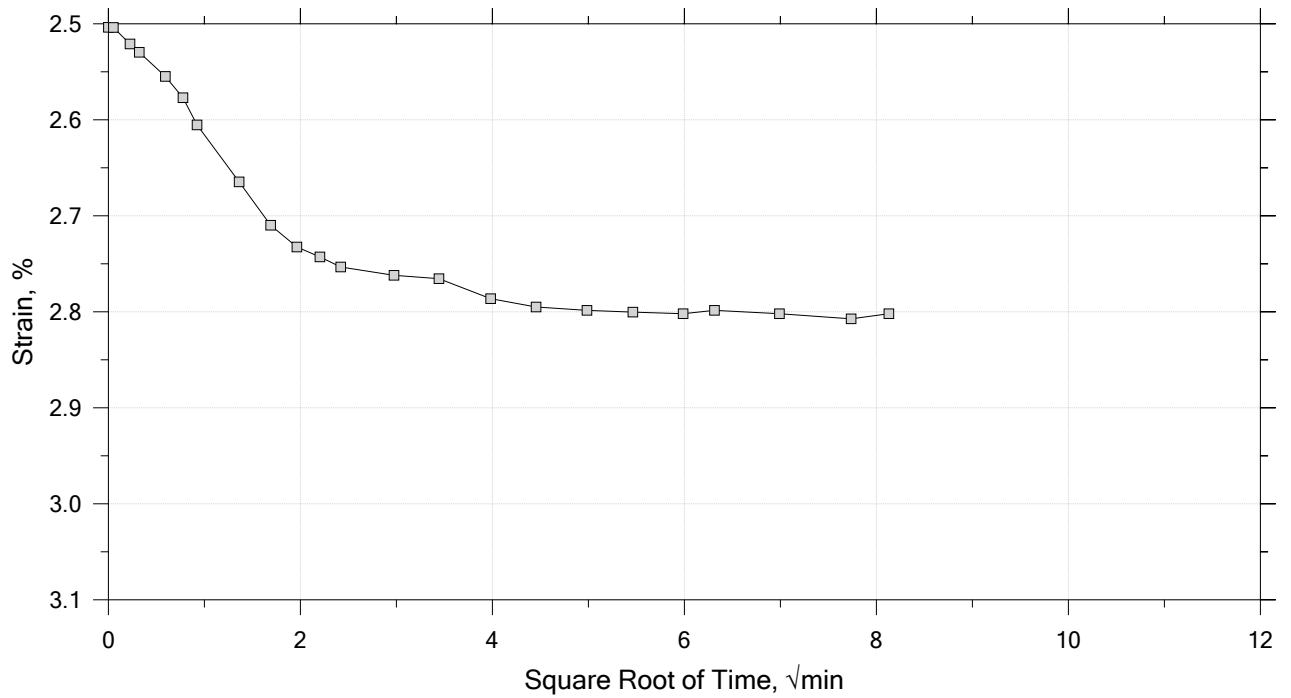
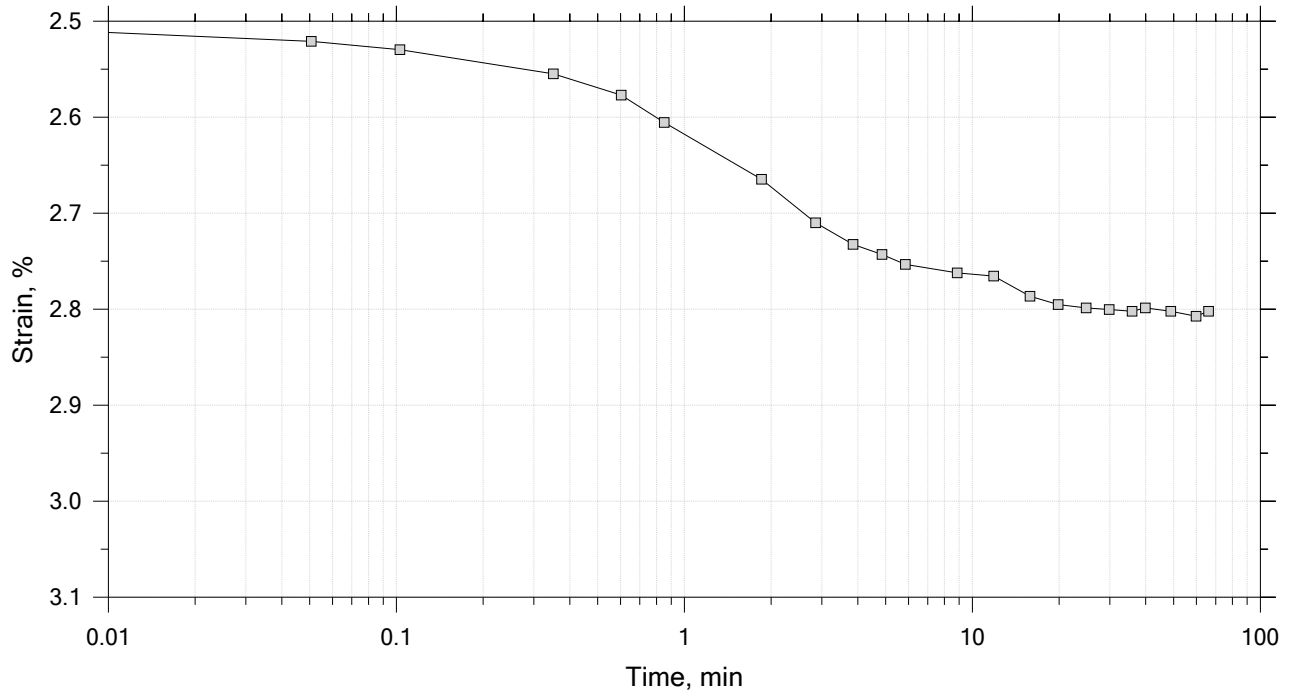
Time Curve 5 of 12  
 Constant Load Step  
 Stress: 100 psf




 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-6	Tested By: jm	Checked By: mcm
	Sample No.: 7	Test Date: 10/16/20	Depth: 12-14 ft
	Test No.: IP-11	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay(CH)		

# One-Dimensional Consolidation by ASTM D2435 - Method B

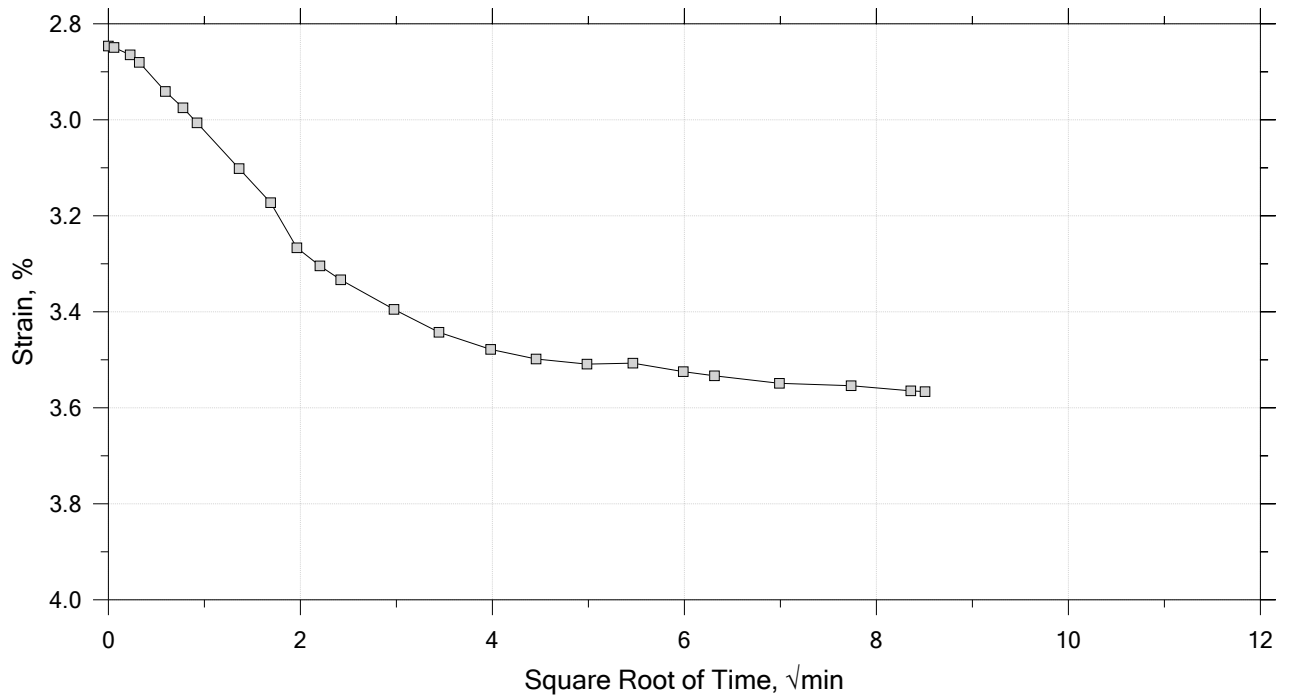
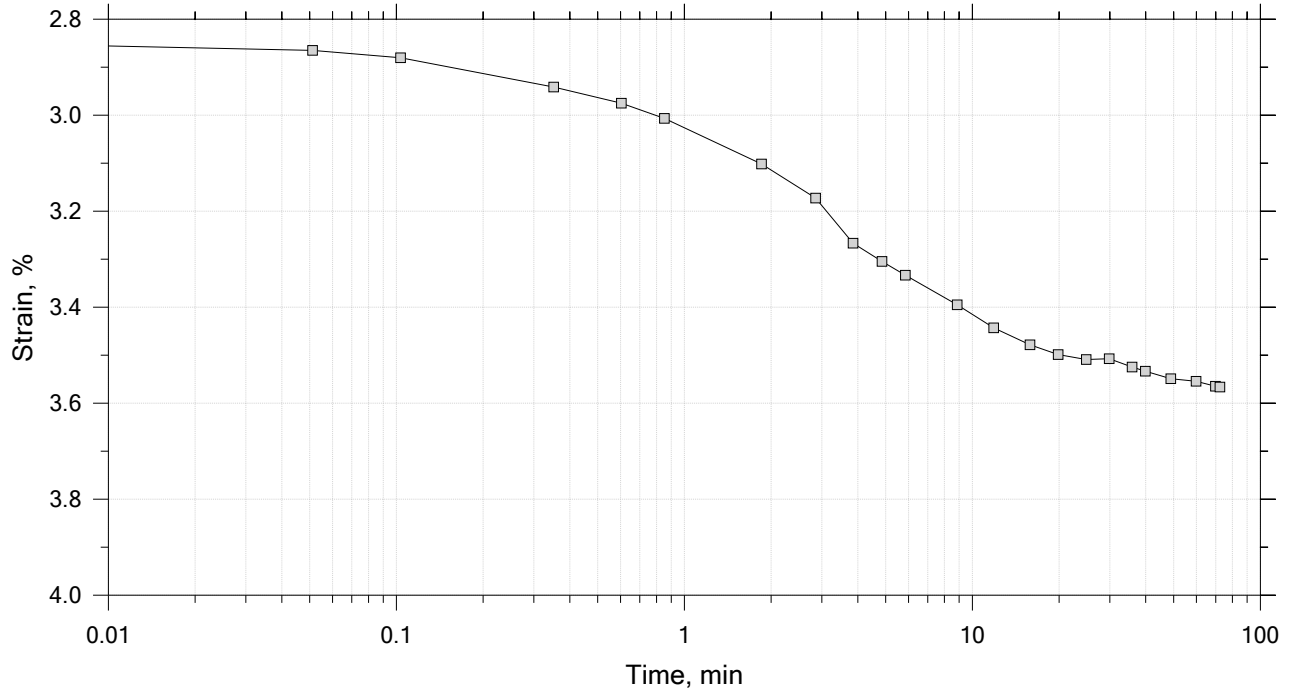
Time Curve 6 of 12  
 Constant Load Step  
 Stress: 250 psf




 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-6	Tested By: jm	Checked By: mcm
	Sample No.: 7	Test Date: 10/16/20	Depth: 12-14 ft
	Test No.: IP-11	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay(CH)		

# One-Dimensional Consolidation by ASTM D2435 - Method B

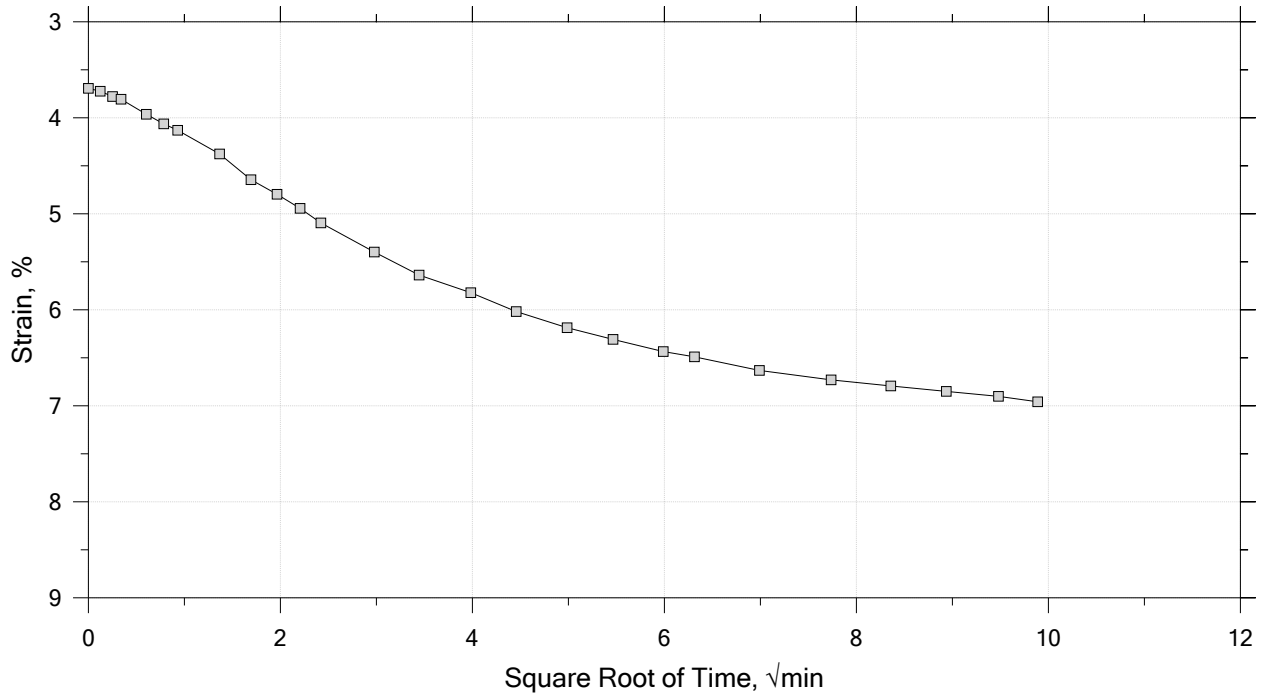
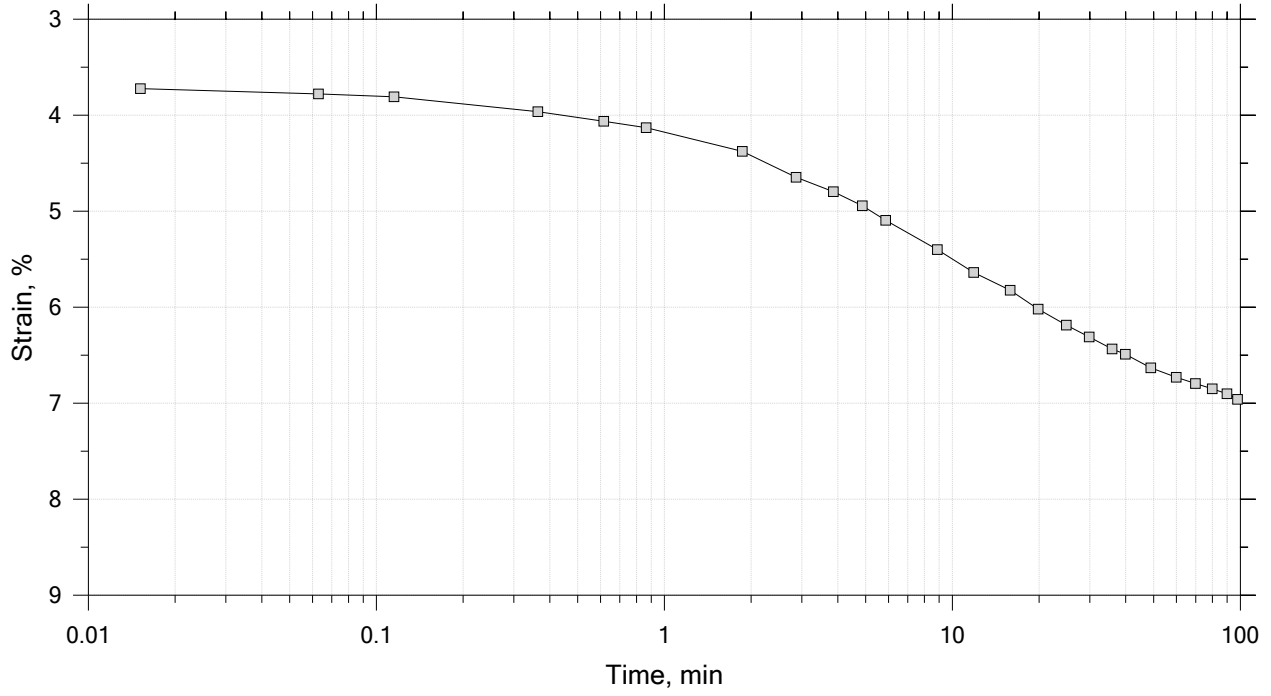
Time Curve 7 of 12  
 Constant Load Step  
 Stress: 500 psf




 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-6	Tested By: jm	Checked By: mcm
	Sample No.: 7	Test Date: 10/16/20	Depth: 12-14 ft
	Test No.: IP-11	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay(CH)		

# One-Dimensional Consolidation by ASTM D2435 - Method B

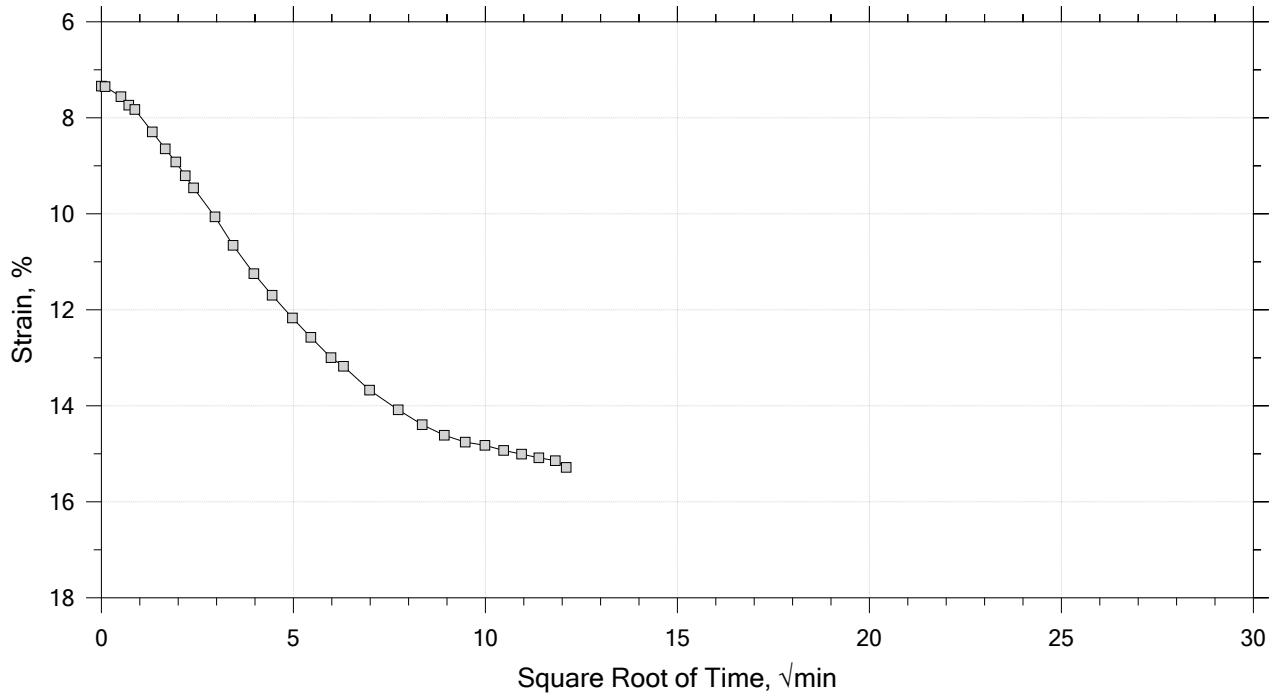
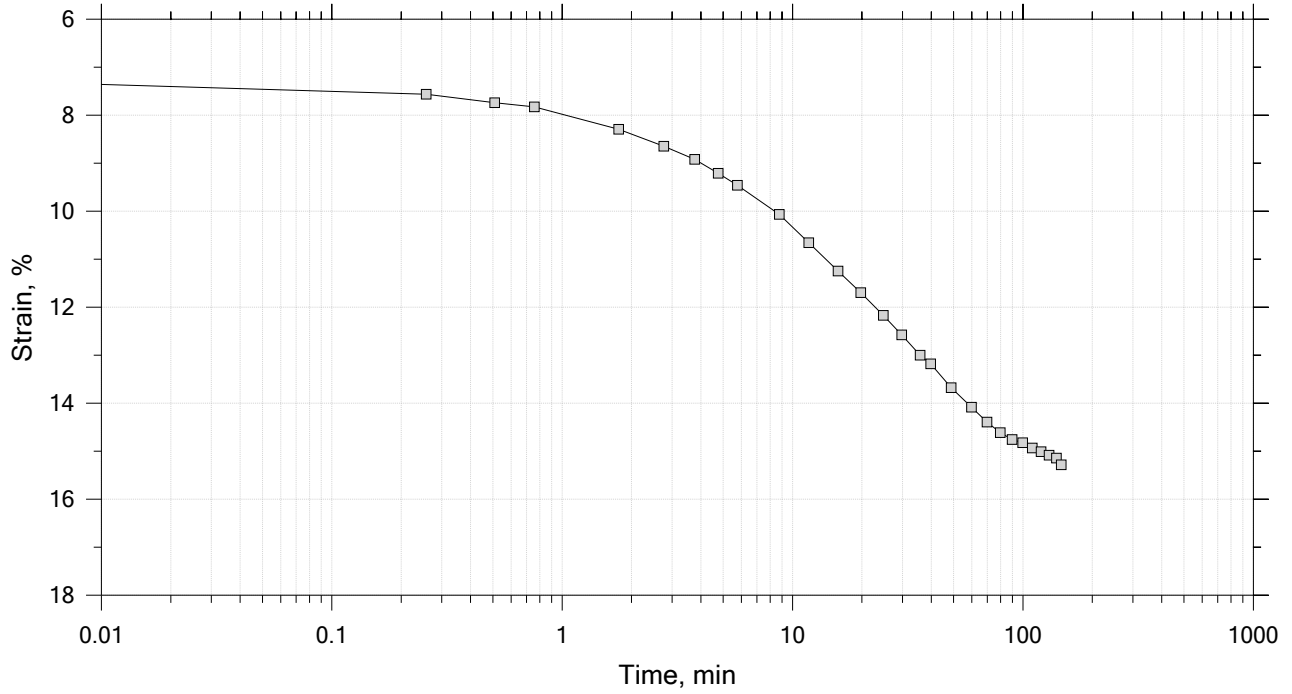
Time Curve 8 of 12  
 Constant Load Step  
 Stress: 1e+03 psf




 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-6	Tested By: jm	Checked By: mcm
	Sample No.: 7	Test Date: 10/16/20	Depth: 12-14 ft
	Test No.: IP-11	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay(CH)		

# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 9 of 12  
 Constant Load Step  
 Stress: 2e+03 psf



 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-6	Tested By: jm	Checked By: mcm
	Sample No.: 7	Test Date: 10/16/20	Depth: 12-14 ft
	Test No.: IP-11	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay(CH)		

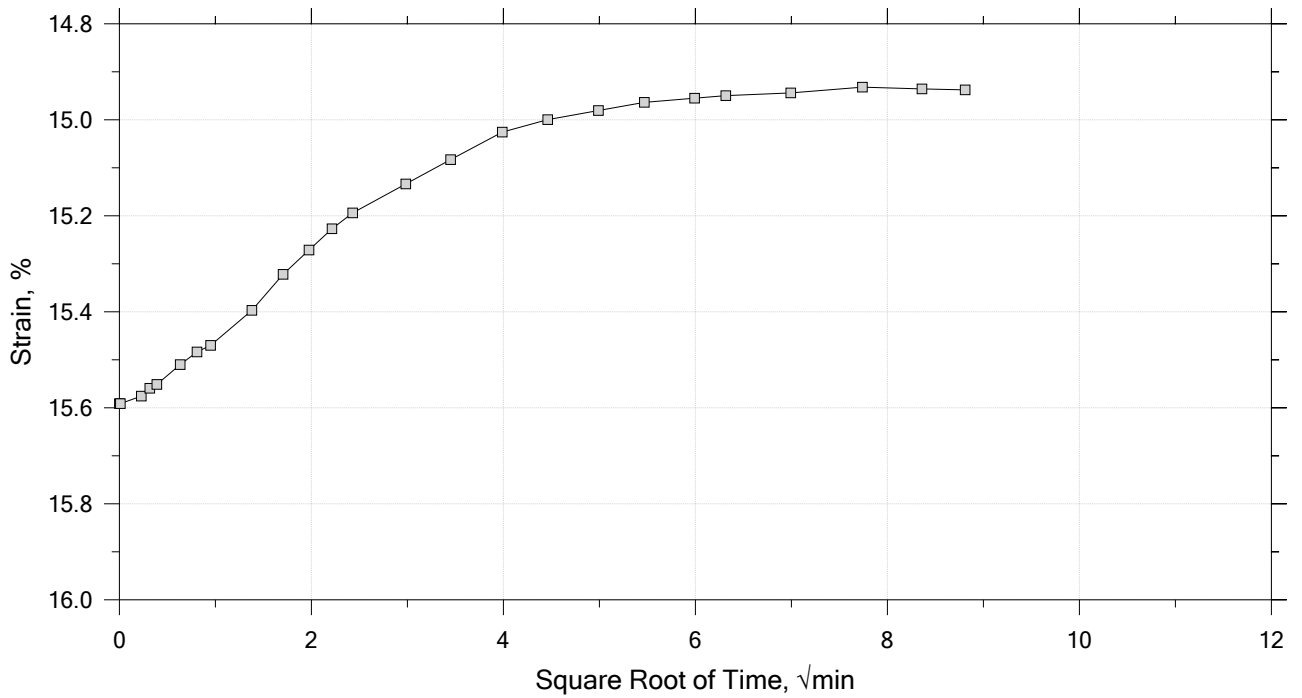
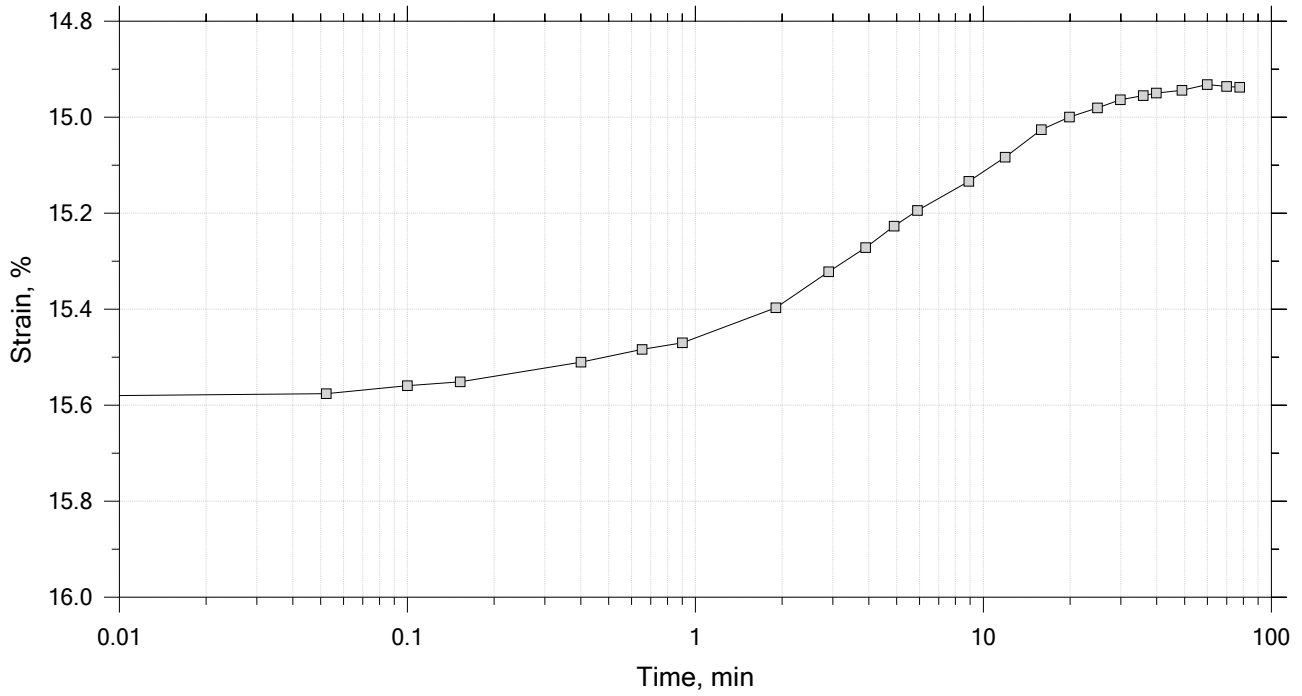



# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 10 of 12

Constant Load Step

Stress: 1e+03 psf



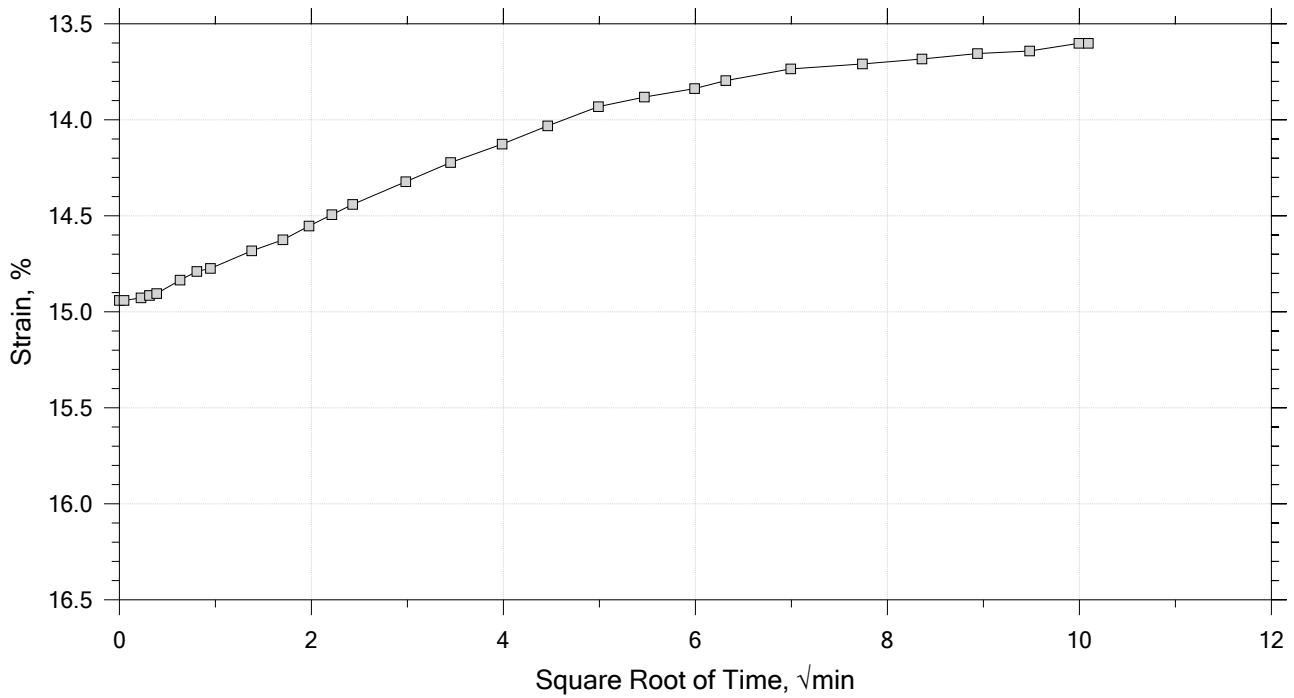
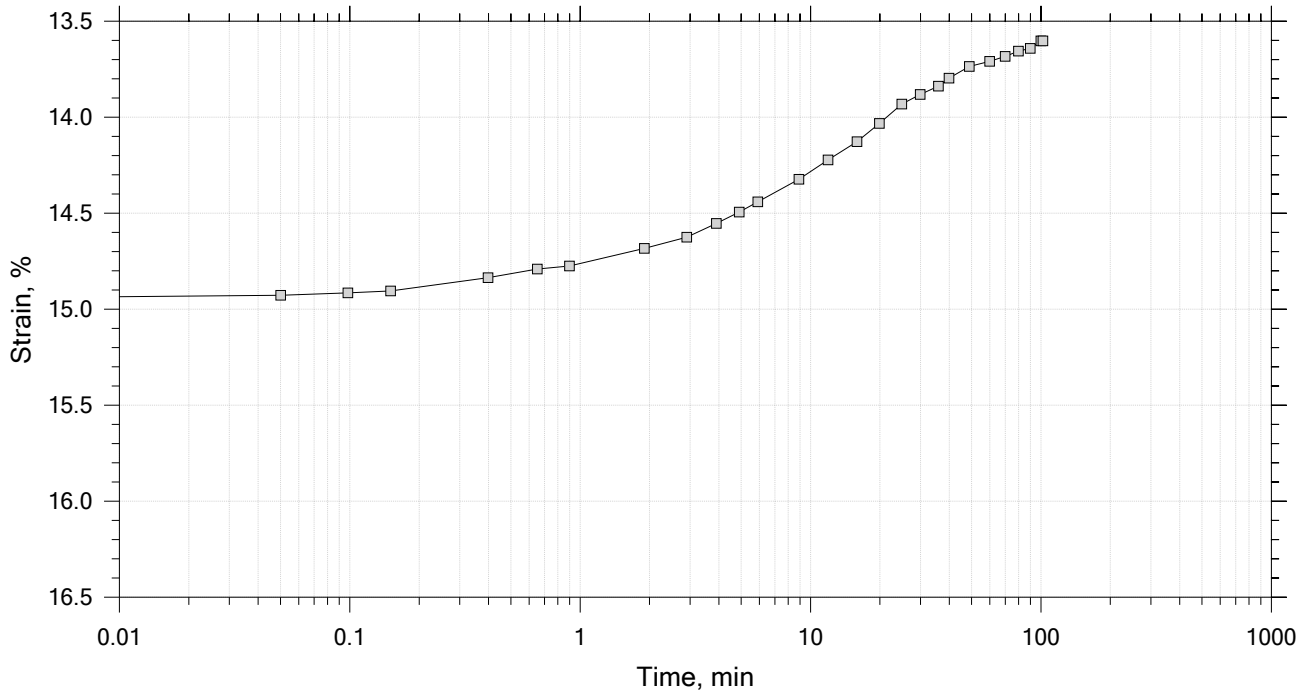
 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-6	Tested By: jm	Checked By: mcm
	Sample No.: 7	Test Date: 10/16/20	Depth: 12-14 ft
	Test No.: IP-11	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay(CH)		


# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 11 of 12

Constant Load Step

Stress: 500 psf



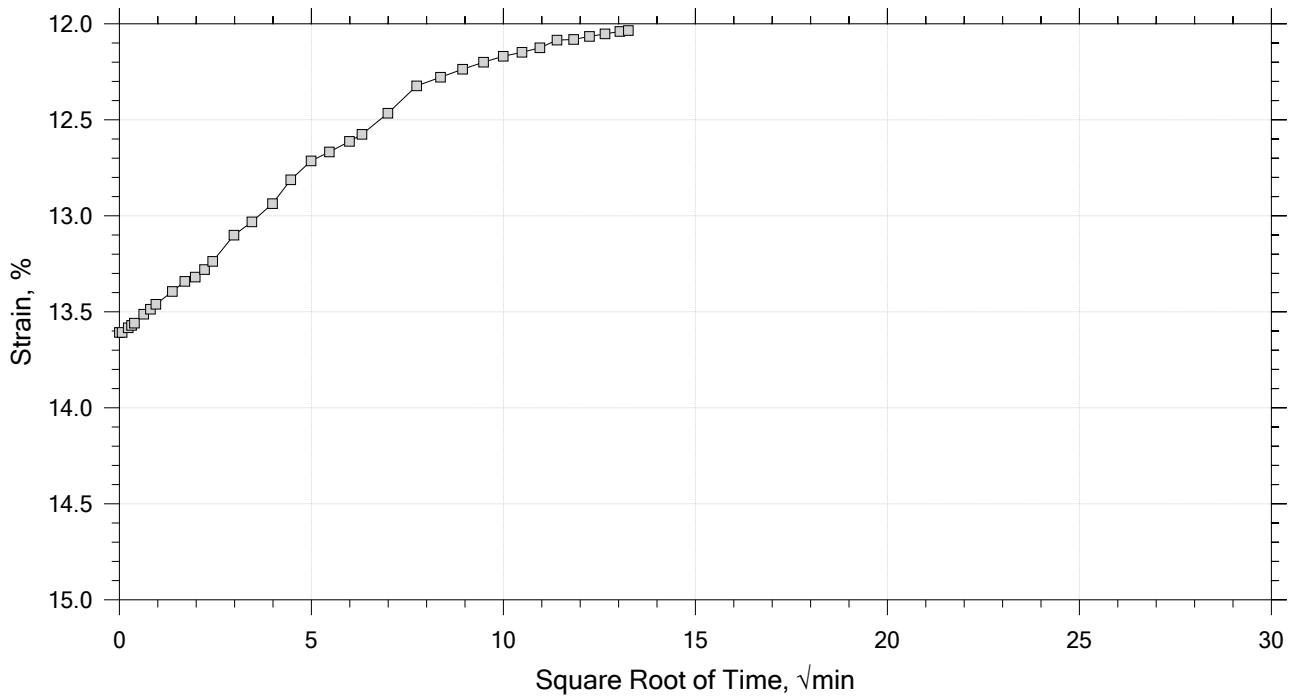
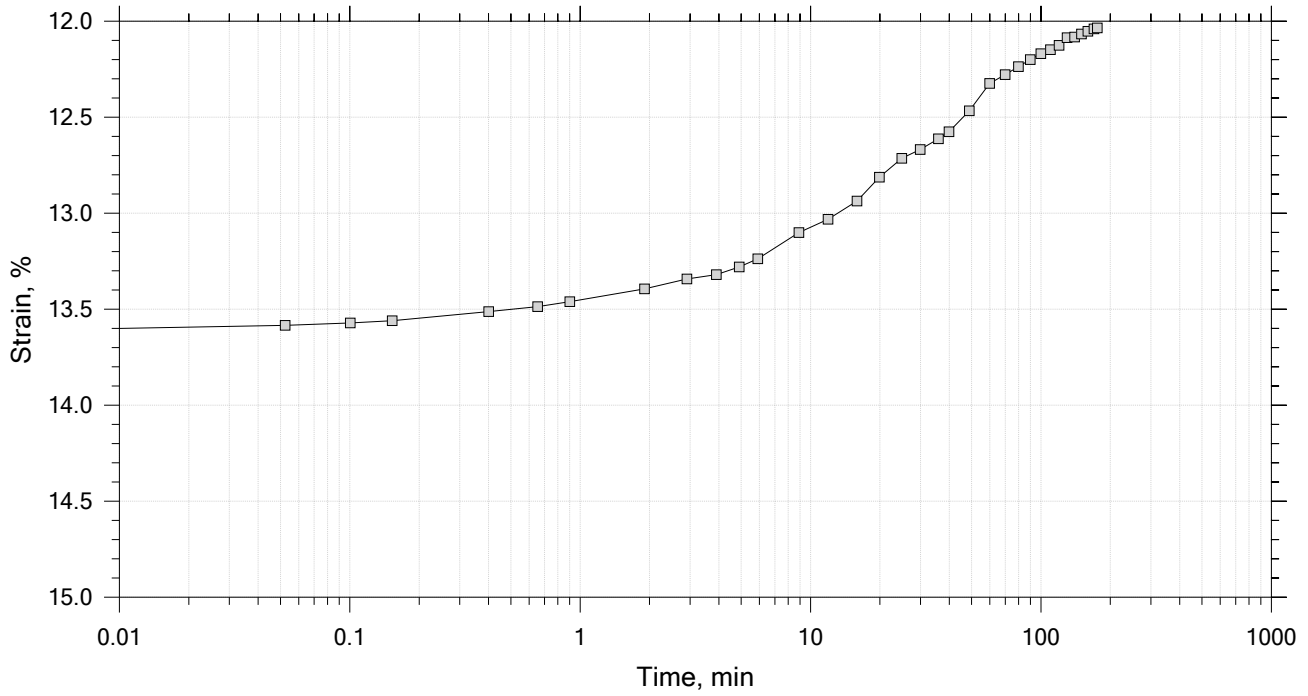
 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-6	Tested By: jm	Checked By: mcm
	Sample No.: 7	Test Date: 10/16/20	Depth: 12-14 ft
	Test No.: IP-11	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay(CH)		


# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 12 of 12

Constant Load Step

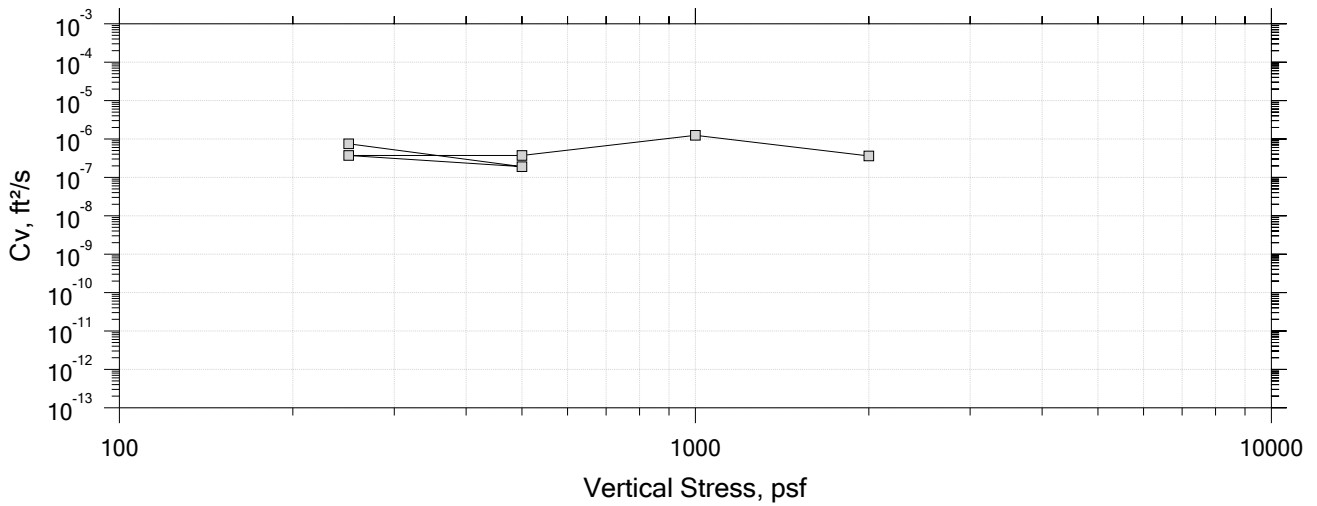
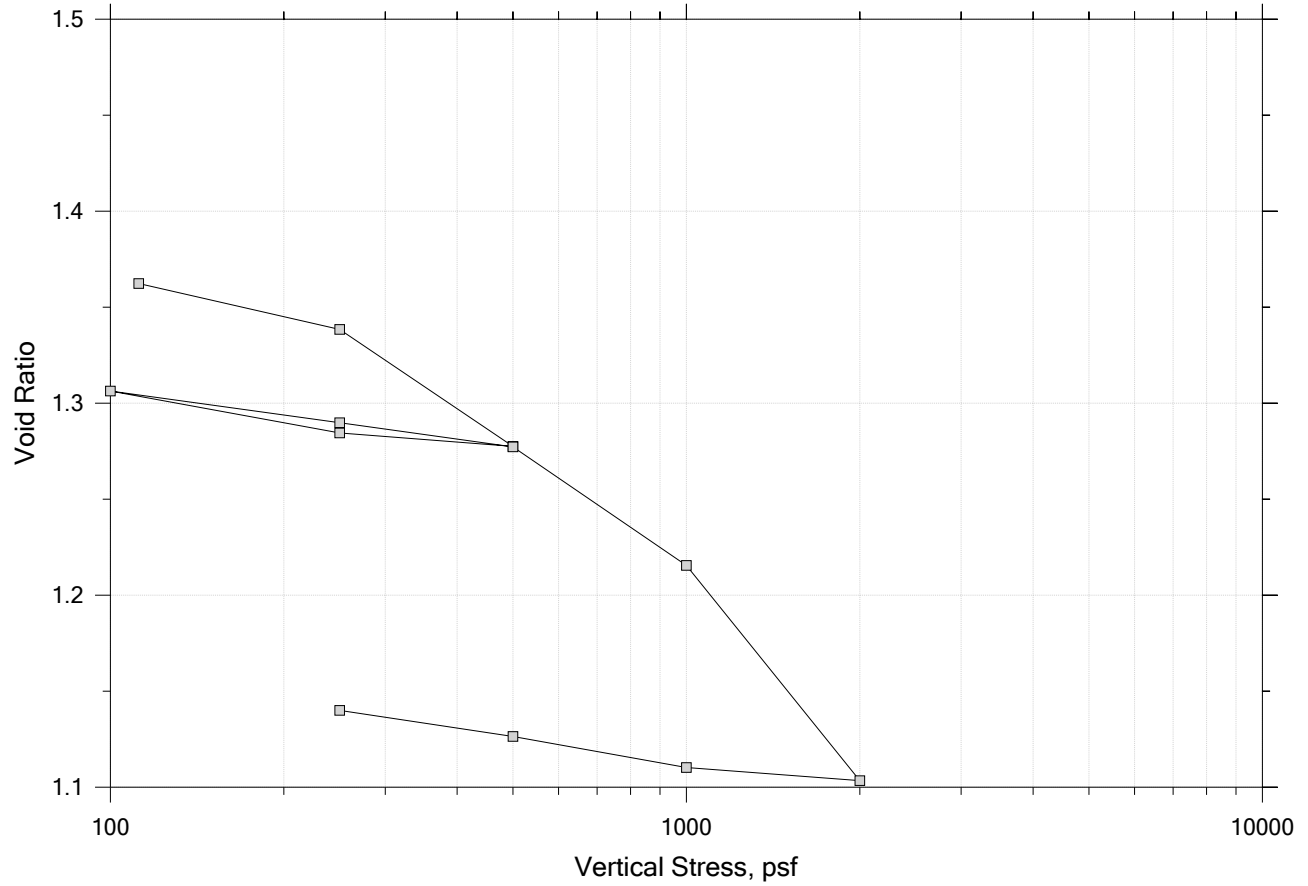
Stress: 250 psf




 Engineering and Testing	Project: Breton Landbridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-6	Tested By: jm	Checked By: mcm
	Sample No.: 7	Test Date: 10/16/20	Depth: 12-14 ft
	Test No.: IP-11	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay(CH)		

# One-Dimensional Consolidation by ASTM D2435 - Method B

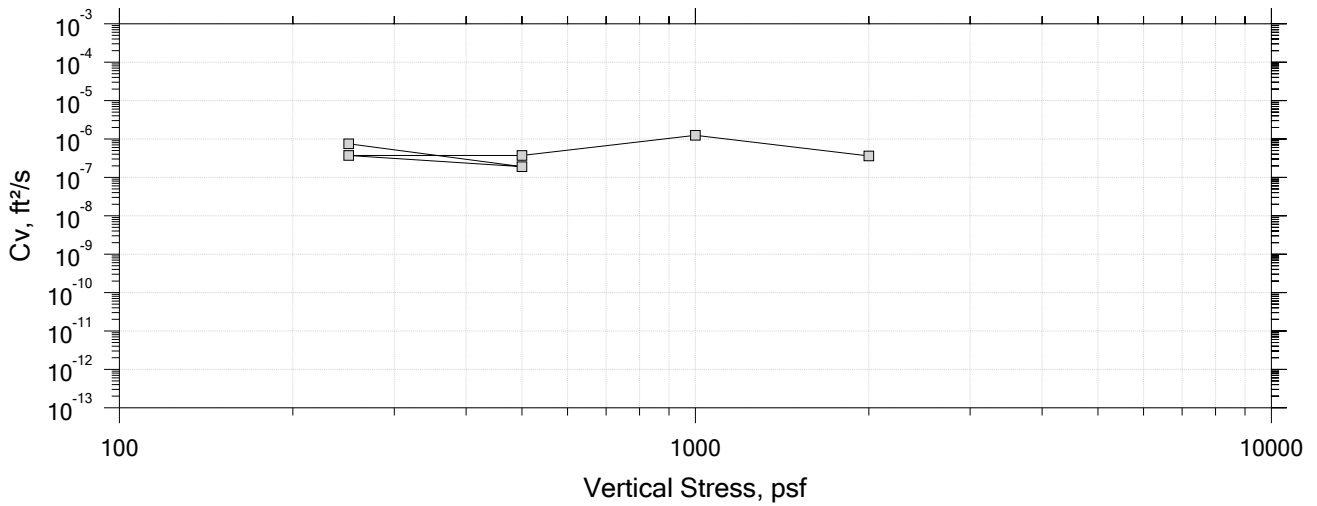
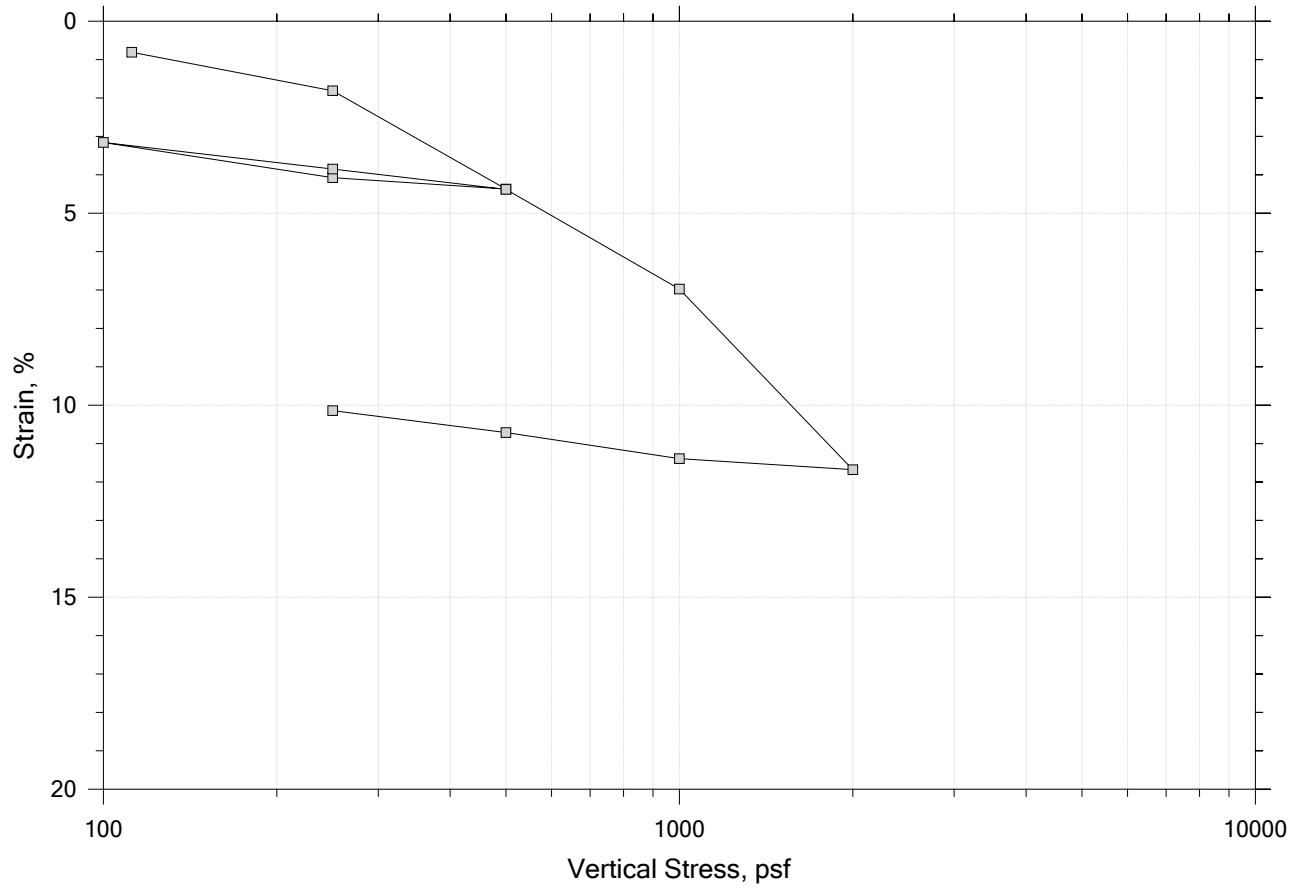
## Summary Report




 <b>APS</b> Engineering and Testing	Project: Breton Lakebridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-6	Tested By: jm	Checked By: mcm
	Sample No.: 12	Test Date: 10/16/20	Depth: 28-30 ft
	Test No.: IP-12	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay(CH)	Measured specific gravity: 2.63	

# One-Dimensional Consolidation by ASTM D2435 - Method B

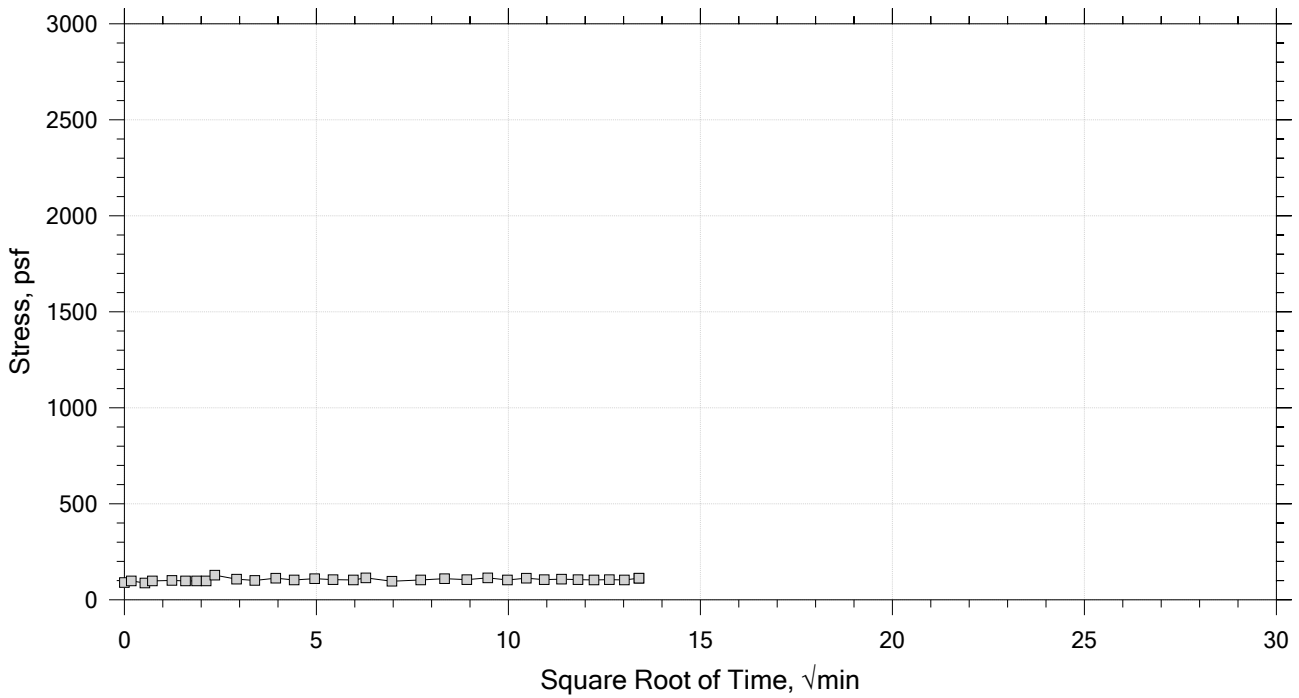
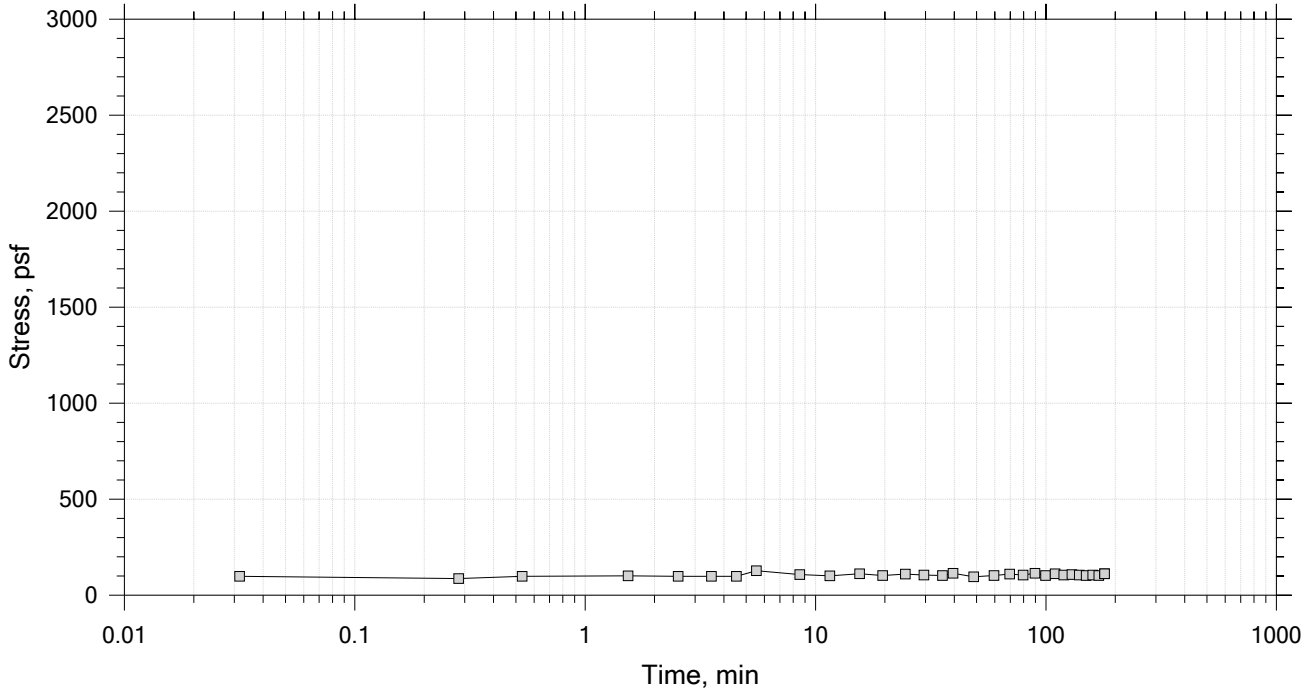
## Summary Report




 <p>APS Engineering and Testing</p>	Project: Breton Lakebridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-6	Tested By: jm	Checked By: mcm
	Sample No.: 12	Test Date: 10/16/20	Depth: 28-30 ft
	Test No.: IP-12	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay (CH)		

# One-Dimensional Consolidation by ASTM D2435 - Method B

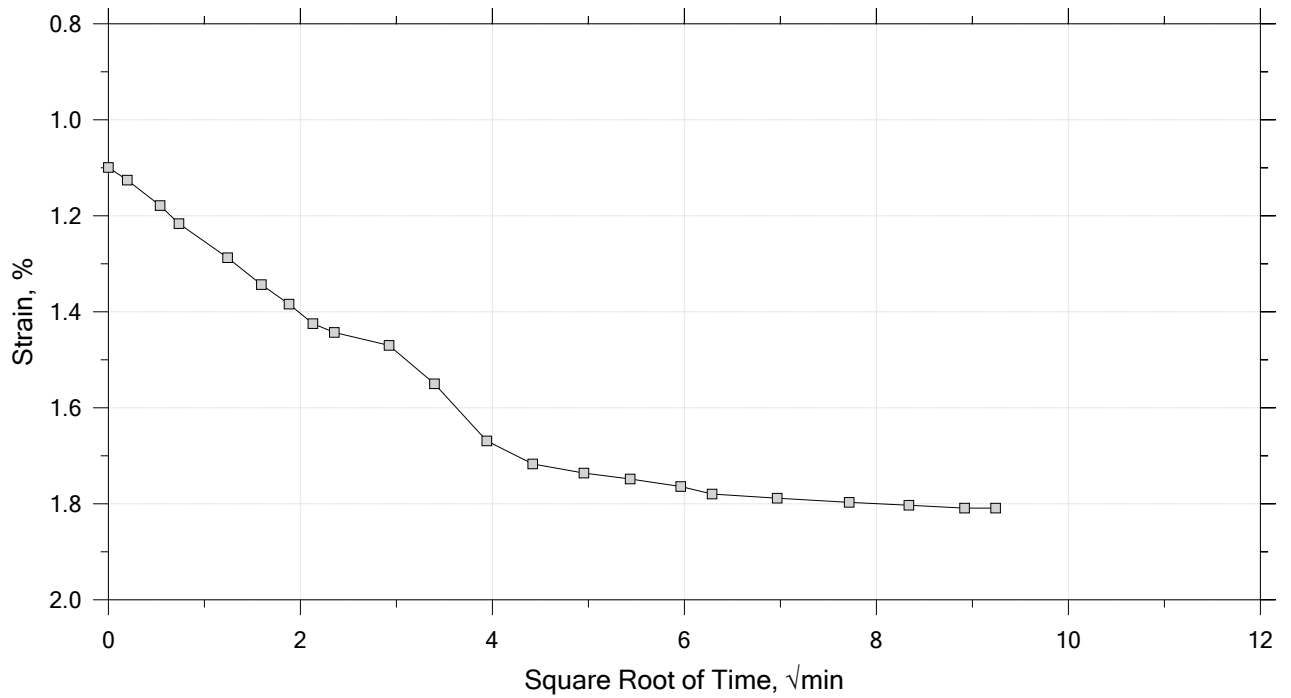
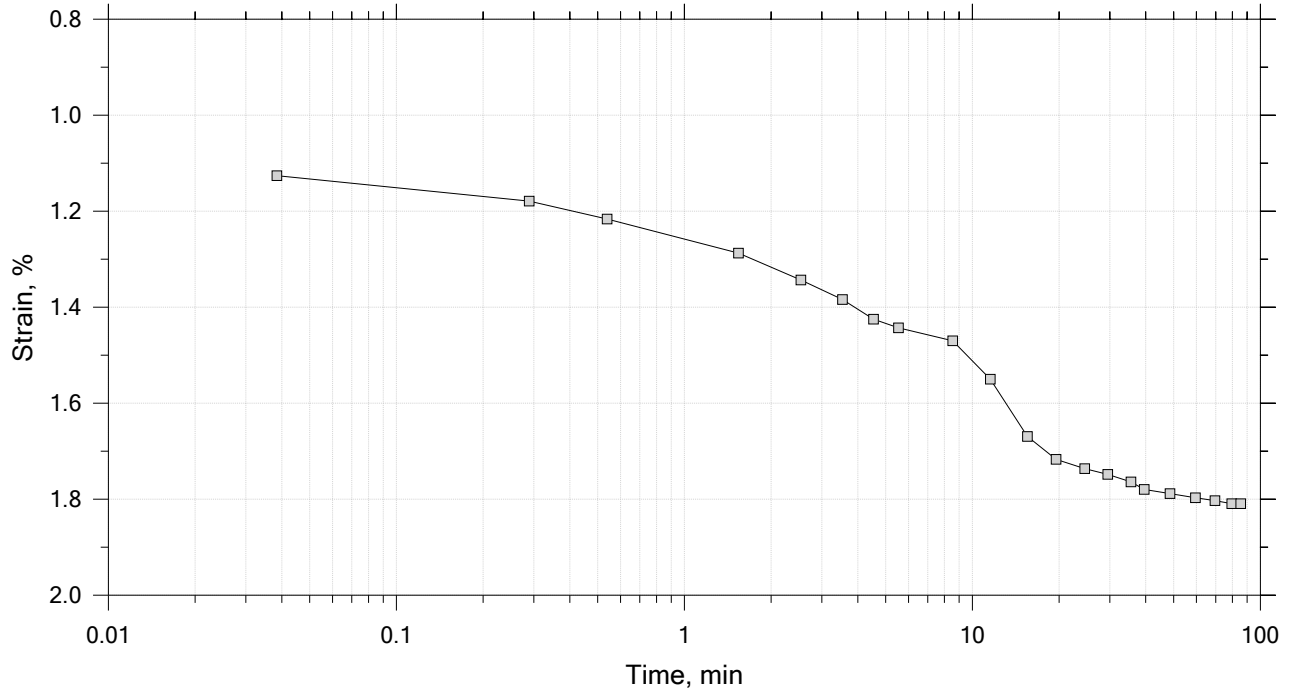
Time Curve 1 of 12  
 Constant Volume Step  
 Stress: 112 psf




 Engineering and Testing	Project: Breton Lakebridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-6	Tested By: jm	Checked By: mcm
	Sample No.: 12	Test Date: 10/16/20	Depth: 28-30 ft
	Test No.: IP-12	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay		

# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 2 of 12  
 Constant Load Step  
 Stress: 250 psf



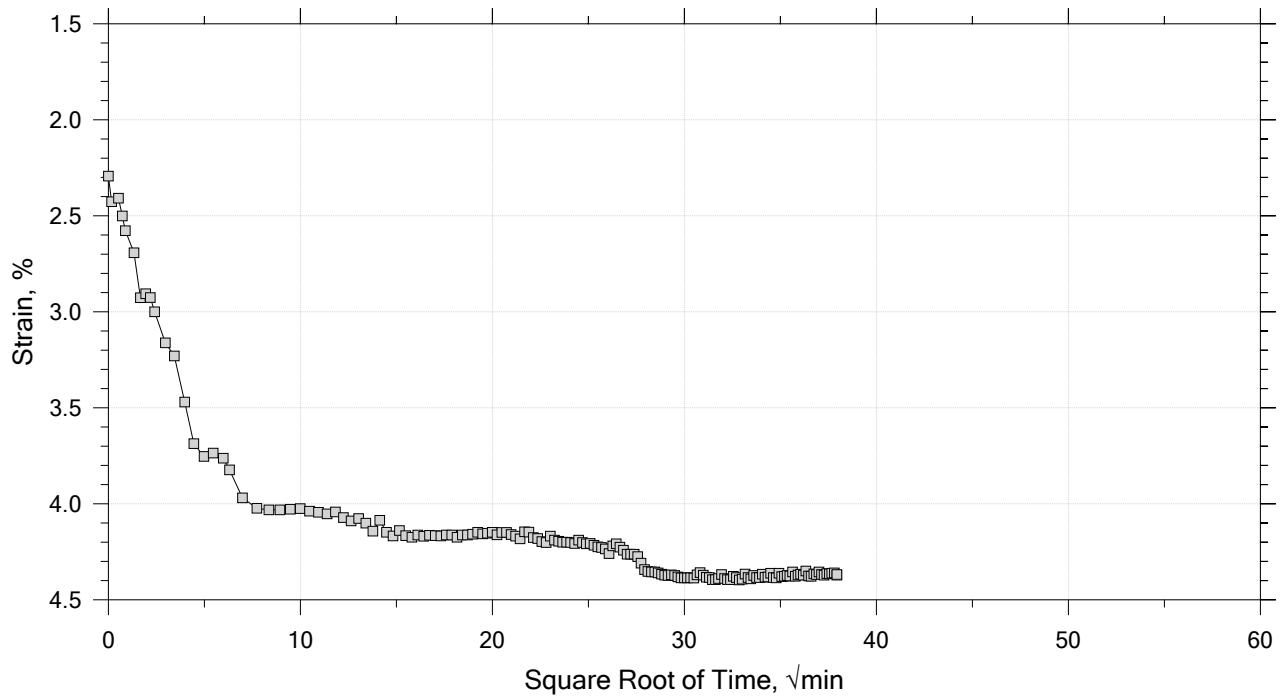
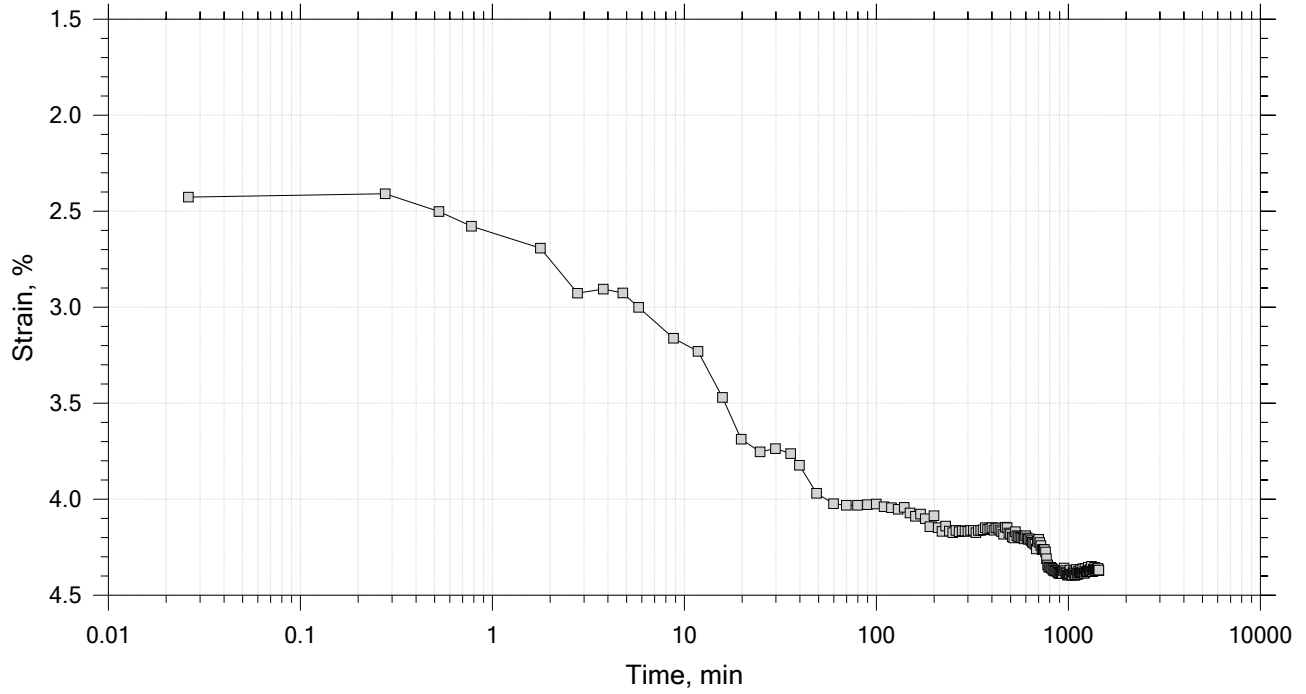
 Engineering and Testing	Project: Breton Lakebridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-6	Tested By: jm	Checked By: mcm
	Sample No.: 12	Test Date: 10/16/20	Depth: 28-30 ft
	Test No.: IP-12	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay(CH)		


# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 3 of 12

Constant Load Step

Stress: 500 psf



 Engineering and Testing	Project: Breton Lakebridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-6	Tested By: jm	Checked By: mcm
	Sample No.: 12	Test Date: 10/16/20	Depth: 28-30 ft
	Test No.: IP-12	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay(CH)		

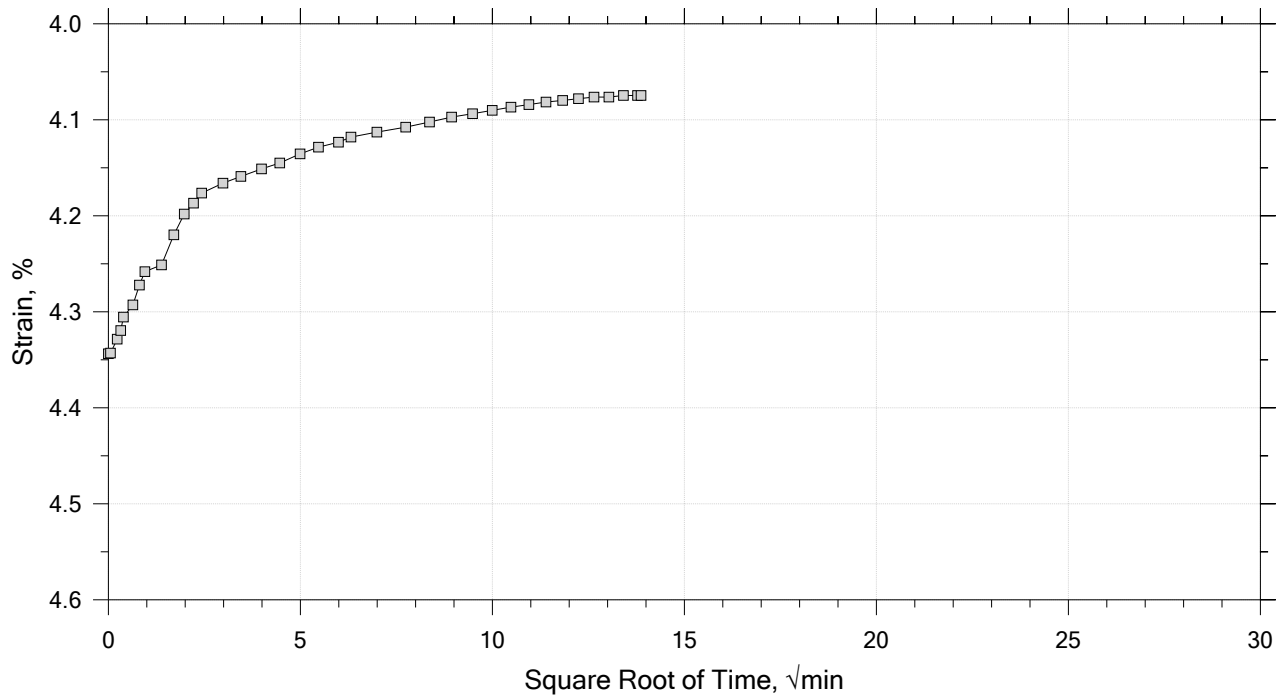
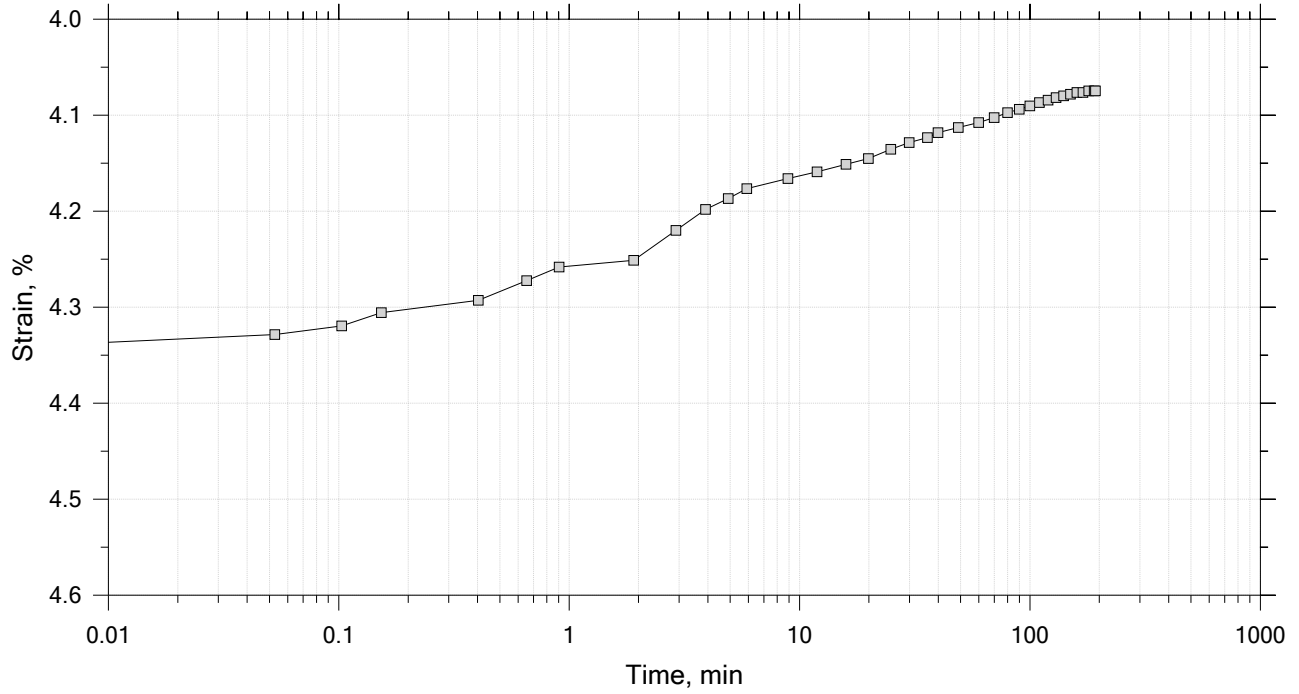



# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 4 of 12

Constant Load Step

Stress: 250 psf



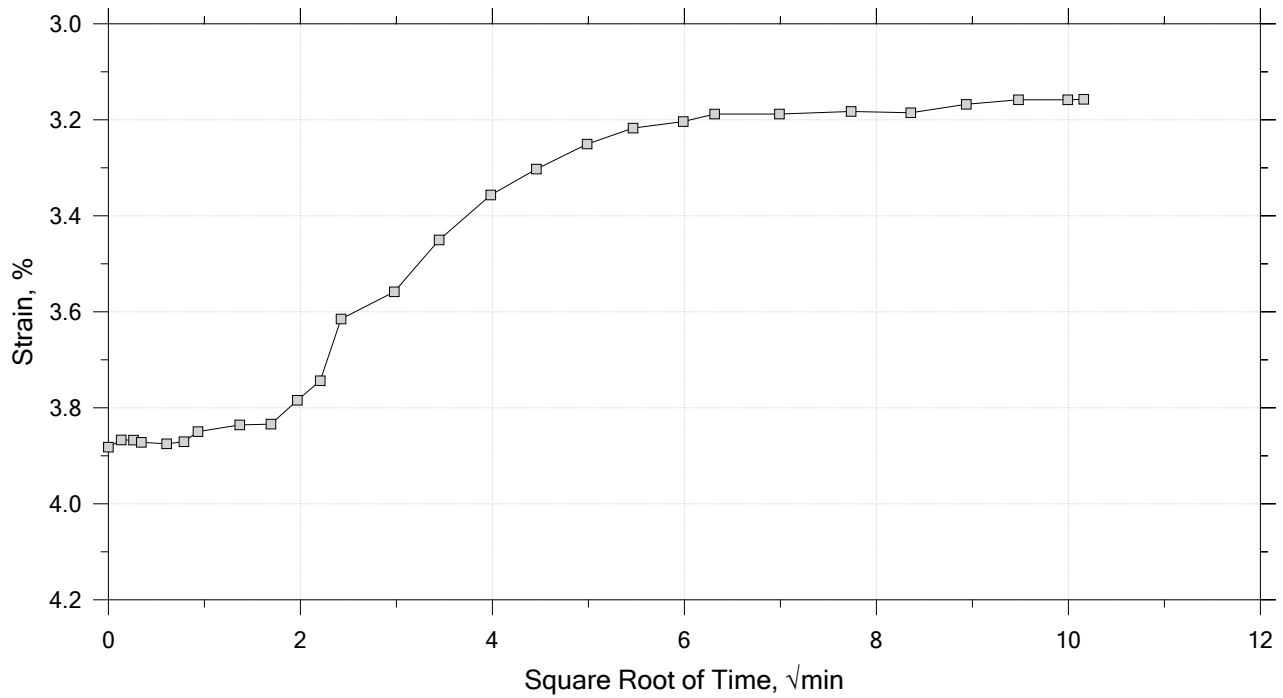
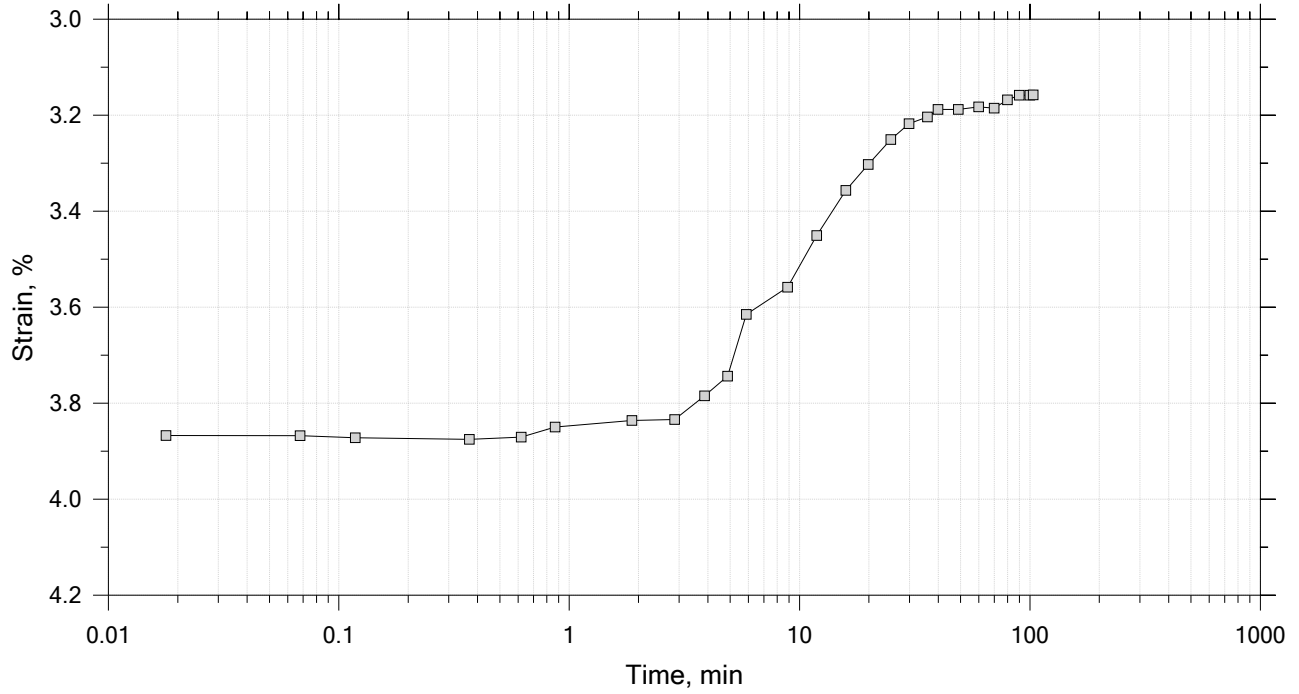
 Engineering and Testing	Project: Breton Lakebridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-6	Tested By: jm	Checked By: mcm
	Sample No.: 12	Test Date: 10/16/20	Depth: 28-30 ft
	Test No.: IP-12	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay		


# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 5 of 12

Constant Load Step

Stress: 100 psf



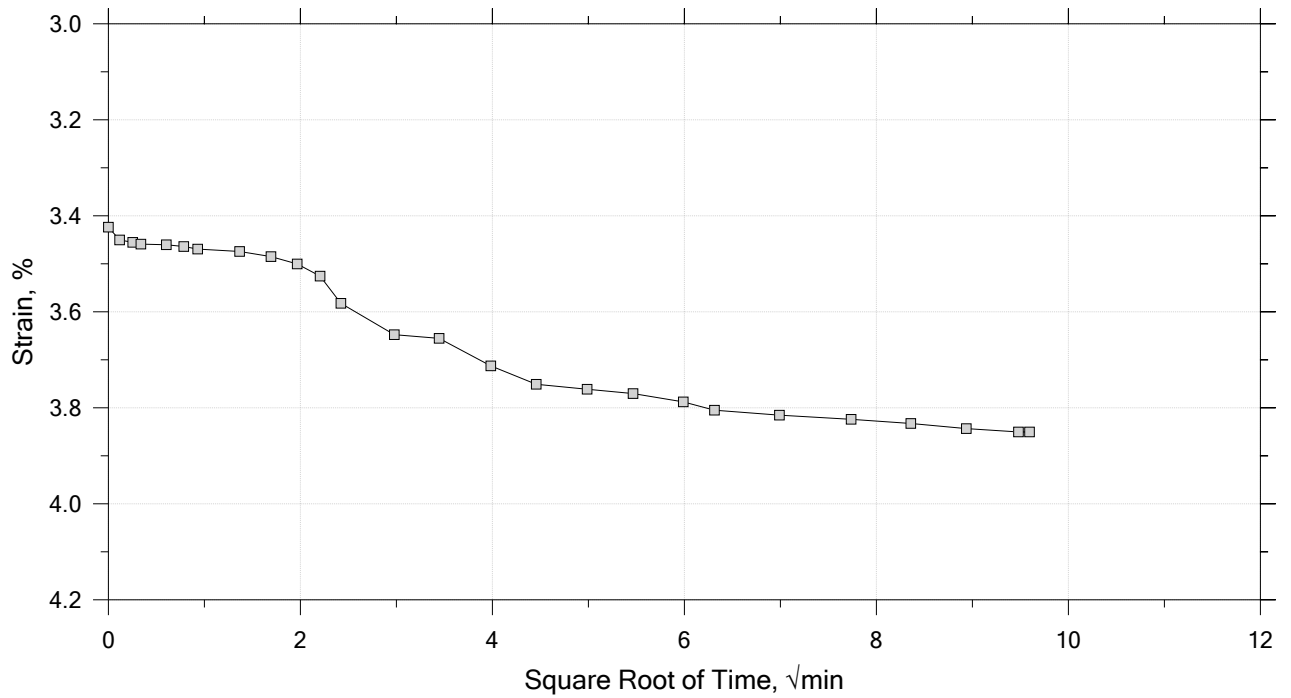
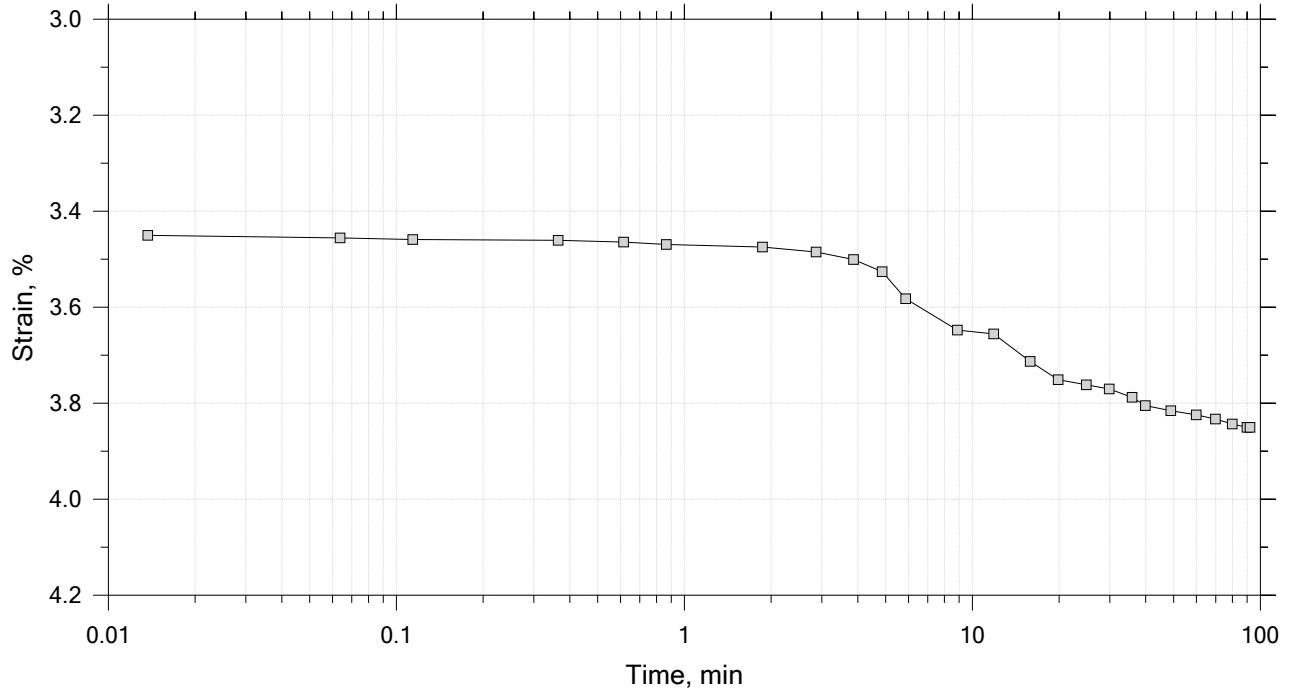
	Project: Breton Lakebridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-6	Tested By: jm	Checked By: mcm
	Sample No.: 12	Test Date: 10/16/20	Depth: 28-30 ft
	Test No.: IP-12	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay(CH)		


# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 6 of 12

Constant Load Step

Stress: 250 psf



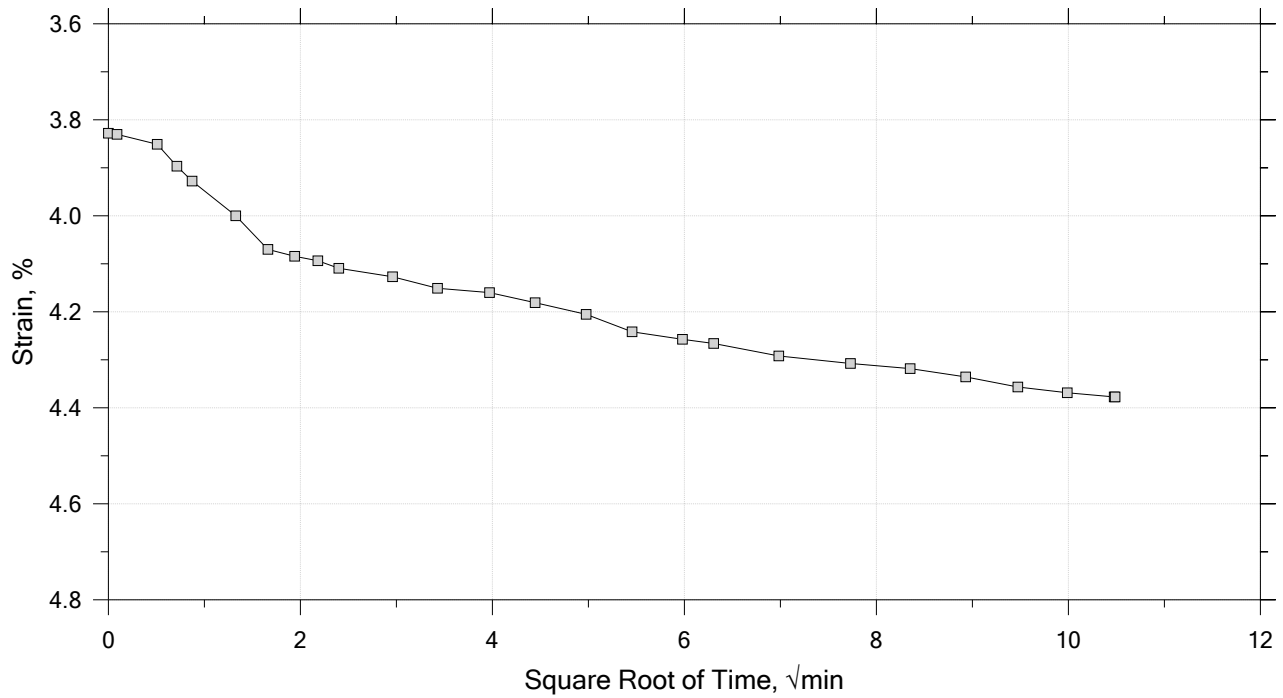
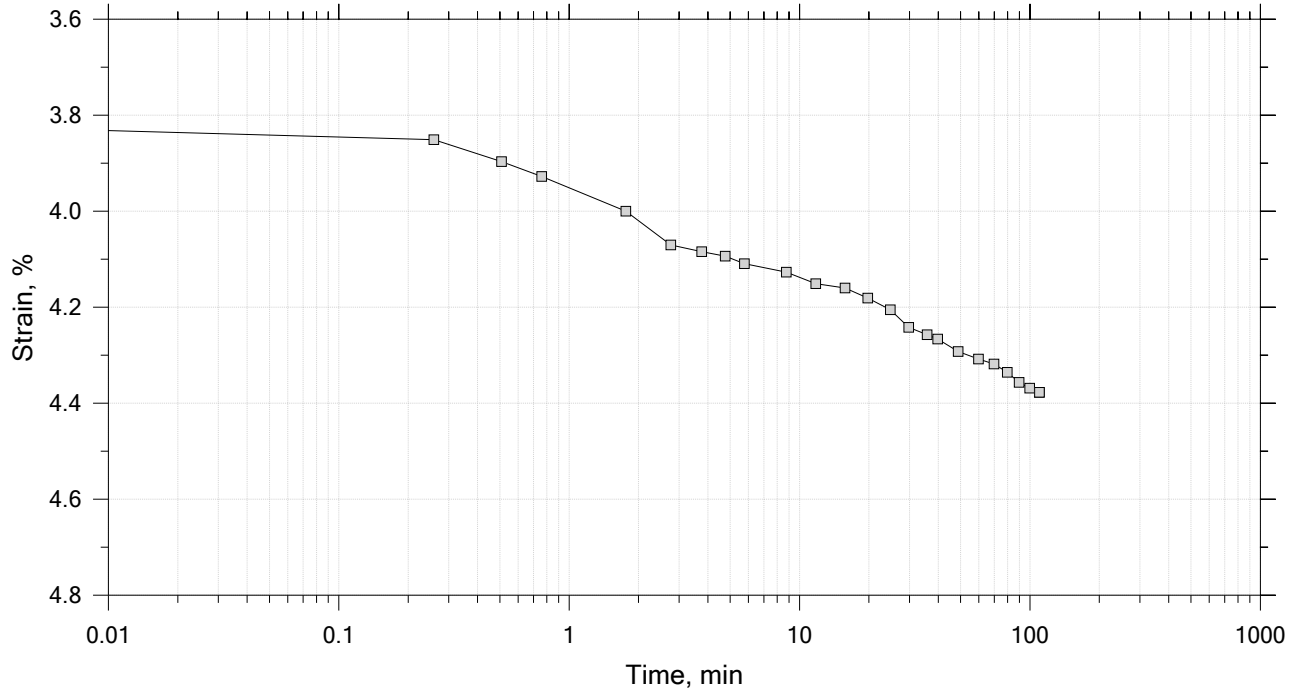
 <p>APS Engineering and Testing</p>	Project: Breton Lakebridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-6	Tested By: jm	Checked By: mcm
	Sample No.: 12	Test Date: 10/16/20	Depth: 28-30 ft
	Test No.: IP-12	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay(CH)		


# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 7 of 12

Constant Load Step

Stress: 500 psf



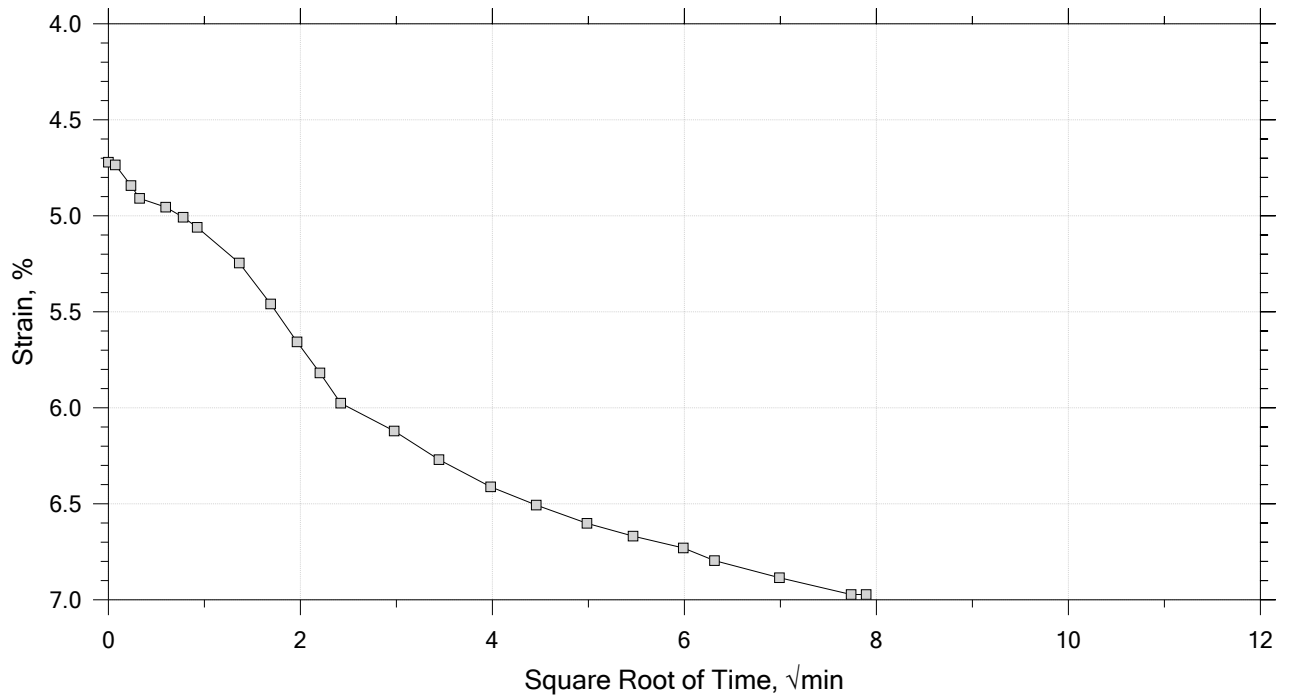
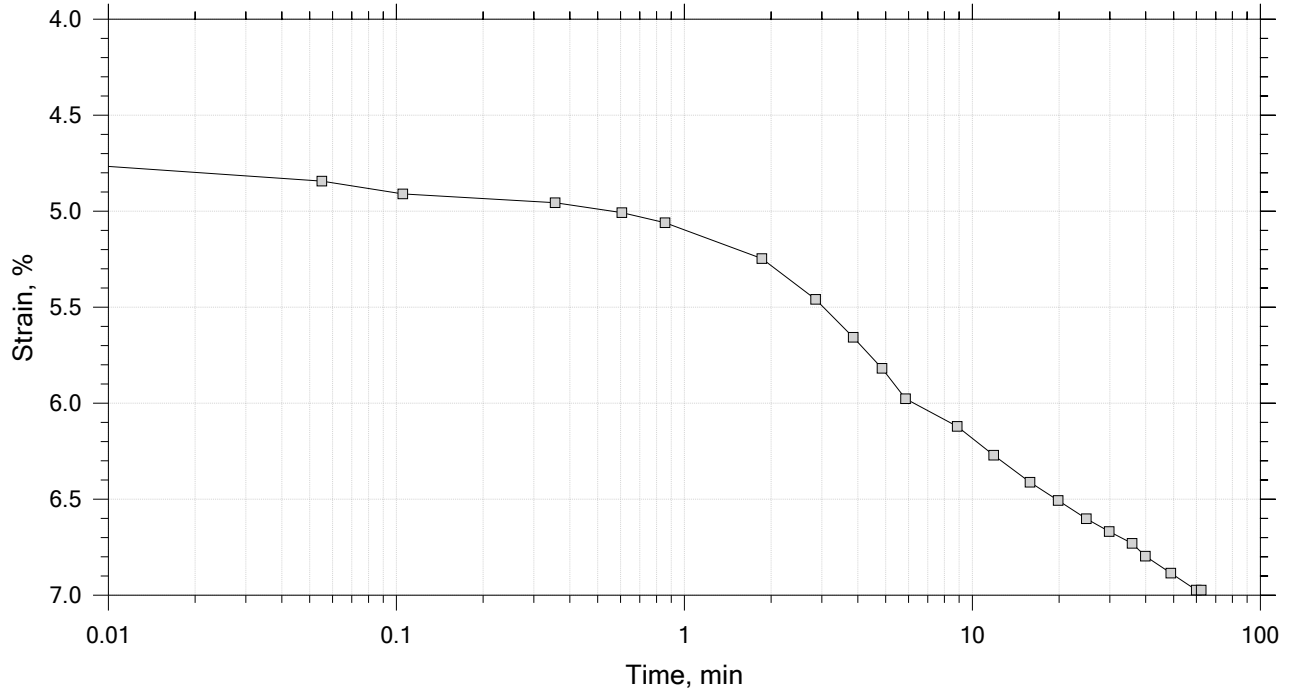
 Engineering and Testing	Project: Breton Lakebridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-6	Tested By: jm	Checked By: mcm
	Sample No.: 12	Test Date: 10/16/20	Depth: 28-30 ft
	Test No.: IP-12	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay(CH)		


# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 8 of 12

Constant Load Step

Stress: 1e+03 psf



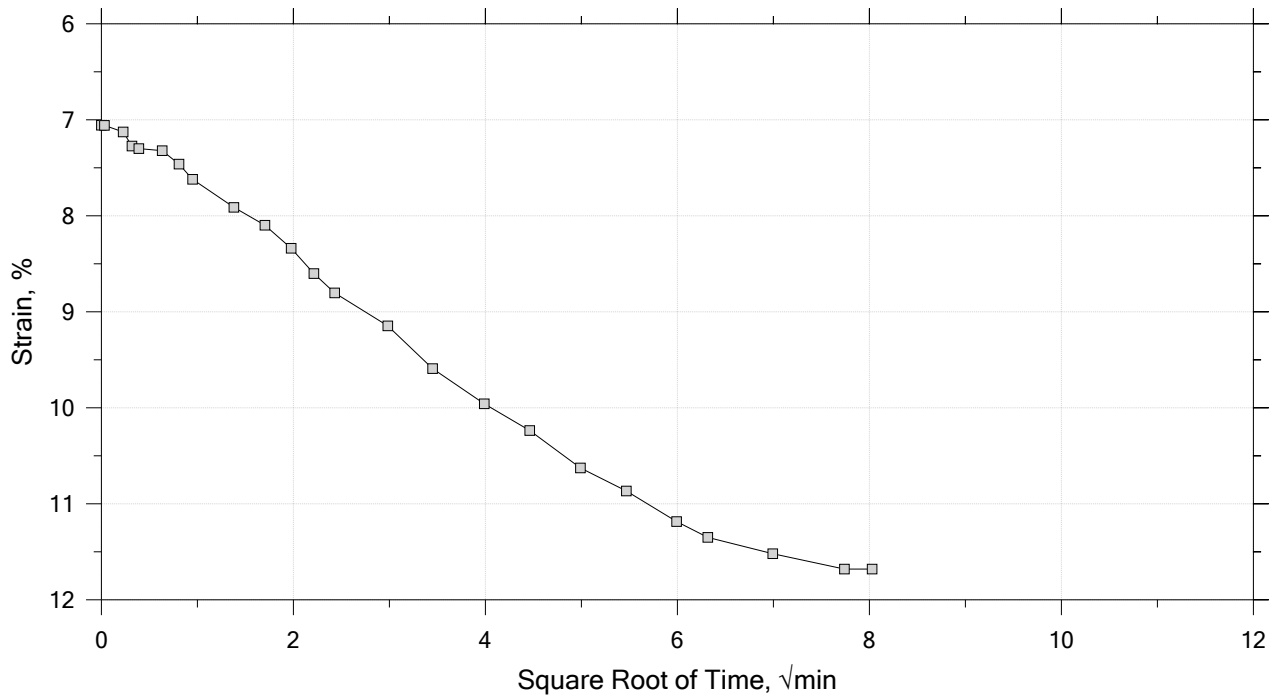
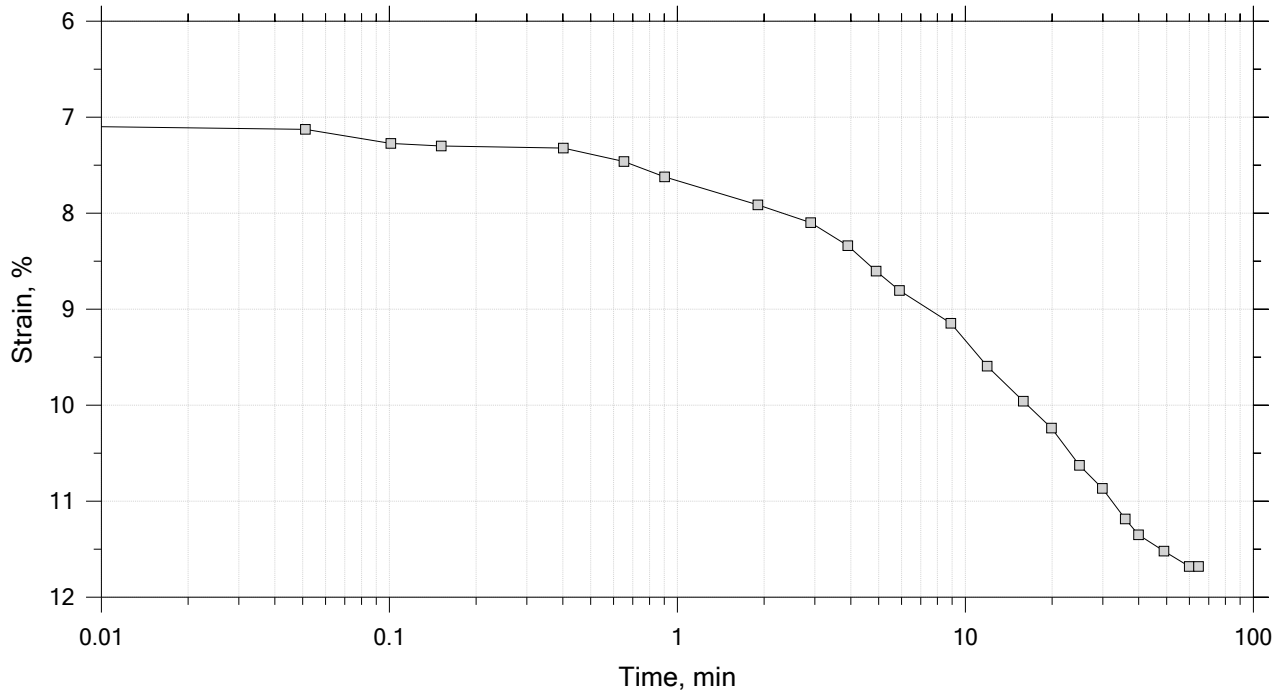
 <p>Engineering and Testing</p>	Project: Breton Lakebridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-6	Tested By: jm	Checked By: mcm
	Sample No.: 12	Test Date: 10/16/20	Depth: 28-30 ft
	Test No.: IP-12	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay(CH)		


# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 9 of 12

Constant Load Step

Stress: 2e+03 psf



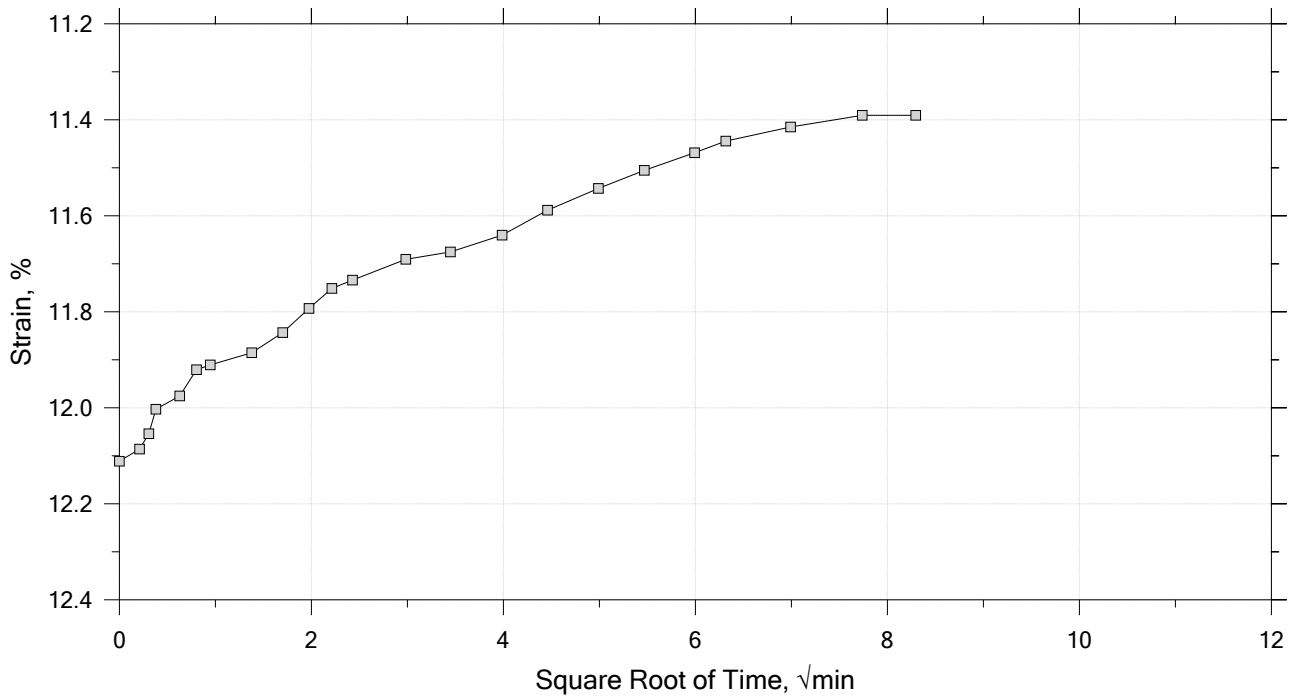
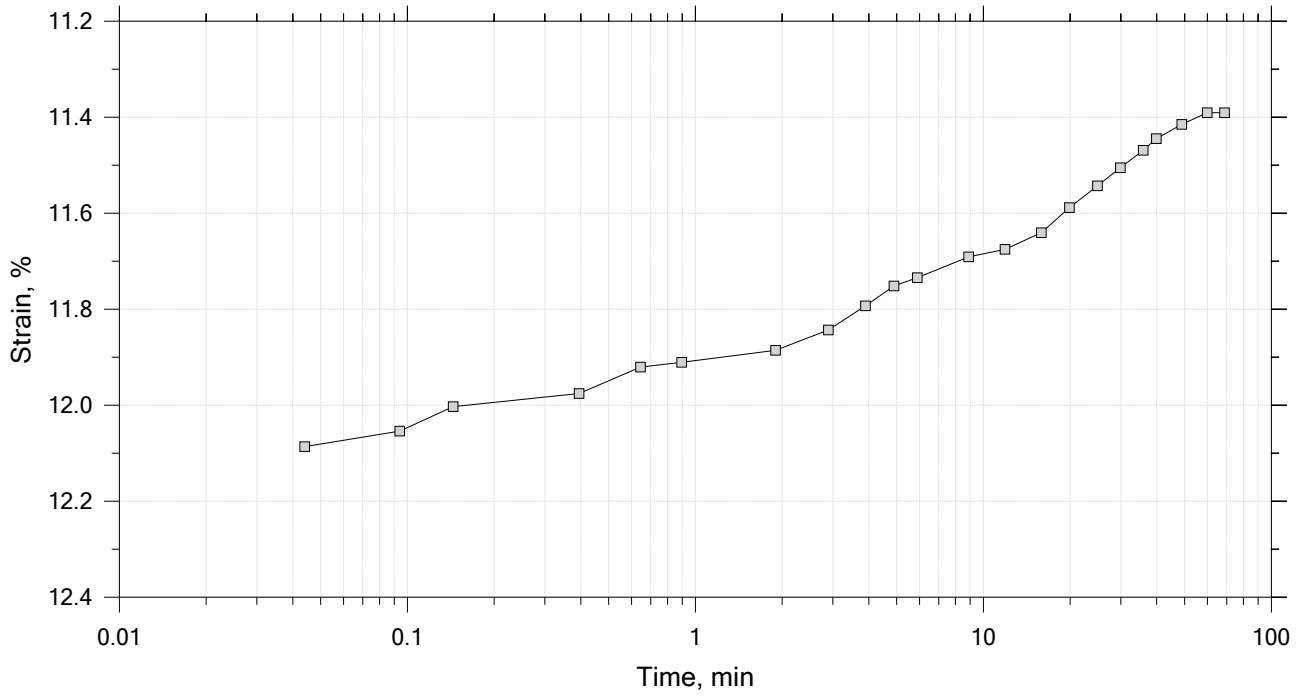
 Engineering and Testing	Project: Breton Lakebridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-6	Tested By: jm	Checked By: mcm
	Sample No.: 12	Test Date: 10/16/20	Depth: 28-30 ft
	Test No.: IP-12	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay(CH)		


# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 10 of 12

Constant Load Step

Stress: 1e+03 psf



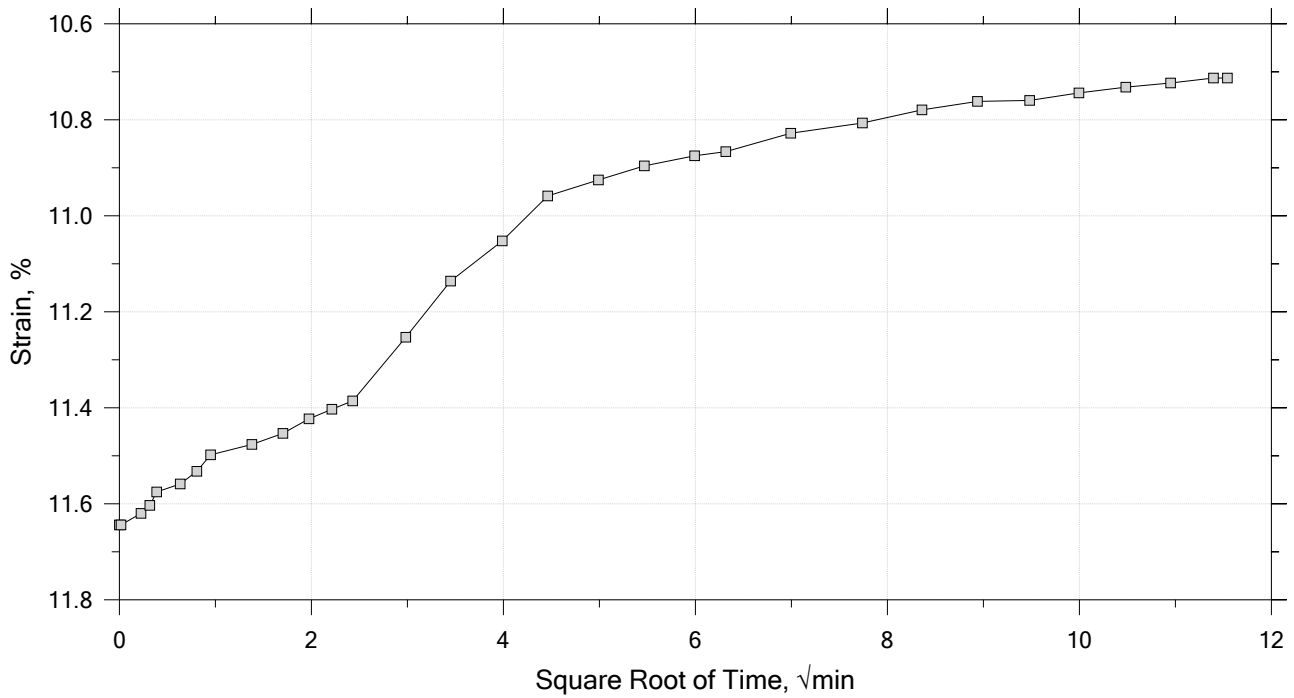
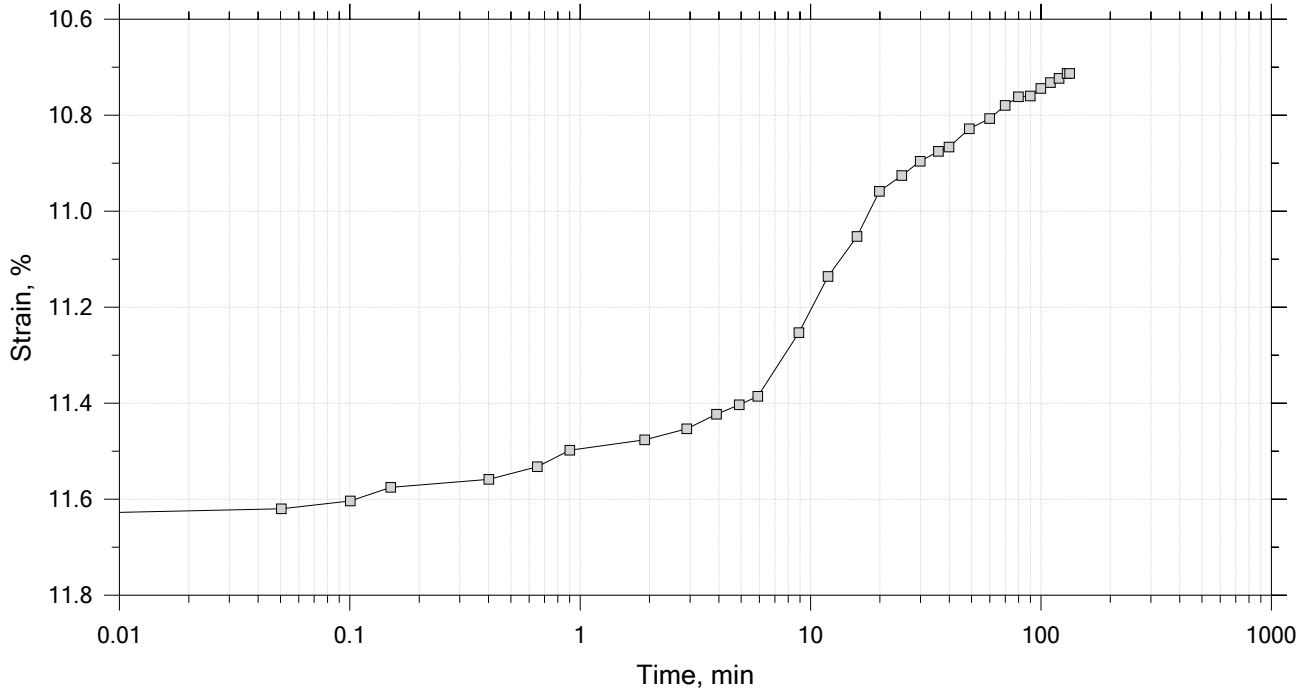
 Engineering and Testing	Project: Breton Lakebridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-6	Tested By: jm	Checked By: mcm
	Sample No.: 12	Test Date: 10/16/20	Depth: 28-30 ft
	Test No.: IP-12	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay(CH)		


# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 11 of 12

Constant Load Step

Stress: 500 psf



 Engineering and Testing	Project: Breton Lakebridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-6	Tested By: jm	Checked By: mcm
	Sample No.: 12	Test Date: 10/16/20	Depth: 28-30 ft
	Test No.: IP-12	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay(CH)		

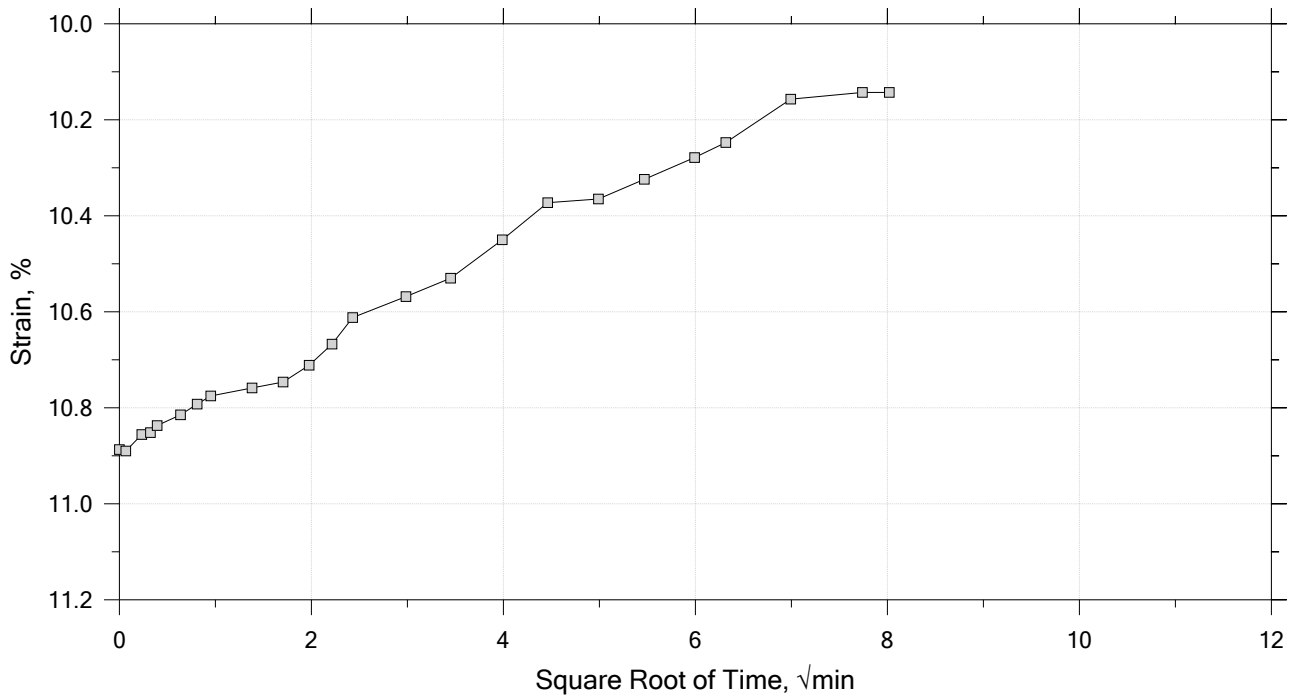
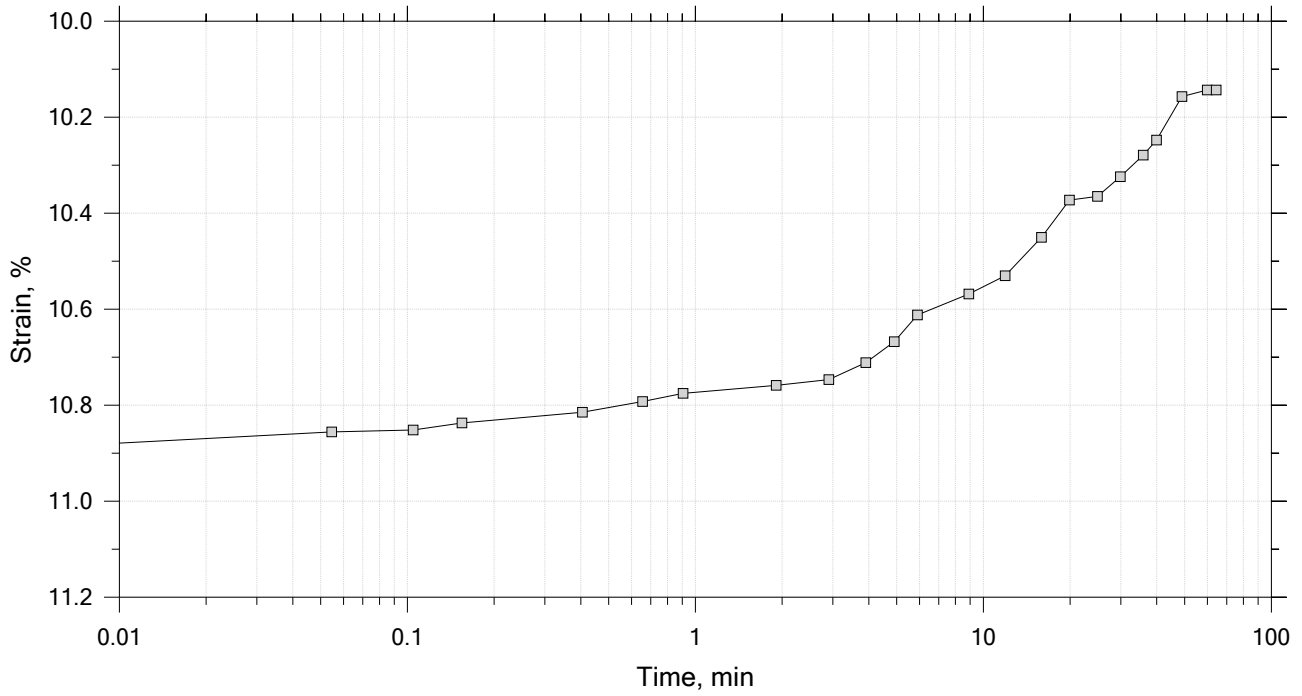



# One-Dimensional Consolidation by ASTM D2435 - Method B

Time Curve 12 of 12

Constant Load Step

Stress: 250 psf



 Engineering and Testing	Project: Breton Lakebridge Project	Location: see map	Project No.: APS2008-G063
	Boring No.: B-6	Tested By: jm	Checked By: mcm
	Sample No.: 12	Test Date: 10/16/20	Depth: 28-30 ft
	Test No.: IP-12	Sample Type: intact	Elevation: ---
	Description: Moist, dark gray clay(CH)		

**APPENDIX G**  
**(CPT Probe Logs)**



Engineering and Testing

# Breton Landbridge Marsh Creation (West) Plaquemines Parish (Louisiana)

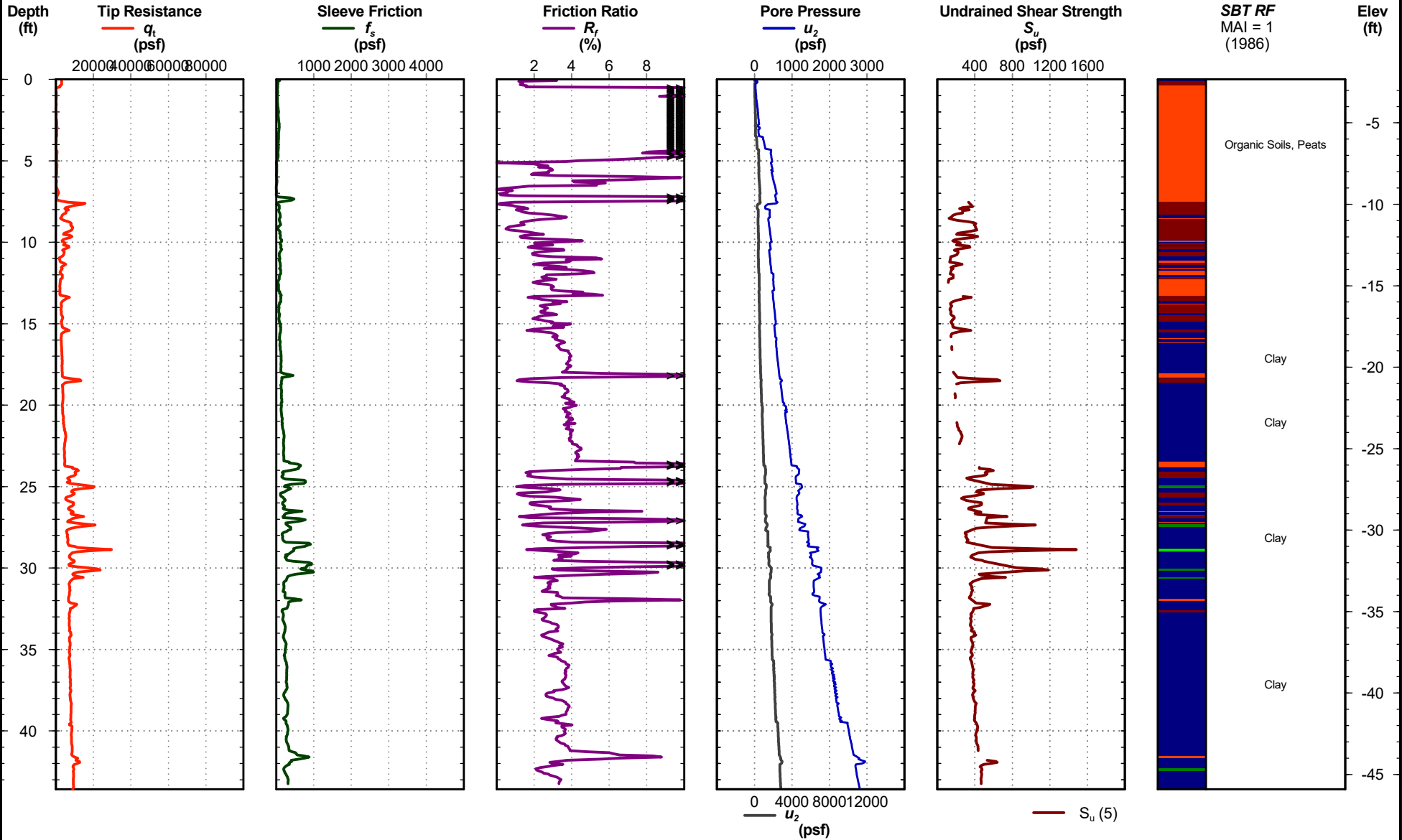
# Cone Penetration Test

# C1

Project #: Brenton CPT  
Date: Aug. 18, 2020

Northing: 445637.4  
Easting: 3762240.1

Elevation: -2.328  
Filename: C1.cpt



- 1 - Sensitive, Fine Grained Soils
- 2 - Organic Soils, Peats
- 3 - Clays-Clay to Silty Clay
- 4 - Silt Mixtures-Clay Silt to Silty Clay
- 5 - Sand Mixtures-Silty Sand to Sandy Silt
- 6 - Sands-Clean Sand to Silty Sand
- 7 - Gravelly Sand to Sand
- 8 - Very Stiff Clay to Clayey Sand
- 9 - Very Stiff Fine Grained Soils

CPT REPORT - DYNAMIC BOTTOM LEGEND CPT-BRETON PSF.GPJ\_DF STD US LAB.GDT\_12/23/20

# C1



Engineering and Testing

# Breton Landbridge Marsh Creation (West) Plaquemines Parish (Louisiana)

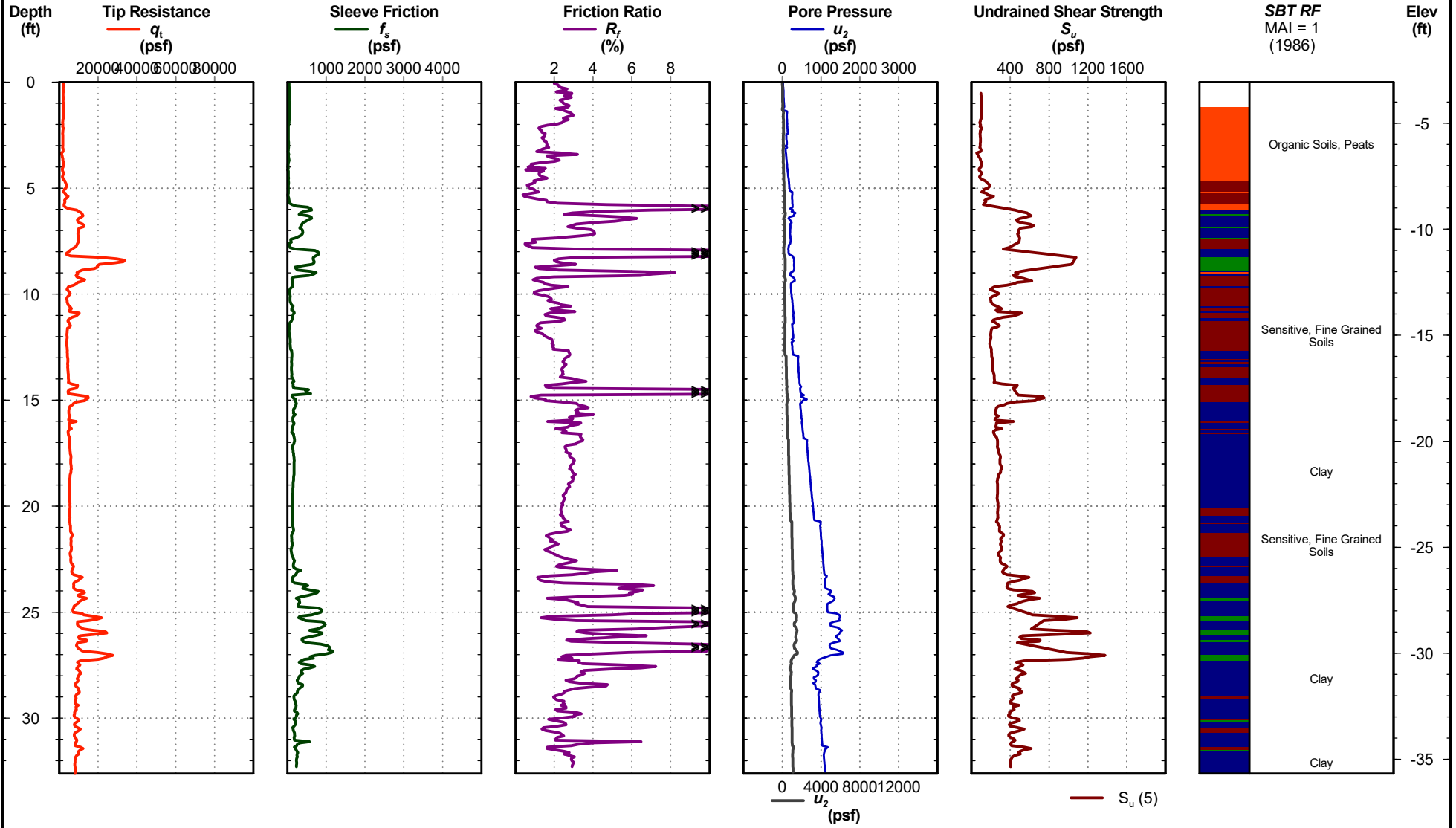
# Cone Penetration Test

# C2

Project #: Brenton CPT  
Date: Aug. 18, 2020

Northing: 443372.5  
Easting: 3761160.9

Elevation: -3.063  
Filename: C2.1.cpt



- |  |  |   |
|--|--|---|
| <span style="color: red;">■</span> 1 - Sensitive, Fine Grained Soils | <span style="color: green;">■</span> 4 - Silt Mixtures-Clay Silt to Silty Clay       | <span style="color: yellow;">■</span> 7 - Gravelly Sand to Sand             |
| <span style="color: orange;">■</span> 2 - Organic Soils, Peats       | <span style="color: lightgreen;">■</span> 5 - Sand Mixtures-Silty Sand to Sandy Silt | <span style="color: lightgrey;">■</span> 8 - Very Stiff Clay to Clayey Sand |
| <span style="color: blue;">■</span> 3 - Clays-Clay to Silty Clay     | <span style="color: yellow;">■</span> 6 - Sands-Clean Sand to Silty Sand             | <span style="color: grey;">■</span> 9 - Very Stiff Fine Grained Soils       |

CPT REPORT - DYNAMIC BOTTOM LEGEND CPT BRETON PSF.GPJ DF STD US LAB.GDT 12/23/20

# C2



Engineering and Testing

# Breton Landbridge Marsh Creation (West) Plaquemines Parish (Louisiana)

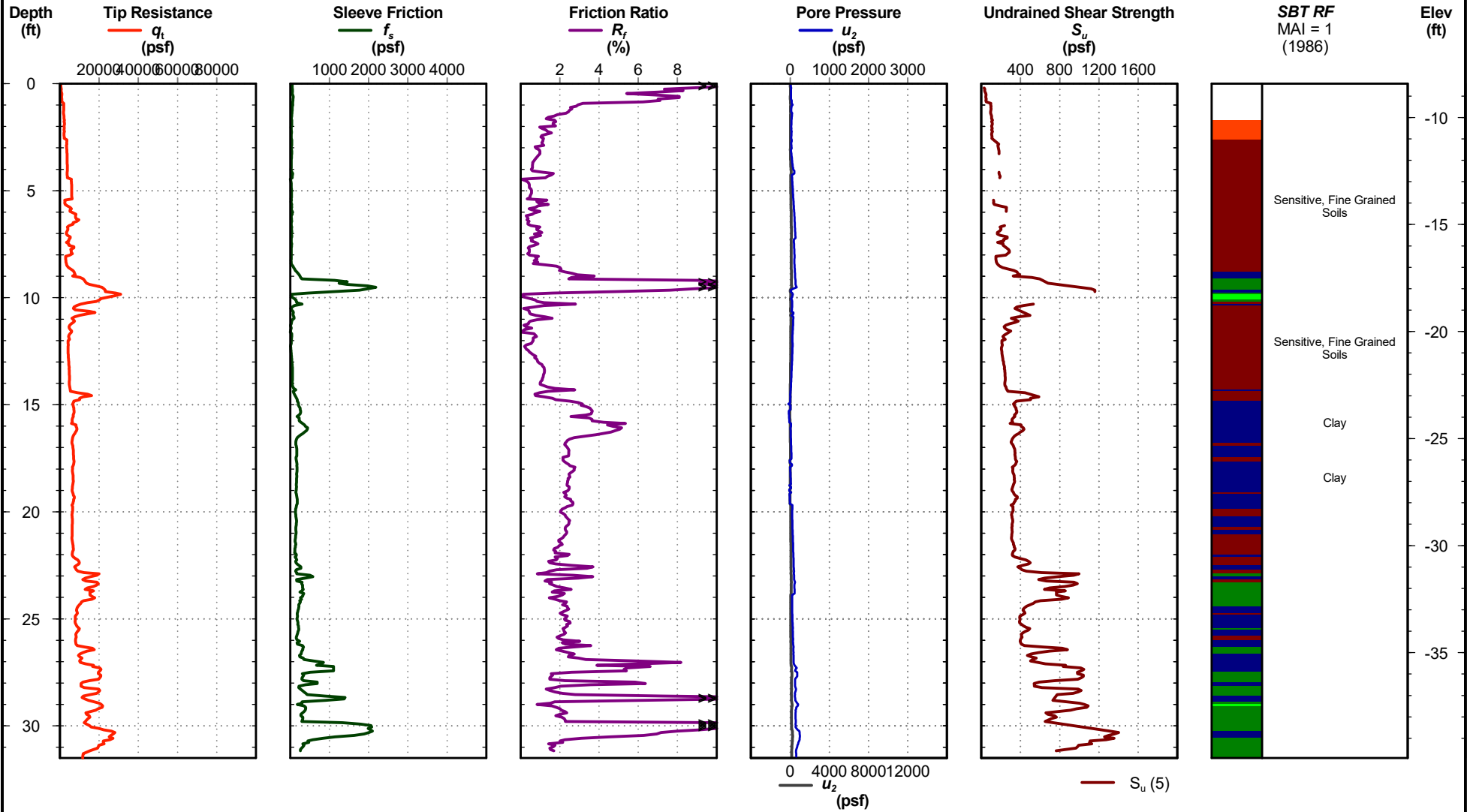
# Cone Penetration Test

# C3

Project #: Brenton CPT  
Date: Aug. 19, 2020

Northing: 443684.7  
Easting: 3759046.5

Elevation: -8.421  
Filename: c3.1.cpt



- 1 - Sensitive, Fine Grained Soils
- 4 - Silt Mixtures-Clay Silt to Silty Clay
- 7 - Gravelly Sand to Sand
- 2 - Organic Soils, Peats
- 5 - Sand Mixtures-Silty Sand to Sandy Silt
- 8 - Very Stiff Clay to Clayey Sand
- 3 - Clays-Clay to Silty Clay
- 6 - Sands-Clean Sand to Silty Sand
- 9 - Very Stiff Fine Grained Soils

CPT REPORT - DYNAMIC BOTTOM LEGEND CPT BRETON PSF.GPJ DF STD US LAB.GDT 12/23/20

# C3



Engineering and Testing

# Breton Landbridge Marsh Creation (West) Plaquemines Parish (Louisiana)

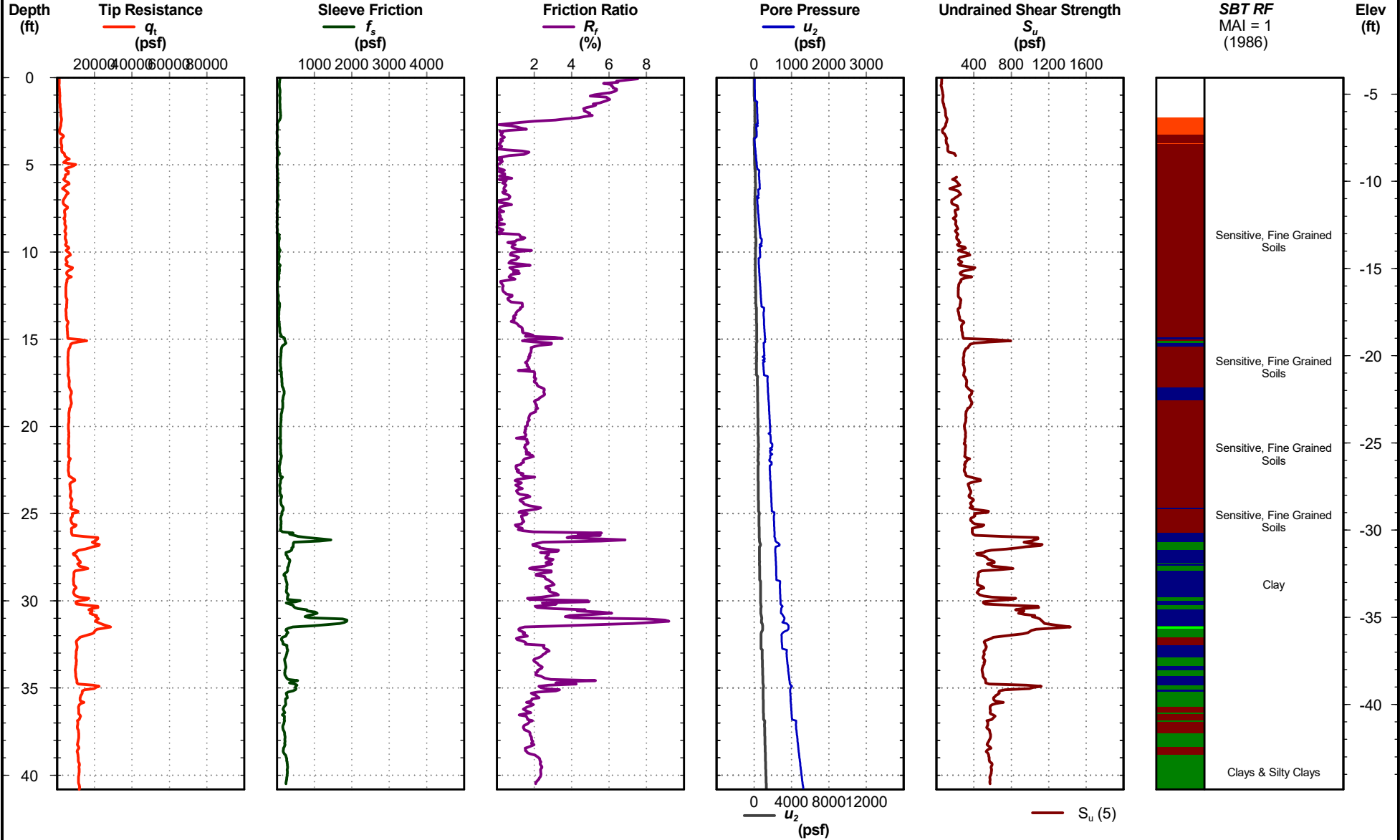
# Cone Penetration Test

# C4

Project #: Brenton CPT  
Date: Aug. 18, 2020

Northing: 444503.2  
Easting: 3758202.1

Elevation: -4.056  
Filename: C4.cpt



- 1 - Sensitive, Fine Grained Soils
- 4 - Silt Mixtures-Clay Silt to Silty Clay
- 7 - Gravelly Sand to Sand
- 2 - Organic Soils, Peats
- 5 - Sand Mixtures-Silty Sand to Sandy Silt
- 8 - Very Stiff Clay to Clayey Sand
- 3 - Clays-Clay to Silty Clay
- 6 - Sands-Clean Sand to Silty Sand
- 9 - Very Stiff Fine Grained Soils

CPT REPORT - DYNAMIC BOTTOM LEGEND CPT BRETON PSF.GPJ DF STD US LAB.GDT 12/23/20

# C4



Engineering and Testing

# Breton Landbridge Marsh Creation (West) Plaquemines Parish (Louisiana)

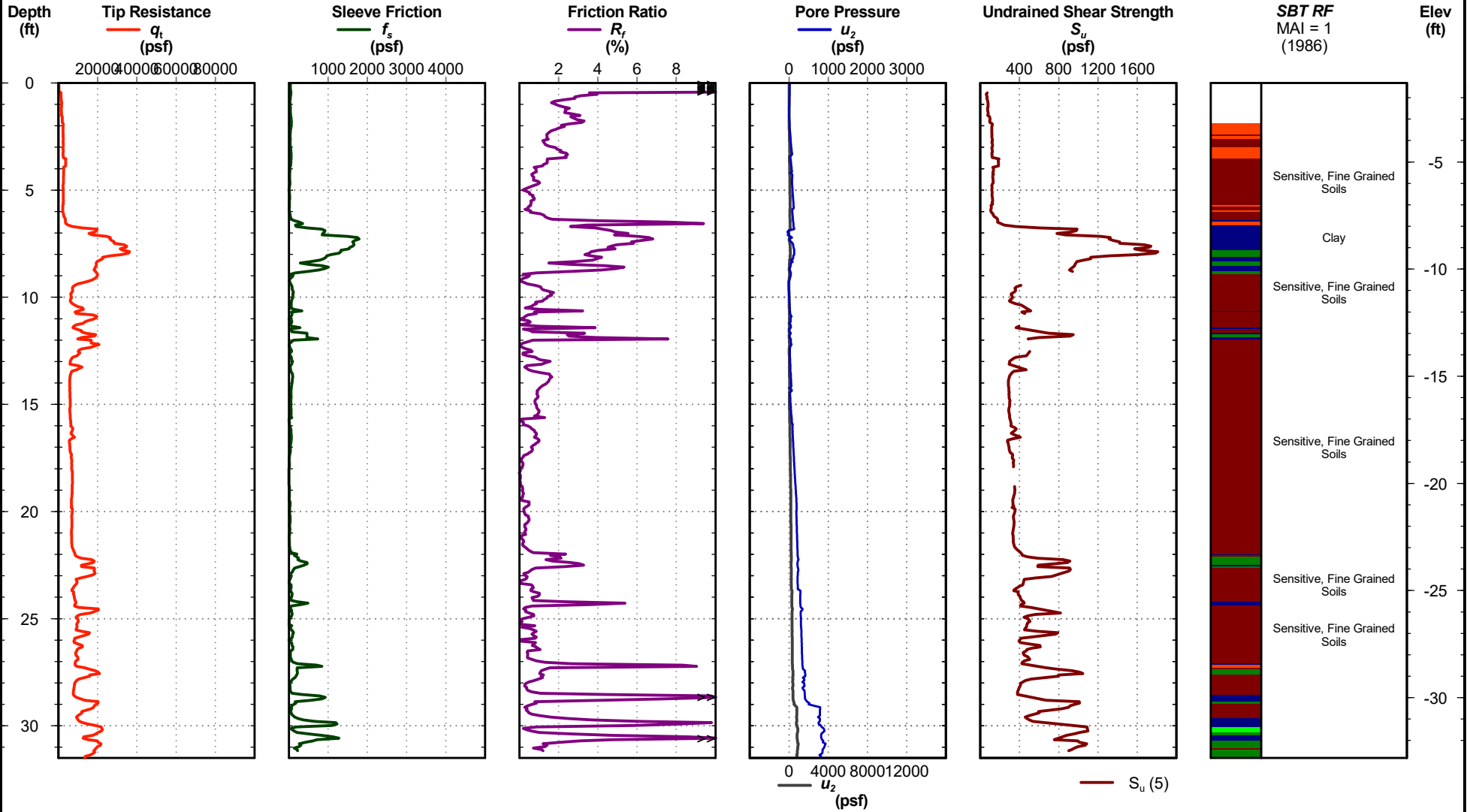
# Cone Penetration Test

# C5

Project #: Brenton CPT  
Date: Aug. 18, 2020

Northing: 441489.0  
Easting: 3759674.0

Elevation: -1.314  
Filename: C5.cpt



- 1 - Sensitive, Fine Grained Soils
- 4 - Silt Mixtures-Clay Silt to Silty Clay
- 7 - Gravelly Sand to Sand
- 2 - Organic Soils, Peats
- 5 - Sand Mixtures-Silty Sand to Sandy Silt
- 8 - Very Stiff Clay to Clayey Sand
- 3 - Clays-Clay to Silty Clay
- 6 - Sands-Clean Sand to Silty Sand
- 9 - Very Stiff Fine Grained Soils

CPT REPORT - DYNAMIC BOTTOM LEGEND CPT BRETON PSF.GPJ DF STD US LAB.GDT 12/23/20

# C5



Engineering and Testing

# Breton Landbridge Marsh Creation (West) Plaquemines Parish (Louisiana)

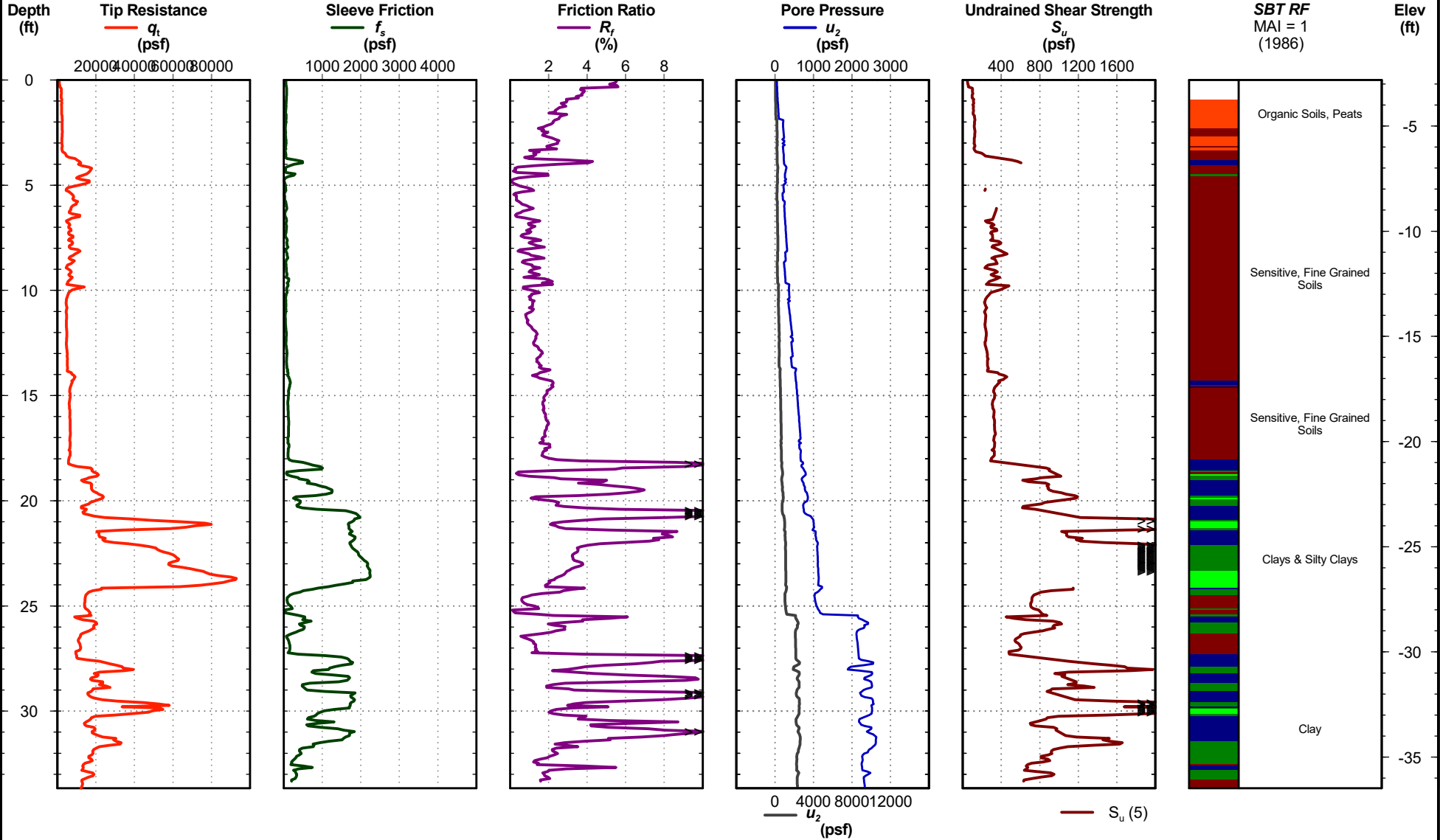
# Cone Penetration Test

# C6

Project #: Brenton CPT  
Date: Aug. 19, 2020

Northing: 440509.8  
Easting: 3757564.0

Elevation: -2.814  
Filename: c6.cpt



- 1 - Sensitive, Fine Grained Soils
- 4 - Silt Mixtures-Clay Silt to Silty Clay
- 7 - Gravelly Sand to Sand
- 2 - Organic Soils, Peats
- 5 - Sand Mixtures-Silty Sand to Sandy Silt
- 8 - Very Stiff Clay to Clayey Sand
- 3 - Clays-Clay to Silty Clay
- 6 - Sands-Clean Sand to Silty Sand
- 9 - Very Stiff Fine Grained Soils

CPT REPORT - DYNAMIC BOTTOM LEGEND CPT BRETON PSF.GPJ DF STD US LAB.GDT 12/23/20

# C6





Engineering and Testing

# Breton Landbridge Marsh Creation (West) Plaquemines Parish (Louisiana)

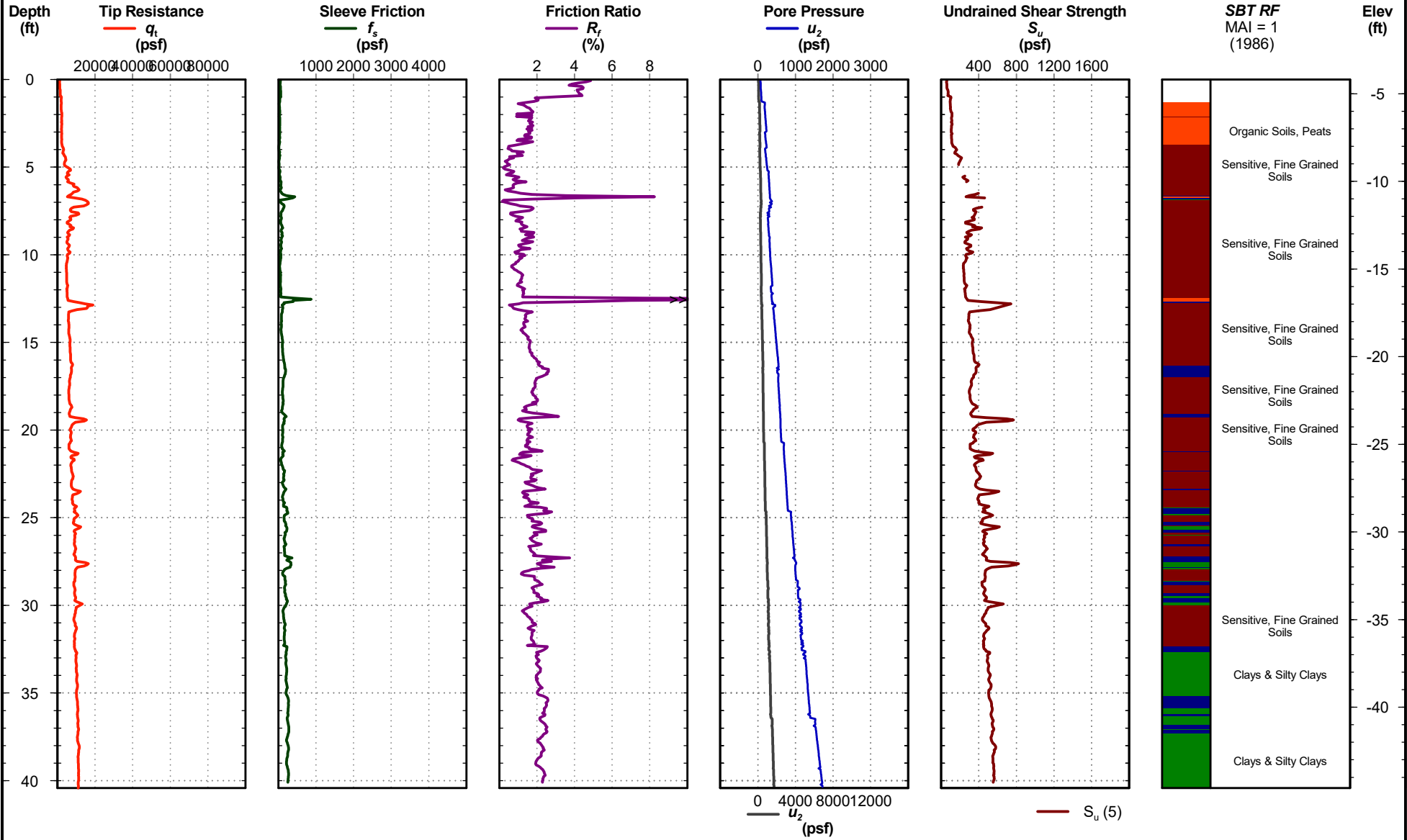
# Cone Penetration Test

# C7

Project #: Brenton CPT  
Date: Aug. 19, 2020

Northing: 440925.8  
Easting: 3755175.3

Elevation: -4.189  
Filename: c7.cpt



- 1 - Sensitive, Fine Grained Soils
- 4 - Silt Mixtures-Clay Silt to Silty Clay
- 7 - Gravelly Sand to Sand
- 2 - Organic Soils, Peats
- 5 - Sand Mixtures-Silty Sand to Sandy Silt
- 8 - Very Stiff Clay to Clayey Sand
- 3 - Clays-Clay to Silty Clay
- 6 - Sands-Clean Sand to Silty Sand
- 9 - Very Stiff Fine Grained Soils

CPT REPORT - DYNAMIC BOTTOM LEGEND CPT BRETON PSF.GPJ DF STD US LAB.GDT 12/23/20

# C7



Engineering and Testing

# Breton Landbridge Marsh Creation (West) Plaquemines Parish (Louisiana)

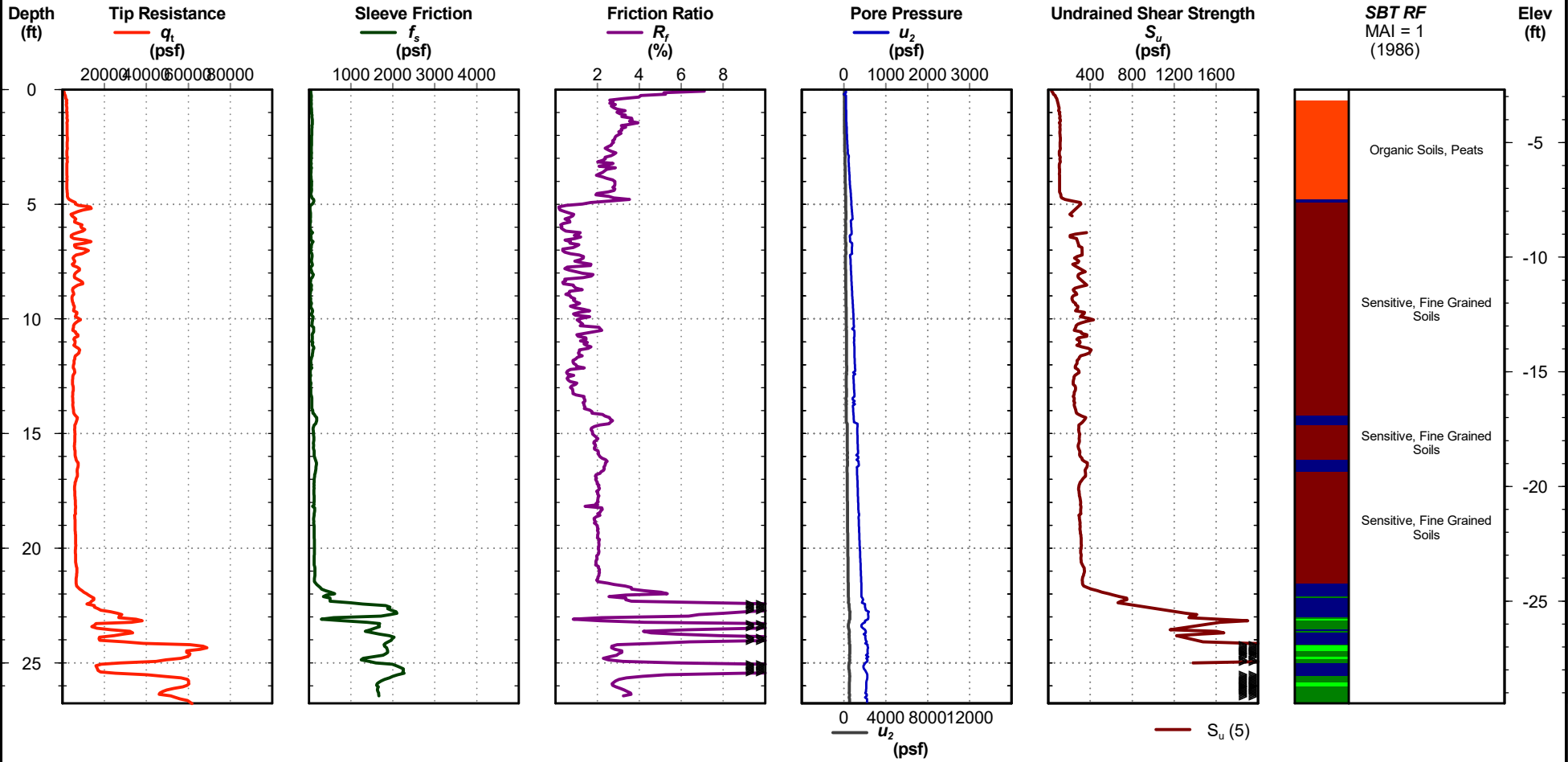
# Cone Penetration Test

# C8

Project #: Brenton CPT  
Date: Aug. 19, 2020

Northing: 439297.7  
Easting: 3754741.2

Elevation: -2.693  
Filename: c8.cpt



- 1 - Sensitive, Fine Grained Soils
- 4 - Silt Mixtures-Clay Silt to Silty Clay
- 7 - Gravelly Sand to Sand
- 2 - Organic Soils, Peats
- 5 - Sand Mixtures-Silty Sand to Sandy Silt
- 8 - Very Stiff Clay to Clayey Sand
- 3 - Clays-Clay to Silty Clay
- 6 - Sands-Clean Sand to Silty Sand
- 9 - Very Stiff Fine Grained Soils

CPT REPORT - DYNAMIC BOTTOM LEGEND CPT BRETON PSF.GPJ\_DF STD US LAB.GDT\_12/23/20

# C8



Engineering and Testing

# Breton Landbridge Marsh Creation (West) Plaquemines Parish (Louisiana)

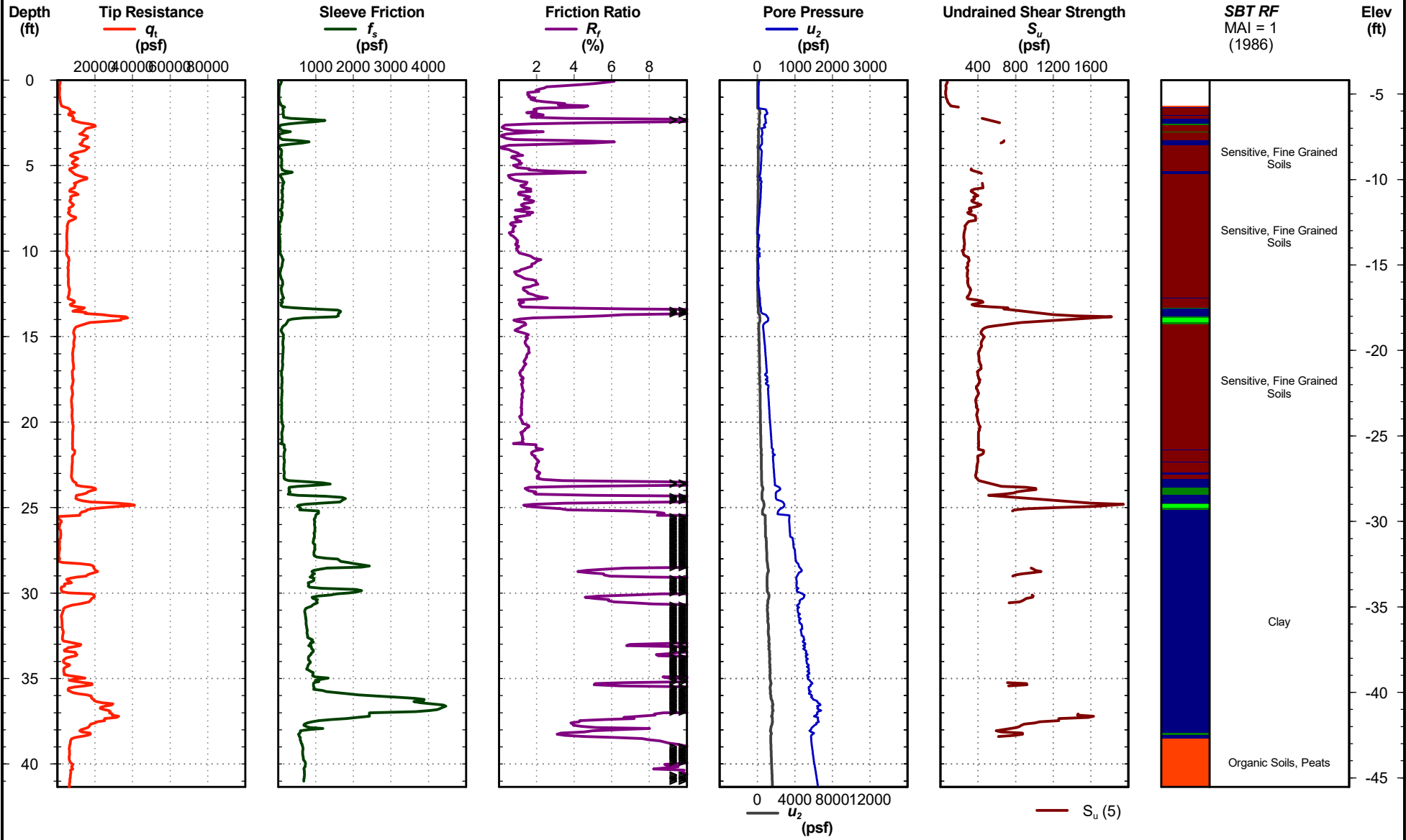
# Cone Penetration Test

# C9

Project #: Breton CPT  
Date: Aug. 19, 2020

Northing: 439170.1  
Easting: 3751593.3

Elevation: -4.191  
Filename: c9.cpt



- 1 - Sensitive, Fine Grained Soils
- 4 - Silt Mixtures-Clay Silt to Silty Clay
- 7 - Gravelly Sand to Sand
- 2 - Organic Soils, Peats
- 5 - Sand Mixtures-Silty Sand to Sandy Silt
- 8 - Very Stiff Clay to Clayey Sand
- 3 - Clays-Clay to Silty Clay
- 6 - Sands-Clean Sand to Silty Sand
- 9 - Very Stiff Fine Grained Soils

CPT REPORT - DYNAMIC BOTTOM LEGEND - CPT-BRETON.PSF.GPJ\_DF STD US LAB.GDT\_12/23/20

# C9



Engineering and Testing

# Breton Landbridge Marsh Creation (West) Plaquemines Parish (Louisiana)

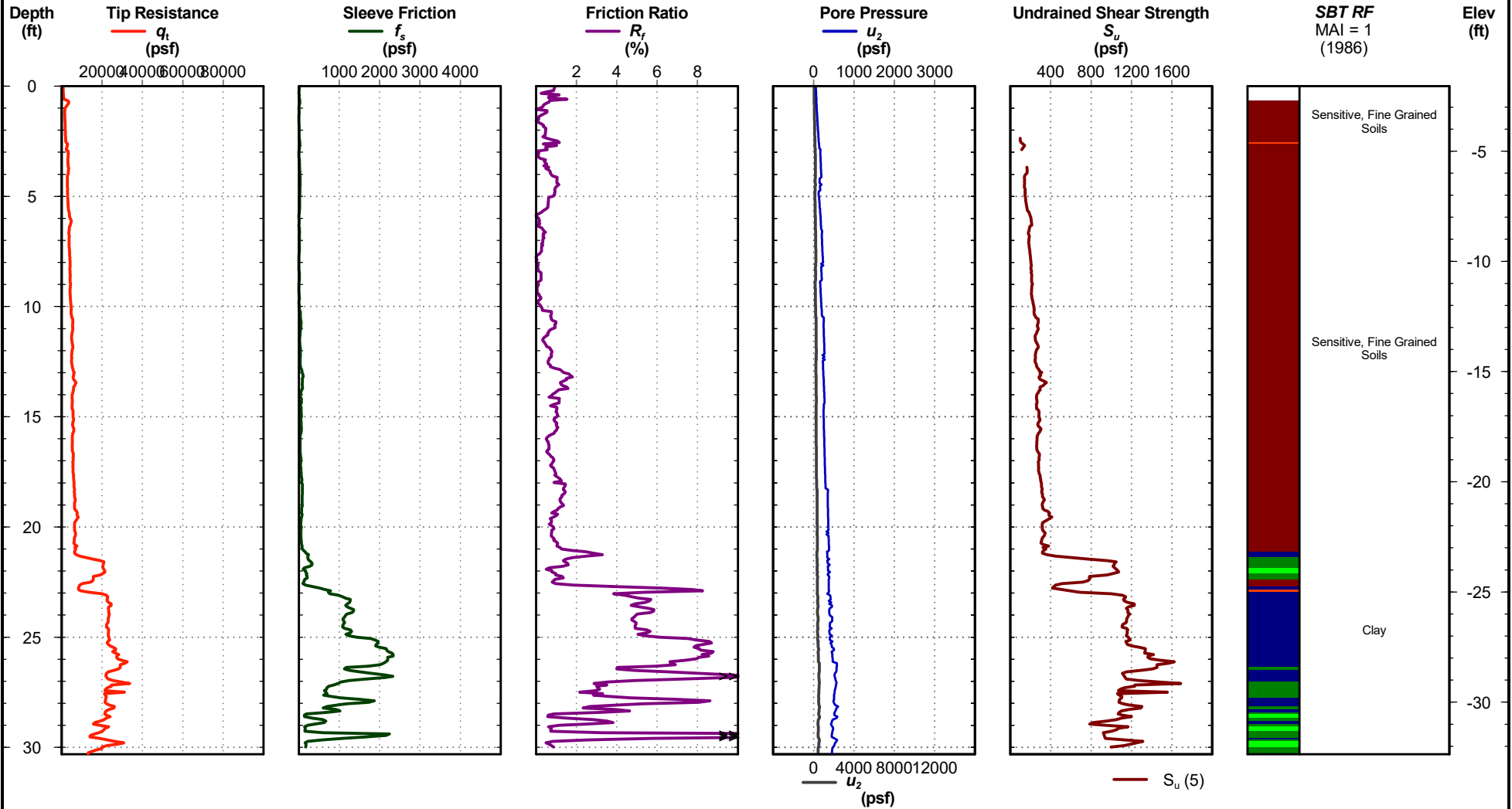
# Cone Penetration Test

# C10

Project #: Brenton CPT  
Date: Aug. 19, 2020

Northing: 438457.6  
Easting: 3749271.4

Elevation: -2.052  
Filename: c10.cpt



- 1 - Sensitive, Fine Grained Soils
- 2 - Organic Soils, Peats
- 3 - Clays-Clay to Silty Clay
- 4 - Silt Mixtures-Clay Silt to Silty Clay
- 5 - Sand Mixtures-Silty Sand to Sandy Silt
- 6 - Sands-Clean Sand to Silty Sand
- 7 - Gravelly Sand to Sand
- 8 - Very Stiff Clay to Clayey Sand
- 9 - Very Stiff Fine Grained Soils

CPT REPORT - DYNAMIC BOTTOM LEGEND CPT BRETON PSF.GPJ DF STD US LAB.GDT 12/23/20

# C10



Engineering and Testing

# Breton Landbridge Marsh Creation (West) Plaquemines Parish (Louisiana)

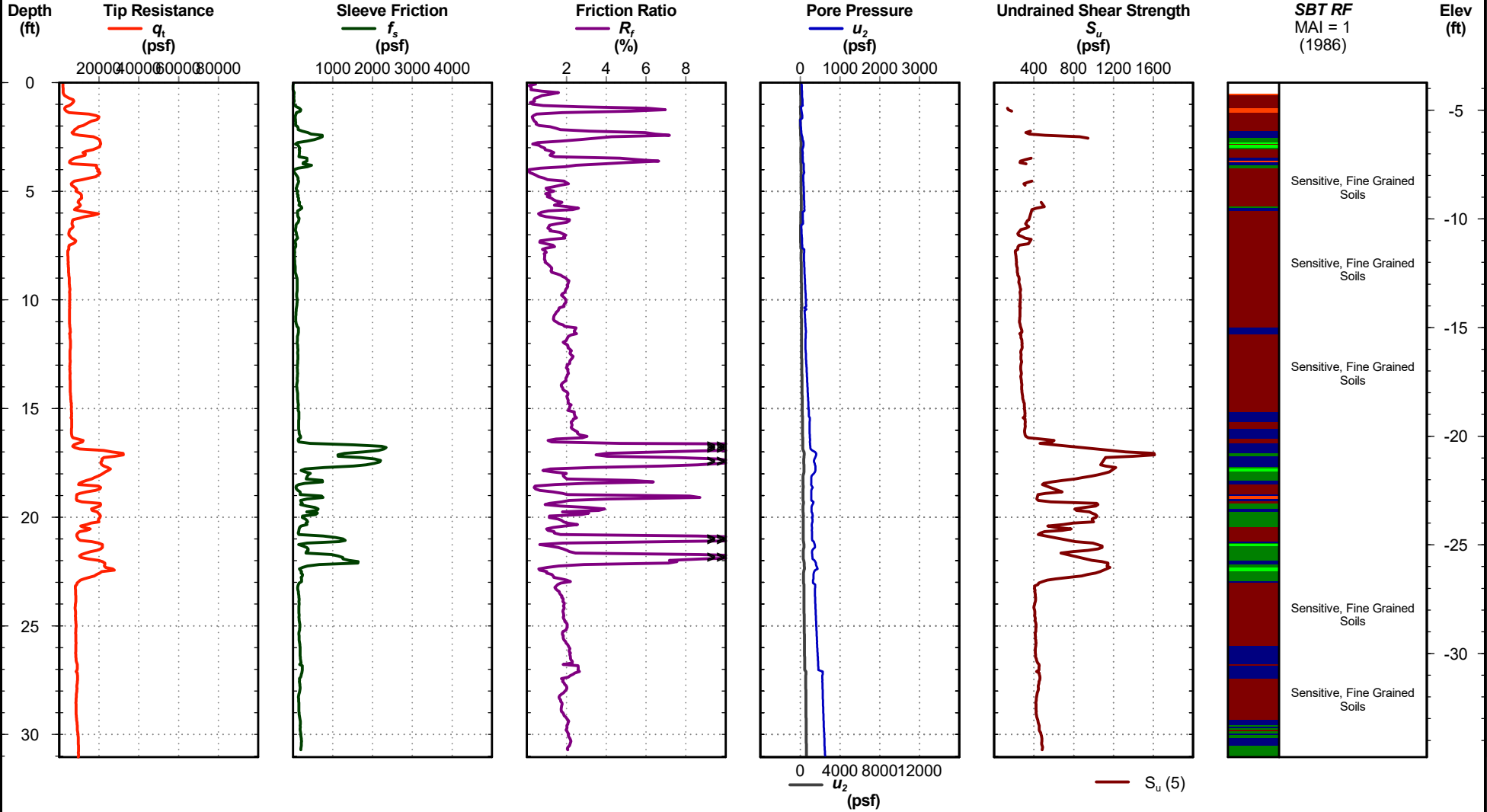
# Cone Penetration Test

# C11

Project #: Brenton CPT  
Date: Aug. 19, 2020

Northing: 436651.6  
Easting: 3749986.0

Elevation: -3.727  
Filename: c11.cpt



- 1 - Sensitive, Fine Grained Soils
- 2 - Organic Soils, Peats
- 3 - Clays-Clay to Silty Clay
- 4 - Silt Mixtures-Clay Silt to Silty Clay
- 5 - Sand Mixtures-Silty Sand to Sandy Silt
- 6 - Sands-Clean Sand to Silty Sand
- 7 - Gravelly Sand to Sand
- 8 - Very Stiff Clay to Clayey Sand
- 9 - Very Stiff Fine Grained Soils

CPT REPORT - DYNAMIC BOTTOM LEGEND - CPT BRETON PSF.GPJ - DF STD US LAB.GDT - 12/23/20

# C11

# CPT Correlations

References are in parenthesis next to the appropriate equation.

## General

$p_a$ =atmospheric pressure (for unit normalization)

$q_t$ =corrected cone tip resistance (tsf)

$f_s$ =friction sleeve resistance (tsf)

$R_f = 100\% \cdot (f_s/q_t)$

$u_2$ =pore pressure behind cone tip (tsf)

$u_0$ =hydrostatic pressure

$$B_q = (u_2 - u_0) / (q_t - \sigma_{v0})$$

$$Q_t = (q_t - \sigma_{v0}) / \sigma'_{v0}$$

$$F_r = 100\% \cdot f_s / (q_t - \sigma_{v0})$$

$$I_c = ((3.47 - \log Q_t)^2 + (\log F_r + 1.22)^2)^{0.5} \quad 2$$

$$I_{SBT} = ((3.47 - \log(q_c/p_a))^2 + (\log F_r + 1.22)^2)^{0.5} \quad 23$$

$$I_{c \text{ J\&D}} = \sqrt{\{3 - \log(Q_t \cdot (1 - B_q))\}^2 + [1.5 + 1.3 \cdot \log(F_r)]^2} \quad 27$$

$$I_{c \text{ J\&B}} = \sqrt{\{3 - \log(Q_t \cdot (1 - B_q) + 1)\}^2 + [1.5 + 1.3 \cdot \log(F_r)]^2} \quad 28$$

## $K_o$

$$K_o(1) \quad K_o = (1 - \sin \phi) OCR^{\sin \phi}$$

$$K_o(2) \quad K_o = 0.1(Q_t) \quad 1$$

## Stress History

$$OCR = \sigma_p' / \sigma'_{v0}$$

$$OCR(1) \quad \sigma_p' = 0.33(q_t - \sigma_{v0}) - \text{clays} \quad 8$$

$$OCR(2) \quad \sigma_p' = 0.53(u_2 - u_0) - \text{clays} \quad 9$$

$$OCR(3) \quad \sigma_p' = 0.60(q_t - u_2) - \text{clays} \quad 9$$

$$OCR(4) \quad OCR = 0.25 Q_t^{1.25} - \text{clays} \quad 37$$

$$OCR(5) \quad OCR = \left[ \frac{0.192 \cdot (q_t/p_a)^{0.22}}{(1 - \sin(\phi')) \cdot (\sigma'_{v0}/p_a)^{0.31}} \right]^{\frac{1}{(\sin(\phi') - 0.27)}} - \text{sands} \quad 35$$

$$OCR(6) \quad \sigma_p' = .101 * p_a^{0.102} * G_{max}^{0.478} * \sigma'_{v0}^{0.420} - \text{all soils} \quad 36$$

## N-Value

$$N_{60} = (q_t/p_a) / [8.5(1 - I_c/4.6)] \quad 6$$

## Undrained Shear Strength

$$S_u(1) \quad S_u = (u_2 - u_0) / N_u \quad \text{where } 7 \leq N_u \leq 9 \quad 10$$

$$S_u(2) \quad S_u = (q_t - \sigma_{v0}) / N_{kT} \quad \text{where } 15 \leq N_{kT} \leq 20 \quad 11$$

$$S_u(3) \quad S_u = 0.091 * ((\sigma'_{v0})^{0.2}) * (q_t - \sigma_{v0})^{0.8} \quad 21$$

$$S_u(4) \quad S_u = (q_c - \sigma_{v0}) / N_k \quad \text{where } 15 \leq N_k \leq 20 \quad 11$$

$$S_u(5) \quad S_u = q_t / N_c \quad \text{where } XXX \leq N_c \leq YYY$$

$$S_u(6) \quad S_u = q_c / N_c \quad \text{where } XXX \leq N_c \leq YYY$$

## Effective Cohesion

$$c' = 0.02 * \sigma_p' \quad 38$$

### Drained Friction Angle

$\phi' (1)$	$\phi' = 17.6 + 11.0 \text{Log}[q_t/(\sigma_{vo}')^{0.5}]$	1
$\phi' (2)$	$\phi' = \arctan[0.1 + 0.38 \text{Log}(q_t/\sigma_{vo}')] ]$	13
$\phi' (3)$	$\phi' = 30.8 \text{Log}[(f_s/\sigma_{vo}') + 1.26]$ (for clays or sands)	14
$\phi' (4)$	$\phi' = 29.5 B_q^{0.121} (0.256 + 0.33 B_q + \text{Log}(Q_t))$	24

### Unit Weight

$$\rho = \gamma/\gamma_w$$

$$\rho = 0.8 \text{Log}(V_s) \quad V_s \text{ in m/sec} \quad 17$$

### Relative Density and Void Ratio

$D_R (1)$	$D_R = 100(q_{c1}/305)^{1/2}$	where, $q_{c1} = q_c/(\sigma_{vo}')^{1/2}$	1
$D_R (2)$	$D_R = -1.292 + 0.268 \text{ln}(q_c \cdot (\sigma_{vo}')^{-0.5})$		18
$D_R (3)$	$D_R = (1/2.41) \cdot \text{ln}(q_{c1}/15.7)$		3
$D_R (4)$	$D_R = 1/2.91 * \text{ln}((q_c/(61 * \sigma_{vo}')^{0.71})) * 100$		20
$D_R (5)$	$D_R = 100 * (0.268 * \text{ln}((q_t/p_a)/(\sigma_{vo}'/p_a)^{0.5}) - 0.675)$		34

$$e_o = 1.099 - 0.204 \text{log}(q_{c1}) \quad 1$$

$$E_D = 5 q_t \quad I_D = 2.0 - 0.14(R_f) \quad K_D = E_D/(34.7 \cdot I_D \cdot \sigma_{vo}')$$

### Compressibility

$$M (1) = R_m E_D \text{ where } R_m = \text{function}(I_D, K_D) \text{ see the following table} \quad 22$$

$I_D \leq 0.6$	$R_M = 0.14 + 2.36 \text{log } K_D$
$I_D \geq 3$	$R_M = 0.5 + 2 \text{log } K_D$
$0.6 < I_D < 3$	$R_M = R_{M,D} + (2.5 - R_{M,D}) \text{log } K_D$
	$R_{M,D} = 0.14 + 0.15(I_D - 0.6)$
$K_D > 10$	$R_M = 0.32 + 2.18 \text{log } K_D$
$R_M < 0.85$	$R_M = 0.85$

$M (2)$	$M = q_c \cdot 10^{(1.09 - 0.0075 D_R)}$ <i>sands</i>	1
$M (3)$	$M = 8.25 (q_t - \sigma_{vo})$ <i>clays</i>	1
$M (4)$	$M = \alpha \cdot G_{max}$ where $0.02 < \alpha < 2$ and $G_{max}$ is from $V_s$	33

### Rigidity Index

$$I_R = \exp \left[ \left( \frac{1.5}{M} + 2.925 \right) \cdot \left( \frac{q_t - \sigma_{vo}}{q_t - u_2} \right) - 2.925 \right] \text{ where } M = 6 \sin \phi' / (3 - \sin \phi') \quad 39$$

### Sensitivity

$S_t (1)$	$S_t = 7.5/R_f$	2
$S_t (2)$	$S_t = (q_t - \sigma_{vo})/(15 \cdot f_s)$	2

### Fines Content

$$FC = [(3.58 - \text{log}(q_t))^2 + (1.43 + \text{log}(R_f))]^{1.8} \quad 4$$

$$FC = [5.31(I_{cfs})^{2.31}] + 9.61, \text{ where } I_{cfs} = [(1.95 - \text{Log} Q_t)^2 + (\text{log} F_r + 1.78)^2]^{0.5}$$

### **Shear Wave Velocity**

$$V_s(1) = 277 \cdot q_t^{0.13} \cdot \sigma'_{vo}{}^{0.27} \quad (\text{sands}) \quad - \text{ m/s and MPa} \quad 29$$

$$V_s(2) = 1.75 \cdot q_t^{0.627} \quad (\text{clays}) - \text{ m/s and kPa} \quad 30$$

$$V_s(3) = (10.1 \cdot \log q_t - 11.4)^{1.67} \cdot \left(\frac{f_s}{q_t} \cdot 100\right)^{0.3} \quad (\text{all soils}) - \text{ m/s and kPa} \quad 31$$

$$V_s(4) = 118.8 \cdot \log f_s + 18.5 \quad (\text{all soils}) - \text{ m/s and kPa} \quad 32$$

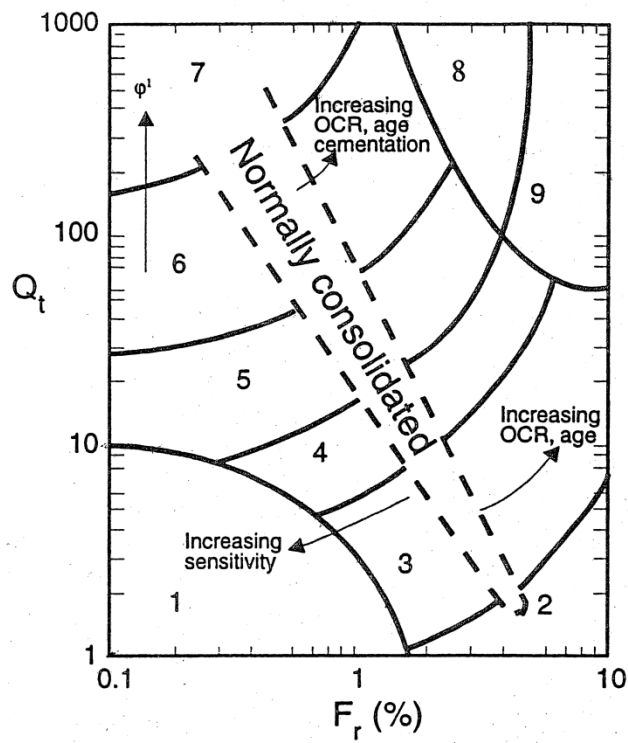
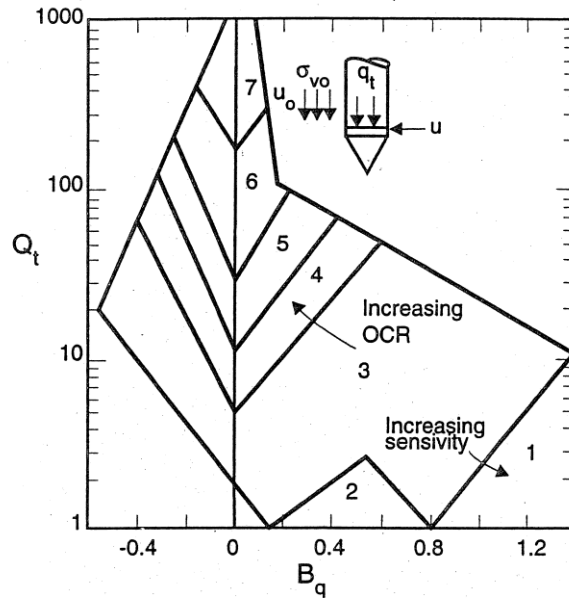
$$G_{max} = \rho V_s^2$$

### **Hydraulic Conductivity**

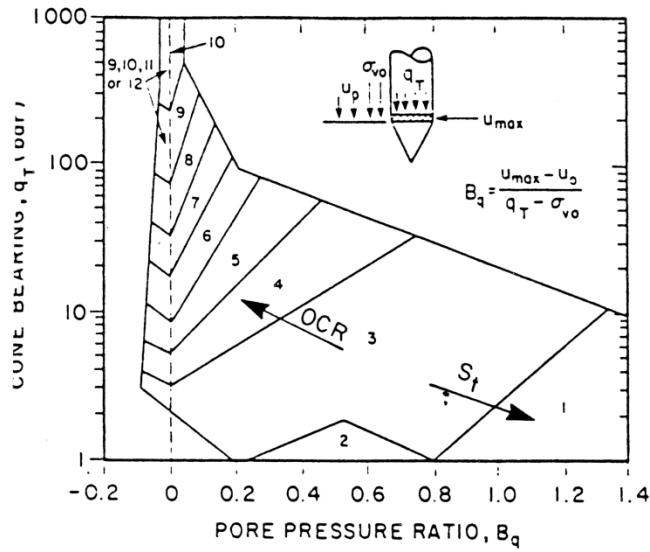
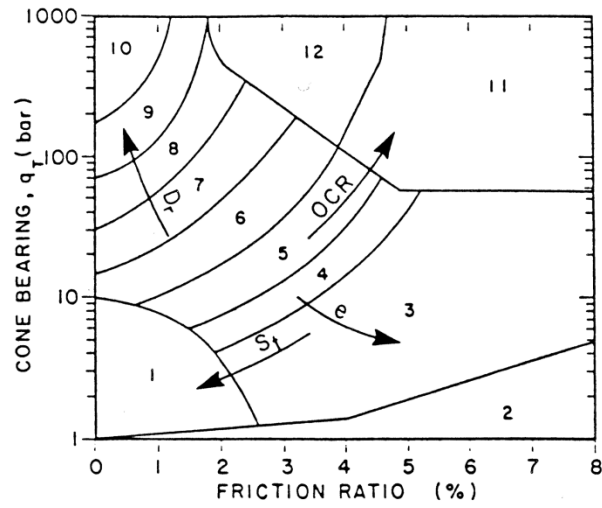
Lookup based on SBT and SBTn (1986 and 1990) 40



# Normalized Soil Behavior Types - Robertson & Campanella (1990)



# Non-Normalized Soil Behavior Types – Robertson & Campanella (1986)



# **APPENDIX H**

## **(CPT Raw Data)**

**CPT -1**  
**Raw Data**

\$  
HA=1,HB=1,HC=CPTLOG-2.00,HD=8/18/2020,HG=-0.762,HP=-0.76,HJ=Brenton  
CPT,HK=C1,HM=07,HN=3206,HO=0.00,HQ=SA,HR=0°0'0.000"E,HS=0°0'0.000"N,HX=0.00,HY=0.00  
,HZ=0.00,KQ=1468.00,KF=6200.00,KU=2136.00,MA=0.590,MB=0.011,MC=10.0,MD=150.0,ME=C1,  
MF=0.000  
RN=,CA=0,CB=0

#  
D=0.000, QC=0.0426, FS=0.1, U=2.5, TA=1.50, B=0, %74769796, NA=6.0387, NB=301.6, NC=432.7  
D=0.020, QC=0.1437, FS=4.6, U=2.5, TA=1.33, B=19, %74774359  
D=0.040, QC=0.1437, FS=4.6, U=1.0, TA=1.38, B=34, %74775031  
D=0.060, QC=0.1437, FS=4.6, U=3.6, TA=1.69, B=34, %74775812  
D=0.080, QC=0.1437, FS=4.6, U=3.6, TA=1.76, B=35, %74776140  
D=0.100, QC=0.1437, FS=4.6, U=1.4, TA=1.24, B=32, %74776937  
D=0.120, QC=0.1052, FS=4.6, U=1.4, TA=1.24, B=34, %74777359  
D=0.140, QC=0.1083, FS=1.7, U=1.4, TA=1.27, B=30, %74778046  
D=0.160, QC=0.0140, FS=2.0, U=1.3, TA=1.15, B=30, %74778828  
D=0.180, QC=0.0026, FS=2.0, U=1.3, TA=1.64, B=29, %74779156  
D=0.200, QC=0.0036, FS=1.8, U=1.4, TA=1.72, B=31, %74779953  
D=0.220, QC=0.0062, FS=1.7, U=1.5, TA=1.71, B=28, %74780734  
D=0.240, QC=0.0104, FS=1.7, U=1.5, TA=1.72, B=29, %74781468  
D=0.260, QC=0.0135, FS=1.7, U=1.7, TA=1.75, B=29, %74782140  
D=0.280, QC=0.0135, FS=1.6, U=1.8, TA=1.75, B=30, %74782609  
D=0.300, QC=0.0135, FS=1.6, U=1.9, TA=1.71, B=30, %74783265  
D=0.320, QC=0.0135, FS=1.8, U=2.1, TA=4.11, B=33, %74784046  
D=0.340, QC=0.0119, FS=1.7, U=2.2, TA=1.47, B=31, %74784828  
D=0.360, QC=0.0109, FS=1.7, U=2.2, TA=1.50, B=30, %74785156  
D=0.380, QC=0.0083, FS=1.4, U=2.3, TA=1.57, B=30, %74785953  
D=0.400, QC=0.0036, FS=1.3, U=2.5, TA=1.68, B=30, %74786734  
D=0.420, QC=0.0031, FS=1.2, U=2.8, TA=1.58, B=28, %74787421  
D=0.440, QC=0.0031, FS=1.6, U=2.8, TA=1.58, B=31, %74787859  
D=0.460, QC=0.0093, FS=1.5, U=3.0, TA=1.90, B=30, %74788531  
D=0.480, QC=0.0104, FS=1.4, U=3.2, TA=1.63, B=33, %74789312  
D=0.500, QC=0.0042, FS=1.4, U=3.2, TA=1.56, B=32, %74789640  
D=0.520, QC=0.0036, FS=1.5, U=3.5, TA=1.59, B=36, %74790406  
D=0.540, QC=0.0016, FS=1.5, U=3.6, TA=1.50, B=35, %74791171  
D=0.560, QC=0.0016, FS=1.7, U=3.8, TA=1.50, B=36, %74791609  
D=0.580, QC=0.0052, FS=1.8, U=4.1, TA=1.57, B=36, %74792281  
D=0.600, QC=0.0068, FS=1.8, U=4.1, TA=1.54, B=37, %74792734  
D=0.620, QC=0.0068, FS=2.0, U=4.2, TA=1.54, B=36, %74793078  
D=0.640, QC=0.0099, FS=2.4, U=4.4, TA=1.51, B=37, %74793765  
D=0.660, QC=0.0088, FS=2.4, U=4.4, TA=1.53, B=35, %74794218  
D=0.680, QC=0.0073, FS=2.7, U=4.6, TA=1.52, B=34, %74794890  
D=0.700, QC=0.0073, FS=2.7, U=4.7, TA=1.52, B=34, %74795343  
D=0.720, QC=0.0073, FS=2.6, U=4.9, TA=1.52, B=36, %74796109  
D=0.740, QC=0.0083, FS=2.6, U=4.9, TA=1.58, B=35, %74796437  
D=0.760, QC=0.0166, FS=2.5, U=5.1, TA=1.58, B=35, %74797218  
D=0.780, QC=0.0166, FS=2.3, U=5.3, TA=1.58, B=34, %74797562  
D=0.800, QC=0.0223, FS=2.6, U=5.5, TA=1.60, B=35, %74798343  
D=0.820, QC=0.0203, FS=2.6, U=5.5, TA=1.54, B=34, %74798671  
D=0.840, QC=0.0239, FS=3.0, U=5.8, TA=1.50, B=35, %74799468

D=0.860, QC=0.0239, FS=3.1, U=6.0, TA=1.50, B=34, %74799812  
D=0.880, QC=0.0244, FS=3.4, U=4.1, TA=1.48, B=35, %74800593 , F=11  
D=0.900, QC=0.0255, FS=3.4, U=4.1, TA=1.60, B=35, %74800937  
D=0.920, QC=0.0255, FS=3.5, U=6.6, TA=1.60, B=35, %74801734  
D=0.940, QC=0.0255, FS=3.9, U=6.8, TA=1.60, B=34, %74802062  
D=0.960, QC=0.0255, FS=3.6, U=4.8, TA=1.62, B=36, %74802765  
D=0.980, QC=0.0239, FS=3.8, U=5.0, TA=1.59, B=34, %74803546  
D=1.000, QC=0.0192, FS=3.8, U=5.0, TA=1.63, B=36, %74803984  
D=1.020, QC=0.0213, FS=3.5, U=5.2, TA=1.63, B=35, %74804656  
D=1.040, QC=0.0213, FS=3.6, U=5.5, TA=1.63, B=35, %74805093  
D=1.060, QC=0.0244, FS=3.4, U=5.7, TA=1.57, B=35, %74805765  
D=1.080, QC=0.0026, FS=3.4, U=5.7, TA=1.64, B=36, %74806203 , F=13  
D=1.100, QC=0.0088, FS=3.1, U=10.6, TA=1.63, B=25, %74824218  
D=1.120, QC=0.0047, FS=3.1, U=10.9, TA=1.63, B=21, %74824906  
D=1.140, QC=0.0088, FS=3.1, U=11.1, TA=1.63, B=21, %74825671  
D=1.160, QC=0.0073, FS=3.0, U=11.6, TA=1.63, B=22, %74826796  
D=1.180, QC=0.0052, FS=2.9, U=11.8, TA=1.63, B=21, %74827609  
D=1.200, QC=0.0042, FS=3.0, U=12.2, TA=1.63, B=25, %74828734  
D=1.220, QC=0.0062, FS=3.0, U=12.4, TA=1.63, B=25, %74829421  
D=1.240, QC=0.0047, FS=2.7, U=12.7, TA=1.63, B=25, %74830187  
D=1.260, QC=0.0026, FS=2.6, U=13.0, TA=1.63, B=25, %74830953  
D=1.280, QC=0.0052, FS=2.6, U=13.2, TA=1.63, B=25, %74831640  
D=1.300, QC=0.0062, FS=2.4, U=13.5, TA=1.63, B=25, %74832421  
D=1.320, QC=0.0047, FS=2.5, U=13.8, TA=1.63, B=25, %74833187 , F=13  
D=1.340, QC=0.0239, FS=2.7, U=21.2, TA=1.61, B=23, %74890031  
D=1.360, QC=0.0239, FS=2.7, U=21.2, TA=1.61, B=23, %74890031  
D=1.380, QC=0.0239, FS=2.7, U=21.2, TA=1.61, B=23, %74890031  
D=1.400, QC=0.0187, FS=2.6, U=20.8, TA=1.61, B=22, %74891218  
D=1.420, QC=0.0187, FS=2.5, U=20.9, TA=1.61, B=21, %74892000  
D=1.440, QC=0.0203, FS=2.5, U=21.2, TA=1.61, B=16, %74893484  
D=1.460, QC=0.0203, FS=2.2, U=21.5, TA=1.61, B=17, %74894578  
D=1.480, QC=0.0197, FS=2.1, U=21.6, TA=1.61, B=16, %74895750  
D=1.500, QC=0.0197, FS=2.5, U=21.8, TA=1.61, B=16, %74896843  
D=1.520, QC=0.0171, FS=2.5, U=22.2, TA=1.61, B=15, %74898281  
D=1.540, QC=0.0156, FS=2.4, U=22.4, TA=1.61, B=16, %74899500  
D=1.560, QC=0.0161, FS=2.0, U=22.7, TA=1.60, B=16, %74900609  
D=1.580, QC=0.0223, FS=1.8, U=20.9, TA=1.61, B=17, %74902062  
D=1.600, QC=0.0234, FS=1.5, U=21.1, TA=1.61, B=16, %74903171  
D=1.620, QC=0.0223, FS=0.9, U=21.7, TA=1.61, B=17, %74904265  
D=1.640, QC=0.0234, FS=0.7, U=21.9, TA=1.61, B=16, %74905500  
D=1.660, QC=0.0218, FS=0.0, U=22.3, TA=1.61, B=17, %74906625  
D=1.680, QC=0.0203, FS=0.5, U=22.8, TA=1.61, B=16, %74908046  
D=1.700, QC=0.0203, FS=0.6, U=23.1, TA=1.61, B=17, %74909265  
D=1.720, QC=0.0218, FS=0.7, U=21.3, TA=1.61, B=16, %74910375  
D=1.740, QC=0.0218, FS=0.6, U=23.7, TA=1.61, B=18, %74911515  
D=1.760, QC=0.0218, FS=0.7, U=21.9, TA=1.61, B=17, %74912625  
D=1.780, QC=0.0182, FS=0.7, U=22.1, TA=1.59, B=17, %74913750  
D=1.800, QC=0.0093, FS=0.7, U=22.6, TA=1.58, B=18, %74914843  
D=1.820, QC=0.0036, FS=0.7, U=22.8, TA=1.52, B=18, %74915984  
D=1.840, QC=0.0016, FS=0.7, U=23.2, TA=1.56, B=17, %74917078

D=1.860, QC=-.0026, FS=0.5, U=23.3, TA=1.55, B=18, %74918171  
D=1.880, QC=0.0036, FS=0.4, U=23.8, TA=1.51, B=18, %74919281  
D=1.900, QC=0.0161, FS=0.4, U=24.0, TA=1.52, B=18, %74920421  
D=1.920, QC=0.0156, FS=0.5, U=24.4, TA=1.51, B=17, %74921531  
D=1.940, QC=0.0083, FS=0.5, U=24.6, TA=1.51, B=17, %74922765  
D=1.960, QC=0.0057, FS=0.4, U=25.1, TA=1.51, B=17, %74923781  
D=1.980, QC=0.0036, FS=0.5, U=25.3, TA=1.49, B=19, %74925000  
D=2.000, QC=0.0078, FS=0.8, U=25.9, TA=1.49, B=17, %74926125  
D=2.020, QC=0.0145, FS=0.8, U=26.1, TA=1.49, B=18, %74927218  
D=2.040, QC=0.0234, FS=0.7, U=26.6, TA=1.50, B=18, %74928328  
D=2.060, QC=0.0338, FS=0.5, U=26.9, TA=1.49, B=18, %74929109  
D=2.080, QC=0.0431, FS=0.4, U=27.1, TA=1.48, B=17, %74930218  
D=2.100, QC=0.0530, FS=0.2, U=27.4, TA=1.48, B=18, %74931328  
D=2.120, QC=0.0649, FS=0.2, U=27.6, TA=1.49, B=17, %74932421  
D=2.140, QC=0.0571, FS=0.1, U=28.1, TA=1.48, B=18, %74933546  
D=2.160, QC=0.0431, FS=0.0, U=28.2, TA=1.48, B=18, %74934656  
D=2.180, QC=0.0338, FS=0.4, U=26.4, TA=1.48, B=22, %74935781  
D=2.200, QC=0.0223, FS=0.3, U=26.6, TA=1.48, B=23, %74936546  
D=2.220, QC=0.0197, FS=0.4, U=26.9, TA=1.48, B=26, %74937312  
D=2.240, QC=0.0203, FS=0.1, U=27.2, TA=1.50, B=24, %74938093  
D=2.260, QC=0.0431, FS=0.1, U=27.3, TA=1.48, B=26, %74938890  
D=2.280, QC=0.1371, FS=0.4, U=27.2, TA=1.49, B=25, %74939562  
D=2.300, QC=0.3132, FS=3.1, U=27.6, TA=1.48, B=25, %74940343  
D=2.320, QC=0.7381, FS=18.2, U=29.6, TA=1.48, B=24, %74941437  
D=2.340, QC=0.6778, FS=22.6, U=28.0, TA=1.48, B=25, %74942218  
D=2.360, QC=0.4514, FS=19.8, U=16.8, TA=1.48, B=26, %74942984  
D=2.380, QC=0.3589, FS=11.7, U=14.8, TA=1.48, B=27, %74943671  
D=2.400, QC=0.2587, FS=3.0, U=13.6, TA=1.48, B=26, %74944453  
D=2.420, QC=0.2249, FS=1.3, U=13.5, TA=1.48, B=28, %74945218  
D=2.440, QC=0.3220, FS=0.7, U=14.0, TA=1.48, B=26, %74945984  
D=2.460, QC=0.2545, FS=3.8, U=19.6, TA=0.77, B=26, %74999500  
D=2.480, QC=0.2545, FS=3.8, U=19.6, TA=0.77, B=26, %74999500  
D=2.500, QC=0.2545, FS=3.8, U=19.6, TA=0.77, B=26, %74999500  
D=2.520, QC=0.1969, FS=3.8, U=19.6, TA=0.79, B=24, %74999953  
D=2.540, QC=0.1605, FS=3.4, U=19.2, TA=0.77, B=26, %75000625  
D=2.560, QC=0.1475, FS=3.2, U=19.5, TA=0.87, B=24, %75001421  
D=2.580, QC=0.1392, FS=3.5, U=19.5, TA=0.89, B=23, %75002109  
D=2.600, QC=0.1174, FS=4.4, U=19.8, TA=0.88, B=18, %75003312  
D=2.620, QC=0.1574, FS=4.8, U=17.6, TA=0.88, B=16, %75004453  
D=2.640, QC=0.2026, FS=4.9, U=17.7, TA=0.89, B=17, %75005484  
D=2.660, QC=0.3002, FS=5.1, U=17.8, TA=0.89, B=13, %75007031  
D=2.680, QC=0.3709, FS=5.3, U=18.0, TA=0.95, B=13, %75008500  
D=2.700, QC=0.3916, FS=4.1, U=18.3, TA=0.98, B=13, %75010062  
D=2.720, QC=0.3714, FS=3.8, U=18.4, TA=1.00, B=13, %75011515  
D=2.740, QC=0.3818, FS=3.9, U=18.5, TA=1.01, B=14, %75012656  
D=2.760, QC=0.4181, FS=4.6, U=18.7, TA=1.01, B=13, %75014109  
D=2.780, QC=0.4254, FS=4.8, U=19.0, TA=1.01, B=13, %75015687  
D=2.800, QC=0.4161, FS=5.4, U=19.2, TA=1.01, B=14, %75017125  
D=2.820, QC=0.3999, FS=5.5, U=19.4, TA=1.01, B=15, %75018328  
D=2.840, QC=0.3407, FS=4.1, U=19.4, TA=1.01, B=14, %75019765

D=2.860, QC=0.2826, FS=2.8, U=19.7, TA=1.01, B=13, %75021218  
D=2.880, QC=0.2062, FS=2.4, U=19.8, TA=1.01, B=14, %75022437  
D=2.900, QC=0.1927, FS=2.1, U=20.1, TA=1.01, B=15, %75023875  
D=2.920, QC=0.3553, FS=2.9, U=20.2, TA=1.01, B=15, %75025437  
D=2.940, QC=0.4098, FS=4.6, U=20.5, TA=1.01, B=14, %75026593  
D=2.960, QC=0.3605, FS=4.9, U=20.7, TA=1.01, B=14, %75028031  
D=2.980, QC=0.2618, FS=4.3, U=20.7, TA=1.01, B=15, %75029125  
D=3.000, QC=0.1776, FS=4.9, U=20.9, TA=1.01, B=15, %75030609  
D=3.020, QC=0.1543, FS=5.4, U=21.3, TA=1.01, B=15, %75031750  
D=3.040, QC=0.1735, FS=5.2, U=21.5, TA=1.01, B=15, %75032843  
D=3.060, QC=0.2306, FS=4.8, U=21.7, TA=1.01, B=16, %75034421  
D=3.080, QC=0.2270, FS=5.3, U=19.6, TA=1.01, B=15, %75035515  
D=3.100, QC=0.1911, FS=6.7, U=19.9, TA=1.01, B=15, %75037078  
D=3.120, QC=0.3236, FS=7.2, U=20.0, TA=1.01, B=15, %75038203  
D=3.140, QC=0.3309, FS=6.5, U=20.2, TA=1.01, B=15, %75039656  
D=3.160, QC=0.2722, FS=4.7, U=20.3, TA=1.01, B=15, %75040750  
D=3.180, QC=0.1943, FS=4.8, U=20.6, TA=1.01, B=14, %75042218  
D=3.200, QC=0.1693, FS=5.8, U=20.6, TA=1.01, B=15, %75043453  
D=3.220, QC=0.2088, FS=6.1, U=18.7, TA=1.01, B=15, %75044890  
D=3.240, QC=0.2104, FS=5.6, U=18.8, TA=1.01, B=17, %75046000  
D=3.260, QC=0.2021, FS=5.9, U=19.0, TA=1.01, B=17, %75047109  
D=3.280, QC=0.1995, FS=7.0, U=19.1, TA=1.01, B=19, %75047875  
D=3.300, QC=0.1709, FS=6.2, U=19.3, TA=1.01, B=20, %75049078  
D=3.320, QC=0.1361, FS=5.4, U=19.4, TA=1.01, B=21, %75049781  
D=3.340, QC=0.0836, FS=4.4, U=19.6, TA=1.01, B=21, %75050890  
D=3.360, QC=0.0826, FS=3.9, U=19.7, TA=1.01, B=21, %75051593  
D=3.380, QC=0.0966, FS=3.9, U=20.0, TA=1.01, B=22, %75052828  
D=3.400, QC=0.1013, FS=4.0, U=20.0, TA=1.01, B=22, %75053500  
D=3.420, QC=0.1226, FS=4.2, U=20.2, TA=1.01, B=21, %75054609  
D=3.440, QC=0.1963, FS=4.6, U=20.2, TA=1.01, B=22, %75055390  
D=3.460, QC=0.2509, FS=4.8, U=20.4, TA=1.01, B=23, %75056156  
D=3.480, QC=0.2005, FS=3.7, U=20.5, TA=1.01, B=22, %75057281  
D=3.500, QC=0.1605, FS=4.1, U=20.7, TA=1.01, B=21, %75058078  
D=3.520, QC=0.1340, FS=4.7, U=20.9, TA=1.01, B=23, %75059187  
D=3.540, QC=0.1589, FS=4.9, U=21.0, TA=1.01, B=23, %75059859  
D=3.560, QC=0.1418, FS=5.0, U=21.1, TA=1.01, B=22, %75060656  
D=3.580, QC=0.1184, FS=5.2, U=21.3, TA=1.01, B=22, %75061750  
D=3.600, QC=0.1060, FS=5.4, U=21.5, TA=1.01, B=21, %75062515  
D=3.620, QC=0.1044, FS=5.1, U=21.6, TA=1.01, B=22, %75063296  
D=3.640, QC=0.1278, FS=4.1, U=21.6, TA=1.01, B=22, %75064421  
D=3.660, QC=0.1579, FS=5.6, U=24.2, TA=1.00, B=31, %75116906  
D=3.680, QC=0.1579, FS=5.6, U=24.2, TA=1.00, B=31, %75116906  
D=3.700, QC=0.1579, FS=5.6, U=24.2, TA=1.00, B=31, %75116906  
D=3.720, QC=0.1579, FS=5.6, U=24.2, TA=1.00, B=31, %75116906  
D=3.740, QC=0.1158, FS=5.6, U=24.2, TA=1.01, B=28, %75117234  
D=3.760, QC=0.1117, FS=4.3, U=23.9, TA=1.01, B=24, %75118343  
D=3.780, QC=0.1101, FS=4.3, U=23.9, TA=1.01, B=25, %75119125  
D=3.800, QC=0.1096, FS=3.9, U=24.1, TA=1.01, B=23, %75119890  
D=3.820, QC=0.1049, FS=4.0, U=24.1, TA=1.01, B=21, %75120671  
D=3.840, QC=0.1013, FS=3.8, U=24.1, TA=1.01, B=22, %75121703



D=3.860, QC=0.0982, FS=3.1, U=24.3, TA=1.01, B=21, %75122484  
D=3.880, QC=0.0982, FS=2.5, U=24.5, TA=1.01, B=18, %75123593  
D=3.900, QC=0.1028, FS=2.2, U=24.5, TA=1.01, B=18, %75124718  
D=3.920, QC=0.1028, FS=2.4, U=24.8, TA=1.01, B=15, %75126281  
D=3.940, QC=0.0976, FS=2.9, U=25.0, TA=1.01, B=17, %75127390  
D=3.960, QC=0.1018, FS=3.0, U=25.0, TA=1.01, B=16, %75128515  
D=3.980, QC=0.0987, FS=3.1, U=23.0, TA=1.01, B=16, %75129656  
D=4.000, QC=0.1023, FS=3.1, U=23.1, TA=1.01, B=16, %75130781  
D=4.020, QC=0.0976, FS=3.1, U=23.2, TA=1.01, B=18, %75131906  
D=4.040, QC=0.1096, FS=3.0, U=23.5, TA=1.01, B=17, %75133046  
D=4.060, QC=0.2581, FS=3.6, U=23.5, TA=1.01, B=16, %75134531  
D=4.080, QC=0.3428, FS=4.7, U=23.7, TA=1.01, B=17, %75135640  
D=4.100, QC=0.2732, FS=4.3, U=23.7, TA=1.01, B=18, %75136765  
D=4.120, QC=0.2337, FS=5.2, U=23.9, TA=1.01, B=18, %75137906  
D=4.140, QC=0.1849, FS=6.4, U=24.0, TA=1.01, B=18, %75138578  
D=4.160, QC=0.1537, FS=5.3, U=24.1, TA=1.01, B=18, %75139781  
D=4.180, QC=0.1397, FS=5.8, U=24.4, TA=1.01, B=19, %75140875  
D=4.200, QC=0.1288, FS=6.0, U=24.5, TA=1.01, B=19, %75141968  
D=4.220, QC=0.1340, FS=5.7, U=24.7, TA=1.01, B=18, %75143062  
D=4.240, QC=0.1428, FS=5.7, U=24.8, TA=1.01, B=18, %75144265  
D=4.260, QC=0.1366, FS=5.9, U=24.8, TA=1.01, B=19, %75145062  
D=4.280, QC=0.1293, FS=4.3, U=25.1, TA=1.01, B=18, %75146078  
D=4.300, QC=0.1247, FS=4.5, U=25.2, TA=1.01, B=18, %75147281  
D=4.320, QC=0.1273, FS=3.5, U=25.4, TA=1.01, B=18, %75148390  
D=4.340, QC=0.1361, FS=3.4, U=25.5, TA=1.01, B=19, %75149515  
D=4.360, QC=0.1361, FS=3.5, U=25.6, TA=1.01, B=19, %75150296  
D=4.380, QC=0.1319, FS=3.6, U=25.8, TA=1.01, B=18, %75151421  
D=4.400, QC=0.1366, FS=3.3, U=25.9, TA=1.01, B=19, %75152515  
D=4.420, QC=0.1460, FS=3.4, U=26.2, TA=1.01, B=19, %75153640  
D=4.440, QC=0.1667, FS=3.3, U=26.2, TA=1.01, B=19, %75154750  
D=4.460, QC=0.1693, FS=3.3, U=26.3, TA=1.01, B=18, %75155531  
D=4.480, QC=0.1667, FS=4.0, U=26.5, TA=1.01, B=18, %75156562  
D=4.500, QC=0.1480, FS=4.5, U=26.6, TA=1.01, B=19, %75157796  
D=4.520, QC=0.1460, FS=3.8, U=26.8, TA=1.01, B=18, %75158906  
D=4.540, QC=0.1330, FS=3.8, U=27.0, TA=1.01, B=18, %75160015  
D=4.560, QC=0.1402, FS=3.6, U=27.0, TA=1.01, B=18, %75160703  
D=4.580, QC=0.1402, FS=3.3, U=27.2, TA=1.01, B=19, %75161843  
D=4.600, QC=0.1548, FS=3.6, U=27.3, TA=1.01, B=19, %75162968  
D=4.620, QC=0.1522, FS=3.9, U=25.3, TA=1.01, B=18, %75164093  
D=4.640, QC=0.1584, FS=4.1, U=25.3, TA=1.01, B=19, %75164890  
D=4.660, QC=0.2104, FS=4.2, U=25.5, TA=1.01, B=20, %75166015  
D=4.680, QC=0.2846, FS=5.7, U=25.6, TA=1.01, B=19, %75167171  
D=4.700, QC=0.3381, FS=5.6, U=25.7, TA=1.01, B=19, %75167828  
D=4.720, QC=0.2265, FS=4.7, U=25.9, TA=1.01, B=20, %75169046  
D=4.740, QC=0.1745, FS=5.8, U=26.0, TA=1.01, B=25, %75169812  
D=4.760, QC=0.1444, FS=5.5, U=26.2, TA=1.01, B=23, %75170828  
D=4.780, QC=0.1376, FS=5.5, U=26.3, TA=1.01, B=22, %75171609  
D=4.800, QC=0.1350, FS=5.5, U=26.5, TA=1.01, B=22, %75172390  
D=4.820, QC=0.1371, FS=5.4, U=26.5, TA=1.01, B=22, %75173515  
D=4.840, QC=0.1236, FS=5.2, U=26.6, TA=1.01, B=22, %75174312

D=4.860, QC=0.1335, FS=4.5, U=28.0, TA=1.01, B=27, %75218234  
D=4.880, QC=0.1335, FS=4.5, U=28.0, TA=1.01, B=27, %75218234  
D=4.900, QC=0.1350, FS=4.5, U=28.0, TA=1.01, B=28, %75218656  
D=4.920, QC=0.1335, FS=4.2, U=27.5, TA=1.01, B=26, %75219437  
D=4.940, QC=0.1350, FS=4.1, U=27.5, TA=1.01, B=28, %75220109  
D=4.960, QC=0.1366, FS=4.3, U=27.6, TA=1.01, B=26, %75220875  
D=4.980, QC=0.1366, FS=4.5, U=27.7, TA=1.01, B=28, %75221656  
D=5.000, QC=0.1428, FS=4.9, U=27.8, TA=1.01, B=27, %75222421  
D=5.020, QC=0.1439, FS=5.0, U=27.8, TA=1.01, B=27, %75223187  
D=5.040, QC=0.1439, FS=4.8, U=28.0, TA=1.01, B=21, %75224296  
D=5.060, QC=0.1454, FS=4.7, U=28.2, TA=1.01, B=22, %75224984  
D=5.080, QC=0.1418, FS=4.5, U=28.2, TA=1.01, B=20, %75226093  
D=5.100, QC=0.1480, FS=4.9, U=28.3, TA=1.01, B=15, %75227203  
D=5.120, QC=0.1454, FS=4.9, U=28.5, TA=1.01, B=17, %75228437  
D=5.140, QC=0.1496, FS=5.0, U=28.6, TA=1.01, B=17, %75229546  
D=5.160, QC=0.1511, FS=5.1, U=28.7, TA=1.01, B=17, %75230687  
D=5.180, QC=0.1517, FS=5.6, U=28.8, TA=1.01, B=18, %75231796  
D=5.200, QC=0.1527, FS=5.8, U=28.9, TA=1.01, B=17, %75232906  
D=5.220, QC=0.1553, FS=5.8, U=29.1, TA=1.01, B=18, %75234031  
D=5.240, QC=0.1569, FS=6.0, U=29.2, TA=1.01, B=17, %75235156  
D=5.260, QC=0.1600, FS=6.1, U=29.4, TA=1.01, B=18, %75236281  
D=5.280, QC=0.1579, FS=6.2, U=29.5, TA=1.01, B=17, %75237406  
D=5.300, QC=0.1563, FS=6.1, U=29.8, TA=1.01, B=18, %75238515  
D=5.320, QC=0.1569, FS=6.2, U=29.9, TA=1.01, B=17, %75239671  
D=5.340, QC=0.1537, FS=6.3, U=30.1, TA=1.01, B=19, %75240796  
D=5.360, QC=0.1496, FS=6.4, U=30.2, TA=1.01, B=18, %75241953  
D=5.380, QC=0.1511, FS=6.2, U=30.4, TA=1.01, B=18, %75243078  
D=5.400, QC=0.1527, FS=6.1, U=30.6, TA=1.01, B=19, %75243734  
D=5.420, QC=0.1543, FS=6.0, U=30.7, TA=1.01, B=19, %75244843  
D=5.440, QC=0.1553, FS=6.0, U=30.8, TA=1.01, B=19, %75246046  
D=5.460, QC=0.1548, FS=6.1, U=30.9, TA=1.01, B=19, %75247187  
D=5.480, QC=0.1584, FS=6.1, U=31.1, TA=1.01, B=19, %75247953  
D=5.500, QC=0.1584, FS=5.9, U=31.2, TA=1.01, B=20, %75249046  
D=5.520, QC=0.1584, FS=6.0, U=31.4, TA=1.01, B=18, %75250140  
D=5.540, QC=0.1574, FS=5.9, U=31.6, TA=1.01, B=19, %75251265  
D=5.560, QC=0.1610, FS=5.8, U=31.8, TA=1.01, B=19, %75252406  
D=5.580, QC=0.2010, FS=5.7, U=31.8, TA=1.01, B=20, %75253187  
D=5.600, QC=0.3823, FS=9.2, U=32.6, TA=1.01, B=18, %75254296  
D=5.620, QC=0.6072, FS=14.8, U=32.5, TA=1.01, B=18, %75255406  
D=5.640, QC=0.6347, FS=21.4, U=34.4, TA=1.01, B=19, %75256546  
D=5.660, QC=0.3724, FS=16.5, U=35.0, TA=1.02, B=19, %75257656  
D=5.680, QC=0.2317, FS=7.2, U=33.7, TA=1.01, B=18, %75258421  
D=5.700, QC=0.1917, FS=7.0, U=33.4, TA=1.01, B=19, %75259531  
D=5.720, QC=0.1605, FS=7.5, U=33.4, TA=1.01, B=19, %75260640  
D=5.740, QC=0.1631, FS=6.9, U=33.7, TA=1.01, B=20, %75261765  
D=5.760, QC=0.1662, FS=6.5, U=33.8, TA=1.01, B=19, %75262546  
D=5.780, QC=0.1683, FS=6.6, U=33.9, TA=1.01, B=19, %75263656  
D=5.800, QC=0.1704, FS=6.8, U=34.2, TA=1.01, B=18, %75264781  
D=5.820, QC=0.1709, FS=5.6, U=34.3, TA=1.01, B=19, %75265906  
D=5.840, QC=0.1704, FS=6.1, U=34.5, TA=1.01, B=18, %75267046

D=5.860, QC=0.1735, FS=6.2, U=34.7, TA=1.01, B=19, %75267734  
D=5.880, QC=0.1756, FS=6.3, U=34.8, TA=1.01, B=18, %75268843  
D=5.900, QC=0.1750, FS=6.6, U=35.0, TA=1.01, B=18, %75270046  
D=5.920, QC=0.1787, FS=6.7, U=35.1, TA=1.01, B=18, %75271171  
D=5.940, QC=0.1787, FS=6.7, U=35.4, TA=1.01, B=19, %75272296  
D=5.960, QC=0.1761, FS=6.7, U=35.4, TA=1.01, B=18, %75273062  
D=5.980, QC=0.1750, FS=6.6, U=35.6, TA=1.01, B=19, %75274171  
D=6.000, QC=0.1750, FS=6.5, U=35.8, TA=1.01, B=18, %75275281  
D=6.020, QC=0.1714, FS=6.7, U=36.0, TA=1.01, B=18, %75276406  
D=6.040, QC=0.1714, FS=6.4, U=36.2, TA=1.01, B=18, %75277562  
D=6.060, QC=0.1631, FS=6.6, U=36.2, TA=1.01, B=18, %75278656 , F=11  
D=6.080, QC=0.1563, FS=7.0, U=38.1, TA=1.12, B=20, %75331109  
D=6.100, QC=0.1563, FS=7.0, U=38.1, TA=1.12, B=20, %75331109  
D=6.120, QC=0.1563, FS=7.0, U=38.1, TA=1.12, B=20, %75331109  
D=6.140, QC=0.1626, FS=7.3, U=40.2, TA=1.12, B=24, %75331906  
D=6.160, QC=0.1688, FS=6.2, U=40.3, TA=1.12, B=19, %75333015  
D=6.180, QC=0.1652, FS=6.3, U=40.4, TA=1.13, B=18, %75333671  
D=6.200, QC=0.1636, FS=6.9, U=41.2, TA=1.11, B=1, %75341187  
D=6.220, QC=0.1688, FS=6.5, U=38.8, TA=1.13, B=26, %75341968  
D=6.240, QC=0.1652, FS=6.6, U=41.4, TA=1.14, B=21, %75342750  
D=6.260, QC=0.1698, FS=6.2, U=39.0, TA=1.13, B=21, %75343875  
D=6.280, QC=0.1782, FS=6.2, U=39.2, TA=1.13, B=15, %75345312  
D=6.300, QC=0.1823, FS=6.3, U=39.4, TA=1.15, B=15, %75346468  
D=6.320, QC=0.1849, FS=6.4, U=39.5, TA=1.13, B=15, %75347578  
D=6.340, QC=0.1854, FS=6.6, U=39.7, TA=1.13, B=15, %75349125  
D=6.360, QC=0.1813, FS=6.9, U=39.8, TA=1.15, B=15, %75350234  
D=6.380, QC=0.1839, FS=6.9, U=40.0, TA=1.15, B=16, %75351343  
D=6.400, QC=0.1880, FS=7.1, U=40.2, TA=1.14, B=15, %75352781  
D=6.420, QC=0.1922, FS=7.1, U=40.4, TA=1.13, B=16, %75354000  
D=6.440, QC=0.1828, FS=7.7, U=40.4, TA=1.14, B=15, %75355093  
D=6.460, QC=0.1969, FS=7.6, U=40.7, TA=1.15, B=16, %75356578  
D=6.480, QC=0.1979, FS=7.3, U=40.9, TA=1.15, B=15, %75357718  
D=6.500, QC=0.2005, FS=7.4, U=41.1, TA=1.15, B=16, %75358843  
D=6.520, QC=0.2067, FS=7.4, U=41.3, TA=1.15, B=16, %75360296  
D=6.540, QC=0.2145, FS=7.9, U=41.6, TA=1.15, B=17, %75361421  
D=6.560, QC=0.2109, FS=7.3, U=41.7, TA=1.15, B=16, %75362656  
D=6.580, QC=0.2239, FS=7.8, U=41.9, TA=1.15, B=16, %75363671  
D=6.600, QC=0.2327, FS=8.0, U=42.1, TA=1.15, B=17, %75364812  
D=6.620, QC=0.2332, FS=8.1, U=42.3, TA=1.15, B=17, %75366015  
D=6.640, QC=0.2389, FS=8.2, U=42.4, TA=1.15, B=16, %75367109  
D=6.660, QC=0.2431, FS=8.8, U=42.6, TA=1.15, B=17, %75368250  
D=6.680, QC=0.2467, FS=9.3, U=42.9, TA=1.15, B=17, %75369703  
D=6.700, QC=0.2441, FS=9.4, U=42.9, TA=1.15, B=18, %75370828  
D=6.720, QC=0.2420, FS=9.5, U=43.2, TA=1.15, B=17, %75371937  
D=6.740, QC=0.2358, FS=9.6, U=43.3, TA=1.15, B=17, %75373046  
D=6.760, QC=0.2348, FS=9.9, U=43.6, TA=1.15, B=17, %75374203  
D=6.780, QC=0.2259, FS=10.0, U=43.7, TA=1.15, B=18, %75375312  
D=6.800, QC=0.2239, FS=9.9, U=43.9, TA=1.15, B=17, %75376437  
D=6.820, QC=0.2187, FS=9.6, U=44.1, TA=1.15, B=16, %75377640  
D=6.840, QC=0.2150, FS=9.5, U=44.2, TA=1.15, B=17, %75378750

D=6.860, QC=0.2140, FS=9.4, U=44.3, TA=1.15, B=17, %75379859  
D=6.880, QC=0.2119, FS=9.4, U=44.6, TA=1.15, B=17, %75380984  
D=6.900, QC=0.2067, FS=9.3, U=44.7, TA=1.15, B=17, %75382093  
D=6.920, QC=0.2062, FS=9.1, U=44.8, TA=1.15, B=17, %75383640  
D=6.940, QC=0.2088, FS=9.5, U=45.0, TA=1.15, B=18, %75384734  
D=6.960, QC=0.2119, FS=9.5, U=45.2, TA=1.15, B=17, %75385875  
D=6.980, QC=0.2140, FS=9.6, U=45.3, TA=1.15, B=17, %75386984  
D=7.000, QC=0.2135, FS=9.6, U=45.4, TA=1.16, B=16, %75388078  
D=7.020, QC=0.2109, FS=9.6, U=45.6, TA=1.15, B=17, %75389203  
D=7.040, QC=0.2119, FS=9.5, U=45.8, TA=1.16, B=16, %75390296  
D=7.060, QC=0.2119, FS=9.4, U=46.0, TA=1.16, B=17, %75391421  
D=7.080, QC=0.2166, FS=9.3, U=46.0, TA=1.15, B=17, %75392546  
D=7.100, QC=0.2187, FS=9.3, U=46.3, TA=1.15, B=16, %75393687  
D=7.120, QC=0.2228, FS=9.5, U=46.5, TA=1.16, B=16, %75395234  
D=7.140, QC=0.2213, FS=9.4, U=46.6, TA=1.19, B=16, %75396375  
D=7.160, QC=0.2208, FS=9.6, U=46.7, TA=1.18, B=16, %75397484  
D=7.180, QC=0.2182, FS=9.6, U=46.8, TA=1.19, B=17, %75398593  
D=7.200, QC=0.2176, FS=9.7, U=47.0, TA=1.20, B=16, %75399687  
D=7.220, QC=0.2156, FS=9.7, U=47.2, TA=1.19, B=16, %75401250  
D=7.240, QC=0.2327, FS=9.6, U=47.3, TA=1.19, B=16, %75402406 , F=13  
D=7.260, QC=0.4212, FS=16.7, U=54.0, TA=1.15, B=20, %75447562  
D=7.280, QC=0.4212, FS=16.7, U=54.0, TA=1.15, B=20, %75447562  
D=7.300, QC=0.5293, FS=27.3, U=55.7, TA=1.15, B=22, %75448359  
D=7.320, QC=0.5646, FS=31.3, U=57.0, TA=1.15, B=21, %75449156  
D=7.340, QC=0.4929, FS=30.8, U=56.9, TA=1.15, B=21, %75450265  
D=7.360, QC=0.4794, FS=28.5, U=56.7, TA=1.15, B=21, %75450921  
D=7.380, QC=0.4997, FS=28.4, U=56.8, TA=1.15, B=23, %75451703  
D=7.400, QC=0.4857, FS=24.7, U=56.6, TA=1.15, B=22, %75452843  
D=7.420, QC=0.4462, FS=16.6, U=55.3, TA=1.15, B=22, %75453625  
D=7.440, QC=0.3496, FS=8.7, U=53.5, TA=1.15, B=22, %75454765  
D=7.460, QC=0.2929, FS=7.6, U=52.7, TA=1.15, B=23, %75455453  
D=7.480, QC=0.3096, FS=9.2, U=52.6, TA=1.15, B=22, %75456218  
D=7.500, QC=0.3490, FS=8.9, U=52.7, TA=1.15, B=22, %75457359  
D=7.520, QC=0.3506, FS=7.5, U=52.9, TA=1.15, B=21, %75458156  
D=7.540, QC=0.2800, FS=7.1, U=52.9, TA=1.15, B=23, %75459265  
D=7.560, QC=0.3584, FS=8.8, U=52.9, TA=1.15, B=21, %75460031  
D=7.580, QC=0.5428, FS=11.8, U=53.2, TA=1.19, B=22, %75460703  
D=7.600, QC=0.7718, FS=35.8, U=59.7, TA=1.22, B=21, %75461828  
D=7.620, QC=0.9687, FS=37.4, U=60.4, TA=1.25, B=22, %75462593  
D=7.640, QC=0.9391, FS=37.3, U=60.6, TA=1.25, B=21, %75463734  
D=7.660, QC=0.6295, FS=35.2, U=60.5, TA=1.25, B=22, %75464515  
D=7.680, QC=0.4373, FS=18.8, U=58.9, TA=1.25, B=22, %75465640  
D=7.700, QC=0.3994, FS=11.5, U=57.0, TA=1.25, B=23, %75466296  
D=7.720, QC=0.3906, FS=10.4, U=55.9, TA=1.24, B=22, %75467093  
D=7.740, QC=0.4602, FS=16.7, U=56.8, TA=1.23, B=24, %75467890  
D=7.760, QC=0.4638, FS=18.4, U=57.2, TA=1.22, B=22, %75469000  
D=7.780, QC=0.4057, FS=15.1, U=56.7, TA=1.21, B=23, %75469765  
D=7.800, QC=0.3376, FS=12.3, U=55.2, TA=1.21, B=24, %75470531  
D=7.820, QC=0.2618, FS=10.7, U=54.1, TA=1.21, B=24, %75471187  
D=7.840, QC=0.2374, FS=5.5, U=53.7, TA=1.21, B=24, %75472390

D=7.860, QC=0.2452, FS=5.2, U=53.8, TA=1.22, B=25, %75473062  
D=7.880, QC=0.2872, FS=5.4, U=53.9, TA=1.21, B=24, %75473828  
D=7.900, QC=0.3532, FS=6.3, U=54.0, TA=1.21, B=25, %75474609  
D=7.920, QC=0.4431, FS=8.5, U=54.4, TA=1.21, B=23, %75475390  
D=7.940, QC=0.4436, FS=9.4, U=54.8, TA=1.21, B=24, %75476500  
D=7.960, QC=0.4420, FS=11.3, U=54.7, TA=1.21, B=24, %75477281  
D=7.980, QC=0.4135, FS=11.4, U=55.0, TA=1.21, B=25, %75477937  
D=8.000, QC=0.3563, FS=9.7, U=54.4, TA=1.21, B=23, %75478718  
D=8.020, QC=0.3137, FS=8.1, U=54.4, TA=1.21, B=25, %75479843  
D=8.040, QC=0.3096, FS=8.0, U=54.4, TA=1.21, B=24, %75480640  
D=8.060, QC=0.3522, FS=8.5, U=54.5, TA=1.21, B=24, %75481328  
D=8.080, QC=0.4161, FS=10.3, U=55.0, TA=1.21, B=23, %75482125  
D=8.100, QC=0.4384, FS=10.5, U=55.0, TA=1.21, B=24, %75482890  
D=8.120, QC=0.3761, FS=9.0, U=54.9, TA=1.21, B=23, %75484015  
D=8.140, QC=0.4025, FS=9.2, U=54.7, TA=1.21, B=25, %75484781  
D=8.160, QC=0.5449, FS=14.7, U=55.5, TA=1.21, B=23, %75485437  
D=8.180, QC=0.7028, FS=32.9, U=60.1, TA=1.21, B=23, %75486203  
D=8.200, QC=0.4992, FS=22.5, U=60.9, TA=1.21, B=23, %75487312  
D=8.220, QC=0.4166, FS=12.6, U=58.2, TA=1.21, B=24, %75488109  
D=8.240, QC=0.3755, FS=10.5, U=56.3, TA=1.21, B=22, %75488875  
D=8.260, QC=0.3049, FS=10.7, U=55.8, TA=1.21, B=24, %75489640  
D=8.280, QC=0.2888, FS=8.6, U=55.8, TA=1.21, B=23, %75490750  
D=8.300, QC=0.4831, FS=8.8, U=55.7, TA=1.21, B=23, %75491515  
D=8.320, QC=0.7422, FS=29.1, U=60.2, TA=1.21, B=23, %75492281  
D=8.340, QC=0.9931, FS=37.1, U=64.9, TA=1.21, B=24, %75493375  
D=8.360, QC=0.7204, FS=31.6, U=64.5, TA=1.21, B=22, %75494156  
D=8.380, QC=0.5059, FS=23.9, U=63.8, TA=1.21, B=23, %75494843  
D=8.400, QC=0.3885, FS=12.3, U=60.5, TA=1.21, B=22, %75495968  
D=8.420, QC=0.3059, FS=12.3, U=58.1, TA=1.21, B=22, %75496734  
D=8.440, QC=0.2722, FS=13.8, U=57.4, TA=1.21, B=22, %75497531  
D=8.460, QC=0.2597, FS=15.8, U=57.3, TA=1.21, B=22, %75498625  
D=8.480, QC=0.2727, FS=18.4, U=68.4, TA=1.21, B=20, %75567312  
D=8.500, QC=0.2727, FS=18.4, U=68.4, TA=1.21, B=20, %75567312  
D=8.520, QC=0.2867, FS=18.4, U=68.4, TA=1.24, B=19, %75567765  
D=8.540, QC=0.2815, FS=15.4, U=68.2, TA=1.24, B=19, %75568828  
D=8.560, QC=0.2784, FS=13.3, U=68.4, TA=1.24, B=20, %75569640  
D=8.580, QC=0.2924, FS=9.2, U=68.6, TA=1.26, B=20, %75570656  
D=8.600, QC=0.2929, FS=7.8, U=68.7, TA=1.25, B=22, %75571437  
D=8.620, QC=0.3028, FS=7.3, U=69.0, TA=1.24, B=20, %75572546  
D=8.640, QC=0.2976, FS=7.9, U=69.1, TA=1.25, B=21, %75573359  
D=8.660, QC=0.2909, FS=8.3, U=69.2, TA=1.24, B=22, %75574453  
D=8.680, QC=0.2950, FS=8.1, U=67.1, TA=1.24, B=22, %75575234  
D=8.700, QC=0.3070, FS=8.3, U=69.7, TA=1.24, B=21, %75576328  
D=8.720, QC=0.3205, FS=8.6, U=69.9, TA=1.24, B=20, %75577109  
D=8.740, QC=0.4633, FS=9.8, U=67.8, TA=1.24, B=21, %75578203  
D=8.760, QC=0.5469, FS=12.3, U=68.5, TA=1.23, B=21, %75578968  
D=8.780, QC=0.9900, FS=42.0, U=81.7, TA=1.25, B=21, %75580093  
D=8.800, QC=1.4081, FS=43.7, U=79.6, TA=1.25, B=19, %75580875  
D=8.820, QC=0.8425, FS=39.0, U=80.2, TA=1.24, B=20, %75582015  
D=8.840, QC=0.5137, FS=36.3, U=81.7, TA=1.24, B=22, %75582687

D=8.860, QC=0.4083, FS=26.7, U=76.9, TA=1.24, B=21, %75583812  
D=8.880, QC=0.3787, FS=22.0, U=70.8, TA=1.24, B=20, %75584593  
D=8.900, QC=0.3496, FS=22.7, U=72.1, TA=1.24, B=21, %75585750  
D=8.920, QC=0.3350, FS=22.4, U=72.2, TA=1.24, B=22, %75586437  
D=8.940, QC=0.3298, FS=19.4, U=72.4, TA=1.24, B=22, %75587546  
D=8.960, QC=0.3522, FS=18.2, U=70.4, TA=1.24, B=22, %75588343  
D=8.980, QC=0.3735, FS=16.2, U=72.8, TA=1.24, B=21, %75589125  
D=9.000, QC=0.4477, FS=11.9, U=73.1, TA=1.24, B=23, %75590218  
D=9.020, QC=0.4664, FS=13.8, U=74.1, TA=1.24, B=22, %75591015  
D=9.040, QC=0.4368, FS=11.3, U=73.9, TA=1.24, B=22, %75592109  
D=9.060, QC=0.3527, FS=12.7, U=73.7, TA=1.24, B=22, %75592781  
D=9.080, QC=0.3200, FS=12.8, U=73.6, TA=1.24, B=23, %75593578  
D=9.100, QC=0.3298, FS=14.0, U=73.7, TA=1.24, B=22, %75594343  
D=9.120, QC=0.5303, FS=22.4, U=75.2, TA=1.24, B=22, %75595468  
D=9.140, QC=0.7947, FS=41.6, U=81.4, TA=1.24, B=22, %75596250  
D=9.160, QC=1.0425, FS=45.3, U=84.8, TA=1.24, B=22, %75596921  
D=9.180, QC=1.1209, FS=44.8, U=85.6, TA=1.24, B=22, %75598062  
D=9.200, QC=0.8679, FS=39.2, U=85.1, TA=1.25, B=21, %75598843  
D=9.220, QC=0.5412, FS=38.9, U=85.0, TA=1.23, B=21, %75599984  
D=9.240, QC=0.4441, FS=37.5, U=84.8, TA=1.22, B=23, %75600750  
D=9.260, QC=0.4150, FS=31.2, U=82.7, TA=1.22, B=22, %75601515  
D=9.280, QC=0.4399, FS=37.0, U=80.4, TA=1.21, B=22, %75602609  
D=9.300, QC=0.5433, FS=46.0, U=83.2, TA=1.21, B=22, %75603281  
D=9.320, QC=0.6851, FS=47.7, U=82.3, TA=1.21, B=23, %75604078  
D=9.340, QC=0.4415, FS=36.0, U=83.7, TA=1.21, B=23, %75605203  
D=9.360, QC=0.4015, FS=24.9, U=80.8, TA=1.23, B=22, %75605984  
D=9.380, QC=0.3771, FS=18.4, U=77.8, TA=1.27, B=22, %75606765  
D=9.400, QC=0.3480, FS=14.8, U=75.8, TA=1.25, B=23, %75607796  
D=9.420, QC=0.3381, FS=14.1, U=75.6, TA=1.29, B=23, %75608562  
D=9.440, QC=0.3226, FS=13.6, U=75.5, TA=1.30, B=22, %75609343  
D=9.460, QC=0.3288, FS=12.9, U=75.4, TA=1.30, B=23, %75610453  
D=9.480, QC=0.3355, FS=12.6, U=75.5, TA=1.32, B=23, %75611218  
D=9.500, QC=0.3459, FS=10.1, U=75.6, TA=1.31, B=22, %75611984  
D=9.520, QC=0.3392, FS=9.5, U=75.6, TA=1.32, B=22, %75613125  
D=9.540, QC=0.3413, FS=9.6, U=75.8, TA=1.32, B=22, %75613781  
D=9.560, QC=0.3501, FS=9.5, U=75.9, TA=1.31, B=24, %75614546  
D=9.580, QC=0.3433, FS=9.9, U=76.0, TA=1.32, B=23, %75615750  
D=9.600, QC=0.3371, FS=9.8, U=76.2, TA=1.32, B=21, %75616406  
D=9.620, QC=0.3361, FS=10.0, U=76.2, TA=1.32, B=20, %75617203  
D=9.640, QC=0.3329, FS=9.5, U=74.1, TA=1.32, B=21, %75618312  
D=9.660, QC=0.3278, FS=9.1, U=74.1, TA=1.32, B=21, %75619109  
D=9.680, QC=0.3189, FS=8.6, U=76.6, TA=1.32, B=18, %75620265  
D=9.700, QC=0.3127, FS=11.3, U=83.0, TA=1.24, B=23, %75681453  
D=9.720, QC=0.3127, FS=11.3, U=83.0, TA=1.24, B=23, %75681453  
D=9.740, QC=0.3127, FS=11.3, U=83.0, TA=1.24, B=23, %75681453  
D=9.760, QC=0.3111, FS=10.8, U=82.6, TA=1.24, B=22, %75682234  
D=9.780, QC=0.3278, FS=11.3, U=82.7, TA=1.26, B=18, %75683328  
D=9.800, QC=0.3823, FS=11.5, U=82.8, TA=1.26, B=20, %75684109  
D=9.820, QC=0.5231, FS=23.2, U=86.6, TA=1.27, B=18, %75685203  
D=9.840, QC=0.5054, FS=31.9, U=91.1, TA=1.30, B=18, %75686296

D=9.860, QC=0.4586, FS=19.9, U=89.3, TA=1.31, B=19, %75687406  
D=9.880, QC=0.4233, FS=16.0, U=86.3, TA=1.33, B=19, %75688171  
D=9.900, QC=0.3574, FS=15.6, U=84.8, TA=1.35, B=18, %75689265  
D=9.920, QC=0.3574, FS=15.6, U=84.4, TA=1.35, B=18, %75690500  
D=9.940, QC=0.3532, FS=15.2, U=84.4, TA=1.36, B=19, %75691609  
D=9.960, QC=0.3480, FS=14.8, U=84.4, TA=1.35, B=19, %75692281  
D=9.980, QC=0.3423, FS=14.0, U=84.4, TA=1.34, B=19, %75693484  
D=10.000, QC=0.3303, FS=13.5, U=84.4, TA=1.34, B=18, %75694593  
D=10.020, QC=0.3298, FS=8.0, U=84.5, TA=1.34, B=19, %75695687  
D=10.040, QC=0.3361, FS=7.4, U=84.6, TA=1.32, B=20, %75696796  
D=10.060, QC=0.3345, FS=7.3, U=84.7, TA=1.33, B=19, %75697578  
D=10.080, QC=0.3241, FS=8.6, U=84.8, TA=1.33, B=18, %75698687  
D=10.100, QC=0.3262, FS=9.0, U=85.0, TA=1.33, B=20, %75699812  
D=10.120, QC=0.3314, FS=9.1, U=85.1, TA=1.32, B=20, %75700593  
D=10.140, QC=0.3350, FS=9.2, U=85.2, TA=1.32, B=20, %75701703  
D=10.160, QC=0.3303, FS=9.0, U=85.4, TA=1.32, B=20, %75702796  
D=10.180, QC=0.3272, FS=8.5, U=85.4, TA=1.32, B=21, %75703562  
D=10.200, QC=0.3257, FS=8.2, U=85.6, TA=1.32, B=21, %75704656  
D=10.220, QC=0.3257, FS=8.4, U=85.8, TA=1.32, B=21, %75705468  
D=10.240, QC=0.3324, FS=9.2, U=85.9, TA=1.32, B=21, %75706593  
D=10.260, QC=0.3402, FS=9.9, U=86.1, TA=1.32, B=21, %75707265  
D=10.280, QC=0.3459, FS=10.0, U=86.2, TA=1.32, B=22, %75708031  
D=10.300, QC=0.3335, FS=10.9, U=86.4, TA=1.32, B=21, %75709140  
D=10.320, QC=0.3340, FS=11.1, U=86.6, TA=1.32, B=21, %75709906  
D=10.340, QC=0.3636, FS=11.4, U=86.7, TA=1.32, B=21, %75711015  
D=10.360, QC=0.3698, FS=11.6, U=86.7, TA=1.32, B=22, %75711796  
D=10.380, QC=0.3615, FS=11.4, U=86.9, TA=1.32, B=22, %75712578  
D=10.400, QC=0.3797, FS=10.9, U=89.3, TA=1.32, B=21, %75713687  
D=10.420, QC=0.3600, FS=11.3, U=89.4, TA=1.32, B=21, %75714468  
D=10.440, QC=0.3319, FS=10.5, U=87.3, TA=1.32, B=22, %75715593  
D=10.460, QC=0.3314, FS=10.2, U=87.4, TA=1.32, B=21, %75716359  
D=10.480, QC=0.3314, FS=9.6, U=87.7, TA=1.32, B=21, %75717468  
D=10.500, QC=0.3355, FS=9.4, U=87.8, TA=1.32, B=21, %75718265  
D=10.520, QC=0.3413, FS=9.1, U=88.0, TA=1.32, B=23, %75718921  
D=10.540, QC=0.3485, FS=9.0, U=88.1, TA=1.32, B=21, %75720062  
D=10.560, QC=0.3485, FS=9.6, U=88.3, TA=1.32, B=21, %75720843  
D=10.580, QC=0.3490, FS=10.1, U=88.5, TA=1.32, B=21, %75721953  
D=10.600, QC=0.3511, FS=10.7, U=88.6, TA=1.32, B=21, %75722750  
D=10.620, QC=0.3402, FS=11.4, U=88.8, TA=1.32, B=22, %75723875  
D=10.640, QC=0.3418, FS=12.1, U=89.0, TA=1.32, B=21, %75724546  
D=10.660, QC=0.3381, FS=12.8, U=89.3, TA=1.32, B=22, %75725640  
D=10.680, QC=0.3309, FS=12.7, U=89.4, TA=1.32, B=22, %75726406  
D=10.700, QC=0.3309, FS=12.2, U=89.5, TA=1.32, B=21, %75727171  
D=10.720, QC=0.3283, FS=12.4, U=89.6, TA=1.32, B=21, %75728281  
D=10.740, QC=0.3402, FS=11.9, U=89.7, TA=1.32, B=21, %75729078  
D=10.760, QC=0.3428, FS=11.4, U=90.0, TA=1.32, B=23, %75730171  
D=10.780, QC=0.3449, FS=11.3, U=90.1, TA=1.32, B=20, %75730937  
D=10.800, QC=0.3361, FS=11.4, U=90.2, TA=1.32, B=20, %75732031  
D=10.820, QC=0.3236, FS=11.7, U=90.4, TA=1.32, B=20, %75732828  
D=10.840, QC=0.3220, FS=10.9, U=90.6, TA=1.32, B=22, %75733968

D=10.860, QC=0.3257, FS=10.6, U=90.8, TA=1.32, B=24, %75734671  
D=10.880, QC=0.3303, FS=10.0, U=90.9, TA=1.32, B=23, %75735453  
D=10.900, QC=0.3376, FS=11.0, U=97.3, TA=1.35, B=19, %75785562  
D=10.920, QC=0.3376, FS=11.0, U=97.3, TA=1.35, B=19, %75785562  
D=10.940, QC=0.3392, FS=11.0, U=97.3, TA=1.32, B=17, %75786000  
D=10.960, QC=0.3407, FS=11.5, U=99.3, TA=1.32, B=17, %75787109  
D=10.980, QC=0.3439, FS=11.9, U=97.2, TA=1.32, B=17, %75788234  
D=11.000, QC=0.3454, FS=12.8, U=97.4, TA=1.32, B=17, %75789328  
D=11.020, QC=0.3480, FS=13.0, U=97.7, TA=1.32, B=17, %75790906  
D=11.040, QC=0.3501, FS=13.1, U=100.1, TA=1.32, B=17, %75792031  
D=11.060, QC=0.3527, FS=13.7, U=98.2, TA=1.32, B=16, %75793125  
D=11.080, QC=0.3485, FS=13.7, U=98.3, TA=1.32, B=17, %75794250  
D=11.100, QC=0.3480, FS=13.8, U=100.8, TA=1.32, B=16, %75795359  
D=11.120, QC=0.3470, FS=13.5, U=98.9, TA=1.32, B=16, %75796828  
D=11.140, QC=0.3490, FS=13.5, U=99.1, TA=1.32, B=16, %75797937  
D=11.160, QC=0.3490, FS=13.4, U=101.6, TA=1.32, B=16, %75799062  
D=11.180, QC=0.3454, FS=13.5, U=99.5, TA=1.32, B=16, %75800171  
D=11.200, QC=0.3475, FS=13.2, U=102.0, TA=1.32, B=18, %75801375  
D=11.220, QC=0.3516, FS=13.2, U=99.9, TA=1.32, B=16, %75802484  
D=11.240, QC=0.3600, FS=13.5, U=102.4, TA=1.32, B=17, %75803593  
D=11.260, QC=0.3527, FS=13.4, U=100.5, TA=1.32, B=17, %75805125  
D=11.280, QC=0.3501, FS=13.3, U=100.6, TA=1.32, B=18, %75805812  
D=11.300, QC=0.3589, FS=13.2, U=103.1, TA=1.32, B=17, %75807015  
D=11.320, QC=0.3605, FS=13.4, U=101.2, TA=1.33, B=18, %75808140  
D=11.340, QC=0.3584, FS=13.3, U=103.6, TA=1.32, B=17, %75809250  
D=11.360, QC=0.3527, FS=12.8, U=101.6, TA=1.32, B=18, %75810359  
D=11.380, QC=0.3480, FS=12.8, U=101.7, TA=1.32, B=18, %75811468  
D=11.400, QC=0.3485, FS=13.3, U=104.3, TA=1.32, B=19, %75812562  
D=11.420, QC=0.3626, FS=13.5, U=102.2, TA=1.32, B=17, %75813687  
D=11.440, QC=0.3709, FS=13.6, U=102.4, TA=1.32, B=19, %75814796  
D=11.460, QC=0.3626, FS=13.7, U=104.8, TA=1.33, B=18, %75815953  
D=11.480, QC=0.3496, FS=14.0, U=102.6, TA=1.32, B=19, %75816750  
D=11.500, QC=0.3475, FS=13.5, U=102.9, TA=1.33, B=18, %75817859  
D=11.520, QC=0.3423, FS=13.1, U=105.3, TA=1.32, B=18, %75819000  
D=11.540, QC=0.3506, FS=11.8, U=103.3, TA=1.33, B=19, %75820093  
D=11.560, QC=0.3475, FS=11.6, U=103.5, TA=1.33, B=19, %75821218  
D=11.580, QC=0.3522, FS=10.0, U=106.0, TA=1.33, B=18, %75822328  
D=11.600, QC=0.3542, FS=9.6, U=104.0, TA=1.33, B=18, %75823437  
D=11.620, QC=0.3594, FS=9.4, U=104.3, TA=1.33, B=18, %75824562  
D=11.640, QC=0.3631, FS=9.7, U=104.6, TA=1.33, B=18, %75825359  
D=11.660, QC=0.3724, FS=10.2, U=104.7, TA=1.33, B=18, %75826484  
D=11.680, QC=0.3823, FS=11.2, U=105.0, TA=1.33, B=18, %75827625  
D=11.700, QC=0.3766, FS=11.6, U=107.4, TA=1.33, B=18, %75828718  
D=11.720, QC=0.3740, FS=13.0, U=105.6, TA=1.33, B=19, %75829812  
D=11.740, QC=0.3709, FS=13.6, U=105.7, TA=1.33, B=18, %75830937  
D=11.760, QC=0.3714, FS=14.4, U=106.1, TA=1.33, B=19, %75832140  
D=11.780, QC=0.3714, FS=14.7, U=106.3, TA=1.33, B=19, %75832812  
D=11.800, QC=0.3703, FS=14.9, U=106.5, TA=1.33, B=19, %75833921  
D=11.820, QC=0.3693, FS=15.1, U=106.7, TA=1.33, B=18, %75835140  
D=11.840, QC=0.3698, FS=15.0, U=106.9, TA=1.33, B=19, %75836265



D=11.860, QC=0.3698, FS=14.7, U=107.3, TA=1.33, B=18, %75837359  
D=11.880, QC=0.3651, FS=14.7, U=107.4, TA=1.33, B=18, %75838468  
D=11.900, QC=0.3651, FS=14.6, U=107.7, TA=1.33, B=18, %75839593  
D=11.920, QC=0.3641, FS=14.4, U=107.9, TA=1.33, B=18, %75840359  
D=11.940, QC=0.3641, FS=14.3, U=108.0, TA=1.33, B=18, %75841453  
D=11.960, QC=0.3651, FS=14.3, U=110.6, TA=1.33, B=18, %75842578  
D=11.980, QC=0.3600, FS=14.1, U=108.4, TA=1.33, B=17, %75843687  
D=12.000, QC=0.3636, FS=13.3, U=108.8, TA=1.33, B=18, %75844906  
D=12.020, QC=0.3698, FS=12.7, U=111.3, TA=1.33, B=18, %75846015  
D=12.040, QC=0.3776, FS=10.2, U=109.3, TA=1.33, B=19, %75847109 , F=11  
D=12.060, QC=0.3283, FS=9.1, U=119.0, TA=1.41, B=6, %75893125  
D=12.080, QC=0.3283, FS=10.3, U=118.7, TA=1.41, B=12, %75893468  
D=12.100, QC=0.3916, FS=12.3, U=118.8, TA=1.37, B=16, %75894578  
D=12.120, QC=0.3942, FS=12.7, U=119.2, TA=1.34, B=21, %75895703  
D=12.140, QC=0.3922, FS=12.5, U=119.4, TA=1.35, B=17, %75896812  
D=12.160, QC=0.3885, FS=12.6, U=119.8, TA=1.34, B=13, %75898015  
D=12.180, QC=0.3932, FS=13.9, U=120.1, TA=1.34, B=16, %75899453  
D=12.200, QC=0.3854, FS=14.2, U=120.3, TA=1.35, B=20, %75900562  
D=12.220, QC=0.3812, FS=14.4, U=120.4, TA=1.37, B=18, %75901343  
D=12.240, QC=0.3766, FS=14.7, U=120.8, TA=1.37, B=18, %75902453  
D=12.260, QC=0.3740, FS=14.9, U=120.9, TA=1.38, B=18, %75903562  
D=12.280, QC=0.3735, FS=15.0, U=121.2, TA=1.37, B=18, %75904671  
D=12.300, QC=0.3787, FS=14.6, U=121.4, TA=1.41, B=18, %75905921  
D=12.320, QC=0.3812, FS=14.5, U=121.8, TA=1.40, B=19, %75906953  
D=12.340, QC=0.3797, FS=14.5, U=122.0, TA=1.38, B=17, %75908062  
D=12.360, QC=0.3781, FS=14.1, U=122.3, TA=1.40, B=18, %75909265  
D=12.380, QC=0.3797, FS=13.5, U=122.5, TA=1.41, B=17, %75910406  
D=12.400, QC=0.3812, FS=12.8, U=122.9, TA=1.42, B=18, %75911500  
D=12.420, QC=0.3833, FS=12.9, U=123.1, TA=1.41, B=17, %75912609  
D=12.440, QC=0.3859, FS=12.6, U=123.5, TA=1.40, B=18, %75913718  
D=12.460, QC=0.3937, FS=12.6, U=123.8, TA=1.40, B=18, %75914828  
D=12.480, QC=0.3958, FS=13.0, U=124.2, TA=1.40, B=18, %75915953  
D=12.500, QC=0.3968, FS=13.4, U=124.3, TA=1.44, B=18, %75917062  
D=12.520, QC=0.3984, FS=13.8, U=124.5, TA=1.43, B=19, %75917828  
D=12.540, QC=0.3968, FS=14.7, U=124.9, TA=1.45, B=18, %75918921  
D=12.560, QC=0.3994, FS=15.1, U=125.1, TA=1.45, B=19, %75920140  
D=12.580, QC=0.4005, FS=15.8, U=125.5, TA=1.50, B=18, %75921265  
D=12.600, QC=0.3937, FS=15.9, U=125.7, TA=1.51, B=19, %75922375  
D=12.620, QC=0.3885, FS=16.1, U=126.0, TA=1.55, B=19, %75923156  
D=12.640, QC=0.3880, FS=16.2, U=126.3, TA=1.55, B=20, %75924250  
D=12.660, QC=0.4062, FS=16.4, U=126.5, TA=1.54, B=18, %75925375  
D=12.680, QC=0.4571, FS=20.3, U=129.2, TA=1.54, B=19, %75926500  
D=12.700, QC=0.5366, FS=24.8, U=131.4, TA=1.55, B=19, %75927265  
D=12.720, QC=0.5002, FS=25.5, U=134.0, TA=1.58, B=20, %75928359  
D=12.740, QC=0.4888, FS=26.7, U=132.7, TA=1.59, B=19, %75929468  
D=12.760, QC=0.5765, FS=35.5, U=136.5, TA=1.60, B=19, %75930578  
D=12.780, QC=0.5906, FS=41.9, U=141.1, TA=1.56, B=19, %75931375  
D=12.800, QC=0.5256, FS=35.9, U=140.6, TA=1.60, B=20, %75932484  
D=12.820, QC=0.4540, FS=28.9, U=137.3, TA=1.60, B=18, %75933593  
D=12.840, QC=0.4290, FS=19.1, U=129.5, TA=1.62, B=19, %75934734

D=12.860, QC=0.4161, FS=19.6, U=129.0, TA=1.68, B=19, %75935828  
D=12.880, QC=0.4285, FS=17.3, U=129.0, TA=1.68, B=19, %75936625  
D=12.900, QC=0.4358, FS=16.3, U=129.3, TA=1.68, B=19, %75937750  
D=12.920, QC=0.4373, FS=16.7, U=129.5, TA=1.69, B=19, %75938843  
D=12.940, QC=0.4290, FS=13.4, U=129.7, TA=1.70, B=19, %75939968  
D=12.960, QC=0.4264, FS=11.6, U=129.9, TA=1.70, B=20, %75940750  
D=12.980, QC=0.4322, FS=10.4, U=130.0, TA=1.71, B=19, %75941843  
D=13.000, QC=0.4337, FS=9.5, U=130.4, TA=1.70, B=19, %75942968  
D=13.020, QC=0.4337, FS=9.7, U=130.5, TA=1.71, B=19, %75944078  
D=13.040, QC=0.4311, FS=10.0, U=130.7, TA=1.70, B=19, %75944859  
D=13.060, QC=0.4296, FS=10.8, U=131.0, TA=1.71, B=18, %75946000  
D=13.080, QC=0.4254, FS=11.3, U=131.2, TA=1.70, B=19, %75947125  
D=13.100, QC=0.4249, FS=12.5, U=131.6, TA=1.71, B=18, %75948234  
D=13.120, QC=0.4275, FS=12.9, U=131.8, TA=1.71, B=18, %75949343  
D=13.140, QC=0.4285, FS=13.9, U=132.2, TA=1.70, B=18, %75950437  
D=13.160, QC=0.4280, FS=14.5, U=132.4, TA=1.71, B=18, %75951218  
D=13.180, QC=0.4285, FS=14.8, U=132.6, TA=1.70, B=18, %75952375  
D=13.200, QC=0.4280, FS=15.3, U=133.0, TA=1.72, B=18, %75953468  
D=13.220, QC=0.4311, FS=15.2, U=133.3, TA=1.73, B=18, %75954578  
D=13.240, QC=0.4296, FS=15.0, U=133.6, TA=1.72, B=19, %75955687  
D=13.260, QC=0.4259, FS=14.9, U=133.8, TA=1.74, B=19, %75956890  
D=13.280, QC=0.4259, FS=14.9, U=134.1, TA=1.75, B=19, %75957984, NA=-0.0758, NB=-0.8, NC=14.  
1, F=15, K=90, T=The test are ended without any stop in the ground.  
#\$  
0:  
1:  
2:  
3:  
4:  
5:  
6:  
7:  
8:  
9:  
11:Tilt derivative alarm  
12:Point resistance alarm  
13:Depth unchanged for 5 second  
14:Transmission lost  
15:End of test  
16:Dissipation start

**CPT -2**  
**Raw Data**

\$  
HA=1,HB=2,HC=CPTLOG-2.00,HD=8/18/2020,HG=0.792,HP=0.79,HJ=Brenton  
CPT,HK=C2.1,HM=07,HN=3206,HO=0.00,HQ=SA,HR=0°0'0.000"E,HS=0°0'0.000"N,HX=0.00,HY=0.00,HZ=0.00,KQ=1468.00,KF=6200.00,KU=2136.00,MA=0.590,MB=0.011,MC=10.0,MD=150.0,ME=C2.1,MF=0.000

RN=,CA=0,CB=0

#

D=0.000, QC=0.0068, FS=0.0, U=1.1, TA=0.54, B=0, %78018390, NA=5.9935, NB=300.2, NC=445.6

D=0.020, QC=0.0998, FS=1.1, U=0.8, TA=0.52, B=10, %78019562

D=0.040, QC=0.0997, FS=1.3, U=1.0, TA=0.46, B=9, %78021453

D=0.060, QC=0.0977, FS=1.6, U=1.0, TA=0.46, B=13, %78022937

D=0.080, QC=0.0977, FS=1.9, U=1.1, TA=0.54, B=22, %78024031

D=0.100, QC=0.0937, FS=1.9, U=1.2, TA=0.53, B=22, %78024812

D=0.120, QC=0.0967, FS=2.0, U=1.2, TA=0.53, B=22, %78025593

D=0.140, QC=0.0997, FS=2.2, U=1.5, TA=0.53, B=23, %78026625

D=0.160, QC=0.0927, FS=2.2, U=1.5, TA=0.53, B=23, %78027390

D=0.180, QC=0.0937, FS=2.3, U=1.5, TA=0.44, B=23, %78028156

D=0.200, QC=0.0957, FS=2.5, U=1.6, TA=0.52, B=24, %78029250

D=0.220, QC=0.0967, FS=2.4, U=1.7, TA=0.51, B=24, %78030015

D=0.240, QC=0.0967, FS=2.1, U=1.7, TA=0.41, B=21, %78030781

D=0.260, QC=0.0955, FS=2.7, U=1.9, TA=0.49, B=20, %78031875

D=0.280, QC=0.0949, FS=2.7, U=2.0, TA=0.48, B=20, %78032656

D=0.300, QC=0.0973, FS=2.4, U=2.0, TA=0.51, B=20, %78033781

D=0.320, QC=0.0992, FS=2.8, U=2.3, TA=0.48, B=20, %78034890

D=0.340, QC=0.0969, FS=2.5, U=2.3, TA=0.46, B=20, %78035671

D=0.360, QC=0.0997, FS=2.2, U=2.4, TA=0.48, B=19, %78036796

D=0.380, QC=0.0969, FS=2.3, U=2.5, TA=0.52, B=20, %78037578

D=0.400, QC=0.0985, FS=2.4, U=0.4, TA=0.50, B=21, %78038687

D=0.420, QC=0.0982, FS=2.6, U=0.5, TA=0.48, B=22, %78039375

D=0.440, QC=0.0980, FS=2.7, U=5.9, TA=0.30, B=23, %78087734

D=0.460, QC=0.0980, FS=2.7, U=5.9, TA=0.30, B=23, %78087734

D=0.480, QC=0.0964, FS=2.0, U=5.6, TA=0.41, B=25, %78088500

D=0.500, QC=0.0969, FS=2.4, U=5.6, TA=0.41, B=27, %78089296

D=0.520, QC=0.0964, FS=2.6, U=5.7, TA=0.26, B=25, %78090078 , F=11

D=0.540, QC=0.0874, FS=2.8, U=5.7, TA=0.35, B=28, %78091171

D=0.560, QC=0.0874, FS=2.9, U=5.9, TA=0.35, B=29, %78091515

D=0.580, QC=0.0816, FS=2.9, U=5.9, TA=0.32, B=29, %78091859

D=0.600, QC=0.0857, FS=2.6, U=5.9, TA=0.38, B=29, %78092640

D=0.620, QC=0.0893, FS=2.4, U=6.2, TA=0.37, B=21, %78093750

D=0.640, QC=0.0819, FS=2.4, U=6.1, TA=0.32, B=17, %78094859

D=0.660, QC=0.0988, FS=2.2, U=6.4, TA=0.33, B=18, %78096078

D=0.680, QC=0.0947, FS=2.0, U=6.4, TA=0.34, B=18, %78096765

D=0.700, QC=0.0864, FS=1.9, U=6.5, TA=0.34, B=17, %78097906

D=0.720, QC=0.0874, FS=1.5, U=6.7, TA=0.33, B=18, %78099015

D=0.740, QC=0.0836, FS=1.1, U=6.8, TA=0.35, B=18, %78100140

D=0.760, QC=0.0857, FS=1.2, U=7.0, TA=0.34, B=19, %78101250

D=0.780, QC=0.0864, FS=1.2, U=4.9, TA=0.36, B=20, %78102453

D=0.800, QC=0.0874, FS=1.2, U=5.1, TA=0.35, B=19, %78103593

D=0.820, QC=0.0890, FS=1.2, U=5.1, TA=0.34, B=19, %78104343

D=0.840, QC=0.0884, FS=1.3, U=5.2, TA=0.36, B=20, %78105468

D=0.860, QC=0.0869, FS=1.3, U=5.5, TA=0.36, B=20, %78106578  
D=0.880, QC=0.0864, FS=1.3, U=5.6, TA=0.36, B=19, %78107234  
D=0.900, QC=0.0848, FS=1.2, U=5.7, TA=0.36, B=20, %78108437  
D=0.920, QC=0.0869, FS=1.3, U=5.8, TA=0.36, B=21, %78109218  
D=0.940, QC=0.0805, FS=1.3, U=3.8, TA=0.37, B=20, %78110328  
D=0.960, QC=0.0914, FS=1.4, U=6.1, TA=0.36, B=20, %78111453  
D=0.980, QC=0.0956, FS=1.4, U=4.0, TA=0.36, B=20, %78112109  
D=1.000, QC=0.0914, FS=1.4, U=4.2, TA=0.36, B=20, %78113312  
D=1.020, QC=0.0509, FS=1.4, U=4.3, TA=0.37, B=20, %78114078  
D=1.040, QC=0.0587, FS=1.4, U=4.4, TA=0.36, B=20, %78115171  
D=1.060, QC=0.0670, FS=1.3, U=4.7, TA=0.36, B=21, %78116281  
D=1.080, QC=0.0774, FS=1.2, U=4.8, TA=0.36, B=21, %78117062  
D=1.100, QC=0.0847, FS=1.0, U=5.0, TA=0.36, B=21, %78118156  
D=1.120, QC=0.0878, FS=1.2, U=5.1, TA=0.36, B=20, %78118921  
D=1.140, QC=0.0930, FS=1.9, U=5.4, TA=0.36, B=20, %78120046  
D=1.160, QC=0.1028, FS=1.1, U=5.5, TA=0.36, B=20, %78121156  
D=1.180, QC=0.0992, FS=1.4, U=5.6, TA=0.36, B=20, %78121953  
D=1.200, QC=0.0982, FS=1.8, U=5.9, TA=0.36, B=19, %78123046  
D=1.220, QC=0.0914, FS=2.0, U=6.0, TA=0.36, B=20, %78123812  
D=1.240, QC=0.0764, FS=1.9, U=6.1, TA=0.36, B=21, %78124937  
D=1.260, QC=0.0743, FS=1.3, U=6.3, TA=0.36, B=20, %78125703  
D=1.280, QC=0.0815, FS=0.8, U=6.6, TA=0.36, B=20, %78126796  
D=1.300, QC=0.0966, FS=0.9, U=6.7, TA=0.36, B=20, %78127906  
D=1.320, QC=0.0971, FS=0.6, U=6.9, TA=0.36, B=20, %78128671  
D=1.340, QC=0.0878, FS=1.2, U=7.1, TA=0.36, B=20, %78129781  
D=1.360, QC=0.0774, FS=0.4, U=7.3, TA=0.36, B=19, %78130906  
D=1.380, QC=0.0847, FS=1.2, U=7.4, TA=0.36, B=19, %78131687  
D=1.400, QC=0.1013, FS=1.2, U=7.7, TA=0.36, B=20, %78132796  
D=1.420, QC=0.1356, FS=1.2, U=7.9, TA=0.36, B=20, %78133906  
D=1.440, QC=0.1475, FS=1.1, U=8.0, TA=0.36, B=19, %78134687  
D=1.460, QC=0.1621, FS=1.1, U=8.2, TA=0.36, B=19, %78135812  
D=1.480, QC=0.1808, FS=1.4, U=8.4, TA=0.36, B=19, %78136906  
D=1.500, QC=0.1771, FS=1.3, U=8.6, TA=0.36, B=19, %78138015  
D=1.520, QC=0.1636, FS=1.3, U=8.7, TA=0.36, B=18, %78138781  
D=1.540, QC=0.1262, FS=1.5, U=8.9, TA=0.36, B=19, %78139906  
D=1.560, QC=0.1153, FS=1.4, U=9.1, TA=0.36, B=19, %78141000  
D=1.580, QC=0.0992, FS=1.1, U=9.3, TA=0.36, B=18, %78142140  
D=1.600, QC=0.1532, FS=1.2, U=12.3, TA=0.32, B=19, %78184062  
D=1.620, QC=0.1532, FS=1.2, U=12.3, TA=0.32, B=19, %78184062  
D=1.640, QC=0.2161, FS=1.2, U=12.3, TA=0.34, B=18, %78184515  
D=1.660, QC=0.2005, FS=1.2, U=12.0, TA=0.34, B=19, %78185625  
D=1.680, QC=0.1517, FS=1.2, U=12.0, TA=0.34, B=18, %78186734  
D=1.700, QC=0.1283, FS=1.2, U=12.2, TA=0.34, B=19, %78187859  
D=1.720, QC=0.1402, FS=0.6, U=12.3, TA=0.36, B=19, %78188968  
D=1.740, QC=0.1273, FS=1.0, U=12.4, TA=0.35, B=19, %78189734  
D=1.760, QC=0.1148, FS=1.5, U=12.5, TA=0.32, B=18, %78190859  
D=1.780, QC=0.1174, FS=1.7, U=12.6, TA=0.34, B=19, %78191968  
D=1.800, QC=0.1517, FS=2.1, U=12.8, TA=0.36, B=19, %78193093  
D=1.820, QC=0.2244, FS=2.3, U=12.7, TA=0.32, B=19, %78193875  
D=1.840, QC=0.4259, FS=2.8, U=9.9, TA=0.31, B=18, %78194984

D=1.860, QC=0.4794, FS=5.5, U=13.3, TA=0.30, B=19, %78196078  
D=1.880, QC=0.5454, FS=11.0, U=11.5, TA=0.29, B=19, %78197203  
D=1.900, QC=0.5662, FS=25.0, U=16.2, TA=0.30, B=19, %78198312  
D=1.920, QC=0.5875, FS=29.0, U=14.5, TA=0.28, B=18, %78199109  
D=1.940, QC=0.5423, FS=30.1, U=14.4, TA=0.29, B=20, %78200218  
D=1.960, QC=0.4784, FS=20.3, U=9.0, TA=0.30, B=19, %78201328  
D=1.980, QC=0.4436, FS=16.1, U=7.7, TA=0.30, B=20, %78202531  
D=2.000, QC=0.4488, FS=14.3, U=9.5, TA=0.28, B=20, %78203203  
D=2.020, QC=0.4851, FS=25.3, U=10.7, TA=0.30, B=20, %78204328  
D=2.040, QC=0.5755, FS=29.5, U=11.6, TA=0.30, B=20, %78205437  
D=2.060, QC=0.6108, FS=30.0, U=9.7, TA=0.29, B=20, %78206203  
D=2.080, QC=0.5958, FS=25.3, U=10.1, TA=0.30, B=20, %78207406  
D=2.100, QC=0.4851, FS=23.0, U=10.2, TA=0.31, B=19, %78208515  
D=2.120, QC=0.4680, FS=19.3, U=10.0, TA=0.29, B=20, %78209203  
D=2.140, QC=0.4628, FS=18.1, U=9.9, TA=0.30, B=20, %78210406  
D=2.160, QC=0.4701, FS=17.8, U=9.9, TA=0.28, B=20, %78211062  
D=2.180, QC=0.4534, FS=16.1, U=9.7, TA=0.30, B=19, %78212281  
D=2.200, QC=0.4592, FS=15.3, U=9.6, TA=0.29, B=19, %78212953  
D=2.220, QC=0.4680, FS=18.2, U=9.9, TA=0.28, B=21, %78214078  
D=2.240, QC=0.4742, FS=18.7, U=10.1, TA=0.31, B=21, %78214859  
D=2.260, QC=0.4815, FS=19.2, U=10.2, TA=0.30, B=21, %78215953  
D=2.280, QC=0.4758, FS=18.6, U=10.4, TA=0.30, B=20, %78217046  
D=2.300, QC=0.4670, FS=17.5, U=10.4, TA=0.31, B=21, %78217828  
D=2.320, QC=0.4441, FS=14.0, U=10.2, TA=0.29, B=20, %78218953  
D=2.340, QC=0.4311, FS=10.2, U=9.9, TA=0.30, B=21, %78219734  
D=2.360, QC=0.4150, FS=4.2, U=8.4, TA=0.30, B=19, %78220828  
D=2.380, QC=0.3657, FS=4.3, U=8.1, TA=0.30, B=21, %78221953  
D=2.400, QC=0.3122, FS=4.9, U=7.8, TA=0.28, B=21, %78222734  
D=2.420, QC=0.2623, FS=2.2, U=7.5, TA=0.28, B=20, %78223843  
D=2.440, QC=0.2296, FS=2.2, U=7.6, TA=0.28, B=20, %78224625  
D=2.460, QC=0.1818, FS=3.0, U=7.6, TA=0.28, B=21, %78225718  
D=2.480, QC=0.1813, FS=3.2, U=7.7, TA=0.28, B=20, %78226484  
D=2.500, QC=0.2810, FS=10.2, U=8.5, TA=0.29, B=21, %78227625  
D=2.520, QC=1.0305, FS=34.2, U=12.6, TA=0.26, B=19, %78228765  
D=2.540, QC=1.4123, FS=37.6, U=13.6, TA=0.26, B=19, %78229437  
D=2.560, QC=1.6102, FS=39.1, U=14.5, TA=0.27, B=18, %78230640  
D=2.580, QC=1.5775, FS=38.2, U=14.5, TA=0.26, B=19, %78231734  
D=2.600, QC=1.3661, FS=34.8, U=14.6, TA=0.27, B=17, %78232828  
D=2.620, QC=0.9879, FS=32.1, U=14.7, TA=0.29, B=18, %78233937  
D=2.640, QC=0.9396, FS=31.7, U=14.4, TA=0.30, B=18, %78235140  
D=2.660, QC=0.9407, FS=32.3, U=14.4, TA=0.29, B=17, %78236250  
D=2.680, QC=0.8622, FS=33.1, U=14.8, TA=0.32, B=18, %78237375  
D=2.700, QC=0.5682, FS=33.0, U=14.9, TA=0.32, B=18, %78238484  
D=2.720, QC=0.4841, FS=30.9, U=14.4, TA=0.30, B=18, %78239187  
D=2.740, QC=0.4327, FS=19.4, U=13.2, TA=0.31, B=18, %78240375 , F=13  
D=2.760, QC=0.4586, FS=9.5, U=10.4, TA=0.34, B=17, %78282000  
D=2.780, QC=0.4114, FS=10.6, U=9.8, TA=0.31, B=18, %78282781  
D=2.800, QC=0.4332, FS=12.8, U=9.7, TA=0.31, B=17, %78283906  
D=2.820, QC=0.5080, FS=28.8, U=12.6, TA=0.31, B=17, %78285015  
D=2.840, QC=0.6238, FS=35.7, U=14.9, TA=0.31, B=16, %78286109

D=2.860, QC=0.5927, FS=32.5, U=15.5, TA=0.32, B=16, %78287234  
D=2.880, QC=0.4519, FS=26.6, U=15.3, TA=0.33, B=16, %78288437  
D=2.900, QC=0.4161, FS=8.6, U=11.9, TA=0.31, B=16, %78289562  
D=2.920, QC=0.3480, FS=5.6, U=10.6, TA=0.33, B=16, %78291015  
D=2.940, QC=0.2275, FS=5.7, U=10.6, TA=0.33, B=16, %78292125  
D=2.960, QC=0.2021, FS=6.7, U=10.7, TA=0.34, B=16, %78293218  
D=2.980, QC=0.1834, FS=6.6, U=10.7, TA=0.34, B=16, %78294343  
D=3.000, QC=0.2145, FS=6.4, U=10.9, TA=0.34, B=15, %78295890  
D=3.020, QC=0.2467, FS=6.5, U=11.0, TA=0.34, B=16, %78297000  
D=3.040, QC=0.2675, FS=6.2, U=11.1, TA=0.34, B=17, %78298093  
D=3.060, QC=0.2446, FS=4.2, U=11.4, TA=0.34, B=16, %78299250  
D=3.080, QC=0.2067, FS=2.9, U=11.5, TA=0.34, B=17, %78300359  
D=3.100, QC=0.1860, FS=2.6, U=11.7, TA=0.34, B=17, %78301500  
D=3.120, QC=0.1823, FS=2.4, U=11.8, TA=0.34, B=17, %78302609  
D=3.140, QC=0.1901, FS=2.6, U=12.0, TA=0.34, B=18, %78304140  
D=3.160, QC=0.1891, FS=3.3, U=12.3, TA=0.34, B=17, %78305234  
D=3.180, QC=0.2026, FS=3.5, U=12.5, TA=0.34, B=18, %78306343  
D=3.200, QC=0.2135, FS=3.4, U=12.7, TA=0.34, B=18, %78307453  
D=3.220, QC=0.2462, FS=3.4, U=12.8, TA=0.34, B=18, %78308687  
D=3.240, QC=0.2800, FS=3.2, U=12.9, TA=0.34, B=17, %78309343  
D=3.260, QC=0.2955, FS=3.6, U=12.9, TA=0.34, B=19, %78310562  
D=3.280, QC=0.2400, FS=4.6, U=13.1, TA=0.34, B=19, %78311593  
D=3.300, QC=0.2550, FS=5.1, U=13.2, TA=0.34, B=19, %78312703  
D=3.320, QC=0.4924, FS=7.1, U=13.5, TA=0.34, B=18, %78313906  
D=3.340, QC=0.4566, FS=6.4, U=13.9, TA=0.34, B=19, %78315046  
D=3.360, QC=0.4145, FS=5.4, U=13.7, TA=0.34, B=18, %78315718  
D=3.380, QC=0.3080, FS=5.3, U=13.7, TA=0.34, B=18, %78316828  
D=3.400, QC=0.2628, FS=7.9, U=14.0, TA=0.34, B=17, %78318062  
D=3.420, QC=0.2145, FS=8.7, U=14.0, TA=0.34, B=17, %78319171  
D=3.440, QC=0.2067, FS=7.0, U=14.1, TA=0.34, B=18, %78320265  
D=3.460, QC=0.2374, FS=6.6, U=14.2, TA=0.34, B=18, %78321375  
D=3.480, QC=0.2556, FS=6.5, U=14.4, TA=0.34, B=17, %78322515  
D=3.500, QC=0.2743, FS=6.6, U=12.2, TA=0.34, B=17, %78323625  
D=3.520, QC=0.2493, FS=5.5, U=12.4, TA=0.34, B=18, %78324718  
D=3.540, QC=0.2000, FS=4.8, U=12.5, TA=0.34, B=18, %78325828  
D=3.560, QC=0.1958, FS=3.1, U=12.8, TA=0.34, B=18, %78327031  
D=3.580, QC=0.1932, FS=3.0, U=12.8, TA=0.34, B=19, %78328125  
D=3.600, QC=0.1896, FS=3.0, U=12.9, TA=0.34, B=19, %78328890  
D=3.620, QC=0.1880, FS=2.9, U=13.1, TA=0.34, B=19, %78330000  
D=3.640, QC=0.1880, FS=2.7, U=13.2, TA=0.34, B=18, %78331093  
D=3.660, QC=0.1891, FS=2.1, U=13.5, TA=0.34, B=19, %78332203  
D=3.680, QC=0.1901, FS=2.0, U=13.5, TA=0.34, B=19, %78332968  
D=3.700, QC=0.1844, FS=2.2, U=13.6, TA=0.34, B=19, %78334093  
D=3.720, QC=0.1828, FS=2.7, U=11.6, TA=0.34, B=19, %78335218  
D=3.740, QC=0.1802, FS=2.8, U=13.9, TA=0.34, B=19, %78336421  
D=3.760, QC=0.1792, FS=3.0, U=11.7, TA=0.34, B=19, %78337093  
D=3.780, QC=0.1808, FS=3.3, U=11.9, TA=0.34, B=19, %78338234  
D=3.800, QC=0.1865, FS=3.5, U=12.1, TA=0.34, B=18, %78339343  
D=3.820, QC=0.1896, FS=3.5, U=12.3, TA=0.34, B=18, %78340484  
D=3.840, QC=0.1943, FS=3.5, U=12.5, TA=0.34, B=19, %78341609

D=3.860, QC=0.1953, FS=3.4, U=12.5, TA=0.34, B=19, %78342375  
D=3.880, QC=0.1943, FS=3.6, U=12.7, TA=0.34, B=18, %78343484  
D=3.900, QC=0.1979, FS=3.6, U=12.9, TA=0.34, B=18, %78344578  
D=3.920, QC=0.1974, FS=3.8, U=13.2, TA=0.34, B=19, %78345703  
D=3.940, QC=0.1969, FS=3.8, U=13.3, TA=0.34, B=18, %78346937  
D=3.960, QC=0.2000, FS=5.4, U=19.8, TA=0.34, B=26, %78391250  
D=3.980, QC=0.2093, FS=5.4, U=19.8, TA=0.34, B=24, %78391593  
D=4.000, QC=0.2078, FS=5.6, U=19.5, TA=0.34, B=28, %78392390  
D=4.020, QC=0.2062, FS=5.6, U=19.5, TA=0.34, B=28, %78393171  
D=4.040, QC=0.2041, FS=5.5, U=19.6, TA=0.34, B=27, %78393875  
D=4.060, QC=0.2041, FS=5.3, U=19.7, TA=0.34, B=28, %78394328  
D=4.080, QC=0.2057, FS=5.3, U=19.7, TA=0.34, B=27, %78395015  
D=4.100, QC=0.2046, FS=5.3, U=19.8, TA=0.34, B=26, %78395781  
D=4.120, QC=0.2062, FS=5.1, U=20.0, TA=0.34, B=26, %78396546  
D=4.140, QC=0.2062, FS=5.2, U=20.0, TA=0.34, B=26, %78397218  
D=4.160, QC=0.2124, FS=5.4, U=20.2, TA=0.34, B=25, %78398437  
D=4.180, QC=0.2150, FS=5.3, U=20.2, TA=0.34, B=26, %78399125  
D=4.200, QC=0.2192, FS=5.1, U=20.4, TA=0.34, B=25, %78399921  
D=4.220, QC=0.2208, FS=5.0, U=20.6, TA=0.34, B=24, %78400687  
D=4.240, QC=0.2223, FS=5.0, U=20.6, TA=0.34, B=22, %78401375  
D=4.260, QC=0.2213, FS=5.3, U=20.8, TA=0.34, B=22, %78402500  
D=4.280, QC=0.2244, FS=5.3, U=21.0, TA=0.34, B=20, %78403296  
D=4.300, QC=0.2249, FS=5.5, U=21.1, TA=0.34, B=21, %78404406  
D=4.320, QC=0.2182, FS=5.3, U=21.1, TA=0.34, B=22, %78405171  
D=4.340, QC=0.2987, FS=5.2, U=21.3, TA=0.34, B=12, %78406625  
D=4.360, QC=0.4498, FS=6.5, U=21.6, TA=0.34, B=15, %78408156  
D=4.380, QC=0.4415, FS=7.3, U=22.0, TA=0.34, B=15, %78409250  
D=4.400, QC=0.4062, FS=8.3, U=23.4, TA=0.34, B=16, %78410359  
D=4.420, QC=0.2514, FS=6.5, U=22.1, TA=0.34, B=17, %78411937  
D=4.440, QC=0.2156, FS=7.2, U=22.1, TA=0.34, B=15, %78413015  
D=4.460, QC=0.2130, FS=7.0, U=22.3, TA=0.34, B=16, %78414125  
D=4.480, QC=0.2187, FS=7.0, U=22.5, TA=0.34, B=17, %78415265  
D=4.500, QC=0.4550, FS=7.9, U=23.3, TA=0.34, B=16, %78416359  
D=4.520, QC=0.6997, FS=26.1, U=26.9, TA=0.39, B=16, %78417890  
D=4.540, QC=0.7137, FS=22.6, U=23.1, TA=0.42, B=16, %78418984  
D=4.560, QC=0.6394, FS=23.6, U=26.4, TA=0.43, B=16, %78420125  
D=4.580, QC=0.6285, FS=28.8, U=30.2, TA=0.43, B=16, %78421234  
D=4.600, QC=0.4264, FS=6.1, U=25.3, TA=0.43, B=15, %78422796  
D=4.620, QC=0.3490, FS=5.6, U=24.4, TA=0.43, B=16, %78423921  
D=4.640, QC=0.3205, FS=7.3, U=22.2, TA=0.43, B=17, %78425062  
D=4.660, QC=0.2618, FS=10.0, U=22.1, TA=0.43, B=16, %78426187  
D=4.680, QC=0.2415, FS=9.7, U=22.3, TA=0.43, B=16, %78427609  
D=4.700, QC=0.2394, FS=10.2, U=22.5, TA=0.43, B=16, %78428812  
D=4.720, QC=0.2327, FS=11.1, U=22.7, TA=0.43, B=17, %78429921  
D=4.740, QC=0.2317, FS=10.5, U=22.9, TA=0.43, B=16, %78431046  
D=4.760, QC=0.2301, FS=9.5, U=23.1, TA=0.43, B=16, %78432187  
D=4.780, QC=0.2348, FS=9.2, U=23.3, TA=0.43, B=17, %78433281  
D=4.800, QC=0.2613, FS=7.8, U=23.3, TA=0.43, B=19, %78434390  
D=4.820, QC=0.2446, FS=7.3, U=23.7, TA=0.43, B=18, %78435500  
D=4.840, QC=0.2296, FS=7.6, U=23.7, TA=0.43, B=18, %78436703



D=4.860, QC=0.2280, FS=7.3, U=23.9, TA=0.43, B=19, %78437828  
D=4.880, QC=0.4114, FS=9.6, U=24.8, TA=0.43, B=18, %78438937  
D=4.900, QC=0.2426, FS=8.0, U=24.1, TA=0.43, B=18, %78439609  
D=4.920, QC=0.2431, FS=6.9, U=24.3, TA=0.43, B=18, %78440718  
D=4.940, QC=0.2384, FS=6.9, U=24.4, TA=0.43, B=18, %78441953  
D=4.960, QC=0.2379, FS=6.7, U=24.7, TA=0.43, B=18, %78443046  
D=4.980, QC=0.2950, FS=6.9, U=24.7, TA=0.43, B=18, %78444156  
D=5.000, QC=0.2358, FS=8.3, U=25.1, TA=0.43, B=17, %78445250  
D=5.020, QC=0.2140, FS=8.0, U=25.2, TA=0.43, B=18, %78446375  
D=5.040, QC=0.2140, FS=6.8, U=25.4, TA=0.43, B=18, %78447500  
D=5.060, QC=0.2202, FS=6.5, U=25.5, TA=0.43, B=18, %78448625  
D=5.080, QC=0.2249, FS=6.2, U=25.8, TA=0.44, B=17, %78449734  
D=5.100, QC=0.2410, FS=6.0, U=25.9, TA=0.43, B=18, %78450843  
D=5.120, QC=0.2462, FS=5.7, U=26.1, TA=0.43, B=17, %78451984  
D=5.140, QC=0.2509, FS=5.2, U=26.2, TA=0.43, B=18, %78452765  
D=5.160, QC=0.2530, FS=7.6, U=30.7, TA=0.38, B=22, %78508468  
D=5.180, QC=0.2530, FS=7.6, U=30.7, TA=0.38, B=22, %78508468  
D=5.200, QC=0.2524, FS=8.2, U=30.4, TA=0.38, B=23, %78509140  
D=5.220, QC=0.2524, FS=8.5, U=30.5, TA=0.38, B=22, %78509953  
D=5.240, QC=0.2504, FS=8.9, U=30.6, TA=0.38, B=22, %78510671  
D=5.260, QC=0.2524, FS=8.8, U=30.7, TA=0.38, B=22, %78511765  
D=5.280, QC=0.2602, FS=8.2, U=30.8, TA=0.38, B=23, %78512531  
D=5.300, QC=0.2613, FS=8.1, U=30.9, TA=0.38, B=22, %78513312  
D=5.320, QC=0.2644, FS=6.9, U=31.2, TA=0.38, B=22, %78514406  
D=5.340, QC=0.2670, FS=6.5, U=31.3, TA=0.38, B=22, %78515203  
D=5.360, QC=0.2753, FS=6.6, U=31.4, TA=0.38, B=21, %78516296  
D=5.380, QC=0.2815, FS=6.9, U=31.5, TA=0.38, B=20, %78517062  
D=5.400, QC=0.2800, FS=7.0, U=31.7, TA=0.38, B=19, %78518187  
D=5.420, QC=0.2763, FS=7.0, U=31.8, TA=0.41, B=17, %78519281  
D=5.440, QC=0.2774, FS=7.7, U=32.1, TA=0.42, B=18, %78520406  
D=5.460, QC=0.2774, FS=7.8, U=32.2, TA=0.41, B=18, %78521546  
D=5.480, QC=0.2768, FS=8.0, U=32.3, TA=0.44, B=19, %78522328  
D=5.500, QC=0.2800, FS=8.2, U=32.6, TA=0.45, B=19, %78523453  
D=5.520, QC=0.2878, FS=8.4, U=32.7, TA=0.47, B=19, %78524562  
D=5.540, QC=0.2898, FS=8.6, U=33.0, TA=0.47, B=18, %78525687  
D=5.560, QC=0.2929, FS=8.4, U=33.2, TA=0.48, B=19, %78526453  
D=5.580, QC=0.2826, FS=8.4, U=33.4, TA=0.50, B=19, %78527578  
D=5.600, QC=0.2820, FS=8.2, U=33.6, TA=0.49, B=20, %78528687  
D=5.620, QC=0.2779, FS=8.3, U=33.7, TA=0.50, B=19, %78529375  
D=5.640, QC=0.2639, FS=8.3, U=33.8, TA=0.50, B=20, %78530578  
D=5.660, QC=0.2597, FS=8.3, U=33.9, TA=0.50, B=21, %78531343  
D=5.680, QC=0.2597, FS=8.4, U=34.2, TA=0.50, B=21, %78532453  
D=5.700, QC=0.2524, FS=8.4, U=34.3, TA=0.50, B=21, %78533140  
D=5.720, QC=0.2514, FS=8.4, U=34.4, TA=0.50, B=21, %78534343  
D=5.740, QC=0.2488, FS=8.3, U=34.7, TA=0.50, B=20, %78535453  
D=5.760, QC=0.2493, FS=8.0, U=34.8, TA=0.50, B=21, %78536125  
D=5.780, QC=0.2524, FS=7.7, U=34.9, TA=0.50, B=20, %78537328  
D=5.800, QC=0.2535, FS=7.7, U=35.0, TA=0.50, B=18, %78538093  
D=5.820, QC=0.2519, FS=7.6, U=35.3, TA=0.50, B=19, %78539218  
D=5.840, QC=0.2514, FS=7.5, U=35.3, TA=0.50, B=20, %78540328

D=5.860, QC=0.2530, FS=7.1, U=35.6, TA=0.50, B=15, %78541421  
D=5.880, QC=0.2530, FS=7.0, U=35.7, TA=0.50, B=15, %78542531  
D=5.900, QC=0.2519, FS=7.2, U=35.9, TA=0.50, B=18, %78544015  
D=5.920, QC=0.2514, FS=7.2, U=36.1, TA=0.50, B=19, %78544828  
D=5.940, QC=0.2509, FS=6.9, U=36.2, TA=0.50, B=17, %78545890  
D=5.960, QC=0.2488, FS=6.8, U=36.4, TA=0.50, B=15, %78547437  
D=5.980, QC=0.2472, FS=6.8, U=36.6, TA=0.50, B=16, %78548531  
D=6.000, QC=0.2488, FS=6.7, U=36.8, TA=0.50, B=17, %78549625  
D=6.020, QC=0.2524, FS=6.5, U=37.0, TA=0.50, B=16, %78550828  
D=6.040, QC=0.2550, FS=6.3, U=37.2, TA=0.50, B=16, %78552281  
D=6.060, QC=0.2566, FS=6.3, U=37.4, TA=0.50, B=17, %78553421  
D=6.080, QC=0.2545, FS=6.4, U=37.6, TA=0.50, B=18, %78554515  
D=6.100, QC=0.2571, FS=6.4, U=37.7, TA=0.50, B=18, %78555281  
D=6.120, QC=0.2566, FS=6.4, U=37.9, TA=0.50, B=18, %78556375  
D=6.140, QC=0.2540, FS=6.4, U=38.1, TA=0.50, B=18, %78557593  
D=6.160, QC=0.2545, FS=6.3, U=38.2, TA=0.50, B=18, %78558687  
D=6.180, QC=0.2509, FS=6.4, U=38.4, TA=0.50, B=19, %78559796  
D=6.200, QC=0.2514, FS=6.3, U=38.6, TA=0.50, B=18, %78560906  
D=6.220, QC=0.2535, FS=6.2, U=38.8, TA=0.50, B=18, %78562031  
D=6.240, QC=0.2550, FS=6.1, U=38.9, TA=0.50, B=18, %78562796  
D=6.260, QC=0.2566, FS=6.1, U=39.2, TA=0.50, B=18, %78563906  
D=6.280, QC=0.2483, FS=6.1, U=39.2, TA=0.50, B=17, %78565015  
D=6.300, QC=0.2462, FS=6.1, U=39.5, TA=0.51, B=18, %78566234  
D=6.320, QC=0.2379, FS=6.0, U=39.6, TA=0.50, B=18, %78567328  
D=6.340, QC=0.2545, FS=6.4, U=47.3, TA=0.50, B=23, %78613921  
D=6.360, QC=0.2545, FS=6.4, U=47.3, TA=0.50, B=23, %78613921  
D=6.380, QC=0.2706, FS=6.4, U=47.3, TA=0.49, B=22, %78614359  
D=6.400, QC=0.2711, FS=6.5, U=46.9, TA=0.49, B=24, %78615140  
D=6.420, QC=0.2685, FS=6.7, U=47.0, TA=0.49, B=23, %78615859  
D=6.440, QC=0.2685, FS=6.1, U=47.2, TA=0.49, B=25, %78616609  
D=6.460, QC=0.2696, FS=6.3, U=47.3, TA=0.49, B=25, %78617343  
D=6.480, QC=0.2888, FS=6.6, U=47.4, TA=0.49, B=23, %78618468  
D=6.500, QC=0.3091, FS=7.1, U=47.5, TA=0.49, B=26, %78619250  
D=6.520, QC=0.3091, FS=7.3, U=47.5, TA=0.49, B=23, %78620015  
D=6.540, QC=0.2950, FS=7.8, U=47.7, TA=0.49, B=24, %78620671  
D=6.560, QC=0.2810, FS=7.4, U=47.8, TA=0.49, B=24, %78621453  
D=6.580, QC=0.2805, FS=6.2, U=48.0, TA=0.50, B=24, %78622218  
D=6.600, QC=0.2878, FS=5.5, U=48.2, TA=0.49, B=24, %78623312  
D=6.620, QC=0.2826, FS=5.0, U=48.4, TA=0.51, B=25, %78624093  
D=6.640, QC=0.2784, FS=5.2, U=48.4, TA=0.49, B=24, %78624796  
D=6.660, QC=0.2815, FS=5.2, U=48.5, TA=0.49, B=23, %78625578  
D=6.680, QC=0.2909, FS=5.5, U=48.6, TA=0.50, B=24, %78626359  
D=6.700, QC=0.2914, FS=5.3, U=48.7, TA=0.49, B=24, %78627031  
D=6.720, QC=0.2904, FS=6.0, U=49.0, TA=0.49, B=24, %78628156  
D=6.740, QC=0.2805, FS=6.3, U=49.2, TA=0.50, B=26, %78628937  
D=6.760, QC=0.2644, FS=5.8, U=49.4, TA=0.49, B=25, %78629734  
D=6.780, QC=0.2576, FS=5.4, U=49.5, TA=0.49, B=26, %78630406  
D=6.800, QC=0.2607, FS=5.1, U=49.7, TA=0.50, B=26, %78631187  
D=6.820, QC=0.2732, FS=4.5, U=49.9, TA=0.49, B=25, %78631968  
D=6.840, QC=0.2800, FS=4.7, U=50.0, TA=0.50, B=25, %78632750

D=6.860, QC=0.2768, FS=5.0, U=50.1, TA=0.51, B=26, %78633437  
D=6.880, QC=0.2753, FS=5.2, U=50.3, TA=0.51, B=27, %78634187  
D=6.900, QC=0.2794, FS=5.7, U=50.5, TA=0.53, B=26, %78634953  
D=6.920, QC=0.2919, FS=6.4, U=50.7, TA=0.53, B=26, %78635750  
D=6.940, QC=0.3241, FS=7.1, U=50.7, TA=0.53, B=26, %78636421  
D=6.960, QC=0.3433, FS=7.8, U=50.8, TA=0.53, B=27, %78637187  
D=6.980, QC=0.3329, FS=8.9, U=50.9, TA=0.54, B=27, %78637968  
D=7.000, QC=0.3127, FS=8.4, U=51.2, TA=0.52, B=26, %78638750  
D=7.020, QC=0.3059, FS=7.7, U=51.3, TA=0.55, B=26, %78639437  
D=7.040, QC=0.2966, FS=7.4, U=51.5, TA=0.56, B=26, %78640218  
D=7.060, QC=0.3080, FS=7.4, U=51.7, TA=0.57, B=27, %78641000  
D=7.080, QC=0.3433, FS=8.1, U=51.7, TA=0.57, B=25, %78641656  
D=7.100, QC=0.4529, FS=10.7, U=52.2, TA=0.57, B=26, %78642421  
D=7.120, QC=0.5584, FS=16.4, U=54.9, TA=0.57, B=26, %78643187  
D=7.140, QC=0.5054, FS=12.2, U=54.4, TA=0.58, B=26, %78643968  
D=7.160, QC=0.4721, FS=11.3, U=52.8, TA=0.57, B=26, %78644734  
D=7.180, QC=0.4005, FS=10.3, U=52.5, TA=0.57, B=26, %78645468  
D=7.200, QC=0.3506, FS=8.0, U=52.5, TA=0.58, B=27, %78646218  
D=7.220, QC=0.3449, FS=6.5, U=52.6, TA=0.57, B=27, %78647000  
D=7.240, QC=0.3490, FS=6.1, U=52.6, TA=0.60, B=26, %78647671  
D=7.260, QC=0.3418, FS=6.1, U=52.7, TA=0.59, B=29, %78648453  
D=7.280, QC=0.3490, FS=6.4, U=52.9, TA=0.59, B=26, %78649234  
D=7.300, QC=0.4072, FS=8.9, U=53.7, TA=0.57, B=25, %78649921  
D=7.320, QC=0.5921, FS=21.9, U=58.6, TA=0.59, B=25, %78650703  
D=7.340, QC=0.6150, FS=25.4, U=60.5, TA=0.57, B=25, %78651484  
D=7.360, QC=0.5085, FS=19.6, U=59.3, TA=0.58, B=25, %78652156  
D=7.380, QC=0.4514, FS=19.0, U=56.9, TA=0.57, B=26, %78652953  
D=7.400, QC=0.5153, FS=27.3, U=59.8, TA=0.57, B=25, %78653765  
D=7.420, QC=0.6643, FS=38.2, U=63.9, TA=0.59, B=25, %78654781  
D=7.440, QC=0.5651, FS=36.6, U=64.8, TA=0.58, B=24, %78655562  
D=7.460, QC=0.5038, FS=31.2, U=64.1, TA=0.59, B=25, %78656328  
D=7.480, QC=0.4623, FS=25.9, U=62.3, TA=0.59, B=24, %78657093  
D=7.500, QC=0.4420, FS=16.7, U=58.7, TA=0.59, B=24, %78657859  
D=7.520, QC=0.3766, FS=11.0, U=55.8, TA=0.61, B=26, %78658546  
D=7.540, QC=0.3511, FS=14.8, U=55.7, TA=0.61, B=20, %78710171  
D=7.560, QC=0.3511, FS=14.8, U=55.7, TA=0.61, B=20, %78710171  
D=7.580, QC=0.3272, FS=15.2, U=55.5, TA=0.61, B=20, %78711281  
D=7.600, QC=0.3257, FS=13.9, U=55.7, TA=0.61, B=21, %78712484  
D=7.620, QC=0.3381, FS=13.2, U=55.8, TA=0.61, B=19, %78713156  
D=7.640, QC=0.5558, FS=13.4, U=56.3, TA=0.61, B=17, %78714296  
D=7.660, QC=0.5927, FS=37.6, U=66.8, TA=0.61, B=16, %78715390  
D=7.680, QC=0.8352, FS=41.8, U=70.6, TA=0.61, B=16, %78716968  
D=7.700, QC=1.0331, FS=42.2, U=71.0, TA=0.61, B=15, %78718078  
D=7.720, QC=0.9251, FS=41.4, U=70.8, TA=0.61, B=15, %78719625  
D=7.740, QC=0.7028, FS=36.2, U=70.0, TA=0.61, B=15, %78720750  
D=7.760, QC=0.4415, FS=30.0, U=70.9, TA=0.61, B=15, %78721781  
D=7.780, QC=0.4363, FS=15.4, U=63.4, TA=0.61, B=15, %78723359  
D=7.800, QC=0.4363, FS=13.8, U=59.5, TA=0.61, B=15, %78724484  
D=7.820, QC=0.4581, FS=18.5, U=59.3, TA=0.61, B=15, %78725921  
D=7.840, QC=0.5246, FS=22.4, U=60.1, TA=0.61, B=16, %78727031

D=7.860, QC=0.5812, FS=42.7, U=68.3, TA=0.61, B=15, %78728234  
D=7.880, QC=0.8295, FS=45.5, U=70.8, TA=0.61, B=15, %78729687  
D=7.900, QC=1.1204, FS=46.8, U=73.7, TA=0.61, B=15, %78730828  
D=7.920, QC=1.1624, FS=45.1, U=72.1, TA=0.61, B=15, %78732265  
D=7.940, QC=0.8394, FS=41.5, U=70.9, TA=0.61, B=15, %78733484  
D=7.960, QC=0.4919, FS=37.0, U=69.8, TA=0.61, B=15, %78734609  
D=7.980, QC=0.4649, FS=27.4, U=66.8, TA=0.61, B=15, %78736046  
D=8.000, QC=0.4851, FS=35.9, U=66.6, TA=0.61, B=16, %78737171  
D=8.020, QC=0.6669, FS=42.8, U=68.9, TA=0.61, B=16, %78738312  
D=8.040, QC=0.6576, FS=41.3, U=70.4, TA=0.61, B=15, %78739437  
D=8.060, QC=0.4425, FS=33.9, U=70.9, TA=0.61, B=19, %78740531  
D=8.080, QC=0.4249, FS=24.6, U=63.0, TA=0.61, B=17, %78742078  
D=8.100, QC=0.4129, FS=18.3, U=58.9, TA=0.61, B=17, %78743171  
D=8.120, QC=0.4368, FS=17.9, U=58.5, TA=0.61, B=17, %78744281  
D=8.140, QC=0.4597, FS=19.2, U=58.8, TA=0.61, B=17, %78745484  
D=8.160, QC=0.5168, FS=24.7, U=60.3, TA=0.61, B=18, %78746593  
D=8.180, QC=0.5579, FS=41.0, U=67.3, TA=0.61, B=17, %78747687  
D=8.200, QC=0.9277, FS=49.2, U=70.7, TA=0.61, B=16, %78748812  
D=8.220, QC=1.1619, FS=52.0, U=75.0, TA=0.61, B=16, %78749937  
D=8.240, QC=1.3094, FS=52.4, U=74.3, TA=0.61, B=16, %78751046  
D=8.260, QC=1.1650, FS=50.6, U=59.7, TA=0.61, B=15, %78752578  
D=8.280, QC=1.0923, FS=56.1, U=55.1, TA=0.61, B=15, %78753703  
D=8.300, QC=0.9485, FS=54.9, U=49.5, TA=0.61, B=15, %78755171  
D=8.320, QC=0.5116, FS=48.0, U=45.9, TA=0.62, B=16, %78756375  
D=8.340, QC=0.4379, FS=34.3, U=43.8, TA=0.62, B=16, %78757468  
D=8.360, QC=0.4732, FS=28.2, U=42.4, TA=0.64, B=16, %78758578  
D=8.380, QC=0.5018, FS=32.1, U=46.3, TA=0.63, B=16, %78760031  
D=8.400, QC=0.4607, FS=21.0, U=42.3, TA=0.65, B=17, %78761250  
D=8.420, QC=0.4311, FS=17.1, U=42.9, TA=0.68, B=17, %78762359  
D=8.440, QC=0.4212, FS=14.4, U=38.2, TA=0.65, B=16, %78763484  
D=8.460, QC=0.4810, FS=16.6, U=38.2, TA=0.65, B=16, %78764593  
D=8.480, QC=0.5012, FS=28.5, U=41.9, TA=0.68, B=17, %78765703  
D=8.500, QC=0.5282, FS=33.8, U=44.5, TA=0.65, B=16, %78766812  
D=8.520, QC=0.4784, FS=28.2, U=44.4, TA=0.67, B=16, %78768375  
D=8.540, QC=0.4602, FS=20.7, U=44.2, TA=0.70, B=15, %78769468  
D=8.560, QC=0.4493, FS=17.2, U=42.1, TA=0.69, B=15, %78770906  
D=8.580, QC=0.4332, FS=17.1, U=38.9, TA=0.71, B=15, %78772109  
D=8.600, QC=0.4550, FS=19.1, U=39.1, TA=0.72, B=15, %78773125  
D=8.620, QC=0.4483, FS=16.7, U=41.6, TA=0.72, B=15, %78774671  
D=8.640, QC=0.3989, FS=14.8, U=41.2, TA=0.73, B=16, %78775765  
D=8.660, QC=0.3922, FS=14.3, U=38.4, TA=0.73, B=15, %78777296  
D=8.680, QC=0.3974, FS=13.3, U=40.7, TA=0.71, B=15, %78778421  
D=8.700, QC=0.4301, FS=12.0, U=40.9, TA=0.71, B=14, %78779890  
D=8.720, QC=0.4747, FS=12.7, U=41.1, TA=0.74, B=15, %78781093  
D=8.740, QC=0.4618, FS=13.5, U=41.7, TA=0.71, B=14, %78782546  
D=8.760, QC=0.4851, FS=18.9, U=46.5, TA=0.74, B=20, %78847609  
D=8.780, QC=0.4851, FS=18.9, U=46.5, TA=0.74, B=20, %78847609  
D=8.800, QC=0.4202, FS=16.7, U=45.0, TA=0.74, B=15, %78848718  
D=8.820, QC=0.3974, FS=14.6, U=44.7, TA=0.74, B=16, %78849859  
D=8.840, QC=0.3968, FS=13.0, U=44.8, TA=0.74, B=22, %78850984

D=8.860, QC=0.4088, FS=12.3, U=44.9, TA=0.74, B=22, %78851750  
D=8.880, QC=0.3927, FS=12.4, U=44.9, TA=0.74, B=22, %78852531  
D=8.900, QC=0.3802, FS=10.1, U=45.1, TA=0.74, B=22, %78853625  
D=8.920, QC=0.3787, FS=8.4, U=45.2, TA=0.76, B=24, %78854406  
D=8.940, QC=0.3968, FS=7.9, U=45.3, TA=0.79, B=22, %78855109  
D=8.960, QC=0.4612, FS=8.4, U=45.4, TA=0.86, B=23, %78856328  
D=8.980, QC=0.4046, FS=8.5, U=45.6, TA=0.86, B=22, %78856984  
D=9.000, QC=0.4010, FS=9.7, U=45.7, TA=0.85, B=22, %78858125  
D=9.020, QC=0.4155, FS=9.5, U=45.8, TA=0.86, B=22, %78858906  
D=9.040, QC=0.3875, FS=10.2, U=45.9, TA=0.85, B=23, %78859687  
D=9.060, QC=0.3677, FS=11.0, U=46.0, TA=0.87, B=22, %78860796  
D=9.080, QC=0.3724, FS=10.7, U=46.2, TA=0.90, B=23, %78861578  
D=9.100, QC=0.3594, FS=10.7, U=46.2, TA=0.89, B=22, %78862250  
D=9.120, QC=0.3605, FS=8.8, U=46.6, TA=0.95, B=23, %78863359  
D=9.140, QC=0.3989, FS=8.5, U=46.6, TA=0.97, B=21, %78864140  
D=9.160, QC=0.4618, FS=11.7, U=47.3, TA=0.97, B=23, %78864921  
D=9.180, QC=0.4659, FS=12.9, U=48.1, TA=0.97, B=23, %78866062  
D=9.200, QC=0.4212, FS=11.1, U=47.5, TA=0.97, B=24, %78866718  
D=9.220, QC=0.3771, FS=11.3, U=47.3, TA=0.97, B=24, %78867484  
D=9.240, QC=0.3646, FS=10.0, U=47.2, TA=0.97, B=24, %78868265  
D=9.260, QC=0.3792, FS=8.0, U=47.6, TA=0.97, B=24, %78869359  
D=9.280, QC=0.4467, FS=9.7, U=47.9, TA=0.97, B=25, %78870125  
D=9.300, QC=0.5137, FS=10.5, U=48.4, TA=0.97, B=24, %78870890  
D=9.320, QC=0.4753, FS=9.9, U=48.1, TA=0.97, B=24, %78871656  
D=9.340, QC=0.4218, FS=9.7, U=48.0, TA=0.98, B=24, %78872453  
D=9.360, QC=0.3761, FS=8.4, U=48.1, TA=0.97, B=24, %78873125  
D=9.380, QC=0.3615, FS=6.6, U=48.3, TA=0.97, B=25, %78873906  
D=9.400, QC=0.3615, FS=7.1, U=48.4, TA=0.98, B=25, %78875015  
D=9.420, QC=0.3787, FS=7.5, U=48.5, TA=0.98, B=24, %78875781  
D=9.440, QC=0.4093, FS=8.4, U=48.5, TA=0.97, B=26, %78876546  
D=9.460, QC=0.4244, FS=8.8, U=48.8, TA=0.98, B=25, %78877312  
D=9.480, QC=0.4129, FS=8.8, U=48.9, TA=0.98, B=25, %78878078  
D=9.500, QC=0.3838, FS=9.2, U=49.0, TA=0.97, B=25, %78878734  
D=9.520, QC=0.3781, FS=8.3, U=49.1, TA=0.98, B=25, %78879500  
D=9.540, QC=0.3885, FS=8.7, U=49.3, TA=0.98, B=25, %78880265  
D=9.560, QC=0.5132, FS=8.9, U=49.4, TA=0.98, B=25, %78881031  
D=9.580, QC=0.5812, FS=27.2, U=56.3, TA=0.98, B=24, %78882125  
D=9.600, QC=0.5080, FS=15.9, U=54.5, TA=0.98, B=25, %78882890  
D=9.620, QC=0.4696, FS=12.5, U=52.1, TA=0.98, B=25, %78883656  
D=9.640, QC=0.4560, FS=11.4, U=52.2, TA=0.97, B=25, %78884421  
D=9.660, QC=0.4763, FS=8.6, U=51.7, TA=0.98, B=24, %78885125  
D=9.680, QC=0.4218, FS=9.6, U=51.4, TA=0.98, B=25, %78885906  
D=9.700, QC=0.3963, FS=10.8, U=51.3, TA=0.98, B=24, %78886671  
D=9.720, QC=0.3896, FS=12.1, U=51.4, TA=0.98, B=25, %78887437  
D=9.740, QC=0.3792, FS=12.9, U=51.6, TA=0.98, B=24, %78888531  
D=9.760, QC=0.3792, FS=12.1, U=51.7, TA=0.98, B=25, %78889218  
D=9.780, QC=0.3781, FS=11.9, U=51.8, TA=0.98, B=24, %78890000  
D=9.800, QC=0.3761, FS=12.3, U=52.0, TA=0.98, B=25, %78890781  
D=9.820, QC=0.3750, FS=11.5, U=52.1, TA=0.98, B=24, %78891546  
D=9.840, QC=0.3787, FS=11.2, U=52.3, TA=0.98, B=24, %78892312

D=9.860, QC=0.3823, FS=11.3, U=52.6, TA=0.98, B=24, %78893421  
D=9.880, QC=0.3859, FS=11.6, U=52.8, TA=0.98, B=25, %78894203  
D=9.900, QC=0.3854, FS=11.4, U=52.9, TA=0.98, B=23, %78894875  
D=9.920, QC=0.3880, FS=11.2, U=53.1, TA=0.98, B=24, %78895640  
D=9.940, QC=0.3880, FS=11.3, U=53.3, TA=0.98, B=24, %78896750, NA=-0.0052, NB=-1.5, NC=1.0, F  
=15, K=90, T=The test are ended without any stop in the ground.

#\$

0:

1:

2:

3:

4:

5:

6:

7:

8:

9:

11:Tilt derivative alarm

12:Point resistance alarm

13:Depth unchanged for 5 second

14:Transmission lost

15:End of test

16:Dissipation start

**CPT -3**  
**Raw Data**

\$  
HA=1,HB=6,HC=CPTLOG-2.00,HD=8/19/2020,HG=-0.396,HP=-0.40,HJ=Brenton  
CPT,HK=c3.1,HM=07,HN=3206,HO=0.00,HQ=SA,HR=0°0'0.000"E,HS=0°0'0.000"N,HX=0.00,HY=0.00,HZ=0.00,KQ=1468.00,KF=6200.00,KU=2136.00,MA=0.590,MB=0.011,MC=10.0,MD=150.0,ME=c3.1,MF=0.000

RN=,CA=0,CB=0

#

D=0.000, QC=0.0218, FS=2.9, U=0.8, TA=0.22, B=25, %162954015, NA=5.4751, NB=329.6, NC=438.3  
D=0.020, QC=0.0218, FS=2.9, U=0.8, TA=0.22, B=25, %162954015  
D=0.040, QC=0.0218, FS=2.9, U=0.8, TA=0.22, B=25, %162954015  
D=0.060, QC=0.0275, FS=2.9, U=0.8, TA=0.24, B=23, %162954343  
D=0.080, QC=0.0353, FS=3.0, U=1.2, TA=0.23, B=26, %162955109  
D=0.100, QC=0.0312, FS=2.7, U=1.1, TA=0.30, B=31, %162955781  
D=0.120, QC=0.0369, FS=2.5, U=1.1, TA=0.30, B=28, %162956578  
D=0.140, QC=0.0442, FS=2.3, U=1.1, TA=0.23, B=28, %162957296  
D=0.160, QC=0.0452, FS=2.4, U=1.1, TA=0.29, B=29, %162958046  
D=0.180, QC=0.0431, FS=2.6, U=1.1, TA=0.28, B=28, %162958812  
D=0.200, QC=0.0431, FS=2.6, U=1.0, TA=0.29, B=28, %162959625  
D=0.220, QC=0.0483, FS=2.6, U=1.0, TA=0.27, B=27, %162960312  
D=0.240, QC=0.0447, FS=2.4, U=1.0, TA=0.31, B=10, %162961406  
D=0.260, QC=0.0478, FS=3.1, U=1.9, TA=0.27, B=12, %162963281  
D=0.280, QC=0.0942, FS=3.5, U=1.8, TA=0.23, B=17, %162964500  
D=0.300, QC=0.0916, FS=3.5, U=1.8, TA=0.28, B=20, %162965609  
D=0.320, QC=0.0947, FS=3.4, U=3.0, TA=0.27, B=20, %162966296  
D=0.340, QC=0.0942, FS=3.2, U=1.6, TA=0.29, B=20, %162967421  
D=0.360, QC=0.0957, FS=3.0, U=1.5, TA=0.26, B=20, %162968218  
D=0.380, QC=0.0921, FS=3.0, U=1.4, TA=0.30, B=19, %162969359  
D=0.400, QC=0.0900, FS=2.7, U=1.3, TA=0.29, B=20, %162970484  
D=0.420, QC=0.0900, FS=2.7, U=1.2, TA=0.28, B=21, %162971171  
D=0.440, QC=0.0952, FS=2.4, U=2.4, TA=0.29, B=20, %162972390  
D=0.460, QC=0.0990, FS=2.5, U=2.2, TA=0.30, B=19, %162973500  
D=0.480, QC=0.0990, FS=2.3, U=2.2, TA=0.27, B=19, %162974203  
D=0.500, QC=0.0995, FS=2.2, U=2.0, TA=0.28, B=20, %162975375  
D=0.520, QC=0.1095, FS=2.1, U=2.0, TA=0.25, B=20, %162976046  
D=0.540, QC=0.1005, FS=1.8, U=1.7, TA=0.28, B=20, %162977171  
D=0.560, QC=0.1084, FS=1.7, U=1.7, TA=0.24, B=20, %162977968  
D=0.580, QC=0.1084, FS=1.4, U=1.6, TA=0.23, B=22, %162979093  
D=0.600, QC=0.1010, FS=1.3, U=1.6, TA=0.23, B=22, %162979875  
D=0.620, QC=0.1031, FS=1.9, U=1.3, TA=0.17, B=21, %162981000  
D=0.640, QC=0.1078, FS=1.8, U=1.3, TA=0.20, B=21, %162981765  
D=0.660, QC=0.1009, FS=1.8, U=1.7, TA=0.19, B=21, %162982875  
D=0.680, QC=0.1088, FS=1.8, U=1.4, TA=0.17, B=21, %162983546  
D=0.700, QC=0.1014, FS=1.8, U=1.9, TA=0.16, B=21, %162984343  
D=0.720, QC=0.1003, FS=1.0, U=1.7, TA=0.18, B=21, %162985453  
D=0.740, QC=0.1017, FS=1.2, U=1.6, TA=0.18, B=22, %162986218  
D=0.760, QC=0.1058, FS=1.3, U=1.5, TA=0.16, B=23, %162987312  
D=0.780, QC=0.1027, FS=1.5, U=1.4, TA=0.16, B=22, %162988078  
D=0.800, QC=0.1670, FS=1.6, U=1.2, TA=0.12, B=21, %162988843  
D=0.820, QC=0.1675, FS=1.3, U=1.9, TA=0.14, B=21, %162989984  
D=0.840, QC=0.1670, FS=1.1, U=2.0, TA=0.11, B=21, %162990765



D=0.860, QC=0.1697, FS=1.1, U=1.2, TA=0.10, B=21, %162991859  
D=0.880, QC=0.1603, FS=1.2, U=1.3, TA=0.14, B=22, %162992640  
D=0.900, QC=0.1628, FS=1.9, U=1.6, TA=0.10, B=21, %162993750  
D=0.920, QC=0.1639, FS=1.9, U=1.7, TA=0.16, B=21, %162994453  
D=0.940, QC=0.1675, FS=1.8, U=1.8, TA=0.09, B=21, %162995546 , F=11  
D=0.960, QC=0.1727, FS=1.9, U=1.0, TA=0.09, B=22, %162996343  
D=0.980, QC=0.1727, FS=1.9, U=1.1, TA=0.09, B=22, %162997062  
D=1.000, QC=0.1732, FS=1.2, U=1.4, TA=0.18, B=22, %162998250  
D=1.020, QC=0.1753, FS=1.3, U=1.5, TA=0.12, B=21, %162999015  
D=1.040, QC=0.1764, FS=1.6, U=1.7, TA=0.13, B=22, %163000125  
D=1.060, QC=0.1758, FS=1.7, U=1.8, TA=0.21, B=21, %163000828  
D=1.080, QC=0.1774, FS=1.7, U=2.1, TA=0.15, B=22, %163001968  
D=1.100, QC=0.1769, FS=1.7, U=2.2, TA=0.20, B=20, %163002750  
D=1.120, QC=0.1774, FS=1.6, U=2.4, TA=0.21, B=22, %163003875  
D=1.140, QC=0.1774, FS=1.5, U=2.6, TA=0.20, B=21, %163004546  
D=1.160, QC=0.1795, FS=1.4, U=2.9, TA=0.24, B=21, %163005671  
D=1.180, QC=0.1810, FS=1.3, U=3.0, TA=0.24, B=20, %163006453  
D=1.200, QC=0.1821, FS=1.2, U=3.1, TA=0.33, B=20, %163007546  
D=1.220, QC=0.1826, FS=1.1, U=3.5, TA=0.26, B=20, %163008750  
D=1.240, QC=0.1821, FS=1.1, U=3.6, TA=0.31, B=20, %163009421  
D=1.260, QC=0.1727, FS=1.1, U=5.1, TA=0.26, B=20, %163050421  
D=1.280, QC=0.1727, FS=1.1, U=5.1, TA=0.26, B=20, %163050421  
D=1.300, QC=0.1779, FS=1.1, U=5.1, TA=0.19, B=22, %163050875  
D=1.320, QC=0.1836, FS=1.0, U=2.3, TA=0.20, B=23, %163051546  
D=1.340, QC=0.1805, FS=1.1, U=2.3, TA=0.18, B=22, %163052359  
D=1.360, QC=0.2800, FS=2.0, U=2.4, TA=0.20, B=23, %163053468  
D=1.380, QC=0.2769, FS=2.9, U=2.6, TA=0.21, B=22, %163054250  
D=1.400, QC=0.2800, FS=2.8, U=2.6, TA=0.18, B=21, %163055359  
D=1.420, QC=0.2836, FS=2.5, U=2.7, TA=0.13, B=24, %163056031  
D=1.440, QC=0.2862, FS=2.3, U=2.8, TA=0.20, B=22, %163056796  
D=1.460, QC=0.2862, FS=0.1, U=2.8, TA=0.13, B=23, %163057562  
D=1.480, QC=0.2857, FS=0.7, U=3.0, TA=0.17, B=23, %163058703  
D=1.500, QC=0.2847, FS=1.0, U=3.1, TA=0.17, B=25, %163059500  
D=1.520, QC=0.2847, FS=1.2, U=3.2, TA=0.12, B=26, %163060187  
D=1.540, QC=0.2857, FS=1.3, U=3.2, TA=0.16, B=26, %163060968  
D=1.560, QC=0.2873, FS=1.3, U=3.4, TA=0.11, B=26, %163061750  
D=1.580, QC=0.2883, FS=1.3, U=3.4, TA=0.12, B=27, %163062406  
D=1.600, QC=0.2893, FS=1.5, U=3.5, TA=0.14, B=27, %163063187  
D=1.620, QC=0.2899, FS=1.6, U=3.7, TA=0.09, B=28, %163063953  
D=1.640, QC=0.2992, FS=1.6, U=3.7, TA=0.14, B=26, %163064750  
D=1.660, QC=0.1189, FS=1.6, U=3.8, TA=0.14, B=27, %163065421  
D=1.680, QC=0.1205, FS=1.5, U=4.0, TA=0.10, B=27, %163066203  
D=1.700, QC=0.1195, FS=1.4, U=4.1, TA=0.18, B=27, %163066968  
D=1.720, QC=0.1257, FS=1.4, U=4.1, TA=0.11, B=26, %163067312  
D=1.740, QC=0.1792, FS=1.0, U=4.2, TA=0.12, B=28, %163068078  
D=1.760, QC=0.2462, FS=1.6, U=4.4, TA=0.16, B=29, %163068765  
D=1.780, QC=0.2789, FS=1.0, U=4.4, TA=0.11, B=30, %163069546  
D=1.800, QC=0.2483, FS=1.1, U=4.5, TA=0.14, B=28, %163070312  
D=1.820, QC=0.2431, FS=1.8, U=4.7, TA=0.18, B=28, %163071078  
D=1.840, QC=0.3220, FS=1.6, U=4.8, TA=0.13, B=27, %163071843

D=1.860, QC=0.3922, FS=1.9, U=5.0, TA=0.15, B=27, %163072546  
D=1.880, QC=0.3792, FS=1.2, U=5.1, TA=0.15, B=28, %163073328  
D=1.900, QC=0.3792, FS=1.5, U=5.2, TA=0.15, B=30, %163073671  
D=1.920, QC=0.3948, FS=2.4, U=5.4, TA=0.13, B=30, %163074468  
D=1.940, QC=0.4654, FS=2.3, U=5.5, TA=0.19, B=33, %163075171  
D=1.960, QC=0.4140, FS=2.3, U=5.5, TA=0.16, B=34, %163075609  
D=1.980, QC=0.3226, FS=1.1, U=5.5, TA=0.15, B=34, %163076296  
D=2.000, QC=0.3226, FS=1.3, U=5.6, TA=0.15, B=35, %163076640  
D=2.020, QC=0.2254, FS=1.5, U=5.7, TA=0.14, B=35, %163077406  
D=2.040, QC=0.1823, FS=1.5, U=5.7, TA=0.15, B=35, %163077859  
D=2.060, QC=0.1922, FS=1.8, U=5.8, TA=0.17, B=36, %163078625  
D=2.080, QC=0.1922, FS=1.2, U=5.9, TA=0.17, B=35, %163078968  
D=2.100, QC=0.1771, FS=1.2, U=6.1, TA=0.15, B=37, %163079656  
D=2.120, QC=0.1569, FS=1.2, U=6.1, TA=0.16, B=39, %163080093  
D=2.140, QC=0.1569, FS=1.8, U=6.2, TA=0.16, B=40, %163080421  
D=2.160, QC=0.1860, FS=1.6, U=6.4, TA=0.16, B=41, %163081187  
D=2.180, QC=0.2530, FS=1.6, U=6.4, TA=0.15, B=42, %163081625  
D=2.200, QC=0.2530, FS=1.7, U=6.6, TA=0.15, B=43, %163081953  
D=2.220, QC=0.2182, FS=1.7, U=6.6, TA=0.16, B=46, %163082296  
D=2.240, QC=0.2182, FS=1.1, U=4.4, TA=0.16, B=45, %163082640  
D=2.260, QC=0.1595, FS=1.9, U=4.6, TA=0.16, B=43, %163083421  
D=2.280, QC=0.2135, FS=1.9, U=4.6, TA=0.17, B=46, %163083781  
D=2.300, QC=0.2135, FS=1.3, U=4.7, TA=0.17, B=46, %163084250  
D=2.320, QC=0.3413, FS=1.3, U=4.7, TA=0.16, B=45, %163084578  
D=2.340, QC=0.3413, FS=1.2, U=4.9, TA=0.16, B=45, %163084906  
D=2.360, QC=0.2639, FS=1.2, U=4.9, TA=0.18, B=44, %163085359  
D=2.380, QC=0.2737, FS=1.9, U=5.0, TA=0.18, B=45, %163086031  
D=2.400, QC=0.2737, FS=1.5, U=5.2, TA=0.18, B=43, %163086500  
D=2.420, QC=0.3028, FS=1.5, U=5.2, TA=0.16, B=41, %163086828  
D=2.440, QC=0.2384, FS=1.3, U=5.2, TA=0.16, B=28, %163087593 , F=13  
D=2.460, QC=0.1418, FS=1.2, U=5.5, TA=0.13, B=28, %163126468  
D=2.480, QC=0.1418, FS=1.2, U=5.5, TA=0.13, B=28, %163126468  
D=2.500, QC=0.1418, FS=1.2, U=5.5, TA=0.13, B=28, %163126468  
D=2.520, QC=0.1444, FS=1.1, U=5.1, TA=0.13, B=28, %163127250  
D=2.540, QC=0.1470, FS=1.1, U=5.1, TA=0.14, B=28, %163128015  
D=2.560, QC=0.1548, FS=1.3, U=5.2, TA=0.13, B=25, %163128687  
D=2.580, QC=0.1662, FS=1.1, U=5.2, TA=0.14, B=24, %163129468  
D=2.600, QC=0.1792, FS=1.2, U=5.4, TA=0.15, B=26, %163130250  
D=2.620, QC=0.2078, FS=1.0, U=5.5, TA=0.16, B=26, %163131015  
D=2.640, QC=0.2607, FS=1.3, U=5.5, TA=0.13, B=25, %163131687  
D=2.660, QC=0.3168, FS=1.0, U=5.7, TA=0.14, B=24, %163132484  
D=2.680, QC=0.3480, FS=2.2, U=5.8, TA=0.17, B=24, %163133265  
D=2.700, QC=0.3548, FS=3.3, U=5.8, TA=0.17, B=25, %163133937  
D=2.720, QC=0.3745, FS=4.2, U=5.9, TA=0.19, B=25, %163135046  
D=2.740, QC=0.3111, FS=5.4, U=5.9, TA=0.15, B=24, %163135843  
D=2.760, QC=0.4919, FS=6.3, U=6.0, TA=0.14, B=24, %163136640  
D=2.780, QC=0.5682, FS=7.9, U=6.1, TA=0.18, B=27, %163137328  
D=2.800, QC=0.5963, FS=9.4, U=6.2, TA=0.16, B=25, %163138125  
D=2.820, QC=0.6238, FS=10.9, U=6.5, TA=0.15, B=24, %163138796  
D=2.840, QC=0.6503, FS=11.7, U=6.6, TA=0.15, B=24, %163139578

D=2.860, QC=0.7225, FS=12.8, U=6.6, TA=0.17, B=26, %163140359  
D=2.880, QC=0.8835, FS=14.0, U=6.7, TA=0.15, B=25, %163141125  
D=2.900, QC=1.0238, FS=54.0, U=7.1, TA=0.16, B=25, %163142218  
D=2.920, QC=1.0710, FS=69.5, U=7.9, TA=0.17, B=25, %163143000  
D=2.940, QC=1.1100, FS=59.5, U=3.6, TA=0.13, B=26, %163143687  
D=2.960, QC=1.1089, FS=69.0, U=0.8, TA=0.10, B=26, %163144453  
D=2.980, QC=1.3635, FS=94.3, U=0.8, TA=0.09, B=24, %163145218  
D=3.000, QC=1.4860, FS=104.4, U=2.5, TA=0.11, B=23, %163146000  
D=3.020, QC=1.3484, FS=94.9, U=3.2, TA=0.11, B=25, %163146671  
D=3.040, QC=1.1754, FS=84.7, U=2.9, TA=0.13, B=25, %163147468  
D=3.060, QC=1.0061, FS=53.2, U=2.4, TA=0.15, B=25, %163148156  
D=3.080, QC=0.9609, FS=22.2, U=1.1, TA=0.17, B=25, %163148968  
D=3.100, QC=0.8882, FS=1.9, U=2.2, TA=0.16, B=26, %163149656  
D=3.120, QC=0.6742, FS=0.8, U=2.4, TA=0.16, B=27, %163150453  
D=3.140, QC=0.5095, FS=2.4, U=2.4, TA=0.18, B=27, %163151218  
D=3.160, QC=0.4129, FS=4.8, U=2.5, TA=0.17, B=26, %163152015  
D=3.180, QC=0.3470, FS=7.2, U=2.4, TA=0.17, B=26, %163152687  
D=3.200, QC=0.3267, FS=7.5, U=2.4, TA=0.19, B=27, %163153453  
D=3.220, QC=0.3750, FS=8.0, U=2.2, TA=0.19, B=26, %163154234  
D=3.240, QC=0.7178, FS=14.3, U=2.1, TA=0.19, B=26, %163155015  
D=3.260, QC=0.8576, FS=4.9, U=1.5, TA=0.17, B=26, %163155765  
D=3.280, QC=0.6586, FS=2.4, U=4.0, TA=0.17, B=26, %163156421  
D=3.300, QC=0.4763, FS=0.5, U=4.0, TA=0.19, B=27, %163157203  
D=3.320, QC=0.3600, FS=1.4, U=1.7, TA=0.19, B=27, %163157984  
D=3.340, QC=0.2914, FS=3.2, U=4.0, TA=0.19, B=27, %163158781  
D=3.360, QC=0.3309, FS=3.8, U=3.8, TA=0.19, B=26, %163159437  
D=3.380, QC=0.3600, FS=3.2, U=3.7, TA=0.19, B=26, %163160218  
D=3.400, QC=0.3303, FS=3.7, U=3.7, TA=0.19, B=26, %163160906  
D=3.420, QC=0.2748, FS=4.5, U=3.6, TA=0.18, B=27, %163161703  
D=3.440, QC=0.2379, FS=4.7, U=3.5, TA=0.19, B=26, %163162500  
D=3.460, QC=0.2228, FS=2.8, U=3.5, TA=0.19, B=25, %163163171  
D=3.480, QC=0.2285, FS=1.8, U=3.4, TA=0.19, B=27, %163163937  
D=3.500, QC=0.2509, FS=1.4, U=3.3, TA=0.20, B=27, %163164718  
D=3.520, QC=0.2883, FS=1.1, U=3.2, TA=0.20, B=26, %163165515  
D=3.540, QC=0.2794, FS=0.4, U=3.1, TA=0.19, B=25, %163166281  
D=3.560, QC=0.2478, FS=0.6, U=3.1, TA=0.19, B=25, %163166953  
D=3.580, QC=0.2254, FS=1.3, U=3.0, TA=0.19, B=26, %163167734  
D=3.600, QC=0.2104, FS=0.5, U=2.9, TA=0.19, B=26, %163168421  
D=3.620, QC=0.2197, FS=0.3, U=2.8, TA=0.20, B=24, %163169203  
D=3.640, QC=0.2327, FS=0.2, U=2.7, TA=0.20, B=24, %163169984  
D=3.660, QC=0.2015, FS=1.7, U=2.7, TA=0.15, B=27, %163207437  
D=3.680, QC=0.2015, FS=1.7, U=2.7, TA=0.15, B=27, %163207437  
D=3.700, QC=0.2015, FS=1.7, U=2.7, TA=0.15, B=27, %163207437  
D=3.720, QC=0.2067, FS=1.4, U=3.1, TA=0.19, B=27, %163208218  
D=3.740, QC=0.2005, FS=1.5, U=3.0, TA=0.19, B=26, %163209000  
D=3.760, QC=0.1969, FS=1.3, U=3.0, TA=0.19, B=27, %163209765  
D=3.780, QC=0.1969, FS=1.2, U=2.9, TA=0.20, B=26, %163210546  
D=3.800, QC=0.1984, FS=1.1, U=2.9, TA=0.20, B=27, %163211265  
D=3.820, QC=0.2000, FS=0.6, U=2.8, TA=0.16, B=25, %163212031  
D=3.840, QC=0.2015, FS=0.4, U=2.7, TA=0.15, B=25, %163212703

D=3.860, QC=0.2026, FS=0.5, U=2.7, TA=0.08, B=24, %163213468  
D=3.880, QC=0.2052, FS=0.6, U=2.5, TA=0.18, B=26, %163214250  
D=3.900, QC=0.2072, FS=0.8, U=2.6, TA=0.23, B=26, %163215015  
D=3.920, QC=0.2104, FS=0.9, U=2.6, TA=0.23, B=26, %163215703  
D=3.940, QC=0.2109, FS=1.1, U=2.4, TA=0.23, B=25, %163216468  
D=3.960, QC=0.2166, FS=1.3, U=2.4, TA=0.23, B=28, %163217234  
D=3.980, QC=0.2182, FS=1.6, U=2.3, TA=0.23, B=28, %163218031  
D=4.000, QC=0.2197, FS=1.5, U=2.2, TA=0.23, B=28, %163218687  
D=4.020, QC=0.2239, FS=1.7, U=2.1, TA=0.23, B=27, %163219484  
D=4.040, QC=0.2259, FS=1.8, U=2.0, TA=0.23, B=27, %163220265  
D=4.060, QC=0.2244, FS=1.9, U=2.0, TA=0.23, B=27, %163220937  
D=4.080, QC=0.2285, FS=2.1, U=1.9, TA=0.23, B=29, %163221703  
D=4.100, QC=0.2296, FS=2.4, U=1.8, TA=0.23, B=26, %163222515  
D=4.120, QC=0.2311, FS=2.5, U=1.6, TA=0.23, B=28, %163223281  
D=4.140, QC=0.2311, FS=2.7, U=1.6, TA=0.23, B=29, %163223953  
D=4.160, QC=0.2327, FS=2.7, U=1.6, TA=0.23, B=30, %163224406  
D=4.180, QC=0.2337, FS=2.8, U=1.5, TA=0.23, B=28, %163225078  
D=4.200, QC=0.2337, FS=2.8, U=1.5, TA=0.23, B=29, %163225843  
D=4.220, QC=0.2337, FS=2.8, U=1.3, TA=0.23, B=28, %163226625  
D=4.240, QC=0.2311, FS=2.7, U=1.2, TA=0.23, B=29, %163227406  
D=4.260, QC=0.2301, FS=2.7, U=1.2, TA=0.23, B=28, %163228093  
D=4.280, QC=0.2301, FS=2.7, U=1.1, TA=0.23, B=30, %163228546  
D=4.300, QC=0.2317, FS=2.6, U=1.0, TA=0.23, B=29, %163229203  
D=4.320, QC=0.2400, FS=2.6, U=0.9, TA=0.23, B=31, %163229968  
D=4.340, QC=0.2446, FS=2.4, U=0.9, TA=0.23, B=28, %163230734  
D=4.360, QC=0.2498, FS=2.3, U=0.7, TA=0.23, B=29, %163231515  
D=4.380, QC=0.2602, FS=2.3, U=0.7, TA=0.23, B=29, %163231843  
D=4.400, QC=0.4259, FS=2.8, U=0.5, TA=0.23, B=29, %163232671  
D=4.420, QC=0.6721, FS=3.3, U=0.5, TA=0.23, B=28, %163233328  
D=4.440, QC=0.7760, FS=4.3, U=0.1, TA=0.23, B=29, %163234109  
D=4.460, QC=0.5625, FS=6.9, U=0.0, TA=0.23, B=28, %163234875  
D=4.480, QC=0.4805, FS=3.7, U=0.3, TA=0.23, B=29, %163235640  
D=4.500, QC=0.4805, FS=4.1, U=0.1, TA=0.23, B=29, %163235984  
D=4.520, QC=0.3423, FS=4.9, U=0.0, TA=0.23, B=29, %163236750  
D=4.540, QC=0.3288, FS=6.0, U=0.1, TA=0.23, B=28, %163237515  
D=4.560, QC=0.3142, FS=6.7, U=0.1, TA=0.23, B=29, %163238281  
D=4.580, QC=0.3210, FS=7.8, U=-2.1, TA=0.23, B=28, %163238937  
D=4.600, QC=0.3288, FS=8.6, U=0.3, TA=0.24, B=29, %163239750  
D=4.620, QC=0.3402, FS=8.6, U=0.3, TA=0.23, B=28, %163240078  
D=4.640, QC=0.3402, FS=9.7, U=0.4, TA=0.24, B=29, %163240890  
D=4.660, QC=0.3470, FS=9.9, U=0.5, TA=0.24, B=28, %163241656  
D=4.680, QC=0.3475, FS=9.9, U=-1.7, TA=0.25, B=29, %163242312  
D=4.700, QC=0.3345, FS=11.0, U=-1.5, TA=0.25, B=28, %163243078  
D=4.720, QC=0.3226, FS=12.0, U=-1.5, TA=0.25, B=27, %163243859  
D=4.740, QC=0.3272, FS=12.2, U=-1.4, TA=0.25, B=27, %163244640  
D=4.760, QC=0.3116, FS=12.7, U=-1.3, TA=0.26, B=28, %163245421  
D=4.780, QC=0.2992, FS=12.6, U=-1.3, TA=0.26, B=27, %163246093  
D=4.800, QC=0.2992, FS=12.0, U=-1.2, TA=0.26, B=27, %163246546  
D=4.820, QC=0.3075, FS=10.7, U=-1.1, TA=0.26, B=26, %163247203  
D=4.840, QC=0.2820, FS=8.4, U=-1.0, TA=0.26, B=24, %163248343

D=4.860, QC=0.3901, FS=10.9, U=1.0, TA=0.23, B=25, %163283562  
D=4.880, QC=0.3901, FS=10.9, U=1.0, TA=0.23, B=25, %163283562  
D=4.900, QC=0.4098, FS=10.9, U=1.0, TA=0.23, B=25, %163284015  
D=4.920, QC=0.4161, FS=13.0, U=0.5, TA=0.23, B=27, %163284796  
D=4.940, QC=0.4062, FS=15.1, U=0.5, TA=0.23, B=24, %163285484  
D=4.960, QC=0.3802, FS=17.3, U=0.6, TA=0.24, B=23, %163286265  
D=4.980, QC=0.3657, FS=18.4, U=0.6, TA=0.25, B=25, %163286937  
D=5.000, QC=0.3423, FS=21.1, U=0.7, TA=0.25, B=26, %163288140  
D=5.020, QC=0.3231, FS=21.0, U=0.7, TA=0.24, B=24, %163288812  
D=5.040, QC=0.3106, FS=19.6, U=0.7, TA=0.25, B=24, %163289593  
D=5.060, QC=0.3033, FS=17.5, U=0.8, TA=0.25, B=26, %163290359  
D=5.080, QC=0.2981, FS=15.3, U=0.9, TA=0.25, B=26, %163291171  
D=5.100, QC=0.2914, FS=13.1, U=1.0, TA=0.24, B=25, %163291828  
D=5.120, QC=0.2955, FS=10.6, U=1.0, TA=0.25, B=25, %163292593  
D=5.140, QC=0.3065, FS=8.5, U=1.1, TA=0.25, B=26, %163293375  
D=5.160, QC=0.3148, FS=7.6, U=1.1, TA=0.25, B=28, %163294140  
D=5.180, QC=0.3194, FS=7.1, U=1.2, TA=0.25, B=26, %163294921  
D=5.200, QC=0.3252, FS=6.8, U=1.2, TA=0.25, B=25, %163295578  
D=5.220, QC=0.3278, FS=6.7, U=1.3, TA=0.26, B=25, %163296359  
D=5.240, QC=0.3288, FS=6.9, U=1.4, TA=0.27, B=27, %163297125  
D=5.260, QC=0.3298, FS=7.3, U=1.4, TA=0.25, B=26, %163297906  
D=5.280, QC=0.3288, FS=7.6, U=1.5, TA=0.25, B=26, %163298671  
D=5.300, QC=0.3314, FS=7.9, U=1.5, TA=0.22, B=27, %163299328  
D=5.320, QC=0.3329, FS=8.1, U=1.6, TA=0.25, B=28, %163300109  
D=5.340, QC=0.3329, FS=8.1, U=1.6, TA=0.25, B=28, %163300890  
D=5.360, QC=0.3387, FS=8.1, U=1.7, TA=0.24, B=27, %163301656  
D=5.380, QC=0.3470, FS=8.1, U=-0.5, TA=0.24, B=26, %163302312  
D=5.400, QC=0.3407, FS=8.1, U=-0.5, TA=0.24, B=28, %163302781  
D=5.420, QC=0.3355, FS=7.2, U=-0.3, TA=0.23, B=16, %163303921  
D=5.440, QC=0.3210, FS=7.2, U=2.1, TA=0.22, B=16, %163305359  
D=5.460, QC=0.3033, FS=7.3, U=2.1, TA=0.21, B=16, %163306531  
D=5.480, QC=0.3085, FS=7.7, U=-0.1, TA=0.21, B=16, %163307671  
D=5.500, QC=0.3065, FS=7.9, U=-0.0, TA=0.19, B=17, %163308812  
D=5.520, QC=0.3075, FS=8.2, U=0.1, TA=0.21, B=16, %163309906  
D=5.540, QC=0.3096, FS=8.1, U=0.2, TA=0.17, B=16, %163311000  
D=5.560, QC=0.3153, FS=8.4, U=0.3, TA=0.18, B=22, %163312109  
D=5.580, QC=0.3210, FS=8.4, U=0.4, TA=0.16, B=21, %163313218  
D=5.600, QC=0.3215, FS=8.4, U=0.4, TA=0.17, B=21, %163314031  
D=5.620, QC=0.3226, FS=8.2, U=0.5, TA=0.17, B=21, %163315125  
D=5.640, QC=0.3205, FS=7.9, U=0.6, TA=0.16, B=21, %163315906  
D=5.660, QC=0.3267, FS=7.8, U=0.7, TA=0.17, B=21, %163316562  
D=5.680, QC=0.3226, FS=8.0, U=0.8, TA=0.15, B=21, %163317781  
D=5.700, QC=0.3163, FS=8.1, U=0.8, TA=0.15, B=21, %163318437  
D=5.720, QC=0.3127, FS=7.8, U=1.0, TA=0.17, B=22, %163319640  
D=5.740, QC=0.3065, FS=7.8, U=-1.2, TA=0.15, B=21, %163320421  
D=5.760, QC=0.3023, FS=7.8, U=1.1, TA=0.15, B=21, %163321546  
D=5.780, QC=0.2987, FS=7.7, U=1.1, TA=0.16, B=21, %163322203  
D=5.800, QC=0.3013, FS=7.5, U=-1.1, TA=0.15, B=22, %163323312  
D=5.820, QC=0.3137, FS=7.4, U=-1.0, TA=0.15, B=21, %163324078  
D=5.840, QC=0.3200, FS=7.6, U=1.4, TA=0.13, B=20, %163325281

D=5.860, QC=0.3303, FS=7.5, U=-0.8, TA=0.12, B=21, %163325968  
D=5.880, QC=0.3511, FS=7.3, U=-0.7, TA=0.12, B=21, %163327078  
D=5.900, QC=0.3511, FS=7.2, U=-0.6, TA=0.12, B=20, %163327859  
D=5.920, QC=0.3340, FS=6.9, U=-0.6, TA=0.11, B=20, %163328953  
D=5.940, QC=0.3319, FS=7.3, U=-0.5, TA=0.11, B=20, %163330171  
D=5.960, QC=0.3200, FS=7.7, U=-0.4, TA=0.11, B=20, %163330859  
D=5.980, QC=0.3174, FS=7.9, U=-0.3, TA=0.11, B=20, %163331953  
D=6.000, QC=0.2909, FS=8.3, U=-0.4, TA=0.09, B=20, %163332734  
D=6.020, QC=0.3080, FS=8.5, U=2.9, TA=0.13, B=30, %163368781  
D=6.040, QC=0.3080, FS=8.5, U=2.9, TA=0.13, B=30, %163368781  
D=6.060, QC=0.3080, FS=8.5, U=2.9, TA=0.13, B=30, %163368781  
D=6.080, QC=0.3106, FS=8.5, U=2.9, TA=0.11, B=29, %163369109  
D=6.100, QC=0.3054, FS=7.7, U=2.5, TA=0.11, B=30, %163369906  
D=6.120, QC=0.2981, FS=7.3, U=2.5, TA=0.09, B=32, %163370578  
D=6.140, QC=0.2945, FS=7.0, U=2.5, TA=0.11, B=30, %163371359  
D=6.160, QC=0.2992, FS=6.5, U=2.6, TA=0.08, B=21, %163372125  
D=6.180, QC=0.3002, FS=6.4, U=2.5, TA=0.05, B=23, %163372906  
D=6.200, QC=0.3054, FS=6.2, U=2.5, TA=0.08, B=23, %163373671  
D=6.220, QC=0.3059, FS=6.5, U=2.6, TA=0.04, B=22, %163374765  
D=6.240, QC=0.3070, FS=6.7, U=2.7, TA=0.02, B=21, %163375437  
D=6.260, QC=0.3028, FS=6.9, U=2.7, TA=0.06, B=22, %163376640  
D=6.280, QC=0.3002, FS=7.1, U=2.7, TA=0.03, B=22, %163377312  
D=6.300, QC=0.3013, FS=7.4, U=2.7, TA=0.04, B=21, %163378093  
D=6.320, QC=0.2971, FS=7.7, U=2.9, TA=0.05, B=21, %163379187  
D=6.340, QC=0.2997, FS=7.6, U=2.9, TA=0.04, B=22, %163379953  
D=6.360, QC=0.3002, FS=7.5, U=2.9, TA=0.03, B=23, %163380734  
D=6.380, QC=0.3007, FS=7.3, U=3.0, TA=0.02, B=22, %163381859  
D=6.400, QC=0.2987, FS=7.1, U=3.0, TA=0.03, B=21, %163382625  
D=6.420, QC=0.2966, FS=6.8, U=3.1, TA=0.03, B=22, %163383734  
D=6.440, QC=0.2971, FS=6.8, U=3.1, TA=0.04, B=23, %163384515  
D=6.460, QC=0.2950, FS=6.9, U=3.2, TA=0.03, B=23, %163385187  
D=6.480, QC=0.2940, FS=7.1, U=3.2, TA=0.03, B=22, %163385984  
D=6.500, QC=0.2992, FS=7.0, U=3.3, TA=0.01, B=23, %163387093  
D=6.520, QC=0.3065, FS=6.8, U=3.4, TA=0.03, B=24, %163387890  
D=6.540, QC=0.3132, FS=6.6, U=3.4, TA=0.00, B=24, %163388656  
D=6.560, QC=0.3142, FS=6.4, U=3.5, TA=0.04, B=23, %163389312  
D=6.580, QC=0.3194, FS=6.1, U=3.5, TA=0.03, B=23, %163390468  
D=6.600, QC=0.3205, FS=5.8, U=3.5, TA=0.03, B=24, %163391281  
D=6.620, QC=0.3303, FS=6.0, U=3.5, TA=0.02, B=23, %163391953  
D=6.640, QC=0.3267, FS=6.5, U=3.5, TA=0.05, B=24, %163392718  
D=6.660, QC=0.3111, FS=6.7, U=3.7, TA=0.04, B=23, %163393484  
D=6.680, QC=0.3065, FS=6.3, U=3.7, TA=0.02, B=24, %163394593  
D=6.700, QC=0.3013, FS=6.1, U=3.8, TA=0.01, B=24, %163395359  
D=6.720, QC=0.3039, FS=5.7, U=3.8, TA=0.04, B=24, %163396156  
D=6.740, QC=0.3283, FS=5.5, U=3.9, TA=0.03, B=23, %163396812  
D=6.760, QC=0.3766, FS=5.6, U=3.9, TA=0.03, B=25, %163397578  
D=6.780, QC=0.4342, FS=5.4, U=4.1, TA=0.02, B=24, %163398687  
D=6.800, QC=0.4612, FS=7.5, U=4.1, TA=0.01, B=23, %163399453  
D=6.820, QC=0.4768, FS=7.3, U=4.1, TA=0.03, B=23, %163400234  
D=6.840, QC=0.4623, FS=5.8, U=4.1, TA=0.01, B=24, %163401000

D=6.860, QC=0.4036, FS=7.1, U=4.2, TA=0.02, B=23, %163401781  
D=6.880, QC=0.3548, FS=7.9, U=4.2, TA=0.02, B=22, %163402812  
D=6.900, QC=0.3802, FS=6.6, U=4.2, TA=0.03, B=21, %163403578  
D=6.920, QC=0.3963, FS=7.1, U=4.4, TA=0.00, B=22, %163404687  
D=6.940, QC=0.4405, FS=8.3, U=4.4, TA=0.01, B=22, %163405453  
D=6.960, QC=0.5864, FS=10.6, U=4.7, TA=0.00, B=21, %163406250  
D=6.980, QC=0.9552, FS=13.1, U=4.5, TA=0.02, B=21, %163407359  
D=7.000, QC=0.9027, FS=12.9, U=4.5, TA=0.03, B=21, %163408125  
D=7.020, QC=0.7464, FS=7.3, U=4.7, TA=0.02, B=20, %163409234  
D=7.040, QC=0.6186, FS=6.5, U=4.7, TA=0.04, B=20, %163410000  
D=7.060, QC=0.5594, FS=7.8, U=4.7, TA=0.02, B=21, %163411125  
D=7.080, QC=0.6347, FS=8.1, U=4.8, TA=0.03, B=21, %163411890  
D=7.100, QC=0.9043, FS=24.2, U=5.4, TA=0.00, B=20, %163413000  
D=7.120, QC=0.9375, FS=27.5, U=5.9, TA=0.01, B=19, %163414093  
D=7.140, QC=0.8970, FS=18.2, U=5.4, TA=0.01, B=20, %163414890  
D=7.160, QC=0.8139, FS=7.6, U=5.1, TA=0.00, B=21, %163416015  
D=7.180, QC=0.6654, FS=7.9, U=5.0, TA=0.03, B=20, %163416671  
D=7.200, QC=0.6165, FS=14.4, U=5.1, TA=0.01, B=19, %163417906  
D=7.220, QC=0.8191, FS=13.8, U=5.4, TA=0.01, B=19, %163418937 , F=11  
D=7.240, QC=0.7339, FS=15.0, U=5.4, TA=0.06, B=22, %163458750  
D=7.260, QC=0.7339, FS=15.0, U=5.4, TA=0.06, B=22, %163458750  
D=7.280, QC=0.7339, FS=15.0, U=5.4, TA=0.06, B=22, %163458750  
D=7.300, QC=0.7812, FS=15.9, U=2.4, TA=0.07, B=19, %163459515  
D=7.320, QC=0.8518, FS=14.1, U=2.4, TA=0.05, B=16, %163460609  
D=7.340, QC=0.7828, FS=11.8, U=2.4, TA=0.11, B=18, %163461703  
D=7.360, QC=0.5797, FS=16.4, U=2.4, TA=0.04, B=19, %163462812  
D=7.380, QC=0.5262, FS=15.6, U=2.4, TA=0.04, B=20, %163463609  
D=7.400, QC=0.5095, FS=15.0, U=2.4, TA=0.05, B=21, %163464718  
D=7.420, QC=0.4768, FS=12.4, U=2.4, TA=0.05, B=19, %163465500  
D=7.440, QC=0.4431, FS=13.8, U=2.4, TA=0.05, B=19, %163466609  
D=7.460, QC=0.4244, FS=11.6, U=2.4, TA=0.04, B=19, %163467703  
D=7.480, QC=0.4109, FS=12.3, U=2.5, TA=0.05, B=20, %163468843  
D=7.500, QC=0.4072, FS=11.6, U=2.5, TA=0.05, B=19, %163469625  
D=7.520, QC=0.4186, FS=10.2, U=2.6, TA=0.05, B=19, %163470718  
D=7.540, QC=0.4264, FS=10.5, U=2.6, TA=0.04, B=20, %163471828  
D=7.560, QC=0.4041, FS=10.2, U=2.6, TA=0.04, B=21, %163472609  
D=7.580, QC=0.3771, FS=10.1, U=2.7, TA=0.05, B=19, %163473718  
D=7.600, QC=0.3750, FS=9.5, U=2.7, TA=0.05, B=19, %163474500  
D=7.620, QC=0.3771, FS=9.1, U=2.8, TA=0.05, B=19, %163475593  
D=7.640, QC=0.3776, FS=8.6, U=2.8, TA=0.05, B=20, %163476703  
D=7.660, QC=0.3714, FS=8.6, U=2.9, TA=0.05, B=20, %163477468  
D=7.680, QC=0.3750, FS=9.0, U=2.9, TA=0.04, B=19, %163478593  
D=7.700, QC=0.3927, FS=8.7, U=3.0, TA=0.05, B=20, %163479703  
D=7.720, QC=0.4119, FS=8.4, U=3.0, TA=0.04, B=22, %163480484  
D=7.740, QC=0.4384, FS=8.6, U=3.0, TA=0.05, B=21, %163481296  
D=7.760, QC=0.4721, FS=9.3, U=3.2, TA=0.03, B=20, %163482296  
D=7.780, QC=0.4623, FS=9.5, U=3.3, TA=0.06, B=20, %163483531  
D=7.800, QC=0.4275, FS=9.2, U=3.1, TA=0.04, B=21, %163484203  
D=7.820, QC=0.4046, FS=9.9, U=3.2, TA=0.06, B=20, %163485328  
D=7.840, QC=0.3885, FS=10.0, U=3.2, TA=0.05, B=20, %163486109

D=7.860, QC=0.3927, FS=10.2, U=3.3, TA=0.04, B=20, %163487234  
D=7.880, QC=0.3984, FS=10.2, U=3.3, TA=0.04, B=20, %163488015  
D=7.900, QC=0.3885, FS=9.5, U=3.4, TA=0.05, B=21, %163489125  
D=7.920, QC=0.3818, FS=9.3, U=3.5, TA=0.08, B=20, %163489812  
D=7.940, QC=0.3802, FS=8.6, U=3.5, TA=0.08, B=20, %163491015  
D=7.960, QC=0.3838, FS=7.9, U=3.4, TA=0.08, B=21, %163491687  
D=7.980, QC=0.3916, FS=7.4, U=3.7, TA=0.09, B=20, %163492890  
D=8.000, QC=0.4218, FS=7.5, U=3.7, TA=0.08, B=20, %163494000  
D=8.020, QC=0.6098, FS=8.3, U=3.8, TA=0.10, B=20, %163494671  
D=8.040, QC=0.7890, FS=11.5, U=4.3, TA=0.09, B=20, %163495906  
D=8.060, QC=0.8404, FS=8.2, U=4.0, TA=0.09, B=20, %163496593  
D=8.080, QC=0.6649, FS=9.0, U=4.0, TA=0.11, B=20, %163497781  
D=8.100, QC=0.5599, FS=15.1, U=4.0, TA=0.13, B=20, %163498890  
D=8.120, QC=0.4841, FS=16.3, U=4.1, TA=0.12, B=21, %163499562  
D=8.140, QC=0.4503, FS=15.4, U=4.0, TA=0.12, B=20, %163500687  
D=8.160, QC=0.4893, FS=15.3, U=4.1, TA=0.10, B=20, %163501515  
D=8.180, QC=0.5371, FS=14.2, U=4.1, TA=0.14, B=20, %163502578  
D=8.200, QC=0.5012, FS=13.6, U=4.3, TA=0.11, B=20, %163503687  
D=8.220, QC=0.4789, FS=13.3, U=4.3, TA=0.12, B=20, %163504453  
D=8.240, QC=0.4955, FS=11.2, U=4.3, TA=0.13, B=19, %163505656  
D=8.260, QC=0.6259, FS=11.9, U=4.2, TA=0.13, B=20, %163506312  
D=8.280, QC=0.8228, FS=15.9, U=4.5, TA=0.13, B=20, %163507468  
D=8.300, QC=0.7983, FS=16.7, U=5.4, TA=0.14, B=19, %163508578  
D=8.320, QC=0.9703, FS=28.4, U=6.7, TA=0.16, B=18, %163509703  
D=8.340, QC=1.0009, FS=40.6, U=7.9, TA=0.15, B=19, %163510468  
D=8.360, QC=0.9770, FS=37.8, U=6.7, TA=0.14, B=19, %163511593  
D=8.380, QC=0.9365, FS=32.0, U=6.0, TA=0.16, B=19, %163512703  
D=8.400, QC=0.9391, FS=52.8, U=8.7, TA=0.17, B=18, %163513828  
D=8.420, QC=0.9968, FS=52.8, U=8.7, TA=0.24, B=22, %163553000  
D=8.440, QC=0.9968, FS=52.8, U=8.7, TA=0.24, B=22, %163553000  
D=8.460, QC=0.9739, FS=52.8, U=8.7, TA=0.19, B=24, %163553437  
D=8.480, QC=0.9412, FS=24.4, U=7.2, TA=0.18, B=26, %163554109  
D=8.500, QC=0.7194, FS=14.7, U=6.1, TA=0.19, B=27, %163554906  
D=8.520, QC=0.5646, FS=16.4, U=6.0, TA=0.18, B=28, %163555656  
D=8.540, QC=0.5153, FS=15.6, U=6.0, TA=0.20, B=26, %163556437  
D=8.560, QC=0.5173, FS=14.5, U=6.0, TA=0.21, B=28, %163557218  
D=8.580, QC=0.5173, FS=14.0, U=6.0, TA=0.21, B=28, %163557546  
D=8.600, QC=0.5916, FS=16.3, U=6.1, TA=0.22, B=28, %163558312  
D=8.620, QC=0.9433, FS=33.0, U=6.7, TA=0.23, B=26, %163559078  
D=8.640, QC=0.9749, FS=32.9, U=7.1, TA=0.19, B=26, %163559734  
D=8.660, QC=0.9453, FS=18.4, U=6.8, TA=0.24, B=26, %163560515  
D=8.680, QC=0.8955, FS=10.6, U=6.2, TA=0.26, B=28, %163561281  
D=8.700, QC=0.7407, FS=10.4, U=5.7, TA=0.28, B=26, %163562078  
D=8.720, QC=0.5745, FS=12.3, U=5.9, TA=0.29, B=26, %163562765  
D=8.740, QC=0.5386, FS=14.6, U=5.8, TA=0.28, B=28, %163563546  
D=8.760, QC=0.6088, FS=16.7, U=5.9, TA=0.30, B=29, %163564312  
D=8.780, QC=0.6971, FS=19.2, U=6.2, TA=0.30, B=27, %163564984  
D=8.800, QC=0.8305, FS=20.7, U=6.3, TA=0.32, B=26, %163565781  
D=8.820, QC=0.9609, FS=41.6, U=7.4, TA=0.30, B=26, %163566578  
D=8.840, QC=1.0056, FS=67.0, U=8.7, TA=0.30, B=28, %163567250



D=8.860, QC=1.0419, FS=65.9, U=9.7, TA=0.30, B=27, %163568031  
D=8.880, QC=1.0295, FS=43.0, U=9.3, TA=0.26, B=25, %163568812  
D=8.900, QC=0.9292, FS=14.5, U=7.5, TA=0.29, B=26, %163569484  
D=8.920, QC=0.8726, FS=14.5, U=7.5, TA=0.29, B=29, %163569921  
D=8.940, QC=0.7396, FS=8.5, U=6.5, TA=0.33, B=27, %163570687  
D=8.960, QC=0.6300, FS=16.7, U=6.8, TA=0.34, B=26, %163571375  
D=8.980, QC=0.6498, FS=18.8, U=6.6, TA=0.34, B=27, %163572156  
D=9.000, QC=0.7152, FS=18.7, U=6.6, TA=0.34, B=28, %163572921  
D=9.020, QC=0.7329, FS=18.2, U=6.5, TA=0.31, B=27, %163573687  
D=9.040, QC=0.6835, FS=16.8, U=6.6, TA=0.34, B=19, %163574453  
D=9.060, QC=0.6524, FS=14.9, U=6.6, TA=0.34, B=20, %163575562  
D=9.080, QC=0.6228, FS=13.1, U=6.8, TA=0.34, B=21, %163576234  
D=9.100, QC=0.5890, FS=12.9, U=6.8, TA=0.34, B=21, %163577453  
D=9.120, QC=0.6493, FS=15.4, U=6.8, TA=0.34, B=20, %163578218  
D=9.140, QC=0.7178, FS=15.2, U=6.6, TA=0.34, B=20, %163579312  
D=9.160, QC=0.7635, FS=14.8, U=7.0, TA=0.34, B=20, %163580406  
D=9.180, QC=0.9531, FS=14.2, U=6.7, TA=0.34, B=20, %163581187  
D=9.200, QC=1.0752, FS=64.0, U=7.7, TA=0.34, B=19, %163582296  
D=9.220, QC=1.2544, FS=86.1, U=9.2, TA=0.34, B=18, %163583406  
D=9.240, QC=1.3396, FS=98.7, U=11.2, TA=0.34, B=18, %163584500  
D=9.260, QC=1.2985, FS=99.5, U=11.6, TA=0.34, B=18, %163585609  
D=9.280, QC=1.2409, FS=95.2, U=11.6, TA=0.34, B=18, %163586859  
D=9.300, QC=1.2019, FS=98.0, U=11.9, TA=0.34, B=18, %163587515  
D=9.320, QC=1.2959, FS=100.4, U=11.8, TA=0.34, B=18, %163588625  
D=9.340, QC=1.2170, FS=96.1, U=11.5, TA=0.34, B=19, %163589750  
D=9.360, QC=1.0617, FS=90.2, U=11.6, TA=0.34, B=19, %163590968  
D=9.380, QC=1.0554, FS=78.1, U=11.1, TA=0.34, B=19, %163591640  
D=9.400, QC=1.0783, FS=54.6, U=10.1, TA=0.34, B=20, %163592734  
D=9.420, QC=0.9495, FS=40.1, U=9.7, TA=0.34, B=19, %163593937  
D=9.440, QC=0.9386, FS=27.6, U=8.9, TA=0.34, B=19, %163595062  
D=9.460, QC=0.9225, FS=21.5, U=8.5, TA=0.34, B=19, %163595828  
D=9.480, QC=0.8160, FS=22.7, U=8.1, TA=0.34, B=20, %163596921  
D=9.500, QC=0.7298, FS=15.4, U=7.4, TA=0.34, B=19, %163598031  
D=9.520, QC=0.6487, FS=16.7, U=7.3, TA=0.34, B=19, %163598796  
D=9.540, QC=0.5688, FS=15.7, U=7.3, TA=0.34, B=19, %163599890  
D=9.560, QC=0.5625, FS=13.8, U=7.4, TA=0.34, B=20, %163601000  
D=9.580, QC=0.5553, FS=12.4, U=7.4, TA=0.34, B=20, %163601781  
D=9.600, QC=0.5553, FS=12.4, U=7.4, TA=0.34, B=20, %163602875, NA=0.0390, NB=-1.2, NC=10.7, F  
=15, K=90, T=The test are ended without any stop in the ground.

#\$

0:

1:

2:

3:

4:

5:

6:

7:

8:

9:

11:Tilt derivative alarm  
12:Point resistance alarm  
13:Depth unchanged for 5 second  
14:Transmission lost  
15:End of test  
16:Dissipation start

**CPT -4**  
**Raw Data**

\$  
HA=1,HB=4,HC=CPTLOG-2.00,HD=8/18/2020,HG=-1.219,HP=-1.22,HJ=Brenton  
CPT,HK=C4,HM=07,HN=3206,HO=0.00,HQ=SA,HR=0°0'0.000"E,HS=0°0'0.000"N,HX=0.00,HY=0.00  
,HZ=0.00,KQ=1468.00,KF=6200.00,KU=2136.00,MA=0.590,MB=0.011,MC=10.0,MD=150.0,ME=C4,  
MF=0.000  
RN=,CA=0,CB=0

#  
D=0.000, QC=0.0530, FS=4.1, U=1.1, TA=1.29, B=26, %82848281, NA=5.4954, NB=330.6, NC=445.0

D=0.020, QC=0.0530, FS=4.1, U=1.1, TA=1.29, B=26, %82848281

D=0.040, QC=0.0530, FS=3.9, U=0.7, TA=1.08, B=27, %82848937

D=0.060, QC=0.0530, FS=4.0, U=0.7, TA=1.03, B=26, %82849703

D=0.080, QC=0.0509, FS=3.9, U=0.7, TA=1.07, B=26, %82850468

D=0.100, QC=0.0525, FS=4.0, U=0.7, TA=1.09, B=26, %82851234

D=0.120, QC=0.0488, FS=4.0, U=0.7, TA=1.17, B=27, %82852000

D=0.140, QC=0.0473, FS=3.7, U=0.7, TA=1.17, B=27, %82852765

D=0.160, QC=0.0499, FS=3.4, U=0.8, TA=1.15, B=27, %82853531

D=0.180, QC=0.0545, FS=3.3, U=0.8, TA=1.14, B=27, %82854203

D=0.200, QC=0.0561, FS=3.0, U=0.8, TA=1.17, B=27, %82854984

D=0.220, QC=0.0592, FS=3.0, U=0.8, TA=1.17, B=26, %82855765

D=0.240, QC=0.0603, FS=2.9, U=0.9, TA=1.06, B=26, %82856453

D=0.260, QC=0.0623, FS=3.1, U=0.9, TA=1.03, B=26, %82857218

D=0.280, QC=0.0639, FS=3.4, U=0.9, TA=1.05, B=27, %82858015

D=0.300, QC=0.0670, FS=3.6, U=1.0, TA=1.04, B=25, %82858781

D=0.320, QC=0.0680, FS=3.8, U=1.0, TA=0.94, B=27, %82859468

D=0.340, QC=0.0665, FS=3.8, U=1.0, TA=1.04, B=26, %82860234

D=0.360, QC=0.0654, FS=3.8, U=1.1, TA=1.15, B=26, %82861000

D=0.380, QC=0.0628, FS=3.6, U=1.1, TA=1.06, B=25, %82861781

D=0.400, QC=0.0628, FS=3.5, U=1.2, TA=1.13, B=26, %82862453

D=0.420, QC=0.0644, FS=3.4, U=1.2, TA=1.13, B=25, %82863218

D=0.440, QC=0.0665, FS=3.9, U=4.0, TA=0.83, B=17, %82908312

D=0.460, QC=0.0732, FS=3.9, U=4.0, TA=0.90, B=17, %82908640

D=0.480, QC=0.0732, FS=3.8, U=3.7, TA=1.02, B=21, %82909406

D=0.500, QC=0.0758, FS=3.7, U=3.7, TA=1.03, B=21, %82910500

D=0.520, QC=0.0784, FS=3.7, U=3.7, TA=1.03, B=21, %82911265

D=0.540, QC=0.0857, FS=3.7, U=3.8, TA=0.92, B=21, %82912375

D=0.560, QC=0.0893, FS=3.8, U=3.8, TA=0.95, B=21, %82913156

D=0.580, QC=0.0914, FS=3.9, U=3.9, TA=0.97, B=20, %82914265

D=0.600, QC=0.0909, FS=3.9, U=3.9, TA=0.95, B=22, %82915031

D=0.620, QC=0.0919, FS=3.8, U=3.9, TA=1.04, B=20, %82916125

D=0.640, QC=0.0925, FS=4.0, U=4.0, TA=1.03, B=21, %82916921

D=0.660, QC=0.0935, FS=4.2, U=4.1, TA=1.03, B=20, %82918031

D=0.680, QC=0.0976, FS=4.3, U=4.1, TA=1.03, B=20, %82919156

D=0.700, QC=0.1028, FS=4.4, U=4.1, TA=1.04, B=20, %82919828

D=0.720, QC=0.1086, FS=4.6, U=4.3, TA=1.04, B=21, %82921046

D=0.740, QC=0.1080, FS=4.6, U=4.3, TA=1.03, B=20, %82922140

D=0.760, QC=0.1039, FS=4.8, U=4.4, TA=1.03, B=21, %82922906

D=0.780, QC=0.1018, FS=4.6, U=4.5, TA=1.03, B=21, %82924000

D=0.800, QC=0.0961, FS=4.5, U=4.6, TA=1.04, B=21, %82924781

D=0.820, QC=0.0945, FS=4.0, U=4.7, TA=1.03, B=19, %82925875

D=0.840, QC=0.0925, FS=3.4, U=2.5, TA=1.04, B=21, %82926640

D=0.860, QC=0.0836, FS=2.1, U=4.9, TA=1.04, B=21, %82927750  
D=0.880, QC=0.0769, FS=1.3, U=2.8, TA=1.04, B=22, %82928515  
D=0.900, QC=0.0628, FS=0.7, U=2.9, TA=1.04, B=21, %82929609  
D=0.920, QC=0.0603, FS=0.1, U=3.0, TA=1.04, B=21, %82930375  
D=0.940, QC=0.0603, FS=0.7, U=3.1, TA=1.04, B=22, %82931484  
D=0.960, QC=0.0649, FS=0.9, U=3.2, TA=1.04, B=23, %82932250  
D=0.980, QC=0.0815, FS=1.0, U=3.2, TA=1.04, B=22, %82933015  
D=1.000, QC=0.1423, FS=1.0, U=3.3, TA=1.04, B=22, %82934109  
D=1.020, QC=0.1626, FS=0.4, U=3.3, TA=1.04, B=22, %82934875  
D=1.040, QC=0.1470, FS=0.1, U=3.3, TA=1.04, B=22, %82935640  
D=1.060, QC=0.1044, FS=0.2, U=2.7, TA=1.04, B=22, %82936734  
D=1.080, QC=0.0976, FS=0.2, U=0.3, TA=1.04, B=22, %82937500  
D=1.100, QC=0.0976, FS=0.3, U=0.3, TA=1.04, B=21, %82938609  
D=1.120, QC=0.0992, FS=0.5, U=0.5, TA=1.04, B=23, %82939375  
D=1.140, QC=0.1002, FS=0.6, U=0.6, TA=1.04, B=22, %82940140  
D=1.160, QC=0.1065, FS=0.3, U=0.8, TA=1.04, B=23, %82941234  
D=1.180, QC=0.1148, FS=0.2, U=0.9, TA=1.04, B=22, %82942000  
D=1.200, QC=0.1169, FS=0.3, U=1.0, TA=1.04, B=23, %82942765  
D=1.220, QC=0.1153, FS=0.2, U=1.1, TA=1.04, B=21, %82943890  
D=1.240, QC=0.1122, FS=0.2, U=1.2, TA=1.04, B=23, %82944671  
D=1.260, QC=0.1148, FS=0.1, U=1.5, TA=1.04, B=22, %82945781  
D=1.280, QC=0.1174, FS=0.2, U=1.6, TA=1.04, B=22, %82946546  
D=1.300, QC=0.1278, FS=0.3, U=1.8, TA=1.04, B=22, %82947203  
D=1.320, QC=0.1813, FS=0.2, U=1.9, TA=1.04, B=22, %82948437  
D=1.340, QC=0.1860, FS=0.0, U=2.0, TA=1.04, B=22, %82949140  
D=1.360, QC=0.1953, FS=0.6, U=2.1, TA=1.04, B=22, %82949921  
D=1.380, QC=0.2140, FS=1.6, U=2.4, TA=1.04, B=21, %82951031  
D=1.400, QC=0.2592, FS=2.2, U=2.5, TA=1.04, B=22, %82951796  
D=1.420, QC=0.3116, FS=2.9, U=2.6, TA=1.05, B=21, %82952890  
D=1.440, QC=0.2441, FS=2.7, U=2.7, TA=1.05, B=22, %82953656  
D=1.460, QC=0.1984, FS=1.3, U=2.9, TA=1.06, B=21, %82954750  
D=1.480, QC=0.1641, FS=0.8, U=3.1, TA=1.07, B=22, %82955515  
D=1.500, QC=0.2867, FS=0.2, U=3.2, TA=1.07, B=21, %82956296  
D=1.520, QC=0.4773, FS=0.8, U=3.2, TA=1.07, B=21, %82957406  
D=1.540, QC=0.4202, FS=0.3, U=3.4, TA=1.07, B=20, %82958500  
D=1.560, QC=0.3568, FS=0.6, U=3.6, TA=1.07, B=21, %82959265  
D=1.580, QC=0.2514, FS=0.4, U=3.7, TA=1.07, B=21, %82960375  
D=1.600, QC=0.2088, FS=0.5, U=3.9, TA=1.07, B=21, %82961140  
D=1.620, QC=0.2208, FS=0.1, U=4.1, TA=1.05, B=20, %82962250  
D=1.640, QC=0.2878, FS=0.1, U=6.6, TA=0.90, B=24, %83002140  
D=1.660, QC=0.2878, FS=0.1, U=6.6, TA=0.90, B=24, %83002140  
D=1.680, QC=0.2878, FS=0.1, U=6.6, TA=0.90, B=24, %83002140 , F=11  
D=1.700, QC=0.2124, FS=0.5, U=6.2, TA=1.00, B=24, %83003250  
D=1.720, QC=0.2124, FS=0.9, U=6.3, TA=1.00, B=25, %83003687  
D=1.740, QC=0.2057, FS=0.3, U=6.4, TA=0.99, B=23, %83004375  
D=1.760, QC=0.1860, FS=0.7, U=6.5, TA=1.00, B=23, %83005125  
D=1.780, QC=0.1626, FS=1.2, U=6.5, TA=1.00, B=20, %83006250  
D=1.800, QC=0.1948, FS=0.9, U=6.6, TA=1.00, B=14, %83007781  
D=1.820, QC=0.2472, FS=0.3, U=6.8, TA=1.01, B=9, %83009640  
D=1.840, QC=0.2976, FS=1.0, U=6.9, TA=1.00, B=21, %83010406

D=1.860, QC=0.3049, FS=1.5, U=7.0, TA=1.02, B=21, %83011515  
D=1.880, QC=0.2379, FS=0.2, U=7.1, TA=1.01, B=21, %83012281  
D=1.900, QC=0.2000, FS=1.0, U=7.1, TA=1.01, B=21, %83013078  
D=1.920, QC=0.1719, FS=1.1, U=7.1, TA=1.01, B=20, %83014171  
D=1.940, QC=0.1356, FS=0.9, U=7.3, TA=1.00, B=22, %83015281  
D=1.960, QC=0.1782, FS=1.3, U=7.4, TA=1.00, B=23, %83016078  
D=1.980, QC=0.2197, FS=1.2, U=5.2, TA=1.00, B=21, %83016765  
D=2.000, QC=0.2556, FS=0.9, U=5.5, TA=1.01, B=21, %83017953  
D=2.020, QC=0.2867, FS=0.7, U=5.5, TA=1.01, B=21, %83018718  
D=2.040, QC=0.2467, FS=0.5, U=5.6, TA=1.00, B=21, %83019843  
D=2.060, QC=0.2265, FS=0.7, U=5.6, TA=0.82, B=22, %83020515  
D=2.080, QC=0.2135, FS=1.1, U=5.7, TA=0.92, B=22, %83021281  
D=2.100, QC=0.1901, FS=0.8, U=3.7, TA=0.77, B=22, %83022375  
D=2.120, QC=0.1776, FS=1.0, U=6.1, TA=0.86, B=23, %83023156  
D=2.140, QC=0.1558, FS=1.3, U=3.9, TA=0.86, B=23, %83023921  
D=2.160, QC=0.1548, FS=1.5, U=3.9, TA=0.86, B=22, %83024703  
D=2.180, QC=0.1532, FS=1.5, U=4.1, TA=0.86, B=23, %83025796  
D=2.200, QC=0.1595, FS=1.3, U=4.2, TA=0.86, B=24, %83026562  
D=2.220, QC=0.1776, FS=1.1, U=4.3, TA=0.86, B=23, %83027265  
D=2.240, QC=0.2135, FS=0.4, U=4.5, TA=0.86, B=23, %83028453  
D=2.260, QC=0.2618, FS=0.1, U=4.7, TA=0.86, B=23, %83029218  
D=2.280, QC=0.2639, FS=0.2, U=4.7, TA=0.85, B=23, %83029875  
D=2.300, QC=0.2208, FS=0.9, U=4.9, TA=0.86, B=23, %83030671  
D=2.320, QC=0.1880, FS=1.4, U=4.9, TA=0.85, B=22, %83031781  
D=2.340, QC=0.1896, FS=0.8, U=5.0, TA=0.84, B=23, %83032546  
D=2.360, QC=0.1885, FS=0.5, U=5.2, TA=0.84, B=22, %83033328  
D=2.380, QC=0.1969, FS=0.4, U=5.2, TA=0.84, B=23, %83034000  
D=2.400, QC=0.2010, FS=0.2, U=5.5, TA=0.85, B=22, %83035187  
D=2.420, QC=0.2005, FS=0.4, U=5.7, TA=0.84, B=23, %83035859  
D=2.440, QC=0.1927, FS=0.7, U=5.7, TA=0.85, B=23, %83036625  
D=2.460, QC=0.1704, FS=0.1, U=5.7, TA=0.86, B=23, %83037843  
D=2.480, QC=0.1860, FS=0.2, U=5.9, TA=0.86, B=23, %83038531  
D=2.500, QC=0.1979, FS=0.3, U=6.0, TA=0.85, B=23, %83039281  
D=2.520, QC=0.1989, FS=0.4, U=6.1, TA=0.84, B=24, %83040046  
D=2.540, QC=0.1937, FS=0.1, U=6.3, TA=0.86, B=23, %83041140  
D=2.560, QC=0.1922, FS=0.4, U=6.4, TA=0.85, B=22, %83041937  
D=2.580, QC=0.2046, FS=0.5, U=6.5, TA=0.84, B=22, %83042718  
D=2.600, QC=0.2239, FS=0.2, U=6.7, TA=0.86, B=23, %83043812  
D=2.620, QC=0.2223, FS=0.2, U=6.8, TA=0.86, B=22, %83044578  
D=2.640, QC=0.2161, FS=0.0, U=6.9, TA=0.83, B=21, %83045234  
D=2.660, QC=0.2026, FS=0.8, U=7.1, TA=0.81, B=22, %83046437  
D=2.680, QC=0.1901, FS=0.1, U=7.2, TA=0.81, B=24, %83047203  
D=2.700, QC=0.1958, FS=0.0, U=7.3, TA=0.82, B=22, %83047875  
D=2.720, QC=0.2192, FS=0.0, U=7.4, TA=0.83, B=21, %83049078  
D=2.740, QC=0.2197, FS=0.4, U=7.5, TA=0.84, B=22, %83049734  
D=2.760, QC=0.2093, FS=0.7, U=7.7, TA=0.82, B=22, %83050937  
D=2.780, QC=0.2046, FS=0.5, U=7.9, TA=0.81, B=22, %83051703  
D=2.800, QC=0.2057, FS=0.0, U=8.0, TA=0.84, B=21, %83052375  
D=2.820, QC=0.2062, FS=0.1, U=8.1, TA=0.78, B=21, %83053578  
D=2.840, QC=0.2259, FS=2.6, U=9.9, TA=0.85, B=26, %83097328

D=2.860, QC=0.2259, FS=2.6, U=9.9, TA=0.85, B=26, %83097328  
D=2.880, QC=0.2389, FS=2.6, U=9.9, TA=0.85, B=23, %83097765  
D=2.900, QC=0.2275, FS=3.1, U=9.5, TA=0.83, B=23, %83098531  
D=2.920, QC=0.2124, FS=2.9, U=9.5, TA=0.84, B=23, %83099203  
D=2.940, QC=0.2254, FS=2.4, U=7.2, TA=0.82, B=22, %83100343  
D=2.960, QC=0.2867, FS=2.3, U=9.7, TA=0.84, B=21, %83101109  
D=2.980, QC=0.2961, FS=1.4, U=7.2, TA=0.83, B=22, %83101875  
D=3.000, QC=0.2592, FS=2.0, U=7.3, TA=0.84, B=24, %83102640  
D=3.020, QC=0.2249, FS=2.1, U=7.4, TA=0.84, B=22, %83103765  
D=3.040, QC=0.2576, FS=1.9, U=7.4, TA=0.84, B=23, %83104531  
D=3.060, QC=0.3013, FS=2.3, U=7.5, TA=0.86, B=22, %83105625  
D=3.080, QC=0.3293, FS=2.6, U=7.5, TA=0.85, B=22, %83106390  
D=3.100, QC=0.3418, FS=3.0, U=7.7, TA=0.85, B=22, %83107156  
D=3.120, QC=0.2888, FS=4.2, U=7.7, TA=0.84, B=21, %83108265  
D=3.140, QC=0.2389, FS=2.8, U=7.8, TA=0.84, B=22, %83108953  
D=3.160, QC=0.2259, FS=2.4, U=7.8, TA=0.84, B=23, %83109734  
D=3.180, QC=0.2244, FS=2.4, U=5.7, TA=0.84, B=22, %83110828  
D=3.200, QC=0.2363, FS=2.5, U=5.9, TA=0.84, B=22, %83111593  
D=3.220, QC=0.2602, FS=3.0, U=5.9, TA=0.85, B=21, %83112359  
D=3.240, QC=0.2493, FS=2.8, U=5.9, TA=0.85, B=24, %83113125  
D=3.260, QC=0.2244, FS=2.5, U=6.0, TA=0.86, B=23, %83114234  
D=3.280, QC=0.2353, FS=2.3, U=6.1, TA=0.84, B=23, %83115000  
D=3.300, QC=0.3075, FS=1.8, U=6.3, TA=0.85, B=23, %83115765  
D=3.320, QC=0.3927, FS=1.8, U=6.4, TA=0.86, B=24, %83116453  
D=3.340, QC=0.3787, FS=1.6, U=6.4, TA=0.86, B=25, %83117218  
D=3.360, QC=0.3303, FS=3.1, U=6.5, TA=0.86, B=23, %83118343  
D=3.380, QC=0.2743, FS=4.2, U=6.6, TA=0.86, B=24, %83119109  
D=3.400, QC=0.2467, FS=3.2, U=6.7, TA=0.85, B=25, %83119875  
D=3.420, QC=0.2394, FS=2.7, U=6.7, TA=0.84, B=24, %83120640  
D=3.440, QC=0.2493, FS=3.0, U=6.8, TA=0.85, B=25, %83121421  
D=3.460, QC=0.2826, FS=2.9, U=6.9, TA=0.84, B=24, %83122078  
D=3.480, QC=0.3600, FS=3.2, U=7.0, TA=0.84, B=25, %83122859  
D=3.500, QC=0.2945, FS=2.2, U=7.1, TA=0.84, B=25, %83124062  
D=3.520, QC=0.2566, FS=2.9, U=7.1, TA=0.84, B=25, %83124718  
D=3.540, QC=0.2462, FS=1.9, U=7.2, TA=0.88, B=24, %83125484  
D=3.560, QC=0.2488, FS=2.0, U=7.2, TA=0.90, B=24, %83126250  
D=3.580, QC=0.2384, FS=2.4, U=7.4, TA=0.88, B=24, %83127015  
D=3.600, QC=0.2317, FS=2.4, U=7.5, TA=0.89, B=25, %83127781  
D=3.620, QC=0.2249, FS=2.5, U=7.6, TA=0.92, B=24, %83128546  
D=3.640, QC=0.2254, FS=1.4, U=7.7, TA=0.92, B=25, %83129656  
D=3.660, QC=0.2244, FS=0.5, U=7.7, TA=0.93, B=24, %83130421  
D=3.680, QC=0.2223, FS=0.5, U=7.9, TA=0.90, B=25, %83131078  
D=3.700, QC=0.2228, FS=0.6, U=8.0, TA=0.90, B=24, %83131875  
D=3.720, QC=0.2202, FS=0.7, U=8.0, TA=0.92, B=25, %83132640  
D=3.740, QC=0.2218, FS=0.8, U=8.2, TA=0.92, B=24, %83133406  
D=3.760, QC=0.2213, FS=0.7, U=8.2, TA=0.93, B=25, %83134062  
D=3.780, QC=0.2213, FS=0.7, U=8.3, TA=0.94, B=24, %83135296  
D=3.800, QC=0.2208, FS=0.7, U=8.4, TA=0.92, B=25, %83135968  
D=3.820, QC=0.2213, FS=0.7, U=8.5, TA=0.93, B=24, %83136734  
D=3.840, QC=0.2291, FS=0.8, U=8.6, TA=0.94, B=24, %83137500

D=3.860, QC=0.2389, FS=1.0, U=8.7, TA=0.94, B=23, %83138281  
D=3.880, QC=0.2483, FS=1.1, U=8.8, TA=0.93, B=24, %83139046  
D=3.900, QC=0.2478, FS=1.8, U=9.0, TA=0.93, B=23, %83140156  
D=3.920, QC=0.2441, FS=1.8, U=9.0, TA=0.94, B=22, %83140812  
D=3.940, QC=0.2436, FS=1.5, U=9.1, TA=0.94, B=23, %83141593  
D=3.960, QC=0.2405, FS=1.4, U=9.2, TA=0.93, B=24, %83142375  
D=3.980, QC=0.2410, FS=1.5, U=9.4, TA=0.92, B=23, %83143484  
D=4.000, QC=0.2384, FS=1.7, U=9.5, TA=0.93, B=23, %83144187  
D=4.020, QC=0.2374, FS=1.9, U=9.6, TA=0.94, B=22, %83144968  
D=4.040, QC=0.2182, FS=3.3, U=12.6, TA=0.86, B=28, %83207796  
D=4.060, QC=0.2182, FS=3.3, U=12.6, TA=0.86, B=28, %83207796  
D=4.080, QC=0.2182, FS=3.3, U=12.6, TA=0.86, B=28, %83207796  
D=4.100, QC=0.2265, FS=3.3, U=12.6, TA=0.86, B=25, %83208125  
D=4.120, QC=0.2249, FS=3.0, U=12.1, TA=0.92, B=27, %83208906  
D=4.140, QC=0.2285, FS=2.8, U=12.2, TA=0.93, B=24, %83209671  
D=4.160, QC=0.2296, FS=2.6, U=12.2, TA=0.92, B=24, %83210437  
D=4.180, QC=0.2337, FS=2.4, U=12.2, TA=0.94, B=26, %83211093  
D=4.200, QC=0.2343, FS=2.4, U=12.4, TA=0.94, B=22, %83212296  
D=4.220, QC=0.2358, FS=2.3, U=12.5, TA=0.93, B=23, %83213062  
D=4.240, QC=0.2467, FS=2.4, U=12.6, TA=0.93, B=21, %83213828  
D=4.260, QC=0.2737, FS=2.1, U=12.6, TA=0.94, B=21, %83214875  
D=4.280, QC=0.2800, FS=2.1, U=12.6, TA=0.93, B=21, %83215656  
D=4.300, QC=0.2659, FS=2.3, U=12.7, TA=0.93, B=21, %83216765  
D=4.320, QC=0.2587, FS=2.1, U=12.8, TA=0.94, B=20, %83217515  
D=4.340, QC=0.2524, FS=2.3, U=12.8, TA=0.94, B=22, %83218609  
D=4.360, QC=0.2524, FS=2.1, U=12.9, TA=0.95, B=22, %83219390  
D=4.380, QC=0.2556, FS=2.8, U=13.0, TA=0.98, B=22, %83220484  
D=4.400, QC=0.2566, FS=2.9, U=13.1, TA=0.99, B=21, %83221265  
D=4.420, QC=0.2566, FS=3.0, U=13.2, TA=1.02, B=22, %83222015  
D=4.440, QC=0.2613, FS=3.0, U=13.2, TA=1.03, B=22, %83223125  
D=4.460, QC=0.2649, FS=3.3, U=13.4, TA=1.05, B=22, %83223906  
D=4.480, QC=0.2628, FS=3.5, U=13.5, TA=1.04, B=22, %83224671  
D=4.500, QC=0.2659, FS=3.5, U=13.6, TA=1.04, B=23, %83225765  
D=4.520, QC=0.2685, FS=3.6, U=13.7, TA=1.05, B=24, %83226531  
D=4.540, QC=0.2701, FS=3.6, U=13.9, TA=1.05, B=24, %83227312  
D=4.560, QC=0.2753, FS=3.8, U=13.9, TA=1.05, B=23, %83227984  
D=4.580, QC=0.5817, FS=4.5, U=13.9, TA=1.04, B=24, %83229093  
D=4.600, QC=0.7573, FS=5.2, U=13.8, TA=1.05, B=23, %83229906  
D=4.620, QC=0.5464, FS=4.1, U=14.0, TA=1.05, B=23, %83230687  
D=4.640, QC=0.3922, FS=8.4, U=14.1, TA=1.05, B=23, %83231406  
D=4.660, QC=0.3423, FS=9.7, U=12.1, TA=1.05, B=23, %83232500  
D=4.680, QC=0.3366, FS=9.7, U=12.3, TA=1.05, B=23, %83233296  
D=4.700, QC=0.3272, FS=10.3, U=12.4, TA=1.05, B=24, %83234062  
D=4.720, QC=0.3205, FS=10.7, U=12.4, TA=1.05, B=24, %83234718  
D=4.740, QC=0.2992, FS=11.5, U=12.5, TA=1.05, B=24, %83235921  
D=4.760, QC=0.2929, FS=10.0, U=12.6, TA=1.05, B=23, %83236687  
D=4.780, QC=0.2872, FS=7.7, U=12.6, TA=1.05, B=23, %83237453  
D=4.800, QC=0.2826, FS=6.6, U=12.7, TA=1.05, B=23, %83238109  
D=4.820, QC=0.2794, FS=5.9, U=13.0, TA=1.05, B=24, %83239234  
D=4.840, QC=0.2789, FS=5.6, U=13.0, TA=1.05, B=23, %83240000



D=4.860, QC=0.2784, FS=5.4, U=13.1, TA=1.05, B=23, %83240765  
D=4.880, QC=0.2763, FS=5.3, U=13.2, TA=1.05, B=24, %83241546  
D=4.900, QC=0.2727, FS=5.2, U=11.0, TA=1.05, B=23, %83242312  
D=4.920, QC=0.2727, FS=5.0, U=13.4, TA=1.05, B=23, %83243421  
D=4.940, QC=0.2758, FS=4.9, U=13.5, TA=1.05, B=24, %83244093  
D=4.960, QC=0.2711, FS=5.0, U=11.3, TA=1.05, B=23, %83244859  
D=4.980, QC=0.2784, FS=4.7, U=13.7, TA=1.05, B=23, %83246062  
D=5.000, QC=0.2727, FS=4.8, U=11.6, TA=1.05, B=23, %83246718  
D=5.020, QC=0.2727, FS=4.6, U=11.7, TA=1.05, B=22, %83247484  
D=5.040, QC=0.2784, FS=4.6, U=11.8, TA=1.05, B=21, %83248687  
D=5.060, QC=0.2815, FS=4.4, U=11.9, TA=1.05, B=21, %83249343  
D=5.080, QC=0.2831, FS=4.3, U=12.0, TA=1.05, B=22, %83250109  
D=5.100, QC=0.2862, FS=4.4, U=12.1, TA=1.05, B=21, %83251250  
D=5.120, QC=0.2862, FS=4.5, U=12.2, TA=1.05, B=20, %83252359  
D=5.140, QC=0.2836, FS=4.5, U=12.3, TA=1.05, B=20, %83253125  
D=5.160, QC=0.2800, FS=4.8, U=12.4, TA=1.05, B=20, %83254218  
D=5.180, QC=0.2789, FS=4.9, U=12.6, TA=1.05, B=20, %83255031  
D=5.200, QC=0.2753, FS=5.0, U=12.6, TA=1.05, B=19, %83256156  
D=5.220, QC=0.2800, FS=3.3, U=12.7, TA=0.97, B=17, %83257250  
D=5.240, QC=0.2940, FS=5.7, U=17.5, TA=1.04, B=22, %83301046  
D=5.260, QC=0.2940, FS=5.7, U=17.5, TA=1.04, B=22, %83301046  
D=5.280, QC=0.3039, FS=5.7, U=17.1, TA=1.05, B=22, %83301703  
D=5.300, QC=0.3075, FS=5.6, U=17.2, TA=1.05, B=23, %83302484  
D=5.320, QC=0.3075, FS=5.7, U=17.2, TA=1.05, B=21, %83303671  
D=5.340, QC=0.3049, FS=5.9, U=17.1, TA=1.05, B=22, %83304437  
D=5.360, QC=0.3044, FS=6.2, U=17.3, TA=1.05, B=22, %83305546  
D=5.380, QC=0.3028, FS=6.3, U=17.3, TA=1.05, B=22, %83306218  
D=5.400, QC=0.3039, FS=6.2, U=17.4, TA=1.05, B=21, %83307421  
D=5.420, QC=0.3168, FS=6.2, U=17.5, TA=1.05, B=21, %83308187  
D=5.440, QC=0.3252, FS=6.5, U=17.6, TA=1.05, B=20, %83309296  
D=5.460, QC=0.3392, FS=6.6, U=17.6, TA=1.05, B=21, %83309968  
D=5.480, QC=0.3620, FS=6.6, U=17.7, TA=1.05, B=20, %83311078  
D=5.500, QC=0.3594, FS=6.9, U=17.7, TA=1.05, B=21, %83311843  
D=5.520, QC=0.3589, FS=7.7, U=17.8, TA=1.05, B=21, %83312984  
D=5.540, QC=0.3501, FS=8.3, U=18.0, TA=1.05, B=22, %83313765  
D=5.560, QC=0.3355, FS=8.7, U=18.1, TA=1.05, B=21, %83314875  
D=5.580, QC=0.3335, FS=9.2, U=18.2, TA=1.05, B=22, %83315640  
D=5.600, QC=0.3371, FS=9.1, U=18.3, TA=1.05, B=21, %83316750  
D=5.620, QC=0.3444, FS=9.2, U=18.4, TA=1.05, B=22, %83317531  
D=5.640, QC=0.3475, FS=9.0, U=18.4, TA=1.05, B=21, %83318296  
D=5.660, QC=0.3568, FS=8.4, U=18.5, TA=1.05, B=22, %83319390  
D=5.680, QC=0.3584, FS=8.0, U=18.6, TA=1.05, B=21, %83320156  
D=5.700, QC=0.3605, FS=7.7, U=18.8, TA=1.05, B=23, %83321250  
D=5.720, QC=0.3516, FS=7.8, U=18.9, TA=1.05, B=23, %83322046  
D=5.740, QC=0.3449, FS=7.2, U=18.9, TA=1.05, B=23, %83322781  
D=5.760, QC=0.3387, FS=7.2, U=19.1, TA=1.05, B=22, %83323546  
D=5.780, QC=0.3168, FS=7.4, U=19.1, TA=1.05, B=24, %83324671  
D=5.800, QC=0.3137, FS=7.5, U=19.2, TA=1.05, B=23, %83325343  
D=5.820, QC=0.3065, FS=7.5, U=19.2, TA=1.05, B=24, %83326140  
D=5.840, QC=0.3002, FS=7.3, U=19.3, TA=1.05, B=22, %83327218

D=5.860, QC=0.2987, FS=7.3, U=19.5, TA=1.05, B=23, %83327984  
D=5.880, QC=0.2981, FS=7.0, U=19.5, TA=1.05, B=22, %83328765  
D=5.900, QC=0.2981, FS=6.6, U=19.6, TA=1.05, B=24, %83329515  
D=5.920, QC=0.2981, FS=6.4, U=19.7, TA=1.05, B=23, %83330609  
D=5.940, QC=0.3013, FS=6.3, U=19.7, TA=1.05, B=23, %83331390  
D=5.960, QC=0.2976, FS=5.8, U=19.7, TA=1.05, B=23, %83332140  
D=5.980, QC=0.2961, FS=5.4, U=19.9, TA=1.05, B=22, %83333234  
D=6.000, QC=0.2971, FS=5.3, U=20.0, TA=1.05, B=22, %83334031  
D=6.020, QC=0.2950, FS=5.2, U=20.0, TA=1.06, B=23, %83334781  
D=6.040, QC=0.2888, FS=5.2, U=20.1, TA=1.05, B=22, %83335906  
D=6.060, QC=0.2857, FS=5.1, U=20.2, TA=1.05, B=22, %83336656  
D=6.080, QC=0.2836, FS=5.2, U=20.3, TA=1.05, B=23, %83337421  
D=6.100, QC=0.2831, FS=5.1, U=20.3, TA=1.05, B=23, %83338187  
D=6.120, QC=0.2852, FS=4.9, U=20.4, TA=1.05, B=22, %83339296  
D=6.140, QC=0.2862, FS=4.8, U=20.5, TA=1.05, B=23, %83340062  
D=6.160, QC=0.2904, FS=4.7, U=20.6, TA=1.05, B=22, %83341203  
D=6.180, QC=0.2929, FS=4.7, U=20.6, TA=1.05, B=23, %83341859  
D=6.200, QC=0.2950, FS=4.4, U=20.6, TA=1.05, B=22, %83342640  
D=6.220, QC=0.2950, FS=4.4, U=20.7, TA=1.05, B=21, %83343718  
D=6.240, QC=0.2914, FS=4.5, U=18.6, TA=1.05, B=21, %83344500  
D=6.260, QC=0.2955, FS=4.4, U=21.0, TA=1.05, B=22, %83345265  
D=6.280, QC=0.2955, FS=4.5, U=21.0, TA=1.05, B=22, %83346375  
D=6.300, QC=0.2919, FS=4.4, U=21.1, TA=1.05, B=21, %83347140  
D=6.320, QC=0.2883, FS=4.5, U=21.2, TA=1.06, B=21, %83348234  
D=6.340, QC=0.2867, FS=4.6, U=21.3, TA=1.05, B=22, %83349000  
D=6.360, QC=0.2904, FS=4.6, U=21.3, TA=1.05, B=21, %83350093  
D=6.380, QC=0.2826, FS=4.4, U=21.3, TA=1.05, B=21, %83350859  
D=6.400, QC=0.2810, FS=3.1, U=21.6, TA=1.05, B=20, %83351984 , F=11  
D=6.420, QC=0.2940, FS=4.7, U=23.3, TA=1.13, B=22, %83393500  
D=6.440, QC=0.2940, FS=4.7, U=23.3, TA=1.13, B=22, %83393500  
D=6.460, QC=0.2940, FS=4.7, U=23.3, TA=1.13, B=22, %83393500  
D=6.480, QC=0.2924, FS=4.8, U=22.9, TA=1.12, B=18, %83394593  
D=6.500, QC=0.2914, FS=4.7, U=20.4, TA=1.10, B=23, %83395359  
D=6.520, QC=0.2919, FS=4.5, U=23.0, TA=1.12, B=21, %83396468  
D=6.540, QC=0.2909, FS=4.5, U=20.5, TA=1.12, B=23, %83397234  
D=6.560, QC=0.2904, FS=4.4, U=20.6, TA=1.10, B=23, %83398359  
D=6.580, QC=0.2904, FS=4.5, U=20.7, TA=1.13, B=23, %83399125  
D=6.600, QC=0.2878, FS=4.7, U=23.2, TA=1.13, B=22, %83399921  
D=6.620, QC=0.2841, FS=4.7, U=20.7, TA=1.15, B=2, %83393171  
D=6.640, QC=0.3023, FS=4.6, U=20.8, TA=1.13, B=21, %83401781  
D=6.660, QC=0.3376, FS=5.1, U=20.8, TA=1.13, B=22, %83402890  
D=6.680, QC=0.3122, FS=4.6, U=20.5, TA=1.12, B=21, %83403656  
D=6.700, QC=0.3065, FS=5.5, U=19.6, TA=1.13, B=22, %83404359  
D=6.720, QC=0.2893, FS=5.6, U=19.7, TA=1.13, B=22, %83405546  
D=6.740, QC=0.2950, FS=5.3, U=22.3, TA=1.13, B=23, %83406203  
D=6.760, QC=0.2831, FS=5.1, U=22.4, TA=1.12, B=22, %83407421  
D=6.780, QC=0.2852, FS=4.5, U=22.5, TA=1.13, B=21, %83408125  
D=6.800, QC=0.2914, FS=4.3, U=20.1, TA=1.13, B=22, %83408890  
D=6.820, QC=0.2862, FS=4.2, U=20.1, TA=1.13, B=23, %83409984  
D=6.840, QC=0.2831, FS=3.9, U=20.1, TA=1.14, B=23, %83410750

D=6.860, QC=0.2794, FS=3.7, U=20.2, TA=1.14, B=24, %83411515  
D=6.880, QC=0.2831, FS=3.0, U=20.2, TA=1.15, B=22, %83412281  
D=6.900, QC=0.2893, FS=3.0, U=20.3, TA=1.14, B=24, %83413390  
D=6.920, QC=0.2961, FS=3.0, U=20.3, TA=1.15, B=24, %83414156  
D=6.940, QC=0.2945, FS=3.0, U=20.5, TA=1.15, B=24, %83414828  
D=6.960, QC=0.3028, FS=3.3, U=20.5, TA=1.15, B=23, %83415593  
D=6.980, QC=0.3470, FS=3.1, U=20.6, TA=1.13, B=25, %83416796  
D=7.000, QC=0.3911, FS=3.4, U=20.6, TA=1.13, B=23, %83417453  
D=7.020, QC=0.4420, FS=4.2, U=20.5, TA=1.14, B=23, %83418218  
D=7.040, QC=0.4503, FS=3.9, U=20.7, TA=1.14, B=23, %83419031  
D=7.060, QC=0.3880, FS=4.3, U=20.8, TA=1.13, B=24, %83419796  
D=7.080, QC=0.3444, FS=7.1, U=21.1, TA=1.14, B=24, %83420890  
D=7.100, QC=0.3210, FS=6.0, U=21.1, TA=1.14, B=23, %83421656  
D=7.120, QC=0.3226, FS=4.9, U=21.1, TA=1.15, B=24, %83422312  
D=7.140, QC=0.3283, FS=4.4, U=21.2, TA=1.14, B=24, %83423125  
D=7.160, QC=0.3329, FS=4.4, U=21.2, TA=1.13, B=24, %83423906  
D=7.180, QC=0.3335, FS=4.6, U=21.2, TA=1.13, B=23, %83425000  
D=7.200, QC=0.3397, FS=3.9, U=21.3, TA=1.13, B=23, %83425796  
D=7.220, QC=0.3490, FS=3.3, U=21.4, TA=1.13, B=24, %83426453  
D=7.240, QC=0.3480, FS=3.7, U=21.5, TA=1.13, B=24, %83427234  
D=7.260, QC=0.3454, FS=4.0, U=21.6, TA=1.13, B=25, %83428000  
D=7.280, QC=0.3387, FS=4.6, U=21.7, TA=1.13, B=23, %83429093  
D=7.300, QC=0.3293, FS=3.9, U=21.7, TA=1.13, B=24, %83429859  
D=7.320, QC=0.3298, FS=3.7, U=21.8, TA=1.13, B=23, %83430640  
D=7.340, QC=0.3418, FS=3.8, U=21.9, TA=1.13, B=24, %83431406  
D=7.360, QC=0.3693, FS=3.9, U=22.0, TA=1.15, B=23, %83432062  
D=7.380, QC=0.3776, FS=4.2, U=22.1, TA=1.14, B=24, %83433265  
D=7.400, QC=0.3662, FS=5.5, U=22.1, TA=1.14, B=23, %83434046  
D=7.420, QC=0.3522, FS=5.9, U=22.2, TA=1.13, B=23, %83434703  
D=7.440, QC=0.3433, FS=5.5, U=22.2, TA=1.14, B=23, %83435812  
D=7.460, QC=0.3490, FS=5.0, U=22.4, TA=1.13, B=24, %83436625  
D=7.480, QC=0.3542, FS=4.7, U=22.5, TA=1.13, B=23, %83437390  
D=7.500, QC=0.3667, FS=4.7, U=22.5, TA=1.13, B=23, %83438156  
D=7.520, QC=0.3387, FS=5.0, U=22.5, TA=1.13, B=22, %83439281  
D=7.540, QC=0.3781, FS=4.9, U=22.6, TA=1.13, B=23, %83439937  
D=7.560, QC=0.4477, FS=5.3, U=22.6, TA=1.13, B=22, %83440734  
D=7.580, QC=0.5293, FS=6.2, U=22.8, TA=1.13, B=21, %83441843  
D=7.600, QC=0.5205, FS=7.5, U=22.8, TA=1.13, B=21, %83442625  
D=7.620, QC=0.3854, FS=8.0, U=25.8, TA=1.15, B=25, %83481812  
D=7.640, QC=0.3854, FS=8.0, U=25.8, TA=1.15, B=25, %83481812  
D=7.660, QC=0.3901, FS=8.0, U=25.8, TA=1.15, B=27, %83482140  
D=7.680, QC=0.3750, FS=6.7, U=25.3, TA=1.15, B=26, %83482921  
D=7.700, QC=0.3496, FS=6.2, U=25.3, TA=1.15, B=25, %83483687  
D=7.720, QC=0.3454, FS=6.4, U=25.4, TA=1.15, B=22, %83484375  
D=7.740, QC=0.3449, FS=6.2, U=25.4, TA=1.15, B=21, %83485125  
D=7.760, QC=0.3605, FS=5.2, U=25.4, TA=1.15, B=22, %83486250  
D=7.780, QC=0.3662, FS=5.0, U=25.5, TA=1.15, B=23, %83487015  
D=7.800, QC=0.3880, FS=4.8, U=25.6, TA=1.15, B=23, %83487781  
D=7.820, QC=0.4820, FS=4.7, U=25.6, TA=1.15, B=22, %83488875  
D=7.840, QC=0.4659, FS=4.9, U=25.6, TA=1.15, B=21, %83489640

D=7.860, QC=0.4010, FS=5.3, U=25.7, TA=1.15, B=22, %83490734  
D=7.880, QC=0.3615, FS=5.0, U=25.8, TA=1.15, B=23, %83491515  
D=7.900, QC=0.3610, FS=5.2, U=25.9, TA=1.15, B=21, %83492296  
D=7.920, QC=0.3631, FS=4.8, U=26.0, TA=1.15, B=21, %83493390  
D=7.940, QC=0.3610, FS=4.9, U=26.0, TA=1.15, B=22, %83494156  
D=7.960, QC=0.3646, FS=4.9, U=26.1, TA=1.15, B=23, %83494921  
D=7.980, QC=0.3714, FS=5.0, U=26.2, TA=1.15, B=23, %83496015  
D=8.000, QC=0.3906, FS=4.2, U=26.2, TA=1.15, B=21, %83496781  
D=8.020, QC=0.6685, FS=5.1, U=26.3, TA=1.15, B=23, %83497890  
D=8.040, QC=1.0321, FS=7.2, U=25.8, TA=1.15, B=22, %83498656  
D=8.060, QC=1.0357, FS=20.6, U=26.5, TA=1.15, B=23, %83499421  
D=8.080, QC=1.0030, FS=16.3, U=27.2, TA=1.15, B=22, %83500515  
D=8.100, QC=0.9713, FS=21.8, U=27.2, TA=1.17, B=22, %83501281  
D=8.120, QC=0.8913, FS=27.0, U=27.5, TA=1.25, B=24, %83502046  
D=8.140, QC=0.9443, FS=39.0, U=29.0, TA=1.25, B=23, %83502812  
D=8.160, QC=1.0773, FS=54.3, U=31.3, TA=1.25, B=22, %83503906  
D=8.180, QC=1.0580, FS=69.1, U=32.8, TA=1.25, B=21, %83504671  
D=8.200, QC=0.9116, FS=54.3, U=32.3, TA=1.25, B=24, %83505437  
D=8.220, QC=0.8233, FS=21.9, U=27.8, TA=1.26, B=24, %83506546  
D=8.240, QC=0.7152, FS=20.8, U=27.3, TA=1.26, B=23, %83507218  
D=8.260, QC=0.5594, FS=20.8, U=27.1, TA=1.26, B=23, %83508000  
D=8.280, QC=0.4950, FS=20.6, U=27.2, TA=1.26, B=23, %83508781  
D=8.300, QC=0.4846, FS=20.9, U=27.2, TA=1.26, B=24, %83509546  
D=8.320, QC=0.4067, FS=18.9, U=27.2, TA=1.26, B=23, %83510640  
D=8.340, QC=0.4155, FS=19.0, U=27.4, TA=1.26, B=23, %83511421  
D=8.360, QC=0.4763, FS=18.6, U=27.5, TA=1.26, B=24, %83512187  
D=8.380, QC=0.5054, FS=16.2, U=27.5, TA=1.26, B=23, %83512843  
D=8.400, QC=0.5132, FS=11.4, U=27.6, TA=1.26, B=23, %83513953  
D=8.420, QC=0.5272, FS=11.4, U=27.6, TA=1.26, B=24, %83514718  
D=8.440, QC=0.5599, FS=11.6, U=27.7, TA=1.26, B=24, %83515484  
D=8.460, QC=0.5859, FS=12.9, U=27.8, TA=1.26, B=23, %83516265  
D=8.480, QC=0.5859, FS=13.3, U=28.1, TA=1.26, B=23, %83517375  
D=8.500, QC=0.5153, FS=13.5, U=28.0, TA=1.26, B=23, %83518140  
D=8.520, QC=0.5553, FS=16.0, U=28.0, TA=1.26, B=24, %83518906  
D=8.540, QC=0.5662, FS=16.5, U=28.0, TA=1.26, B=23, %83519671  
D=8.560, QC=0.7069, FS=16.1, U=28.2, TA=1.26, B=22, %83520765  
D=8.580, QC=0.7796, FS=15.5, U=28.2, TA=1.26, B=22, %83521531  
D=8.600, QC=0.6410, FS=15.3, U=28.2, TA=1.26, B=23, %83522296  
D=8.620, QC=0.4592, FS=15.1, U=28.2, TA=1.26, B=23, %83523406  
D=8.640, QC=0.4327, FS=14.6, U=28.2, TA=1.26, B=22, %83524187  
D=8.660, QC=0.4244, FS=13.6, U=28.2, TA=1.26, B=22, %83524875  
D=8.680, QC=0.4238, FS=13.7, U=28.3, TA=1.26, B=21, %83525984  
D=8.700, QC=0.4249, FS=13.5, U=28.4, TA=1.26, B=22, %83526750  
D=8.720, QC=0.4238, FS=13.5, U=28.4, TA=1.26, B=21, %83527859  
D=8.740, QC=0.4176, FS=12.7, U=28.5, TA=1.26, B=21, %83528625  
D=8.760, QC=0.4150, FS=10.6, U=28.5, TA=1.26, B=22, %83529406  
D=8.780, QC=0.4119, FS=9.0, U=28.6, TA=1.26, B=22, %83530500  
D=8.800, QC=0.4114, FS=9.0, U=28.6, TA=1.26, B=21, %83531265  
D=8.820, QC=0.4155, FS=10.9, U=33.3, TA=1.25, B=24, %83579984  
D=8.840, QC=0.4155, FS=10.9, U=33.3, TA=1.25, B=24, %83579984

D=8.860, QC=0.4155, FS=10.9, U=33.3, TA=1.25, B=24, %83579984  
D=8.880, QC=0.4399, FS=11.5, U=32.9, TA=1.26, B=23, %83580750  
D=8.900, QC=0.4721, FS=11.8, U=33.0, TA=1.26, B=21, %83581515  
D=8.920, QC=0.4799, FS=12.4, U=33.0, TA=1.26, B=22, %83582281  
D=8.940, QC=0.4322, FS=12.6, U=33.1, TA=1.26, B=20, %83583390  
D=8.960, QC=0.4285, FS=12.9, U=33.2, TA=1.26, B=21, %83584156  
D=8.980, QC=0.4171, FS=12.8, U=33.3, TA=1.26, B=21, %83585250  
D=9.000, QC=0.4109, FS=12.5, U=33.3, TA=1.26, B=21, %83586015  
D=9.020, QC=0.4238, FS=12.7, U=33.4, TA=1.26, B=20, %83587109  
D=9.040, QC=0.4384, FS=12.4, U=33.4, TA=1.26, B=21, %83587875  
D=9.060, QC=0.4768, FS=12.0, U=33.6, TA=1.26, B=20, %83589078  
D=9.080, QC=0.5656, FS=11.9, U=33.7, TA=1.26, B=21, %83589765  
D=9.100, QC=0.8061, FS=12.4, U=33.7, TA=1.26, B=21, %83590875  
D=9.120, QC=0.7609, FS=13.7, U=33.7, TA=1.26, B=22, %83591640  
D=9.140, QC=0.6046, FS=14.6, U=33.9, TA=1.26, B=22, %83592750  
D=9.160, QC=0.4763, FS=13.7, U=33.8, TA=1.26, B=23, %83593515  
D=9.180, QC=0.4763, FS=13.5, U=33.9, TA=1.26, B=22, %83594625  
D=9.200, QC=0.4945, FS=13.3, U=33.9, TA=1.26, B=21, %83595390  
D=9.220, QC=0.7428, FS=13.3, U=34.0, TA=1.26, B=22, %83596171  
D=9.240, QC=1.0347, FS=29.6, U=34.9, TA=1.26, B=23, %83597265  
D=9.260, QC=1.0399, FS=23.7, U=36.4, TA=1.26, B=23, %83598031  
D=9.280, QC=0.8747, FS=11.7, U=35.4, TA=1.26, B=23, %83598843  
D=9.300, QC=0.8041, FS=15.9, U=34.7, TA=1.26, B=22, %83599937  
D=9.320, QC=0.8918, FS=20.5, U=34.6, TA=1.26, B=25, %83600703  
D=9.340, QC=0.8783, FS=21.3, U=34.5, TA=1.26, B=23, %83601406  
D=9.360, QC=0.8337, FS=22.6, U=34.4, TA=1.27, B=24, %83602156  
D=9.380, QC=0.8929, FS=26.8, U=34.3, TA=1.26, B=23, %83603250  
D=9.400, QC=1.0014, FS=38.2, U=36.1, TA=1.26, B=24, %83604031  
D=9.420, QC=0.9755, FS=38.6, U=36.8, TA=1.27, B=23, %83604796  
D=9.440, QC=1.0243, FS=49.0, U=38.1, TA=1.27, B=24, %83605562  
D=9.460, QC=1.0523, FS=51.5, U=38.7, TA=1.27, B=23, %83606328  
D=9.480, QC=0.9905, FS=46.7, U=38.9, TA=1.28, B=23, %83607421  
D=9.500, QC=0.9661, FS=39.4, U=38.4, TA=1.27, B=23, %83608234  
D=9.520, QC=1.0305, FS=35.9, U=37.6, TA=1.28, B=25, %83608906  
D=9.540, QC=1.1006, FS=42.2, U=36.3, TA=1.28, B=23, %83609671  
D=9.560, QC=1.1817, FS=84.1, U=41.9, TA=1.29, B=24, %83610812  
D=9.580, QC=1.2710, FS=89.6, U=43.3, TA=1.28, B=23, %83611578  
D=9.600, QC=1.3629, FS=89.3, U=44.0, TA=1.28, B=23, %83612343  
D=9.620, QC=1.1941, FS=86.3, U=44.1, TA=1.28, B=22, %83613453  
D=9.640, QC=1.0144, FS=80.2, U=44.0, TA=1.29, B=23, %83614140  
D=9.660, QC=0.9661, FS=63.0, U=43.7, TA=1.33, B=23, %83614921  
D=9.680, QC=0.9485, FS=45.0, U=42.4, TA=1.35, B=25, %83615687  
D=9.700, QC=0.9313, FS=20.4, U=38.7, TA=1.35, B=23, %83616781  
D=9.720, QC=0.8794, FS=14.9, U=36.7, TA=1.37, B=24, %83617546  
D=9.740, QC=0.7760, FS=11.9, U=35.6, TA=1.38, B=23, %83618328  
D=9.760, QC=0.6758, FS=11.6, U=35.1, TA=1.40, B=24, %83619015  
D=9.780, QC=0.5771, FS=12.9, U=35.2, TA=1.41, B=23, %83620203  
D=9.800, QC=0.5573, FS=14.0, U=35.2, TA=1.41, B=24, %83620859  
D=9.820, QC=0.5236, FS=12.4, U=35.2, TA=1.42, B=23, %83621656  
D=9.840, QC=0.4934, FS=12.0, U=35.3, TA=1.41, B=23, %83622406

D=9.860, QC=0.4831, FS=11.2, U=35.3, TA=1.41, B=23, %83623171  
D=9.880, QC=0.4882, FS=7.1, U=35.4, TA=1.42, B=23, %83624281  
D=9.900, QC=0.4940, FS=5.9, U=35.6, TA=1.42, B=23, %83625046  
D=9.920, QC=0.4966, FS=5.7, U=35.7, TA=1.43, B=23, %83625828  
D=9.940, QC=0.5064, FS=6.5, U=35.8, TA=1.43, B=22, %83626921  
D=9.960, QC=0.5028, FS=7.3, U=35.8, TA=1.43, B=23, %83627687  
D=9.980, QC=0.4986, FS=7.7, U=35.9, TA=1.43, B=23, %83628468  
D=10.000, QC=0.4924, FS=7.6, U=36.1, TA=1.43, B=23, %83629578  
D=10.020, QC=0.4799, FS=12.7, U=41.9, TA=1.32, B=21, %83672156  
D=10.040, QC=0.4799, FS=12.7, U=41.9, TA=1.32, B=21, %83672156  
D=10.060, QC=0.4820, FS=12.7, U=41.9, TA=1.37, B=21, %83672484  
D=10.080, QC=0.4831, FS=13.0, U=41.6, TA=1.42, B=19, %83673593  
D=10.100, QC=0.4768, FS=13.6, U=41.7, TA=1.42, B=18, %83674375  
D=10.120, QC=0.4721, FS=13.6, U=41.7, TA=1.43, B=19, %83675468  
D=10.140, QC=0.4706, FS=12.8, U=41.9, TA=1.43, B=20, %83676671  
D=10.160, QC=0.4784, FS=12.7, U=42.0, TA=1.43, B=18, %83677781  
D=10.180, QC=0.4888, FS=12.1, U=42.1, TA=1.43, B=18, %83678453  
D=10.200, QC=0.4888, FS=11.7, U=42.4, TA=1.43, B=19, %83679671  
D=10.220, QC=0.4799, FS=11.2, U=42.4, TA=1.43, B=20, %83680765  
D=10.240, QC=0.4831, FS=10.5, U=42.6, TA=1.43, B=18, %83681546  
D=10.260, QC=0.4799, FS=9.8, U=42.8, TA=1.43, B=18, %83682640  
D=10.280, QC=0.4690, FS=9.7, U=42.9, TA=1.43, B=18, %83683734  
D=10.300, QC=0.4675, FS=9.9, U=43.1, TA=1.43, B=19, %83684828  
D=10.320, QC=0.4623, FS=10.2, U=43.2, TA=1.43, B=18, %83686031  
D=10.340, QC=0.4592, FS=10.7, U=43.5, TA=1.43, B=18, %83687140  
D=10.360, QC=0.4592, FS=10.8, U=43.7, TA=1.43, B=19, %83687828  
D=10.380, QC=0.4633, FS=11.1, U=43.6, TA=1.43, B=20, %83689031  
D=10.400, QC=0.4638, FS=11.5, U=43.9, TA=1.43, B=18, %83690125  
D=10.420, QC=0.4675, FS=11.2, U=44.1, TA=1.43, B=18, %83691218  
D=10.440, QC=0.4690, FS=10.6, U=44.2, TA=1.43, B=19, %83692421  
D=10.460, QC=0.4685, FS=10.1, U=44.4, TA=1.43, B=19, %83693187  
D=10.480, QC=0.4742, FS=10.3, U=44.6, TA=1.43, B=19, %83694281  
D=10.500, QC=0.4825, FS=9.8, U=44.8, TA=1.43, B=18, %83695375  
D=10.520, QC=0.4940, FS=10.0, U=45.0, TA=1.43, B=19, %83696468  
D=10.540, QC=0.4955, FS=9.9, U=45.1, TA=1.43, B=21, %83697250  
D=10.560, QC=0.4981, FS=11.2, U=45.3, TA=1.43, B=21, %83698359  
D=10.580, QC=0.4981, FS=11.8, U=45.5, TA=1.43, B=21, %83699156  
D=10.600, QC=0.5324, FS=12.6, U=45.6, TA=1.43, B=21, %83700250  
D=10.620, QC=0.9147, FS=14.5, U=45.8, TA=1.43, B=23, %83701015  
D=10.640, QC=1.0653, FS=26.5, U=47.2, TA=1.43, B=21, %83701781  
D=10.660, QC=0.9796, FS=19.0, U=48.6, TA=1.43, B=21, %83702890  
D=10.680, QC=0.9464, FS=15.9, U=46.9, TA=1.43, B=21, %83703671  
D=10.700, QC=0.6950, FS=22.9, U=46.4, TA=1.43, B=22, %83704765  
D=10.720, QC=0.6389, FS=25.5, U=46.2, TA=1.43, B=22, %83705531  
D=10.740, QC=0.6321, FS=24.1, U=46.2, TA=1.43, B=21, %83706296  
D=10.760, QC=0.6347, FS=23.2, U=46.3, TA=1.43, B=22, %83707390  
D=10.780, QC=0.6212, FS=24.4, U=46.4, TA=1.43, B=23, %83708171  
D=10.800, QC=0.5999, FS=23.5, U=46.5, TA=1.44, B=22, %83709296  
D=10.820, QC=0.5911, FS=20.4, U=46.5, TA=1.43, B=21, %83709953  
D=10.840, QC=0.5781, FS=14.0, U=46.7, TA=1.46, B=22, %83710750

D=10.860, QC=0.5781, FS=11.8, U=46.7, TA=1.47, B=22, %83711859  
D=10.880, QC=0.5807, FS=12.2, U=46.8, TA=1.47, B=22, %83712640  
D=10.900, QC=0.5994, FS=12.8, U=46.9, TA=1.46, B=22, %83713421  
D=10.920, QC=0.6773, FS=12.9, U=46.9, TA=1.46, B=21, %83714546  
D=10.940, QC=0.6030, FS=13.2, U=47.0, TA=1.45, B=22, %83715218  
D=10.960, QC=0.5620, FS=11.0, U=47.2, TA=1.44, B=22, %83716421  
D=10.980, QC=0.5475, FS=11.0, U=47.4, TA=1.46, B=21, %83717078  
D=11.000, QC=0.5412, FS=10.9, U=47.4, TA=1.48, B=21, %83718281  
D=11.020, QC=0.5412, FS=10.9, U=47.4, TA=1.48, B=22, %83719062  
D=11.040, QC=0.5423, FS=11.2, U=47.6, TA=1.49, B=21, %83719718  
D=11.060, QC=0.5459, FS=11.1, U=47.7, TA=1.50, B=21, %83720937  
D=11.080, QC=0.5443, FS=10.1, U=47.7, TA=1.48, B=21, %83721593  
D=11.100, QC=0.5417, FS=8.9, U=47.8, TA=1.50, B=21, %83722796  
D=11.120, QC=0.5469, FS=8.3, U=47.9, TA=1.48, B=21, %83723453  
D=11.140, QC=0.5745, FS=7.8, U=48.0, TA=1.48, B=20, %83724671  
D=11.160, QC=0.5921, FS=8.5, U=48.2, TA=1.49, B=20, %83725343  
D=11.180, QC=0.5807, FS=9.1, U=48.2, TA=1.50, B=21, %83726546  
D=11.200, QC=0.5703, FS=10.0, U=48.2, TA=1.51, B=20, %83727203  
D=11.220, QC=0.5573, FS=8.1, U=48.4, TA=1.50, B=20, %83728406  
D=11.240, QC=0.5069, FS=6.9, U=48.5, TA=1.48, B=19, %83729515 , F=11  
D=11.260, QC=0.5179, FS=9.4, U=53.9, TA=1.55, B=27, %83768937  
D=11.280, QC=0.5179, FS=9.4, U=53.9, TA=1.55, B=27, %83768937  
D=11.300, QC=0.5179, FS=9.4, U=53.9, TA=1.55, B=27, %83768937  
D=11.320, QC=0.5163, FS=9.3, U=53.6, TA=1.53, B=25, %83769718  
D=11.340, QC=0.5090, FS=9.8, U=53.6, TA=1.53, B=26, %83770484  
D=11.360, QC=0.5064, FS=9.2, U=53.8, TA=1.54, B=19, %83771578  
D=11.380, QC=0.5153, FS=8.9, U=53.9, TA=1.53, B=18, %83772359  
D=11.400, QC=0.5329, FS=8.5, U=53.9, TA=1.53, B=18, %83773453  
D=11.420, QC=0.5360, FS=7.7, U=54.2, TA=1.54, B=18, %83774578  
D=11.440, QC=0.5386, FS=7.4, U=54.3, TA=1.56, B=17, %83775687  
D=11.460, QC=0.5417, FS=7.3, U=54.4, TA=1.57, B=18, %83776890  
D=11.480, QC=0.5454, FS=7.6, U=54.7, TA=1.57, B=16, %83778328  
D=11.500, QC=0.5454, FS=8.0, U=54.7, TA=1.55, B=17, %83779437  
D=11.520, QC=0.5454, FS=9.0, U=55.0, TA=1.53, B=17, %83780640  
D=11.540, QC=0.5433, FS=9.5, U=55.2, TA=1.54, B=18, %83781765  
D=11.560, QC=0.5376, FS=9.8, U=55.3, TA=1.56, B=17, %83782859  
D=11.580, QC=0.5319, FS=9.8, U=55.5, TA=1.61, B=19, %83783984  
D=11.600, QC=0.5267, FS=9.9, U=55.5, TA=1.66, B=18, %83784750  
D=11.620, QC=0.5199, FS=10.2, U=55.7, TA=1.68, B=19, %83785843  
D=11.640, QC=0.5121, FS=10.2, U=55.8, TA=1.66, B=18, %83786937  
D=11.660, QC=0.5101, FS=10.1, U=56.1, TA=1.67, B=19, %83788031  
D=11.680, QC=0.5236, FS=10.1, U=56.2, TA=1.68, B=19, %83789250  
D=11.700, QC=0.5412, FS=10.3, U=56.4, TA=1.68, B=20, %83790343  
D=11.720, QC=0.5495, FS=9.9, U=56.5, TA=1.71, B=19, %83791125  
D=11.740, QC=0.5231, FS=9.7, U=56.6, TA=1.69, B=20, %83792218  
D=11.760, QC=0.5064, FS=10.3, U=56.8, TA=1.73, B=20, %83793312  
D=11.780, QC=0.4992, FS=9.8, U=56.9, TA=1.73, B=20, %83794109  
D=11.800, QC=0.5142, FS=9.3, U=57.0, TA=1.73, B=19, %83795203  
D=11.820, QC=0.5205, FS=8.4, U=57.4, TA=1.75, B=20, %83796296  
D=11.840, QC=0.5251, FS=8.2, U=57.5, TA=1.77, B=20, %83797078

D=11.860, QC=0.5262, FS=7.9, U=57.7, TA=1.79, B=20, %83798171  
D=11.880, QC=0.5303, FS=8.1, U=57.9, TA=1.74, B=19, %83799312  
D=11.900, QC=0.5303, FS=8.5, U=58.0, TA=1.83, B=20, %83800078  
D=11.920, QC=0.5298, FS=9.5, U=58.1, TA=1.80, B=20, %83801171  
D=11.940, QC=0.5329, FS=10.9, U=58.5, TA=1.83, B=21, %83802375  
D=11.960, QC=0.5381, FS=11.4, U=58.5, TA=1.83, B=19, %83803140  
D=11.980, QC=0.5553, FS=11.9, U=58.8, TA=1.83, B=19, %83804234  
D=12.000, QC=0.5604, FS=12.3, U=59.0, TA=1.84, B=19, %83805343  
D=12.020, QC=0.5589, FS=12.4, U=59.1, TA=1.83, B=20, %83806109  
D=12.040, QC=0.5506, FS=12.5, U=59.2, TA=1.85, B=19, %83807203  
D=12.060, QC=0.5501, FS=12.9, U=59.5, TA=1.84, B=19, %83808296  
D=12.080, QC=0.5542, FS=13.1, U=59.6, TA=1.83, B=18, %83809500  
D=12.100, QC=0.5537, FS=13.2, U=59.7, TA=1.85, B=20, %83810265  
D=12.120, QC=0.5542, FS=13.4, U=60.0, TA=1.83, B=19, %83811375  
D=12.140, QC=0.5516, FS=13.5, U=60.2, TA=1.85, B=19, %83812500  
D=12.160, QC=0.5506, FS=13.5, U=60.3, TA=1.87, B=19, %83813171  
D=12.180, QC=0.5469, FS=13.3, U=60.5, TA=1.83, B=19, %83814375  
D=12.200, QC=0.5423, FS=13.1, U=60.7, TA=1.85, B=19, %83815468  
D=12.220, QC=0.5381, FS=13.2, U=60.9, TA=1.84, B=19, %83816578  
D=12.240, QC=0.5381, FS=13.2, U=61.0, TA=1.84, B=18, %83817375  
D=12.260, QC=0.5386, FS=13.2, U=61.2, TA=1.85, B=19, %83818468  
D=12.280, QC=0.5386, FS=13.1, U=61.4, TA=1.83, B=18, %83819562  
D=12.300, QC=0.5376, FS=12.9, U=61.5, TA=1.86, B=19, %83820656  
D=12.320, QC=0.5381, FS=12.7, U=61.8, TA=1.85, B=18, %83821859  
D=12.340, QC=0.5402, FS=12.4, U=62.0, TA=1.85, B=18, %83822640  
D=12.360, QC=0.5511, FS=12.3, U=62.1, TA=1.86, B=18, %83823750  
D=12.380, QC=0.5584, FS=12.0, U=62.4, TA=1.86, B=18, %83824828  
D=12.400, QC=0.5656, FS=11.7, U=62.5, TA=1.87, B=18, %83825937  
D=12.420, QC=0.5620, FS=11.4, U=62.8, TA=1.85, B=18, %83827046  
D=12.440, QC=0.5625, FS=11.4, U=62.9, TA=1.85, B=18, %83828250, NA=0.0062, NB=0.6, NC=3.5, F=15, K=90, T=The test are ended without any stop in the ground.

#\$

0:

1:

2:

3:

4:

5:

6:

7:

8:

9:

11:Tilt derivative alarm

12:Point resistance alarm

13:Depth unchanged for 5 second

14:Transmission lost

15:End of test

16:Dissipation start



**CPT -5**  
**Raw Data**

\$  
HA=1,HB=5,HC=CPTLOG-2.00,HD=8/18/2020,HG=-0.457,HP=-0.46,HJ=Brenton  
CPT,HK=C5,HM=07,HN=3206,HO=0.00,HQ=SA,HR=0°0'0.000"E,HS=0°0'0.000"N,HX=0.00,HY=0.00  
,HZ=0.00,KQ=1468.00,KF=6200.00,KU=2136.00,MA=0.590,MB=0.011,MC=10.0,MD=150.0,ME=C5,  
MF=0.000  
RN=,CA=0,CB=0

#  
D=0.000, QC=0.0073, FS=0.1, U=1.5, TA=2.62, B=0, %85880031, NA=5.5328, NB=330.2, NC=436.6  
D=0.020, QC=0.0042, FS=1.2, U=0.9, TA=2.58, B=9, %85886765  
D=0.040, QC=0.0099, FS=1.3, U=0.9, TA=2.61, B=24, %85887859  
D=0.060, QC=0.0109, FS=1.5, U=0.8, TA=2.58, B=24, %85888640  
D=0.080, QC=0.0130, FS=1.6, U=0.8, TA=2.56, B=25, %85889406  
D=0.100, QC=0.0140, FS=1.7, U=0.8, TA=2.63, B=22, %85890093  
D=0.120, QC=0.0135, FS=1.8, U=0.7, TA=2.59, B=23, %85890828  
D=0.140, QC=0.0671, FS=1.9, U=0.7, TA=2.60, B=24, %85892031  
D=0.160, QC=0.0580, FS=1.8, U=0.6, TA=2.60, B=24, %85892718  
D=0.180, QC=0.0636, FS=1.9, U=0.6, TA=2.60, B=22, %85893484  
D=0.200, QC=0.0673, FS=2.2, U=0.6, TA=2.60, B=23, %85894265  
D=0.220, QC=0.0632, FS=2.4, U=0.5, TA=2.67, B=22, %85895390  
D=0.240, QC=0.0708, FS=2.4, U=0.5, TA=2.63, B=23, %85896187  
D=0.260, QC=0.0725, FS=2.3, U=0.5, TA=2.61, B=23, %85896859  
D=0.280, QC=0.0799, FS=2.0, U=0.4, TA=2.60, B=23, %85897656  
D=0.300, QC=0.0766, FS=1.9, U=0.4, TA=2.64, B=27, %85898343  
D=0.320, QC=0.0749, FS=1.8, U=0.4, TA=2.61, B=26, %85899125  
D=0.340, QC=0.0765, FS=1.6, U=0.3, TA=2.65, B=26, %85899890  
D=0.360, QC=0.0706, FS=1.3, U=0.2, TA=2.64, B=25, %85900968  
D=0.380, QC=0.0722, FS=1.3, U=0.2, TA=2.63, B=24, %85901734  
D=0.400, QC=0.0722, FS=1.4, U=0.2, TA=2.67, B=20, %85902515  
D=0.420, QC=0.0780, FS=1.5, U=0.1, TA=2.72, B=20, %85903609  
D=0.440, QC=0.0775, FS=1.7, U=0.1, TA=2.72, B=19, %85904375  
D=0.460, QC=0.0712, FS=1.8, U=0.0, TA=2.72, B=20, %85905515  
D=0.480, QC=0.0921, FS=1.7, U=0.1, TA=2.76, B=20, %85906640  
D=0.500, QC=0.0942, FS=1.7, U=0.2, TA=2.75, B=21, %85907406  
D=0.520, QC=0.0957, FS=1.8, U=0.2, TA=2.72, B=20, %85908531  
D=0.540, QC=0.0909, FS=2.1, U=0.4, TA=2.73, B=22, %85909296  
D=0.560, QC=0.0940, FS=2.2, U=0.5, TA=2.73, B=22, %85909968  
D=0.580, QC=0.1177, FS=2.4, U=0.5, TA=2.68, B=25, %85911171  
D=0.600, QC=0.1166, FS=2.6, U=0.6, TA=2.71, B=25, %85911843  
D=0.620, QC=0.1130, FS=2.8, U=0.7, TA=2.71, B=24, %85912609  
D=0.640, QC=0.1130, FS=3.0, U=0.7, TA=2.70, B=25, %85913375  
D=0.660, QC=0.1125, FS=3.0, U=0.8, TA=2.68, B=28, %85914140  
D=0.680, QC=0.1109, FS=3.0, U=0.9, TA=2.68, B=23, %85914906  
D=0.700, QC=0.1109, FS=2.5, U=1.1, TA=2.59, B=20, %85916031  
D=0.720, QC=0.1109, FS=2.6, U=1.2, TA=2.71, B=11, %85917453  
D=0.740, QC=0.1147, FS=2.3, U=1.4, TA=2.67, B=19, %85919031  
D=0.760, QC=0.1126, FS=2.1, U=1.6, TA=2.65, B=19, %85919796  
D=0.780, QC=0.1142, FS=1.8, U=1.6, TA=2.67, B=18, %85920906  
D=0.800, QC=0.1157, FS=1.7, U=1.8, TA=2.67, B=18, %85922015  
D=0.820, QC=0.1178, FS=1.6, U=1.9, TA=2.66, B=20, %85922796  
D=0.840, QC=0.1130, FS=1.6, U=2.0, TA=2.68, B=19, %85923828

D=0.860, QC=0.1161, FS=1.6, U=2.3, TA=2.67, B=19, %85925046  
D=0.880, QC=0.1187, FS=1.6, U=2.3, TA=2.68, B=19, %85926156  
D=0.900, QC=0.1192, FS=1.7, U=2.5, TA=2.73, B=19, %85926937  
D=0.920, QC=0.1128, FS=1.4, U=2.6, TA=2.72, B=19, %85928046  
D=0.940, QC=0.1139, FS=1.4, U=2.7, TA=2.76, B=19, %85929078  
D=0.960, QC=0.1170, FS=1.5, U=3.1, TA=2.76, B=18, %85930281  
D=0.980, QC=0.1191, FS=1.6, U=3.1, TA=2.76, B=19, %85931046  
D=1.000, QC=0.1122, FS=1.8, U=3.3, TA=2.77, B=19, %85932078  
D=1.020, QC=0.1138, FS=2.1, U=3.5, TA=2.77, B=18, %85933296  
D=1.040, QC=0.1153, FS=2.2, U=3.6, TA=2.77, B=19, %85934406  
D=1.060, QC=0.1169, FS=2.5, U=1.5, TA=2.84, B=19, %85935171  
D=1.080, QC=0.1815, FS=2.5, U=1.7, TA=2.85, B=19, %85936281  
D=1.100, QC=0.1753, FS=2.7, U=1.8, TA=2.81, B=18, %85937390  
D=1.120, QC=0.1748, FS=2.8, U=2.1, TA=2.81, B=19, %85938484  
D=1.140, QC=0.1774, FS=2.7, U=2.2, TA=2.80, B=18, %85939593  
D=1.160, QC=0.1784, FS=2.8, U=2.4, TA=2.77, B=18, %85940359  
D=1.180, QC=0.1779, FS=2.6, U=2.6, TA=2.81, B=19, %85941468  
D=1.200, QC=0.1200, FS=2.5, U=2.7, TA=2.83, B=18, %85942609  
D=1.220, QC=0.1284, FS=2.5, U=3.0, TA=2.82, B=18, %85943718  
D=1.240, QC=0.1284, FS=2.5, U=3.1, TA=2.81, B=18, %85944843  
D=1.260, QC=0.1264, FS=2.2, U=3.3, TA=2.82, B=17, %85946046  
D=1.280, QC=0.1212, FS=2.1, U=3.5, TA=2.85, B=18, %85947093  
D=1.300, QC=0.1269, FS=0.9, U=1.5, TA=2.85, B=14, %85948312  
D=1.320, QC=0.1218, FS=1.1, U=3.9, TA=2.84, B=28, %85988609  
D=1.340, QC=0.1218, FS=1.1, U=3.9, TA=2.84, B=28, %85988609  
D=1.360, QC=0.1232, FS=1.1, U=3.9, TA=2.82, B=24, %85988968  
D=1.380, QC=0.1243, FS=0.9, U=3.5, TA=2.77, B=25, %85989734  
D=1.400, QC=0.1253, FS=0.8, U=3.6, TA=2.78, B=24, %85990859  
D=1.420, QC=0.1253, FS=0.8, U=3.6, TA=2.74, B=26, %85991531  
D=1.440, QC=0.1164, FS=0.9, U=3.7, TA=2.75, B=18, %85992296  
D=1.460, QC=0.1121, FS=0.9, U=3.7, TA=2.77, B=21, %85993500  
D=1.480, QC=0.1136, FS=0.9, U=3.8, TA=2.74, B=20, %85994156  
D=1.500, QC=0.1147, FS=1.2, U=4.0, TA=2.74, B=21, %85995312  
D=1.520, QC=0.1126, FS=1.3, U=4.1, TA=2.78, B=19, %85996421  
D=1.540, QC=0.1141, FS=1.1, U=4.1, TA=2.74, B=20, %85997187  
D=1.560, QC=0.1152, FS=0.8, U=4.3, TA=2.77, B=19, %85998296  
D=1.580, QC=0.1147, FS=0.6, U=4.3, TA=2.78, B=20, %85999062  
D=1.600, QC=0.1141, FS=0.4, U=4.5, TA=2.78, B=21, %86000187  
D=1.620, QC=0.1167, FS=0.2, U=4.6, TA=2.78, B=21, %86001312  
D=1.640, QC=0.1183, FS=0.4, U=4.7, TA=2.78, B=20, %86002093  
D=1.660, QC=0.1188, FS=0.6, U=4.9, TA=2.79, B=22, %86003187  
D=1.680, QC=0.1199, FS=0.6, U=5.0, TA=2.80, B=20, %86003953  
D=1.700, QC=0.1135, FS=0.8, U=5.1, TA=2.80, B=21, %86005062  
D=1.720, QC=0.1197, FS=0.8, U=5.3, TA=2.81, B=21, %86005843  
D=1.740, QC=0.1034, FS=0.9, U=5.4, TA=2.80, B=22, %86006953  
D=1.760, QC=0.1076, FS=0.9, U=5.5, TA=2.78, B=21, %86007718  
D=1.780, QC=0.1071, FS=0.7, U=5.6, TA=2.79, B=22, %86008500  
D=1.800, QC=0.1030, FS=0.7, U=5.8, TA=2.78, B=21, %86009531  
D=1.820, QC=0.1034, FS=0.7, U=3.8, TA=2.78, B=23, %86010328  
D=1.840, QC=0.1060, FS=0.6, U=3.8, TA=2.81, B=21, %86011109

D=1.860, QC=0.1226, FS=0.5, U=4.0, TA=2.81, B=23, %86012218  
D=1.880, QC=0.1267, FS=0.5, U=4.1, TA=2.80, B=22, %86013000  
D=1.900, QC=0.1371, FS=0.3, U=4.2, TA=2.83, B=22, %86013671  
D=1.920, QC=0.1579, FS=0.6, U=4.4, TA=2.83, B=22, %86014875  
D=1.940, QC=0.1667, FS=0.6, U=4.5, TA=2.84, B=23, %86015531  
D=1.960, QC=0.1698, FS=1.3, U=4.7, TA=2.84, B=23, %86016296  
D=1.980, QC=0.1683, FS=1.6, U=4.9, TA=2.85, B=23, %86017437  
D=2.000, QC=0.1792, FS=1.8, U=5.0, TA=2.83, B=22, %86018203  
D=2.020, QC=0.2311, FS=2.3, U=5.3, TA=2.82, B=23, %86019296  
D=2.040, QC=0.3413, FS=2.8, U=5.4, TA=2.83, B=22, %86020078  
D=2.060, QC=0.5797, FS=6.9, U=5.5, TA=2.84, B=22, %86020859  
D=2.080, QC=0.9433, FS=13.0, U=6.0, TA=2.85, B=21, %86021953  
D=2.100, QC=0.9396, FS=16.9, U=6.4, TA=2.86, B=21, %86022750  
D=2.120, QC=0.8861, FS=8.0, U=-0.6, TA=2.86, B=22, %86023859  
D=2.140, QC=0.7480, FS=8.9, U=-1.8, TA=2.86, B=22, %86024531  
D=2.160, QC=0.8337, FS=22.5, U=-0.8, TA=2.88, B=21, %86025328  
D=2.180, QC=1.1734, FS=40.0, U=-1.7, TA=2.95, B=21, %86026437  
D=2.200, QC=1.2679, FS=44.0, U=1.5, TA=2.95, B=20, %86027640  
D=2.220, QC=1.2575, FS=43.4, U=3.5, TA=2.95, B=21, %86028296  
D=2.240, QC=1.2944, FS=41.4, U=0.7, TA=2.95, B=20, %86029421  
D=2.260, QC=1.3598, FS=40.4, U=0.8, TA=2.95, B=20, %86030218  
D=2.280, QC=1.3593, FS=70.7, U=2.7, TA=2.95, B=19, %86031328  
D=2.300, QC=1.5993, FS=83.7, U=4.3, TA=2.95, B=20, %86032453  
D=2.320, QC=1.6642, FS=85.6, U=5.2, TA=2.95, B=18, %86033250  
D=2.340, QC=1.6455, FS=80.7, U=5.2, TA=2.95, B=18, %86034343  
D=2.360, QC=1.5058, FS=77.8, U=5.4, TA=2.95, B=18, %86035437  
D=2.380, QC=1.5702, FS=79.1, U=6.1, TA=2.95, B=19, %86036562  
D=2.400, QC=1.7333, FS=79.5, U=6.3, TA=2.95, B=18, %86037687  
D=2.420, QC=1.7089, FS=77.7, U=6.2, TA=2.95, B=18, %86038468  
D=2.440, QC=1.5390, FS=74.4, U=6.4, TA=2.95, B=19, %86039562  
D=2.460, QC=1.2648, FS=73.5, U=6.4, TA=2.95, B=19, %86040687  
D=2.480, QC=1.0788, FS=63.5, U=5.2, TA=2.96, B=10, %86084921  
D=2.500, QC=1.0788, FS=63.5, U=5.2, TA=2.96, B=10, %86084921  
D=2.520, QC=1.0077, FS=61.0, U=4.7, TA=2.95, B=17, %86085593  
D=2.540, QC=0.9433, FS=51.4, U=2.2, TA=2.95, B=25, %86086359  
D=2.560, QC=0.9225, FS=46.2, U=4.5, TA=2.95, B=23, %86087468  
D=2.580, QC=0.9240, FS=45.3, U=2.1, TA=2.95, B=23, %86088234  
D=2.600, QC=0.9209, FS=42.7, U=2.1, TA=2.95, B=23, %86089031  
D=2.620, QC=0.9043, FS=37.6, U=2.0, TA=2.95, B=25, %86089796  
D=2.640, QC=0.8877, FS=26.9, U=1.6, TA=2.95, B=24, %86090468  
D=2.660, QC=0.8711, FS=13.8, U=0.5, TA=2.95, B=24, %86091671  
D=2.680, QC=0.9007, FS=24.8, U=1.0, TA=2.95, B=24, %86092437  
D=2.700, QC=0.9334, FS=39.9, U=1.6, TA=2.95, B=22, %86093093  
D=2.720, QC=0.9578, FS=48.3, U=2.2, TA=2.95, B=22, %86093859  
D=2.740, QC=0.9505, FS=43.9, U=2.3, TA=2.95, B=24, %86094968  
D=2.760, QC=0.9329, FS=36.4, U=2.0, TA=2.95, B=23, %86095781  
D=2.780, QC=0.8918, FS=23.3, U=1.5, TA=2.95, B=23, %86096546  
D=2.800, QC=0.8300, FS=8.1, U=1.0, TA=2.95, B=24, %86097203  
D=2.820, QC=0.7282, FS=1.8, U=0.4, TA=2.95, B=24, %86097968  
D=2.840, QC=0.5916, FS=4.9, U=-0.4, TA=2.95, B=23, %86099187

D=2.860, QC=0.4716, FS=3.9, U=-0.6, TA=2.95, B=24, %86099859  
D=2.880, QC=0.3974, FS=1.7, U=-0.6, TA=2.95, B=24, %86100625  
D=2.900, QC=0.3527, FS=0.7, U=-0.5, TA=2.95, B=26, %86101390  
D=2.920, QC=0.3387, FS=0.6, U=-0.4, TA=2.95, B=25, %86102156  
D=2.940, QC=0.3449, FS=1.6, U=-0.4, TA=2.95, B=25, %86102937  
D=2.960, QC=0.3433, FS=2.0, U=-0.3, TA=2.95, B=24, %86103593  
D=2.980, QC=0.3226, FS=3.2, U=-0.2, TA=2.95, B=27, %86104703  
D=3.000, QC=0.3013, FS=3.8, U=-0.1, TA=2.95, B=24, %86105484  
D=3.020, QC=0.3023, FS=3.8, U=-0.1, TA=2.95, B=23, %86106250  
D=3.040, QC=0.3142, FS=4.1, U=-0.1, TA=2.95, B=24, %86107031  
D=3.060, QC=0.3148, FS=5.0, U=0.1, TA=2.95, B=24, %86107796  
D=3.080, QC=0.2950, FS=5.6, U=0.1, TA=2.95, B=24, %86108468  
D=3.100, QC=0.2846, FS=4.8, U=0.3, TA=2.95, B=22, %86109687  
D=3.120, QC=0.3054, FS=5.0, U=0.4, TA=2.95, B=22, %86110359  
D=3.140, QC=0.3418, FS=4.5, U=0.4, TA=2.95, B=23, %86111125  
D=3.160, QC=0.4005, FS=4.4, U=0.6, TA=2.95, B=22, %86112218  
D=3.180, QC=0.4721, FS=3.7, U=0.7, TA=2.95, B=22, %86112984  
D=3.200, QC=0.5927, FS=3.4, U=0.7, TA=2.95, B=21, %86113750  
D=3.220, QC=0.6093, FS=2.5, U=1.0, TA=2.95, B=23, %86114843  
D=3.240, QC=0.4924, FS=3.0, U=1.1, TA=2.95, B=22, %86115609  
D=3.260, QC=0.4062, FS=2.8, U=1.1, TA=2.95, B=23, %86116390  
D=3.280, QC=0.4347, FS=2.9, U=1.2, TA=2.95, B=23, %86117515  
D=3.300, QC=0.8451, FS=1.8, U=1.2, TA=2.95, B=24, %86118281  
D=3.320, QC=0.9370, FS=6.4, U=1.9, TA=2.95, B=24, %86118953  
D=3.340, QC=0.9230, FS=15.9, U=3.0, TA=2.95, B=24, %86119718  
D=3.360, QC=0.8456, FS=3.1, U=2.0, TA=2.95, B=23, %86120921  
D=3.380, QC=0.7158, FS=3.8, U=1.8, TA=2.95, B=25, %86121593  
D=3.400, QC=0.6472, FS=3.6, U=1.9, TA=2.95, B=24, %86122359  
D=3.420, QC=0.6030, FS=2.8, U=2.0, TA=2.95, B=24, %86123125  
D=3.440, QC=0.4368, FS=2.0, U=0.4, TA=2.95, B=24, %86124234  
D=3.460, QC=0.3771, FS=0.2, U=2.0, TA=2.95, B=24, %86125000  
D=3.480, QC=0.3490, FS=3.2, U=2.1, TA=2.95, B=24, %86125765  
D=3.500, QC=0.4425, FS=3.6, U=2.2, TA=2.95, B=24, %86126531  
D=3.520, QC=0.5589, FS=2.6, U=0.2, TA=2.95, B=23, %86127296  
D=3.540, QC=0.5625, FS=0.3, U=0.0, TA=2.95, B=24, %86128421  
D=3.560, QC=0.6654, FS=3.7, U=0.7, TA=2.95, B=23, %86129093  
D=3.580, QC=0.9079, FS=13.5, U=2.2, TA=2.95, B=22, %86129875  
D=3.600, QC=0.8763, FS=0.9, U=1.0, TA=2.95, B=22, %86130640  
D=3.620, QC=0.5693, FS=3.2, U=0.6, TA=2.95, B=25, %86131734  
D=3.640, QC=0.4664, FS=3.7, U=0.5, TA=2.95, B=24, %86132531  
D=3.660, QC=0.7963, FS=22.2, U=2.1, TA=2.94, B=28, %86176796  
D=3.680, QC=0.7963, FS=22.2, U=2.1, TA=2.94, B=28, %86176796  
D=3.700, QC=0.7963, FS=22.2, U=2.1, TA=2.94, B=28, %86176796  
D=3.720, QC=0.9905, FS=22.2, U=2.1, TA=2.95, B=25, %86177125  
D=3.740, QC=0.8773, FS=35.4, U=3.1, TA=2.95, B=23, %86177890  
D=3.760, QC=0.7890, FS=5.4, U=2.0, TA=2.95, B=25, %86178687  
D=3.780, QC=0.5750, FS=3.7, U=1.2, TA=2.95, B=23, %86179343  
D=3.800, QC=0.5064, FS=1.6, U=1.0, TA=2.95, B=19, %86180484  
D=3.820, QC=0.4825, FS=0.3, U=0.9, TA=2.95, B=20, %86181281  
D=3.840, QC=0.5231, FS=0.7, U=0.9, TA=2.95, B=20, %86182375

D=3.860, QC=0.4898, FS=1.1, U=1.0, TA=2.95, B=20, %86183140  
D=3.880, QC=0.4503, FS=1.9, U=1.0, TA=2.95, B=19, %86184265  
D=3.900, QC=0.3501, FS=2.9, U=1.1, TA=2.95, B=19, %86185359  
D=3.920, QC=0.3236, FS=3.2, U=1.1, TA=2.95, B=20, %86186453  
D=3.940, QC=0.3054, FS=1.0, U=1.2, TA=2.95, B=20, %86187218  
D=3.960, QC=0.2867, FS=0.9, U=1.3, TA=2.95, B=19, %86188343  
D=3.980, QC=0.2852, FS=1.9, U=1.4, TA=2.95, B=20, %86189156  
D=4.000, QC=0.2815, FS=2.9, U=1.4, TA=2.95, B=20, %86190250  
D=4.020, QC=0.4737, FS=2.9, U=1.6, TA=2.94, B=20, %86191343  
D=4.040, QC=0.5729, FS=3.3, U=1.6, TA=2.95, B=20, %86192125  
D=4.060, QC=0.5153, FS=4.5, U=1.6, TA=2.93, B=20, %86193218  
D=4.080, QC=0.4483, FS=3.8, U=1.7, TA=2.94, B=20, %86194015  
D=4.100, QC=0.3309, FS=3.2, U=1.7, TA=2.94, B=22, %86195109  
D=4.120, QC=0.3091, FS=1.8, U=1.7, TA=2.93, B=21, %86195906  
D=4.140, QC=0.2992, FS=1.6, U=2.0, TA=2.95, B=20, %86197015  
D=4.160, QC=0.2883, FS=1.9, U=2.1, TA=2.94, B=21, %86198140  
D=4.180, QC=0.2826, FS=2.1, U=2.1, TA=2.95, B=23, %86198906  
D=4.200, QC=0.2805, FS=2.3, U=2.2, TA=2.94, B=21, %86199687  
D=4.220, QC=0.2763, FS=3.3, U=2.3, TA=2.95, B=21, %86200812  
D=4.240, QC=0.2727, FS=4.6, U=2.4, TA=2.95, B=21, %86201484  
D=4.260, QC=0.2727, FS=4.5, U=2.5, TA=2.95, B=22, %86202687  
D=4.280, QC=0.2727, FS=4.7, U=2.6, TA=2.94, B=22, %86203375  
D=4.300, QC=0.2748, FS=4.4, U=2.7, TA=2.95, B=21, %86204500  
D=4.320, QC=0.2758, FS=4.2, U=2.9, TA=2.94, B=21, %86205281  
D=4.340, QC=0.2794, FS=4.1, U=2.9, TA=2.95, B=23, %86206046  
D=4.360, QC=0.2774, FS=3.9, U=0.8, TA=2.95, B=21, %86207140  
D=4.380, QC=0.2774, FS=3.7, U=3.1, TA=2.95, B=21, %86207921  
D=4.400, QC=0.2836, FS=3.3, U=3.2, TA=2.95, B=21, %86209046  
D=4.420, QC=0.2794, FS=3.1, U=1.1, TA=2.95, B=22, %86209718  
D=4.440, QC=0.2815, FS=2.9, U=1.2, TA=2.95, B=21, %86210921  
D=4.460, QC=0.2815, FS=2.7, U=1.3, TA=2.95, B=21, %86211593  
D=4.480, QC=0.2820, FS=2.5, U=1.3, TA=2.95, B=21, %86212375  
D=4.500, QC=0.2867, FS=2.6, U=1.5, TA=2.95, B=22, %86213500  
D=4.520, QC=0.2893, FS=2.5, U=1.6, TA=2.95, B=22, %86214265  
D=4.540, QC=0.2857, FS=2.6, U=1.7, TA=2.95, B=21, %86215359  
D=4.560, QC=0.2872, FS=2.7, U=1.7, TA=2.95, B=20, %86216140  
D=4.580, QC=0.2857, FS=2.6, U=1.8, TA=2.95, B=22, %86216906  
D=4.600, QC=0.2846, FS=2.4, U=2.0, TA=2.95, B=21, %86218015  
D=4.620, QC=0.2815, FS=2.3, U=2.1, TA=2.95, B=22, %86218812  
D=4.640, QC=0.2774, FS=2.3, U=2.1, TA=2.95, B=21, %86219953  
D=4.660, QC=0.2768, FS=2.3, U=2.2, TA=2.95, B=21, %86220609  
D=4.680, QC=0.2805, FS=2.5, U=2.5, TA=2.95, B=22, %86221812  
D=4.700, QC=0.2810, FS=2.5, U=2.5, TA=2.95, B=21, %86222468  
D=4.720, QC=0.2862, FS=2.5, U=2.6, TA=2.95, B=21, %86223687  
D=4.740, QC=0.2862, FS=2.6, U=2.7, TA=2.95, B=21, %86224359  
D=4.760, QC=0.2857, FS=2.8, U=3.0, TA=2.95, B=21, %86225468  
D=4.780, QC=0.2898, FS=2.8, U=3.0, TA=2.95, B=20, %86226234  
D=4.800, QC=0.2966, FS=2.7, U=3.2, TA=2.95, B=21, %86227343  
D=4.820, QC=0.2981, FS=2.7, U=3.2, TA=2.95, B=21, %86228140  
D=4.840, QC=0.2992, FS=2.2, U=3.4, TA=2.95, B=20, %86229250

D=4.860, QC=0.3023, FS=3.7, U=3.5, TA=2.95, B=20, %86230031  
D=4.880, QC=0.2961, FS=0.4, U=4.6, TA=2.94, B=0, %86280906  
D=4.900, QC=0.3324, FS=0.0, U=4.2, TA=2.95, B=28, %86281687  
D=4.920, QC=0.3506, FS=0.6, U=4.2, TA=2.95, B=20, %86282796  
D=4.940, QC=0.3381, FS=0.6, U=4.2, TA=2.95, B=19, %86283593  
D=4.960, QC=0.3215, FS=0.6, U=4.3, TA=2.95, B=20, %86284703  
D=4.980, QC=0.3023, FS=1.3, U=4.4, TA=2.96, B=19, %86285796  
D=5.000, QC=0.3220, FS=1.9, U=4.3, TA=2.96, B=19, %86286562  
D=5.020, QC=0.3589, FS=2.2, U=4.4, TA=2.96, B=19, %86287687  
D=5.040, QC=0.3911, FS=2.6, U=4.4, TA=2.96, B=20, %86288781  
D=5.060, QC=0.3184, FS=2.5, U=4.5, TA=2.94, B=19, %86289562  
D=5.080, QC=0.2670, FS=2.6, U=4.7, TA=2.95, B=20, %86290687  
D=5.100, QC=0.2633, FS=2.8, U=4.8, TA=2.95, B=19, %86291781  
D=5.120, QC=0.2701, FS=3.0, U=4.9, TA=2.95, B=19, %86292921  
D=5.140, QC=0.2737, FS=3.0, U=5.0, TA=2.94, B=20, %86293687  
D=5.160, QC=0.2768, FS=3.0, U=5.0, TA=2.94, B=20, %86294796  
D=5.180, QC=0.2794, FS=2.7, U=5.1, TA=2.92, B=20, %86295890  
D=5.200, QC=0.2810, FS=2.6, U=5.2, TA=2.92, B=20, %86296687  
D=5.220, QC=0.2826, FS=2.4, U=5.3, TA=2.91, B=19, %86297812  
D=5.240, QC=0.2872, FS=2.2, U=5.4, TA=2.91, B=21, %86298906  
D=5.260, QC=0.2929, FS=1.9, U=5.5, TA=2.90, B=20, %86299687  
D=5.280, QC=0.3142, FS=1.7, U=5.6, TA=2.92, B=21, %86300812  
D=5.300, QC=0.3153, FS=1.9, U=5.6, TA=2.90, B=21, %86301593  
D=5.320, QC=0.3116, FS=1.9, U=5.7, TA=2.90, B=21, %86302718  
D=5.340, QC=0.3142, FS=1.8, U=5.9, TA=2.91, B=20, %86303390  
D=5.360, QC=0.3241, FS=1.5, U=6.0, TA=2.90, B=22, %86304531  
D=5.380, QC=0.3252, FS=1.3, U=6.1, TA=2.89, B=21, %86305296  
D=5.400, QC=0.3194, FS=0.7, U=6.1, TA=2.89, B=21, %86306390  
D=5.420, QC=0.3231, FS=0.6, U=6.2, TA=2.91, B=21, %86307187  
D=5.440, QC=0.3257, FS=0.4, U=6.4, TA=2.89, B=22, %86308296  
D=5.460, QC=0.3231, FS=0.3, U=6.4, TA=2.89, B=22, %86309062  
D=5.480, QC=0.3236, FS=0.3, U=6.5, TA=2.90, B=21, %86309843  
D=5.500, QC=0.3262, FS=0.5, U=6.7, TA=2.89, B=21, %86310937  
D=5.520, QC=0.3324, FS=0.6, U=6.7, TA=2.89, B=21, %86311703  
D=5.540, QC=0.3376, FS=0.6, U=6.9, TA=2.88, B=22, %86312750  
D=5.560, QC=0.3387, FS=0.5, U=6.9, TA=2.88, B=22, %86313515  
D=5.580, QC=0.3418, FS=0.2, U=7.0, TA=2.88, B=20, %86314718  
D=5.600, QC=0.3387, FS=0.2, U=7.1, TA=2.88, B=22, %86315406  
D=5.620, QC=0.3381, FS=0.2, U=7.3, TA=2.89, B=22, %86316187  
D=5.640, QC=0.3387, FS=0.0, U=7.3, TA=2.89, B=22, %86317296  
D=5.660, QC=0.3418, FS=0.0, U=7.4, TA=2.88, B=21, %86318078  
D=5.680, QC=0.3428, FS=0.2, U=7.5, TA=2.88, B=21, %86319171  
D=5.700, QC=0.3407, FS=0.2, U=7.5, TA=2.88, B=21, %86319953  
D=5.720, QC=0.3350, FS=0.2, U=7.7, TA=2.88, B=22, %86321062  
D=5.740, QC=0.3345, FS=0.1, U=7.7, TA=2.88, B=21, %86321828  
D=5.760, QC=0.3340, FS=0.1, U=8.0, TA=2.87, B=21, %86322937  
D=5.780, QC=0.3355, FS=0.2, U=8.0, TA=2.88, B=21, %86323734  
D=5.800, QC=0.3355, FS=0.2, U=8.1, TA=2.87, B=21, %86324843  
D=5.820, QC=0.3350, FS=0.2, U=8.2, TA=2.87, B=20, %86325515  
D=5.840, QC=0.3345, FS=0.5, U=8.3, TA=2.87, B=21, %86326750

D=5.860, QC=0.3293, FS=0.5, U=8.4, TA=2.88, B=21, %86327406  
D=5.880, QC=0.3252, FS=0.6, U=8.5, TA=2.86, B=21, %86328500  
D=5.900, QC=0.3226, FS=0.5, U=8.6, TA=2.84, B=20, %86329281  
D=5.920, QC=0.3184, FS=0.6, U=8.8, TA=2.83, B=21, %86330390  
D=5.940, QC=0.3148, FS=0.7, U=8.9, TA=2.81, B=20, %86331171  
D=5.960, QC=0.3179, FS=0.6, U=8.9, TA=2.79, B=21, %86332296  
D=5.980, QC=0.3174, FS=0.6, U=9.0, TA=2.77, B=20, %86333062  
D=6.000, QC=0.3174, FS=0.4, U=9.1, TA=2.75, B=21, %86334187  
D=6.020, QC=0.3257, FS=0.4, U=9.2, TA=2.75, B=20, %86335328  
D=6.040, QC=0.3080, FS=0.4, U=9.2, TA=2.78, B=20, %86336109  
D=6.060, QC=0.3392, FS=1.6, U=9.2, TA=2.79, B=22, %86386812  
D=6.080, QC=0.3392, FS=1.6, U=9.2, TA=2.79, B=22, %86386812  
D=6.100, QC=0.3361, FS=1.6, U=9.2, TA=2.79, B=22, %86387265  
D=6.120, QC=0.3314, FS=1.3, U=8.9, TA=2.72, B=23, %86387937  
D=6.140, QC=0.3272, FS=0.9, U=8.9, TA=2.72, B=23, %86389046  
D=6.160, QC=0.3220, FS=0.8, U=9.0, TA=2.72, B=22, %86389843  
D=6.180, QC=0.3226, FS=0.8, U=9.1, TA=2.72, B=24, %86390625  
D=6.200, QC=0.3246, FS=0.8, U=9.0, TA=2.72, B=22, %86391750  
D=6.220, QC=0.3278, FS=0.9, U=9.1, TA=2.72, B=22, %86392421  
D=6.240, QC=0.3288, FS=1.0, U=9.1, TA=2.72, B=22, %86393218  
D=6.260, QC=0.3293, FS=1.5, U=9.2, TA=2.72, B=22, %86394312  
D=6.280, QC=0.3272, FS=1.5, U=9.2, TA=2.72, B=22, %86395078  
D=6.300, QC=0.3272, FS=1.6, U=9.3, TA=2.72, B=23, %86395843  
D=6.320, QC=0.3246, FS=1.6, U=9.4, TA=2.72, B=22, %86396953  
D=6.340, QC=0.3220, FS=1.5, U=9.4, TA=2.72, B=22, %86397750  
D=6.360, QC=0.3205, FS=1.3, U=9.4, TA=2.72, B=23, %86398500  
D=6.380, QC=0.3163, FS=0.9, U=9.5, TA=2.72, B=23, %86399593  
D=6.400, QC=0.3158, FS=0.9, U=9.6, TA=2.72, B=22, %86400359  
D=6.420, QC=0.3153, FS=0.9, U=9.6, TA=2.72, B=24, %86401140  
D=6.440, QC=0.3205, FS=1.1, U=9.7, TA=2.72, B=23, %86402250  
D=6.460, QC=0.3194, FS=1.1, U=9.8, TA=2.72, B=24, %86403031  
D=6.480, QC=0.3194, FS=0.9, U=9.8, TA=2.72, B=23, %86403703  
D=6.500, QC=0.3226, FS=0.9, U=9.9, TA=2.72, B=24, %86404484  
D=6.520, QC=0.3200, FS=1.0, U=9.9, TA=2.72, B=24, %86405250  
D=6.540, QC=0.3215, FS=0.4, U=10.0, TA=2.72, B=26, %86406406  
D=6.560, QC=0.3262, FS=0.3, U=10.1, TA=2.74, B=24, %86407062  
D=6.580, QC=0.3293, FS=0.4, U=10.1, TA=2.73, B=24, %86407828  
D=6.600, QC=0.3340, FS=0.6, U=10.2, TA=2.72, B=24, %86408593  
D=6.620, QC=0.3459, FS=0.7, U=10.2, TA=2.76, B=24, %86409375  
D=6.640, QC=0.3600, FS=0.6, U=10.2, TA=2.76, B=24, %86410046  
D=6.660, QC=0.3755, FS=0.5, U=10.3, TA=2.76, B=25, %86410828  
D=6.680, QC=0.3922, FS=0.6, U=10.4, TA=2.80, B=24, %86411937  
D=6.700, QC=0.4046, FS=0.9, U=10.5, TA=2.79, B=26, %86412687  
D=6.720, QC=0.4077, FS=1.3, U=10.4, TA=2.79, B=24, %86413500  
D=6.740, QC=0.4566, FS=1.6, U=10.5, TA=2.82, B=24, %86414171  
D=6.760, QC=0.5573, FS=2.1, U=10.6, TA=2.80, B=23, %86414937  
D=6.780, QC=0.8077, FS=2.8, U=10.9, TA=2.75, B=25, %86415703  
D=6.800, QC=0.8726, FS=9.6, U=11.5, TA=2.76, B=24, %86416843  
D=6.820, QC=0.8492, FS=6.5, U=10.6, TA=2.78, B=23, %86417609  
D=6.840, QC=0.7303, FS=9.4, U=10.4, TA=2.76, B=23, %86418390



D=6.860, QC=0.5630, FS=11.9, U=10.2, TA=2.74, B=25, %86419062  
D=6.880, QC=0.5589, FS=10.9, U=10.3, TA=2.73, B=25, %86419843  
D=6.900, QC=0.8700, FS=14.8, U=10.3, TA=2.73, B=23, %86420953  
D=6.920, QC=0.8773, FS=22.1, U=11.0, TA=2.72, B=22, %86421765  
D=6.940, QC=0.8674, FS=22.4, U=11.4, TA=2.72, B=24, %86422453  
D=6.960, QC=0.8840, FS=18.5, U=11.3, TA=2.73, B=23, %86423234  
D=6.980, QC=0.8887, FS=13.0, U=10.7, TA=2.71, B=23, %86424328  
D=7.000, QC=0.8269, FS=7.2, U=10.6, TA=2.76, B=22, %86425125  
D=7.020, QC=0.6939, FS=5.6, U=10.6, TA=2.74, B=23, %86425906  
D=7.040, QC=0.5433, FS=4.8, U=10.4, TA=2.73, B=23, %86426562  
D=7.060, QC=0.4275, FS=4.0, U=10.5, TA=2.71, B=23, %86427671  
D=7.080, QC=0.4446, FS=2.0, U=10.5, TA=2.72, B=23, %86428453  
D=7.100, QC=0.4581, FS=2.1, U=10.5, TA=2.71, B=23, %86429234  
D=7.120, QC=0.4420, FS=2.8, U=10.4, TA=2.72, B=23, %86430000  
D=7.140, QC=0.4124, FS=2.1, U=10.5, TA=2.72, B=22, %86431125  
D=7.160, QC=0.3812, FS=1.3, U=10.6, TA=2.71, B=23, %86431796  
D=7.180, QC=0.3605, FS=0.3, U=10.6, TA=2.68, B=23, %86432578  
D=7.200, QC=0.3355, FS=0.3, U=10.6, TA=2.71, B=17, %86433671  
D=7.220, QC=0.3241, FS=0.3, U=10.7, TA=2.70, B=15, %86435218  
D=7.240, QC=0.3693, FS=2.6, U=14.0, TA=2.72, B=28, %86479015  
D=7.260, QC=0.3693, FS=2.6, U=14.0, TA=2.72, B=28, %86479015  
D=7.280, QC=0.3693, FS=2.6, U=14.0, TA=2.72, B=28, %86479015  
D=7.300, QC=0.3859, FS=2.0, U=13.6, TA=2.73, B=27, %86479781  
D=7.320, QC=0.3870, FS=1.9, U=13.6, TA=2.73, B=27, %86480546  
D=7.340, QC=0.3948, FS=2.8, U=13.7, TA=2.73, B=27, %86481203  
D=7.360, QC=0.4015, FS=3.8, U=13.7, TA=2.75, B=30, %86481968  
D=7.380, QC=0.4207, FS=3.8, U=13.7, TA=2.73, B=27, %86482750  
D=7.400, QC=0.4270, FS=3.7, U=13.7, TA=2.72, B=28, %86483531  
D=7.420, QC=0.3948, FS=2.5, U=13.7, TA=2.75, B=23, %86484187  
D=7.440, QC=0.3901, FS=2.7, U=13.8, TA=2.70, B=20, %86485312  
D=7.460, QC=0.4924, FS=2.9, U=13.9, TA=2.71, B=14, %86486453  
D=7.480, QC=0.9687, FS=9.7, U=14.5, TA=2.72, B=18, %86487656  
D=7.500, QC=0.9739, FS=23.1, U=16.5, TA=2.68, B=18, %86488750  
D=7.520, QC=0.8788, FS=14.3, U=16.1, TA=2.65, B=18, %86489843  
D=7.540, QC=0.7807, FS=2.6, U=14.2, TA=2.64, B=18, %86490953  
D=7.560, QC=0.5355, FS=1.5, U=14.2, TA=2.65, B=18, %86492140  
D=7.580, QC=0.4586, FS=2.0, U=14.2, TA=2.65, B=18, %86493250  
D=7.600, QC=0.4244, FS=3.2, U=14.3, TA=2.65, B=18, %86493953  
D=7.620, QC=0.4654, FS=2.7, U=14.4, TA=2.64, B=18, %86495140  
D=7.640, QC=0.4768, FS=3.9, U=14.4, TA=2.64, B=20, %86496265  
D=7.660, QC=0.4841, FS=3.9, U=14.5, TA=2.65, B=20, %86497359  
D=7.680, QC=0.4586, FS=3.4, U=14.4, TA=2.65, B=19, %86498125  
D=7.700, QC=0.4451, FS=2.0, U=14.5, TA=2.64, B=18, %86499218  
D=7.720, QC=0.4514, FS=0.8, U=14.5, TA=2.65, B=21, %86500312  
D=7.740, QC=0.4488, FS=0.1, U=14.6, TA=2.65, B=21, %86501078  
D=7.760, QC=0.4358, FS=0.7, U=14.7, TA=2.65, B=19, %86502281  
D=7.780, QC=0.4280, FS=0.4, U=14.8, TA=2.65, B=19, %86503375  
D=7.800, QC=0.5532, FS=0.2, U=15.0, TA=2.65, B=19, %86504156  
D=7.820, QC=0.7563, FS=3.6, U=15.2, TA=2.65, B=19, %86505265  
D=7.840, QC=0.7329, FS=0.6, U=15.0, TA=2.65, B=20, %86506375

D=7.860, QC=0.6114, FS=2.1, U=15.1, TA=2.65, B=18, %86507500  
D=7.880, QC=0.4966, FS=3.1, U=15.1, TA=2.65, B=20, %86508281  
D=7.900, QC=0.3942, FS=4.8, U=15.2, TA=2.65, B=20, %86509375  
D=7.920, QC=0.3916, FS=5.5, U=15.3, TA=2.65, B=20, %86510156  
D=7.940, QC=0.3761, FS=4.7, U=15.3, TA=2.65, B=19, %86511250  
D=7.960, QC=0.3875, FS=4.5, U=15.3, TA=2.65, B=20, %86512343  
D=7.980, QC=0.4789, FS=4.3, U=15.4, TA=2.65, B=20, %86513109  
D=8.000, QC=0.5786, FS=3.2, U=15.7, TA=2.64, B=21, %86514203  
D=8.020, QC=0.5849, FS=0.1, U=15.5, TA=2.64, B=19, %86515406  
D=8.040, QC=0.5038, FS=0.3, U=15.6, TA=2.64, B=20, %86516093  
D=8.060, QC=0.4524, FS=3.2, U=15.7, TA=2.64, B=20, %86517265  
D=8.080, QC=0.4457, FS=3.6, U=15.8, TA=2.63, B=20, %86518031  
D=8.100, QC=0.4176, FS=3.8, U=15.7, TA=2.65, B=20, %86519062  
D=8.120, QC=0.4181, FS=5.0, U=15.8, TA=2.64, B=20, %86520187  
D=8.140, QC=0.4280, FS=4.7, U=15.8, TA=2.65, B=20, %86520968  
D=8.160, QC=0.4586, FS=4.8, U=16.0, TA=2.65, B=20, %86522078  
D=8.180, QC=0.4721, FS=1.9, U=16.0, TA=2.65, B=19, %86523281  
D=8.200, QC=0.4805, FS=1.7, U=16.1, TA=2.65, B=19, %86523937  
D=8.220, QC=0.4280, FS=1.8, U=16.1, TA=2.65, B=19, %86525062  
D=8.240, QC=0.4083, FS=1.8, U=16.2, TA=2.65, B=20, %86526265  
D=8.260, QC=0.4025, FS=1.9, U=16.3, TA=2.65, B=19, %86527375  
D=8.280, QC=0.4077, FS=2.0, U=16.3, TA=2.65, B=18, %86528140  
D=8.300, QC=0.4420, FS=3.1, U=16.4, TA=2.65, B=19, %86529250  
D=8.320, QC=0.6425, FS=3.7, U=16.5, TA=2.65, B=18, %86530359  
D=8.340, QC=0.7557, FS=5.3, U=16.7, TA=2.65, B=18, %86531453  
D=8.360, QC=0.8924, FS=10.7, U=17.1, TA=2.64, B=18, %86532656  
D=8.380, QC=0.9651, FS=34.2, U=19.6, TA=2.64, B=17, %86533765  
D=8.400, QC=0.9983, FS=40.2, U=19.1, TA=2.64, B=18, %86534890  
D=8.420, QC=0.7599, FS=10.0, U=19.7, TA=2.66, B=20, %86581109  
D=8.440, QC=0.7599, FS=10.0, U=19.7, TA=2.66, B=20, %86581109  
D=8.460, QC=0.6233, FS=10.0, U=19.7, TA=2.65, B=20, %86581437  
D=8.480, QC=0.4919, FS=10.4, U=16.7, TA=2.65, B=20, %86582203  
D=8.500, QC=0.4389, FS=10.4, U=18.7, TA=2.65, B=20, %86583312  
D=8.520, QC=0.4129, FS=9.4, U=18.6, TA=2.65, B=20, %86584109  
D=8.540, QC=0.3890, FS=8.5, U=16.4, TA=2.65, B=21, %86585203  
D=8.560, QC=0.3916, FS=7.4, U=18.7, TA=2.65, B=20, %86586296  
D=8.580, QC=0.3854, FS=4.8, U=18.7, TA=2.65, B=20, %86587062  
D=8.600, QC=0.3771, FS=3.3, U=18.8, TA=2.65, B=20, %86588171  
D=8.620, QC=0.3719, FS=2.0, U=16.5, TA=2.65, B=20, %86588937  
D=8.640, QC=0.3683, FS=1.3, U=16.7, TA=2.65, B=19, %86590046  
D=8.660, QC=0.3610, FS=1.1, U=19.0, TA=2.67, B=19, %86591250  
D=8.680, QC=0.3600, FS=1.1, U=19.0, TA=2.65, B=19, %86591937  
D=8.700, QC=0.3600, FS=1.4, U=19.2, TA=2.65, B=20, %86593125  
D=8.720, QC=0.3828, FS=1.4, U=19.2, TA=2.67, B=19, %86594234  
D=8.740, QC=0.4399, FS=1.6, U=19.3, TA=2.66, B=20, %86595000  
D=8.760, QC=0.5366, FS=2.3, U=19.4, TA=2.66, B=20, %86596093  
D=8.780, QC=0.6394, FS=3.9, U=19.6, TA=2.66, B=21, %86596859  
D=8.800, QC=0.9635, FS=15.8, U=20.6, TA=2.65, B=20, %86597953  
D=8.820, QC=0.9656, FS=37.7, U=22.2, TA=2.65, B=19, %86599078  
D=8.840, QC=0.9194, FS=44.5, U=24.8, TA=2.63, B=19, %86599843

D=8.860, QC=0.8716, FS=40.5, U=24.0, TA=2.63, B=21, %86600953  
D=8.880, QC=0.8581, FS=27.2, U=30.5, TA=2.65, B=20, %86601734  
D=8.900, QC=0.7963, FS=7.6, U=38.1, TA=2.64, B=20, %86602859  
D=8.920, QC=0.6804, FS=8.5, U=37.9, TA=2.65, B=22, %86603625  
D=8.940, QC=0.5610, FS=6.0, U=37.8, TA=2.65, B=23, %86604734  
D=8.960, QC=0.5719, FS=3.7, U=37.7, TA=2.65, B=22, %86605500  
D=8.980, QC=0.5220, FS=2.4, U=37.6, TA=2.65, B=22, %86606609  
D=9.000, QC=0.4711, FS=3.2, U=37.6, TA=2.65, B=22, %86607375  
D=9.020, QC=0.4322, FS=2.4, U=37.6, TA=2.65, B=23, %86608046  
D=9.040, QC=0.4503, FS=2.5, U=35.3, TA=2.65, B=23, %86609156  
D=9.060, QC=0.4742, FS=2.7, U=37.6, TA=2.65, B=22, %86609921  
D=9.080, QC=0.5080, FS=3.4, U=37.6, TA=2.65, B=22, %86610687  
D=9.100, QC=0.5786, FS=5.0, U=37.5, TA=2.65, B=22, %86611890  
D=9.120, QC=0.7173, FS=7.0, U=35.8, TA=2.65, B=22, %86612578  
D=9.140, QC=0.8991, FS=11.3, U=36.2, TA=2.65, B=21, %86613359  
D=9.160, QC=1.0368, FS=18.0, U=38.9, TA=2.59, B=21, %86614453  
D=9.180, QC=1.0549, FS=31.7, U=39.6, TA=2.59, B=22, %86615234  
D=9.200, QC=1.0648, FS=57.2, U=42.2, TA=2.59, B=21, %86616328  
D=9.220, QC=1.0445, FS=58.7, U=43.0, TA=2.59, B=20, %86617093  
D=9.240, QC=0.9640, FS=52.5, U=43.3, TA=2.58, B=19, %86618187  
D=9.260, QC=0.9095, FS=9.2, U=41.1, TA=2.63, B=21, %86619312  
D=9.280, QC=0.8357, FS=2.1, U=39.5, TA=2.61, B=21, %86620093  
D=9.300, QC=0.6181, FS=4.1, U=39.2, TA=2.59, B=21, %86621187  
D=9.320, QC=0.5989, FS=6.5, U=39.2, TA=2.59, B=21, %86621953  
D=9.340, QC=0.7173, FS=9.8, U=39.3, TA=2.59, B=22, %86622718  
D=9.360, QC=0.9453, FS=24.1, U=40.3, TA=2.60, B=21, %86623843  
D=9.380, QC=0.9630, FS=39.7, U=41.8, TA=2.61, B=21, %86624609  
D=9.400, QC=1.0316, FS=53.4, U=41.1, TA=2.61, B=20, %86625718  
D=9.420, QC=1.0181, FS=61.0, U=44.8, TA=2.59, B=20, %86626484  
D=9.440, QC=0.9490, FS=34.5, U=43.9, TA=2.58, B=20, %86627578  
D=9.460, QC=0.9142, FS=29.4, U=43.3, TA=2.59, B=20, %86628687  
D=9.480, QC=0.8866, FS=20.0, U=42.3, TA=2.59, B=20, %86629484  
D=9.500, QC=0.8581, FS=12.6, U=41.0, TA=2.63, B=21, %86630578  
D=9.520, QC=0.8788, FS=14.6, U=40.8, TA=2.63, B=21, %86631359  
D=9.540, QC=0.8326, FS=12.5, U=40.8, TA=2.64, B=20, %86632468  
D=9.560, QC=0.7698, FS=6.5, U=39.9, TA=2.60, B=20, %86633250  
D=9.580, QC=0.6436, FS=10.1, U=37.0, TA=2.64, B=21, %86634296  
D=9.600, QC=0.6436, FS=10.5, U=39.2, TA=2.64, B=21, %86635093, NA=0.0488, NB=-5.8, NC=14.9, F  
=15, K=90, T=The test are ended without any stop in the ground.

#\$

0:

1:

2:

3:

4:

5:

6:

7:

8:

9:

11:Tilt derivative alarm  
12:Point resistance alarm  
13:Depth unchanged for 5 second  
14:Transmission lost  
15:End of test  
16:Dissipation start

**CPT -6**  
**Raw Data**

\$  
HA=1,HB=1,HC=CPTLOG-2.00,HD=8/19/2020,HG=-0.732,HP=-0.73,HJ=Brenton  
CPT,HK=c6,HM=07,HN=3206,HO=0.00,HQ=SA,HR=0°0'0.000"E,HS=0°0'0.000"N,HX=0.00,HY=0.00  
,HZ=0.00,KQ=1468.00,KF=6200.00,KU=2136.00,MA=0.590,MB=0.011,MC=10.0,MD=150.0,ME=c6,  
MF=0.000  
RN=,CA=0,CB=0

#  
D=0.000, QC=0.0379, FS=1.5, U=2.5, TA=0.84, B=0, %148274546, NA=5.6388, NB=318.0, NC=440.8

D=0.020, QC=0.0467, FS=1.6, U=2.3, TA=0.85, B=12, %148275671

D=0.040, QC=0.0493, FS=2.0, U=2.4, TA=0.84, B=15, %148276796

D=0.060, QC=0.0519, FS=2.2, U=2.5, TA=0.89, B=20, %148277953

D=0.080, QC=0.0556, FS=2.4, U=2.5, TA=0.84, B=21, %148279046

D=0.100, QC=0.0566, FS=2.5, U=2.6, TA=0.85, B=20, %148279843

D=0.120, QC=0.0944, FS=2.6, U=2.7, TA=0.84, B=22, %148280937

D=0.140, QC=0.0980, FS=2.7, U=2.7, TA=0.82, B=22, %148281703

D=0.160, QC=0.0953, FS=2.7, U=2.8, TA=0.80, B=22, %148282515

D=0.180, QC=0.0969, FS=3.1, U=2.9, TA=0.77, B=23, %148283625

D=0.200, QC=0.0990, FS=3.2, U=3.0, TA=0.78, B=23, %148284390

D=0.220, QC=0.0931, FS=3.5, U=3.1, TA=0.80, B=24, %148285046

D=0.240, QC=0.0926, FS=3.6, U=3.1, TA=0.80, B=23, %148285812

D=0.260, QC=0.0926, FS=3.7, U=3.1, TA=0.83, B=22, %148287015

D=0.280, QC=0.1090, FS=3.7, U=3.2, TA=0.82, B=22, %148287687

D=0.300, QC=0.1043, FS=3.7, U=3.3, TA=0.82, B=24, %148288484

D=0.320, QC=0.1058, FS=3.5, U=3.4, TA=0.84, B=23, %148289156

D=0.340, QC=0.1090, FS=3.2, U=3.6, TA=0.82, B=22, %148290390

D=0.360, QC=0.1005, FS=3.3, U=3.7, TA=0.83, B=23, %148291062

D=0.380, QC=0.1064, FS=3.2, U=3.8, TA=0.83, B=25, %148291843

D=0.400, QC=0.1048, FS=3.1, U=3.9, TA=0.82, B=25, %148292640

D=0.420, QC=0.1053, FS=3.1, U=4.0, TA=0.82, B=25, %148293312

D=0.440, QC=0.1058, FS=2.9, U=4.1, TA=0.83, B=27, %148294109

D=0.460, QC=0.1053, FS=2.8, U=4.2, TA=0.83, B=29, %148294875

D=0.480, QC=0.1032, FS=3.1, U=4.3, TA=0.81, B=28, %148295578

D=0.500, QC=0.1048, FS=2.7, U=4.4, TA=0.81, B=27, %148296343

D=0.520, QC=0.1158, FS=2.6, U=4.5, TA=0.82, B=28, %148297125

D=0.540, QC=0.1164, FS=2.5, U=4.6, TA=0.83, B=28, %148297796

D=0.560, QC=0.1174, FS=2.5, U=4.7, TA=0.84, B=27, %148298593

D=0.580, QC=0.1190, FS=2.1, U=4.9, TA=0.82, B=25, %148299375

D=0.600, QC=0.1148, FS=3.1, U=10.3, TA=0.83, B=22, %148342156

D=0.620, QC=0.1148, FS=3.1, U=10.3, TA=0.83, B=22, %148342156

D=0.640, QC=0.1157, FS=3.0, U=10.0, TA=0.86, B=21, %148342906

D=0.660, QC=0.1141, FS=3.0, U=10.1, TA=0.85, B=19, %148343671

D=0.680, QC=0.1131, FS=2.8, U=10.1, TA=0.85, B=19, %148344828

D=0.700, QC=0.1147, FS=2.6, U=10.2, TA=0.87, B=18, %148345953

D=0.720, QC=0.1183, FS=2.6, U=10.4, TA=0.84, B=20, %148347062

D=0.740, QC=0.1193, FS=2.5, U=10.4, TA=0.85, B=20, %148347765

D=0.760, QC=0.1199, FS=2.2, U=10.7, TA=0.85, B=19, %148348906

D=0.780, QC=0.1183, FS=2.0, U=10.8, TA=0.85, B=18, %148350046

D=0.800, QC=0.1173, FS=1.7, U=10.9, TA=0.85, B=19, %148350843

D=0.820, QC=0.1173, FS=2.1, U=11.1, TA=0.86, B=19, %148351890

D=0.840, QC=0.1125, FS=2.0, U=11.2, TA=0.84, B=18, %148353109

D=0.860, QC=0.1130, FS=2.4, U=11.4, TA=0.83, B=19, %148354218  
D=0.880, QC=0.1125, FS=2.1, U=9.2, TA=0.84, B=19, %148354890  
D=0.900, QC=0.1125, FS=2.0, U=11.6, TA=0.86, B=19, %148356109  
D=0.920, QC=0.1119, FS=2.3, U=11.7, TA=0.85, B=19, %148357250  
D=0.940, QC=0.1183, FS=2.5, U=9.6, TA=0.83, B=19, %148358281  
D=0.960, QC=0.1193, FS=2.7, U=12.0, TA=0.82, B=19, %148359062  
D=0.980, QC=0.1104, FS=2.9, U=9.9, TA=0.83, B=19, %148360171  
D=1.000, QC=0.1102, FS=2.8, U=10.0, TA=0.82, B=19, %148361343  
D=1.020, QC=0.1170, FS=2.8, U=10.1, TA=0.81, B=20, %148362109  
D=1.040, QC=0.1293, FS=2.6, U=10.4, TA=0.82, B=21, %148363218  
D=1.060, QC=0.1865, FS=2.3, U=10.5, TA=0.80, B=20, %148364312  
D=1.080, QC=0.2067, FS=2.2, U=10.6, TA=0.81, B=21, %148365078  
D=1.100, QC=0.2239, FS=2.7, U=10.9, TA=0.80, B=20, %148366187  
D=1.120, QC=0.2914, FS=1.2, U=11.0, TA=0.80, B=21, %148366968  
D=1.140, QC=0.4379, FS=2.0, U=11.1, TA=0.80, B=20, %148368093  
D=1.160, QC=0.4831, FS=2.3, U=11.1, TA=0.80, B=21, %148368875  
D=1.180, QC=0.5428, FS=2.8, U=11.1, TA=0.80, B=20, %148369984  
D=1.200, QC=0.5776, FS=2.7, U=11.2, TA=0.80, B=21, %148370640  
D=1.220, QC=0.5179, FS=2.2, U=11.3, TA=0.80, B=20, %148371781  
D=1.240, QC=0.5999, FS=4.3, U=11.7, TA=0.80, B=20, %148372921  
D=1.260, QC=0.7713, FS=14.5, U=12.9, TA=0.80, B=20, %148373718  
D=1.280, QC=0.8492, FS=23.3, U=14.1, TA=0.80, B=20, %148374843  
D=1.300, QC=0.8331, FS=23.6, U=14.2, TA=0.80, B=20, %148375609  
D=1.320, QC=0.8082, FS=12.9, U=13.5, TA=0.80, B=19, %148376718  
D=1.340, QC=0.7708, FS=7.8, U=13.2, TA=0.80, B=20, %148377828  
D=1.360, QC=0.7282, FS=3.2, U=13.0, TA=0.80, B=20, %148378625  
D=1.380, QC=0.6233, FS=2.1, U=12.3, TA=0.80, B=20, %148379734  
D=1.400, QC=0.5308, FS=2.5, U=12.3, TA=0.80, B=21, %148380406  
D=1.420, QC=0.4737, FS=1.4, U=12.5, TA=0.80, B=20, %148381609  
D=1.440, QC=0.5708, FS=2.8, U=12.5, TA=0.80, B=21, %148382265  
D=1.460, QC=0.7880, FS=14.2, U=13.9, TA=0.80, B=20, %148383406  
D=1.480, QC=0.7895, FS=12.4, U=12.0, TA=0.80, B=19, %148384625  
D=1.500, QC=0.6986, FS=5.9, U=13.6, TA=0.80, B=20, %148385296  
D=1.520, QC=0.5480, FS=2.1, U=12.6, TA=0.80, B=21, %148386453  
D=1.540, QC=0.4145, FS=1.0, U=10.5, TA=0.80, B=20, %148387234  
D=1.560, QC=0.2618, FS=0.4, U=10.6, TA=0.80, B=20, %148388328  
D=1.580, QC=0.2239, FS=0.8, U=10.8, TA=0.80, B=20, %148389453  
D=1.600, QC=0.2176, FS=1.5, U=11.0, TA=0.80, B=20, %148390218  
D=1.620, QC=0.2940, FS=2.1, U=11.1, TA=0.80, B=20, %148391312  
D=1.640, QC=0.3350, FS=2.2, U=11.3, TA=0.80, B=20, %148392109  
D=1.660, QC=0.3667, FS=2.3, U=9.4, TA=0.80, B=19, %148393250  
D=1.680, QC=0.3958, FS=2.5, U=9.5, TA=0.80, B=20, %148394343  
D=1.700, QC=0.4057, FS=2.7, U=9.6, TA=0.80, B=19, %148395015  
D=1.720, QC=0.3823, FS=1.9, U=9.7, TA=0.80, B=19, %148396156  
D=1.740, QC=0.4025, FS=0.9, U=9.8, TA=0.80, B=19, %148397281  
D=1.760, QC=0.5033, FS=0.7, U=10.0, TA=0.80, B=14, %148398421  
D=1.780, QC=0.4649, FS=1.3, U=12.0, TA=0.81, B=22, %148441453  
D=1.800, QC=0.4649, FS=1.3, U=12.0, TA=0.81, B=22, %148441453  
D=1.820, QC=0.3870, FS=1.3, U=12.0, TA=0.80, B=23, %148441796  
D=1.840, QC=0.3496, FS=1.3, U=11.6, TA=0.80, B=21, %148442578

D=1.860, QC=0.3329, FS=2.3, U=11.7, TA=0.80, B=17, %148443671  
D=1.880, QC=0.3303, FS=2.6, U=11.8, TA=0.80, B=17, %148444812  
D=1.900, QC=0.3002, FS=2.9, U=11.8, TA=0.80, B=17, %148445937  
D=1.920, QC=0.2898, FS=3.3, U=11.9, TA=0.80, B=18, %148447046  
D=1.940, QC=0.3698, FS=3.5, U=12.0, TA=0.80, B=18, %148448140  
D=1.960, QC=0.5547, FS=4.0, U=12.2, TA=0.80, B=17, %148449359  
D=1.980, QC=0.5490, FS=3.2, U=12.2, TA=0.80, B=17, %148450468  
D=2.000, QC=0.3600, FS=2.0, U=12.1, TA=0.80, B=17, %148451609  
D=2.020, QC=0.2955, FS=1.6, U=12.3, TA=0.80, B=17, %148452640  
D=2.040, QC=0.2239, FS=1.3, U=12.4, TA=0.80, B=17, %148453796  
D=2.060, QC=0.2394, FS=1.5, U=12.6, TA=0.80, B=17, %148454906  
D=2.080, QC=0.2914, FS=1.8, U=12.6, TA=0.80, B=18, %148456109  
D=2.100, QC=0.3101, FS=2.9, U=12.8, TA=0.80, B=18, %148457203  
D=2.120, QC=0.2774, FS=3.4, U=12.9, TA=0.80, B=17, %148458328  
D=2.140, QC=0.2826, FS=3.5, U=13.2, TA=0.80, B=17, %148459437  
D=2.160, QC=0.3329, FS=2.9, U=13.2, TA=0.80, B=18, %148460531  
D=2.180, QC=0.3387, FS=2.8, U=13.3, TA=0.80, B=17, %148461734  
D=2.200, QC=0.2841, FS=3.1, U=13.3, TA=0.80, B=17, %148462828  
D=2.220, QC=0.2737, FS=3.6, U=13.5, TA=0.80, B=18, %148463953  
D=2.240, QC=0.2940, FS=3.2, U=13.7, TA=0.80, B=18, %148464718  
D=2.260, QC=0.3828, FS=3.4, U=13.9, TA=0.80, B=18, %148465828  
D=2.280, QC=0.3838, FS=2.9, U=14.0, TA=0.81, B=18, %148466937  
D=2.300, QC=0.2950, FS=3.1, U=14.0, TA=0.80, B=18, %148468031  
D=2.320, QC=0.2737, FS=2.7, U=14.2, TA=0.80, B=19, %148469250  
D=2.340, QC=0.3558, FS=1.9, U=14.2, TA=0.80, B=19, %148470343  
D=2.360, QC=0.3771, FS=2.2, U=14.2, TA=0.80, B=19, %148471000  
D=2.380, QC=0.3600, FS=2.8, U=14.5, TA=0.80, B=19, %148472203  
D=2.400, QC=0.2976, FS=3.9, U=14.5, TA=0.81, B=20, %148473312  
D=2.420, QC=0.2893, FS=4.4, U=14.7, TA=0.80, B=19, %148474437  
D=2.440, QC=0.3278, FS=4.1, U=14.9, TA=0.80, B=19, %148475203  
D=2.460, QC=0.5054, FS=3.7, U=15.0, TA=0.80, B=19, %148476312  
D=2.480, QC=0.5615, FS=4.3, U=15.0, TA=0.80, B=20, %148477421  
D=2.500, QC=0.5106, FS=4.2, U=15.1, TA=0.80, B=19, %148478218  
D=2.520, QC=0.4384, FS=5.2, U=12.7, TA=0.80, B=19, %148479328  
D=2.540, QC=0.3916, FS=3.8, U=12.9, TA=0.80, B=19, %148480437  
D=2.560, QC=0.3174, FS=2.7, U=13.0, TA=0.81, B=21, %148481562  
D=2.580, QC=0.2857, FS=2.3, U=13.0, TA=0.80, B=19, %148482343  
D=2.600, QC=0.3194, FS=3.7, U=13.2, TA=0.80, B=19, %148483453  
D=2.620, QC=0.4202, FS=4.3, U=13.4, TA=0.80, B=19, %148484546  
D=2.640, QC=0.3802, FS=4.3, U=13.4, TA=0.80, B=20, %148485343  
D=2.660, QC=0.3402, FS=4.8, U=11.3, TA=0.80, B=19, %148486453  
D=2.680, QC=0.2509, FS=5.1, U=11.3, TA=0.80, B=18, %148487546  
D=2.700, QC=0.2306, FS=3.6, U=11.5, TA=0.80, B=19, %148488640  
D=2.720, QC=0.2182, FS=2.9, U=11.7, TA=0.80, B=19, %148489421  
D=2.740, QC=0.2659, FS=2.4, U=11.8, TA=0.80, B=19, %148490546  
D=2.760, QC=0.3189, FS=2.8, U=12.0, TA=0.80, B=19, %148491656  
D=2.780, QC=0.3428, FS=2.9, U=12.1, TA=0.80, B=18, %148492765  
D=2.800, QC=0.3127, FS=2.7, U=12.3, TA=0.80, B=19, %148493984  
D=2.820, QC=0.2789, FS=3.4, U=12.4, TA=0.80, B=19, %148494640  
D=2.840, QC=0.3101, FS=3.4, U=12.5, TA=0.80, B=18, %148495843



D=2.860, QC=0.3662, FS=3.4, U=12.7, TA=0.80, B=18, %148496937  
D=2.880, QC=0.3413, FS=3.4, U=12.8, TA=0.80, B=18, %148498062  
D=2.900, QC=0.3002, FS=4.0, U=12.9, TA=0.80, B=18, %148499171  
D=2.920, QC=0.2613, FS=4.3, U=12.9, TA=0.80, B=18, %148500265  
D=2.940, QC=0.2488, FS=3.5, U=13.1, TA=0.80, B=18, %148501031  
D=2.960, QC=0.2327, FS=2.6, U=13.2, TA=0.80, B=18, %148502171  
D=2.980, QC=0.4560, FS=6.1, U=17.6, TA=0.81, B=0, %148551593  
D=3.000, QC=0.6649, FS=6.1, U=17.6, TA=0.80, B=16, %148552031  
D=3.020, QC=0.5116, FS=5.8, U=17.3, TA=0.80, B=13, %148553500  
D=3.040, QC=0.3698, FS=4.2, U=17.4, TA=0.80, B=15, %148555046  
D=3.060, QC=0.3215, FS=5.2, U=17.4, TA=0.80, B=15, %148556171  
D=3.080, QC=0.2763, FS=5.4, U=17.5, TA=0.80, B=16, %148557296  
D=3.100, QC=0.2654, FS=4.6, U=17.6, TA=0.80, B=15, %148558718  
D=3.120, QC=0.2561, FS=3.5, U=17.7, TA=0.80, B=15, %148559859  
D=3.140, QC=0.2410, FS=3.8, U=17.8, TA=0.80, B=14, %148561421  
D=3.160, QC=0.2322, FS=4.3, U=18.0, TA=0.80, B=12, %148562875  
D=3.180, QC=0.2233, FS=4.3, U=18.1, TA=0.80, B=10, %148564765  
D=3.200, QC=0.2187, FS=3.0, U=16.1, TA=0.80, B=10, %148566578  
D=3.220, QC=0.2119, FS=2.9, U=18.7, TA=0.80, B=10, %148568484  
D=3.240, QC=0.2171, FS=2.4, U=16.6, TA=0.80, B=10, %148570390  
D=3.260, QC=0.2218, FS=2.5, U=16.7, TA=0.80, B=10, %148572281  
D=3.280, QC=0.2280, FS=2.3, U=17.0, TA=0.80, B=10, %148574171  
D=3.300, QC=0.2374, FS=2.8, U=17.2, TA=0.80, B=10, %148575984  
D=3.320, QC=0.2265, FS=2.5, U=17.5, TA=0.80, B=11, %148577875  
D=3.340, QC=0.2187, FS=2.6, U=17.7, TA=0.80, B=11, %148579343  
D=3.360, QC=0.2130, FS=2.6, U=18.0, TA=0.80, B=11, %148581234  
D=3.380, QC=0.2197, FS=2.7, U=18.1, TA=0.80, B=12, %148582765  
D=3.400, QC=0.2233, FS=2.4, U=18.3, TA=0.80, B=13, %148584234  
D=3.420, QC=0.2259, FS=2.8, U=18.6, TA=0.80, B=12, %148586109  
D=3.440, QC=0.2233, FS=2.6, U=18.8, TA=0.80, B=13, %148587687  
D=3.460, QC=0.2254, FS=2.3, U=19.0, TA=0.80, B=12, %148589140  
D=3.480, QC=0.2208, FS=2.0, U=19.2, TA=0.80, B=13, %148590671  
D=3.500, QC=0.2223, FS=1.8, U=19.3, TA=0.80, B=14, %148592125  
D=3.520, QC=0.2202, FS=1.9, U=19.6, TA=0.80, B=13, %148593687  
D=3.540, QC=0.2176, FS=1.9, U=19.8, TA=0.80, B=13, %148595125  
D=3.560, QC=0.2192, FS=2.0, U=19.9, TA=0.80, B=14, %148596218  
D=3.580, QC=0.2192, FS=2.1, U=20.1, TA=0.80, B=13, %148597750  
D=3.600, QC=0.2249, FS=2.0, U=20.3, TA=0.79, B=14, %148599312  
D=3.620, QC=0.2265, FS=2.0, U=20.5, TA=0.80, B=14, %148600765  
D=3.640, QC=0.2296, FS=2.1, U=20.7, TA=0.75, B=14, %148602296  
D=3.660, QC=0.2301, FS=2.3, U=21.0, TA=0.77, B=14, %148603718  
D=3.680, QC=0.2301, FS=2.5, U=21.2, TA=0.77, B=14, %148604859  
D=3.700, QC=0.2317, FS=2.6, U=21.3, TA=0.76, B=13, %148606421  
D=3.720, QC=0.2296, FS=2.8, U=21.6, TA=0.75, B=14, %148607859  
D=3.740, QC=0.2265, FS=3.1, U=19.5, TA=0.73, B=13, %148609343  
D=3.760, QC=0.2254, FS=3.2, U=21.9, TA=0.73, B=14, %148610453  
D=3.780, QC=0.2233, FS=3.3, U=22.1, TA=0.73, B=14, %148611984  
D=3.800, QC=0.2182, FS=3.2, U=22.3, TA=0.71, B=15, %148613531  
D=3.820, QC=0.2187, FS=3.1, U=20.3, TA=0.71, B=14, %148614656  
D=3.840, QC=0.2202, FS=3.1, U=20.6, TA=0.70, B=15, %148616093

D=3.860, QC=0.2233, FS=3.0, U=20.6, TA=0.71, B=15, %148617234  
D=3.880, QC=0.2280, FS=2.9, U=20.9, TA=0.71, B=15, %148618796  
D=3.900, QC=0.2317, FS=2.7, U=21.0, TA=0.70, B=15, %148619921  
D=3.920, QC=0.2363, FS=2.7, U=21.2, TA=0.70, B=15, %148621359  
D=3.940, QC=0.2379, FS=2.8, U=21.3, TA=0.70, B=15, %148622468  
D=3.960, QC=0.2415, FS=3.2, U=21.5, TA=0.70, B=15, %148624046  
D=3.980, QC=0.2426, FS=3.4, U=21.7, TA=0.70, B=15, %148625171  
D=4.000, QC=0.2394, FS=3.5, U=21.8, TA=0.70, B=16, %148626281  
D=4.020, QC=0.2431, FS=3.8, U=22.0, TA=0.70, B=16, %148627718  
D=4.040, QC=0.2509, FS=4.0, U=19.9, TA=0.70, B=16, %148628843  
D=4.060, QC=0.2441, FS=4.1, U=20.1, TA=0.70, B=16, %148629953  
D=4.080, QC=0.2436, FS=3.9, U=20.3, TA=0.70, B=17, %148631156  
D=4.100, QC=0.2431, FS=3.8, U=20.4, TA=0.70, B=17, %148632250  
D=4.120, QC=0.2420, FS=3.6, U=20.7, TA=0.70, B=17, %148633359  
D=4.140, QC=0.2431, FS=3.5, U=20.8, TA=0.70, B=17, %148634484  
D=4.160, QC=0.2483, FS=3.5, U=20.9, TA=0.70, B=17, %148635687  
D=4.180, QC=0.2509, FS=3.4, U=21.1, TA=0.72, B=16, %148636812  
D=4.200, QC=0.2420, FS=3.7, U=26.1, TA=0.73, B=18, %148676546  
D=4.220, QC=0.2420, FS=3.7, U=26.1, TA=0.73, B=18, %148676546  
D=4.240, QC=0.3439, FS=4.0, U=25.7, TA=0.73, B=16, %148677312  
D=4.260, QC=0.3568, FS=3.8, U=25.2, TA=0.72, B=20, %148677984  
D=4.280, QC=0.4098, FS=4.2, U=25.4, TA=0.70, B=19, %148679093  
D=4.300, QC=0.4337, FS=5.1, U=25.4, TA=0.70, B=22, %148679875  
D=4.320, QC=0.4161, FS=4.6, U=25.7, TA=0.70, B=23, %148680984  
D=4.340, QC=0.3999, FS=5.4, U=25.7, TA=0.70, B=18, %148682125  
D=4.360, QC=0.3522, FS=5.2, U=26.0, TA=0.70, B=17, %148683218  
D=4.380, QC=0.3636, FS=4.8, U=26.0, TA=0.70, B=18, %148684343  
D=4.400, QC=0.3480, FS=6.2, U=26.4, TA=0.70, B=17, %148685453  
D=4.420, QC=0.3361, FS=6.4, U=26.5, TA=0.69, B=18, %148686671  
D=4.440, QC=0.3226, FS=7.4, U=26.7, TA=0.68, B=17, %148687781  
D=4.460, QC=0.3127, FS=7.7, U=26.8, TA=0.68, B=17, %148688890  
D=4.480, QC=0.3080, FS=8.2, U=26.9, TA=0.66, B=17, %148690031  
D=4.500, QC=0.3033, FS=7.9, U=27.1, TA=0.65, B=18, %148691125  
D=4.520, QC=0.3039, FS=7.3, U=27.3, TA=0.65, B=17, %148692218  
D=4.540, QC=0.3127, FS=7.3, U=27.4, TA=0.64, B=17, %148693421  
D=4.560, QC=0.3142, FS=6.8, U=27.5, TA=0.64, B=18, %148694546  
D=4.580, QC=0.3122, FS=6.5, U=27.7, TA=0.64, B=18, %148695656  
D=4.600, QC=0.3111, FS=5.9, U=27.9, TA=0.64, B=18, %148696750  
D=4.620, QC=0.3080, FS=5.9, U=27.9, TA=0.64, B=19, %148697531  
D=4.640, QC=0.2981, FS=6.1, U=28.1, TA=0.64, B=18, %148698640  
D=4.660, QC=0.2935, FS=5.9, U=28.2, TA=0.64, B=19, %148699765  
D=4.680, QC=0.2909, FS=5.7, U=28.3, TA=0.65, B=18, %148700859  
D=4.700, QC=0.2893, FS=5.5, U=28.5, TA=0.64, B=19, %148702062  
D=4.720, QC=0.2940, FS=5.5, U=28.6, TA=0.64, B=18, %148703171  
D=4.740, QC=0.2929, FS=5.4, U=28.7, TA=0.64, B=19, %148703828  
D=4.760, QC=0.2955, FS=5.1, U=28.9, TA=0.64, B=18, %148705046  
D=4.780, QC=0.3059, FS=5.0, U=28.9, TA=0.64, B=19, %148706187  
D=4.800, QC=0.3075, FS=5.0, U=29.2, TA=0.64, B=19, %148707296  
D=4.820, QC=0.3065, FS=5.2, U=29.3, TA=0.64, B=19, %148708406  
D=4.840, QC=0.3049, FS=5.2, U=29.4, TA=0.64, B=19, %148709078

D=4.860, QC=0.3049, FS=5.3, U=29.5, TA=0.64, B=19, %148710281  
D=4.880, QC=0.3007, FS=5.3, U=29.7, TA=0.64, B=18, %148711375  
D=4.900, QC=0.3049, FS=5.5, U=29.9, TA=0.64, B=19, %148712484  
D=4.920, QC=0.3106, FS=5.5, U=30.0, TA=0.64, B=18, %148713578  
D=4.940, QC=0.3116, FS=5.7, U=30.1, TA=0.64, B=19, %148714812  
D=4.960, QC=0.3127, FS=5.7, U=30.1, TA=0.64, B=19, %148715468  
D=4.980, QC=0.3111, FS=5.6, U=30.3, TA=0.64, B=18, %148716687  
D=5.000, QC=0.3101, FS=5.8, U=30.5, TA=0.64, B=18, %148717781  
D=5.020, QC=0.3111, FS=5.9, U=30.5, TA=0.64, B=19, %148718875  
D=5.040, QC=0.3122, FS=6.1, U=30.7, TA=0.64, B=18, %148719984  
D=5.060, QC=0.3127, FS=6.3, U=30.8, TA=0.64, B=18, %148721093  
D=5.080, QC=0.3137, FS=6.3, U=30.9, TA=0.64, B=18, %148721890  
D=5.100, QC=0.3163, FS=6.1, U=31.1, TA=0.64, B=19, %148722984  
D=5.120, QC=0.3200, FS=6.0, U=31.2, TA=0.64, B=18, %148724093  
D=5.140, QC=0.3179, FS=6.0, U=31.4, TA=0.64, B=19, %148725296  
D=5.160, QC=0.3101, FS=6.0, U=31.4, TA=0.64, B=18, %148726406  
D=5.180, QC=0.3080, FS=5.8, U=31.6, TA=0.64, B=18, %148727546  
D=5.200, QC=0.3049, FS=5.8, U=31.7, TA=0.64, B=19, %148728671  
D=5.220, QC=0.3018, FS=5.8, U=31.8, TA=0.64, B=19, %148729359  
D=5.240, QC=0.3106, FS=5.8, U=29.8, TA=0.64, B=18, %148730500  
D=5.260, QC=0.3142, FS=5.8, U=29.8, TA=0.64, B=19, %148731609  
D=5.280, QC=0.3111, FS=5.3, U=32.3, TA=0.64, B=19, %148732750  
D=5.300, QC=0.3127, FS=5.1, U=30.1, TA=0.64, B=20, %148733531  
D=5.320, QC=0.3091, FS=5.3, U=30.3, TA=0.64, B=19, %148734671  
D=5.340, QC=0.3059, FS=5.3, U=30.4, TA=0.64, B=19, %148735796  
D=5.360, QC=0.2852, FS=4.9, U=30.5, TA=0.64, B=18, %148736890  
D=5.380, QC=0.3096, FS=6.5, U=32.2, TA=0.65, B=26, %148772343  
D=5.400, QC=0.3096, FS=6.5, U=32.2, TA=0.65, B=26, %148772343  
D=5.420, QC=0.3101, FS=6.5, U=32.2, TA=0.64, B=26, %148772781  
D=5.440, QC=0.3096, FS=5.6, U=31.8, TA=0.64, B=22, %148773890  
D=5.460, QC=0.2955, FS=5.5, U=31.8, TA=0.64, B=20, %148774671  
D=5.480, QC=0.2815, FS=5.5, U=31.9, TA=0.64, B=18, %148775796  
D=5.500, QC=0.2774, FS=5.3, U=31.9, TA=0.64, B=19, %148776906  
D=5.520, QC=0.2717, FS=5.3, U=32.1, TA=0.64, B=18, %148778046  
D=5.540, QC=0.2685, FS=5.2, U=32.2, TA=0.64, B=18, %148779140  
D=5.560, QC=0.2701, FS=5.4, U=34.8, TA=0.64, B=13, %148780265  
D=5.580, QC=0.3605, FS=5.8, U=35.0, TA=0.64, B=16, %148781703  
D=5.600, QC=0.4966, FS=6.9, U=32.9, TA=0.64, B=16, %148782937  
D=5.620, QC=0.8217, FS=10.2, U=33.0, TA=0.64, B=16, %148784046  
D=5.640, QC=0.8570, FS=23.5, U=34.7, TA=0.64, B=15, %148785500  
D=5.660, QC=0.8524, FS=30.2, U=35.7, TA=0.64, B=16, %148786656  
D=5.680, QC=0.8950, FS=36.2, U=36.4, TA=0.65, B=16, %148787781  
D=5.700, QC=0.9801, FS=45.3, U=37.6, TA=0.64, B=15, %148789234  
D=5.720, QC=1.0149, FS=48.3, U=38.2, TA=0.64, B=15, %148790343  
D=5.740, QC=0.9703, FS=46.9, U=38.2, TA=0.64, B=15, %148791562  
D=5.760, QC=0.7822, FS=19.2, U=36.1, TA=0.64, B=15, %148793031  
D=5.780, QC=0.7194, FS=3.9, U=34.1, TA=0.64, B=16, %148794156  
D=5.800, QC=0.5906, FS=3.2, U=33.4, TA=0.64, B=16, %148795265  
D=5.820, QC=0.6472, FS=4.5, U=33.6, TA=0.63, B=17, %148796359  
D=5.840, QC=0.8170, FS=9.8, U=34.4, TA=0.64, B=16, %148797562

D=5.860, QC=0.8508, FS=17.9, U=35.6, TA=0.64, B=17, %148798671  
D=5.880, QC=0.8321, FS=19.1, U=35.7, TA=0.65, B=17, %148799781  
D=5.900, QC=0.8451, FS=29.9, U=36.4, TA=0.68, B=17, %148801218  
D=5.920, QC=0.8404, FS=31.6, U=37.5, TA=0.69, B=16, %148802437  
D=5.940, QC=0.8555, FS=29.2, U=37.2, TA=0.67, B=16, %148803531  
D=5.960, QC=0.8939, FS=39.8, U=37.3, TA=0.67, B=17, %148804578  
D=5.980, QC=0.9744, FS=44.8, U=38.0, TA=0.65, B=17, %148805703  
D=6.000, QC=1.0222, FS=52.7, U=39.8, TA=0.69, B=16, %148806921  
D=6.020, QC=1.1069, FS=55.9, U=40.1, TA=0.70, B=16, %148808015  
D=6.040, QC=1.1354, FS=59.9, U=40.6, TA=0.69, B=16, %148809515  
D=6.060, QC=1.1193, FS=60.1, U=41.0, TA=0.69, B=17, %148810640  
D=6.080, QC=1.0227, FS=59.5, U=41.0, TA=0.68, B=16, %148811734  
D=6.100, QC=0.9147, FS=52.7, U=40.5, TA=0.70, B=16, %148812859  
D=6.120, QC=0.8113, FS=39.3, U=40.0, TA=0.69, B=16, %148813953  
D=6.140, QC=0.7791, FS=15.3, U=36.8, TA=0.69, B=17, %148815171  
D=6.160, QC=0.6747, FS=12.2, U=35.7, TA=0.68, B=17, %148816281  
D=6.180, QC=0.5958, FS=16.4, U=35.1, TA=0.68, B=16, %148817718  
D=6.200, QC=0.5875, FS=20.7, U=35.3, TA=0.69, B=17, %148818859  
D=6.220, QC=0.7168, FS=20.7, U=35.3, TA=0.69, B=17, %148819968  
D=6.240, QC=0.6846, FS=19.2, U=35.8, TA=0.68, B=16, %148821062  
D=6.260, QC=0.6275, FS=16.2, U=35.9, TA=0.68, B=16, %148822265  
D=6.280, QC=0.6451, FS=16.8, U=36.3, TA=0.67, B=16, %148823359  
D=6.300, QC=0.7651, FS=22.8, U=37.7, TA=0.68, B=17, %148824453  
D=6.320, QC=0.9095, FS=41.1, U=40.1, TA=0.68, B=16, %148826031  
D=6.340, QC=1.1645, FS=77.0, U=44.5, TA=0.69, B=15, %148827140  
D=6.360, QC=1.8372, FS=84.1, U=45.5, TA=0.68, B=15, %148828265  
D=6.380, QC=2.3483, FS=89.8, U=47.1, TA=0.69, B=15, %148829718  
D=6.400, QC=3.0744, FS=91.6, U=47.8, TA=0.69, B=13, %148831250  
D=6.420, QC=3.6650, FS=93.5, U=48.0, TA=0.68, B=13, %148832703  
D=6.440, QC=3.8198, FS=94.7, U=48.1, TA=0.68, B=12, %148834250  
D=6.460, QC=3.4110, FS=88.0, U=48.2, TA=0.69, B=13, %148835812  
D=6.480, QC=3.1902, FS=87.6, U=48.3, TA=0.67, B=13, %148837296  
D=6.500, QC=2.7898, FS=84.9, U=48.8, TA=0.69, B=15, %148838390  
D=6.520, QC=1.6060, FS=80.7, U=47.5, TA=0.68, B=15, %148839859  
D=6.540, QC=0.9749, FS=80.1, U=46.7, TA=0.66, B=16, %148840968  
D=6.560, QC=1.0248, FS=80.9, U=50.5, TA=0.60, B=21, %148879875  
D=6.580, QC=1.0248, FS=80.9, U=50.5, TA=0.60, B=21, %148879875  
D=6.600, QC=1.0248, FS=80.9, U=50.5, TA=0.60, B=21, %148879875  
D=6.620, QC=1.0445, FS=83.0, U=50.3, TA=0.60, B=20, %148880640  
D=6.640, QC=1.1827, FS=85.2, U=50.8, TA=0.60, B=21, %148881750  
D=6.660, QC=1.1199, FS=82.1, U=51.1, TA=0.60, B=14, %148882890  
D=6.680, QC=1.1661, FS=81.6, U=51.1, TA=0.60, B=13, %148884328  
D=6.700, QC=1.3977, FS=85.1, U=52.1, TA=0.60, B=13, %148885875  
D=6.720, QC=1.7468, FS=88.8, U=53.1, TA=0.61, B=14, %148887328  
D=6.740, QC=2.0377, FS=88.6, U=53.2, TA=0.61, B=13, %148888875  
D=6.760, QC=2.2735, FS=87.1, U=52.9, TA=0.61, B=12, %148890296  
D=6.780, QC=2.4392, FS=85.0, U=52.4, TA=0.61, B=12, %148891828  
D=6.800, QC=2.4766, FS=82.2, U=52.5, TA=0.61, B=13, %148893375  
D=6.820, QC=2.5425, FS=82.1, U=52.5, TA=0.61, B=12, %148894796  
D=6.840, QC=2.6324, FS=83.3, U=52.7, TA=0.61, B=13, %148896375

D=6.860, QC=2.7742, FS=84.2, U=52.8, TA=0.61, B=11, %148898265  
D=6.880, QC=2.8651, FS=85.3, U=52.9, TA=0.62, B=12, %148899718  
D=6.900, QC=2.9181, FS=87.6, U=52.9, TA=0.64, B=11, %148901625  
D=6.920, QC=2.9549, FS=89.9, U=53.1, TA=0.64, B=11, %148903062  
D=6.940, QC=3.0064, FS=91.8, U=53.2, TA=0.64, B=10, %148904937  
D=6.960, QC=2.9887, FS=92.8, U=53.1, TA=0.65, B=10, %148906828  
D=6.980, QC=2.8708, FS=93.0, U=53.2, TA=0.65, B=11, %148908734  
D=7.000, QC=2.7700, FS=94.4, U=53.4, TA=0.65, B=12, %148910156  
D=7.020, QC=2.7555, FS=96.5, U=53.3, TA=0.65, B=11, %148912062  
D=7.040, QC=2.8318, FS=98.2, U=53.3, TA=0.64, B=12, %148913609  
D=7.060, QC=3.0962, FS=100.2, U=53.3, TA=0.63, B=11, %148915484  
D=7.080, QC=3.2993, FS=102.5, U=53.4, TA=0.61, B=12, %148916937  
D=7.100, QC=3.4344, FS=104.1, U=53.7, TA=0.61, B=11, %148918828  
D=7.120, QC=3.6188, FS=104.4, U=53.8, TA=0.59, B=11, %148920734  
D=7.140, QC=3.6925, FS=103.6, U=53.9, TA=0.63, B=11, %148922203  
D=7.160, QC=3.7881, FS=104.9, U=53.9, TA=0.61, B=11, %148924109  
D=7.180, QC=3.9875, FS=105.6, U=54.0, TA=0.59, B=11, %148925546  
D=7.200, QC=4.2961, FS=107.0, U=54.2, TA=0.58, B=17, %148927125  
D=7.220, QC=4.4400, FS=107.1, U=54.3, TA=0.59, B=17, %148928250  
D=7.240, QC=4.4228, FS=106.8, U=54.3, TA=0.59, B=17, %148929343  
D=7.260, QC=4.2483, FS=107.1, U=54.3, TA=0.58, B=17, %148930437  
D=7.280, QC=4.1179, FS=107.3, U=54.1, TA=0.57, B=16, %148931531  
D=7.300, QC=3.8452, FS=107.3, U=54.0, TA=0.59, B=15, %148932656  
D=7.320, QC=3.5414, FS=104.7, U=53.8, TA=0.60, B=12, %148934562  
D=7.340, QC=3.0318, FS=102.2, U=53.7, TA=0.57, B=11, %148936125  
D=7.360, QC=1.0892, FS=85.8, U=58.5, TA=0.69, B=19, %149099015  
D=7.380, QC=1.0892, FS=85.8, U=58.5, TA=0.69, B=19, %149099015  
D=7.400, QC=0.8705, FS=75.9, U=56.4, TA=0.58, B=19, %149099796  
D=7.420, QC=0.7713, FS=64.9, U=55.1, TA=0.59, B=18, %149100890  
D=7.440, QC=0.7396, FS=55.8, U=53.0, TA=0.58, B=19, %149101671  
D=7.460, QC=0.7017, FS=42.5, U=49.8, TA=0.60, B=18, %149102812  
D=7.480, QC=0.6882, FS=35.9, U=49.4, TA=0.60, B=18, %149103906  
D=7.500, QC=0.6825, FS=24.3, U=49.2, TA=0.58, B=18, %149105015  
D=7.520, QC=0.6789, FS=20.2, U=49.4, TA=0.59, B=19, %149106109  
D=7.540, QC=0.6794, FS=12.4, U=49.7, TA=0.60, B=18, %149107312  
D=7.560, QC=0.6763, FS=8.0, U=49.9, TA=0.60, B=18, %149107984  
D=7.580, QC=0.6685, FS=6.3, U=50.2, TA=0.59, B=17, %149109203  
D=7.600, QC=0.6685, FS=4.5, U=50.8, TA=0.60, B=17, %149110312  
D=7.620, QC=0.6674, FS=4.2, U=51.2, TA=0.60, B=18, %149111437  
D=7.640, QC=0.6737, FS=4.2, U=51.8, TA=0.59, B=17, %149112546  
D=7.660, QC=0.6955, FS=4.5, U=52.7, TA=0.59, B=15, %149114093  
D=7.680, QC=0.7464, FS=5.0, U=53.2, TA=0.60, B=16, %149115203  
D=7.700, QC=0.7781, FS=6.1, U=54.3, TA=0.60, B=16, %149116312  
D=7.720, QC=0.8067, FS=8.6, U=55.6, TA=0.60, B=15, %149117750  
D=7.740, QC=0.7848, FS=9.8, U=56.3, TA=0.60, B=14, %149118890  
D=7.760, QC=0.8222, FS=10.5, U=59.7, TA=0.60, B=14, %149120468  
D=7.780, QC=0.4150, FS=1.0, U=103.0, TA=0.61, B=13, %149176718  
D=7.800, QC=0.4914, FS=1.4, U=103.0, TA=0.59, B=14, %149177484  
D=7.820, QC=0.6119, FS=2.2, U=104.2, TA=0.59, B=12, %149178953  
D=7.840, QC=0.8820, FS=11.6, U=108.6, TA=0.57, B=12, %149180515

D=7.860, QC=0.9500, FS=18.9, U=111.8, TA=0.57, B=11, %149182375  
D=7.880, QC=0.9646, FS=26.2, U=115.7, TA=0.57, B=10, %149184281  
D=7.900, QC=0.8939, FS=26.2, U=115.7, TA=0.57, B=10, %149186140  
D=7.920, QC=0.8804, FS=23.6, U=111.1, TA=0.59, B=10, %149188031  
D=7.940, QC=0.8975, FS=34.0, U=111.6, TA=0.60, B=10, %149189906  
D=7.960, QC=0.8331, FS=26.5, U=110.3, TA=0.60, B=10, %149191703  
D=7.980, QC=0.7791, FS=19.4, U=105.1, TA=0.60, B=11, %149193593  
D=8.000, QC=0.6841, FS=20.6, U=102.4, TA=0.60, B=11, %149195140  
D=8.020, QC=0.5947, FS=25.7, U=101.6, TA=0.60, B=12, %149196593  
D=8.040, QC=0.5594, FS=25.7, U=101.3, TA=0.60, B=12, %149198484  
D=8.060, QC=0.5579, FS=24.2, U=101.3, TA=0.60, B=13, %149199609  
D=8.080, QC=0.5340, FS=18.9, U=101.6, TA=0.60, B=14, %149201171  
D=8.100, QC=0.5101, FS=15.0, U=101.7, TA=0.60, B=15, %149202625  
D=8.120, QC=0.5033, FS=10.0, U=102.0, TA=0.60, B=15, %149203718  
D=8.140, QC=0.5111, FS=6.5, U=102.2, TA=0.60, B=16, %149204921  
D=8.160, QC=0.5355, FS=3.2, U=102.5, TA=0.60, B=15, %149206359  
D=8.180, QC=0.5464, FS=4.0, U=102.7, TA=0.60, B=17, %149207484  
D=8.200, QC=0.5542, FS=5.0, U=102.8, TA=0.60, B=19, %149208593  
D=8.220, QC=0.5651, FS=5.8, U=103.1, TA=0.60, B=20, %149209359  
D=8.240, QC=0.5599, FS=6.5, U=103.1, TA=0.60, B=21, %149210453  
D=8.260, QC=0.5381, FS=6.7, U=103.4, TA=0.60, B=22, %149211218  
D=8.280, QC=0.4436, FS=7.5, U=103.5, TA=0.60, B=23, %149212328  
D=8.300, QC=0.4436, FS=7.6, U=103.7, TA=0.60, B=23, %149213125  
D=8.320, QC=0.4488, FS=7.6, U=103.8, TA=0.60, B=23, %149213906  
D=8.340, QC=0.4633, FS=7.8, U=103.9, TA=0.60, B=25, %149214671  
D=8.360, QC=0.4592, FS=7.3, U=104.0, TA=0.60, B=24, %149215343  
D=8.380, QC=0.4851, FS=6.6, U=104.2, TA=0.60, B=28, %149216109  
D=8.400, QC=0.7173, FS=5.2, U=104.3, TA=0.60, B=28, %149216890  
D=8.420, QC=1.0331, FS=17.6, U=107.1, TA=0.60, B=27, %149217656  
D=8.440, QC=1.1495, FS=51.1, U=116.7, TA=0.60, B=25, %149218328  
D=8.460, QC=1.2881, FS=71.6, U=122.3, TA=0.60, B=22, %149219125  
D=8.480, QC=1.4564, FS=78.7, U=121.8, TA=0.61, B=14, %149220671  
D=8.500, QC=1.5951, FS=81.3, U=109.9, TA=0.66, B=20, %149221781  
D=8.520, QC=1.6232, FS=82.3, U=94.5, TA=0.68, B=13, %149223203  
D=8.540, QC=1.8756, FS=85.7, U=91.7, TA=0.65, B=13, %149224421  
D=8.560, QC=1.6465, FS=84.6, U=90.4, TA=0.62, B=13, %149225859  
D=8.580, QC=1.0326, FS=72.2, U=105.9, TA=0.61, B=14, %149227328  
D=8.600, QC=0.8975, FS=63.3, U=120.5, TA=0.62, B=14, %149228890  
D=8.620, QC=0.9988, FS=57.1, U=121.1, TA=0.60, B=14, %149230328  
D=8.640, QC=0.9671, FS=55.9, U=119.8, TA=0.60, B=14, %149231531  
D=8.660, QC=0.8331, FS=36.6, U=115.8, TA=0.60, B=15, %149233015  
D=8.680, QC=0.8077, FS=34.9, U=111.3, TA=0.60, B=14, %149234468  
D=8.700, QC=0.8466, FS=39.8, U=111.1, TA=0.60, B=15, %149235578  
D=8.720, QC=1.1110, FS=61.0, U=115.9, TA=0.60, B=15, %149237140  
D=8.740, QC=1.1074, FS=80.2, U=119.6, TA=0.60, B=17, %149238234  
D=8.760, QC=1.0269, FS=81.8, U=120.2, TA=0.66, B=18, %149239328  
D=8.780, QC=1.1900, FS=80.5, U=120.3, TA=0.65, B=19, %149240125  
D=8.800, QC=1.2897, FS=78.7, U=120.7, TA=0.66, B=18, %149241203  
D=8.820, QC=0.8716, FS=68.3, U=120.0, TA=0.67, B=20, %149242421  
D=8.840, QC=0.8596, FS=32.2, U=113.6, TA=0.68, B=20, %149243546

D=8.860, QC=0.8217, FS=23.3, U=110.0, TA=0.67, B=21, %149244203  
D=8.880, QC=0.7438, FS=22.8, U=108.1, TA=0.68, B=19, %149245328  
D=8.900, QC=0.7396, FS=25.0, U=105.8, TA=0.68, B=21, %149246453  
D=8.920, QC=0.7786, FS=27.1, U=106.6, TA=0.68, B=21, %149247234  
D=8.940, QC=0.8295, FS=29.1, U=107.5, TA=0.68, B=22, %149248015  
D=8.960, QC=0.9235, FS=51.5, U=111.6, TA=0.68, B=20, %149249140  
D=8.980, QC=1.0986, FS=88.8, U=120.0, TA=0.67, B=21, %149250265  
D=9.000, QC=1.4746, FS=86.1, U=121.5, TA=0.68, B=20, %149251031  
D=9.020, QC=2.1228, FS=83.0, U=121.8, TA=0.67, B=21, %149252140  
D=9.040, QC=2.4901, FS=83.8, U=121.9, TA=0.68, B=21, %149252921  
D=9.060, QC=2.7628, FS=86.1, U=122.7, TA=0.68, B=20, %149254015  
D=9.080, QC=1.5873, FS=88.0, U=119.8, TA=0.65, B=16, %149307468  
D=9.100, QC=2.5223, FS=87.3, U=120.4, TA=0.60, B=15, %149308562  
D=9.120, QC=2.6033, FS=83.8, U=120.8, TA=0.60, B=15, %149309703  
D=9.140, QC=2.3478, FS=82.6, U=120.7, TA=0.61, B=17, %149310796  
D=9.160, QC=2.2397, FS=82.9, U=120.7, TA=0.64, B=19, %149311937  
D=9.180, QC=1.8346, FS=81.7, U=120.5, TA=0.71, B=19, %149313031  
D=9.200, QC=1.4159, FS=81.7, U=120.1, TA=0.73, B=19, %149313812  
D=9.220, QC=0.9349, FS=63.1, U=117.2, TA=0.74, B=19, %149314921  
D=9.240, QC=0.8269, FS=50.6, U=113.6, TA=0.77, B=21, %149316015  
D=9.260, QC=0.8124, FS=45.5, U=109.3, TA=0.77, B=21, %149316781  
D=9.280, QC=0.7635, FS=41.7, U=105.1, TA=0.77, B=21, %149317875  
D=9.300, QC=0.7022, FS=40.2, U=104.5, TA=0.77, B=20, %149318640  
D=9.320, QC=0.6539, FS=37.6, U=104.6, TA=0.77, B=20, %149319781  
D=9.340, QC=0.6628, FS=30.9, U=106.1, TA=0.77, B=19, %149320890  
D=9.360, QC=0.7069, FS=29.3, U=107.1, TA=0.77, B=19, %149321671  
D=9.380, QC=0.8840, FS=40.1, U=111.4, TA=0.77, B=17, %149322796  
D=9.400, QC=0.9183, FS=62.6, U=119.9, TA=0.77, B=17, %149323890  
D=9.420, QC=0.9095, FS=42.0, U=119.7, TA=0.77, B=16, %149325437  
D=9.440, QC=0.8466, FS=28.4, U=117.1, TA=0.77, B=17, %149326546  
D=9.460, QC=0.8492, FS=30.5, U=114.2, TA=0.77, B=16, %149327656  
D=9.480, QC=0.9323, FS=46.2, U=117.4, TA=0.77, B=16, %149328796  
D=9.500, QC=1.0035, FS=67.1, U=122.3, TA=0.77, B=17, %149329890  
D=9.520, QC=1.1105, FS=74.5, U=123.9, TA=0.78, B=16, %149331093  
D=9.540, QC=1.4372, FS=87.8, U=125.9, TA=0.77, B=15, %149332531  
D=9.560, QC=1.3754, FS=82.0, U=125.7, TA=0.78, B=16, %149333656  
D=9.580, QC=1.4424, FS=81.8, U=125.5, TA=0.77, B=16, %149334796  
D=9.600, QC=1.5681, FS=81.6, U=125.3, TA=0.80, B=17, %149336328  
D=9.620, QC=1.5411, FS=77.0, U=125.3, TA=0.80, B=15, %149337421  
D=9.640, QC=1.2788, FS=74.3, U=125.0, TA=0.84, B=15, %149338546  
D=9.660, QC=1.0258, FS=72.5, U=123.8, TA=0.87, B=15, %149340000  
D=9.680, QC=0.9495, FS=56.2, U=121.9, TA=0.88, B=15, %149341109  
D=9.700, QC=0.8846, FS=45.0, U=120.0, TA=0.88, B=15, %149342328  
D=9.720, QC=0.8638, FS=36.4, U=117.2, TA=0.87, B=16, %149343828  
D=9.740, QC=0.8622, FS=37.7, U=116.1, TA=0.88, B=16, %149344937  
D=9.760, QC=0.8705, FS=36.8, U=115.5, TA=0.88, B=17, %149346062  
D=9.780, QC=0.8331, FS=23.3, U=110.9, TA=0.88, B=17, %149347171  
D=9.800, QC=0.7635, FS=19.8, U=109.4, TA=0.88, B=18, %149348265  
D=9.820, QC=0.7620, FS=19.5, U=108.3, TA=0.88, B=16, %149349359  
D=9.840, QC=0.8300, FS=20.8, U=108.6, TA=0.88, B=17, %149350515

D=9.860, QC=0.8492, FS=21.9, U=109.1, TA=0.88, B=16, %149351656  
D=9.880, QC=0.7776, FS=19.4, U=108.9, TA=0.88, B=16, %149352796  
D=9.900, QC=0.6680, FS=16.0, U=108.3, TA=0.88, B=16, %149354234  
D=9.920, QC=0.6285, FS=15.0, U=107.8, TA=0.88, B=16, %149355453  
D=9.940, QC=0.6139, FS=13.2, U=107.8, TA=0.88, B=15, %149356593  
D=9.960, QC=0.6311, FS=11.1, U=108.0, TA=0.88, B=15, %149358046  
D=9.980, QC=0.6191, FS=9.7, U=108.3, TA=0.88, B=15, %149359156  
D=10.000, QC=0.5958, FS=10.1, U=108.5, TA=0.88, B=15, %149360265  
D=10.020, QC=0.7074, FS=9.0, U=109.0, TA=0.88, B=16, %149361843  
D=10.040, QC=0.8565, FS=24.5, U=114.6, TA=0.88, B=17, %149362937  
D=10.060, QC=0.8903, FS=35.6, U=118.6, TA=0.88, B=17, %149364031  
D=10.080, QC=0.8679, FS=18.5, U=116.0, TA=0.88, B=18, %149365125  
D=10.100, QC=0.7594, FS=12.4, U=112.8, TA=0.88, B=17, %149366343  
D=10.120, QC=0.6737, FS=14.3, U=110.4, TA=0.88, B=18, %149367453  
D=10.140, QC=0.5942, FS=14.9, U=110.4, TA=0.88, B=18, %149368562  
D=10.160, QC=0.5895, FS=16.1, U=110.6, TA=0.88, B=18, %149369656  
D=10.180, QC=0.6062, FS=15.9, U=110.6, TA=0.88, B=17, %149370750  
D=10.200, QC=0.6098, FS=15.2, U=111.1, TA=0.88, B=17, %149371875  
D=10.220, QC=0.5968, FS=14.2, U=111.2, TA=0.88, B=17, %149373000  
D=10.240, QC=0.5859, FS=9.6, U=111.6, TA=0.88, B=17, %149374125  
D=10.260, QC=0.5859, FS=9.6, U=111.7, TA=0.88, B=17, %149375328, NA=0.0789, NB=-2.6, NC=7.0,  
F=15, K=90, T=The test are ended without any stop in the ground.

#\$

0:

1:

2:

3:

4:

5:

6:

7:

8:

9:

11:Tilt derivative alarm

12:Point resistance alarm

13:Depth unchanged for 5 second

14:Transmission lost

15:End of test

16:Dissipation start



**CPT -7**  
**Raw Data**

\$  
HA=1,HB=1,HC=CPTLOG-2.00,HD=8/19/2020,HG=-1.158,HP=-1.16,HJ=Brenton  
CPT,HK=c7,HM=07,HN=3206,HO=0.00,HQ=SA,HR=0°0'0.000"E,HS=0°0'0.000"N,HX=0.00,HY=0.00  
,HZ=0.00,KQ=1468.00,KF=6200.00,KU=2136.00,MA=0.590,MB=0.011,MC=10.0,MD=150.0,ME=c7,  
MF=0.000  
RN=,CA=0,CB=0

#  
D=0.000, QC=0.0031, FS=0.0, U=0.3, TA=0.38, B=0, %150825437, NA=5.6871, NB=315.5, NC=441.5

D=0.020, QC=0.0571, FS=3.0, U=3.4, TA=1.82, B=18, %150854046

D=0.040, QC=0.0535, FS=3.1, U=3.4, TA=1.86, B=20, %150854718

D=0.060, QC=0.0545, FS=3.0, U=3.4, TA=1.91, B=20, %150855859

D=0.080, QC=0.0566, FS=3.0, U=3.5, TA=1.86, B=21, %150856656

D=0.100, QC=0.0587, FS=2.9, U=3.6, TA=1.84, B=21, %150857765

D=0.120, QC=0.0587, FS=2.8, U=3.6, TA=1.87, B=21, %150858531

D=0.140, QC=0.0577, FS=2.5, U=3.7, TA=2.08, B=21, %150859656

D=0.160, QC=0.0603, FS=2.3, U=3.7, TA=2.09, B=21, %150860343

D=0.180, QC=0.0670, FS=2.2, U=3.7, TA=1.88, B=21, %150861468

D=0.200, QC=0.0691, FS=2.2, U=3.9, TA=1.85, B=21, %150862250

D=0.220, QC=0.0706, FS=2.6, U=4.0, TA=1.90, B=21, %150863421

D=0.240, QC=0.0701, FS=2.6, U=4.1, TA=1.93, B=22, %150864078

D=0.260, QC=0.0706, FS=2.7, U=4.2, TA=1.98, B=20, %150865234

D=0.280, QC=0.0675, FS=2.8, U=4.2, TA=1.99, B=19, %150866031

D=0.300, QC=0.0980, FS=2.9, U=4.3, TA=2.01, B=20, %150867156

D=0.320, QC=0.0991, FS=3.0, U=4.4, TA=2.00, B=22, %150867921

D=0.340, QC=0.0917, FS=3.0, U=4.5, TA=2.03, B=21, %150868953

D=0.360, QC=0.0917, FS=3.1, U=4.5, TA=1.93, B=22, %150869750

D=0.380, QC=0.0906, FS=3.0, U=4.6, TA=2.01, B=23, %150870437

D=0.400, QC=0.0991, FS=3.0, U=4.7, TA=1.98, B=25, %150871656

D=0.420, QC=0.0991, FS=1.9, U=8.9, TA=1.98, B=25, %150872312

D=0.440, QC=0.0930, FS=1.9, U=8.9, TA=1.62, B=18, %150912156

D=0.460, QC=0.0930, FS=1.9, U=8.9, TA=1.62, B=18, %150912156

D=0.480, QC=0.0944, FS=1.7, U=8.5, TA=1.64, B=18, %150912828

D=0.500, QC=0.0912, FS=1.4, U=8.6, TA=1.66, B=13, %150913937

D=0.520, QC=0.0953, FS=1.0, U=8.7, TA=1.63, B=20, %150915156

D=0.540, QC=0.0974, FS=1.2, U=8.8, TA=1.65, B=19, %150916187

D=0.560, QC=0.0984, FS=1.3, U=8.9, TA=1.63, B=19, %150916968

D=0.580, QC=0.1074, FS=1.4, U=9.1, TA=1.63, B=21, %150918109

D=0.600, QC=0.1074, FS=1.5, U=9.1, TA=1.65, B=20, %150919234

D=0.620, QC=0.1084, FS=1.6, U=9.3, TA=1.66, B=20, %150920015

D=0.640, QC=0.1079, FS=1.7, U=9.4, TA=1.63, B=19, %150921125

D=0.660, QC=0.1026, FS=1.8, U=9.5, TA=1.63, B=20, %150922234

D=0.680, QC=0.1047, FS=1.9, U=9.6, TA=1.63, B=20, %150923031

D=0.700, QC=0.1057, FS=1.0, U=9.7, TA=1.63, B=19, %150924140

D=0.720, QC=0.1083, FS=1.9, U=9.9, TA=1.63, B=19, %150925281

D=0.740, QC=0.1004, FS=1.0, U=10.0, TA=1.62, B=21, %150925937

D=0.760, QC=0.1093, FS=1.8, U=10.1, TA=1.63, B=20, %150927140

D=0.780, QC=0.1099, FS=1.8, U=10.2, TA=1.63, B=20, %150927812

D=0.800, QC=0.1040, FS=1.7, U=10.3, TA=1.62, B=19, %150928937

D=0.820, QC=0.1040, FS=1.7, U=10.5, TA=1.62, B=21, %150930062

D=0.840, QC=0.1025, FS=1.8, U=10.6, TA=1.61, B=20, %150930843

D=0.860, QC=0.1009, FS=1.8, U=10.7, TA=1.63, B=20, %150931953  
D=0.880, QC=0.1019, FS=1.9, U=10.8, TA=1.61, B=21, %150932750  
D=0.900, QC=0.1014, FS=1.9, U=11.0, TA=1.61, B=21, %150933890  
D=0.920, QC=0.1025, FS=1.6, U=11.1, TA=1.62, B=22, %150934562  
D=0.940, QC=0.1099, FS=1.8, U=9.0, TA=1.62, B=21, %150935703  
D=0.960, QC=0.1019, FS=1.5, U=9.1, TA=1.63, B=21, %150936484  
D=0.980, QC=0.1030, FS=1.8, U=9.4, TA=1.62, B=21, %150937593  
D=1.000, QC=0.1030, FS=1.6, U=9.5, TA=1.62, B=18, %150938359  
D=1.020, QC=0.1045, FS=1.7, U=9.6, TA=1.63, B=17, %150939484  
D=1.040, QC=0.1071, FS=1.8, U=9.8, TA=1.62, B=19, %150940625  
D=1.060, QC=0.1049, FS=1.4, U=9.9, TA=1.62, B=19, %150941750  
D=1.080, QC=0.1049, FS=1.4, U=10.1, TA=1.62, B=19, %150942515  
D=1.100, QC=0.1054, FS=1.8, U=10.3, TA=1.62, B=20, %150943625  
D=1.120, QC=0.1096, FS=1.8, U=10.5, TA=1.61, B=19, %150944765  
D=1.140, QC=0.1163, FS=1.1, U=10.6, TA=1.61, B=20, %150945437  
D=1.160, QC=0.1200, FS=1.0, U=10.9, TA=1.61, B=19, %150946578  
D=1.180, QC=0.1408, FS=1.9, U=11.0, TA=1.61, B=20, %150947781  
D=1.200, QC=0.1522, FS=1.6, U=11.3, TA=1.61, B=19, %150948921  
D=1.220, QC=0.1579, FS=1.3, U=9.2, TA=1.61, B=20, %150949578  
D=1.240, QC=0.1480, FS=1.0, U=9.3, TA=1.61, B=19, %150950687  
D=1.260, QC=0.1397, FS=0.6, U=9.5, TA=1.61, B=19, %150951906  
D=1.280, QC=0.1361, FS=0.7, U=9.6, TA=1.61, B=19, %150952593  
D=1.300, QC=0.1610, FS=0.7, U=9.7, TA=1.61, B=20, %150953703  
D=1.320, QC=0.1698, FS=1.0, U=10.0, TA=1.61, B=19, %150954921  
D=1.340, QC=0.1974, FS=1.0, U=10.1, TA=1.61, B=19, %150956015  
D=1.360, QC=0.2062, FS=1.8, U=10.2, TA=1.63, B=19, %150956703  
D=1.380, QC=0.2088, FS=1.3, U=10.6, TA=1.61, B=20, %150957843  
D=1.400, QC=0.2150, FS=1.6, U=10.7, TA=1.61, B=19, %150958937  
D=1.420, QC=0.1943, FS=2.1, U=10.8, TA=1.61, B=19, %150959734  
D=1.440, QC=0.1787, FS=1.1, U=11.0, TA=1.61, B=18, %150960875  
D=1.460, QC=0.1756, FS=1.6, U=11.1, TA=1.61, B=19, %150962000  
D=1.480, QC=0.1771, FS=1.1, U=11.3, TA=1.61, B=19, %150963109  
D=1.500, QC=0.1875, FS=1.0, U=11.4, TA=1.61, B=18, %150964265  
D=1.520, QC=0.2317, FS=0.6, U=11.5, TA=1.61, B=18, %150965031  
D=1.540, QC=0.2805, FS=0.7, U=11.8, TA=1.61, B=18, %150966125  
D=1.560, QC=0.3288, FS=0.8, U=11.9, TA=1.61, B=18, %150967234  
D=1.580, QC=0.3350, FS=1.0, U=12.1, TA=1.61, B=19, %150968359  
D=1.600, QC=0.2800, FS=0.8, U=12.2, TA=1.61, B=17, %150969453  
D=1.620, QC=0.2504, FS=0.6, U=13.9, TA=1.61, B=15, %151010875  
D=1.640, QC=0.2504, FS=0.6, U=13.9, TA=1.61, B=15, %151010875  
D=1.660, QC=0.2976, FS=1.0, U=13.6, TA=1.61, B=15, %151011984  
D=1.680, QC=0.2394, FS=1.9, U=13.6, TA=1.61, B=14, %151013546  
D=1.700, QC=0.2176, FS=2.2, U=13.8, TA=1.61, B=15, %151014656  
D=1.720, QC=0.2301, FS=1.8, U=13.9, TA=1.61, B=15, %151015765  
D=1.740, QC=0.2737, FS=1.2, U=14.0, TA=1.61, B=14, %151017203  
D=1.760, QC=0.2722, FS=1.1, U=14.1, TA=1.61, B=14, %151018796  
D=1.780, QC=0.2566, FS=1.9, U=14.2, TA=1.61, B=14, %151019921  
D=1.800, QC=0.3288, FS=2.3, U=14.2, TA=1.61, B=14, %151021375  
D=1.820, QC=0.4176, FS=2.1, U=14.4, TA=1.61, B=15, %151022828  
D=1.840, QC=0.3948, FS=2.0, U=14.5, TA=1.61, B=25, %151023968

D=1.860, QC=0.4155, FS=2.3, U=14.5, TA=1.61, B=21, %151024765  
D=1.880, QC=0.4986, FS=3.7, U=14.6, TA=1.61, B=17, %151026203  
D=1.900, QC=0.5267, FS=3.2, U=14.7, TA=1.61, B=18, %151027343  
D=1.920, QC=0.5495, FS=3.3, U=14.7, TA=1.61, B=17, %151028468  
D=1.940, QC=0.5095, FS=2.9, U=14.9, TA=1.61, B=18, %151029593  
D=1.960, QC=0.4025, FS=3.1, U=15.0, TA=1.61, B=18, %151030718  
D=1.980, QC=0.3771, FS=3.8, U=15.0, TA=1.61, B=18, %151031515  
D=2.000, QC=0.3454, FS=3.2, U=15.2, TA=1.61, B=18, %151032671  
D=2.020, QC=0.2836, FS=1.7, U=15.3, TA=1.61, B=18, %151033718  
D=2.040, QC=0.2498, FS=2.4, U=15.4, TA=1.61, B=19, %151034843  
D=2.060, QC=0.4399, FS=3.5, U=15.5, TA=1.61, B=20, %151035968  
D=2.080, QC=0.6171, FS=4.3, U=15.4, TA=1.61, B=18, %151036734  
D=2.100, QC=0.7085, FS=6.1, U=16.0, TA=1.61, B=18, %151037859  
D=2.120, QC=0.7547, FS=10.1, U=16.7, TA=1.61, B=19, %151038968  
D=2.140, QC=0.7822, FS=20.8, U=18.0, TA=1.61, B=19, %151040078  
D=2.160, QC=0.7807, FS=18.2, U=15.5, TA=1.62, B=18, %151041312  
D=2.180, QC=0.7376, FS=11.2, U=17.6, TA=1.62, B=18, %151042000  
D=2.200, QC=0.6659, FS=1.6, U=16.8, TA=1.62, B=19, %151043093  
D=2.220, QC=0.4124, FS=1.1, U=14.2, TA=1.61, B=19, %151044218  
D=2.240, QC=0.3563, FS=3.0, U=16.7, TA=1.61, B=19, %151045343  
D=2.260, QC=0.3262, FS=4.6, U=14.3, TA=1.62, B=19, %151046140  
D=2.280, QC=0.3272, FS=6.7, U=14.3, TA=1.62, B=19, %151047281  
D=2.300, QC=0.3548, FS=7.4, U=14.5, TA=1.62, B=19, %151048421  
D=2.320, QC=0.5241, FS=7.1, U=14.5, TA=1.63, B=19, %151049531  
D=2.340, QC=0.5412, FS=6.5, U=12.2, TA=1.63, B=19, %151050296  
D=2.360, QC=0.4747, FS=5.7, U=14.6, TA=1.63, B=19, %151051421  
D=2.380, QC=0.3309, FS=5.3, U=12.4, TA=1.63, B=18, %151052515  
D=2.400, QC=0.3116, FS=3.9, U=14.9, TA=1.63, B=19, %151053609  
D=2.420, QC=0.3355, FS=3.2, U=12.6, TA=1.63, B=19, %151054718  
D=2.440, QC=0.3366, FS=3.2, U=12.7, TA=1.63, B=19, %151055515  
D=2.460, QC=0.2940, FS=3.4, U=12.9, TA=1.63, B=19, %151056609  
D=2.480, QC=0.2457, FS=3.0, U=13.0, TA=1.63, B=18, %151057734  
D=2.500, QC=0.2472, FS=3.9, U=13.2, TA=1.63, B=19, %151058843  
D=2.520, QC=0.3007, FS=3.8, U=13.2, TA=1.63, B=19, %151059656  
D=2.540, QC=0.3413, FS=3.2, U=13.1, TA=1.63, B=18, %151060781  
D=2.560, QC=0.3174, FS=2.6, U=13.4, TA=1.63, B=17, %151061921  
D=2.580, QC=0.4109, FS=3.0, U=13.4, TA=1.63, B=19, %151063031  
D=2.600, QC=0.3890, FS=2.9, U=13.5, TA=1.63, B=18, %151064171  
D=2.620, QC=0.3075, FS=3.6, U=13.6, TA=1.63, B=18, %151065281  
D=2.640, QC=0.2794, FS=4.5, U=13.7, TA=1.63, B=17, %151066406  
D=2.660, QC=0.2587, FS=4.7, U=13.8, TA=1.63, B=18, %151067515  
D=2.680, QC=0.2665, FS=5.5, U=14.0, TA=1.63, B=18, %151068656  
D=2.700, QC=0.3080, FS=4.3, U=14.1, TA=1.63, B=18, %151069765  
D=2.720, QC=0.2929, FS=3.7, U=14.2, TA=1.63, B=16, %151070906  
D=2.740, QC=0.2436, FS=3.3, U=14.3, TA=1.63, B=16, %151072031 , F=13  
D=2.760, QC=0.2691, FS=4.8, U=15.1, TA=1.59, B=19, %151135046  
D=2.780, QC=0.2665, FS=4.8, U=15.1, TA=1.58, B=18, %151135390  
D=2.800, QC=0.2519, FS=4.3, U=14.8, TA=1.56, B=18, %151136187  
D=2.820, QC=0.2400, FS=5.2, U=14.7, TA=1.57, B=19, %151137296  
D=2.840, QC=0.2400, FS=4.5, U=14.8, TA=1.60, B=19, %151138421

D=2.860, QC=0.2675, FS=4.0, U=15.0, TA=1.58, B=19, %151139546  
D=2.880, QC=0.3002, FS=3.6, U=15.0, TA=1.60, B=18, %151140328  
D=2.900, QC=0.2997, FS=3.1, U=15.0, TA=1.59, B=19, %151141468  
D=2.920, QC=0.2794, FS=4.3, U=15.2, TA=1.58, B=19, %151142578  
D=2.940, QC=0.2550, FS=3.8, U=15.2, TA=1.59, B=18, %151143703  
D=2.960, QC=0.2623, FS=3.4, U=15.3, TA=1.62, B=18, %151144375  
D=2.980, QC=0.2805, FS=3.1, U=15.5, TA=1.57, B=18, %151145593  
D=3.000, QC=0.3215, FS=3.2, U=15.5, TA=1.65, B=18, %151146703  
D=3.020, QC=0.3080, FS=3.4, U=15.6, TA=1.65, B=18, %151147812  
D=3.040, QC=0.2535, FS=4.2, U=15.7, TA=1.61, B=17, %151148937  
D=3.060, QC=0.2462, FS=3.0, U=15.8, TA=1.65, B=19, %151150062  
D=3.080, QC=0.2509, FS=2.9, U=15.8, TA=1.62, B=20, %151150750  
D=3.100, QC=0.2623, FS=2.7, U=15.8, TA=1.67, B=18, %151151875  
D=3.120, QC=0.2530, FS=2.7, U=16.0, TA=1.68, B=18, %151153031  
D=3.140, QC=0.2509, FS=3.3, U=16.1, TA=1.68, B=19, %151154125  
D=3.160, QC=0.2452, FS=3.4, U=16.1, TA=1.69, B=20, %151154906  
D=3.180, QC=0.2358, FS=2.7, U=16.3, TA=1.67, B=20, %151156031  
D=3.200, QC=0.2244, FS=3.2, U=16.3, TA=1.69, B=19, %151157140  
D=3.220, QC=0.2249, FS=2.8, U=16.5, TA=1.70, B=20, %151157937  
D=3.240, QC=0.2233, FS=2.6, U=16.6, TA=1.69, B=21, %151159000  
D=3.260, QC=0.2249, FS=2.5, U=16.7, TA=1.65, B=21, %151159828  
D=3.280, QC=0.2233, FS=2.1, U=16.7, TA=1.63, B=20, %151160921  
D=3.300, QC=0.2259, FS=2.0, U=17.0, TA=1.69, B=21, %151162078  
D=3.320, QC=0.2265, FS=1.7, U=17.0, TA=1.64, B=21, %151162765  
D=3.340, QC=0.2275, FS=1.5, U=17.1, TA=1.68, B=21, %151163968  
D=3.360, QC=0.2301, FS=1.5, U=17.2, TA=1.69, B=20, %151164656  
D=3.380, QC=0.2317, FS=1.7, U=17.4, TA=1.67, B=21, %151165781  
D=3.400, QC=0.2301, FS=1.8, U=17.5, TA=1.71, B=21, %151166562  
D=3.420, QC=0.2301, FS=2.1, U=17.6, TA=1.71, B=22, %151167671  
D=3.440, QC=0.2317, FS=2.3, U=17.6, TA=1.71, B=21, %151168468  
D=3.460, QC=0.2317, FS=2.6, U=17.8, TA=1.70, B=21, %151169500  
D=3.480, QC=0.2317, FS=2.8, U=17.9, TA=1.73, B=21, %151170296  
D=3.500, QC=0.2322, FS=2.9, U=18.0, TA=1.71, B=21, %151171390  
D=3.520, QC=0.2327, FS=2.8, U=18.1, TA=1.73, B=20, %151172171  
D=3.540, QC=0.2358, FS=2.8, U=18.2, TA=1.75, B=21, %151173265  
D=3.560, QC=0.2446, FS=2.8, U=18.4, TA=1.76, B=21, %151174046  
D=3.580, QC=0.2607, FS=2.7, U=18.4, TA=1.76, B=21, %151175171  
D=3.600, QC=0.2519, FS=2.6, U=18.5, TA=1.76, B=21, %151175859  
D=3.620, QC=0.2488, FS=2.8, U=16.5, TA=1.77, B=21, %151177062  
D=3.640, QC=0.2348, FS=2.5, U=16.5, TA=1.79, B=21, %151177750  
D=3.660, QC=0.2420, FS=2.4, U=16.6, TA=1.78, B=21, %151178875  
D=3.680, QC=0.2379, FS=2.5, U=16.8, TA=1.76, B=20, %151179640  
D=3.700, QC=0.2410, FS=2.8, U=16.9, TA=1.83, B=20, %151180765  
D=3.720, QC=0.2426, FS=3.1, U=17.0, TA=1.82, B=21, %151181546  
D=3.740, QC=0.2436, FS=3.2, U=19.3, TA=1.82, B=20, %151182640  
D=3.760, QC=0.2446, FS=3.0, U=17.3, TA=1.83, B=20, %151183750  
D=3.780, QC=0.2467, FS=3.1, U=17.4, TA=1.81, B=20, %151184531  
D=3.800, QC=0.2530, FS=3.1, U=17.5, TA=1.82, B=20, %151185640  
D=3.820, QC=0.2592, FS=3.2, U=17.6, TA=1.81, B=20, %151186406  
D=3.840, QC=0.2680, FS=3.1, U=17.8, TA=1.81, B=19, %151187500

D=3.860, QC=0.4010, FS=3.1, U=17.9, TA=1.80, B=20, %151188625  
D=3.880, QC=0.5641, FS=3.1, U=17.9, TA=1.77, B=20, %151189390  
D=3.900, QC=0.7085, FS=19.5, U=19.2, TA=1.74, B=19, %151190484  
D=3.920, QC=0.9022, FS=41.6, U=18.0, TA=1.83, B=18, %151191718  
D=3.940, QC=0.7646, FS=18.8, U=22.0, TA=1.76, B=18, %151231703  
D=3.960, QC=0.7646, FS=18.8, U=22.0, TA=1.76, B=18, %151231703  
D=3.980, QC=0.7350, FS=7.2, U=19.8, TA=1.77, B=16, %151232500  
D=4.000, QC=0.4966, FS=7.3, U=19.6, TA=1.81, B=17, %151233531  
D=4.020, QC=0.3812, FS=4.8, U=19.9, TA=1.80, B=18, %151234750  
D=4.040, QC=0.2872, FS=5.2, U=20.0, TA=1.81, B=18, %151235875  
D=4.060, QC=0.2820, FS=5.5, U=20.2, TA=1.80, B=18, %151237000  
D=4.080, QC=0.2784, FS=5.6, U=20.3, TA=1.81, B=18, %151238109  
D=4.100, QC=0.2800, FS=5.0, U=20.5, TA=1.79, B=19, %151239234  
D=4.120, QC=0.2784, FS=5.1, U=20.6, TA=1.81, B=19, %151239906  
D=4.140, QC=0.2774, FS=5.1, U=20.7, TA=1.81, B=17, %151241015  
D=4.160, QC=0.2774, FS=4.4, U=20.8, TA=1.81, B=17, %151242218  
D=4.180, QC=0.2732, FS=4.0, U=20.8, TA=1.78, B=17, %151243328  
D=4.200, QC=0.2743, FS=3.9, U=21.1, TA=1.83, B=18, %151244453  
D=4.220, QC=0.2815, FS=4.0, U=21.1, TA=1.83, B=17, %151245562  
D=4.240, QC=0.2836, FS=3.9, U=21.3, TA=1.82, B=17, %151246687  
D=4.260, QC=0.2888, FS=3.8, U=21.4, TA=1.82, B=17, %151247781  
D=4.280, QC=0.2929, FS=3.9, U=21.6, TA=1.83, B=19, %151248906  
D=4.300, QC=0.2872, FS=4.2, U=21.7, TA=1.82, B=17, %151250046  
D=4.320, QC=0.2909, FS=3.7, U=21.9, TA=1.79, B=17, %151251187  
D=4.340, QC=0.2852, FS=3.7, U=22.0, TA=1.79, B=18, %151252328  
D=4.360, QC=0.2862, FS=3.8, U=22.1, TA=1.77, B=19, %151253015  
D=4.380, QC=0.2836, FS=4.0, U=22.2, TA=1.81, B=19, %151254250  
D=4.400, QC=0.2831, FS=4.0, U=22.3, TA=1.78, B=18, %151255359  
D=4.420, QC=0.2867, FS=3.7, U=22.5, TA=1.80, B=18, %151256484  
D=4.440, QC=0.2981, FS=3.4, U=22.6, TA=1.78, B=20, %151257609  
D=4.460, QC=0.3018, FS=3.3, U=22.7, TA=1.81, B=19, %151258312  
D=4.480, QC=0.3059, FS=3.6, U=22.8, TA=1.80, B=19, %151259437  
D=4.500, QC=0.3153, FS=3.6, U=23.0, TA=1.78, B=18, %151260546  
D=4.520, QC=0.3189, FS=3.9, U=23.1, TA=1.83, B=19, %151261687  
D=4.540, QC=0.3194, FS=4.3, U=23.2, TA=1.80, B=19, %151262468  
D=4.560, QC=0.3163, FS=4.5, U=23.4, TA=1.83, B=19, %151263562  
D=4.580, QC=0.3132, FS=4.8, U=23.6, TA=1.84, B=19, %151264687  
D=4.600, QC=0.3132, FS=4.8, U=23.7, TA=1.83, B=19, %151265468  
D=4.620, QC=0.3142, FS=4.9, U=23.8, TA=1.83, B=20, %151266578  
D=4.640, QC=0.3158, FS=5.3, U=24.0, TA=1.82, B=19, %151267734  
D=4.660, QC=0.3205, FS=5.3, U=24.1, TA=1.83, B=19, %151268421  
D=4.680, QC=0.3205, FS=5.2, U=24.2, TA=1.80, B=20, %151269546  
D=4.700, QC=0.3200, FS=5.1, U=24.3, TA=1.80, B=20, %151270671  
D=4.720, QC=0.3200, FS=5.1, U=24.5, TA=1.81, B=19, %151271796  
D=4.740, QC=0.3210, FS=5.1, U=24.5, TA=1.79, B=19, %151272562  
D=4.760, QC=0.3220, FS=5.1, U=24.8, TA=1.80, B=18, %151273687  
D=4.780, QC=0.3283, FS=5.2, U=24.8, TA=1.80, B=18, %151274781  
D=4.800, QC=0.3324, FS=5.3, U=25.1, TA=1.79, B=19, %151275937  
D=4.820, QC=0.3314, FS=5.3, U=25.2, TA=1.79, B=19, %151276718  
D=4.840, QC=0.3309, FS=5.3, U=25.3, TA=1.79, B=20, %151277859

D=4.860, QC=0.3314, FS=5.7, U=25.5, TA=1.80, B=19, %151278906  
D=4.880, QC=0.3329, FS=5.7, U=25.6, TA=1.79, B=19, %151280046  
D=4.900, QC=0.3366, FS=5.8, U=25.7, TA=1.79, B=19, %151280812  
D=4.920, QC=0.3449, FS=6.1, U=25.9, TA=1.79, B=19, %151281953  
D=4.940, QC=0.3703, FS=6.2, U=26.0, TA=1.79, B=18, %151283062  
D=4.960, QC=0.3833, FS=6.6, U=26.2, TA=1.79, B=18, %151284171  
D=4.980, QC=0.3724, FS=6.7, U=26.2, TA=1.79, B=19, %151284953  
D=5.000, QC=0.3553, FS=6.8, U=26.3, TA=1.79, B=19, %151286062  
D=5.020, QC=0.3501, FS=7.5, U=26.5, TA=1.79, B=18, %151287171  
D=5.040, QC=0.3511, FS=7.7, U=24.3, TA=1.79, B=18, %151288296  
D=5.060, QC=0.3522, FS=8.0, U=26.8, TA=1.79, B=18, %151289406  
D=5.080, QC=0.3522, FS=8.1, U=24.6, TA=1.79, B=18, %151290546  
D=5.100, QC=0.3496, FS=8.3, U=24.9, TA=1.79, B=18, %151291703  
D=5.120, QC=0.3407, FS=8.1, U=24.9, TA=1.79, B=17, %151292812  
D=5.140, QC=0.3272, FS=9.3, U=26.1, TA=1.82, B=21, %151328500  
D=5.160, QC=0.3272, FS=9.3, U=26.1, TA=1.82, B=21, %151328500  
D=5.180, QC=0.3272, FS=9.3, U=26.1, TA=1.82, B=21, %151328500  
D=5.200, QC=0.3116, FS=8.9, U=25.8, TA=1.85, B=20, %151329609  
D=5.220, QC=0.3070, FS=8.8, U=25.8, TA=1.85, B=20, %151330312  
D=5.240, QC=0.3039, FS=8.0, U=25.9, TA=1.86, B=22, %151331500  
D=5.260, QC=0.3018, FS=7.6, U=26.0, TA=1.83, B=20, %151332171  
D=5.280, QC=0.3054, FS=7.0, U=26.0, TA=1.83, B=21, %151333296  
D=5.300, QC=0.3065, FS=6.2, U=26.1, TA=1.83, B=21, %151334437  
D=5.320, QC=0.3059, FS=6.1, U=26.2, TA=1.85, B=21, %151335234  
D=5.340, QC=0.2981, FS=5.9, U=26.2, TA=1.83, B=20, %151336343  
D=5.360, QC=0.2940, FS=5.8, U=26.3, TA=1.81, B=20, %151337125  
D=5.380, QC=0.2898, FS=5.8, U=26.5, TA=1.82, B=19, %151338250  
D=5.400, QC=0.2831, FS=5.9, U=26.6, TA=1.80, B=20, %151339343  
D=5.420, QC=0.2810, FS=5.9, U=26.6, TA=1.79, B=20, %151340125  
D=5.440, QC=0.2815, FS=5.8, U=26.8, TA=1.80, B=20, %151341250  
D=5.460, QC=0.2831, FS=5.6, U=26.8, TA=1.80, B=20, %151342390  
D=5.480, QC=0.2878, FS=5.3, U=26.9, TA=1.79, B=21, %151343046  
D=5.500, QC=0.2904, FS=5.2, U=27.0, TA=1.79, B=20, %151344156  
D=5.520, QC=0.2893, FS=5.0, U=27.0, TA=1.79, B=21, %151344921  
D=5.540, QC=0.2909, FS=4.9, U=27.1, TA=1.79, B=20, %151346125  
D=5.560, QC=0.2919, FS=5.1, U=27.2, TA=1.79, B=21, %151347265  
D=5.580, QC=0.2950, FS=5.2, U=27.3, TA=1.79, B=20, %151347953  
D=5.600, QC=0.3013, FS=5.5, U=27.4, TA=1.79, B=21, %151349062  
D=5.620, QC=0.3075, FS=5.7, U=27.5, TA=1.79, B=20, %151349859  
D=5.640, QC=0.3142, FS=5.7, U=27.6, TA=1.79, B=22, %151350968  
D=5.660, QC=0.3413, FS=6.0, U=27.7, TA=1.79, B=22, %151351765  
D=5.680, QC=0.3558, FS=6.1, U=27.9, TA=1.79, B=22, %151352421  
D=5.700, QC=0.3646, FS=6.1, U=27.9, TA=1.79, B=21, %151353546  
D=5.720, QC=0.3407, FS=5.5, U=27.8, TA=1.79, B=22, %151354312  
D=5.740, QC=0.3231, FS=6.2, U=27.9, TA=1.79, B=21, %151355421  
D=5.760, QC=0.3200, FS=5.6, U=28.0, TA=1.79, B=22, %151356218  
D=5.780, QC=0.3075, FS=5.2, U=28.0, TA=1.79, B=21, %151357359  
D=5.800, QC=0.2976, FS=4.9, U=28.2, TA=1.79, B=22, %151358109  
D=5.820, QC=0.2961, FS=4.9, U=28.2, TA=1.79, B=21, %151358796  
D=5.840, QC=0.3044, FS=4.7, U=28.5, TA=1.79, B=21, %151359921

D=5.860, QC=0.3127, FS=4.0, U=28.6, TA=1.79, B=21, %151360734  
D=5.880, QC=0.4555, FS=4.5, U=28.6, TA=1.79, B=22, %151361843  
D=5.900, QC=0.6607, FS=5.4, U=28.5, TA=1.79, B=21, %151362625  
D=5.920, QC=0.7329, FS=7.1, U=28.9, TA=1.79, B=20, %151363718  
D=5.940, QC=0.6742, FS=8.6, U=28.9, TA=1.79, B=21, %151364500  
D=5.960, QC=0.4560, FS=10.0, U=28.9, TA=1.79, B=21, %151365625  
D=5.980, QC=0.4135, FS=8.1, U=28.9, TA=1.79, B=21, %151366296  
D=6.000, QC=0.3755, FS=7.1, U=28.9, TA=1.79, B=22, %151367078  
D=6.020, QC=0.3594, FS=7.4, U=29.0, TA=1.79, B=21, %151368187  
D=6.040, QC=0.3511, FS=7.6, U=29.0, TA=1.79, B=22, %151368968  
D=6.060, QC=0.3355, FS=6.8, U=29.0, TA=1.79, B=21, %151370093  
D=6.080, QC=0.3200, FS=7.3, U=29.0, TA=1.79, B=22, %151370890  
D=6.100, QC=0.3200, FS=5.9, U=29.1, TA=1.79, B=21, %151371984  
D=6.120, QC=0.3439, FS=5.4, U=29.2, TA=1.79, B=22, %151372750  
D=6.140, QC=0.3485, FS=5.3, U=29.2, TA=1.79, B=21, %151373859  
D=6.160, QC=0.3407, FS=5.2, U=29.3, TA=1.79, B=21, %151374531  
D=6.180, QC=0.3293, FS=5.6, U=29.4, TA=1.79, B=21, %151375671  
D=6.200, QC=0.3278, FS=5.0, U=29.5, TA=1.79, B=21, %151376453  
D=6.220, QC=0.3241, FS=5.7, U=29.6, TA=1.79, B=20, %151377546  
D=6.240, QC=0.3355, FS=5.6, U=29.6, TA=1.79, B=21, %151378312  
D=6.260, QC=0.3444, FS=5.2, U=29.7, TA=1.79, B=20, %151379421  
D=6.280, QC=0.3506, FS=5.0, U=29.8, TA=1.79, B=21, %151380187  
D=6.300, QC=0.3252, FS=5.4, U=29.8, TA=1.79, B=20, %151381390  
D=6.320, QC=0.3205, FS=5.8, U=29.9, TA=1.79, B=20, %151382062  
D=6.340, QC=0.2904, FS=5.2, U=33.4, TA=1.79, B=19, %151418687  
D=6.360, QC=0.2904, FS=5.2, U=33.4, TA=1.79, B=19, %151418687  
D=6.380, QC=0.2904, FS=5.2, U=33.4, TA=1.79, B=19, %151418687  
D=6.400, QC=0.2893, FS=5.4, U=33.0, TA=1.79, B=19, %151419781  
D=6.420, QC=0.2909, FS=4.8, U=33.1, TA=1.79, B=18, %151420875  
D=6.440, QC=0.3101, FS=4.5, U=33.1, TA=1.79, B=20, %151422109  
D=6.460, QC=0.3376, FS=4.1, U=33.1, TA=1.79, B=18, %151422765  
D=6.480, QC=0.4119, FS=4.1, U=33.3, TA=1.79, B=18, %151423984  
D=6.500, QC=0.5205, FS=4.7, U=33.4, TA=1.79, B=19, %151425093  
D=6.520, QC=0.4914, FS=4.7, U=33.4, TA=1.79, B=19, %151426203  
D=6.540, QC=0.3620, FS=6.2, U=33.4, TA=1.79, B=18, %151427328  
D=6.560, QC=0.3329, FS=7.8, U=33.5, TA=1.79, B=18, %151428015  
D=6.580, QC=0.3423, FS=5.2, U=33.6, TA=1.79, B=18, %151429156  
D=6.600, QC=0.4145, FS=5.9, U=33.7, TA=1.79, B=19, %151430296  
D=6.620, QC=0.4238, FS=5.3, U=33.8, TA=1.79, B=18, %151431390  
D=6.640, QC=0.3745, FS=6.2, U=33.8, TA=1.79, B=18, %151432500  
D=6.660, QC=0.3579, FS=4.9, U=34.0, TA=1.79, B=19, %151433656  
D=6.680, QC=0.3407, FS=3.6, U=34.1, TA=1.79, B=20, %151434421  
D=6.700, QC=0.3324, FS=3.1, U=34.1, TA=1.79, B=19, %151435531  
D=6.720, QC=0.3376, FS=2.9, U=34.3, TA=1.79, B=18, %151436734  
D=6.740, QC=0.3485, FS=3.3, U=34.4, TA=1.79, B=18, %151437843  
D=6.760, QC=0.3490, FS=3.8, U=34.5, TA=1.80, B=20, %151438609  
D=6.780, QC=0.3501, FS=4.0, U=34.7, TA=1.79, B=20, %151439718  
D=6.800, QC=0.3501, FS=4.5, U=34.8, TA=1.80, B=19, %151440828  
D=6.820, QC=0.3594, FS=4.9, U=34.9, TA=1.81, B=19, %151441515  
D=6.840, QC=0.3709, FS=5.7, U=35.1, TA=1.81, B=21, %151442625



D=6.860, QC=0.3838, FS=5.9, U=35.2, TA=1.82, B=20, %151443421  
D=6.880, QC=0.3854, FS=6.3, U=35.2, TA=1.81, B=19, %151444546  
D=6.900, QC=0.3984, FS=8.0, U=35.4, TA=1.82, B=19, %151445687  
D=6.920, QC=0.3906, FS=7.6, U=35.5, TA=1.82, B=21, %151446453  
D=6.940, QC=0.3864, FS=7.3, U=35.5, TA=1.83, B=20, %151447562  
D=6.960, QC=0.3672, FS=6.6, U=35.6, TA=1.83, B=20, %151448328  
D=6.980, QC=0.3537, FS=7.0, U=35.7, TA=1.83, B=20, %151449437  
D=7.000, QC=0.3527, FS=6.8, U=35.8, TA=1.83, B=20, %151450140  
D=7.020, QC=0.3490, FS=6.6, U=35.9, TA=1.82, B=21, %151451343  
D=7.040, QC=0.3444, FS=6.6, U=36.0, TA=1.82, B=20, %151452453  
D=7.060, QC=0.3439, FS=7.3, U=36.1, TA=1.83, B=20, %151453125  
D=7.080, QC=0.3516, FS=6.7, U=36.2, TA=1.83, B=21, %151454375  
D=7.100, QC=0.3683, FS=4.9, U=36.2, TA=1.82, B=20, %151455078  
D=7.120, QC=0.3885, FS=5.0, U=36.4, TA=1.83, B=20, %151456203  
D=7.140, QC=0.4638, FS=5.6, U=36.4, TA=1.82, B=20, %151456984  
D=7.160, QC=0.5833, FS=6.2, U=36.5, TA=1.83, B=20, %151458015  
D=7.180, QC=0.5454, FS=6.8, U=36.7, TA=1.83, B=20, %151459140  
D=7.200, QC=0.4862, FS=7.9, U=36.7, TA=1.82, B=20, %151459906  
D=7.220, QC=0.3864, FS=9.6, U=36.8, TA=1.83, B=20, %151461046  
D=7.240, QC=0.3755, FS=9.0, U=36.8, TA=1.83, B=20, %151461812  
D=7.260, QC=0.3740, FS=7.6, U=37.0, TA=1.83, B=20, %151462921  
D=7.280, QC=0.3683, FS=6.8, U=37.1, TA=1.83, B=20, %151464031  
D=7.300, QC=0.3667, FS=6.4, U=37.2, TA=1.83, B=20, %151464812  
D=7.320, QC=0.3755, FS=6.0, U=37.3, TA=1.83, B=21, %151465937  
D=7.340, QC=0.3823, FS=5.2, U=37.3, TA=1.84, B=20, %151466703  
D=7.360, QC=0.3755, FS=4.9, U=37.5, TA=1.84, B=19, %151467828  
D=7.380, QC=0.3854, FS=5.7, U=37.6, TA=1.85, B=19, %151468921  
D=7.400, QC=0.4129, FS=5.9, U=37.7, TA=1.85, B=20, %151469703  
D=7.420, QC=0.4820, FS=6.0, U=37.8, TA=1.86, B=19, %151470812  
D=7.440, QC=0.4659, FS=6.4, U=37.9, TA=1.87, B=19, %151471921  
D=7.460, QC=0.4228, FS=7.9, U=38.1, TA=1.86, B=19, %151473046  
D=7.480, QC=0.4290, FS=6.5, U=38.1, TA=1.87, B=20, %151473859  
D=7.500, QC=0.4425, FS=6.5, U=38.2, TA=1.86, B=19, %151474968  
D=7.520, QC=0.4161, FS=6.6, U=38.3, TA=1.87, B=18, %151476109  
D=7.540, QC=0.4670, FS=10.3, U=42.4, TA=1.79, B=12, %151516781  
D=7.560, QC=0.4924, FS=10.8, U=42.0, TA=1.82, B=12, %151517562  
D=7.580, QC=0.5179, FS=10.8, U=42.1, TA=1.82, B=11, %151519468  
D=7.600, QC=0.4888, FS=10.6, U=42.2, TA=1.83, B=11, %151520921  
D=7.620, QC=0.4493, FS=11.8, U=42.3, TA=1.84, B=11, %151522796  
D=7.640, QC=0.4171, FS=12.0, U=42.4, TA=1.85, B=12, %151524265  
D=7.660, QC=0.4124, FS=9.9, U=42.5, TA=1.87, B=11, %151526156  
D=7.680, QC=0.4166, FS=7.8, U=42.7, TA=1.86, B=11, %151527718  
D=7.700, QC=0.3984, FS=7.5, U=42.8, TA=1.87, B=12, %151529593  
D=7.720, QC=0.3963, FS=7.2, U=43.1, TA=1.87, B=12, %151531031  
D=7.740, QC=0.4347, FS=7.5, U=43.2, TA=1.86, B=15, %151532609  
D=7.760, QC=0.4981, FS=7.5, U=43.3, TA=1.87, B=15, %151533640  
D=7.780, QC=0.5859, FS=7.3, U=43.4, TA=1.87, B=15, %151535250  
D=7.800, QC=0.5542, FS=8.8, U=43.4, TA=1.87, B=16, %151536343  
D=7.820, QC=0.4877, FS=9.1, U=43.5, TA=1.87, B=15, %151537812  
D=7.840, QC=0.4275, FS=9.6, U=43.6, TA=1.87, B=15, %151538921

D=7.860, QC=0.4150, FS=9.1, U=43.8, TA=1.87, B=15, %151540406  
D=7.880, QC=0.4394, FS=10.3, U=44.0, TA=1.87, B=16, %151541546  
D=7.900, QC=0.4581, FS=10.8, U=44.1, TA=1.87, B=15, %151542656  
D=7.920, QC=0.4337, FS=11.0, U=44.1, TA=1.87, B=15, %151544140  
D=7.940, QC=0.4322, FS=10.7, U=44.3, TA=1.87, B=15, %151545265  
D=7.960, QC=0.4389, FS=10.4, U=44.2, TA=1.87, B=16, %151546390  
D=7.980, QC=0.4311, FS=8.2, U=44.5, TA=1.87, B=16, %151547593  
D=8.000, QC=0.4254, FS=8.9, U=44.6, TA=1.87, B=16, %151549062  
D=8.020, QC=0.4285, FS=8.9, U=44.7, TA=1.87, B=16, %151550234  
D=8.040, QC=0.4347, FS=7.9, U=44.9, TA=1.87, B=17, %151551328  
D=8.060, QC=0.4218, FS=7.9, U=45.0, TA=1.87, B=17, %151552421  
D=8.080, QC=0.4238, FS=7.2, U=45.1, TA=1.87, B=16, %151553546  
D=8.100, QC=0.4285, FS=7.3, U=45.4, TA=1.87, B=16, %151555093  
D=8.120, QC=0.4472, FS=7.6, U=45.4, TA=1.87, B=17, %151556187  
D=8.140, QC=0.4519, FS=8.2, U=45.6, TA=1.87, B=16, %151557312  
D=8.160, QC=0.4638, FS=8.4, U=45.7, TA=1.87, B=16, %151558421  
D=8.180, QC=0.4524, FS=9.6, U=45.9, TA=1.87, B=17, %151559531  
D=8.200, QC=0.4405, FS=8.9, U=46.0, TA=1.87, B=17, %151560656  
D=8.220, QC=0.4373, FS=7.1, U=46.1, TA=1.87, B=17, %151561796  
D=8.240, QC=0.4223, FS=7.5, U=46.1, TA=1.87, B=16, %151562890  
D=8.260, QC=0.4124, FS=7.8, U=46.3, TA=1.87, B=16, %151564109  
D=8.280, QC=0.4306, FS=7.6, U=46.4, TA=1.87, B=17, %151565250  
D=8.300, QC=0.4488, FS=7.6, U=46.6, TA=1.87, B=17, %151566359  
D=8.320, QC=0.4586, FS=7.9, U=46.7, TA=1.87, B=16, %151567453  
D=8.340, QC=0.4519, FS=8.0, U=44.6, TA=1.87, B=17, %151568890  
D=8.360, QC=0.4529, FS=8.0, U=47.0, TA=1.87, B=17, %151570015  
D=8.380, QC=0.4929, FS=7.9, U=47.1, TA=1.87, B=16, %151571234  
D=8.400, QC=0.6971, FS=12.2, U=47.9, TA=1.87, B=16, %151572375  
D=8.420, QC=0.7812, FS=17.4, U=48.7, TA=1.87, B=16, %151573390  
D=8.440, QC=0.7428, FS=11.7, U=48.8, TA=1.87, B=16, %151574625  
D=8.460, QC=0.6747, FS=10.5, U=47.8, TA=1.87, B=16, %151576015  
D=8.480, QC=0.5095, FS=13.9, U=47.6, TA=1.87, B=16, %151577140  
D=8.500, QC=0.4789, FS=15.9, U=47.5, TA=1.87, B=16, %151578265  
D=8.520, QC=0.4581, FS=15.9, U=47.5, TA=1.87, B=17, %151579406  
D=8.540, QC=0.4441, FS=16.3, U=47.7, TA=1.87, B=16, %151580984  
D=8.560, QC=0.4425, FS=15.3, U=47.7, TA=1.87, B=16, %151582015  
D=8.580, QC=0.4399, FS=15.1, U=47.8, TA=1.87, B=16, %151583234  
D=8.600, QC=0.4384, FS=10.7, U=48.0, TA=1.87, B=16, %151584250  
D=8.620, QC=0.4373, FS=8.0, U=48.0, TA=1.87, B=15, %151585781  
D=8.640, QC=0.4431, FS=7.1, U=48.1, TA=1.87, B=15, %151586906  
D=8.660, QC=0.4431, FS=5.9, U=48.2, TA=1.87, B=16, %151588046  
D=8.680, QC=0.4394, FS=5.3, U=48.4, TA=1.87, B=16, %151589593  
D=8.700, QC=0.4347, FS=5.2, U=48.5, TA=1.87, B=15, %151590703  
D=8.720, QC=0.4373, FS=5.9, U=48.6, TA=1.87, B=15, %151591812  
D=8.740, QC=0.4083, FS=8.4, U=50.9, TA=1.86, B=22, %151636812  
D=8.760, QC=0.4083, FS=8.4, U=50.9, TA=1.86, B=22, %151636812  
D=8.780, QC=0.4098, FS=8.4, U=50.9, TA=1.87, B=23, %151637156  
D=8.800, QC=0.4093, FS=8.3, U=50.6, TA=1.87, B=22, %151637937  
D=8.820, QC=0.4186, FS=9.1, U=50.6, TA=1.87, B=23, %151638703  
D=8.840, QC=0.4322, FS=8.8, U=50.6, TA=1.87, B=24, %151639406

D=8.860, QC=0.4389, FS=9.0, U=53.0, TA=1.87, B=22, %151640484  
D=8.880, QC=0.4436, FS=9.5, U=53.2, TA=1.87, B=23, %151641281  
D=8.900, QC=0.4332, FS=8.5, U=51.0, TA=1.87, B=25, %151642062  
D=8.920, QC=0.4285, FS=7.9, U=51.1, TA=1.87, B=26, %151642718  
D=8.940, QC=0.4244, FS=7.6, U=51.1, TA=1.87, B=24, %151643578  
D=8.960, QC=0.4306, FS=8.0, U=51.2, TA=1.87, B=24, %151644218  
D=8.980, QC=0.4399, FS=8.3, U=51.3, TA=1.87, B=25, %151645000  
D=9.000, QC=0.4540, FS=8.1, U=51.3, TA=1.87, B=26, %151646140  
D=9.020, QC=0.4534, FS=8.0, U=51.4, TA=1.87, B=25, %151646921  
D=9.040, QC=0.4415, FS=8.8, U=51.5, TA=1.87, B=18, %151647687  
D=9.060, QC=0.4327, FS=9.2, U=54.0, TA=1.87, B=18, %151648796  
D=9.080, QC=0.4789, FS=8.9, U=54.0, TA=1.87, B=20, %151649890  
D=9.100, QC=0.5527, FS=9.8, U=51.9, TA=1.87, B=18, %151651031  
D=9.120, QC=0.6243, FS=10.4, U=54.4, TA=1.87, B=18, %151652125  
D=9.140, QC=0.5714, FS=9.9, U=54.4, TA=1.87, B=18, %151652890  
D=9.160, QC=0.5179, FS=11.4, U=54.4, TA=1.87, B=20, %151654031  
D=9.180, QC=0.4696, FS=11.5, U=54.4, TA=1.87, B=19, %151655171  
D=9.200, QC=0.4675, FS=10.6, U=52.3, TA=1.87, B=19, %151656312  
D=9.220, QC=0.4602, FS=10.2, U=54.6, TA=1.87, B=19, %151656984  
D=9.240, QC=0.4519, FS=9.5, U=54.6, TA=1.87, B=21, %151658125  
D=9.260, QC=0.4483, FS=9.2, U=52.4, TA=1.87, B=20, %151659218  
D=9.280, QC=0.4467, FS=7.4, U=52.5, TA=1.87, B=19, %151660015  
D=9.300, QC=0.4332, FS=6.8, U=54.8, TA=1.87, B=20, %151661140  
D=9.320, QC=0.4301, FS=6.2, U=54.9, TA=1.87, B=20, %151661921  
D=9.340, QC=0.4238, FS=5.6, U=52.8, TA=1.87, B=19, %151663031  
D=9.360, QC=0.4150, FS=5.9, U=55.2, TA=1.87, B=20, %151664140  
D=9.380, QC=0.4114, FS=6.1, U=53.0, TA=1.87, B=20, %151664937  
D=9.400, QC=0.4109, FS=6.4, U=53.1, TA=1.87, B=20, %151666078  
D=9.420, QC=0.4202, FS=6.5, U=55.4, TA=1.87, B=21, %151666750  
D=9.440, QC=0.4322, FS=6.6, U=55.5, TA=1.87, B=20, %151667859  
D=9.460, QC=0.4477, FS=6.9, U=55.6, TA=1.87, B=20, %151668968  
D=9.480, QC=0.4462, FS=6.9, U=53.5, TA=1.87, B=21, %151669765  
D=9.500, QC=0.4462, FS=7.3, U=53.6, TA=1.87, B=20, %151670875  
D=9.520, QC=0.4716, FS=7.5, U=53.7, TA=1.87, B=20, %151671640  
D=9.540, QC=0.4784, FS=7.7, U=56.0, TA=1.87, B=20, %151672781  
D=9.560, QC=0.4737, FS=8.7, U=56.1, TA=1.87, B=20, %151673546  
D=9.580, QC=0.4550, FS=8.8, U=54.0, TA=1.87, B=20, %151674656  
D=9.600, QC=0.4488, FS=7.9, U=56.3, TA=1.87, B=20, %151675781  
D=9.620, QC=0.4368, FS=7.8, U=54.2, TA=1.87, B=20, %151676468  
D=9.640, QC=0.4275, FS=7.4, U=56.4, TA=1.87, B=20, %151677609  
D=9.660, QC=0.4254, FS=7.9, U=56.5, TA=1.87, B=20, %151678390  
D=9.680, QC=0.4228, FS=8.6, U=54.5, TA=1.87, B=20, %151679500  
D=9.700, QC=0.4270, FS=8.1, U=54.6, TA=1.87, B=20, %151680593  
D=9.720, QC=0.4353, FS=7.7, U=54.7, TA=1.87, B=21, %151681406  
D=9.740, QC=0.4296, FS=7.6, U=54.9, TA=1.87, B=20, %151682515  
D=9.760, QC=0.4202, FS=7.6, U=54.9, TA=1.87, B=19, %151683625  
D=9.780, QC=0.4223, FS=7.4, U=57.3, TA=1.87, B=19, %151684421  
D=9.800, QC=0.4254, FS=7.4, U=55.3, TA=1.87, B=20, %151685578  
D=9.820, QC=0.4212, FS=7.5, U=57.5, TA=1.87, B=19, %151686671  
D=9.840, QC=0.4280, FS=7.5, U=55.4, TA=1.87, B=19, %151687453

D=9.860, QC=0.4223, FS=7.7, U=57.8, TA=1.87, B=19, %151688562  
D=9.880, QC=0.4259, FS=7.9, U=57.8, TA=1.87, B=21, %151689671  
D=9.900, QC=0.4296, FS=8.0, U=55.7, TA=1.87, B=21, %151690437  
D=9.920, QC=0.4472, FS=8.1, U=55.8, TA=1.87, B=19, %151691546  
D=9.940, QC=0.4472, FS=6.5, U=56.0, TA=1.87, B=18, %151692640  
D=9.960, QC=0.4851, FS=11.0, U=60.7, TA=1.87, B=17, %151730484  
D=9.980, QC=0.4851, FS=11.0, U=60.7, TA=1.87, B=17, %151730484  
D=10.000, QC=0.4638, FS=10.7, U=58.1, TA=1.87, B=21, %151731625  
D=10.020, QC=0.4618, FS=10.7, U=58.0, TA=1.87, B=21, %151732406  
D=10.040, QC=0.4654, FS=10.1, U=60.5, TA=1.87, B=22, %151733546  
D=10.060, QC=0.4680, FS=9.8, U=60.5, TA=1.87, B=21, %151734312  
D=10.080, QC=0.4612, FS=9.9, U=58.4, TA=1.87, B=21, %151735421  
D=10.100, QC=0.4597, FS=9.8, U=60.8, TA=1.87, B=22, %151736218  
D=10.120, QC=0.4592, FS=9.2, U=60.8, TA=1.87, B=23, %151736906  
D=10.140, QC=0.4659, FS=9.3, U=60.9, TA=1.87, B=20, %151738031  
D=10.160, QC=0.4716, FS=9.5, U=61.0, TA=1.87, B=22, %151738812  
D=10.180, QC=0.4753, FS=9.7, U=61.1, TA=1.87, B=21, %151739953  
D=10.200, QC=0.4758, FS=10.0, U=61.3, TA=1.87, B=21, %151740625  
D=10.220, QC=0.4711, FS=9.8, U=61.4, TA=1.87, B=21, %151741859  
D=10.240, QC=0.4680, FS=9.5, U=61.6, TA=1.87, B=22, %151742531  
D=10.260, QC=0.4696, FS=9.4, U=61.6, TA=1.87, B=21, %151743640  
D=10.280, QC=0.4701, FS=9.8, U=61.8, TA=1.87, B=23, %151744406  
D=10.300, QC=0.4742, FS=10.0, U=61.9, TA=1.87, B=21, %151745203  
D=10.320, QC=0.4810, FS=10.3, U=62.0, TA=1.87, B=21, %151746328  
D=10.340, QC=0.4908, FS=10.5, U=62.1, TA=1.87, B=21, %151747000  
D=10.360, QC=0.4934, FS=10.5, U=62.1, TA=1.87, B=22, %151748109  
D=10.380, QC=0.4862, FS=10.5, U=62.3, TA=1.87, B=22, %151748875  
D=10.400, QC=0.4836, FS=10.5, U=62.4, TA=1.87, B=23, %151749640  
D=10.420, QC=0.4753, FS=10.2, U=62.6, TA=1.87, B=21, %151750765  
D=10.440, QC=0.4747, FS=10.2, U=62.7, TA=1.87, B=23, %151751546  
D=10.460, QC=0.4789, FS=9.9, U=62.8, TA=1.87, B=23, %151752328  
D=10.480, QC=0.4825, FS=9.7, U=62.9, TA=1.87, B=22, %151753453  
D=10.500, QC=0.4893, FS=9.6, U=63.0, TA=1.87, B=22, %151754140  
D=10.520, QC=0.4986, FS=9.9, U=63.1, TA=1.87, B=23, %151754921  
D=10.540, QC=0.5002, FS=9.5, U=63.4, TA=1.87, B=22, %151756062  
D=10.560, QC=0.4992, FS=9.8, U=63.4, TA=1.87, B=23, %151756828  
D=10.580, QC=0.4955, FS=10.0, U=63.5, TA=1.87, B=23, %151757515  
D=10.600, QC=0.4919, FS=10.3, U=63.6, TA=1.87, B=23, %151758281  
D=10.620, QC=0.4753, FS=10.6, U=63.6, TA=1.87, B=23, %151759406  
D=10.640, QC=0.4753, FS=11.0, U=63.8, TA=1.87, B=22, %151760187  
D=10.660, QC=0.4742, FS=11.2, U=63.9, TA=1.87, B=22, %151760937  
D=10.680, QC=0.4737, FS=11.5, U=63.9, TA=1.87, B=23, %151761703  
D=10.700, QC=0.4758, FS=10.6, U=64.2, TA=1.87, B=23, %151762812  
D=10.720, QC=0.4768, FS=10.2, U=64.3, TA=1.87, B=23, %151763484  
D=10.740, QC=0.4784, FS=9.9, U=64.5, TA=1.87, B=22, %151764281  
D=10.760, QC=0.4805, FS=9.7, U=64.6, TA=1.87, B=23, %151765390  
D=10.780, QC=0.4872, FS=9.8, U=64.6, TA=1.87, B=22, %151766156  
D=10.800, QC=0.4929, FS=10.2, U=64.7, TA=1.87, B=24, %151766937  
D=10.820, QC=0.4986, FS=11.3, U=64.9, TA=1.87, B=22, %151768031  
D=10.840, QC=0.5018, FS=11.9, U=65.0, TA=1.87, B=22, %151768796

D=10.860, QC=0.5028, FS=12.5, U=65.1, TA=1.87, B=22, %151769484  
D=10.880, QC=0.5028, FS=12.8, U=65.3, TA=1.87, B=22, %151770703  
D=10.900, QC=0.5044, FS=13.0, U=65.4, TA=1.87, B=22, %151771406  
D=10.920, QC=0.5085, FS=13.0, U=65.5, TA=1.87, B=23, %151772218  
D=10.940, QC=0.5101, FS=12.7, U=65.7, TA=1.87, B=22, %151773296  
D=10.960, QC=0.5111, FS=12.8, U=65.8, TA=1.87, B=22, %151774078  
D=10.980, QC=0.5095, FS=12.9, U=65.9, TA=1.87, B=22, %151774765  
D=11.000, QC=0.5033, FS=12.8, U=66.0, TA=1.87, B=22, %151775875  
D=11.020, QC=0.4986, FS=12.7, U=66.1, TA=1.87, B=22, %151776656  
D=11.040, QC=0.4971, FS=12.4, U=66.3, TA=1.87, B=21, %151777765  
D=11.060, QC=0.4981, FS=12.5, U=64.1, TA=1.87, B=21, %151778546  
D=11.080, QC=0.5023, FS=12.4, U=66.5, TA=1.87, B=21, %151779312  
D=11.100, QC=0.5085, FS=12.2, U=66.6, TA=1.87, B=22, %151780421  
D=11.120, QC=0.5095, FS=11.7, U=66.8, TA=1.87, B=21, %151781109  
D=11.140, QC=0.5179, FS=12.3, U=73.2, TA=1.87, B=19, %151826171  
D=11.160, QC=0.5179, FS=12.3, U=73.2, TA=1.87, B=19, %151826171  
D=11.180, QC=0.5116, FS=11.7, U=72.8, TA=1.87, B=18, %151827281  
D=11.200, QC=0.5080, FS=11.2, U=73.0, TA=1.87, B=19, %151828406  
D=11.220, QC=0.5106, FS=11.2, U=73.1, TA=1.87, B=18, %151829171  
D=11.240, QC=0.5121, FS=11.5, U=73.2, TA=1.87, B=19, %151830265  
D=11.260, QC=0.5132, FS=11.8, U=71.2, TA=1.87, B=20, %151831375  
D=11.280, QC=0.5236, FS=12.1, U=73.6, TA=1.87, B=18, %151832484  
D=11.300, QC=0.5267, FS=12.4, U=73.8, TA=1.87, B=19, %151833593  
D=11.320, QC=0.5205, FS=12.8, U=73.9, TA=1.87, B=18, %151834375  
D=11.340, QC=0.5095, FS=12.9, U=74.0, TA=1.87, B=19, %151835468  
D=11.360, QC=0.5116, FS=13.3, U=74.2, TA=1.87, B=17, %151836671  
D=11.380, QC=0.5090, FS=13.4, U=74.4, TA=1.87, B=17, %151837765  
D=11.400, QC=0.5054, FS=13.3, U=74.6, TA=1.87, B=18, %151838875  
D=11.420, QC=0.5012, FS=13.3, U=74.7, TA=1.87, B=19, %151840000  
D=11.440, QC=0.4955, FS=13.2, U=74.9, TA=1.87, B=18, %151841093  
D=11.460, QC=0.4966, FS=13.1, U=75.0, TA=1.87, B=18, %151842218  
D=11.480, QC=0.4997, FS=12.4, U=75.3, TA=1.87, B=19, %151843328  
D=11.500, QC=0.5018, FS=12.0, U=75.3, TA=1.87, B=19, %151844093  
D=11.520, QC=0.5095, FS=11.8, U=75.5, TA=1.87, B=18, %151845218  
D=11.540, QC=0.5142, FS=11.2, U=75.7, TA=1.87, B=18, %151846343  
D=11.560, QC=0.5277, FS=11.0, U=75.9, TA=1.87, B=18, %151847453  
D=11.580, QC=0.5381, FS=10.4, U=76.1, TA=1.87, B=19, %151848609  
D=11.600, QC=0.5449, FS=10.4, U=76.3, TA=1.87, B=20, %151849812  
D=11.620, QC=0.5443, FS=10.8, U=76.4, TA=1.87, B=18, %151850468  
D=11.640, QC=0.5428, FS=11.4, U=76.6, TA=1.87, B=18, %151851671  
D=11.660, QC=0.5272, FS=11.9, U=76.7, TA=1.87, B=20, %151852781  
D=11.680, QC=0.5298, FS=12.4, U=77.0, TA=1.87, B=19, %151853546  
D=11.700, QC=0.5308, FS=12.8, U=77.2, TA=1.89, B=19, %151854671  
D=11.720, QC=0.5231, FS=13.0, U=77.3, TA=1.88, B=19, %151855781  
D=11.740, QC=0.5199, FS=12.9, U=77.5, TA=1.89, B=19, %151856875  
D=11.760, QC=0.5147, FS=12.9, U=77.6, TA=1.90, B=19, %151857640  
D=11.780, QC=0.5132, FS=12.5, U=77.7, TA=1.91, B=19, %151858765  
D=11.800, QC=0.5163, FS=12.1, U=78.0, TA=1.91, B=19, %151859875  
D=11.820, QC=0.5158, FS=11.9, U=78.1, TA=1.90, B=20, %151860656  
D=11.840, QC=0.5168, FS=11.8, U=78.2, TA=1.92, B=19, %151861750

D=11.860, QC=0.5163, FS=11.8, U=78.4, TA=1.92, B=19, %151862843  
D=11.880, QC=0.5142, FS=11.4, U=78.6, TA=1.92, B=18, %151863625  
D=11.900, QC=0.5220, FS=11.0, U=78.7, TA=1.91, B=20, %151864718  
D=11.920, QC=0.5220, FS=10.7, U=78.9, TA=1.92, B=19, %151865828  
D=11.940, QC=0.5241, FS=10.5, U=79.1, TA=1.92, B=19, %151866625  
D=11.960, QC=0.5231, FS=10.3, U=79.3, TA=1.92, B=19, %151867765  
D=11.980, QC=0.5225, FS=10.2, U=79.5, TA=1.92, B=19, %151868906  
D=12.000, QC=0.5256, FS=10.3, U=77.4, TA=1.92, B=20, %151870000  
D=12.020, QC=0.5267, FS=10.5, U=79.8, TA=1.92, B=19, %151870765  
D=12.040, QC=0.5267, FS=11.2, U=80.0, TA=1.92, B=19, %151871859  
D=12.060, QC=0.5246, FS=11.6, U=80.2, TA=1.92, B=19, %151872968  
D=12.080, QC=0.5262, FS=11.9, U=80.3, TA=1.92, B=19, %151873734  
D=12.100, QC=0.5205, FS=12.4, U=80.6, TA=1.92, B=19, %151874859  
D=12.120, QC=0.5267, FS=12.6, U=80.8, TA=1.92, B=18, %151875968  
D=12.140, QC=0.5262, FS=12.8, U=80.9, TA=1.92, B=19, %151877187  
D=12.160, QC=0.5293, FS=12.9, U=81.1, TA=1.92, B=18, %151877875  
D=12.180, QC=0.5256, FS=13.0, U=81.2, TA=1.92, B=18, %151878984  
D=12.200, QC=0.5205, FS=13.0, U=81.5, TA=1.92, B=18, %151880093  
D=12.220, QC=0.5179, FS=12.7, U=81.6, TA=1.92, B=18, %151881218  
D=12.240, QC=0.5173, FS=12.6, U=81.9, TA=1.92, B=19, %151882421  
D=12.260, QC=0.5168, FS=12.5, U=82.0, TA=1.92, B=18, %151883078  
D=12.280, QC=0.5205, FS=12.5, U=79.8, TA=1.92, B=18, %151884250  
D=12.300, QC=0.5231, FS=12.2, U=82.3, TA=1.92, B=18, %151885359  
D=12.320, QC=0.5272, FS=12.2, U=82.4, TA=1.92, B=18, %151886453, NA=-0.0115, NB=1.6, NC=2.8,  
F=15, K=90, T=The test are ended without any stop in the ground.

#\$

0:

1:

2:

3:

4:

5:

6:

7:

8:

9:

11:Tilt derivative alarm

12:Point resistance alarm

13:Depth unchanged for 5 second

14:Transmission lost

15:End of test

16:Dissipation start

**CPT -8**  
**Raw Data**

\$  
HA=1,HB=2,HC=CPTLOG-2.00,HD=8/19/2020,HG=-0.853,HP=-0.85,HJ=Brenton  
CPT,HK=c8,HM=07,HN=3206,HO=0.00,HQ=SA,HR=0°0'0.000"E,HS=0°0'0.000"N,HX=0.00,HY=0.00  
,HZ=0.00,KQ=1468.00,KF=6200.00,KU=2136.00,MA=0.590,MB=0.011,MC=10.0,MD=150.0,ME=c8,  
MF=0.000  
RN=,CA=0,CB=0

#  
D=0.000,QC=0.0306,FS=2.3,U=2.9,TA=1.08,B=0,%153220359,NA=5.6694,NB=317.5,NC=439.6

D=0.020,QC=0.0306,FS=2.3,U=2.9,TA=1.08,B=0,%153220359

D=0.040,QC=0.0421,FS=2.5,U=2.5,TA=1.23,B=14,%153221890

D=0.060,QC=0.0457,FS=2.3,U=2.5,TA=1.41,B=13,%153223328

D=0.080,QC=0.0636,FS=2.4,U=0.1,TA=1.46,B=15,%153224875

D=0.100,QC=0.0673,FS=2.3,U=2.5,TA=1.26,B=14,%153226000

D=0.120,QC=0.0773,FS=2.2,U=2.4,TA=1.35,B=14,%153227437

D=0.140,QC=0.0999,FS=2.2,U=2.4,TA=1.50,B=13,%153228968

D=0.160,QC=0.0904,FS=2.4,U=2.5,TA=1.57,B=14,%153230062

D=0.180,QC=0.0999,FS=2.6,U=2.4,TA=1.48,B=16,%153231593

D=0.200,QC=0.0904,FS=2.7,U=2.5,TA=1.45,B=16,%153232734

D=0.220,QC=0.0935,FS=2.5,U=2.5,TA=1.48,B=18,%153233843

D=0.240,QC=0.0971,FS=2.6,U=2.5,TA=1.48,B=18,%153234953

D=0.260,QC=0.0982,FS=2.5,U=2.6,TA=1.57,B=17,%153236046

D=0.280,QC=0.0928,FS=2.6,U=2.6,TA=1.50,B=15,%153237250

D=0.300,QC=0.1054,FS=2.6,U=2.7,TA=1.53,B=15,%153238359

D=0.320,QC=0.1001,FS=2.5,U=2.7,TA=1.41,B=17,%153239500

D=0.340,QC=0.1043,FS=2.7,U=2.7,TA=1.46,B=22,%153240609

D=0.360,QC=0.1069,FS=2.9,U=2.7,TA=1.45,B=22,%153241312

D=0.380,QC=0.1015,FS=3.1,U=2.7,TA=1.54,B=18,%153242515

D=0.400,QC=0.1088,FS=3.1,U=2.8,TA=1.55,B=19,%153243171

D=0.420,QC=0.1099,FS=3.1,U=2.9,TA=1.54,B=19,%153244390

D=0.440,QC=0.1010,FS=3.5,U=2.9,TA=1.46,B=19,%153245484

D=0.460,QC=0.1067,FS=3.4,U=3.0,TA=1.39,B=20,%153246250

D=0.480,QC=0.1078,FS=3.7,U=3.0,TA=1.43,B=21,%153247343

D=0.500,QC=0.1041,FS=4.0,U=3.1,TA=1.46,B=20,%153248109

D=0.520,QC=0.1079,FS=3.9,U=3.2,TA=1.54,B=20,%153249203

D=0.540,QC=0.1069,FS=4.0,U=3.2,TA=1.58,B=20,%153250343

D=0.560,QC=0.1053,FS=3.8,U=3.3,TA=1.60,B=20,%153251109

D=0.580,QC=0.1048,FS=3.4,U=3.4,TA=1.56,B=21,%153252234

D=0.600,QC=0.1064,FS=3.5,U=3.4,TA=1.51,B=21,%153253015

D=0.620,QC=0.1069,FS=3.4,U=3.5,TA=1.59,B=19,%153254140

D=0.640,QC=0.1090,FS=3.4,U=3.6,TA=1.63,B=20,%153255250

D=0.660,QC=0.1095,FS=3.2,U=3.6,TA=1.61,B=20,%153255906

D=0.680,QC=0.1095,FS=3.3,U=3.7,TA=1.64,B=19,%153257109 ,F=11

D=0.700,QC=0.1074,FS=3.2,U=3.8,TA=1.77,B=19,%153258265

D=0.720,QC=0.1074,FS=3.1,U=3.9,TA=1.77,B=20,%153258937

D=0.740,QC=0.1079,FS=3.1,U=4.0,TA=1.71,B=20,%153260046

D=0.760,QC=0.1069,FS=3.1,U=4.1,TA=1.65,B=20,%153260828

D=0.780,QC=0.1090,FS=3.0,U=4.2,TA=1.63,B=22,%153261953

D=0.800,QC=0.1069,FS=3.0,U=4.2,TA=1.77,B=23,%153262656

D=0.820,QC=0.1005,FS=2.9,U=4.4,TA=1.68,B=23,%153263421

D=0.840,QC=0.1000,FS=2.9,U=4.5,TA=1.68,B=23,%153264625



D=0.860, QC=0.1000, FS=2.7, U=4.6, TA=1.71, B=22, %153265281  
D=0.880, QC=0.1010, FS=2.6, U=4.7, TA=1.69, B=22, %153266046  
D=0.900, QC=0.1087, FS=2.7, U=5.8, TA=1.71, B=20, %153303359  
D=0.920, QC=0.1043, FS=2.7, U=5.8, TA=1.66, B=11, %153303687  
D=0.940, QC=0.1058, FS=2.9, U=5.5, TA=1.64, B=20, %153304812  
D=0.960, QC=0.1084, FS=2.8, U=5.5, TA=1.64, B=20, %153305937  
D=0.980, QC=0.1010, FS=2.7, U=5.5, TA=1.63, B=20, %153306718  
D=1.000, QC=0.1000, FS=2.6, U=5.6, TA=1.63, B=18, %153307828  
D=1.020, QC=0.1005, FS=2.5, U=5.7, TA=1.66, B=18, %153308953  
D=1.040, QC=0.1005, FS=2.4, U=5.8, TA=1.64, B=18, %153310046  
D=1.060, QC=0.1015, FS=2.2, U=5.9, TA=1.67, B=18, %153311171  
D=1.080, QC=0.1010, FS=2.8, U=6.0, TA=1.67, B=18, %153312265  
D=1.100, QC=0.1011, FS=2.5, U=6.1, TA=1.64, B=17, %153313500  
D=1.120, QC=0.1000, FS=2.1, U=6.2, TA=1.64, B=17, %153314593  
D=1.140, QC=0.1014, FS=2.9, U=6.3, TA=1.64, B=18, %153315703  
D=1.160, QC=0.1019, FS=2.5, U=6.5, TA=1.64, B=18, %153316859  
D=1.180, QC=0.1014, FS=2.4, U=6.5, TA=1.65, B=17, %153317968  
D=1.200, QC=0.1019, FS=2.3, U=6.6, TA=1.64, B=19, %153318734  
D=1.220, QC=0.1010, FS=2.1, U=6.7, TA=1.66, B=18, %153319843  
D=1.240, QC=0.1010, FS=2.0, U=6.8, TA=1.63, B=18, %153320937  
D=1.260, QC=0.1015, FS=2.3, U=6.9, TA=1.63, B=17, %153322031  
D=1.280, QC=0.1016, FS=2.5, U=7.0, TA=1.63, B=18, %153323171  
D=1.300, QC=0.1011, FS=2.8, U=7.2, TA=1.63, B=18, %153324281  
D=1.320, QC=0.1015, FS=2.9, U=7.3, TA=1.63, B=19, %153325406  
D=1.340, QC=0.1026, FS=2.9, U=7.4, TA=1.64, B=18, %153326187  
D=1.360, QC=0.1026, FS=2.9, U=7.6, TA=1.66, B=19, %153327281  
D=1.380, QC=0.1098, FS=2.9, U=7.6, TA=1.63, B=19, %153328484  
D=1.400, QC=0.1130, FS=2.8, U=7.9, TA=1.63, B=20, %153329609  
D=1.420, QC=0.1128, FS=2.9, U=8.0, TA=1.66, B=19, %153330281  
D=1.440, QC=0.1215, FS=2.9, U=8.1, TA=1.66, B=19, %153331390  
D=1.460, QC=0.1517, FS=2.6, U=8.2, TA=1.64, B=19, %153332500  
D=1.480, QC=0.2166, FS=2.2, U=8.4, TA=1.66, B=20, %153333296  
D=1.500, QC=0.2904, FS=2.2, U=8.6, TA=1.69, B=19, %153334421  
D=1.520, QC=0.2955, FS=2.9, U=8.6, TA=1.68, B=19, %153335515  
D=1.540, QC=0.3646, FS=3.4, U=8.6, TA=1.72, B=18, %153336281  
D=1.560, QC=0.6337, FS=5.4, U=8.6, TA=1.76, B=20, %153337375  
D=1.580, QC=0.6560, FS=5.7, U=8.9, TA=1.75, B=19, %153338578  
D=1.600, QC=0.4701, FS=4.9, U=9.0, TA=1.74, B=18, %153339718  
D=1.620, QC=0.3511, FS=3.8, U=9.1, TA=1.74, B=19, %153340500  
D=1.640, QC=0.2654, FS=1.9, U=9.3, TA=1.75, B=20, %153341625  
D=1.660, QC=0.1948, FS=1.1, U=9.4, TA=1.76, B=20, %153342703  
D=1.680, QC=0.2161, FS=1.2, U=9.6, TA=1.77, B=18, %153343812  
D=1.700, QC=0.2644, FS=1.1, U=9.7, TA=1.77, B=19, %153344578  
D=1.720, QC=0.3028, FS=1.5, U=9.8, TA=1.76, B=20, %153345718  
D=1.740, QC=0.2826, FS=1.8, U=10.1, TA=1.77, B=20, %153346828  
D=1.760, QC=0.2743, FS=1.7, U=7.9, TA=1.75, B=20, %153347515  
D=1.780, QC=0.3636, FS=1.8, U=8.0, TA=1.77, B=19, %153348734  
D=1.800, QC=0.4441, FS=1.8, U=8.2, TA=1.82, B=19, %153349843  
D=1.820, QC=0.4181, FS=1.4, U=8.3, TA=1.82, B=19, %153350968  
D=1.840, QC=0.4405, FS=1.9, U=8.4, TA=1.78, B=19, %153351734

D=1.860, QC=0.5080, FS=1.9, U=8.5, TA=1.83, B=18, %153352765  
D=1.880, QC=0.4597, FS=1.3, U=8.6, TA=1.83, B=19, %153353984  
D=1.900, QC=0.3470, FS=1.1, U=8.8, TA=1.82, B=19, %153355093  
D=1.920, QC=0.2446, FS=1.3, U=8.9, TA=1.85, B=18, %153356187  
D=1.940, QC=0.1979, FS=1.2, U=9.0, TA=1.84, B=19, %153356968  
D=1.960, QC=0.1979, FS=1.9, U=6.9, TA=1.85, B=23, %153357640  
D=1.980, QC=0.2556, FS=2.3, U=7.0, TA=1.85, B=24, %153358843  
D=2.000, QC=0.5225, FS=4.1, U=7.1, TA=1.85, B=22, %153359609  
D=2.020, QC=0.6524, FS=2.7, U=7.2, TA=1.85, B=23, %153360265  
D=2.040, QC=0.5033, FS=1.8, U=7.3, TA=1.85, B=23, %153361031  
D=2.060, QC=0.2753, FS=2.4, U=9.6, TA=1.81, B=19, %153397250  
D=2.080, QC=0.2753, FS=2.4, U=9.6, TA=1.81, B=19, %153397250  
D=2.100, QC=0.3059, FS=2.4, U=9.6, TA=1.81, B=19, %153397593  
D=2.120, QC=0.5116, FS=4.7, U=9.2, TA=1.81, B=19, %153398718  
D=2.140, QC=0.5916, FS=3.5, U=9.2, TA=1.81, B=20, %153399828  
D=2.160, QC=0.5194, FS=3.1, U=9.2, TA=1.81, B=19, %153400593  
D=2.180, QC=0.4457, FS=2.8, U=9.3, TA=1.81, B=19, %153401703  
D=2.200, QC=0.3080, FS=2.6, U=9.4, TA=1.81, B=19, %153402828  
D=2.220, QC=0.2602, FS=1.8, U=7.2, TA=1.82, B=20, %153403609  
D=2.240, QC=0.2389, FS=2.1, U=7.3, TA=1.83, B=19, %153404718  
D=2.260, QC=0.2587, FS=2.3, U=7.4, TA=1.83, B=19, %153405828  
D=2.280, QC=0.2784, FS=3.2, U=7.6, TA=1.83, B=19, %153406968  
D=2.300, QC=0.2685, FS=3.5, U=7.6, TA=1.84, B=18, %153407750  
D=2.320, QC=0.2223, FS=3.5, U=7.6, TA=1.84, B=18, %153408859  
D=2.340, QC=0.2389, FS=3.2, U=7.8, TA=1.84, B=19, %153410000  
D=2.360, QC=0.3345, FS=3.1, U=7.9, TA=1.85, B=19, %153411093  
D=2.380, QC=0.3838, FS=2.6, U=7.9, TA=1.82, B=18, %153411890  
D=2.400, QC=0.3854, FS=3.4, U=8.0, TA=1.85, B=19, %153413000  
D=2.420, QC=0.3361, FS=3.8, U=8.1, TA=1.84, B=19, %153414140  
D=2.440, QC=0.2940, FS=4.0, U=8.2, TA=1.86, B=18, %153415250  
D=2.460, QC=0.2722, FS=1.9, U=8.2, TA=1.84, B=19, %153415906  
D=2.480, QC=0.2680, FS=1.7, U=8.4, TA=1.82, B=18, %153417109  
D=2.500, QC=0.2722, FS=2.6, U=8.5, TA=1.83, B=20, %153418234  
D=2.520, QC=0.3413, FS=3.3, U=8.5, TA=1.83, B=19, %153419359  
D=2.540, QC=0.4041, FS=3.8, U=8.6, TA=1.80, B=19, %153420140  
D=2.560, QC=0.4555, FS=4.9, U=8.7, TA=1.83, B=20, %153421250  
D=2.580, QC=0.4597, FS=4.6, U=8.8, TA=1.84, B=20, %153421921  
D=2.600, QC=0.3506, FS=3.6, U=8.9, TA=1.79, B=20, %153423046  
D=2.620, QC=0.2914, FS=1.5, U=9.0, TA=1.80, B=20, %153424265  
D=2.640, QC=0.2415, FS=2.0, U=9.1, TA=1.81, B=20, %153424921  
D=2.660, QC=0.2254, FS=1.6, U=9.1, TA=1.81, B=21, %153426125  
D=2.680, QC=0.2322, FS=1.8, U=9.2, TA=1.80, B=21, %153426812  
D=2.700, QC=0.2514, FS=3.0, U=9.4, TA=1.80, B=21, %153428000  
D=2.720, QC=0.2587, FS=2.6, U=9.5, TA=1.81, B=20, %153428703  
D=2.740, QC=0.2285, FS=2.4, U=9.6, TA=1.80, B=22, %153429875  
D=2.760, QC=0.2156, FS=2.9, U=9.6, TA=1.76, B=22, %153430578  
D=2.780, QC=0.2150, FS=1.6, U=9.7, TA=1.75, B=21, %153431687  
D=2.800, QC=0.2197, FS=1.7, U=9.8, TA=1.76, B=20, %153432890  
D=2.820, QC=0.2259, FS=1.3, U=10.0, TA=1.76, B=20, %153433578  
D=2.840, QC=0.2478, FS=1.6, U=10.1, TA=1.75, B=21, %153434703

D=2.860, QC=0.2462, FS=1.6, U=10.1, TA=1.76, B=21, %153435468  
D=2.880, QC=0.2675, FS=2.0, U=10.3, TA=1.75, B=20, %153436562  
D=2.900, QC=0.2680, FS=1.9, U=10.3, TA=1.77, B=20, %153437328  
D=2.920, QC=0.2587, FS=2.2, U=10.5, TA=1.75, B=21, %153438468  
D=2.940, QC=0.2478, FS=2.9, U=10.7, TA=1.74, B=21, %153439250  
D=2.960, QC=0.3298, FS=2.5, U=10.7, TA=1.75, B=20, %153440375  
D=2.980, QC=0.3241, FS=1.9, U=10.8, TA=1.75, B=20, %153441500  
D=3.000, QC=0.3023, FS=2.5, U=10.9, TA=1.75, B=20, %153442265  
D=3.020, QC=0.2909, FS=3.5, U=10.9, TA=1.75, B=20, %153443375  
D=3.040, QC=0.3631, FS=4.1, U=11.1, TA=1.74, B=20, %153444140  
D=3.060, QC=0.4109, FS=3.8, U=11.1, TA=1.75, B=20, %153445281  
D=3.080, QC=0.3449, FS=2.8, U=11.2, TA=1.74, B=20, %153446375  
D=3.100, QC=0.2987, FS=2.9, U=11.3, TA=1.72, B=20, %153447140  
D=3.120, QC=0.2680, FS=4.8, U=11.4, TA=1.72, B=19, %153448250  
D=3.140, QC=0.2524, FS=4.6, U=11.4, TA=1.71, B=19, %153449359  
D=3.160, QC=0.2478, FS=4.3, U=11.6, TA=1.70, B=20, %153450156  
D=3.180, QC=0.2420, FS=3.9, U=11.7, TA=1.70, B=21, %153451265  
D=3.200, QC=0.2337, FS=3.7, U=9.5, TA=1.69, B=21, %153451937  
D=3.220, QC=0.2987, FS=3.5, U=11.9, TA=1.70, B=22, %153453062  
D=3.240, QC=0.3018, FS=3.0, U=12.0, TA=1.69, B=24, %153453828  
D=3.260, QC=0.3496, FS=5.2, U=12.1, TA=1.70, B=24, %153494843  
D=3.280, QC=0.3496, FS=5.2, U=12.1, TA=1.70, B=24, %153494843  
D=3.300, QC=0.2743, FS=5.2, U=12.1, TA=1.71, B=26, %153495187  
D=3.320, QC=0.2592, FS=5.4, U=11.7, TA=1.70, B=25, %153495859  
D=3.340, QC=0.2846, FS=4.2, U=11.8, TA=1.70, B=25, %153497078  
D=3.360, QC=0.2883, FS=3.6, U=11.8, TA=1.70, B=24, %153497765  
D=3.380, QC=0.2784, FS=3.8, U=11.7, TA=1.70, B=25, %153498546  
D=3.400, QC=0.2581, FS=4.0, U=11.8, TA=1.70, B=24, %153499312  
D=3.420, QC=0.3033, FS=3.8, U=11.9, TA=1.69, B=27, %153499984  
D=3.440, QC=0.3646, FS=3.4, U=12.0, TA=1.67, B=27, %153500750  
D=3.460, QC=0.3890, FS=4.4, U=12.0, TA=1.68, B=30, %153501515  
D=3.480, QC=0.3812, FS=3.8, U=12.0, TA=1.69, B=28, %153502312  
D=3.500, QC=0.3729, FS=3.8, U=12.0, TA=1.68, B=29, %153502656  
D=3.520, QC=0.3350, FS=5.2, U=12.1, TA=1.68, B=28, %153503421  
D=3.540, QC=0.2940, FS=5.7, U=12.0, TA=1.67, B=29, %153504218  
D=3.560, QC=0.2826, FS=4.5, U=12.2, TA=1.67, B=22, %153504921  
D=3.580, QC=0.2774, FS=4.4, U=12.2, TA=1.66, B=17, %153506015  
D=3.600, QC=0.2607, FS=4.1, U=12.3, TA=1.66, B=21, %153507218  
D=3.620, QC=0.2613, FS=3.8, U=12.4, TA=1.66, B=19, %153507875  
D=3.640, QC=0.2602, FS=3.8, U=12.5, TA=1.66, B=18, %153509078  
D=3.660, QC=0.2514, FS=3.0, U=12.5, TA=1.66, B=20, %153510187  
D=3.680, QC=0.2446, FS=2.7, U=12.7, TA=1.66, B=19, %153511312  
D=3.700, QC=0.2436, FS=2.2, U=12.8, TA=1.66, B=21, %153512093  
D=3.720, QC=0.2670, FS=2.2, U=12.8, TA=1.66, B=19, %153513187  
D=3.740, QC=0.2758, FS=2.3, U=13.0, TA=1.66, B=20, %153514296  
D=3.760, QC=0.2794, FS=2.5, U=13.0, TA=1.66, B=20, %153515062  
D=3.780, QC=0.2571, FS=2.5, U=10.8, TA=1.66, B=21, %153516156  
D=3.800, QC=0.2410, FS=3.4, U=13.1, TA=1.66, B=20, %153516921  
D=3.820, QC=0.2322, FS=1.9, U=11.0, TA=1.66, B=21, %153518015  
D=3.840, QC=0.2322, FS=1.6, U=11.0, TA=1.66, B=20, %153518796

D=3.860, QC=0.2280, FS=1.5, U=11.1, TA=1.66, B=21, %153519906  
D=3.880, QC=0.2254, FS=1.5, U=11.2, TA=1.66, B=21, %153520687  
D=3.900, QC=0.2244, FS=2.1, U=11.3, TA=1.66, B=22, %153521796  
D=3.920, QC=0.2265, FS=1.4, U=11.4, TA=1.66, B=21, %153522578  
D=3.940, QC=0.2415, FS=1.3, U=11.5, TA=1.66, B=23, %153523671  
D=3.960, QC=0.2472, FS=1.4, U=11.6, TA=1.66, B=22, %153524453  
D=3.980, QC=0.2457, FS=1.6, U=11.6, TA=1.66, B=22, %153525218  
D=4.000, QC=0.2431, FS=2.3, U=11.7, TA=1.66, B=21, %153526312  
D=4.020, QC=0.2353, FS=2.2, U=11.8, TA=1.66, B=22, %153527093  
D=4.040, QC=0.2358, FS=1.9, U=11.9, TA=1.66, B=22, %153528203  
D=4.060, QC=0.2322, FS=1.8, U=12.0, TA=1.66, B=22, %153528859  
D=4.080, QC=0.2265, FS=2.0, U=12.1, TA=1.66, B=21, %153530000  
D=4.100, QC=0.2348, FS=2.0, U=12.2, TA=1.66, B=22, %153530781  
D=4.120, QC=0.2348, FS=2.0, U=10.0, TA=1.66, B=22, %153531546  
D=4.140, QC=0.2306, FS=2.0, U=10.1, TA=1.66, B=22, %153532656  
D=4.160, QC=0.2400, FS=2.3, U=12.4, TA=1.66, B=21, %153533437  
D=4.180, QC=0.2337, FS=3.1, U=10.3, TA=1.66, B=21, %153534562  
D=4.200, QC=0.2343, FS=3.2, U=12.6, TA=1.66, B=21, %153535328  
D=4.220, QC=0.2400, FS=3.3, U=10.4, TA=1.66, B=21, %153536437  
D=4.240, QC=0.2441, FS=3.3, U=10.5, TA=1.66, B=21, %153537203  
D=4.260, QC=0.2488, FS=3.2, U=10.7, TA=1.66, B=21, %153538312  
D=4.280, QC=0.2514, FS=3.2, U=10.7, TA=1.66, B=21, %153539078  
D=4.300, QC=0.2561, FS=3.2, U=10.8, TA=1.66, B=22, %153539750  
D=4.320, QC=0.2743, FS=3.4, U=10.9, TA=1.66, B=20, %153540875  
D=4.340, QC=0.3028, FS=3.4, U=11.0, TA=1.66, B=21, %153541640  
D=4.360, QC=0.3397, FS=4.1, U=11.2, TA=1.66, B=20, %153542734  
D=4.380, QC=0.3345, FS=4.4, U=11.3, TA=1.66, B=21, %153543875  
D=4.400, QC=0.3220, FS=4.5, U=11.4, TA=1.66, B=20, %153544640  
D=4.420, QC=0.3101, FS=6.2, U=11.5, TA=1.66, B=21, %153545750  
D=4.440, QC=0.2940, FS=7.2, U=11.6, TA=1.66, B=20, %153546531  
D=4.460, QC=0.2768, FS=8.8, U=15.8, TA=1.66, B=26, %153586578  
D=4.480, QC=0.2768, FS=8.8, U=15.8, TA=1.66, B=26, %153586578  
D=4.500, QC=0.2768, FS=8.8, U=15.8, TA=1.66, B=26, %153586578  
D=4.520, QC=0.2753, FS=8.2, U=15.3, TA=1.66, B=20, %153587796  
D=4.540, QC=0.2768, FS=7.6, U=15.4, TA=1.66, B=21, %153588453  
D=4.560, QC=0.2800, FS=5.9, U=15.4, TA=1.66, B=20, %153589671  
D=4.580, QC=0.2857, FS=5.2, U=15.4, TA=1.66, B=20, %153590781  
D=4.600, QC=0.2820, FS=4.8, U=15.5, TA=1.66, B=21, %153591453  
D=4.620, QC=0.2810, FS=4.7, U=15.6, TA=1.66, B=20, %153592562  
D=4.640, QC=0.2789, FS=4.9, U=15.6, TA=1.66, B=20, %153593359  
D=4.660, QC=0.2800, FS=5.0, U=15.7, TA=1.66, B=21, %153594546  
D=4.680, QC=0.2810, FS=5.1, U=15.7, TA=1.66, B=20, %153595234  
D=4.700, QC=0.2763, FS=5.3, U=15.8, TA=1.66, B=19, %153596328  
D=4.720, QC=0.2706, FS=5.5, U=15.8, TA=1.66, B=20, %153597453  
D=4.740, QC=0.2685, FS=5.7, U=15.9, TA=1.66, B=20, %153598234  
D=4.760, QC=0.2711, FS=5.5, U=16.1, TA=1.66, B=20, %153599343  
D=4.780, QC=0.2758, FS=5.2, U=16.1, TA=1.66, B=21, %153600125  
D=4.800, QC=0.2836, FS=5.1, U=16.1, TA=1.66, B=20, %153601234  
D=4.820, QC=0.2857, FS=5.2, U=16.2, TA=1.66, B=21, %153602000  
D=4.840, QC=0.2831, FS=5.2, U=16.4, TA=1.66, B=20, %153603093

D=4.860, QC=0.2831, FS=5.1, U=16.4, TA=1.65, B=20, %153604203  
D=4.880, QC=0.2893, FS=5.2, U=14.2, TA=1.66, B=21, %153605000  
D=4.900, QC=0.3039, FS=5.8, U=16.6, TA=1.66, B=22, %153606109  
D=4.920, QC=0.3065, FS=5.9, U=16.6, TA=1.66, B=22, %153606890  
D=4.940, QC=0.3252, FS=5.8, U=14.5, TA=1.66, B=22, %153607656  
D=4.960, QC=0.3542, FS=5.9, U=16.7, TA=1.66, B=22, %153608765  
D=4.980, QC=0.3548, FS=6.2, U=16.9, TA=1.66, B=22, %153609453  
D=5.000, QC=0.3532, FS=6.8, U=17.0, TA=1.66, B=21, %153610671  
D=5.020, QC=0.3490, FS=7.4, U=17.0, TA=1.65, B=21, %153611328  
D=5.040, QC=0.3407, FS=8.1, U=14.9, TA=1.67, B=21, %153612109  
D=5.060, QC=0.3319, FS=8.5, U=15.0, TA=1.68, B=23, %153613250  
D=5.080, QC=0.3345, FS=8.5, U=15.0, TA=1.67, B=22, %153614031  
D=5.100, QC=0.3376, FS=8.4, U=15.1, TA=1.66, B=23, %153614687  
D=5.120, QC=0.3381, FS=8.1, U=15.2, TA=1.66, B=22, %153615890  
D=5.140, QC=0.3376, FS=8.0, U=15.2, TA=1.66, B=23, %153616562  
D=5.160, QC=0.3215, FS=7.7, U=15.3, TA=1.66, B=22, %153617781  
D=5.180, QC=0.3101, FS=7.3, U=15.5, TA=1.68, B=21, %153618453  
D=5.200, QC=0.3007, FS=7.2, U=15.5, TA=1.67, B=21, %153619218  
D=5.220, QC=0.2872, FS=6.6, U=15.7, TA=1.66, B=25, %153620421  
D=5.240, QC=0.2846, FS=6.5, U=15.7, TA=1.65, B=25, %153621078  
D=5.260, QC=0.2779, FS=6.3, U=15.8, TA=1.66, B=24, %153621843  
D=5.280, QC=0.2763, FS=6.0, U=15.7, TA=1.67, B=24, %153622609  
D=5.300, QC=0.2737, FS=5.9, U=15.8, TA=1.64, B=27, %153623406  
D=5.320, QC=0.2748, FS=5.8, U=16.0, TA=1.65, B=25, %153624078  
D=5.340, QC=0.2779, FS=5.7, U=15.9, TA=1.66, B=25, %153624843  
D=5.360, QC=0.2779, FS=5.8, U=16.0, TA=1.66, B=25, %153625625  
D=5.380, QC=0.2805, FS=5.7, U=16.1, TA=1.65, B=26, %153626390  
D=5.400, QC=0.2820, FS=5.8, U=16.1, TA=1.64, B=26, %153627156  
D=5.420, QC=0.2867, FS=5.7, U=16.1, TA=1.65, B=25, %153627812  
D=5.440, QC=0.2878, FS=5.5, U=16.3, TA=1.65, B=25, %153628656  
D=5.460, QC=0.2914, FS=5.7, U=16.3, TA=1.65, B=26, %153629312  
D=5.480, QC=0.2919, FS=5.7, U=16.3, TA=1.65, B=25, %153630125  
D=5.500, QC=0.2919, FS=5.9, U=16.4, TA=1.65, B=26, %153630812  
D=5.520, QC=0.2914, FS=5.9, U=16.5, TA=1.64, B=25, %153632000  
D=5.540, QC=0.2950, FS=5.9, U=16.5, TA=1.65, B=26, %153632765  
D=5.560, QC=0.2955, FS=5.9, U=16.5, TA=1.65, B=26, %153633453  
D=5.580, QC=0.2935, FS=6.0, U=16.6, TA=1.64, B=26, %153634218  
D=5.600, QC=0.2935, FS=5.7, U=16.6, TA=1.64, B=27, %153635000  
D=5.620, QC=0.2935, FS=5.9, U=16.7, TA=1.64, B=28, %153635343  
D=5.640, QC=0.2940, FS=4.2, U=16.7, TA=1.65, B=29, %153636109  
D=5.660, QC=0.2758, FS=6.6, U=17.3, TA=1.57, B=17, %153673218  
D=5.680, QC=0.2805, FS=6.6, U=17.3, TA=1.62, B=17, %153673562  
D=5.700, QC=0.2805, FS=6.4, U=16.9, TA=1.63, B=16, %153674656  
D=5.720, QC=0.2826, FS=6.3, U=16.9, TA=1.62, B=18, %153675781  
D=5.740, QC=0.2862, FS=6.0, U=17.0, TA=1.63, B=17, %153676890  
D=5.760, QC=0.2878, FS=5.9, U=17.0, TA=1.62, B=17, %153678109  
D=5.780, QC=0.2862, FS=5.5, U=17.1, TA=1.63, B=16, %153679203  
D=5.800, QC=0.2872, FS=5.2, U=17.2, TA=1.63, B=17, %153680671  
D=5.820, QC=0.2878, FS=5.3, U=17.2, TA=1.63, B=17, %153681781  
D=5.840, QC=0.2862, FS=5.5, U=17.3, TA=1.63, B=16, %153682875

D=5.860, QC=0.2872, FS=5.4, U=17.3, TA=1.63, B=16, %153684078  
D=5.880, QC=0.2909, FS=5.6, U=17.3, TA=1.64, B=17, %153685203  
D=5.900, QC=0.2914, FS=5.8, U=17.4, TA=1.64, B=16, %153686312  
D=5.920, QC=0.2945, FS=5.8, U=17.6, TA=1.63, B=16, %153687765  
D=5.940, QC=0.2955, FS=5.9, U=17.6, TA=1.64, B=16, %153688968  
D=5.960, QC=0.2976, FS=5.8, U=17.7, TA=1.63, B=16, %153690093  
D=5.980, QC=0.2971, FS=6.0, U=17.8, TA=1.63, B=16, %153691203  
D=6.000, QC=0.2966, FS=6.0, U=17.8, TA=1.63, B=16, %153692312  
D=6.020, QC=0.2981, FS=6.0, U=17.9, TA=1.63, B=16, %153693421  
D=6.040, QC=0.2961, FS=6.0, U=18.0, TA=1.63, B=16, %153694859  
D=6.060, QC=0.3007, FS=6.0, U=18.1, TA=1.63, B=17, %153696078  
D=6.080, QC=0.2981, FS=6.3, U=18.1, TA=1.62, B=16, %153697203  
D=6.100, QC=0.2966, FS=6.2, U=18.2, TA=1.62, B=18, %153698343  
D=6.120, QC=0.2935, FS=6.2, U=18.3, TA=1.63, B=18, %153699437  
D=6.140, QC=0.2924, FS=6.2, U=18.3, TA=1.63, B=18, %153700562  
D=6.160, QC=0.2929, FS=6.3, U=18.5, TA=1.63, B=18, %153701687  
D=6.180, QC=0.2966, FS=6.2, U=18.5, TA=1.63, B=18, %153702781  
D=6.200, QC=0.2981, FS=6.1, U=18.6, TA=1.63, B=17, %153703875  
D=6.220, QC=0.2945, FS=6.1, U=18.6, TA=1.61, B=16, %153705015  
D=6.240, QC=0.2940, FS=6.1, U=18.7, TA=1.63, B=15, %153706140  
D=6.260, QC=0.2961, FS=6.1, U=18.8, TA=1.62, B=16, %153707687  
D=6.280, QC=0.2971, FS=6.1, U=19.0, TA=1.63, B=15, %153708796  
D=6.300, QC=0.3007, FS=5.9, U=19.0, TA=1.62, B=15, %153709906  
D=6.320, QC=0.3091, FS=5.9, U=19.1, TA=1.61, B=16, %153711062  
D=6.340, QC=0.3148, FS=5.9, U=19.2, TA=1.62, B=18, %153712140  
D=6.360, QC=0.3241, FS=5.8, U=19.3, TA=1.61, B=19, %153713343  
D=6.380, QC=0.3252, FS=5.8, U=19.3, TA=1.61, B=19, %153714375  
D=6.400, QC=0.3278, FS=5.9, U=19.3, TA=1.61, B=19, %153715500  
D=6.420, QC=0.3262, FS=6.0, U=19.5, TA=1.61, B=19, %153716296  
D=6.440, QC=0.3215, FS=6.5, U=19.6, TA=1.59, B=20, %153717421  
D=6.460, QC=0.3189, FS=6.7, U=19.6, TA=1.61, B=20, %153718187  
D=6.480, QC=0.3116, FS=6.9, U=19.6, TA=1.62, B=20, %153719281  
D=6.500, QC=0.3080, FS=6.9, U=19.8, TA=1.61, B=21, %153720375  
D=6.520, QC=0.3070, FS=6.9, U=19.8, TA=1.61, B=21, %153721140  
D=6.540, QC=0.3080, FS=6.7, U=19.8, TA=1.59, B=20, %153722343  
D=6.560, QC=0.3091, FS=6.7, U=19.8, TA=1.62, B=20, %153723000  
D=6.580, QC=0.3111, FS=6.4, U=20.0, TA=1.61, B=21, %153724218  
D=6.600, QC=0.3210, FS=6.3, U=20.1, TA=1.60, B=22, %153724875  
D=6.620, QC=0.3537, FS=6.1, U=20.1, TA=1.58, B=21, %153726015  
D=6.640, QC=0.3906, FS=6.3, U=20.1, TA=1.59, B=21, %153726781  
D=6.660, QC=0.4446, FS=7.8, U=20.2, TA=1.61, B=22, %153727890  
D=6.680, QC=0.4862, FS=8.8, U=20.1, TA=1.61, B=22, %153728656  
D=6.700, QC=0.5480, FS=10.8, U=20.1, TA=1.61, B=23, %153729750  
D=6.720, QC=0.5895, FS=12.9, U=20.1, TA=1.62, B=22, %153730515  
D=6.740, QC=0.6456, FS=14.3, U=20.0, TA=1.63, B=22, %153731312  
D=6.760, QC=0.7111, FS=18.9, U=20.1, TA=1.63, B=23, %153732421  
D=6.780, QC=0.7137, FS=24.6, U=21.1, TA=1.63, B=24, %153733203  
D=6.800, QC=0.6602, FS=29.4, U=22.1, TA=1.62, B=24, %153733859  
D=6.820, QC=0.6321, FS=19.9, U=21.3, TA=1.62, B=24, %153734625  
D=6.840, QC=0.5527, FS=16.6, U=20.7, TA=1.61, B=22, %153735843

D=6.860, QC=0.7220, FS=24.0, U=24.3, TA=1.56, B=20, %153772109  
D=6.880, QC=0.7220, FS=24.0, U=24.3, TA=1.56, B=20, %153772109  
D=6.900, QC=0.8077, FS=24.0, U=24.3, TA=1.61, B=20, %153772546  
D=6.920, QC=0.8711, FS=47.1, U=24.7, TA=1.63, B=20, %153773656  
D=6.940, QC=1.0918, FS=61.5, U=25.2, TA=1.64, B=19, %153774750  
D=6.960, QC=1.2544, FS=87.4, U=28.6, TA=1.64, B=19, %153775906  
D=6.980, QC=1.3510, FS=92.4, U=27.8, TA=1.64, B=18, %153776671  
D=7.000, QC=1.2923, FS=89.9, U=27.7, TA=1.63, B=19, %153777796  
D=7.020, QC=1.2798, FS=93.8, U=28.0, TA=1.63, B=19, %153778890  
D=7.040, QC=1.6730, FS=99.4, U=28.0, TA=1.64, B=18, %153779984  
D=7.060, QC=1.8174, FS=100.5, U=27.6, TA=1.64, B=17, %153781187  
D=7.080, QC=1.5660, FS=92.7, U=24.3, TA=1.63, B=18, %153781843  
D=7.100, QC=0.7583, FS=82.3, U=24.2, TA=1.64, B=18, %153783046  
D=7.120, QC=0.7298, FS=28.2, U=21.4, TA=1.64, B=18, %153784156  
D=7.140, QC=0.6680, FS=14.2, U=20.0, TA=1.64, B=17, %153785281  
D=7.160, QC=0.7838, FS=39.1, U=20.0, TA=1.64, B=17, %153786375  
D=7.180, QC=1.1074, FS=66.5, U=21.7, TA=1.64, B=16, %153787531  
D=7.200, QC=1.5307, FS=80.8, U=24.2, TA=1.65, B=16, %153789078  
D=7.220, QC=1.5988, FS=79.7, U=25.0, TA=1.65, B=17, %153790187  
D=7.240, QC=1.3874, FS=80.4, U=25.0, TA=1.64, B=17, %153791312  
D=7.260, QC=1.1676, FS=75.2, U=22.6, TA=1.64, B=18, %153792437  
D=7.280, QC=0.8420, FS=70.2, U=24.8, TA=1.65, B=18, %153793546  
D=7.300, QC=0.8279, FS=64.4, U=24.5, TA=1.64, B=18, %153794312  
D=7.320, QC=0.8461, FS=73.0, U=24.7, TA=1.64, B=19, %153795406  
D=7.340, QC=1.4092, FS=80.3, U=25.2, TA=1.64, B=18, %153796531  
D=7.360, QC=1.8465, FS=91.6, U=26.3, TA=1.64, B=18, %153797656  
D=7.380, QC=2.9061, FS=97.1, U=24.4, TA=1.64, B=18, %153798750  
D=7.400, QC=3.2027, FS=95.0, U=27.1, TA=1.64, B=17, %153799906  
D=7.420, QC=3.2962, FS=94.0, U=27.2, TA=1.64, B=16, %153801015  
D=7.440, QC=3.1399, FS=90.4, U=27.6, TA=1.64, B=16, %153802125  
D=7.460, QC=2.8282, FS=87.2, U=27.2, TA=1.59, B=17, %153803328  
D=7.480, QC=2.8298, FS=85.8, U=27.0, TA=1.59, B=17, %153804468  
D=7.500, QC=2.9087, FS=86.2, U=27.2, TA=1.57, B=17, %153805484  
D=7.520, QC=2.8921, FS=88.6, U=27.4, TA=1.56, B=17, %153806625  
D=7.540, QC=2.8386, FS=89.3, U=25.3, TA=1.56, B=17, %153807750  
D=7.560, QC=2.7015, FS=89.9, U=28.0, TA=1.55, B=18, %153808859  
D=7.580, QC=2.3529, FS=89.7, U=25.5, TA=1.55, B=17, %153810062  
D=7.600, QC=2.1327, FS=87.9, U=27.1, TA=1.55, B=17, %153811171  
D=7.620, QC=1.3167, FS=84.6, U=26.8, TA=1.55, B=17, %153812296  
D=7.640, QC=0.8840, FS=73.3, U=24.5, TA=1.55, B=19, %153813390  
D=7.660, QC=0.7589, FS=62.0, U=23.6, TA=1.55, B=19, %153814609  
D=7.680, QC=0.7781, FS=59.6, U=22.5, TA=1.55, B=18, %153815609  
D=7.700, QC=0.7963, FS=68.8, U=22.3, TA=1.55, B=18, %153816812  
D=7.720, QC=0.8056, FS=76.4, U=23.1, TA=1.55, B=19, %153817500  
D=7.740, QC=0.8664, FS=95.0, U=24.6, TA=1.53, B=18, %153818718  
D=7.760, QC=1.2061, FS=99.9, U=25.3, TA=1.48, B=18, %153819812  
D=7.780, QC=1.9249, FS=103.8, U=26.2, TA=1.48, B=16, %153821234  
D=7.800, QC=2.3010, FS=107.8, U=26.8, TA=1.48, B=15, %153822453  
D=7.820, QC=2.7020, FS=107.6, U=26.9, TA=1.47, B=15, %153823546  
D=7.840, QC=2.8454, FS=107.2, U=26.7, TA=1.48, B=14, %153824984

D=7.860, QC=2.8770, FS=108.7, U=26.5, TA=1.49, B=12, %153826546  
D=7.880, QC=2.8708, FS=101.3, U=26.0, TA=1.53, B=12, %153828421  
D=7.900, QC=2.8853, FS=95.8, U=25.7, TA=1.55, B=12, %153829953  
D=7.920, QC=2.8422, FS=91.8, U=25.7, TA=1.56, B=11, %153831765  
D=7.940, QC=2.7435, FS=86.3, U=25.6, TA=1.56, B=10, %153833640  
D=7.960, QC=2.5394, FS=82.6, U=25.5, TA=1.56, B=10, %153835546  
D=7.980, QC=2.3779, FS=79.6, U=25.5, TA=1.56, B=10, %153837734  
D=8.000, QC=2.2870, FS=77.9, U=25.4, TA=1.56, B=10, %153839656  
D=8.020, QC=2.2179, FS=77.3, U=25.3, TA=1.56, B=10, %153841531 , F=13  
D=8.040, QC=2.2023, FS=79.3, U=24.4, TA=1.56, B=13, %153894218  
D=8.060, QC=2.4636, FS=78.5, U=26.2, TA=1.56, B=14, %153894984  
D=8.080, QC=2.5711, FS=78.2, U=26.2, TA=1.56, B=12, %153896875  
D=8.100, QC=2.6817, FS=78.6, U=24.1, TA=1.56, B=12, %153898312  
D=8.120, QC=2.8448, FS=79.5, U=26.5, TA=1.56, B=7, %153900984  
D=8.140, QC=2.8983, FS=79.6, U=26.6, TA=1.56, B=7, %153903562  
D=8.160, QC=2.9586, FS=80.0, U=26.6, TA=1.56, B=7, %153906546, NA=0.0426, NB=-3.4, NC=7.7, F=15, K=90, T=The test are ended without any stop in the ground.

#\$

0:

1:

2:

3:

4:

5:

6:

7:

8:

9:

11:Tilt derivative alarm

12:Point resistance alarm

13:Depth unchanged for 5 second

14:Transmission lost

15:End of test

16:Dissipation start



**CPT -9**  
**Raw Data**

\$  
HA=1,HB=3,HC=CPTLOG-2.00,HD=8/19/2020,HG=-1.250,HP=-1.25,HJ=Brenton  
CPT,HK=c9,HM=07,HN=3206,HO=0.00,HQ=SA,HR=0°0'0.000"E,HS=0°0'0.000"N,HX=0.00,HY=0.00  
,HZ=0.00,KQ=1468.00,KF=6200.00,KU=2136.00,MA=0.590,MB=0.011,MC=10.0,MD=150.0,ME=c9,  
MF=0.000  
RN=,CA=0,CB=0

#  
D=0.000,QC=0.0665,FS=4.9,U=2.4,TA=2.19,B=20,%155489953,NA=5.6788,NB=314.2,NC=442.5  
D=0.020,QC=0.0665,FS=4.9,U=2.4,TA=2.19,B=20,%155489953  
D=0.040,QC=0.0691,FS=4.9,U=2.4,TA=2.25,B=19,%155490390  
D=0.060,QC=0.0628,FS=5.2,U=1.9,TA=2.36,B=19,%155491531  
D=0.080,QC=0.0587,FS=5.0,U=1.8,TA=2.28,B=19,%155492296  
D=0.100,QC=0.0540,FS=4.7,U=1.8,TA=2.43,B=19,%155493390  
D=0.120,QC=0.0551,FS=4.1,U=1.7,TA=2.12,B=18,%155494500  
D=0.140,QC=0.0577,FS=3.9,U=1.6,TA=2.28,B=19,%155495609  
D=0.160,QC=0.0556,FS=3.2,U=1.6,TA=2.33,B=19,%155496796  
D=0.180,QC=0.0556,FS=2.6,U=1.6,TA=2.30,B=18,%155497468  
D=0.200,QC=0.0514,FS=1.9,U=1.6,TA=2.21,B=18,%155498578  
D=0.220,QC=0.0525,FS=1.4,U=1.5,TA=2.12,B=18,%155499812  
D=0.240,QC=0.0514,FS=1.4,U=1.6,TA=2.31,B=19,%155500937  
D=0.260,QC=0.0525,FS=1.2,U=1.5,TA=2.17,B=18,%155502046  
D=0.280,QC=0.0545,FS=1.1,U=1.5,TA=2.16,B=18,%155503171  
D=0.300,QC=0.0566,FS=1.1,U=1.5,TA=2.31,B=19,%155503828  
D=0.320,QC=0.0571,FS=0.8,U=1.5,TA=2.31,B=19,%155505062  
D=0.340,QC=0.0644,FS=0.8,U=1.5,TA=2.15,B=18,%155506187  
D=0.360,QC=0.0686,FS=0.8,U=1.5,TA=2.14,B=18,%155507281  
D=0.380,QC=0.0732,FS=0.9,U=1.5,TA=2.12,B=18,%155508406  
D=0.400,QC=0.0758,FS=0.9,U=1.5,TA=2.24,B=19,%155509500  
D=0.420,QC=0.0852,FS=1.1,U=1.5,TA=2.19,B=18,%155510265  
D=0.440,QC=0.0951,FS=1.1,U=1.6,TA=2.26,B=17,%155511390  
D=0.460,QC=0.1054,FS=1.3,U=1.6,TA=2.17,B=17,%155512515  
D=0.480,QC=0.1834,FS=1.7,U=1.6,TA=2.22,B=20,%155513625  
D=0.500,QC=0.2763,FS=2.2,U=1.7,TA=2.24,B=25,%155514437  
D=0.520,QC=0.3179,FS=3.0,U=1.6,TA=2.24,B=29,%155515093  
D=0.540,QC=0.3220,FS=3.0,U=10.9,TA=2.20,B=31,%155515890  
D=0.560,QC=0.3220,FS=5.0,U=11.7,TA=2.20,B=31,%155516234  
D=0.580,QC=0.4342,FS=8.3,U=11.6,TA=2.30,B=30,%155517000 ,F=11  
D=0.600,QC=0.2867,FS=5.9,U=12.8,TA=2.40,B=31,%155518125  
D=0.620,QC=0.2867,FS=5.9,U=12.8,TA=2.40,B=31,%155518125 ,F=13  
D=0.640,QC=0.3906,FS=6.4,U=9.7,TA=2.26,B=19,%155556140  
D=0.660,QC=0.3906,FS=6.4,U=9.7,TA=2.26,B=19,%155556140  
D=0.680,QC=0.4233,FS=6.4,U=9.7,TA=2.24,B=19,%155556484  
D=0.700,QC=0.3802,FS=5.8,U=10.1,TA=2.26,B=21,%155557265  
D=0.720,QC=0.3932,FS=6.8,U=10.7,TA=2.26,B=22,%155558375  
D=0.740,QC=0.4929,FS=6.7,U=10.7,TA=2.26,B=23,%155559140  
D=0.760,QC=0.5999,FS=6.8,U=10.5,TA=2.26,B=21,%155559828  
D=0.780,QC=0.8051,FS=15.5,U=11.2,TA=2.26,B=21,%155561031  
D=0.800,QC=0.9360,FS=44.4,U=9.6,TA=2.26,B=23,%155561703  
D=0.820,QC=0.9666,FS=59.7,U=8.2,TA=2.26,B=21,%155562906  
D=0.840,QC=0.8695,FS=48.5,U=9.5,TA=2.26,B=20,%155563671

D=0.860, QC=0.7334, FS=28.6, U=10.2, TA=2.26, B=21, %155564781  
D=0.880, QC=0.7106, FS=13.6, U=4.9, TA=2.26, B=22, %155565468  
D=0.900, QC=0.6882, FS=3.2, U=5.7, TA=2.26, B=23, %155566562  
D=0.920, QC=0.6550, FS=2.1, U=6.1, TA=2.26, B=21, %155567343  
D=0.940, QC=0.6254, FS=1.4, U=6.3, TA=2.26, B=21, %155568093  
D=0.960, QC=0.5646, FS=1.9, U=6.5, TA=2.26, B=22, %155569218  
D=0.980, QC=0.6778, FS=3.6, U=6.2, TA=2.26, B=23, %155569984  
D=1.000, QC=0.7656, FS=5.3, U=5.9, TA=2.26, B=21, %155570750  
D=1.020, QC=0.7656, FS=15.5, U=4.8, TA=2.26, B=21, %155571859  
D=1.040, QC=0.7506, FS=7.7, U=5.4, TA=2.26, B=22, %155572640  
D=1.060, QC=0.6654, FS=2.3, U=5.9, TA=2.26, B=22, %155573765  
D=1.080, QC=0.6467, FS=1.0, U=6.1, TA=2.26, B=22, %155574546  
D=1.100, QC=0.6410, FS=0.9, U=6.1, TA=2.26, B=22, %155575203  
D=1.120, QC=0.6150, FS=2.2, U=6.0, TA=2.26, B=23, %155576406  
D=1.140, QC=0.5703, FS=3.0, U=6.1, TA=2.26, B=23, %155577078  
D=1.160, QC=0.6181, FS=5.3, U=5.9, TA=2.26, B=23, %155577875  
D=1.180, QC=0.7646, FS=27.3, U=4.4, TA=2.26, B=23, %155578671  
D=1.200, QC=0.8056, FS=39.5, U=3.1, TA=2.26, B=23, %155579328  
D=1.220, QC=0.7537, FS=30.6, U=3.0, TA=2.26, B=23, %155580531  
D=1.240, QC=0.7350, FS=15.5, U=3.7, TA=2.26, B=23, %155581203  
D=1.260, QC=0.6882, FS=3.3, U=4.7, TA=2.26, B=23, %155581984  
D=1.280, QC=0.5984, FS=-0.3, U=5.7, TA=2.26, B=20, %155583093  
D=1.300, QC=0.4192, FS=0.3, U=5.8, TA=2.26, B=19, %155584187  
D=1.320, QC=0.3740, FS=1.5, U=5.7, TA=2.26, B=19, %155584968  
D=1.340, QC=0.3293, FS=4.0, U=5.5, TA=2.26, B=20, %155586078  
D=1.360, QC=0.3667, FS=4.5, U=5.4, TA=2.26, B=20, %155587218  
D=1.380, QC=0.4763, FS=4.3, U=5.3, TA=2.26, B=18, %155587984  
D=1.400, QC=0.5225, FS=4.3, U=5.1, TA=2.26, B=19, %155589078  
D=1.420, QC=0.4644, FS=3.9, U=5.1, TA=2.26, B=18, %155590281  
D=1.440, QC=0.4238, FS=4.2, U=5.1, TA=2.26, B=20, %155590937  
D=1.460, QC=0.3823, FS=2.6, U=5.0, TA=2.26, B=18, %155592046  
D=1.480, QC=0.3740, FS=3.2, U=4.9, TA=2.26, B=18, %155593265  
D=1.500, QC=0.4244, FS=4.5, U=4.7, TA=2.26, B=19, %155594375  
D=1.520, QC=0.5121, FS=4.5, U=4.7, TA=2.26, B=19, %155595468  
D=1.540, QC=0.4732, FS=4.7, U=4.6, TA=2.26, B=18, %155596234  
D=1.560, QC=0.4233, FS=4.1, U=4.5, TA=2.26, B=18, %155597328  
D=1.580, QC=0.3142, FS=4.5, U=4.5, TA=2.26, B=20, %155598531  
D=1.600, QC=0.3116, FS=4.6, U=4.4, TA=2.26, B=20, %155599218  
D=1.620, QC=0.3439, FS=3.9, U=4.2, TA=2.26, B=20, %155600328  
D=1.640, QC=0.3880, FS=4.2, U=4.2, TA=2.26, B=19, %155601437  
D=1.660, QC=0.4161, FS=4.2, U=4.0, TA=2.26, B=18, %155602640  
D=1.680, QC=0.4462, FS=5.1, U=3.9, TA=2.26, B=20, %155603406  
D=1.700, QC=0.5210, FS=5.0, U=3.7, TA=2.26, B=18, %155604437  
D=1.720, QC=0.6243, FS=9.2, U=3.0, TA=2.26, B=18, %155605609  
D=1.740, QC=0.7500, FS=17.9, U=2.1, TA=2.26, B=18, %155606703  
D=1.760, QC=0.7490, FS=11.9, U=4.2, TA=2.26, B=19, %155607843  
D=1.780, QC=0.6394, FS=4.0, U=4.6, TA=2.26, B=19, %155608953  
D=1.800, QC=0.5594, FS=2.6, U=3.1, TA=2.26, B=18, %155609734  
D=1.820, QC=0.5007, FS=3.3, U=5.4, TA=2.26, B=18, %155610859  
D=1.840, QC=0.4264, FS=4.3, U=5.4, TA=2.18, B=18, %155611968

D=1.860, QC=0.4566, FS=5.3, U=4.4, TA=2.26, B=19, %155650265  
D=1.880, QC=0.4566, FS=5.3, U=4.4, TA=2.26, B=19, %155650265  
D=1.900, QC=0.4322, FS=6.4, U=4.8, TA=2.26, B=20, %155651375  
D=1.920, QC=0.4342, FS=7.5, U=4.7, TA=2.26, B=20, %155652500  
D=1.940, QC=0.3480, FS=6.2, U=4.7, TA=2.26, B=19, %155653625  
D=1.960, QC=0.3153, FS=6.6, U=4.6, TA=2.26, B=19, %155654296  
D=1.980, QC=0.3101, FS=5.3, U=4.5, TA=2.26, B=18, %155655437  
D=2.000, QC=0.4249, FS=5.3, U=4.5, TA=2.26, B=19, %155656640  
D=2.020, QC=0.4810, FS=5.9, U=4.4, TA=2.26, B=19, %155657312  
D=2.040, QC=0.5293, FS=5.9, U=4.3, TA=2.26, B=19, %155658515  
D=2.060, QC=0.3807, FS=4.6, U=4.2, TA=2.26, B=17, %155659609  
D=2.080, QC=0.3366, FS=5.3, U=4.2, TA=2.26, B=19, %155660703  
D=2.100, QC=0.3459, FS=4.6, U=4.1, TA=2.26, B=19, %155661843  
D=2.120, QC=0.3464, FS=5.0, U=4.1, TA=2.26, B=20, %155662625  
D=2.140, QC=0.3184, FS=5.6, U=3.9, TA=2.26, B=18, %155663718  
D=2.160, QC=0.3179, FS=5.3, U=3.8, TA=2.26, B=19, %155664843  
D=2.180, QC=0.3387, FS=5.5, U=3.6, TA=2.26, B=20, %155665953  
D=2.200, QC=0.3750, FS=5.1, U=3.5, TA=2.26, B=21, %155666734  
D=2.220, QC=0.4129, FS=4.7, U=3.5, TA=2.26, B=20, %155667828  
D=2.240, QC=0.3916, FS=5.5, U=3.3, TA=2.26, B=20, %155669031  
D=2.260, QC=0.3480, FS=5.9, U=3.3, TA=2.26, B=20, %155669703  
D=2.280, QC=0.2950, FS=6.0, U=3.2, TA=2.26, B=20, %155670828  
D=2.300, QC=0.2924, FS=5.0, U=3.1, TA=2.26, B=20, %155671609  
D=2.320, QC=0.3116, FS=4.9, U=2.9, TA=2.26, B=21, %155672734  
D=2.340, QC=0.3127, FS=4.8, U=2.8, TA=2.26, B=20, %155673421  
D=2.360, QC=0.2758, FS=5.0, U=2.8, TA=2.26, B=22, %155674625  
D=2.380, QC=0.2852, FS=4.8, U=2.7, TA=2.26, B=21, %155675312  
D=2.400, QC=0.3210, FS=3.5, U=2.6, TA=2.26, B=21, %155676421  
D=2.420, QC=0.3568, FS=2.7, U=2.4, TA=2.26, B=21, %155677187  
D=2.440, QC=0.4623, FS=3.8, U=2.2, TA=2.26, B=22, %155678312  
D=2.460, QC=0.4628, FS=5.0, U=2.2, TA=2.26, B=21, %155679093  
D=2.480, QC=0.4275, FS=4.3, U=2.0, TA=2.26, B=22, %155680218  
D=2.500, QC=0.3579, FS=5.3, U=2.0, TA=2.26, B=21, %155681000  
D=2.520, QC=0.2878, FS=4.7, U=1.9, TA=2.26, B=21, %155682093  
D=2.540, QC=0.2763, FS=3.9, U=1.8, TA=2.26, B=21, %155682875  
D=2.560, QC=0.2665, FS=4.5, U=1.6, TA=2.26, B=21, %155683984  
D=2.580, QC=0.2581, FS=3.8, U=1.5, TA=2.27, B=20, %155684781  
D=2.600, QC=0.2488, FS=3.5, U=1.4, TA=2.27, B=21, %155685890  
D=2.620, QC=0.2519, FS=3.4, U=1.3, TA=2.26, B=20, %155686562  
D=2.640, QC=0.2519, FS=1.9, U=1.0, TA=2.27, B=22, %155687687  
D=2.660, QC=0.2514, FS=1.6, U=0.9, TA=2.26, B=21, %155688453  
D=2.680, QC=0.2457, FS=1.7, U=0.8, TA=2.28, B=21, %155689656  
D=2.700, QC=0.2436, FS=2.2, U=0.7, TA=2.27, B=21, %155690328  
D=2.720, QC=0.2420, FS=2.0, U=0.5, TA=2.26, B=22, %155691093  
D=2.740, QC=0.2384, FS=1.9, U=0.3, TA=2.26, B=21, %155692187  
D=2.760, QC=0.2384, FS=1.9, U=0.2, TA=2.26, B=21, %155692968  
D=2.780, QC=0.2369, FS=1.8, U=2.4, TA=2.27, B=21, %155694093  
D=2.800, QC=0.2379, FS=1.9, U=2.2, TA=2.26, B=21, %155694875  
D=2.820, QC=0.2369, FS=1.3, U=2.1, TA=2.28, B=21, %155695984  
D=2.840, QC=0.2400, FS=1.4, U=1.9, TA=2.28, B=21, %155696750

D=2.860, QC=0.2405, FS=1.5, U=1.8, TA=2.26, B=21, %155697843  
D=2.880, QC=0.2426, FS=1.8, U=1.7, TA=2.27, B=21, %155698609  
D=2.900, QC=0.2436, FS=1.9, U=1.4, TA=2.26, B=21, %155699718  
D=2.920, QC=0.2457, FS=2.1, U=1.3, TA=2.26, B=21, %155700515  
D=2.940, QC=0.2431, FS=2.2, U=1.1, TA=2.26, B=20, %155701625  
D=2.960, QC=0.2379, FS=2.4, U=1.1, TA=2.27, B=21, %155702390  
D=2.980, QC=0.2420, FS=2.3, U=0.8, TA=2.26, B=21, %155703484  
D=3.000, QC=0.2384, FS=2.4, U=0.7, TA=2.28, B=21, %155704281  
D=3.020, QC=0.2415, FS=2.2, U=2.8, TA=2.29, B=20, %155705406  
D=3.040, QC=0.2208, FS=2.2, U=2.7, TA=2.30, B=20, %155706062  
D=3.060, QC=0.2306, FS=2.5, U=0.9, TA=2.29, B=23, %155744062  
D=3.080, QC=0.2306, FS=2.5, U=0.9, TA=2.29, B=23, %155744062  
D=3.100, QC=0.2337, FS=2.2, U=3.1, TA=2.33, B=22, %155744828  
D=3.120, QC=0.2394, FS=2.3, U=3.1, TA=2.34, B=23, %155745609  
D=3.140, QC=0.2581, FS=2.2, U=0.8, TA=2.37, B=22, %155746718  
D=3.160, QC=0.2857, FS=2.4, U=3.4, TA=2.33, B=22, %155747515  
D=3.180, QC=0.2867, FS=2.5, U=1.0, TA=2.35, B=22, %155748187  
D=3.200, QC=0.2914, FS=3.1, U=1.0, TA=2.35, B=23, %155749296  
D=3.220, QC=0.2924, FS=3.6, U=1.0, TA=2.38, B=22, %155750093  
D=3.240, QC=0.2841, FS=4.4, U=1.0, TA=2.37, B=23, %155750859  
D=3.260, QC=0.2763, FS=5.1, U=1.1, TA=2.38, B=21, %155751953  
D=3.280, QC=0.2794, FS=5.4, U=1.2, TA=2.39, B=22, %155752718  
D=3.300, QC=0.2815, FS=6.5, U=1.4, TA=2.39, B=21, %155753828  
D=3.320, QC=0.2763, FS=6.0, U=1.6, TA=2.38, B=23, %155754625  
D=3.340, QC=0.2654, FS=5.6, U=1.6, TA=2.39, B=21, %155755750  
D=3.360, QC=0.2701, FS=5.3, U=1.6, TA=2.40, B=22, %155756531  
D=3.380, QC=0.2789, FS=4.9, U=1.8, TA=2.39, B=22, %155757187  
D=3.400, QC=0.2779, FS=4.9, U=1.4, TA=2.43, B=22, %155758390  
D=3.420, QC=0.2774, FS=4.8, U=1.1, TA=2.42, B=22, %155759062  
D=3.440, QC=0.2727, FS=4.1, U=1.2, TA=2.43, B=23, %155759828  
D=3.460, QC=0.2763, FS=3.7, U=1.1, TA=2.47, B=22, %155760921  
D=3.480, QC=0.2706, FS=3.2, U=1.2, TA=2.49, B=23, %155761687  
D=3.500, QC=0.2727, FS=3.1, U=1.1, TA=2.48, B=23, %155762468  
D=3.520, QC=0.2763, FS=2.3, U=1.3, TA=2.49, B=24, %155763609  
D=3.540, QC=0.2815, FS=2.4, U=1.5, TA=2.48, B=22, %155764390  
D=3.560, QC=0.2789, FS=2.5, U=1.5, TA=2.47, B=25, %155765062  
D=3.580, QC=0.2748, FS=2.7, U=1.6, TA=2.49, B=21, %155766203  
D=3.600, QC=0.2794, FS=3.2, U=1.8, TA=2.47, B=18, %155766968  
D=3.620, QC=0.2774, FS=3.5, U=1.0, TA=2.49, B=18, %155768109  
D=3.640, QC=0.2805, FS=4.0, U=1.1, TA=2.49, B=19, %155769218  
D=3.660, QC=0.2831, FS=5.1, U=1.3, TA=2.49, B=18, %155770312  
D=3.680, QC=0.2878, FS=5.4, U=1.4, TA=2.47, B=19, %155771437  
D=3.700, QC=0.2987, FS=5.5, U=1.6, TA=2.45, B=18, %155772640  
D=3.720, QC=0.3028, FS=5.6, U=1.7, TA=2.46, B=19, %155773421  
D=3.740, QC=0.3080, FS=5.8, U=1.9, TA=2.45, B=18, %155774421  
D=3.760, QC=0.3044, FS=5.1, U=2.1, TA=2.46, B=19, %155775625  
D=3.780, QC=0.3007, FS=4.8, U=2.2, TA=2.43, B=18, %155776734  
D=3.800, QC=0.2981, FS=3.9, U=2.4, TA=2.44, B=19, %155777828  
D=3.820, QC=0.2904, FS=3.9, U=2.5, TA=2.42, B=18, %155778953  
D=3.840, QC=0.2846, FS=4.0, U=2.6, TA=2.43, B=19, %155779734

D=3.860, QC=0.2711, FS=4.3, U=2.8, TA=2.41, B=18, %155780859  
D=3.880, QC=0.2706, FS=4.6, U=2.9, TA=2.39, B=19, %155781968  
D=3.900, QC=0.2784, FS=4.6, U=3.2, TA=2.40, B=18, %155783078  
D=3.920, QC=0.3688, FS=5.2, U=3.2, TA=2.39, B=19, %155784187  
D=3.940, QC=0.4249, FS=5.5, U=3.4, TA=2.41, B=18, %155785328  
D=3.960, QC=0.4327, FS=5.9, U=3.4, TA=2.43, B=18, %155786453  
D=3.980, QC=0.3781, FS=7.0, U=3.4, TA=2.42, B=17, %155787234  
D=4.000, QC=0.3210, FS=6.0, U=3.7, TA=2.43, B=18, %155788343  
D=4.020, QC=0.3506, FS=3.8, U=3.7, TA=2.42, B=18, %155789453  
D=4.040, QC=0.5132, FS=4.9, U=3.4, TA=2.48, B=18, %155790578  
D=4.060, QC=0.6877, FS=5.7, U=4.2, TA=2.46, B=17, %155791671  
D=4.080, QC=0.6436, FS=4.1, U=4.6, TA=2.42, B=18, %155792890  
D=4.100, QC=0.4696, FS=3.5, U=4.6, TA=2.41, B=18, %155794031  
D=4.120, QC=0.3922, FS=4.0, U=4.7, TA=2.40, B=18, %155795125  
D=4.140, QC=0.7287, FS=6.2, U=4.6, TA=2.48, B=17, %155796250  
D=4.160, QC=0.7038, FS=19.4, U=5.1, TA=2.47, B=17, %155797375  
D=4.180, QC=1.1495, FS=44.4, U=6.6, TA=2.50, B=16, %155798468  
D=4.200, QC=1.3702, FS=75.8, U=10.6, TA=2.50, B=16, %155799578  
D=4.220, QC=1.7421, FS=79.6, U=12.2, TA=2.48, B=15, %155801125  
D=4.240, QC=1.7857, FS=79.1, U=12.5, TA=2.43, B=15, %155802250  
D=4.260, QC=1.6164, FS=76.5, U=13.9, TA=2.46, B=19, %155840093  
D=4.280, QC=1.6164, FS=76.5, U=13.9, TA=2.46, B=19, %155840093  
D=4.300, QC=1.2523, FS=76.5, U=13.9, TA=2.49, B=20, %155840562  
D=4.320, QC=0.8233, FS=73.8, U=12.9, TA=2.50, B=22, %155841250  
D=4.340, QC=0.7235, FS=32.8, U=10.4, TA=2.48, B=21, %155842343  
D=4.360, QC=0.6368, FS=18.0, U=8.5, TA=2.50, B=20, %155843453  
D=4.380, QC=0.5615, FS=12.8, U=7.7, TA=2.50, B=20, %155844250  
D=4.400, QC=0.4810, FS=12.0, U=7.4, TA=2.50, B=22, %155845359  
D=4.420, QC=0.4488, FS=11.1, U=7.4, TA=2.50, B=21, %155846156  
D=4.440, QC=0.4311, FS=10.2, U=7.5, TA=2.50, B=21, %155847265  
D=4.460, QC=0.4238, FS=9.1, U=7.6, TA=2.51, B=20, %155848031  
D=4.480, QC=0.4140, FS=7.2, U=7.8, TA=2.50, B=21, %155849125  
D=4.500, QC=0.4109, FS=5.7, U=7.9, TA=2.50, B=20, %155849906  
D=4.520, QC=0.4140, FS=4.9, U=8.1, TA=2.51, B=21, %155851046  
D=4.540, QC=0.4249, FS=4.1, U=8.2, TA=2.50, B=20, %155851703  
D=4.560, QC=0.4353, FS=3.6, U=8.4, TA=2.51, B=20, %155852921  
D=4.580, QC=0.4462, FS=4.2, U=8.5, TA=2.51, B=21, %155853609  
D=4.600, QC=0.4358, FS=5.1, U=8.6, TA=2.50, B=22, %155854734  
D=4.620, QC=0.4306, FS=6.0, U=8.7, TA=2.48, B=20, %155855500  
D=4.640, QC=0.4238, FS=6.7, U=8.9, TA=2.51, B=21, %155856593  
D=4.660, QC=0.4171, FS=6.5, U=9.0, TA=2.50, B=21, %155857359  
D=4.680, QC=0.4145, FS=6.4, U=9.2, TA=2.51, B=22, %155858453  
D=4.700, QC=0.4135, FS=6.7, U=9.3, TA=2.49, B=21, %155859218  
D=4.720, QC=0.4135, FS=6.3, U=9.5, TA=2.50, B=22, %155860421  
D=4.740, QC=0.4186, FS=6.1, U=9.6, TA=2.50, B=21, %155861109  
D=4.760, QC=0.4129, FS=5.8, U=9.7, TA=2.51, B=22, %155862234  
D=4.780, QC=0.4046, FS=5.8, U=9.8, TA=2.50, B=21, %155863000  
D=4.800, QC=0.3984, FS=5.8, U=9.9, TA=2.51, B=22, %155863781  
D=4.820, QC=0.3968, FS=6.0, U=10.0, TA=2.50, B=22, %155864890  
D=4.840, QC=0.3901, FS=6.2, U=10.1, TA=2.49, B=24, %155865656

D=4.860, QC=0.3864, FS=6.5, U=10.2, TA=2.51, B=24, %155866437  
D=4.880, QC=0.3833, FS=6.4, U=10.3, TA=2.49, B=24, %155867109  
D=4.900, QC=0.3864, FS=6.3, U=10.4, TA=2.51, B=25, %155867875  
D=4.920, QC=0.3901, FS=6.3, U=10.5, TA=2.51, B=26, %155868968  
D=4.940, QC=0.3906, FS=6.2, U=10.6, TA=2.51, B=25, %155869750  
D=4.960, QC=0.3916, FS=6.3, U=10.8, TA=2.51, B=26, %155870531  
D=4.980, QC=0.3906, FS=5.8, U=10.9, TA=2.51, B=24, %155871218  
D=5.000, QC=0.3932, FS=5.8, U=11.0, TA=2.51, B=26, %155871984  
D=5.020, QC=0.3979, FS=5.7, U=11.1, TA=2.51, B=25, %155872750  
D=5.040, QC=0.3994, FS=5.8, U=11.2, TA=2.50, B=26, %155873546  
D=5.060, QC=0.4020, FS=5.6, U=11.3, TA=2.49, B=24, %155874250  
D=5.080, QC=0.4098, FS=5.5, U=11.4, TA=2.51, B=25, %155875015  
D=5.100, QC=0.4103, FS=5.3, U=11.5, TA=2.50, B=25, %155875796  
D=5.120, QC=0.4103, FS=5.3, U=11.6, TA=2.51, B=27, %155876484  
D=5.140, QC=0.4124, FS=5.4, U=11.7, TA=2.51, B=26, %155877296  
D=5.160, QC=0.3994, FS=5.8, U=11.9, TA=2.51, B=27, %155877953  
D=5.180, QC=0.3849, FS=5.7, U=11.9, TA=2.50, B=28, %155878734  
D=5.200, QC=0.3740, FS=5.5, U=12.0, TA=2.49, B=30, %155879515  
D=5.220, QC=0.3787, FS=5.4, U=12.2, TA=2.49, B=29, %155880296  
D=5.240, QC=0.3792, FS=5.2, U=12.2, TA=2.47, B=28, %155880968  
D=5.260, QC=0.3792, FS=5.1, U=10.1, TA=2.47, B=28, %155881421  
D=5.280, QC=0.3833, FS=4.5, U=10.2, TA=2.50, B=29, %155882093  
D=5.300, QC=0.3880, FS=4.3, U=12.5, TA=2.49, B=26, %155882875  
D=5.320, QC=0.3870, FS=4.2, U=12.6, TA=2.49, B=24, %155883656  
D=5.340, QC=0.4005, FS=4.3, U=12.7, TA=2.49, B=23, %155884781  
D=5.360, QC=0.3948, FS=4.3, U=10.6, TA=2.47, B=23, %155885562  
D=5.380, QC=0.3958, FS=4.6, U=13.0, TA=2.46, B=23, %155886203  
D=5.400, QC=0.3916, FS=5.0, U=13.1, TA=2.46, B=24, %155887000  
D=5.420, QC=0.3833, FS=5.0, U=11.1, TA=2.48, B=22, %155888109  
D=5.440, QC=0.3807, FS=4.7, U=11.2, TA=2.48, B=23, %155888890  
D=5.460, QC=0.3641, FS=5.0, U=14.2, TA=2.48, B=27, %155927328  
D=5.480, QC=0.3641, FS=5.0, U=14.2, TA=2.48, B=27, %155927328  
D=5.500, QC=0.3641, FS=5.0, U=14.2, TA=2.48, B=27, %155927328  
D=5.520, QC=0.3729, FS=4.6, U=13.7, TA=2.51, B=25, %155928015  
D=5.540, QC=0.3781, FS=4.7, U=13.7, TA=2.49, B=26, %155928796  
D=5.560, QC=0.3797, FS=4.5, U=13.9, TA=2.51, B=24, %155929562  
D=5.580, QC=0.3859, FS=4.6, U=13.9, TA=2.50, B=25, %155930328  
D=5.600, QC=0.3833, FS=4.6, U=14.0, TA=2.51, B=23, %155930984  
D=5.620, QC=0.3771, FS=4.8, U=14.0, TA=2.51, B=24, %155932218  
D=5.640, QC=0.3714, FS=5.0, U=14.1, TA=2.51, B=23, %155932859  
D=5.660, QC=0.3646, FS=4.9, U=14.1, TA=2.51, B=25, %155933640  
D=5.680, QC=0.3615, FS=4.8, U=14.2, TA=2.51, B=22, %155934421  
D=5.700, QC=0.3558, FS=4.7, U=14.4, TA=2.50, B=23, %155935187  
D=5.720, QC=0.3553, FS=4.7, U=14.5, TA=2.51, B=24, %155936296  
D=5.740, QC=0.3584, FS=4.6, U=14.6, TA=2.51, B=25, %155937062  
D=5.760, QC=0.3610, FS=4.6, U=14.7, TA=2.50, B=24, %155937718  
D=5.780, QC=0.3636, FS=4.4, U=14.7, TA=2.51, B=25, %155938484  
D=5.800, QC=0.3662, FS=4.3, U=14.8, TA=2.50, B=24, %155939250  
D=5.820, QC=0.3610, FS=4.3, U=14.9, TA=2.50, B=24, %155940375  
D=5.840, QC=0.3657, FS=4.4, U=15.0, TA=2.49, B=24, %155941187

D=5.860, QC=0.3740, FS=4.4, U=15.0, TA=2.48, B=25, %155941843  
D=5.880, QC=0.3807, FS=4.4, U=15.1, TA=2.50, B=25, %155942640  
D=5.900, QC=0.3755, FS=4.4, U=15.3, TA=2.48, B=27, %155943406  
D=5.920, QC=0.3719, FS=4.4, U=15.3, TA=2.50, B=25, %155944187  
D=5.940, QC=0.3714, FS=4.3, U=15.5, TA=2.49, B=26, %155944953  
D=5.960, QC=0.3662, FS=4.6, U=15.5, TA=2.51, B=25, %155945625  
D=5.980, QC=0.3662, FS=4.6, U=15.6, TA=2.50, B=26, %155946421  
D=6.000, QC=0.3693, FS=4.5, U=15.7, TA=2.48, B=26, %155947093  
D=6.020, QC=0.3735, FS=4.5, U=15.8, TA=2.48, B=26, %155947843  
D=6.040, QC=0.3740, FS=4.5, U=15.8, TA=2.47, B=26, %155948625  
D=6.060, QC=0.3766, FS=4.5, U=16.0, TA=2.49, B=27, %155949421  
D=6.080, QC=0.3776, FS=4.3, U=16.1, TA=2.47, B=26, %155950187  
D=6.100, QC=0.3812, FS=4.1, U=16.2, TA=2.49, B=26, %155950890  
D=6.120, QC=0.3870, FS=4.2, U=16.2, TA=2.48, B=24, %155951687  
D=6.140, QC=0.3885, FS=4.4, U=16.3, TA=2.48, B=26, %155952453  
D=6.160, QC=0.3942, FS=4.5, U=16.5, TA=2.49, B=25, %155953578  
D=6.180, QC=0.4031, FS=4.7, U=16.6, TA=2.49, B=26, %155954250  
D=6.200, QC=0.3979, FS=4.8, U=16.7, TA=2.50, B=25, %155955031  
D=6.220, QC=0.3927, FS=4.9, U=16.8, TA=2.51, B=25, %155955796  
D=6.240, QC=0.3953, FS=5.7, U=16.9, TA=2.50, B=25, %155956562  
D=6.260, QC=0.3875, FS=6.3, U=17.0, TA=2.49, B=26, %155957234  
D=6.280, QC=0.3838, FS=6.5, U=17.1, TA=2.51, B=25, %155958000  
D=6.300, QC=0.3849, FS=5.9, U=17.2, TA=2.51, B=25, %155958781  
D=6.320, QC=0.3844, FS=5.5, U=17.3, TA=2.50, B=25, %155959546  
D=6.340, QC=0.3838, FS=5.5, U=17.4, TA=2.50, B=26, %155960328  
D=6.360, QC=0.3833, FS=5.0, U=17.5, TA=2.49, B=25, %155961000  
D=6.380, QC=0.3849, FS=4.5, U=17.6, TA=2.50, B=25, %155961765  
D=6.400, QC=0.3844, FS=4.8, U=17.7, TA=2.52, B=24, %155962531  
D=6.420, QC=0.3849, FS=4.6, U=17.8, TA=2.50, B=26, %155963312  
D=6.440, QC=0.3854, FS=4.8, U=17.9, TA=2.50, B=25, %155964078  
D=6.460, QC=0.3859, FS=4.9, U=18.0, TA=2.49, B=24, %155965218  
D=6.480, QC=0.3807, FS=4.8, U=18.1, TA=2.49, B=24, %155965875  
D=6.500, QC=0.3854, FS=5.0, U=18.2, TA=2.46, B=25, %155966687  
D=6.520, QC=0.3854, FS=4.8, U=18.2, TA=2.49, B=24, %155967359  
D=6.540, QC=0.3828, FS=4.9, U=18.4, TA=2.47, B=25, %155968125  
D=6.560, QC=0.3849, FS=5.0, U=18.4, TA=2.49, B=23, %155968890  
D=6.580, QC=0.3854, FS=2.9, U=18.7, TA=2.46, B=23, %155969984 , F=11  
D=6.600, QC=0.4353, FS=7.7, U=20.1, TA=2.76, B=19, %156025375  
D=6.620, QC=0.4353, FS=7.7, U=20.1, TA=2.76, B=19, %156025375  
D=6.640, QC=0.4353, FS=7.6, U=19.6, TA=2.76, B=22, %156025718  
D=6.660, QC=0.4306, FS=7.7, U=19.7, TA=2.76, B=23, %156026484  
D=6.680, QC=0.4093, FS=9.0, U=19.7, TA=2.77, B=21, %156027296  
D=6.700, QC=0.3766, FS=8.7, U=22.3, TA=2.79, B=20, %156028312  
D=6.720, QC=0.3771, FS=8.0, U=19.9, TA=2.78, B=21, %156029109  
D=6.740, QC=0.3771, FS=7.6, U=20.0, TA=2.79, B=22, %156030234  
D=6.760, QC=0.3802, FS=7.5, U=20.1, TA=2.79, B=22, %156031015  
D=6.780, QC=0.3792, FS=7.3, U=20.2, TA=2.78, B=20, %156031687  
D=6.800, QC=0.3792, FS=7.3, U=20.2, TA=2.79, B=22, %156032796  
D=6.820, QC=0.3766, FS=7.2, U=20.3, TA=2.79, B=22, %156033609  
D=6.840, QC=0.3724, FS=7.5, U=20.5, TA=2.79, B=22, %156034703



D=6.860, QC=0.3709, FS=7.7, U=20.6, TA=2.79, B=20, %156035484  
D=6.880, QC=0.3683, FS=7.9, U=20.6, TA=2.79, B=21, %156036578  
D=6.900, QC=0.3667, FS=8.1, U=20.6, TA=2.78, B=22, %156037343  
D=6.920, QC=0.3662, FS=7.9, U=20.8, TA=2.78, B=22, %156038125  
D=6.940, QC=0.3672, FS=7.5, U=21.0, TA=2.78, B=21, %156039234  
D=6.960, QC=0.3657, FS=7.5, U=21.0, TA=2.77, B=21, %156040000  
D=6.980, QC=0.3615, FS=7.5, U=21.1, TA=2.78, B=22, %156041125  
D=7.000, QC=0.3594, FS=7.3, U=21.2, TA=2.77, B=23, %156041906  
D=7.020, QC=0.3600, FS=7.2, U=21.3, TA=2.80, B=22, %156042546  
D=7.040, QC=0.3532, FS=7.2, U=21.4, TA=2.81, B=23, %156043781  
D=7.060, QC=0.3563, FS=7.3, U=21.5, TA=2.78, B=23, %156044453  
D=7.080, QC=0.3574, FS=7.6, U=21.6, TA=2.78, B=23, %156045218  
D=7.100, QC=0.3662, FS=7.9, U=21.7, TA=2.80, B=23, %156046328  
D=7.120, QC=0.3761, FS=7.8, U=21.8, TA=2.81, B=23, %156047109  
D=7.140, QC=0.3880, FS=7.5, U=22.0, TA=2.80, B=23, %156047875  
D=7.160, QC=0.4212, FS=7.3, U=22.1, TA=2.80, B=23, %156048656  
D=7.180, QC=0.4721, FS=7.6, U=22.2, TA=2.81, B=23, %156049671  
D=7.200, QC=0.4805, FS=7.5, U=22.3, TA=2.81, B=24, %156050437  
D=7.220, QC=0.4836, FS=8.9, U=22.4, TA=2.82, B=23, %156051203  
D=7.240, QC=0.6186, FS=13.2, U=22.4, TA=2.83, B=23, %156051968  
D=7.260, QC=0.8664, FS=37.4, U=25.5, TA=2.84, B=23, %156053078  
D=7.280, QC=0.9661, FS=57.2, U=28.0, TA=2.84, B=23, %156053843  
D=7.300, QC=0.9703, FS=66.3, U=29.1, TA=2.84, B=23, %156054609  
D=7.320, QC=0.8539, FS=48.5, U=29.1, TA=2.84, B=23, %156055703  
D=7.340, QC=0.7734, FS=24.6, U=26.7, TA=2.84, B=22, %156056500  
D=7.360, QC=0.7396, FS=14.1, U=24.6, TA=2.85, B=23, %156057265  
D=7.380, QC=0.6394, FS=13.5, U=23.7, TA=2.84, B=24, %156057937  
D=7.400, QC=0.4857, FS=14.3, U=23.5, TA=2.87, B=23, %156059062  
D=7.420, QC=0.4732, FS=13.6, U=23.5, TA=2.87, B=23, %156059859  
D=7.440, QC=0.4716, FS=15.3, U=23.5, TA=2.85, B=23, %156060625  
D=7.460, QC=0.4675, FS=13.9, U=23.7, TA=2.84, B=23, %156061718  
D=7.480, QC=0.5303, FS=12.6, U=23.9, TA=2.84, B=24, %156062484  
D=7.500, QC=0.6436, FS=24.9, U=25.1, TA=2.88, B=22, %156063250  
D=7.520, QC=0.8446, FS=60.5, U=29.8, TA=2.88, B=22, %156063937  
D=7.540, QC=1.5286, FS=81.5, U=32.6, TA=2.90, B=21, %156065062  
D=7.560, QC=1.8605, FS=85.7, U=33.7, TA=2.89, B=21, %156065828  
D=7.580, QC=1.9623, FS=82.7, U=34.4, TA=2.92, B=19, %156066921  
D=7.600, QC=1.5640, FS=80.7, U=34.3, TA=2.88, B=21, %156068125  
D=7.620, QC=1.1941, FS=78.7, U=34.1, TA=2.87, B=20, %156068828  
D=7.640, QC=0.8851, FS=54.2, U=32.3, TA=2.88, B=22, %156070015  
D=7.660, QC=0.7490, FS=33.7, U=29.8, TA=2.86, B=21, %156070687  
D=7.680, QC=0.7313, FS=26.0, U=28.0, TA=2.89, B=21, %156071453  
D=7.700, QC=0.6093, FS=24.4, U=26.7, TA=2.88, B=22, %156072609  
D=7.720, QC=0.5823, FS=27.7, U=26.1, TA=2.88, B=23, %156073390  
D=7.740, QC=0.5714, FS=29.2, U=26.0, TA=2.88, B=22, %156074062  
D=7.760, QC=0.5615, FS=27.4, U=25.9, TA=2.85, B=22, %156075250  
D=7.780, QC=0.0234, FS=51.5, U=40.9, TA=2.63, B=26, %156121312  
D=7.800, QC=0.0234, FS=51.5, U=40.9, TA=2.63, B=26, %156121312  
D=7.820, QC=0.0234, FS=51.5, U=40.9, TA=2.63, B=26, %156121312  
D=7.840, QC=0.0670, FS=48.8, U=40.6, TA=2.64, B=26, %156121984

D=7.860, QC=0.0919, FS=47.8, U=40.7, TA=2.62, B=20, %156122750  
D=7.880, QC=0.0909, FS=47.6, U=40.6, TA=2.61, B=20, %156123890  
D=7.900, QC=0.0613, FS=47.3, U=40.7, TA=2.61, B=19, %156124671  
D=7.920, QC=0.0286, FS=46.2, U=40.8, TA=2.62, B=21, %156125781  
D=7.940, QC=0.0551, FS=45.8, U=40.9, TA=2.61, B=20, %156126890  
D=7.960, QC=0.0488, FS=46.6, U=41.0, TA=2.62, B=20, %156127656  
D=7.980, QC=0.0306, FS=46.4, U=41.2, TA=2.62, B=23, %156128765  
D=8.000, QC=0.0416, FS=46.4, U=41.2, TA=2.63, B=24, %156129546  
D=8.020, QC=0.0706, FS=46.0, U=41.3, TA=2.62, B=23, %156130234  
D=8.040, QC=0.0758, FS=46.5, U=41.4, TA=2.62, B=23, %156131000  
D=8.060, QC=0.0753, FS=46.8, U=41.5, TA=2.62, B=22, %156132109  
D=8.080, QC=0.0738, FS=47.1, U=41.5, TA=2.62, B=23, %156132875  
D=8.100, QC=0.0795, FS=46.7, U=41.7, TA=2.62, B=24, %156133671  
D=8.120, QC=0.0784, FS=46.7, U=41.7, TA=2.62, B=23, %156134343  
D=8.140, QC=0.0764, FS=46.9, U=41.8, TA=2.62, B=22, %156135562  
D=8.160, QC=0.0774, FS=46.2, U=42.1, TA=2.63, B=23, %156136250 , F=13  
D=8.180, QC=0.0545, FS=45.6, U=45.1, TA=2.63, B=0, %156165453  
D=8.200, QC=0.0426, FS=46.1, U=45.3, TA=2.61, B=12, %156167015  
D=8.220, QC=0.0483, FS=46.2, U=45.4, TA=2.61, B=11, %156168875  
D=8.240, QC=0.0452, FS=46.4, U=45.7, TA=2.65, B=11, %156170421  
D=8.260, QC=0.0483, FS=45.6, U=45.8, TA=2.62, B=19, %156171531  
D=8.280, QC=0.0467, FS=45.2, U=45.9, TA=2.61, B=20, %156172656  
D=8.300, QC=0.0452, FS=44.9, U=46.0, TA=2.61, B=18, %156173421  
D=8.320, QC=0.0467, FS=45.0, U=46.2, TA=2.62, B=18, %156174546  
D=8.340, QC=0.0488, FS=44.5, U=46.3, TA=2.62, B=19, %156175640  
D=8.360, QC=0.0504, FS=44.8, U=46.5, TA=2.60, B=19, %156176750 , F=13  
D=8.380, QC=0.0467, FS=46.8, U=47.7, TA=2.60, B=1, %156185734  
D=8.400, QC=0.0374, FS=46.8, U=47.8, TA=2.59, B=25, %156186531  
D=8.420, QC=0.0348, FS=46.8, U=47.9, TA=2.59, B=25, %156187296  
D=8.440, QC=0.0338, FS=46.5, U=48.0, TA=2.59, B=26, %156187984  
D=8.460, QC=0.0260, FS=47.0, U=48.2, TA=2.60, B=26, %156188750  
D=8.480, QC=0.0244, FS=46.4, U=48.3, TA=2.60, B=28, %156189515  
D=8.500, QC=0.0358, FS=45.8, U=48.4, TA=2.60, B=21, %156190296  
D=8.520, QC=0.0431, FS=45.5, U=48.5, TA=2.60, B=23, %156191390  
D=8.540, QC=0.0384, FS=45.4, U=48.5, TA=2.60, B=22, %156192187  
D=8.560, QC=0.0270, FS=45.5, U=48.7, TA=2.60, B=23, %156192859  
D=8.580, QC=0.0177, FS=46.0, U=49.0, TA=2.60, B=23, %156194062  
D=8.600, QC=0.1350, FS=49.1, U=49.3, TA=2.60, B=23, %156194734  
D=8.620, QC=0.5817, FS=60.0, U=50.4, TA=2.61, B=23, %156195484  
D=8.640, QC=0.8300, FS=76.0, U=51.9, TA=2.62, B=22, %156196250  
D=8.660, QC=0.9064, FS=77.9, U=52.6, TA=2.61, B=22, %156197359  
D=8.680, QC=0.9116, FS=79.7, U=52.9, TA=2.61, B=21, %156198140  
D=8.700, QC=0.9168, FS=89.2, U=53.6, TA=2.61, B=22, %156199234  
D=8.720, QC=0.9422, FS=97.3, U=54.6, TA=2.62, B=22, %156200015  
D=8.740, QC=0.9573, FS=106.8, U=55.9, TA=2.65, B=22, %156200796  
D=8.760, QC=1.0160, FS=116.2, U=56.8, TA=2.59, B=22, %156201890  
D=8.780, QC=0.9308, FS=106.0, U=56.3, TA=2.63, B=21, %156202687  
D=8.800, QC=0.8259, FS=62.2, U=52.9, TA=2.64, B=23, %156203781  
D=8.820, QC=0.7578, FS=53.6, U=52.3, TA=2.63, B=22, %156204562  
D=8.840, QC=0.7282, FS=45.2, U=51.4, TA=2.63, B=22, %156205218

D=8.860, QC=0.4981, FS=43.0, U=50.5, TA=2.62, B=22, %156206421  
D=8.880, QC=0.3288, FS=44.2, U=50.0, TA=2.62, B=23, %156207187  
D=8.900, QC=0.2275, FS=46.4, U=49.7, TA=2.64, B=23, %156207859  
D=8.920, QC=0.2509, FS=42.8, U=49.7, TA=2.63, B=23, %156208953  
D=8.940, QC=0.3189, FS=43.4, U=50.0, TA=2.61, B=21, %156209734  
D=8.960, QC=0.3516, FS=40.6, U=50.2, TA=2.64, B=21, %156210515 , F=11  
D=8.980, QC=0.1771, FS=45.4, U=50.2, TA=2.70, B=19, %156255750  
D=9.000, QC=0.1771, FS=45.4, U=50.2, TA=2.70, B=19, %156255750  
D=9.020, QC=0.1771, FS=45.6, U=49.8, TA=2.70, B=19, %156256093  
D=9.040, QC=0.0925, FS=42.5, U=49.9, TA=2.65, B=19, %156257203  
D=9.060, QC=0.0883, FS=38.1, U=50.0, TA=2.70, B=20, %156258406  
D=9.080, QC=0.0857, FS=38.4, U=52.4, TA=2.57, B=19, %156259078  
D=9.100, QC=0.1028, FS=39.0, U=50.2, TA=2.59, B=19, %156260250  
D=9.120, QC=0.1112, FS=38.1, U=50.4, TA=2.59, B=19, %156261375  
D=9.140, QC=0.2768, FS=40.0, U=51.0, TA=2.57, B=21, %156262171  
D=9.160, QC=0.8550, FS=55.2, U=55.3, TA=2.53, B=19, %156263265  
D=9.180, QC=0.9256, FS=99.2, U=57.3, TA=2.52, B=17, %156264390  
D=9.200, QC=0.9360, FS=106.2, U=60.2, TA=2.52, B=17, %156265515  
D=9.220, QC=0.9298, FS=101.3, U=59.7, TA=2.53, B=18, %156266625  
D=9.240, QC=0.8659, FS=90.8, U=59.3, TA=2.52, B=14, %156267750  
D=9.260, QC=0.8482, FS=75.0, U=58.3, TA=2.52, B=14, %156269281  
D=9.280, QC=0.8264, FS=66.6, U=55.4, TA=2.58, B=14, %156270750  
D=9.300, QC=0.7978, FS=50.0, U=53.7, TA=2.57, B=15, %156271890  
D=9.320, QC=0.6908, FS=43.1, U=54.2, TA=2.60, B=15, %156273375  
D=9.340, QC=0.5553, FS=44.5, U=53.8, TA=2.60, B=14, %156274515  
D=9.360, QC=0.3683, FS=50.1, U=53.3, TA=2.61, B=15, %156275968  
D=9.380, QC=0.2711, FS=48.6, U=50.9, TA=2.61, B=15, %156277078  
D=9.400, QC=0.1927, FS=49.4, U=50.9, TA=2.61, B=15, %156278296  
D=9.420, QC=0.1486, FS=49.9, U=53.3, TA=2.62, B=15, %156279734  
D=9.440, QC=0.1475, FS=46.1, U=51.2, TA=2.62, B=15, %156280859  
D=9.460, QC=0.1382, FS=43.9, U=51.5, TA=2.62, B=15, %156282406  
D=9.480, QC=0.1288, FS=42.2, U=51.5, TA=2.62, B=16, %156283531  
D=9.500, QC=0.1205, FS=38.2, U=51.8, TA=2.63, B=15, %156284640  
D=9.520, QC=0.1112, FS=35.0, U=52.0, TA=2.63, B=16, %156286062  
D=9.540, QC=0.0982, FS=34.3, U=54.4, TA=2.63, B=16, %156287265  
D=9.560, QC=0.0940, FS=33.8, U=52.4, TA=2.62, B=15, %156288375  
D=9.580, QC=0.0971, FS=33.8, U=52.7, TA=2.62, B=15, %156289828  
D=9.600, QC=0.1023, FS=34.1, U=52.8, TA=2.62, B=15, %156290953  
D=9.620, QC=0.1034, FS=34.5, U=55.3, TA=2.62, B=15, %156292515  
D=9.640, QC=0.1065, FS=34.8, U=53.3, TA=2.62, B=15, %156293609  
D=9.660, QC=0.1101, FS=34.8, U=53.4, TA=2.61, B=15, %156294750  
D=9.680, QC=0.1117, FS=35.2, U=53.7, TA=2.63, B=16, %156296296  
D=9.700, QC=0.1080, FS=35.1, U=53.9, TA=2.64, B=16, %156297406  
D=9.720, QC=0.1148, FS=35.5, U=56.4, TA=2.62, B=16, %156298515  
D=9.740, QC=0.1112, FS=35.6, U=56.7, TA=2.63, B=16, %156299625  
D=9.760, QC=0.1148, FS=35.7, U=57.0, TA=2.63, B=16, %156301171  
D=9.780, QC=0.1138, FS=35.7, U=57.1, TA=2.62, B=17, %156302281  
D=9.800, QC=0.1252, FS=35.7, U=57.4, TA=2.63, B=16, %156303390  
D=9.820, QC=0.1382, FS=35.8, U=55.3, TA=2.63, B=16, %156304515  
D=9.840, QC=0.1454, FS=36.2, U=55.7, TA=2.63, B=16, %156305640

D=9.860, QC=0.1387, FS=36.5, U=55.8, TA=2.64, B=17, %156306765  
D=9.880, QC=0.1299, FS=36.5, U=56.2, TA=2.63, B=16, %156308234  
D=9.900, QC=0.1267, FS=37.1, U=56.4, TA=2.67, B=16, %156309328  
D=9.920, QC=0.1189, FS=37.1, U=56.5, TA=2.67, B=16, %156310546  
D=9.940, QC=0.1184, FS=36.8, U=59.0, TA=2.64, B=16, %156311640  
D=9.960, QC=0.1163, FS=36.8, U=59.2, TA=2.65, B=15, %156312750  
D=9.980, QC=0.1247, FS=37.1, U=59.5, TA=2.66, B=15, %156314281  
D=10.000, QC=0.1454, FS=37.6, U=60.0, TA=2.65, B=15, %156315375  
D=10.020, QC=0.3028, FS=37.2, U=58.3, TA=2.64, B=15, %156316906  
D=10.040, QC=0.4332, FS=38.0, U=58.3, TA=2.65, B=15, %156318031  
D=10.060, QC=0.5890, FS=40.9, U=60.9, TA=2.66, B=14, %156319468  
D=10.080, QC=0.5636, FS=43.7, U=61.1, TA=2.66, B=14, %156320671  
D=10.100, QC=0.4119, FS=42.6, U=58.5, TA=2.64, B=15, %156322109  
D=10.120, QC=0.2581, FS=44.9, U=60.5, TA=2.66, B=15, %156323203  
D=10.140, QC=0.2327, FS=40.8, U=60.5, TA=2.66, B=14, %156324734  
D=10.160, QC=0.1673, FS=41.7, U=58.4, TA=2.67, B=14, %156326296  
D=10.180, QC=0.1698, FS=38.9, U=60.8, TA=2.65, B=14, %156327421  
D=10.200, QC=0.4467, FS=42.2, U=62.3, TA=2.71, B=22, %156368187  
D=10.220, QC=0.4467, FS=42.2, U=62.3, TA=2.71, B=22, %156368187  
D=10.240, QC=0.4872, FS=42.9, U=61.8, TA=2.69, B=23, %156368968  
D=10.260, QC=0.4623, FS=44.6, U=64.0, TA=2.70, B=24, %156369750  
D=10.280, QC=0.3496, FS=44.9, U=61.8, TA=2.71, B=22, %156370437  
D=10.300, QC=0.2228, FS=43.9, U=62.1, TA=2.68, B=23, %156371640  
D=10.320, QC=0.1787, FS=42.1, U=62.3, TA=2.70, B=23, %156372343  
D=10.340, QC=0.1506, FS=41.6, U=64.5, TA=2.69, B=25, %156373109  
D=10.360, QC=0.1428, FS=40.0, U=62.4, TA=2.68, B=23, %156373875  
D=10.380, QC=0.1517, FS=38.9, U=62.8, TA=2.69, B=22, %156374984  
D=10.400, QC=0.1953, FS=38.4, U=63.0, TA=2.68, B=23, %156375765  
D=10.420, QC=0.2987, FS=38.4, U=63.1, TA=2.67, B=24, %156376421  
D=10.440, QC=0.2872, FS=38.9, U=65.2, TA=2.73, B=23, %156377656  
D=10.460, QC=0.2197, FS=40.4, U=65.4, TA=2.68, B=22, %156378421  
D=10.480, QC=0.1641, FS=41.1, U=63.2, TA=2.67, B=22, %156379093  
D=10.500, QC=0.1511, FS=39.7, U=65.5, TA=2.70, B=25, %156379875  
D=10.520, QC=0.1532, FS=38.5, U=65.6, TA=2.70, B=23, %156380984  
D=10.540, QC=0.1517, FS=38.0, U=65.8, TA=2.69, B=23, %156381750  
D=10.560, QC=0.1626, FS=37.7, U=63.8, TA=2.67, B=24, %156382421  
D=10.580, QC=0.1693, FS=36.9, U=66.1, TA=2.69, B=25, %156383203  
D=10.600, QC=0.1605, FS=36.0, U=66.3, TA=2.74, B=23, %156383984  
D=10.620, QC=0.3075, FS=39.0, U=64.2, TA=2.76, B=24, %156385109  
D=10.640, QC=0.5329, FS=41.5, U=63.5, TA=2.77, B=24, %156385890  
D=10.660, QC=0.6939, FS=44.6, U=65.5, TA=2.75, B=25, %156386546  
D=10.680, QC=0.4041, FS=44.0, U=64.1, TA=2.77, B=25, %156387328  
D=10.700, QC=0.2872, FS=44.5, U=64.6, TA=2.75, B=24, %156388093  
D=10.720, QC=0.4690, FS=43.7, U=66.9, TA=2.76, B=24, %156388859  
D=10.740, QC=0.6716, FS=47.4, U=67.5, TA=2.77, B=25, %156389640  
D=10.760, QC=0.8674, FS=63.6, U=69.6, TA=2.73, B=24, %156390296  
D=10.780, QC=0.8726, FS=55.6, U=70.3, TA=2.72, B=23, %156391500  
D=10.800, QC=0.6841, FS=47.4, U=67.8, TA=2.74, B=24, %156392171  
D=10.820, QC=0.4197, FS=51.9, U=67.9, TA=2.76, B=25, %156392953  
D=10.840, QC=0.2774, FS=45.4, U=65.6, TA=2.75, B=25, %156393734

D=10.860, QC=0.2592, FS=44.9, U=65.6, TA=2.73, B=24, %156394500  
D=10.880, QC=0.2649, FS=44.8, U=65.8, TA=2.75, B=24, %156395171  
D=10.900, QC=0.3345, FS=45.0, U=65.9, TA=2.74, B=24, %156395937  
D=10.920, QC=0.3781, FS=45.5, U=68.1, TA=2.75, B=24, %156397140  
D=10.940, QC=0.5199, FS=45.5, U=66.0, TA=2.74, B=24, %156397796  
D=10.960, QC=0.7381, FS=45.2, U=65.9, TA=2.73, B=25, %156398578  
D=10.980, QC=0.8534, FS=56.7, U=69.0, TA=2.72, B=24, %156399343  
D=11.000, QC=0.8539, FS=61.6, U=69.6, TA=2.72, B=23, %156400125  
D=11.020, QC=0.8659, FS=73.3, U=68.6, TA=2.73, B=23, %156400796  
D=11.040, QC=0.9095, FS=88.0, U=70.5, TA=2.72, B=24, %156402000  
D=11.060, QC=0.9251, FS=101.8, U=71.1, TA=2.71, B=24, %156402671  
D=11.080, QC=0.9786, FS=125.2, U=75.2, TA=2.72, B=23, %156403453  
D=11.100, QC=1.1173, FS=150.5, U=76.8, TA=2.72, B=22, %156404218  
D=11.120, QC=1.3993, FS=173.6, U=77.0, TA=2.75, B=22, %156405328  
D=11.140, QC=1.3640, FS=186.0, U=79.5, TA=2.76, B=22, %156406093  
D=11.160, QC=1.1998, FS=185.3, U=80.4, TA=2.77, B=21, %156406859  
D=11.180, QC=1.0923, FS=172.8, U=76.1, TA=2.76, B=21, %156407953  
D=11.200, QC=1.0809, FS=180.7, U=77.5, TA=2.79, B=22, %156408750  
D=11.220, QC=1.1780, FS=195.1, U=76.3, TA=2.80, B=22, %156409859  
D=11.240, QC=1.2881, FS=210.2, U=78.1, TA=2.80, B=21, %156410578  
D=11.260, QC=1.3354, FS=213.5, U=81.4, TA=2.80, B=20, %156411671  
D=11.280, QC=1.3136, FS=209.9, U=77.3, TA=2.78, B=20, %156412453  
D=11.300, QC=1.3905, FS=206.6, U=76.2, TA=2.84, B=21, %156413546  
D=11.320, QC=1.3853, FS=202.7, U=76.8, TA=2.84, B=23, %156414328  
D=11.340, QC=1.5499, FS=193.5, U=75.0, TA=2.84, B=23, %156415109  
D=11.360, QC=1.4964, FS=174.9, U=72.4, TA=2.84, B=25, %156415890  
D=11.380, QC=1.1936, FS=116.1, U=77.2, TA=2.78, B=26, %156467890  
D=11.400, QC=1.1936, FS=116.1, U=77.2, TA=2.78, B=26, %156467890  
D=11.420, QC=1.1936, FS=116.1, U=77.2, TA=2.78, B=26, %156467890  
D=11.440, QC=0.9988, FS=116.1, U=77.2, TA=2.78, B=27, %156468343  
D=11.460, QC=0.9516, FS=100.3, U=78.5, TA=2.78, B=26, %156469046  
D=11.480, QC=0.8420, FS=86.8, U=75.1, TA=2.78, B=26, %156469812  
D=11.500, QC=0.8150, FS=68.6, U=75.4, TA=2.78, B=26, %156470578  
D=11.520, QC=0.7963, FS=51.8, U=73.0, TA=2.78, B=27, %156471234  
D=11.540, QC=0.7667, FS=43.3, U=71.3, TA=2.78, B=26, %156472015  
D=11.560, QC=0.7007, FS=36.9, U=69.6, TA=2.78, B=28, %156472781  
D=11.580, QC=0.5994, FS=33.5, U=68.9, TA=2.78, B=27, %156473562  
D=11.600, QC=0.5584, FS=32.7, U=68.6, TA=2.78, B=27, %156474328  
D=11.620, QC=0.6098, FS=35.5, U=66.4, TA=2.78, B=18, %156475453  
D=11.640, QC=0.8243, FS=40.3, U=68.8, TA=2.78, B=16, %156476546  
D=11.660, QC=0.8279, FS=57.0, U=72.4, TA=2.78, B=18, %156477640  
D=11.680, QC=0.7448, FS=39.1, U=70.5, TA=2.78, B=18, %156478765  
D=11.700, QC=0.5817, FS=28.3, U=68.8, TA=2.78, B=18, %156479890  
D=11.720, QC=0.4493, FS=28.2, U=68.6, TA=2.79, B=20, %156480671  
D=11.740, QC=0.3579, FS=27.6, U=68.6, TA=2.80, B=19, %156481781  
D=11.760, QC=0.3387, FS=25.9, U=68.7, TA=2.80, B=20, %156482875  
D=11.780, QC=0.3257, FS=26.5, U=68.8, TA=2.83, B=18, %156484078  
D=11.800, QC=0.3184, FS=27.0, U=68.8, TA=2.83, B=20, %156484750  
D=11.820, QC=0.3153, FS=28.2, U=69.0, TA=2.85, B=19, %156485859  
D=11.840, QC=0.3106, FS=28.1, U=69.1, TA=2.87, B=21, %156487078

D=11.860, QC=0.3023, FS=27.8, U=69.3, TA=2.87, B=19, %156487843  
D=11.880, QC=0.2981, FS=28.8, U=69.5, TA=2.88, B=20, %156488953  
D=11.900, QC=0.2950, FS=29.0, U=69.6, TA=2.89, B=20, %156489609  
D=11.920, QC=0.2883, FS=29.5, U=69.8, TA=2.93, B=21, %156490750  
D=11.940, QC=0.2929, FS=30.6, U=70.0, TA=2.95, B=20, %156491859  
D=11.960, QC=0.2981, FS=30.7, U=70.2, TA=2.95, B=20, %156492625  
D=11.980, QC=0.2966, FS=31.2, U=70.4, TA=2.96, B=19, %156493750  
D=12.000, QC=0.2981, FS=31.5, U=70.5, TA=2.96, B=20, %156494515  
D=12.020, QC=0.2992, FS=31.8, U=70.8, TA=2.96, B=19, %156495718  
D=12.040, QC=0.2950, FS=31.5, U=70.9, TA=2.96, B=19, %156496734  
D=12.060, QC=0.2909, FS=31.2, U=71.1, TA=2.96, B=18, %156497937  
D=12.080, QC=0.2914, FS=31.2, U=71.4, TA=2.96, B=21, %156498609  
D=12.100, QC=0.2898, FS=31.2, U=71.5, TA=2.96, B=19, %156499843  
D=12.120, QC=0.2945, FS=31.2, U=71.8, TA=2.97, B=19, %156500953  
D=12.140, QC=0.3059, FS=31.4, U=71.9, TA=2.96, B=18, %156502046  
D=12.160, QC=0.3163, FS=31.6, U=72.1, TA=2.97, B=19, %156502812  
D=12.180, QC=0.3475, FS=31.9, U=72.4, TA=2.97, B=17, %156503921  
D=12.200, QC=0.3823, FS=32.0, U=72.6, TA=2.97, B=17, %156505062  
D=12.220, QC=0.3714, FS=32.4, U=73.0, TA=2.97, B=16, %156506515  
D=12.240, QC=0.3485, FS=33.7, U=73.2, TA=2.96, B=17, %156507609  
D=12.260, QC=0.3620, FS=34.5, U=73.3, TA=2.97, B=16, %156508812  
D=12.280, QC=0.3849, FS=35.1, U=73.8, TA=2.95, B=16, %156509953  
D=12.300, QC=0.3257, FS=34.7, U=73.8, TA=2.96, B=16, %156511078  
D=12.320, QC=0.3298, FS=34.3, U=74.1, TA=2.94, B=17, %156512203  
D=12.340, QC=0.3319, FS=34.3, U=74.3, TA=2.95, B=17, %156513343  
D=12.360, QC=0.3278, FS=33.2, U=74.6, TA=2.95, B=18, %156514437  
D=12.380, QC=0.3215, FS=32.6, U=74.7, TA=2.96, B=18, %156515546  
D=12.400, QC=0.3200, FS=33.2, U=75.0, TA=2.96, B=19, %156516640  
D=12.420, QC=0.3189, FS=33.4, U=75.1, TA=2.95, B=17, %156517750  
D=12.440, QC=0.3174, FS=33.3, U=75.4, TA=2.94, B=19, %156518859  
D=12.460, QC=0.3075, FS=33.6, U=75.6, TA=2.94, B=18, %156520078  
D=12.480, QC=0.3033, FS=33.4, U=75.9, TA=2.94, B=17, %156521171  
D=12.500, QC=0.3049, FS=33.4, U=76.0, TA=2.92, B=17, %156522265  
D=12.520, QC=0.3059, FS=33.2, U=76.3, TA=2.92, B=18, %156523375  
D=12.540, QC=0.2924, FS=33.1, U=76.5, TA=2.90, B=18, %156524515  
D=12.560, QC=0.2919, FS=32.6, U=76.7, TA=2.89, B=18, %156525625  
D=12.580, QC=0.2966, FS=32.6, U=76.9, TA=2.89, B=18, %156526734  
D=12.600, QC=0.3007, FS=32.6, U=77.1, TA=2.89, B=18, %156527937, NA=-0.2660, NB=23.9, NC=3.2  
, F=15, K=90, T=The test are ended without any stop in the ground.

#\$

0:

1:

2:

3:

4:

5:

6:

7:

8:

9:

11:Tilt derivative alarm  
12:Point resistance alarm  
13:Depth unchanged for 5 second  
14:Transmission lost  
15:End of test  
16:Dissipation start

**CPT -10**  
**Raw Data**



\$

HA=1,HB=4,HC=CPTLOG-2.00,HD=8/19/2020,HG=-0.640,HP=-0.64,HJ=Brenton  
CPT,HK=c10,HM=07,HN=3206,HO=0.00,HQ=SA,HR=0°0'0.000"E,HS=0°0'0.000"N,HX=0.00,HY=0.00,  
HZ=0.00,KQ=1468.00,KF=6200.00,KU=2136.00,MA=0.590,MB=0.011,MC=10.0,MD=150.0,ME=c10,  
MF=0.000  
RN=,CA=0,CB=0

#

D=0.000, QC=0.0203, FS=0.6, U=3.1, TA=0.50, B=0, %157858078, NA=5.4071, NB=332.4, NC=435.4  
D=0.020, QC=0.0322, FS=0.5, U=2.6, TA=0.27, B=5, %157859281  
D=0.040, QC=0.0332, FS=0.3, U=2.8, TA=0.55, B=14, %157860703  
D=0.060, QC=0.0338, FS=0.3, U=2.8, TA=0.42, B=17, %157861906  
D=0.080, QC=0.0364, FS=0.3, U=2.9, TA=0.47, B=19, %157863015  
D=0.100, QC=0.0390, FS=0.3, U=3.0, TA=0.48, B=18, %157864140  
D=0.120, QC=0.0431, FS=0.3, U=3.0, TA=0.40, B=20, %157865250  
D=0.140, QC=0.0457, FS=0.3, U=3.1, TA=0.58, B=20, %157866031  
D=0.160, QC=0.0483, FS=0.3, U=3.1, TA=0.56, B=20, %157867125  
D=0.180, QC=0.0514, FS=0.2, U=3.2, TA=0.60, B=19, %157867921  
D=0.200, QC=0.1325, FS=0.1, U=3.2, TA=0.58, B=19, %157869000  
D=0.220, QC=0.1678, FS=0.5, U=3.3, TA=0.60, B=20, %157870125  
D=0.240, QC=0.1605, FS=0.3, U=3.4, TA=0.64, B=21, %157870890  
D=0.260, QC=0.1345, FS=0.3, U=3.4, TA=0.69, B=19, %157872031  
D=0.280, QC=0.1138, FS=0.8, U=3.5, TA=0.59, B=18, %157873171  
D=0.300, QC=0.0815, FS=0.9, U=3.6, TA=0.57, B=18, %157874265  
D=0.320, QC=0.0743, FS=1.1, U=3.6, TA=0.56, B=17, %157875359  
D=0.340, QC=0.0738, FS=0.8, U=3.8, TA=0.57, B=17, %157876562  
D=0.360, QC=0.0722, FS=0.5, U=3.9, TA=0.57, B=16, %157877656  
D=0.380, QC=0.0712, FS=0.4, U=3.9, TA=0.56, B=17, %157878796  
D=0.400, QC=0.0732, FS=0.2, U=4.1, TA=0.58, B=18, %157879906  
D=0.420, QC=0.0722, FS=0.0, U=4.1, TA=0.54, B=18, %157881015  
D=0.440, QC=0.0743, FS=0.4, U=4.3, TA=0.56, B=17, %157882125  
D=0.460, QC=0.0764, FS=0.4, U=4.4, TA=0.58, B=20, %157883250  
D=0.480, QC=0.0779, FS=0.3, U=4.5, TA=0.58, B=20, %157884015  
D=0.500, QC=0.0805, FS=0.2, U=4.6, TA=0.56, B=19, %157885125  
D=0.520, QC=0.0795, FS=0.1, U=4.7, TA=0.54, B=19, %157886250  
D=0.540, QC=0.0795, FS=0.1, U=4.8, TA=0.56, B=19, %157887046  
D=0.560, QC=0.0805, FS=0.1, U=4.9, TA=0.55, B=23, %157888156  
D=0.580, QC=0.0821, FS=0.0, U=5.0, TA=0.56, B=24, %157888828  
D=0.600, QC=0.0831, FS=0.1, U=5.1, TA=0.55, B=24, %157889593  
D=0.620, QC=0.0847, FS=0.2, U=5.2, TA=0.56, B=24, %157890375  
D=0.640, QC=0.0852, FS=0.3, U=5.4, TA=0.54, B=24, %157891484  
D=0.660, QC=0.0867, FS=0.3, U=5.4, TA=0.54, B=25, %157892250  
D=0.680, QC=0.0888, FS=0.4, U=5.6, TA=0.54, B=23, %157893015  
D=0.700, QC=0.0909, FS=0.4, U=5.6, TA=0.54, B=23, %157893812  
D=0.720, QC=0.0919, FS=0.4, U=5.8, TA=0.55, B=22, %157894906  
D=0.740, QC=0.0925, FS=0.4, U=5.9, TA=0.54, B=21, %157895671  
D=0.760, QC=0.0935, FS=0.4, U=6.0, TA=0.55, B=21, %157896343  
D=0.780, QC=0.1028, FS=0.4, U=6.1, TA=0.57, B=22, %157897546  
D=0.800, QC=0.1376, FS=0.3, U=6.2, TA=0.56, B=22, %157898250  
D=0.820, QC=0.1356, FS=0.5, U=6.5, TA=0.56, B=20, %157899375  
D=0.840, QC=0.1236, FS=0.7, U=6.6, TA=0.63, B=17, %157900484

D=0.860, QC=0.1189, FS=1.0, U=6.9, TA=0.67, B=17, %157901609  
D=0.880, QC=0.1054, FS=1.2, U=7.0, TA=0.66, B=15, %157902734 , F=11  
D=0.900, QC=0.1527, FS=0.5, U=8.2, TA=0.92, B=25, %157942281  
D=0.920, QC=0.1537, FS=1.4, U=8.0, TA=0.93, B=13, %157943437  
D=0.940, QC=0.1548, FS=0.6, U=8.0, TA=0.91, B=22, %157945328  
D=0.960, QC=0.1527, FS=0.6, U=8.1, TA=0.94, B=21, %157946000  
D=0.980, QC=0.1491, FS=0.6, U=8.1, TA=0.94, B=22, %157946765  
D=1.000, QC=0.1465, FS=0.1, U=8.2, TA=0.95, B=22, %157947890  
D=1.020, QC=0.1480, FS=0.2, U=8.4, TA=0.91, B=34, %157948687  
D=1.040, QC=0.1460, FS=0.2, U=8.4, TA=0.93, B=28, %157949015  
D=1.060, QC=0.1465, FS=0.1, U=8.4, TA=0.93, B=29, %157949781  
D=1.080, QC=0.1491, FS=0.2, U=8.5, TA=0.90, B=27, %157950562  
D=1.100, QC=0.1522, FS=0.3, U=8.5, TA=0.93, B=29, %157951234  
D=1.120, QC=0.1563, FS=0.7, U=8.5, TA=0.98, B=27, %157952015  
D=1.140, QC=0.1667, FS=0.6, U=8.5, TA=0.90, B=27, %157952812 , F=11  
D=1.160, QC=0.1569, FS=0.7, U=8.6, TA=0.99, B=29, %157953515  
D=1.180, QC=0.1569, FS=0.8, U=8.8, TA=0.99, B=29, %157954281  
D=1.200, QC=0.1569, FS=0.6, U=8.9, TA=0.99, B=27, %157954609  
D=1.220, QC=0.1444, FS=1.0, U=8.9, TA=0.94, B=28, %157955390  
D=1.240, QC=0.1340, FS=0.8, U=9.1, TA=0.92, B=28, %157956187  
D=1.260, QC=0.1319, FS=1.0, U=9.2, TA=0.85, B=29, %157956953  
D=1.280, QC=0.1325, FS=1.1, U=9.2, TA=0.85, B=29, %157957625  
D=1.300, QC=0.1335, FS=1.1, U=7.1, TA=0.84, B=28, %157958406  
D=1.320, QC=0.1330, FS=1.1, U=7.1, TA=0.84, B=29, %157959203  
D=1.340, QC=0.1340, FS=1.1, U=7.1, TA=0.83, B=30, %157959531  
D=1.360, QC=0.1309, FS=1.4, U=7.3, TA=0.84, B=21, %157960640  
D=1.380, QC=0.1319, FS=1.4, U=9.6, TA=0.84, B=19, %157961421  
D=1.400, QC=0.1330, FS=1.4, U=7.5, TA=0.83, B=14, %157962890  
D=1.420, QC=0.1376, FS=1.4, U=7.6, TA=0.82, B=14, %157964421  
D=1.440, QC=0.1408, FS=1.4, U=7.7, TA=0.82, B=14, %157965546  
D=1.460, QC=0.1361, FS=1.5, U=8.0, TA=0.81, B=15, %157967109  
D=1.480, QC=0.1423, FS=1.4, U=5.9, TA=0.81, B=14, %157968109  
D=1.500, QC=0.1382, FS=1.3, U=6.0, TA=0.80, B=14, %157969656  
D=1.520, QC=0.1402, FS=1.3, U=6.1, TA=0.81, B=15, %157970750  
D=1.540, QC=0.1423, FS=1.3, U=6.3, TA=0.80, B=15, %157972328  
D=1.560, QC=0.1444, FS=1.3, U=6.5, TA=0.80, B=14, %157973781  
D=1.580, QC=0.1449, FS=1.3, U=6.6, TA=0.80, B=15, %157974906  
D=1.600, QC=0.1465, FS=1.3, U=6.9, TA=0.80, B=14, %157976375  
D=1.620, QC=0.1486, FS=1.2, U=7.0, TA=0.80, B=15, %157977578  
D=1.640, QC=0.1517, FS=0.9, U=7.2, TA=0.80, B=27, %157978687  
D=1.660, QC=0.1527, FS=0.9, U=7.2, TA=0.80, B=27, %157979375  
D=1.680, QC=0.1548, FS=0.9, U=7.3, TA=0.80, B=27, %157980140  
D=1.700, QC=0.1584, FS=0.9, U=7.3, TA=0.80, B=27, %157980562  
D=1.720, QC=0.1610, FS=0.9, U=7.6, TA=0.80, B=20, %157981671  
D=1.740, QC=0.1735, FS=0.9, U=7.6, TA=0.80, B=22, %157982812  
D=1.760, QC=0.1787, FS=0.9, U=7.8, TA=0.80, B=21, %157983484  
D=1.780, QC=0.1802, FS=0.9, U=7.9, TA=0.80, B=22, %157984281  
D=1.800, QC=0.1865, FS=0.8, U=8.0, TA=0.80, B=21, %157985375  
D=1.820, QC=0.1937, FS=0.6, U=8.2, TA=0.81, B=22, %157986156  
D=1.840, QC=0.2119, FS=0.5, U=8.2, TA=0.82, B=21, %157987250

D=1.860, QC=0.2249, FS=0.3, U=8.3, TA=0.84, B=22, %157988031  
D=1.880, QC=0.2239, FS=0.0, U=8.5, TA=0.83, B=21, %157989156  
D=1.900, QC=0.2119, FS=0.0, U=8.6, TA=0.83, B=22, %157989953  
D=1.920, QC=0.2021, FS=0.2, U=8.7, TA=0.83, B=21, %157990625  
D=1.940, QC=0.1839, FS=0.3, U=8.7, TA=0.85, B=22, %157991765  
D=1.960, QC=0.1802, FS=0.4, U=8.9, TA=0.86, B=22, %157992531  
D=1.980, QC=0.1776, FS=0.3, U=9.0, TA=0.84, B=22, %157993625  
D=2.000, QC=0.1766, FS=0.4, U=9.2, TA=0.87, B=22, %157994421  
D=2.020, QC=0.1704, FS=0.2, U=10.2, TA=0.80, B=22, %158035062  
D=2.040, QC=0.1704, FS=0.2, U=10.2, TA=0.80, B=22, %158035062  
D=2.060, QC=0.1771, FS=0.5, U=9.9, TA=0.81, B=21, %158035843  
D=2.080, QC=0.1782, FS=0.6, U=9.9, TA=0.81, B=21, %158036625  
D=2.100, QC=0.1756, FS=0.7, U=9.9, TA=0.81, B=20, %158037718  
D=2.120, QC=0.1745, FS=0.8, U=9.9, TA=0.83, B=20, %158038531  
D=2.140, QC=0.1750, FS=0.6, U=10.0, TA=0.81, B=22, %158039609  
D=2.160, QC=0.1724, FS=0.7, U=10.1, TA=0.84, B=21, %158040375  
D=2.180, QC=0.1750, FS=0.6, U=10.1, TA=0.83, B=21, %158041515  
D=2.200, QC=0.1756, FS=0.7, U=10.2, TA=0.83, B=21, %158042187  
D=2.220, QC=0.1766, FS=0.6, U=10.2, TA=0.86, B=21, %158042984  
D=2.240, QC=0.1797, FS=0.6, U=10.4, TA=0.85, B=20, %158044078  
D=2.260, QC=0.1808, FS=0.6, U=10.4, TA=0.85, B=22, %158044843  
D=2.280, QC=0.1839, FS=0.5, U=10.5, TA=0.85, B=21, %158045937  
D=2.300, QC=0.1834, FS=0.6, U=10.5, TA=0.84, B=22, %158046718  
D=2.320, QC=0.1854, FS=0.5, U=10.7, TA=0.87, B=21, %158047859  
D=2.340, QC=0.1870, FS=0.5, U=10.8, TA=0.83, B=22, %158048640  
D=2.360, QC=0.1911, FS=0.5, U=10.8, TA=0.88, B=22, %158049734  
D=2.380, QC=0.1932, FS=0.5, U=10.9, TA=0.88, B=22, %158050515  
D=2.400, QC=0.1937, FS=0.4, U=11.0, TA=0.85, B=21, %158051203  
D=2.420, QC=0.1963, FS=0.3, U=11.1, TA=0.86, B=21, %158052312  
D=2.440, QC=0.1969, FS=0.1, U=11.2, TA=0.87, B=21, %158053093  
D=2.460, QC=0.1953, FS=0.0, U=11.3, TA=0.87, B=23, %158054250  
D=2.480, QC=0.1974, FS=0.0, U=8.8, TA=0.86, B=22, %158055031  
D=2.500, QC=0.1989, FS=0.1, U=11.5, TA=0.86, B=22, %158055687  
D=2.520, QC=0.1937, FS=0.0, U=9.0, TA=0.84, B=23, %158056812  
D=2.540, QC=0.1932, FS=0.1, U=9.1, TA=0.86, B=24, %158057609  
D=2.560, QC=0.2005, FS=0.2, U=9.2, TA=0.85, B=23, %158058375  
D=2.580, QC=0.1958, FS=0.2, U=9.3, TA=0.84, B=24, %158059140  
D=2.600, QC=0.2010, FS=0.1, U=9.4, TA=0.86, B=22, %158060281  
D=2.620, QC=0.2021, FS=0.2, U=9.5, TA=0.86, B=24, %158060968  
D=2.640, QC=0.2005, FS=0.1, U=9.6, TA=0.85, B=22, %158061750  
D=2.660, QC=0.2000, FS=0.3, U=9.6, TA=0.84, B=24, %158062515  
D=2.680, QC=0.2005, FS=0.5, U=9.8, TA=0.86, B=22, %158063656  
D=2.700, QC=0.1995, FS=0.5, U=9.9, TA=0.86, B=23, %158064312  
D=2.720, QC=0.2067, FS=0.5, U=7.7, TA=0.85, B=24, %158065093  
D=2.740, QC=0.2098, FS=0.5, U=7.8, TA=0.85, B=24, %158065890  
D=2.760, QC=0.2031, FS=0.5, U=7.9, TA=0.85, B=22, %158067000  
D=2.780, QC=0.2031, FS=0.5, U=8.0, TA=0.85, B=23, %158067781  
D=2.800, QC=0.2005, FS=0.3, U=8.0, TA=0.85, B=23, %158068437  
D=2.820, QC=0.1984, FS=0.1, U=8.2, TA=0.85, B=23, %158069562  
D=2.840, QC=0.1979, FS=0.2, U=8.2, TA=0.85, B=22, %158070343

D=2.860, QC=0.1979, FS=0.2, U=8.4, TA=0.85, B=23, %158071109  
D=2.880, QC=0.1984, FS=0.1, U=8.4, TA=0.85, B=23, %158071890  
D=2.900, QC=0.2031, FS=0.1, U=8.5, TA=0.85, B=23, %158072984  
D=2.920, QC=0.2031, FS=0.1, U=8.6, TA=0.85, B=22, %158073765  
D=2.940, QC=0.2057, FS=0.1, U=8.7, TA=0.85, B=23, %158074468  
D=2.960, QC=0.2083, FS=0.1, U=8.8, TA=0.85, B=23, %158075265  
D=2.980, QC=0.2114, FS=0.3, U=9.0, TA=0.85, B=22, %158076390  
D=3.000, QC=0.2145, FS=0.3, U=9.0, TA=0.85, B=22, %158077062  
D=3.020, QC=0.2161, FS=0.5, U=9.1, TA=0.85, B=23, %158077828  
D=3.040, QC=0.2208, FS=0.5, U=9.2, TA=0.85, B=22, %158079046  
D=3.060, QC=0.2218, FS=0.3, U=9.3, TA=0.85, B=23, %158079703  
D=3.080, QC=0.2249, FS=0.2, U=9.4, TA=0.85, B=22, %158080468  
D=3.100, QC=0.2228, FS=0.2, U=9.6, TA=0.85, B=23, %158081671  
D=3.120, QC=0.2228, FS=0.4, U=9.7, TA=0.85, B=21, %158082328  
D=3.140, QC=0.2233, FS=0.5, U=9.7, TA=0.85, B=21, %158083531  
D=3.160, QC=0.2265, FS=0.6, U=9.9, TA=0.85, B=21, %158084187  
D=3.180, QC=0.2343, FS=0.7, U=9.9, TA=0.85, B=22, %158084968  
D=3.200, QC=0.2384, FS=0.7, U=10.1, TA=0.85, B=21, %158086125  
D=3.220, QC=0.2633, FS=1.7, U=12.2, TA=0.81, B=25, %158124125  
D=3.240, QC=0.2633, FS=1.7, U=12.2, TA=0.81, B=25, %158124125  
D=3.260, QC=0.2633, FS=1.7, U=12.2, TA=0.81, B=25, %158124125  
D=3.280, QC=0.2597, FS=1.7, U=12.2, TA=0.85, B=23, %158124578  
D=3.300, QC=0.2556, FS=1.8, U=11.9, TA=0.85, B=23, %158125687  
D=3.320, QC=0.2535, FS=2.0, U=11.9, TA=0.85, B=22, %158126468  
D=3.340, QC=0.2602, FS=2.2, U=11.9, TA=0.85, B=18, %158127562  
D=3.360, QC=0.2628, FS=2.6, U=11.9, TA=0.85, B=21, %158128671  
D=3.380, QC=0.2550, FS=2.6, U=12.0, TA=0.85, B=21, %158129437  
D=3.400, QC=0.2509, FS=2.4, U=12.0, TA=0.85, B=21, %158130218  
D=3.420, QC=0.2457, FS=2.4, U=12.0, TA=0.85, B=20, %158131250  
D=3.440, QC=0.2374, FS=2.5, U=12.1, TA=0.85, B=23, %158132046  
D=3.460, QC=0.2327, FS=2.0, U=12.2, TA=0.85, B=22, %158133156  
D=3.480, QC=0.2343, FS=1.7, U=12.2, TA=0.85, B=23, %158133921  
D=3.500, QC=0.2337, FS=1.6, U=12.3, TA=0.85, B=22, %158134687  
D=3.520, QC=0.2363, FS=1.4, U=12.4, TA=0.85, B=39, %158135484  
D=3.540, QC=0.2446, FS=1.4, U=12.4, TA=0.85, B=24, %158136593  
D=3.560, QC=0.2504, FS=1.1, U=12.5, TA=0.85, B=25, %158137265  
D=3.580, QC=0.2571, FS=0.9, U=12.6, TA=0.85, B=23, %158138031  
D=3.600, QC=0.2628, FS=0.8, U=12.6, TA=0.85, B=24, %158138812  
D=3.620, QC=0.2602, FS=0.8, U=12.6, TA=0.85, B=23, %158139515  
D=3.640, QC=0.2488, FS=1.0, U=12.7, TA=0.83, B=25, %158140625  
D=3.660, QC=0.2431, FS=1.1, U=12.8, TA=0.83, B=24, %158141390  
D=3.680, QC=0.2400, FS=1.3, U=12.8, TA=0.81, B=24, %158142156  
D=3.700, QC=0.2374, FS=1.4, U=12.9, TA=0.82, B=23, %158142921  
D=3.720, QC=0.2343, FS=1.8, U=13.0, TA=0.78, B=26, %158143718  
D=3.740, QC=0.2343, FS=1.8, U=10.8, TA=0.78, B=25, %158144390  
D=3.760, QC=0.2363, FS=1.9, U=13.1, TA=0.77, B=26, %158145171  
D=3.780, QC=0.2317, FS=1.9, U=11.0, TA=0.77, B=25, %158145953  
D=3.800, QC=0.2332, FS=1.8, U=13.3, TA=0.77, B=26, %158147078  
D=3.820, QC=0.2343, FS=1.8, U=11.1, TA=0.76, B=26, %158147859  
D=3.840, QC=0.2415, FS=1.8, U=11.1, TA=0.74, B=24, %158148515

D=3.860, QC=0.2472, FS=1.6, U=11.2, TA=0.74, B=24, %158149296  
D=3.880, QC=0.2488, FS=1.5, U=11.2, TA=0.76, B=27, %158150093  
D=3.900, QC=0.2592, FS=1.4, U=11.3, TA=0.73, B=25, %158150781  
D=3.920, QC=0.2696, FS=1.4, U=11.3, TA=0.75, B=25, %158151546  
D=3.940, QC=0.2727, FS=1.5, U=11.4, TA=0.74, B=24, %158152312  
D=3.960, QC=0.2955, FS=1.8, U=11.5, TA=0.73, B=25, %158153078  
D=3.980, QC=0.2784, FS=1.8, U=11.5, TA=0.73, B=25, %158153859  
D=4.000, QC=0.2872, FS=2.4, U=11.5, TA=0.73, B=25, %158154515  
D=4.020, QC=0.2696, FS=3.2, U=11.7, TA=0.73, B=25, %158155281  
D=4.040, QC=0.2722, FS=3.5, U=11.8, TA=0.73, B=25, %158156421  
D=4.060, QC=0.2831, FS=4.0, U=11.9, TA=0.73, B=25, %158157187  
D=4.080, QC=0.3163, FS=4.6, U=12.0, TA=0.73, B=24, %158157953  
D=4.100, QC=0.3407, FS=4.9, U=12.1, TA=0.73, B=25, %158158718  
D=4.120, QC=0.3226, FS=4.9, U=12.1, TA=0.73, B=24, %158159390  
D=4.140, QC=0.3091, FS=4.1, U=12.1, TA=0.73, B=24, %158160156  
D=4.160, QC=0.2789, FS=4.3, U=12.2, TA=0.74, B=26, %158160953  
D=4.180, QC=0.2805, FS=4.3, U=12.3, TA=0.73, B=24, %158161718  
D=4.200, QC=0.2810, FS=4.1, U=12.3, TA=0.73, B=24, %158162812  
D=4.220, QC=0.2665, FS=4.0, U=12.4, TA=0.73, B=24, %158163593  
D=4.240, QC=0.2618, FS=4.1, U=12.5, TA=0.73, B=24, %158164250  
D=4.260, QC=0.2509, FS=4.3, U=12.6, TA=0.73, B=24, %158165046  
D=4.280, QC=0.2462, FS=4.5, U=12.6, TA=0.73, B=24, %158165828  
D=4.300, QC=0.2467, FS=3.2, U=12.7, TA=0.74, B=24, %158166906  
D=4.320, QC=0.2472, FS=2.8, U=12.8, TA=0.74, B=23, %158167671  
D=4.340, QC=0.2493, FS=2.5, U=12.9, TA=0.75, B=23, %158168453  
D=4.360, QC=0.2509, FS=2.1, U=13.0, TA=0.76, B=24, %158169234  
D=4.380, QC=0.2504, FS=1.9, U=13.0, TA=0.75, B=23, %158169906  
D=4.400, QC=0.2452, FS=1.6, U=13.1, TA=0.77, B=22, %158171000  
D=4.420, QC=0.2472, FS=2.9, U=12.2, TA=0.72, B=27, %158211781  
D=4.440, QC=0.2472, FS=2.9, U=12.2, TA=0.72, B=27, %158211781  
D=4.460, QC=0.2472, FS=2.9, U=12.2, TA=0.72, B=27, %158211781  
D=4.480, QC=0.2633, FS=2.9, U=12.2, TA=0.73, B=25, %158212109  
D=4.500, QC=0.2706, FS=2.2, U=11.8, TA=0.58, B=27, %158212875  
D=4.520, QC=0.2696, FS=1.8, U=11.8, TA=0.40, B=26, %158213656  
D=4.540, QC=0.2706, FS=2.6, U=11.9, TA=0.40, B=24, %158214437  
D=4.560, QC=0.2665, FS=2.6, U=11.9, TA=0.40, B=26, %158215093  
D=4.580, QC=0.2680, FS=2.7, U=11.9, TA=0.39, B=25, %158215875  
D=4.600, QC=0.2774, FS=2.7, U=11.9, TA=0.40, B=26, %158216640  
D=4.620, QC=0.2784, FS=2.8, U=12.0, TA=0.40, B=26, %158217734  
D=4.640, QC=0.2706, FS=2.9, U=12.0, TA=0.40, B=25, %158218515  
D=4.660, QC=0.2613, FS=2.9, U=12.0, TA=0.40, B=26, %158219296  
D=4.680, QC=0.2581, FS=2.7, U=12.1, TA=0.40, B=24, %158220062  
D=4.700, QC=0.2633, FS=2.5, U=12.1, TA=0.39, B=26, %158220843  
D=4.720, QC=0.2763, FS=2.5, U=12.2, TA=0.40, B=25, %158221515  
D=4.740, QC=0.2883, FS=2.6, U=12.2, TA=0.40, B=26, %158222281  
D=4.760, QC=0.2846, FS=2.7, U=12.2, TA=0.41, B=26, %158223062  
D=4.780, QC=0.2774, FS=2.6, U=12.3, TA=0.40, B=24, %158223734  
D=4.800, QC=0.2644, FS=2.7, U=12.3, TA=0.41, B=25, %158224531  
D=4.820, QC=0.2581, FS=3.0, U=12.4, TA=0.40, B=25, %158225312  
D=4.840, QC=0.2530, FS=3.0, U=12.5, TA=0.40, B=28, %158225984

D=4.860, QC=0.2504, FS=2.9, U=12.5, TA=0.41, B=26, %158226750  
D=4.880, QC=0.2509, FS=2.6, U=12.6, TA=0.41, B=26, %158227531  
D=4.900, QC=0.2509, FS=2.4, U=12.6, TA=0.42, B=27, %158228296  
D=4.920, QC=0.2483, FS=1.9, U=12.6, TA=0.42, B=27, %158228984  
D=4.940, QC=0.2488, FS=1.6, U=12.7, TA=0.42, B=28, %158229781  
D=4.960, QC=0.2483, FS=1.4, U=12.7, TA=0.42, B=26, %158230546  
D=4.980, QC=0.2467, FS=1.3, U=12.7, TA=0.42, B=27, %158231234  
D=5.000, QC=0.2488, FS=1.4, U=12.8, TA=0.42, B=27, %158232000  
D=5.020, QC=0.2493, FS=1.5, U=12.9, TA=0.42, B=28, %158232765  
D=5.040, QC=0.2524, FS=1.5, U=12.9, TA=0.42, B=27, %158233531  
D=5.060, QC=0.2613, FS=1.6, U=13.0, TA=0.42, B=28, %158234296  
D=5.080, QC=0.2732, FS=1.6, U=13.0, TA=0.41, B=29, %158234625  
D=5.100, QC=0.2748, FS=1.6, U=13.0, TA=0.42, B=28, %158235406  
D=5.120, QC=0.2711, FS=1.6, U=13.0, TA=0.42, B=27, %158236187  
D=5.140, QC=0.2706, FS=1.4, U=13.1, TA=0.41, B=27, %158236859  
D=5.160, QC=0.2732, FS=1.4, U=13.2, TA=0.42, B=28, %158237625  
D=5.180, QC=0.2675, FS=1.7, U=13.2, TA=0.41, B=29, %158238390  
D=5.200, QC=0.2639, FS=1.9, U=13.3, TA=0.42, B=27, %158239171  
D=5.220, QC=0.2654, FS=2.0, U=13.3, TA=0.42, B=27, %158239859  
D=5.240, QC=0.2654, FS=2.3, U=13.4, TA=0.41, B=28, %158240625  
D=5.260, QC=0.2644, FS=2.4, U=13.4, TA=0.43, B=29, %158241406  
D=5.280, QC=0.2665, FS=2.4, U=13.4, TA=0.42, B=26, %158242171  
D=5.300, QC=0.2659, FS=2.2, U=13.5, TA=0.42, B=27, %158242859  
D=5.320, QC=0.2659, FS=2.1, U=13.5, TA=0.42, B=28, %158243296  
D=5.340, QC=0.2691, FS=1.9, U=13.7, TA=0.42, B=27, %158244062  
D=5.360, QC=0.2717, FS=2.0, U=13.7, TA=0.42, B=27, %158244734  
D=5.380, QC=0.2800, FS=2.3, U=13.7, TA=0.42, B=26, %158245515  
D=5.400, QC=0.2815, FS=2.4, U=13.8, TA=0.42, B=27, %158246281  
D=5.420, QC=0.2820, FS=2.5, U=13.9, TA=0.42, B=27, %158246968  
D=5.440, QC=0.2852, FS=2.6, U=13.9, TA=0.43, B=26, %158247734  
D=5.460, QC=0.2867, FS=2.7, U=14.0, TA=0.43, B=26, %158248531  
D=5.480, QC=0.2898, FS=2.6, U=14.0, TA=0.42, B=26, %158249296  
D=5.500, QC=0.2935, FS=2.9, U=14.0, TA=0.42, B=26, %158249968  
D=5.520, QC=0.2935, FS=3.2, U=14.1, TA=0.46, B=25, %158250750  
D=5.540, QC=0.2940, FS=3.5, U=14.2, TA=0.45, B=26, %158251515  
D=5.560, QC=0.2971, FS=3.6, U=14.2, TA=0.43, B=27, %158252281  
D=5.580, QC=0.3007, FS=2.6, U=14.2, TA=0.49, B=26, %158253046  
D=5.600, QC=0.2961, FS=4.3, U=17.1, TA=0.38, B=25, %158288187  
D=5.620, QC=0.2961, FS=4.3, U=17.1, TA=0.38, B=25, %158288187  
D=5.640, QC=0.3028, FS=4.2, U=16.8, TA=0.42, B=25, %158288968  
D=5.660, QC=0.3023, FS=4.1, U=16.7, TA=0.43, B=26, %158289734  
D=5.680, QC=0.3033, FS=4.1, U=16.7, TA=0.45, B=26, %158290500  
D=5.700, QC=0.3132, FS=4.3, U=16.7, TA=0.48, B=25, %158291281  
D=5.720, QC=0.3205, FS=4.3, U=16.8, TA=0.48, B=25, %158292046  
D=5.740, QC=0.3116, FS=4.2, U=16.8, TA=0.49, B=24, %158292734  
D=5.760, QC=0.3044, FS=3.9, U=16.8, TA=0.51, B=26, %158293515  
D=5.780, QC=0.3007, FS=3.9, U=16.8, TA=0.48, B=25, %158294187  
D=5.800, QC=0.2997, FS=3.8, U=16.8, TA=0.50, B=25, %158294953  
D=5.820, QC=0.3049, FS=3.8, U=16.9, TA=0.51, B=25, %158296171  
D=5.840, QC=0.3054, FS=3.8, U=16.9, TA=0.50, B=24, %158296828

D=5.860, QC=0.3189, FS=3.8, U=17.0, TA=0.50, B=25, %158297593  
D=5.880, QC=0.3527, FS=4.0, U=17.0, TA=0.50, B=24, %158298359  
D=5.900, QC=0.3672, FS=4.1, U=17.0, TA=0.49, B=24, %158299156  
D=5.920, QC=0.3636, FS=3.7, U=17.1, TA=0.50, B=24, %158299828  
D=5.940, QC=0.3657, FS=3.4, U=17.1, TA=0.51, B=25, %158300625  
D=5.960, QC=0.3911, FS=3.4, U=17.1, TA=0.50, B=26, %158301390  
D=5.980, QC=0.3688, FS=3.2, U=17.1, TA=0.51, B=24, %158302156  
D=6.000, QC=0.3459, FS=2.9, U=17.3, TA=0.50, B=24, %158303281  
D=6.020, QC=0.3220, FS=3.9, U=17.3, TA=0.50, B=26, %158304062  
D=6.040, QC=0.3028, FS=3.7, U=17.3, TA=0.51, B=26, %158304750  
D=6.060, QC=0.3007, FS=3.4, U=17.4, TA=0.50, B=27, %158305515  
D=6.080, QC=0.3002, FS=2.6, U=17.4, TA=0.51, B=26, %158306218  
D=6.100, QC=0.3013, FS=2.7, U=17.5, TA=0.50, B=28, %158307015  
D=6.120, QC=0.3007, FS=2.5, U=17.5, TA=0.51, B=26, %158307687  
D=6.140, QC=0.3054, FS=2.3, U=17.6, TA=0.52, B=27, %158308453  
D=6.160, QC=0.3168, FS=2.0, U=17.6, TA=0.51, B=26, %158309234  
D=6.180, QC=0.3278, FS=2.4, U=15.4, TA=0.51, B=27, %158310046  
D=6.200, QC=0.3241, FS=2.6, U=17.8, TA=0.51, B=27, %158310703  
D=6.220, QC=0.3179, FS=2.7, U=15.5, TA=0.50, B=28, %158311500  
D=6.240, QC=0.3039, FS=2.4, U=17.9, TA=0.50, B=26, %158312296  
D=6.260, QC=0.2976, FS=2.5, U=17.8, TA=0.50, B=27, %158312953  
D=6.280, QC=0.2955, FS=2.5, U=18.0, TA=0.50, B=27, %158313718  
D=6.300, QC=0.2909, FS=2.5, U=18.0, TA=0.49, B=27, %158314156  
D=6.320, QC=0.2872, FS=2.4, U=18.0, TA=0.49, B=26, %158314921  
D=6.340, QC=0.3096, FS=2.5, U=18.0, TA=0.49, B=26, %158315593  
D=6.360, QC=0.3615, FS=2.7, U=18.1, TA=0.49, B=27, %158316375  
D=6.380, QC=0.3075, FS=2.6, U=18.3, TA=0.49, B=26, %158317156  
D=6.400, QC=0.3345, FS=2.9, U=18.3, TA=0.49, B=26, %158317812  
D=6.420, QC=0.3142, FS=3.1, U=18.4, TA=0.49, B=26, %158318593  
D=6.440, QC=0.3028, FS=3.3, U=18.4, TA=0.49, B=27, %158319359  
D=6.460, QC=0.3013, FS=3.8, U=16.1, TA=0.49, B=27, %158320140  
D=6.480, QC=0.3444, FS=3.7, U=16.2, TA=0.49, B=26, %158320843  
D=6.500, QC=0.4301, FS=4.2, U=16.2, TA=0.49, B=25, %158321625  
D=6.520, QC=0.5864, FS=5.7, U=16.2, TA=0.49, B=27, %158322390  
D=6.540, QC=0.7412, FS=7.5, U=16.2, TA=0.49, B=26, %158323078  
D=6.560, QC=0.9157, FS=8.6, U=18.5, TA=0.49, B=25, %158323828  
D=6.580, QC=1.0009, FS=11.4, U=16.4, TA=0.49, B=25, %158324968  
D=6.600, QC=0.9884, FS=10.7, U=16.6, TA=0.49, B=25, %158325734  
D=6.620, QC=0.9807, FS=10.6, U=16.7, TA=0.49, B=26, %158326500  
D=6.640, QC=0.9718, FS=11.0, U=19.1, TA=0.49, B=25, %158327265  
D=6.660, QC=0.9775, FS=12.4, U=16.9, TA=0.49, B=24, %158327937  
D=6.680, QC=0.9973, FS=14.4, U=17.0, TA=0.49, B=24, %158328734  
D=6.700, QC=1.0175, FS=15.5, U=17.1, TA=0.49, B=24, %158329500  
D=6.720, QC=1.0243, FS=15.7, U=17.2, TA=0.49, B=24, %158330281  
D=6.740, QC=0.9744, FS=12.9, U=19.6, TA=0.49, B=25, %158331359  
D=6.760, QC=0.9136, FS=6.4, U=17.2, TA=0.49, B=24, %158332156  
D=6.780, QC=0.7474, FS=5.1, U=16.9, TA=0.47, B=24, %158332828  
D=6.800, QC=0.7474, FS=8.1, U=18.7, TA=0.47, B=16, %158369609  
D=6.820, QC=0.7474, FS=8.1, U=18.7, TA=0.47, B=16, %158369609  
D=6.840, QC=0.7345, FS=9.5, U=18.1, TA=0.49, B=20, %158370375

D=6.860, QC=0.6846, FS=8.9, U=18.0, TA=0.49, B=20, %158371156  
D=6.880, QC=0.4872, FS=9.7, U=18.0, TA=0.49, B=21, %158372250  
D=6.900, QC=0.4259, FS=10.1, U=18.0, TA=0.49, B=21, %158373031  
D=6.920, QC=0.4093, FS=6.9, U=18.0, TA=0.49, B=20, %158374156  
D=6.940, QC=0.3953, FS=6.4, U=17.9, TA=0.49, B=20, %158374937  
D=6.960, QC=0.3974, FS=5.5, U=17.9, TA=0.49, B=21, %158376046  
D=6.980, QC=0.4519, FS=4.7, U=18.0, TA=0.49, B=21, %158376828  
D=7.000, QC=0.6534, FS=8.0, U=18.2, TA=0.50, B=20, %158377937  
D=7.020, QC=0.9536, FS=16.1, U=18.1, TA=0.50, B=20, %158378703  
D=7.040, QC=1.0606, FS=24.7, U=16.4, TA=0.49, B=19, %158379781  
D=7.060, QC=1.0897, FS=31.0, U=19.4, TA=0.49, B=20, %158380562  
D=7.080, QC=1.0856, FS=37.5, U=20.0, TA=0.50, B=20, %158381687  
D=7.100, QC=1.0684, FS=35.1, U=20.1, TA=0.49, B=20, %158382812  
D=7.120, QC=1.0793, FS=36.7, U=20.3, TA=0.50, B=20, %158383578  
D=7.140, QC=1.1095, FS=46.9, U=18.1, TA=0.50, B=20, %158384703  
D=7.160, QC=1.1723, FS=51.8, U=20.9, TA=0.49, B=20, %158385812  
D=7.180, QC=1.1723, FS=55.5, U=18.7, TA=0.49, B=19, %158386578  
D=7.200, QC=1.1173, FS=61.0, U=21.7, TA=0.49, B=19, %158387703  
D=7.220, QC=1.0986, FS=60.8, U=21.8, TA=0.49, B=20, %158388828  
D=7.240, QC=1.1100, FS=60.2, U=19.1, TA=0.49, B=21, %158389484  
D=7.260, QC=1.1131, FS=57.5, U=18.7, TA=0.49, B=21, %158390703  
D=7.280, QC=1.1110, FS=55.4, U=18.5, TA=0.49, B=19, %158391406  
D=7.300, QC=1.1297, FS=57.4, U=18.6, TA=0.49, B=22, %158392515  
D=7.320, QC=1.1157, FS=61.4, U=19.0, TA=0.49, B=21, %158393296  
D=7.340, QC=1.1100, FS=65.0, U=19.5, TA=0.49, B=21, %158394421  
D=7.360, QC=1.1027, FS=65.0, U=22.0, TA=0.49, B=20, %158395546  
D=7.380, QC=1.0991, FS=63.2, U=22.0, TA=0.49, B=20, %158396312  
D=7.400, QC=1.1001, FS=56.9, U=22.0, TA=0.49, B=20, %158397421  
D=7.420, QC=1.0949, FS=55.2, U=22.0, TA=0.49, B=20, %158398109  
D=7.440, QC=1.0674, FS=54.2, U=19.5, TA=0.49, B=19, %158399328  
D=7.460, QC=1.0580, FS=52.6, U=19.5, TA=0.49, B=20, %158400453  
D=7.480, QC=1.0586, FS=52.2, U=19.2, TA=0.49, B=21, %158401125  
D=7.500, QC=1.1006, FS=53.4, U=19.1, TA=0.49, B=19, %158402218  
D=7.520, QC=1.1110, FS=54.4, U=21.5, TA=0.49, B=18, %158403375  
D=7.540, QC=1.1038, FS=53.0, U=18.9, TA=0.49, B=19, %158404484  
D=7.560, QC=1.1064, FS=52.1, U=18.6, TA=0.50, B=19, %158405265  
D=7.580, QC=1.1032, FS=52.1, U=19.0, TA=0.49, B=19, %158406390  
D=7.600, QC=1.0975, FS=54.3, U=19.1, TA=0.49, B=18, %158407531  
D=7.620, QC=1.1152, FS=61.0, U=21.9, TA=0.49, B=19, %158408625  
D=7.640, QC=1.1266, FS=62.5, U=19.3, TA=0.50, B=19, %158409406  
D=7.660, QC=1.1339, FS=61.0, U=19.2, TA=0.54, B=19, %158410500  
D=7.680, QC=1.0923, FS=55.9, U=19.6, TA=0.54, B=19, %158411625  
D=7.700, QC=1.0741, FS=59.7, U=22.3, TA=0.53, B=18, %158412406  
D=7.720, QC=1.1074, FS=68.9, U=20.2, TA=0.58, B=19, %158413546  
D=7.740, QC=1.1479, FS=85.0, U=21.1, TA=0.57, B=19, %158414671  
D=7.760, QC=1.2134, FS=90.4, U=21.5, TA=0.59, B=18, %158415765  
D=7.780, QC=1.2772, FS=94.2, U=21.7, TA=0.57, B=18, %158416875  
D=7.800, QC=1.2772, FS=93.6, U=24.2, TA=0.60, B=19, %158417656  
D=7.820, QC=1.2040, FS=91.9, U=24.1, TA=0.61, B=18, %158418781  
D=7.840, QC=1.2700, FS=91.0, U=21.5, TA=0.60, B=18, %158419921



D=7.860, QC=1.3546, FS=95.2, U=21.8, TA=0.61, B=17, %158421015  
D=7.880, QC=1.3027, FS=103.6, U=22.5, TA=0.61, B=17, %158422125  
D=7.900, QC=1.3006, FS=104.3, U=22.2, TA=0.61, B=17, %158423234  
D=7.920, QC=1.3240, FS=106.0, U=22.3, TA=0.61, B=16, %158424437  
D=7.940, QC=1.4216, FS=110.5, U=22.7, TA=0.61, B=17, %158425875  
D=7.960, QC=1.5530, FS=111.7, U=22.7, TA=0.61, B=17, %158427093  
D=7.980, QC=1.4985, FS=111.8, U=22.6, TA=0.61, B=20, %158427765  
D=8.000, QC=1.3874, FS=105.4, U=27.7, TA=0.62, B=25, %158472218  
D=8.020, QC=1.3874, FS=105.4, U=27.7, TA=0.62, B=25, %158472218  
D=8.040, QC=1.3874, FS=105.4, U=27.7, TA=0.62, B=25, %158472218  
D=8.060, QC=1.3458, FS=103.2, U=27.2, TA=0.61, B=23, %158473437  
D=8.080, QC=1.2310, FS=100.3, U=27.3, TA=0.61, B=24, %158474109  
D=8.100, QC=1.0970, FS=96.2, U=27.2, TA=0.61, B=22, %158474875  
D=8.120, QC=1.0591, FS=82.1, U=26.9, TA=0.61, B=24, %158475671  
D=8.140, QC=1.0461, FS=56.0, U=25.4, TA=0.61, B=23, %158476750  
D=8.160, QC=1.0451, FS=54.0, U=24.8, TA=0.61, B=24, %158477531  
D=8.180, QC=1.0705, FS=60.2, U=25.1, TA=0.61, B=23, %158478296  
D=8.200, QC=1.0965, FS=72.9, U=25.4, TA=0.61, B=25, %158478968  
D=8.220, QC=1.2180, FS=86.2, U=25.9, TA=0.61, B=23, %158480078  
D=8.240, QC=1.4076, FS=101.3, U=26.3, TA=0.61, B=23, %158480875  
D=8.260, QC=1.6117, FS=111.5, U=27.2, TA=0.65, B=22, %158481671 , F=11  
D=8.280, QC=1.1770, FS=101.6, U=27.2, TA=0.80, B=22, %158483125  
D=8.300, QC=1.1770, FS=79.3, U=26.6, TA=0.80, B=22, %158483453  
D=8.320, QC=1.0809, FS=59.6, U=26.4, TA=0.83, B=24, %158484234  
D=8.340, QC=1.0404, FS=49.7, U=26.0, TA=0.85, B=23, %158485453  
D=8.360, QC=1.0222, FS=46.4, U=25.6, TA=0.86, B=24, %158486125  
D=8.380, QC=1.4855, FS=41.4, U=25.2, TA=0.77, B=2, %158482781  
D=8.400, QC=1.0113, FS=35.6, U=25.1, TA=0.91, B=24, %158487687  
D=8.420, QC=1.0279, FS=33.2, U=24.8, TA=0.93, B=23, %158488375  
D=8.440, QC=1.0544, FS=33.0, U=24.1, TA=0.96, B=23, %158489531  
D=8.460, QC=1.0529, FS=30.3, U=24.5, TA=0.96, B=24, %158490312  
D=8.480, QC=1.0336, FS=32.1, U=24.1, TA=0.97, B=25, %158490968  
D=8.500, QC=1.0362, FS=33.5, U=24.6, TA=0.98, B=24, %158491765  
D=8.520, QC=1.0253, FS=29.4, U=23.5, TA=0.98, B=25, %158492531  
D=8.540, QC=1.0653, FS=38.0, U=23.8, TA=0.98, B=24, %158493625  
D=8.560, QC=1.1225, FS=49.5, U=24.7, TA=0.98, B=25, %158494406  
D=8.580, QC=1.2445, FS=72.2, U=25.5, TA=0.98, B=23, %158495093  
D=8.600, QC=1.2341, FS=89.6, U=29.1, TA=0.98, B=23, %158495875  
D=8.620, QC=1.1230, FS=82.9, U=27.5, TA=0.98, B=22, %158496640  
D=8.640, QC=1.0487, FS=56.6, U=26.6, TA=0.98, B=23, %158497750  
D=8.660, QC=1.0290, FS=45.6, U=26.0, TA=0.98, B=23, %158498515  
D=8.680, QC=1.0181, FS=33.4, U=25.2, TA=0.98, B=24, %158499312  
D=8.700, QC=1.0591, FS=28.9, U=24.4, TA=0.98, B=23, %158500421  
D=8.720, QC=1.1458, FS=44.2, U=24.9, TA=0.98, B=25, %158501187  
D=8.740, QC=1.0497, FS=48.8, U=28.2, TA=0.98, B=24, %158501843  
D=8.760, QC=1.0035, FS=32.0, U=27.1, TA=0.98, B=24, %158502609  
D=8.780, QC=0.9079, FS=8.9, U=22.6, TA=0.98, B=23, %158503750  
D=8.800, QC=0.7822, FS=6.5, U=21.8, TA=0.98, B=24, %158504531  
D=8.820, QC=0.7506, FS=6.7, U=21.5, TA=0.98, B=24, %158505312  
D=8.840, QC=0.9001, FS=16.0, U=20.6, TA=0.98, B=25, %158505968

D=8.860, QC=1.1141, FS=28.5, U=21.2, TA=0.98, B=23, %158506734  
D=8.880, QC=1.0232, FS=32.0, U=22.4, TA=0.98, B=24, %158507875  
D=8.900, QC=1.0025, FS=30.0, U=23.2, TA=0.98, B=25, %158508656  
D=8.920, QC=0.9568, FS=19.0, U=22.9, TA=0.98, B=24, %158509437  
D=8.940, QC=0.8794, FS=10.3, U=22.5, TA=0.98, B=24, %158510125  
D=8.960, QC=0.7750, FS=6.9, U=22.1, TA=0.98, B=26, %158510890  
D=8.980, QC=0.6789, FS=7.8, U=21.8, TA=0.98, B=25, %158511687  
D=9.000, QC=0.6674, FS=7.3, U=21.6, TA=0.98, B=26, %158512359  
D=9.020, QC=0.8975, FS=7.0, U=21.5, TA=0.98, B=24, %158513109  
D=9.040, QC=1.0773, FS=28.7, U=24.9, TA=0.98, B=24, %158513875  
D=9.060, QC=1.2544, FS=107.4, U=27.9, TA=0.98, B=22, %158514984  
D=9.080, QC=1.4679, FS=103.4, U=27.2, TA=0.98, B=23, %158515765  
D=9.100, QC=1.3297, FS=79.5, U=25.7, TA=0.98, B=22, %158516875  
D=9.120, QC=1.0773, FS=51.6, U=25.1, TA=0.98, B=26, %158517656  
D=9.140, QC=0.9510, FS=28.0, U=24.6, TA=0.98, B=28, %158518406  
D=9.160, QC=0.9510, FS=10.3, U=23.3, TA=0.98, B=29, %158518750  
D=9.180, QC=0.8134, FS=7.3, U=22.1, TA=0.98, B=28, %158519546  
D=9.200, QC=0.7121, FS=8.5, U=22.0, TA=0.98, B=30, %158520203  
D=9.220, QC=0.6306, FS=8.2, U=21.8, TA=0.98, B=28, %158520984  
D=9.240, QC=0.6306, FS=8.4, U=21.8, TA=0.98, B=28, %158521765, NA=0.0961, NB=-6.1, NC=11.4, F  
=15, K=90, T=The test are ended without any stop in the ground.

#\$

0:

1:

2:

3:

4:

5:

6:

7:

8:

9:

11:Tilt derivative alarm

12:Point resistance alarm

13:Depth unchanged for 5 second

14:Transmission lost

15:End of test

16:Dissipation start

**CPT -11**  
**Raw Data**

\$  
HA=1,HB=5,HC=CPTLOG-2.00,HD=8/19/2020,HG=-1.128,HP=-1.13,HJ=Brenton  
CPT,HK=c11,HM=07,HN=3206,HO=0.00,HQ=SA,HR=0°0'0.000"E,HS=0°0'0.000"N,HX=0.00,HY=0.0  
0,HZ=0.00,KQ=1468.00,KF=6200.00,KU=2136.00,MA=0.590,MB=0.011,MC=10.0,MD=150.0,ME=c1  
1,MF=0.000

RN=,CA=0,CB=0

#

D=0.000,QC=0.0753,FS=0.6,U=2.1,TA=1.12,B=10,%160415015,NA=5.4725,NB=331.1,NC=443.7  
D=0.020,QC=0.0893,FS=0.6,U=2.1,TA=1.12,B=10,%160415453  
D=0.040,QC=0.0904,FS=1.2,U=1.7,TA=1.13,B=23,%160416218  
D=0.060,QC=0.0904,FS=0.6,U=1.9,TA=1.14,B=22,%160417343  
D=0.080,QC=0.0914,FS=0.8,U=1.8,TA=1.13,B=16,%160418109  
D=0.100,QC=0.0930,FS=0.6,U=1.9,TA=1.15,B=21,%160419218  
D=0.120,QC=0.0935,FS=0.4,U=2.0,TA=1.14,B=23,%160419890  
D=0.140,QC=0.0935,FS=0.1,U=2.1,TA=1.14,B=21,%160421015  
D=0.160,QC=0.1060,FS=0.2,U=2.2,TA=1.19,B=22,%160421796  
D=0.180,QC=0.1288,FS=0.2,U=2.2,TA=1.15,B=22,%160422562  
D=0.200,QC=0.1735,FS=0.2,U=2.3,TA=1.13,B=23,%160423656  
D=0.220,QC=0.2400,FS=0.7,U=2.3,TA=1.14,B=22,%160424421  
D=0.240,QC=0.3335,FS=1.5,U=2.5,TA=1.13,B=22,%160425203  
D=0.260,QC=0.3501,FS=1.3,U=2.7,TA=1.15,B=22,%160426312  
D=0.280,QC=0.3267,FS=1.0,U=2.7,TA=1.15,B=24,%160427015  
D=0.300,QC=0.2955,FS=1.1,U=2.8,TA=1.15,B=22,%160427781  
D=0.320,QC=0.2394,FS=1.0,U=2.8,TA=1.15,B=21,%160428906  
D=0.340,QC=0.1584,FS=1.2,U=3.0,TA=1.13,B=11,%160430453  
D=0.360,QC=0.1283,FS=1.4,U=0.9,TA=1.10,B=14,%160431921  
D=0.380,QC=0.1361,FS=0.6,U=1.1,TA=1.10,B=15,%160433015  
D=0.400,QC=0.1683,FS=0.8,U=1.2,TA=1.10,B=17,%160434140  
D=0.420,QC=0.2327,FS=2.0,U=1.5,TA=1.10,B=18,%160435343  
D=0.440,QC=0.7142,FS=4.1,U=1.8,TA=1.11,B=19,%160436468  
D=0.460,QC=0.8799,FS=7.8,U=2.2,TA=1.11,B=19,%160437578  
D=0.480,QC=0.9568,FS=9.5,U=2.4,TA=1.11,B=19,%160438359  
D=0.500,QC=0.9427,FS=8.8,U=2.4,TA=1.13,B=19,%160439453  
D=0.520,QC=0.9116,FS=4.2,U=2.4,TA=1.12,B=20,%160440609  
D=0.540,QC=0.7744,FS=3.5,U=0.1,TA=1.12,B=19,%160441750  
D=0.560,QC=0.7048,FS=3.1,U=0.2,TA=1.12,B=20,%160442406  
D=0.580,QC=0.6378,FS=2.7,U=0.4,TA=1.13,B=21,%160443531  
D=0.600,QC=0.5734,FS=2.8,U=0.4,TA=1.12,B=21,%160444328  
D=0.620,QC=0.4644,FS=3.0,U=0.5,TA=1.13,B=20,%160445437  
D=0.640,QC=0.4306,FS=3.0,U=0.6,TA=1.13,B=13,%160446562  
D=0.660,QC=0.3703,FS=3.4,U=0.9,TA=1.13,B=8,%160448812  
D=0.680,QC=0.3496,FS=3.0,U=1.1,TA=1.11,B=17,%160450265  
D=0.700,QC=0.3033,FS=3.6,U=1.2,TA=1.11,B=23,%160451031  
D=0.720,QC=0.3387,FS=5.5,U=1.4,TA=1.11,B=25,%160451796  
D=0.740,QC=0.4903,FS=6.3,U=1.6,TA=1.10,B=24,%160452578  
D=0.760,QC=0.8233,FS=6.3,U=1.9,TA=1.12,B=23,%160453671  
D=0.780,QC=0.9033,FS=11.1,U=2.4,TA=1.11,B=23,%160454484  
D=0.800,QC=0.9666,FS=18.1,U=2.7,TA=1.12,B=24,%160455171  
D=0.820,QC=0.9791,FS=21.9,U=2.8,TA=1.13,B=24,%160455937  
D=0.840,QC=0.9931,FS=35.2,U=3.6,TA=1.13,B=22,%160457078

D=0.860, QC=0.9994, FS=35.2, U=4.0, TA=1.13, B=22, %160457859  
D=0.880, QC=0.9822, FS=31.3, U=4.0, TA=1.13, B=23, %160458515  
D=0.900, QC=0.9739, FS=25.5, U=3.9, TA=1.13, B=23, %160459296  
D=0.920, QC=0.8965, FS=16.8, U=3.7, TA=1.13, B=23, %160460390  
D=0.940, QC=0.8098, FS=5.6, U=3.1, TA=1.13, B=22, %160461156  
D=0.960, QC=0.6498, FS=3.0, U=2.6, TA=1.13, B=23, %160461921  
D=0.980, QC=0.5708, FS=6.1, U=2.9, TA=1.13, B=23, %160463015  
D=1.000, QC=0.6269, FS=7.1, U=3.0, TA=1.13, B=24, %160463796  
D=1.020, QC=0.6238, FS=8.2, U=3.0, TA=1.13, B=22, %160464578  
D=1.040, QC=0.4919, FS=7.5, U=2.9, TA=1.13, B=23, %160465250  
D=1.060, QC=0.3558, FS=7.9, U=3.0, TA=1.13, B=23, %160466468  
D=1.080, QC=0.2987, FS=7.8, U=3.0, TA=1.13, B=24, %160467234  
D=1.100, QC=0.2514, FS=7.8, U=3.1, TA=1.14, B=24, %160467890  
D=1.120, QC=0.2478, FS=7.3, U=3.1, TA=1.13, B=24, %160468671  
D=1.140, QC=0.3070, FS=7.0, U=3.3, TA=1.14, B=24, %160469453  
D=1.160, QC=0.8996, FS=16.7, U=4.2, TA=1.15, B=26, %160510093  
D=1.180, QC=0.8996, FS=16.7, U=4.2, TA=1.15, B=26, %160510093  
D=1.200, QC=0.8996, FS=16.7, U=4.2, TA=1.15, B=26, %160510093  
D=1.220, QC=0.9495, FS=12.4, U=4.2, TA=1.13, B=25, %160510750  
D=1.240, QC=0.9178, FS=12.0, U=4.3, TA=1.10, B=27, %160511531  
D=1.260, QC=0.9791, FS=22.3, U=4.5, TA=1.10, B=27, %160512328  
D=1.280, QC=0.9708, FS=17.4, U=4.9, TA=1.11, B=26, %160513000  
D=1.300, QC=0.9204, FS=6.1, U=4.3, TA=1.13, B=26, %160513781  
D=1.320, QC=0.8783, FS=1.1, U=3.7, TA=1.11, B=25, %160514578  
D=1.340, QC=0.7074, FS=0.9, U=3.7, TA=1.11, B=25, %160515234  
D=1.360, QC=0.5594, FS=1.5, U=3.7, TA=1.12, B=25, %160516015  
D=1.380, QC=0.3620, FS=3.0, U=3.7, TA=1.11, B=24, %160517125  
D=1.400, QC=0.3236, FS=4.3, U=3.7, TA=1.11, B=24, %160517906  
D=1.420, QC=0.2857, FS=5.4, U=3.8, TA=1.12, B=24, %160518718  
D=1.440, QC=0.2966, FS=6.2, U=3.8, TA=1.12, B=26, %160519375  
D=1.460, QC=0.3496, FS=5.9, U=3.9, TA=1.11, B=22, %160520156  
D=1.480, QC=0.4010, FS=6.8, U=4.1, TA=1.13, B=19, %160521281  
D=1.500, QC=0.4207, FS=6.4, U=4.2, TA=1.13, B=23, %160522062  
D=1.520, QC=0.3999, FS=6.0, U=4.2, TA=1.13, B=23, %160523171  
D=1.540, QC=0.4509, FS=5.0, U=4.3, TA=1.13, B=22, %160523937  
D=1.560, QC=0.5158, FS=4.8, U=4.4, TA=1.14, B=23, %160524703  
D=1.580, QC=0.5308, FS=3.9, U=4.5, TA=1.13, B=23, %160525828  
D=1.600, QC=0.5314, FS=4.3, U=4.6, TA=1.13, B=23, %160526515  
D=1.620, QC=0.5402, FS=5.5, U=4.6, TA=1.13, B=23, %160527281  
D=1.640, QC=0.4903, FS=5.3, U=4.6, TA=1.13, B=23, %160528406  
D=1.660, QC=0.4638, FS=4.9, U=4.6, TA=1.13, B=23, %160529171  
D=1.680, QC=0.4509, FS=6.2, U=4.7, TA=1.13, B=23, %160529953  
D=1.700, QC=0.4862, FS=5.5, U=4.9, TA=1.13, B=22, %160530625  
D=1.720, QC=0.5085, FS=6.7, U=4.9, TA=1.13, B=22, %160531828  
D=1.740, QC=0.4825, FS=6.6, U=4.9, TA=1.13, B=23, %160532500  
D=1.760, QC=0.4067, FS=6.8, U=5.0, TA=1.13, B=24, %160533281  
D=1.780, QC=0.3636, FS=8.0, U=4.9, TA=1.13, B=24, %160534078  
D=1.800, QC=0.4981, FS=7.8, U=5.0, TA=1.14, B=23, %160535187  
D=1.820, QC=0.7064, FS=7.1, U=5.2, TA=1.13, B=24, %160535968  
D=1.840, QC=0.9417, FS=10.0, U=2.9, TA=1.15, B=25, %160536640

D=1.860, QC=0.8238, FS=10.6, U=3.0, TA=1.15, B=24, %160537421  
D=1.880, QC=0.6093, FS=8.4, U=3.1, TA=1.16, B=23, %160538109  
D=1.900, QC=0.4882, FS=5.5, U=3.1, TA=1.16, B=19, %160539343  
D=1.920, QC=0.3340, FS=5.2, U=3.1, TA=1.20, B=21, %160540453  
D=1.940, QC=0.3174, FS=5.6, U=3.1, TA=1.23, B=20, %160541125  
D=1.960, QC=0.3111, FS=5.6, U=3.3, TA=1.25, B=18, %160542234  
D=1.980, QC=0.3028, FS=5.9, U=3.3, TA=1.23, B=19, %160543453  
D=2.000, QC=0.3148, FS=7.5, U=3.4, TA=1.22, B=19, %160544218  
D=2.020, QC=0.3329, FS=7.2, U=1.3, TA=1.21, B=20, %160545312  
D=2.040, QC=0.3101, FS=6.8, U=1.4, TA=1.21, B=22, %160546078  
D=2.060, QC=0.2576, FS=6.3, U=1.4, TA=1.24, B=22, %160547109  
D=2.080, QC=0.2472, FS=4.6, U=1.5, TA=1.23, B=22, %160547890  
D=2.100, QC=0.2353, FS=3.6, U=1.6, TA=1.25, B=22, %160549015  
D=2.120, QC=0.2259, FS=3.7, U=1.6, TA=1.23, B=21, %160549796  
D=2.140, QC=0.2343, FS=3.3, U=1.7, TA=1.24, B=21, %160550500  
D=2.160, QC=0.2706, FS=3.1, U=1.9, TA=1.20, B=23, %160551718  
D=2.180, QC=0.2971, FS=2.9, U=1.9, TA=1.23, B=23, %160552390  
D=2.200, QC=0.3558, FS=3.9, U=2.1, TA=1.24, B=23, %160553171  
D=2.220, QC=0.3989, FS=4.1, U=2.1, TA=1.26, B=21, %160554281  
D=2.240, QC=0.3823, FS=4.6, U=2.2, TA=1.26, B=22, %160555062  
D=2.260, QC=0.3298, FS=5.0, U=2.2, TA=1.26, B=22, %160555828  
D=2.280, QC=0.2420, FS=5.7, U=2.3, TA=1.27, B=22, %160556937  
D=2.300, QC=0.2285, FS=4.3, U=2.4, TA=1.27, B=21, %160557640  
D=2.320, QC=0.2270, FS=2.7, U=2.5, TA=1.27, B=22, %160558843  
D=2.340, QC=0.2270, FS=2.5, U=2.6, TA=1.28, B=21, %160559531  
D=2.360, QC=0.2026, FS=3.2, U=4.8, TA=1.21, B=21, %160595484  
D=2.380, QC=0.2026, FS=3.2, U=4.8, TA=1.21, B=21, %160595484  
D=2.400, QC=0.2062, FS=3.2, U=4.8, TA=1.23, B=21, %160595828  
D=2.420, QC=0.2072, FS=2.2, U=4.4, TA=1.25, B=22, %160596921  
D=2.440, QC=0.2093, FS=1.8, U=4.4, TA=1.22, B=23, %160597703  
D=2.460, QC=0.2104, FS=1.9, U=4.5, TA=1.23, B=23, %160598500  
D=2.480, QC=0.2119, FS=2.0, U=4.5, TA=1.25, B=23, %160599609  
D=2.500, QC=0.2130, FS=1.8, U=4.5, TA=1.23, B=24, %160600390  
D=2.520, QC=0.2140, FS=1.9, U=4.5, TA=1.26, B=22, %160601062  
D=2.540, QC=0.2130, FS=1.9, U=4.7, TA=1.25, B=23, %160602171  
D=2.560, QC=0.2145, FS=1.9, U=4.7, TA=1.26, B=22, %160602953  
D=2.580, QC=0.2176, FS=1.9, U=4.8, TA=1.25, B=22, %160603734  
D=2.600, QC=0.2228, FS=2.0, U=4.9, TA=1.24, B=22, %160604843  
D=2.620, QC=0.2223, FS=2.0, U=5.0, TA=1.26, B=22, %160605625  
D=2.640, QC=0.2213, FS=2.2, U=5.1, TA=1.26, B=22, %160606734  
D=2.660, QC=0.2228, FS=2.4, U=5.1, TA=1.27, B=24, %160607406  
D=2.680, QC=0.2254, FS=2.6, U=5.2, TA=1.27, B=22, %160608171  
D=2.700, QC=0.2270, FS=2.8, U=5.2, TA=1.27, B=22, %160608968  
D=2.720, QC=0.2353, FS=2.8, U=5.3, TA=1.26, B=22, %160610093  
D=2.740, QC=0.2389, FS=2.7, U=5.5, TA=1.27, B=23, %160610859  
D=2.760, QC=0.2415, FS=2.8, U=5.5, TA=1.27, B=22, %160611531  
D=2.780, QC=0.2389, FS=3.4, U=5.6, TA=1.27, B=23, %160612734  
D=2.800, QC=0.2369, FS=3.9, U=5.7, TA=1.28, B=23, %160613500  
D=2.820, QC=0.2410, FS=4.3, U=5.7, TA=1.31, B=24, %160614203  
D=2.840, QC=0.2457, FS=4.7, U=5.8, TA=1.30, B=24, %160614968

D=2.860, QC=0.2472, FS=4.9, U=5.9, TA=1.33, B=24, %160615734  
D=2.880, QC=0.2498, FS=5.1, U=6.0, TA=1.36, B=23, %160616859  
D=2.900, QC=0.2545, FS=5.0, U=6.0, TA=1.36, B=25, %160617531  
D=2.920, QC=0.2514, FS=5.0, U=6.1, TA=1.35, B=24, %160618296  
D=2.940, QC=0.2483, FS=5.0, U=6.2, TA=1.37, B=24, %160619062  
D=2.960, QC=0.2504, FS=5.1, U=6.3, TA=1.36, B=25, %160619828  
D=2.980, QC=0.2509, FS=5.1, U=6.5, TA=1.36, B=25, %160620921  
D=3.000, QC=0.2514, FS=5.0, U=6.5, TA=1.36, B=24, %160621718  
D=3.020, QC=0.2524, FS=4.9, U=6.6, TA=1.37, B=25, %160622500  
D=3.040, QC=0.2504, FS=4.8, U=6.7, TA=1.35, B=24, %160623171  
D=3.060, QC=0.2472, FS=4.5, U=6.8, TA=1.36, B=24, %160623953  
D=3.080, QC=0.2514, FS=4.4, U=6.8, TA=1.35, B=23, %160624734  
D=3.100, QC=0.2446, FS=4.6, U=6.9, TA=1.37, B=25, %160625812  
D=3.120, QC=0.2504, FS=4.8, U=7.0, TA=1.39, B=24, %160626593  
D=3.140, QC=0.2431, FS=4.9, U=7.1, TA=1.38, B=24, %160627375  
D=3.160, QC=0.2514, FS=4.9, U=7.1, TA=1.38, B=23, %160628062  
D=3.180, QC=0.2472, FS=5.0, U=4.9, TA=1.34, B=24, %160628843  
D=3.200, QC=0.2478, FS=4.7, U=7.4, TA=1.40, B=19, %160629968  
D=3.220, QC=0.2478, FS=4.7, U=5.2, TA=1.37, B=19, %160630750  
D=3.240, QC=0.2478, FS=4.6, U=5.4, TA=1.37, B=18, %160631890  
D=3.260, QC=0.2483, FS=4.1, U=5.5, TA=1.38, B=19, %160633000  
D=3.280, QC=0.2478, FS=4.0, U=5.6, TA=1.38, B=19, %160634093  
D=3.300, QC=0.2441, FS=3.9, U=5.6, TA=1.38, B=19, %160634781  
D=3.320, QC=0.2446, FS=3.7, U=5.7, TA=1.37, B=18, %160636000  
D=3.340, QC=0.2431, FS=3.6, U=5.9, TA=1.37, B=19, %160637125  
D=3.360, QC=0.2426, FS=3.5, U=6.0, TA=1.37, B=19, %160638250  
D=3.380, QC=0.2467, FS=3.4, U=6.1, TA=1.37, B=19, %160639359  
D=3.400, QC=0.2498, FS=3.3, U=6.2, TA=1.36, B=18, %160640156  
D=3.420, QC=0.2509, FS=3.3, U=6.4, TA=1.37, B=18, %160641281  
D=3.440, QC=0.2566, FS=3.4, U=6.4, TA=1.38, B=18, %160642296  
D=3.460, QC=0.2618, FS=3.7, U=6.6, TA=1.37, B=19, %160643437  
D=3.480, QC=0.2654, FS=4.0, U=6.7, TA=1.36, B=18, %160644546  
D=3.500, QC=0.2670, FS=4.6, U=6.8, TA=1.37, B=18, %160645765  
D=3.520, QC=0.2457, FS=4.8, U=6.9, TA=1.37, B=18, %160646875  
D=3.540, QC=0.2576, FS=6.4, U=6.6, TA=1.38, B=31, %160687609  
D=3.560, QC=0.2576, FS=6.4, U=6.6, TA=1.38, B=31, %160687609  
D=3.580, QC=0.2576, FS=6.4, U=6.6, TA=1.38, B=31, %160687609  
D=3.600, QC=0.2633, FS=6.4, U=6.6, TA=1.40, B=29, %160687937  
D=3.620, QC=0.2670, FS=6.2, U=6.2, TA=1.40, B=29, %160688718  
D=3.640, QC=0.2670, FS=5.8, U=6.2, TA=1.40, B=29, %160689062  
D=3.660, QC=0.2675, FS=5.4, U=6.2, TA=1.39, B=30, %160689828  
D=3.680, QC=0.2670, FS=5.3, U=6.3, TA=1.39, B=29, %160690609  
D=3.700, QC=0.2680, FS=5.3, U=6.3, TA=1.38, B=28, %160691281  
D=3.720, QC=0.2685, FS=5.3, U=6.3, TA=1.33, B=30, %160691718  
D=3.740, QC=0.2649, FS=4.9, U=6.4, TA=1.38, B=18, %160692843  
D=3.760, QC=0.2566, FS=5.1, U=6.4, TA=1.38, B=16, %160693937  
D=3.780, QC=0.2550, FS=5.5, U=6.5, TA=1.37, B=15, %160695031  
D=3.800, QC=0.2561, FS=5.6, U=6.6, TA=1.37, B=16, %160696171  
D=3.820, QC=0.2581, FS=5.6, U=6.8, TA=1.39, B=17, %160697718  
D=3.840, QC=0.2566, FS=5.8, U=6.8, TA=1.37, B=17, %160698859

D=3.860, QC=0.2556, FS=5.8, U=6.8, TA=1.37, B=17, %160699984  
D=3.880, QC=0.2576, FS=5.6, U=6.9, TA=1.38, B=18, %160701078  
D=3.900, QC=0.2607, FS=5.6, U=7.0, TA=1.36, B=17, %160702187  
D=3.920, QC=0.2633, FS=5.8, U=7.1, TA=1.37, B=17, %160703296  
D=3.940, QC=0.2581, FS=6.0, U=7.2, TA=1.38, B=18, %160704406  
D=3.960, QC=0.2556, FS=5.9, U=7.3, TA=1.36, B=18, %160705531  
D=3.980, QC=0.2540, FS=5.8, U=7.4, TA=1.37, B=17, %160706640  
D=4.000, QC=0.2550, FS=5.7, U=7.4, TA=1.37, B=19, %160707437  
D=4.020, QC=0.2535, FS=5.7, U=7.6, TA=1.37, B=18, %160708562  
D=4.040, QC=0.2566, FS=5.6, U=7.6, TA=1.36, B=19, %160709656  
D=4.060, QC=0.2587, FS=5.2, U=7.7, TA=1.37, B=18, %160710765  
D=4.080, QC=0.2607, FS=5.2, U=7.8, TA=1.37, B=18, %160711906  
D=4.100, QC=0.2581, FS=5.1, U=7.9, TA=1.35, B=18, %160713140  
D=4.120, QC=0.2550, FS=5.3, U=8.1, TA=1.36, B=19, %160713796  
D=4.140, QC=0.2561, FS=5.3, U=8.1, TA=1.36, B=18, %160714906  
D=4.160, QC=0.2587, FS=5.4, U=8.2, TA=1.37, B=18, %160716109  
D=4.180, QC=0.2613, FS=5.5, U=8.2, TA=1.37, B=19, %160717140  
D=4.200, QC=0.2613, FS=5.3, U=8.3, TA=1.37, B=19, %160718375  
D=4.220, QC=0.2633, FS=5.2, U=8.4, TA=1.39, B=18, %160719046  
D=4.240, QC=0.2649, FS=5.1, U=8.5, TA=1.36, B=18, %160720187  
D=4.260, QC=0.2633, FS=5.1, U=8.6, TA=1.39, B=18, %160721296  
D=4.280, QC=0.2633, FS=5.2, U=8.7, TA=1.36, B=19, %160722390  
D=4.300, QC=0.2628, FS=4.9, U=8.8, TA=1.36, B=18, %160723609  
D=4.320, QC=0.2649, FS=4.7, U=8.9, TA=1.36, B=18, %160724640  
D=4.340, QC=0.2649, FS=4.6, U=9.0, TA=1.38, B=18, %160725843  
D=4.360, QC=0.2685, FS=4.6, U=9.0, TA=1.37, B=19, %160726531  
D=4.380, QC=0.2711, FS=4.8, U=9.1, TA=1.40, B=18, %160727656  
D=4.400, QC=0.2717, FS=4.8, U=9.2, TA=1.38, B=17, %160728781  
D=4.420, QC=0.2737, FS=5.0, U=9.3, TA=1.39, B=18, %160729906  
D=4.440, QC=0.2758, FS=5.4, U=9.4, TA=1.37, B=18, %160731109  
D=4.460, QC=0.2805, FS=5.6, U=9.5, TA=1.40, B=18, %160732203  
D=4.480, QC=0.2831, FS=5.6, U=9.6, TA=1.38, B=17, %160733328  
D=4.500, QC=0.2898, FS=5.5, U=9.7, TA=1.41, B=17, %160734437  
D=4.520, QC=0.2883, FS=5.6, U=9.7, TA=1.41, B=18, %160735203  
D=4.540, QC=0.2898, FS=5.7, U=9.9, TA=1.37, B=18, %160736296  
D=4.560, QC=0.2904, FS=5.9, U=9.9, TA=1.41, B=18, %160737421  
D=4.580, QC=0.2888, FS=5.9, U=10.1, TA=1.41, B=17, %160738531  
D=4.600, QC=0.2935, FS=6.1, U=10.1, TA=1.43, B=18, %160739734  
D=4.620, QC=0.2945, FS=6.5, U=10.3, TA=1.43, B=21, %160740828  
D=4.640, QC=0.2966, FS=6.3, U=10.4, TA=1.43, B=22, %160741609  
D=4.660, QC=0.2929, FS=6.3, U=10.4, TA=1.41, B=22, %160742281  
D=4.680, QC=0.2961, FS=6.2, U=10.4, TA=1.43, B=24, %160743390  
D=4.700, QC=0.2779, FS=6.1, U=10.5, TA=1.41, B=23, %160744187  
D=4.720, QC=0.2961, FS=7.1, U=11.6, TA=1.44, B=26, %160781078  
D=4.740, QC=0.2961, FS=7.1, U=11.6, TA=1.44, B=26, %160781078  
D=4.760, QC=0.2976, FS=7.1, U=11.6, TA=1.39, B=26, %160781406  
D=4.780, QC=0.2961, FS=7.2, U=11.2, TA=1.38, B=27, %160782203  
D=4.800, QC=0.2971, FS=7.0, U=11.2, TA=1.40, B=24, %160782875  
D=4.820, QC=0.2987, FS=7.0, U=11.2, TA=1.39, B=25, %160783640  
D=4.840, QC=0.2971, FS=6.9, U=11.2, TA=1.41, B=26, %160784437



D=4.860, QC=0.2935, FS=6.7, U=11.2, TA=1.41, B=26, %160785203  
D=4.880, QC=0.2914, FS=6.7, U=11.2, TA=1.42, B=24, %160785859  
D=4.900, QC=0.2914, FS=6.8, U=11.3, TA=1.41, B=24, %160786640  
D=4.920, QC=0.2929, FS=6.8, U=11.3, TA=1.43, B=25, %160787406  
D=4.940, QC=0.2950, FS=6.7, U=11.4, TA=1.43, B=25, %160788203  
D=4.960, QC=0.3018, FS=6.8, U=11.5, TA=1.43, B=24, %160789296  
D=4.980, QC=0.3267, FS=7.1, U=11.6, TA=1.42, B=25, %160789984  
D=5.000, QC=0.4457, FS=7.5, U=11.7, TA=1.41, B=25, %160790765  
D=5.020, QC=0.5755, FS=7.5, U=11.8, TA=1.41, B=26, %160791531  
D=5.040, QC=0.5532, FS=7.9, U=11.8, TA=1.42, B=25, %160792328  
D=5.060, QC=0.4394, FS=9.2, U=11.7, TA=1.43, B=25, %160793000  
D=5.080, QC=0.3496, FS=9.2, U=11.8, TA=1.43, B=26, %160793781  
D=5.100, QC=0.3205, FS=6.6, U=11.9, TA=1.42, B=25, %160794562  
D=5.120, QC=0.3703, FS=6.2, U=12.1, TA=1.42, B=24, %160795234  
D=5.140, QC=0.4919, FS=7.0, U=12.2, TA=1.38, B=25, %160796031  
D=5.160, QC=1.0632, FS=20.7, U=12.4, TA=1.43, B=25, %160797125  
D=5.180, QC=1.2637, FS=73.0, U=14.5, TA=1.44, B=26, %160797890  
D=5.200, QC=1.5369, FS=106.9, U=17.6, TA=1.43, B=25, %160798671  
D=5.220, QC=1.5401, FS=112.2, U=19.1, TA=1.41, B=25, %160799437  
D=5.240, QC=1.3333, FS=109.5, U=19.2, TA=1.40, B=24, %160800109  
D=5.260, QC=1.0695, FS=103.1, U=18.6, TA=1.43, B=25, %160800906  
D=5.280, QC=1.0222, FS=84.9, U=17.9, TA=1.42, B=24, %160801703  
D=5.300, QC=1.0284, FS=62.1, U=17.1, TA=1.44, B=25, %160802375  
D=5.320, QC=0.9983, FS=53.9, U=16.6, TA=1.46, B=26, %160803140  
D=5.340, QC=1.0009, FS=54.3, U=16.5, TA=1.47, B=25, %160803921  
D=5.360, QC=1.0232, FS=81.1, U=17.3, TA=1.47, B=25, %160805046  
D=5.380, QC=1.0700, FS=98.4, U=17.8, TA=1.46, B=26, %160805828  
D=5.400, QC=1.1676, FS=105.4, U=18.2, TA=1.47, B=25, %160806500  
D=5.420, QC=1.2305, FS=104.4, U=18.3, TA=1.48, B=25, %160807265  
D=5.440, QC=1.1770, FS=97.7, U=18.2, TA=1.48, B=24, %160808031  
D=5.460, QC=1.1069, FS=88.1, U=18.2, TA=1.48, B=25, %160808812  
D=5.480, QC=1.0554, FS=72.9, U=17.8, TA=1.48, B=25, %160809578  
D=5.500, QC=0.9973, FS=38.0, U=16.6, TA=1.48, B=25, %160810250  
D=5.520, QC=0.9386, FS=14.5, U=14.9, TA=1.49, B=24, %160811046  
D=5.540, QC=0.8508, FS=9.6, U=13.6, TA=1.49, B=26, %160811812  
D=5.560, QC=0.7765, FS=14.5, U=13.3, TA=1.49, B=27, %160812593  
D=5.580, QC=0.6565, FS=21.0, U=13.3, TA=1.49, B=26, %160813296  
D=5.600, QC=0.5563, FS=18.3, U=13.3, TA=1.49, B=25, %160814062  
D=5.620, QC=0.4773, FS=17.3, U=13.2, TA=1.49, B=25, %160814718  
D=5.640, QC=0.4618, FS=16.4, U=13.2, TA=1.49, B=26, %160815484  
D=5.660, QC=0.9453, FS=15.8, U=13.0, TA=1.49, B=26, %160816609  
D=5.680, QC=0.9978, FS=35.2, U=14.0, TA=1.49, B=24, %160817390  
D=5.700, QC=0.9739, FS=35.5, U=15.0, TA=1.49, B=25, %160818171  
D=5.720, QC=0.8653, FS=14.0, U=13.9, TA=1.49, B=25, %160818937  
D=5.740, QC=0.6534, FS=6.7, U=13.4, TA=1.49, B=25, %160819609  
D=5.760, QC=0.4955, FS=4.0, U=13.3, TA=1.49, B=24, %160820406  
D=5.780, QC=0.4192, FS=3.7, U=13.3, TA=1.49, B=24, %160821171  
D=5.800, QC=0.4166, FS=4.3, U=13.3, TA=1.49, B=25, %160821859  
D=5.820, QC=0.4140, FS=5.8, U=13.3, TA=1.49, B=24, %160822625  
D=5.840, QC=0.4083, FS=8.7, U=13.3, TA=1.49, B=24, %160823828

D=5.860, QC=0.4233, FS=8.9, U=13.3, TA=1.49, B=24, %160824484  
D=5.880, QC=0.5433, FS=8.6, U=13.2, TA=1.49, B=23, %160825250  
D=5.900, QC=0.9858, FS=34.3, U=16.0, TA=1.50, B=0, %160867734  
D=5.920, QC=0.9978, FS=36.2, U=15.7, TA=1.49, B=13, %160868859  
D=5.940, QC=0.9755, FS=17.0, U=14.8, TA=1.49, B=17, %160869984  
D=5.960, QC=0.8669, FS=9.1, U=13.9, TA=1.49, B=16, %160871078  
D=5.980, QC=0.7750, FS=9.6, U=13.6, TA=1.49, B=16, %160872171  
D=6.000, QC=0.7900, FS=11.3, U=13.6, TA=1.49, B=17, %160873375  
D=6.020, QC=0.9157, FS=9.3, U=13.5, TA=1.49, B=16, %160874828  
D=6.040, QC=0.9391, FS=16.5, U=13.5, TA=1.49, B=15, %160875921  
D=6.060, QC=0.9744, FS=26.6, U=14.4, TA=1.49, B=15, %160877453  
D=6.080, QC=0.9879, FS=30.4, U=14.7, TA=1.49, B=15, %160878562  
D=6.100, QC=0.9760, FS=28.7, U=15.2, TA=1.49, B=15, %160880015  
D=6.120, QC=0.9401, FS=16.5, U=14.0, TA=1.49, B=15, %160881234  
D=6.140, QC=0.9443, FS=29.4, U=14.7, TA=1.49, B=15, %160882687  
D=6.160, QC=0.9557, FS=27.0, U=14.8, TA=1.49, B=15, %160883781  
D=6.180, QC=0.7583, FS=11.4, U=14.7, TA=1.49, B=16, %160885312  
D=6.200, QC=0.6607, FS=11.1, U=14.1, TA=1.49, B=15, %160886406  
D=6.220, QC=0.5132, FS=14.7, U=14.0, TA=1.49, B=15, %160887953  
D=6.240, QC=0.5901, FS=16.7, U=14.0, TA=1.49, B=15, %160889093  
D=6.260, QC=0.7402, FS=17.7, U=14.1, TA=1.49, B=16, %160890515  
D=6.280, QC=0.6534, FS=15.6, U=14.1, TA=1.50, B=16, %160891640  
D=6.300, QC=0.4841, FS=16.9, U=14.0, TA=1.49, B=16, %160892828  
D=6.320, QC=0.4425, FS=9.8, U=14.1, TA=1.49, B=18, %160893968  
D=6.340, QC=0.4212, FS=7.9, U=14.1, TA=1.49, B=19, %160895109  
D=6.360, QC=0.4228, FS=7.4, U=14.1, TA=1.49, B=18, %160896234  
D=6.380, QC=0.4394, FS=7.0, U=14.2, TA=1.49, B=19, %160897359  
D=6.400, QC=0.4581, FS=6.7, U=14.2, TA=1.49, B=19, %160898031  
D=6.420, QC=0.5023, FS=6.2, U=14.3, TA=1.49, B=19, %160899140  
D=6.440, QC=0.7781, FS=7.2, U=14.4, TA=1.49, B=18, %160900265  
D=6.460, QC=0.9479, FS=36.5, U=16.2, TA=1.49, B=19, %160901500  
D=6.480, QC=1.0352, FS=51.1, U=16.9, TA=1.49, B=18, %160902609  
D=6.500, QC=1.0373, FS=60.2, U=17.5, TA=1.49, B=18, %160903640  
D=6.520, QC=1.0378, FS=62.9, U=17.7, TA=1.49, B=18, %160904406  
D=6.540, QC=0.9978, FS=55.6, U=17.6, TA=1.49, B=18, %160905531  
D=6.560, QC=0.8986, FS=17.0, U=15.6, TA=1.51, B=19, %160906734  
D=6.580, QC=0.7563, FS=6.9, U=14.4, TA=1.51, B=19, %160907765  
D=6.600, QC=0.6399, FS=12.1, U=14.2, TA=1.49, B=18, %160908984  
D=6.620, QC=0.5308, FS=16.5, U=14.3, TA=1.50, B=19, %160909656  
D=6.640, QC=0.4877, FS=18.3, U=14.4, TA=1.51, B=19, %160910765  
D=6.660, QC=0.5194, FS=18.3, U=14.6, TA=1.49, B=19, %160911984  
D=6.680, QC=0.6830, FS=16.3, U=14.7, TA=1.50, B=18, %160913093  
D=6.700, QC=0.9407, FS=15.7, U=14.8, TA=1.50, B=19, %160913765  
D=6.720, QC=1.0342, FS=46.3, U=17.2, TA=1.50, B=19, %160914890  
D=6.740, QC=1.0934, FS=54.2, U=18.1, TA=1.51, B=18, %160916109  
D=6.760, QC=1.0923, FS=60.0, U=18.8, TA=1.53, B=17, %160917218  
D=6.780, QC=1.0840, FS=60.3, U=19.0, TA=1.53, B=17, %160918328  
D=6.800, QC=1.1105, FS=67.6, U=19.5, TA=1.51, B=18, %160919453  
D=6.820, QC=1.2840, FS=78.3, U=20.3, TA=1.49, B=17, %160920562  
D=6.840, QC=1.3235, FS=78.1, U=21.0, TA=1.49, B=16, %160921656

D=6.860, QC=1.0191, FS=31.7, U=18.1, TA=1.52, B=17, %160923187  
D=6.880, QC=0.9739, FS=17.5, U=16.9, TA=1.52, B=18, %160923984  
D=6.900, QC=0.8950, FS=11.6, U=16.3, TA=1.50, B=18, %160925093  
D=6.920, QC=0.8409, FS=7.7, U=16.0, TA=1.50, B=17, %160926218  
D=6.940, QC=0.7116, FS=8.8, U=16.0, TA=1.53, B=17, %160927640  
D=6.960, QC=0.5895, FS=10.3, U=16.0, TA=1.50, B=17, %160928765  
D=6.980, QC=0.5090, FS=9.8, U=15.9, TA=1.50, B=17, %160929546  
D=7.000, QC=0.4649, FS=11.4, U=15.5, TA=1.52, B=18, %160930656  
D=7.020, QC=0.4275, FS=11.2, U=15.5, TA=1.50, B=17, %160931765  
D=7.040, QC=0.4192, FS=9.8, U=15.4, TA=1.50, B=17, %160932984  
D=7.060, QC=0.3854, FS=10.3, U=18.0, TA=1.56, B=21, %160967078  
D=7.080, QC=0.3854, FS=10.3, U=18.0, TA=1.56, B=21, %160967078  
D=7.100, QC=0.3844, FS=10.3, U=18.0, TA=1.52, B=21, %160967515  
D=7.120, QC=0.3901, FS=7.4, U=17.6, TA=1.52, B=22, %160968640  
D=7.140, QC=0.3885, FS=6.6, U=17.7, TA=1.50, B=21, %160969296  
D=7.160, QC=0.3901, FS=5.8, U=17.8, TA=1.52, B=21, %160970500  
D=7.180, QC=0.3932, FS=5.5, U=17.7, TA=1.53, B=21, %160971265  
D=7.200, QC=0.3937, FS=5.6, U=17.7, TA=1.53, B=21, %160972031  
D=7.220, QC=0.3953, FS=6.0, U=17.8, TA=1.52, B=22, %160973140  
D=7.240, QC=0.3953, FS=6.4, U=17.9, TA=1.52, B=22, %160973812  
D=7.260, QC=0.3963, FS=6.5, U=18.0, TA=1.52, B=21, %160975031  
D=7.280, QC=0.3937, FS=6.7, U=18.0, TA=1.50, B=21, %160975718  
D=7.300, QC=0.3890, FS=7.0, U=18.1, TA=1.53, B=21, %160976828  
D=7.320, QC=0.3864, FS=7.0, U=18.1, TA=1.52, B=21, %160977593  
D=7.340, QC=0.3823, FS=7.3, U=18.2, TA=1.54, B=20, %160978703  
D=7.360, QC=0.3797, FS=7.3, U=18.2, TA=1.54, B=21, %160979484  
D=7.380, QC=0.3812, FS=7.2, U=18.3, TA=1.53, B=21, %160980593  
D=7.400, QC=0.3854, FS=7.4, U=18.4, TA=1.53, B=21, %160981390  
D=7.420, QC=0.3880, FS=7.3, U=18.5, TA=1.56, B=21, %160982515  
D=7.440, QC=0.3880, FS=7.1, U=18.6, TA=1.54, B=22, %160983296  
D=7.460, QC=0.3896, FS=7.2, U=18.6, TA=1.53, B=21, %160984406  
D=7.480, QC=0.3870, FS=7.2, U=18.7, TA=1.55, B=21, %160985078  
D=7.500, QC=0.3901, FS=7.1, U=18.8, TA=1.52, B=21, %160985843  
D=7.520, QC=0.3927, FS=7.1, U=18.8, TA=1.54, B=22, %160986953  
D=7.540, QC=0.3911, FS=7.2, U=18.9, TA=1.53, B=21, %160987734  
D=7.560, QC=0.3937, FS=7.3, U=19.0, TA=1.54, B=23, %160988500  
D=7.580, QC=0.3979, FS=7.3, U=19.1, TA=1.54, B=22, %160989625  
D=7.600, QC=0.3994, FS=7.2, U=19.2, TA=1.55, B=23, %160990390  
D=7.620, QC=0.4015, FS=7.3, U=19.3, TA=1.55, B=22, %160991500  
D=7.640, QC=0.3994, FS=7.5, U=19.3, TA=1.56, B=21, %160992296  
D=7.660, QC=0.3968, FS=7.6, U=19.4, TA=1.55, B=21, %160992968  
D=7.680, QC=0.3968, FS=8.0, U=19.5, TA=1.56, B=22, %160994078  
D=7.700, QC=0.3984, FS=8.2, U=19.6, TA=1.56, B=22, %160994843  
D=7.720, QC=0.3911, FS=8.2, U=19.7, TA=1.56, B=22, %160995625  
D=7.740, QC=0.3942, FS=8.2, U=19.7, TA=1.56, B=23, %160996734  
D=7.760, QC=0.3942, FS=8.0, U=19.9, TA=1.56, B=23, %160997500  
D=7.780, QC=0.3958, FS=7.9, U=19.9, TA=1.55, B=23, %160998281  
D=7.800, QC=0.3942, FS=7.3, U=20.1, TA=1.56, B=22, %160999375  
D=7.820, QC=0.3968, FS=7.1, U=20.1, TA=1.55, B=23, %161000078  
D=7.840, QC=0.3968, FS=7.1, U=20.2, TA=1.55, B=24, %161000859

D=7.860, QC=0.4005, FS=7.3, U=20.3, TA=1.53, B=23, %161001625  
D=7.880, QC=0.3979, FS=7.3, U=20.2, TA=1.58, B=22, %161002734  
D=7.900, QC=0.3979, FS=7.3, U=20.4, TA=1.58, B=23, %161003500  
D=7.920, QC=0.3958, FS=7.5, U=20.5, TA=1.61, B=24, %161004281  
D=7.940, QC=0.3932, FS=7.8, U=20.5, TA=1.61, B=23, %161004953  
D=7.960, QC=0.3942, FS=8.0, U=20.6, TA=1.64, B=22, %161006062  
D=7.980, QC=0.3937, FS=8.2, U=20.7, TA=1.63, B=23, %161006843  
D=8.000, QC=0.3922, FS=8.4, U=20.8, TA=1.63, B=24, %161007609  
D=8.020, QC=0.3958, FS=8.5, U=20.9, TA=1.63, B=23, %161008703  
D=8.040, QC=0.3948, FS=8.6, U=20.9, TA=1.64, B=22, %161009468  
D=8.060, QC=0.3963, FS=8.5, U=21.0, TA=1.64, B=22, %161010234  
D=8.080, QC=0.4015, FS=8.5, U=21.1, TA=1.64, B=23, %161011000  
D=8.100, QC=0.4046, FS=8.7, U=21.3, TA=1.63, B=23, %161012109  
D=8.120, QC=0.4098, FS=8.6, U=21.3, TA=1.64, B=22, %161012875  
D=8.140, QC=0.4171, FS=8.7, U=21.4, TA=1.64, B=21, %161013671  
D=8.160, QC=0.4285, FS=8.8, U=21.5, TA=1.64, B=23, %161014687  
D=8.180, QC=0.4301, FS=8.9, U=21.5, TA=1.64, B=22, %161015453  
D=8.200, QC=0.4285, FS=9.1, U=21.6, TA=1.63, B=23, %161016281  
D=8.220, QC=0.4290, FS=9.5, U=21.8, TA=1.64, B=21, %161017406  
D=8.240, QC=0.4275, FS=9.6, U=21.8, TA=1.64, B=22, %161018062  
D=8.260, QC=0.4031, FS=7.9, U=21.9, TA=1.63, B=14, %161019265  
D=8.280, QC=0.4296, FS=11.2, U=27.0, TA=1.57, B=27, %161072750  
D=8.300, QC=0.4296, FS=11.2, U=27.0, TA=1.57, B=27, %161072750  
D=8.320, QC=0.4347, FS=11.2, U=27.0, TA=1.58, B=27, %161073203  
D=8.340, QC=0.4358, FS=11.1, U=26.5, TA=1.59, B=26, %161073890  
D=8.360, QC=0.4363, FS=10.8, U=26.6, TA=1.63, B=28, %161074656  
D=8.380, QC=0.4337, FS=10.5, U=26.6, TA=1.53, B=26, %161075421 , F=11  
D=8.400, QC=0.4275, FS=10.1, U=26.7, TA=1.60, B=27, %161076203  
D=8.420, QC=0.4275, FS=9.6, U=26.6, TA=1.60, B=28, %161076968 , F=11  
D=8.440, QC=0.4259, FS=9.2, U=26.7, TA=1.85, B=28, %161077640 , F=11  
D=8.460, QC=0.4197, FS=7.7, U=26.7, TA=1.98, B=26, %161078421  
D=8.480, QC=0.4197, FS=8.0, U=26.7, TA=1.98, B=2, %161078750  
D=8.500, QC=0.4238, FS=7.8, U=26.8, TA=1.98, B=26, %161080000  
D=8.520, QC=0.4212, FS=8.1, U=26.8, TA=1.98, B=27, %161080718  
D=8.540, QC=0.4161, FS=8.2, U=27.0, TA=1.98, B=25, %161081484  
D=8.560, QC=0.4119, FS=8.4, U=27.0, TA=1.98, B=27, %161082156  
D=8.580, QC=0.4093, FS=8.5, U=27.1, TA=1.98, B=27, %161082921  
D=8.600, QC=0.4067, FS=8.6, U=27.1, TA=1.99, B=28, %161083703  
D=8.620, QC=0.4041, FS=8.4, U=27.2, TA=1.99, B=26, %161084484  
D=8.640, QC=0.4010, FS=8.0, U=27.1, TA=2.00, B=27, %161085156  
D=8.660, QC=0.4005, FS=7.7, U=27.2, TA=2.00, B=26, %161085921  
D=8.680, QC=0.3999, FS=7.2, U=27.3, TA=2.00, B=28, %161086718  
D=8.700, QC=0.3968, FS=6.8, U=27.3, TA=2.00, B=27, %161087390  
D=8.720, QC=0.3999, FS=6.6, U=27.4, TA=2.00, B=28, %161088171  
D=8.740, QC=0.3999, FS=6.7, U=27.5, TA=2.00, B=27, %161088515  
D=8.760, QC=0.3989, FS=6.9, U=27.5, TA=2.01, B=29, %161089296  
D=8.780, QC=0.3994, FS=6.9, U=27.6, TA=2.01, B=28, %161090078  
D=8.800, QC=0.3999, FS=7.1, U=27.6, TA=2.01, B=28, %161090859  
D=8.820, QC=0.4010, FS=7.2, U=27.7, TA=2.01, B=28, %161091515  
D=8.840, QC=0.3979, FS=7.1, U=27.7, TA=2.01, B=29, %161092312

D=8.860, QC=0.4015, FS=7.0, U=27.8, TA=2.01, B=27, %161093078  
D=8.880, QC=0.4046, FS=7.0, U=27.9, TA=2.01, B=29, %161093843  
D=8.900, QC=0.4067, FS=7.0, U=27.9, TA=2.01, B=28, %161094171  
D=8.920, QC=0.4119, FS=7.1, U=28.0, TA=2.01, B=28, %161094968  
D=8.940, QC=0.4150, FS=7.3, U=28.1, TA=2.01, B=28, %161095734  
D=8.960, QC=0.4176, FS=7.5, U=28.1, TA=2.01, B=29, %161096406  
D=8.980, QC=0.4212, FS=7.7, U=28.2, TA=2.01, B=28, %161097171  
D=9.000, QC=0.4238, FS=8.1, U=28.2, TA=2.01, B=28, %161097937  
D=9.020, QC=0.4290, FS=8.4, U=28.2, TA=2.01, B=27, %161098718  
D=9.040, QC=0.4290, FS=8.7, U=28.3, TA=2.01, B=28, %161099375  
D=9.060, QC=0.4290, FS=8.9, U=28.4, TA=2.01, B=28, %161099828  
D=9.080, QC=0.4290, FS=8.8, U=28.5, TA=2.01, B=28, %161100515  
D=9.100, QC=0.4347, FS=8.8, U=28.5, TA=2.01, B=27, %161101281  
D=9.120, QC=0.4431, FS=8.7, U=28.7, TA=2.01, B=29, %161102062  
D=9.140, QC=0.4462, FS=8.8, U=28.8, TA=2.01, B=28, %161102734  
D=9.160, QC=0.4498, FS=8.7, U=28.8, TA=2.01, B=28, %161103515  
D=9.180, QC=0.4540, FS=8.6, U=29.0, TA=2.01, B=27, %161104281  
D=9.200, QC=0.4550, FS=8.9, U=29.0, TA=2.01, B=28, %161105062  
D=9.220, QC=0.4550, FS=9.2, U=29.1, TA=2.01, B=28, %161105843  
D=9.240, QC=0.4545, FS=9.5, U=29.1, TA=2.01, B=26, %161106609  
D=9.260, QC=0.4540, FS=9.5, U=29.1, TA=2.01, B=27, %161106937  
D=9.280, QC=0.4534, FS=9.7, U=29.2, TA=2.00, B=27, %161107625  
D=9.300, QC=0.4571, FS=10.0, U=29.3, TA=2.00, B=27, %161108390  
D=9.320, QC=0.4618, FS=10.1, U=29.3, TA=2.00, B=27, %161109156  
D=9.340, QC=0.4607, FS=10.2, U=29.4, TA=1.99, B=26, %161109921  
D=9.360, QC=0.4576, FS=10.1, U=29.5, TA=1.99, B=27, %161110687  
D=9.380, QC=0.4576, FS=10.0, U=29.5, TA=1.99, B=27, %161111453  
D=9.400, QC=0.4555, FS=9.9, U=29.7, TA=1.99, B=27, %161112218  
D=9.420, QC=0.4586, FS=9.7, U=29.7, TA=1.99, B=26, %161112890  
D=9.440, QC=0.4586, FS=9.5, U=29.8, TA=1.99, B=26, %161113671  
D=9.460, QC=0.4586, FS=9.5, U=29.9, TA=1.99, B=26, %161114437, NA=0.0094, NB=-0.3, NC=9.9, F=15, K=90, T=The test are ended without any stop in the ground.

#\$

0:

1:

2:

3:

4:

5:

6:

7:

8:

9:

11:Tilt derivative alarm

12:Point resistance alarm

13:Depth unchanged for 5 second

14:Transmission lost

15:End of test

16:Dissipation start

**APPENDIX I**  
**(Settlement Column**  
**Report)**

**Final Report:**

**Settling Properties of Fine-Grained Sediments:  
Breton Landbridge Marsh Creation (West) (BS-0038)  
(APS Project No. APS2008-G063)**

**Submitted to:**

**Sergio Aviles, P.E.  
President  
APS Design and Testing, LLC  
5261 Highland Rd., PMB #320  
Baton Rouge, LA 70808  
Phone: (225) 456-5714  
Email: [sergio@aps-testing.com](mailto:sergio@aps-testing.com)**

**Submitted by:**

**William M. Moe, Ph.D., P.E.  
Principal and Project Manager  
SCTCS Group LLC  
LBTC, Building 3000  
8000 Innovation Park Drive  
Baton Rouge, LA 70820  
Phone: (225) 803-3945  
Email: [wmoe@sctcs.com](mailto:wmoe@sctcs.com)**

**November 20, 2020**



## **1.0 Introduction, Scope, and Objectives**

The objective of the testing reported here was to evaluate the settling properties of fine-grained sediments which may be hydraulically dredged in support of the Breton Landbridge Marsh Creation (West) (BS-0038) project in Plaquemines Parish, LA (APS Project No. APS2008-G063).

## **2.0 Experimental Procedures and Results**

### **2.1 Materials Provided for Testing**

Four five-gallon buckets of composited sediment samples from the proposed dredging area (labeled as “G063 Breton Composite”) and two five-gallon buckets of water (labeled as “G063 sample from B-8, 8/12/20”) were provided by APS Design and Testing, LLC (APS) for pilot-scale settling column testing. The salinity of the water from the proposed dredge location, measured gravimetrically with drying at 180 °C<sup>1</sup>, was 0.60 parts per thousand (ppt) indicative of a freshwater environment.

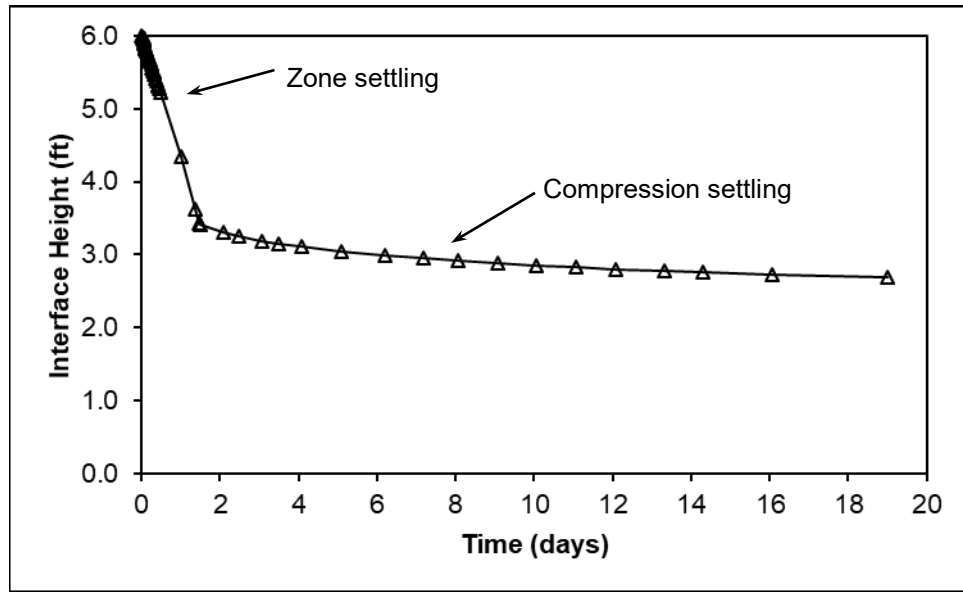
As requested by APS, two separate settling column tests were conducted using composited sediment with initial slurry depth of six feet and target initial fine-grained particulate concentrations of 160 and 300 g/L. Testing procedures and results from each of the two tests, hereafter arbitrarily referred to as tests A and B, are presented in the following sections.

### **2.2 Pilot-Scale Settling Column Test A (target initial concentration 160 g/L)**

Slurry was prepared by mixing an equal amount of composited sediment from each of the four provided buckets with a combination of site water and tap water supplemented with a small amount of synthetic sea salts (Instant Ocean) to match the average salinity of the site water samples [salinity of 0.60 parts per thousand (ppt)]. Slurry containing the fine-grained fraction of sediments was obtained by thoroughly mixing the slurry and then allowing coarse grained materials (e.g., sand and shells), to separate by differential settling as described in the US Army Corps of Engineers Manual No. 1110-2-5027<sup>1</sup>. The fine-grained sediment slurry was transferred to a second mixing barrel, thoroughly mixed, and then loaded into a large-scale (8.0 inch ID) column while mixing with air sparging as described in the US Army Corps of Engineers Manual No. 1110-2-5027<sup>1</sup>. Solids concentrations in the slurry at the start of the settling test were measured in samples collected along the height of the column at one foot intervals (see Table A1 in Appendix A for tabulated data). The average particulate concentration at the start of the settling test was 158.9 g/L, close to but slightly less than the target concentration of 160 g/L. An aliquot of the slurry mix prepared for loading into the pilot-scale column was set aside for return to APS for use in determining grain size distribution or other parameters.

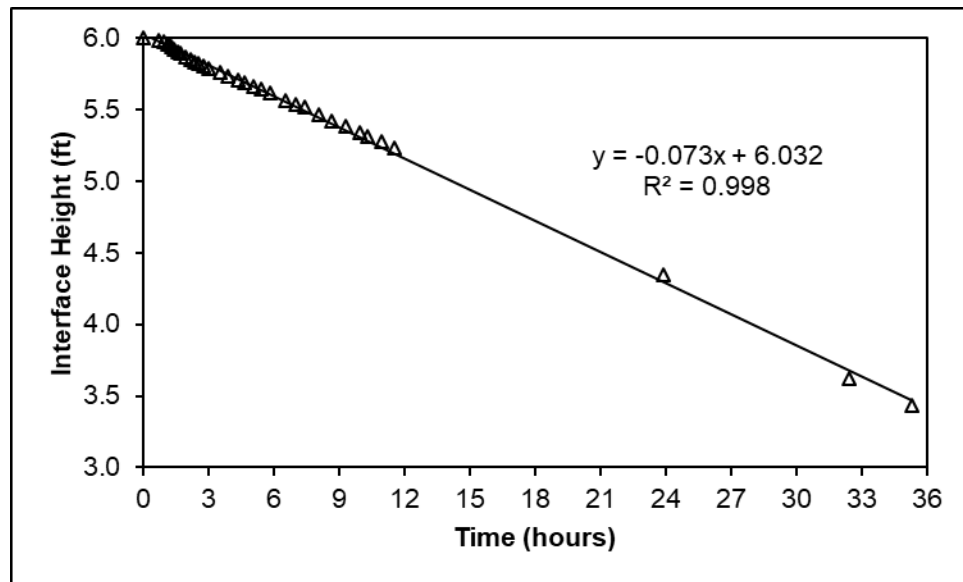
A readily visible sediment-water interface was observed less than one hour after the start of the settling test, indicating zone settling. The height of the sediment-water interface above the bottom of the column was measured and recorded over a period lasting more than 15 days as depicted in Figure 1 (see Table A2 in Appendix A for tabulated data). As shown in Figure 1, zone settling was observed during the first portion of the settling test, followed by compression settling thereafter.





**Figure 1.** Interface height as a function of time during pilot-scale settling test A (initial particulate concentration 158.9 g/L).

Interface heights from the first 36 hours of the settling test, during which zone settling was observed, are depicted separately in Figure 2. A linear regression was performed for settling data in this time interval with the resulting equation and correlation coefficient shown on the graph. The slope of the regression line, which corresponds to the zone settling velocity, was 0.073 ft/hr (1.74 ft/day).



**Figure 2.** Interface height as a function of time during the zone settling portion of pilot-scale settling test A ( $C_o=158.9$  g/L).

For the portion of the settling test during which compression settling was observed, the concentration in the settled solids at each time interval was calculated using the following equation (equation 3-11 in ref. 1).

$$C = \frac{C_o H_i}{H_t}$$

Where:

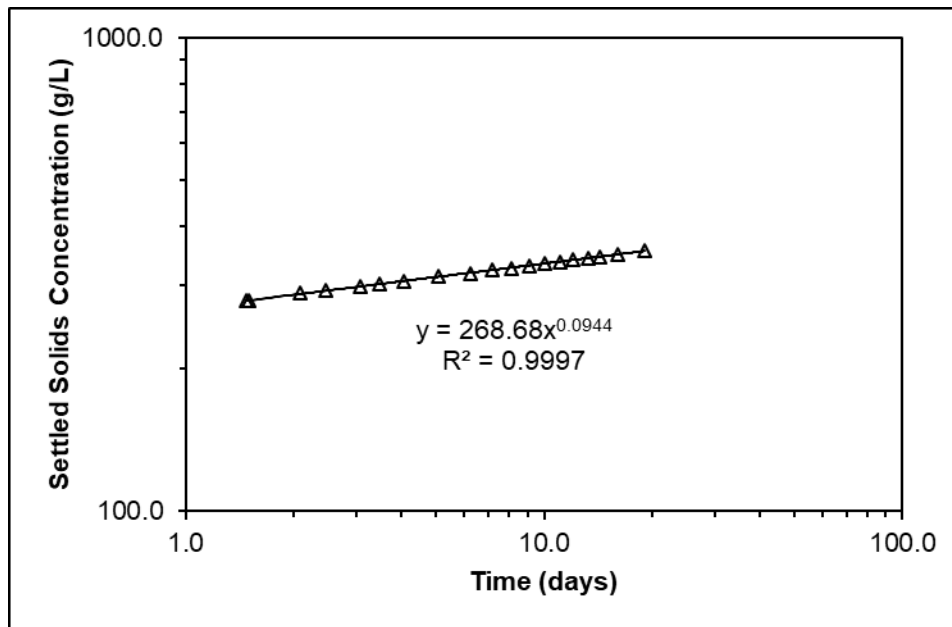
$C$  = slurry suspended solids concentration at time  $t$  (g/L)

$C_o$  = initial slurry suspended solids concentration (g/L)

$H_i$  = initial slurry height (ft)

$H_t$  = height of the interface at time  $t$  (ft)

The corresponding particulate concentration in the settled sediment as a function of time during compression settling is depicted in Figure 3. The transition from behavior dominated by zone settling to behavior best described as compression settling occurred when the calculated concentration of settled particulates was approximately 270 g/L.



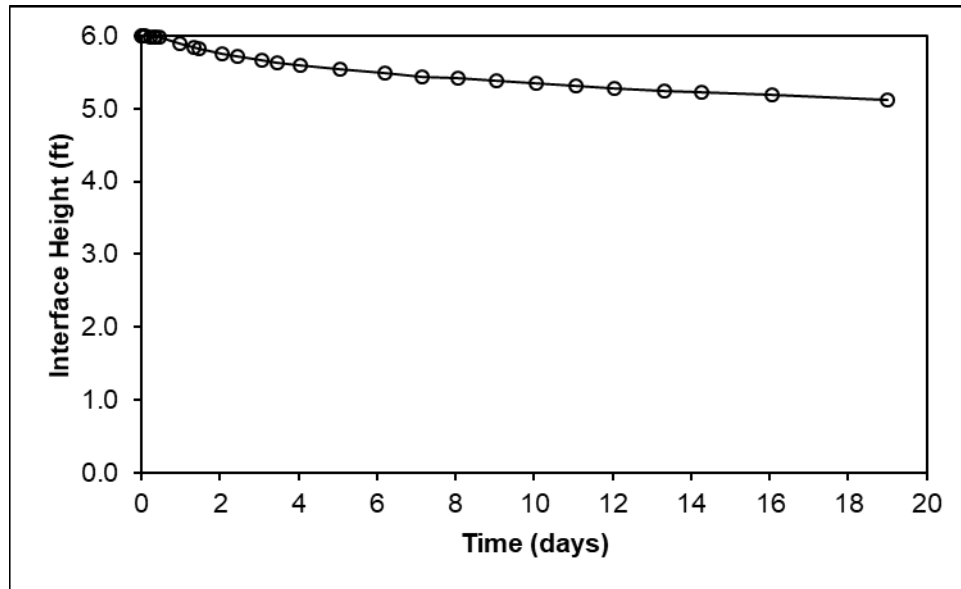
**Figure 3.** Concentration of settled solids as a function of time during compression settling portion of pilot-scale settling test A.

For analysis of flocculent settling as described in the US Army Corps of Engineers Manual No. 1110-2-5027<sup>1</sup>, water samples were collected from the clarified layer above the sediment-water interface for measurement of total suspended (TSS) following Standard Method 2450D<sup>2</sup>. The first of these samples, collected 8 hours after the start of settling when the sediment-water interface was sufficiently below the uppermost sample port (height of 5.5 ft) to allow sample collection, had a TSS concentration of 230 mg/L. TSS concentrations decreased over time and were below 25 mg/L for all sampling heights after 173 hours (7.2 days) settling. Tabulated data are provided in Table A3 in Appendix A.

### 2.3 Pilot-Scale Settling Column Test B (Target initial concentration 300 g/L)

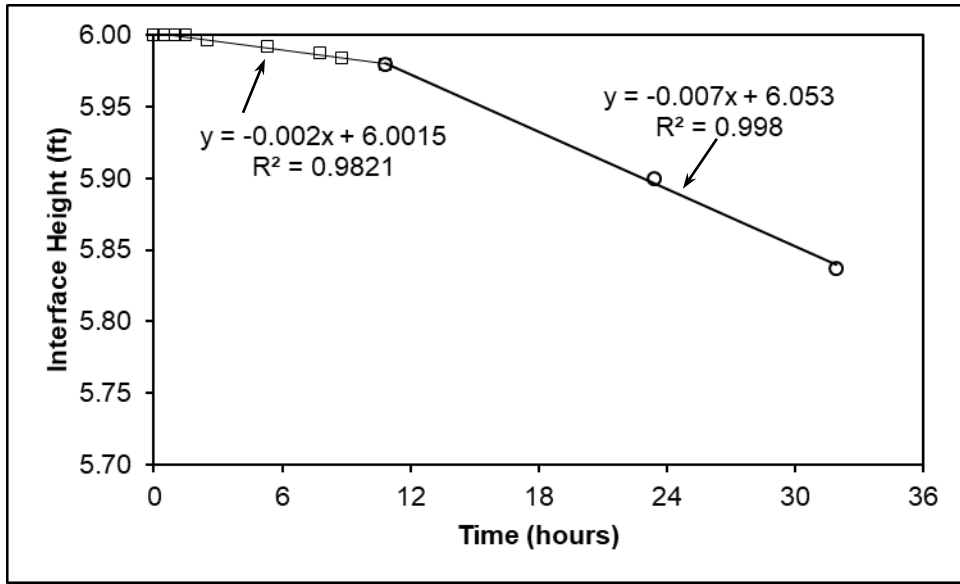
Slurry was prepared by mixing an equal amount of sediment from each of the four provided buckets with a combination of site water and tap water supplemented with a small amount of synthetic sea salts (Instant Ocean) to match the average salinity of the site water samples [salinity of 0.60 parts per thousand (ppt)]. Slurry containing the fine-grained fraction of sediments was obtained by thoroughly mixing the slurry and then allowing coarse grained materials (e.g., sand and shells), to separate by differential settling as described in the US Army Corps of Engineers Manual No. 1110-2-5027<sup>1</sup>. The fine-grained sediment slurry was transferred to a second mixing barrel, thoroughly mixed, and then loaded into a large-scale (8.0 inch ID) column while mixing with air sparging as described in the US Army Corps of Engineers Manual No. 1110-2-5027<sup>1</sup>. Solids concentrations in the slurry at the start of the settling test were measured in samples collected along the height of the column at one foot intervals (tabulated data in Table B1 in Appendix B). The average particulate concentration at the start of the settling test was 310.9 g/L.

A small but readily visible sediment-water interface was observed shortly (2.5 hours) after the start of the settling test. The height of the sediment-water interface above the bottom of the column was measured and recorded over a period lasting more than 15 days as depicted in Figure 4 (see Table B2 in Appendix B for tabulated data).



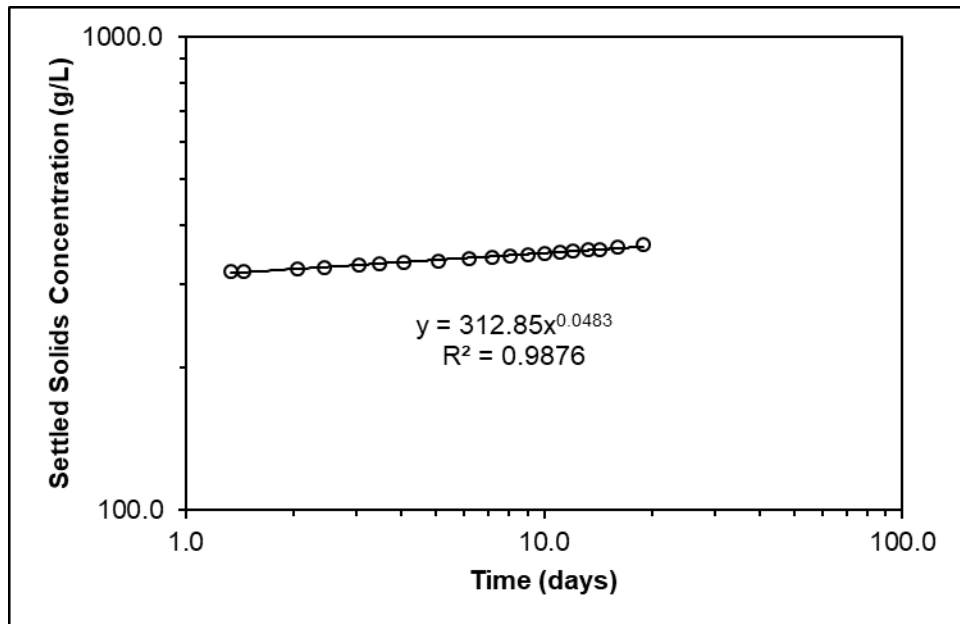
**Figure 4.** Interface height as a function of time during pilot-scale settling test B (initial particulate concentration 310.9 g/L).

Data from the first 36 hours of the settling test are depicted separately in Figure 5. As shown in the figure, there were two discrete intervals near the start of the test during which the interface height decreased in a roughly linear fashion but at different rates. A linear regression was performed separately for each of the intervals. The slope of the regression line, which corresponds to settling velocity, was 0.002 ft/hr (0.048 ft/day) during the initial interval followed by somewhat faster (but still quite slow) settling at a rate of 0.007 ft/hr (0.17 ft/day) before subsequently slowing.



**Figure 5.** Interface height as a function of time during the initial 36 hours of pilot-scale settling test B ( $C_o=310.9$  g/L).

For the portion of the settling test during which compression settling was observed, the concentration in the settled solids at each time interval was calculated as described previously (using equation 3-11 in ref. 1). The corresponding settled particulate concentration as a function of time during compression settling is depicted in Figure 6.

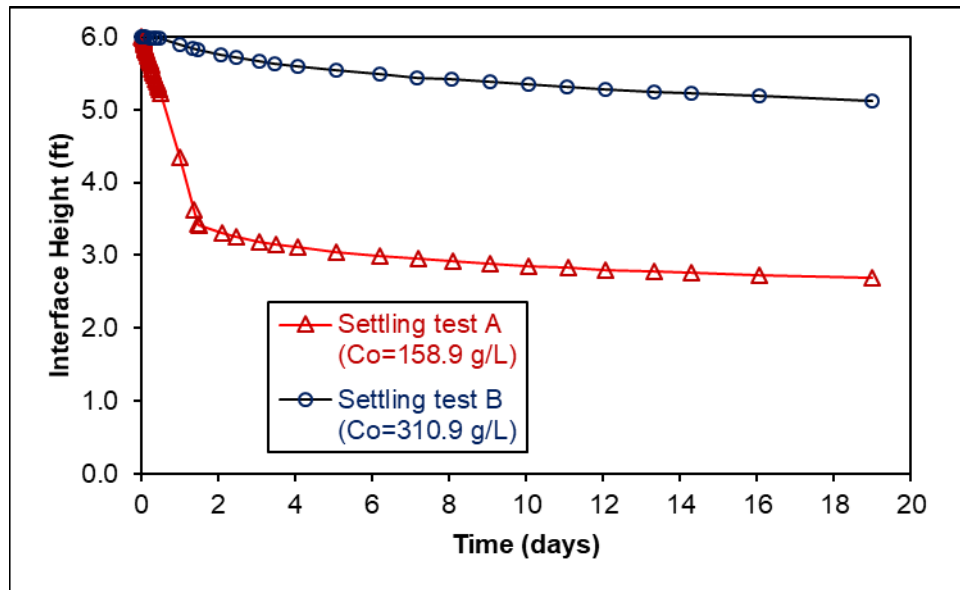


**Figure 6:** Concentration of settled solids as a function of time during the compression settling portion of pilot-scale settling test B.

When the sediment-water interface was sufficiently below the uppermost sample port (height of 5.5 ft), a water sample was collected from the well-clarified layer above the sediment-water interface for measurement of total suspended (TSS) following Standard Method 2450D<sup>2</sup>. The sample, collected 149 hours (6.2 days) after the start of settling, had a TSS concentration of <25 mg/L (Table B3 in Appendix B).

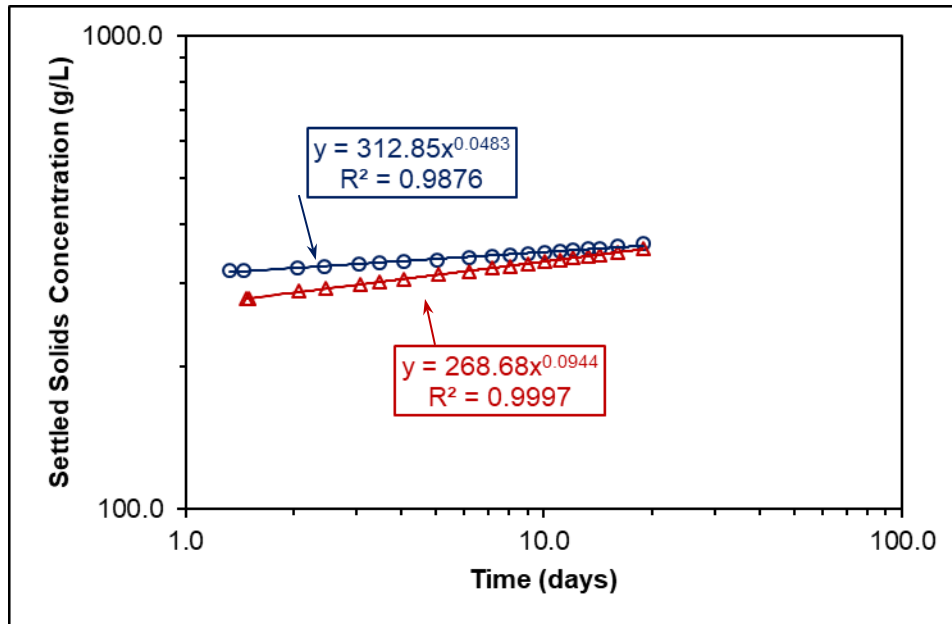
## 2.4 Data Comparisons

For comparison purposes, the overall settling observed in the two pilot-scale columns are shown together in Figure 7.



**Figure 7.** Interface heights as a function of time during the two pilot-scale settling tests.

Also for comparison purposes, the compression settling behavior of the settled solids in the two pilot-scale settling column tests is shown in Figure 8. As shown in the figure, the sediment slurries exhibited different compression settling rates towards the start of the test, but concentrations of settled particulates converged over time in the two tests. At the end of the test ( $t=19$  days), the calculated settled solids concentrations in the two settling columns were quite close, 355.3 g/L in settling column test A ( $C_o=158.9$  g/L) and 364.3 g/L in settling column test B ( $C_o=310.9$  g/L).



**Figure 8:** Concentrations of settled solids as a function of time during the compression settling portion of the pilot-scale settling tests conducted with fine-grained sediment slurry. Data and best fit line from settling test A ( $C_o=158.9$  g/L) shown in red. Data and best fit line from settling test B ( $C_o=310.9$  g/L) shown in blue.

### 3.0 References

- [1] US Army Corps of Engineers (1987) *Engineering and Design - Confined Disposal of Dredged Material*, Engineer Manual No. 1110-2-5027.
- [2] American Public Health Association (1998) *Standard Methods for the Examination of Water and Wastewater*, 20<sup>th</sup> Edition, American Water Works Association, Water Pollution Control Federation, Washington, DC.

## Appendix A

**Table A1.** Particulate concentrations measured in samples collected from side ports at the start ( $t=0$ ) of the pilot-scale settling column test designated as test A (target initial particulate concentration 160 g/L).

<b>Port height (ft)<sup>a</sup></b>	<b>Particulate Conc. (g/L)</b>
1.0	159.3
2.0	159.3
3.0	159.3
4.0	158.9
5.0	158.5
6.0	157.9
<b>Average</b>	<b>158.9</b>

<sup>a</sup> As measured from the bottom of the column

**Table A2.** Interface height as a function of time during pilot-scale column settling test A.

The height of the sediment-water interface above the bottom of the column was recorded as a function of time as summarized in the table below.

<b>Elapsed Time (hr)</b>	<b>Elapsed Time (days)</b>	<b>Solids Interface Height (ft)</b>	<b>Head height (ft)</b>	<b>Settled Solids Conc. (g/L)<sup>a</sup></b>
0.00	0.000	6.000	6.000	158.9
0.68	0.028	5.983	6.000	159.3
0.93	0.039	5.975	6.000	159.6
1.10	0.046	5.963	6.000	159.9
1.15	0.048	5.958	6.000	160.0
1.30	0.054	5.942	6.000	160.5
1.43	0.060	5.925	6.000	160.9
1.57	0.065	5.908	6.000	161.4
1.70	0.071	5.892	6.000	161.8
1.95	0.081	5.867	6.000	162.5
2.15	0.090	5.850	6.000	163.0
2.37	0.099	5.833	6.000	163.4
2.52	0.105	5.825	6.000	163.7
2.75	0.115	5.808	6.000	164.1
3.00	0.125	5.792	6.000	164.6
3.53	0.147	5.758	6.000	165.6
3.90	0.163	5.738	6.000	166.2
4.35	0.181	5.708	6.000	167.0
4.63	0.193	5.692	6.000	167.5
5.03	0.210	5.667	6.000	168.2
5.43	0.226	5.642	6.000	169.0
5.82	0.242	5.617	6.000	169.7
6.52	0.272	5.567	6.000	171.3
7.00	0.292	5.533	6.000	172.3
7.38	0.308	5.517	6.000	172.8
8.03	0.335	5.467	5.975	174.4
8.63	0.360	5.425	5.975	175.7
9.27	0.386	5.383	5.975	177.1
9.92	0.413	5.342	5.975	178.5
10.32	0.430	5.317	5.958	179.3

<sup>a</sup> Calculated using equation 3-11 in ref. 1 based on the measured particulate concentrations at t=0 and the height of the sediment-water interface at each time interval.



**Table A2.** Continued from previous page

<b>Elapsed Time (hr)</b>	<b>Elapsed Time (days)</b>	<b>Solids Interface Height (ft)</b>	<b>Head height (ft)</b>	<b>Settled Solids Conc. (g/L)<sup>a</sup></b>
10.92	0.455	5.275	5.958	180.7
11.53	0.481	5.229	5.946	182.3
23.90	0.996	4.350	5.946	219.2
32.40	1.350	3.625	5.892	263.0
35.32	1.472	3.429	5.892	278.0
35.92	1.497	3.421	5.813	278.7
49.85	2.077	3.304	5.813	288.5
59.17	2.465	3.250	5.758	293.4
73.63	3.068	3.188	5.758	299.1
83.52	3.480	3.150	5.700	302.7
97.65	4.069	3.108	5.700	306.7
121.75	5.073	3.046	5.700	313.0
148.90	6.204	2.992	5.642	318.7
172.35	7.181	2.950	5.642	323.2
193.85	8.077	2.917	5.558	326.9
217.65	9.069	2.883	5.558	330.7
241.60	10.067	2.854	5.558	334.0
265.93	11.081	2.829	5.558	337.0
289.63	12.068	2.804	5.558	340.0
319.88	13.328	2.779	5.558	343.1
343.13	14.297	2.758	5.558	345.6
385.60	16.067	2.729	5.558	349.3
456.18	19.008	2.683	5.558	355.3

<sup>a</sup> Calculated using equation 3-11 in ref. 1 based on the measured particulate concentrations at t=0 and the height of the sediment-water interface at each time interval.

**Table A3.** Total suspended solids (TSS) concentrations measured above the sediment-water interface for characterization of flocculent settling during pilot-scale column settling test A.

Sample Extraction Time (hr)	Port Height (ft) <sup>a</sup>	Head Height (ft) <sup>a</sup>	Depth of Sample Extraction (ft) <sup>b</sup>	TSS (mg/L)	% Remaining <sup>c</sup>
8.0	5.50	6.00	0.50	230	100.0
10.0	5.50	5.98	0.48	120	52.2
11.5	5.50	5.96	0.46	115	50.0
24	5.50	5.94	0.44	62	27.0
24	5.00	5.94	0.94	75	32.6
24	4.50	5.94	1.44	207	90.0
36	5.50	5.89	0.39	58	25.2
36	5.00	5.89	0.89	65	28.3
36	4.50	5.89	1.39	71	30.9
36	4.00	5.89	1.89	118	51.3
36	3.50	5.89	2.39	229	99.6
50	5.50	5.81	0.31	48	20.9
50	5.00	5.81	0.81	47	20.4
50	4.50	5.81	1.31	47	20.4
50	4.00	5.81	1.81	51	22.2
50	3.50	5.81	2.31	52	22.6
74	5.50	5.76	0.26	25	10.9
74	5.00	5.76	0.76	30	13.0
74	4.50	5.76	1.26	34	14.8
74	4.00	5.76	1.76	36	15.7
74	3.50	5.76	2.26	43	18.7
122	5.50	5.70	0.20	<25 <sup>d</sup>	<10.9
122	5.00	5.70	0.70	<25 <sup>d</sup>	<10.9
122	4.50	5.70	1.20	25	10.9
122	4.00	5.70	1.70	30	13.0
122	3.50	5.70	2.20	31	13.5

<sup>a</sup> As measured from the bottom of the column

<sup>b</sup> Relative to the top liquid level

<sup>c</sup> Relative to the TSS concentration measured at t=8 hr

<sup>d</sup> The mass of dry residue retained on the filter was less than 2.5 mg (the minimum required for an acceptable analysis). The result is reported here as <25 mg/L [calculated as the minimum residue mass required for acceptable analysis, 2.5 mg, divided by the sample volume filtered (0.10 L)].

**Table A3.** Continued from previous page

Sample Extraction Time (hr)	Port Height (ft) <sup>a</sup>	Head Height (ft) <sup>a</sup>	Depth of Sample Extraction (ft) <sup>b</sup>	TSS (mg/L)	% Remaining <sup>c</sup>
173	5.50	5.64	0.14	<25 <sup>d</sup>	<10.9
173	5.00	5.64	0.64	<25 <sup>d</sup>	<10.9
173	4.50	5.64	1.14	<25 <sup>d</sup>	<10.9
173	4.00	5.64	1.64	<25 <sup>d</sup>	<10.9
173	3.50	5.64	2.14	<25 <sup>d</sup>	<10.9
173	3.00	5.64	2.64	<25 <sup>d</sup>	<10.9

<sup>a</sup> As measured from the bottom of the column

<sup>b</sup> Relative to the top liquid level

<sup>c</sup> Relative to the TSS concentration measured at t=8 hr

<sup>d</sup> The mass of dry residue retained on the filter was less than 2.5 mg (the minimum required for an acceptable analysis). The result is reported here as <25 mg/L [calculated as the minimum residue mass required for acceptable analysis, 2.5 mg, divided by the sample volume filtered (0.10 L)].

## Appendix B

**Table B1.** Experimentally measured particulate concentrations measured in samples collected from side ports at the start ( $t=0$ ) of the pilot-scale settling column test designated as test B (target initial particulate concentration 300 g/L).

<b>Port height (ft)<sup>a</sup></b>	<b>Particulate Conc. (g/L)</b>
1.0	311.6
2.0	312.3
3.0	310.7
4.0	311.5
5.0	310.6
6.0	309.0
<b>Average</b>	<b>310.9</b>

<sup>a</sup> As measured from the bottom of the column

**Table B2.** Interface height as a function of time during pilot-scale column settling test B.

The height of the sediment-water interface above the bottom of the column was recorded as a function of time as summarized in the table below.

<b>Elapsed Time (hr)</b>	<b>Elapsed Time (days)</b>	<b>Solids Interface Height (ft)</b>	<b>Head height (ft)</b>	<b>Settled Solids Conc. (g/L)<sup>a</sup></b>
0.00	0.000	6.000	6.000	310.9
0.50	0.021	6.000	6.000	310.9
1.00	0.042	6.000	6.000	310.9
1.50	0.063	6.000	6.000	310.9
2.50	0.104	5.996	6.000	311.1
5.37	0.224	5.992	6.000	311.3
7.80	0.325	5.988	6.000	311.5
8.82	0.367	5.983	6.000	311.8
10.85	0.452	5.979	6.000	312.0
23.43	0.976	5.900	6.000	316.2
31.93	1.331	5.838	6.000	319.6
34.85	1.452	5.821	6.000	320.5
49.30	2.054	5.750	6.000	324.4
58.70	2.446	5.713	6.000	326.5
73.20	3.050	5.667	6.000	329.2
83.13	3.464	5.633	6.000	331.1
97.23	4.051	5.596	6.000	333.4
121.25	5.052	5.538	6.000	336.9
148.47	6.186	5.483	6.000	340.2
171.90	7.163	5.446	5.967	342.5
193.30	8.054	5.413	5.967	344.6
217.17	9.049	5.379	5.967	346.8
241.33	10.056	5.346	5.967	348.9
265.52	11.063	5.317	5.967	350.9
289.27	12.053	5.288	5.967	352.8
319.47	13.311	5.253	5.967	355.1
342.75	14.281	5.229	5.967	356.7
385.33	16.056	5.186	5.967	359.7
455.77	18.990	5.121	5.958	364.3

<sup>a</sup> Calculated using equation 3-11 in ref. 1 based on the measured particulate concentrations at t=0 and the height of the sediment-water interface at each time interval.

**Table B3.** Total suspended solids (TSS) concentration measured above the sediment-water interface for characterization of flocculent settling during pilot-scale column settling test B.

Sample Extraction Time (hr)	Port Height (ft) <sup>a</sup>	Head Height (ft) <sup>a</sup>	Depth of Sample Extraction (ft) <sup>b</sup>	TSS (mg/L)
149	5.50	6.00	0.50	<25 <sup>c</sup>

<sup>a</sup> As measured from the bottom of the column

<sup>b</sup> Relative to the top liquid level

<sup>c</sup> The mass of dry residue retained on the filter was less than 2.5 mg (the minimum required for an acceptable analysis). The result is reported here as <25 mg/L [calculated as the minimum residue mass required for acceptable analysis, 2.5 mg, divided by the sample volume filtered (0.10 L)].

**APPENDIX J**  
**(Low Stress Consolidation**  
**Test Report)**

### Low Stress Consolidation Test Procedure

- A composite sample of the prepared slurry (from Settling Column Test) was obtained to perform the Low Stress Consolidation Test.
- The initial moisture content, Atterberg limits, hydrometer and percent fines (-200) tests were performed on the samples according to ASTM procedures.
- Then the slurry was prepared with a pre-determined moisture content equal to approximately three times its liquid limit.
- The slurry was then placed into the consolidometer setup and the initial weight was measured.
- The load cell was lowered in order to contact the slurry sample. It was very critical to perform this task with the minimum disturbance to the sample prior to loading.
- It is also very important to commence the test as practically as possible after the slurry was placed into the ring setup.
- The incremental loading cycles with a minimum applied duration of 24 hours were as follows: 5, 10, 25, 50, 100, 200 and 400 psf.
- The final weight of the consolidated sample with the consolidometer setup and the final moisture content of the consolidated sample were measured.
- The Casagrande (or Log time) and Taylor (or Root time) methods were employed to analyze the results to determine the coefficient of consolidation,  $c_v$ .

**TABLE 1.0**

Sample ID	g/L	%M	LL	PL	PI	% Clay	%Silt	%Sand	%Org.
Sample 1	160	587.7	81	27	54	58.9	40.3	0.8	5.5
Sample 2	300	282.6	55	17	38	44.7	48.7	6.6	4.3

The properties, weights and low stress test results of sample 1 (160 g/L) are presented in the following tables.

**TABLE 2.0: Properties of Slurry Sample 1 used in Low Stress Consolidation Test**

Sample ID	Initial Water Content of Slurry (%)	Liquid Limit (LL)	Plastic Limit (PL)	Plasticity Index (PI)	Percentage of		
					Clay	Silt	Sand
Sample 1	247.9	81	27	54	58.9	40.3	0.8

**TABLE 3.0: Slurry Sample initial (before test) and final (after test) weights**

Sample ID	Initial Water Content of Slurry (%)	Initial weight of Slurry Sample (grams)	Final weight of Slurry sample (grams)	Final weight of oven dry sample ( $W_{solids}$ ) (grams)
1	247.9	93.8	60	26.9



**Sample 1**

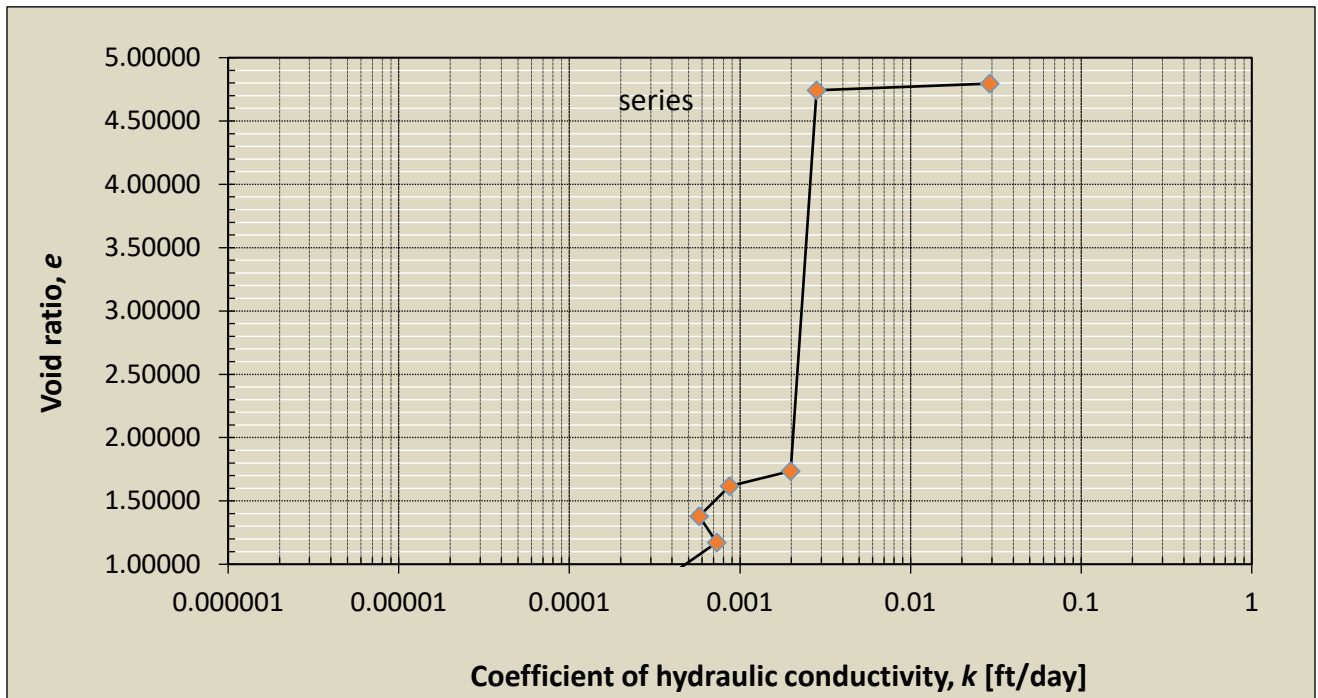
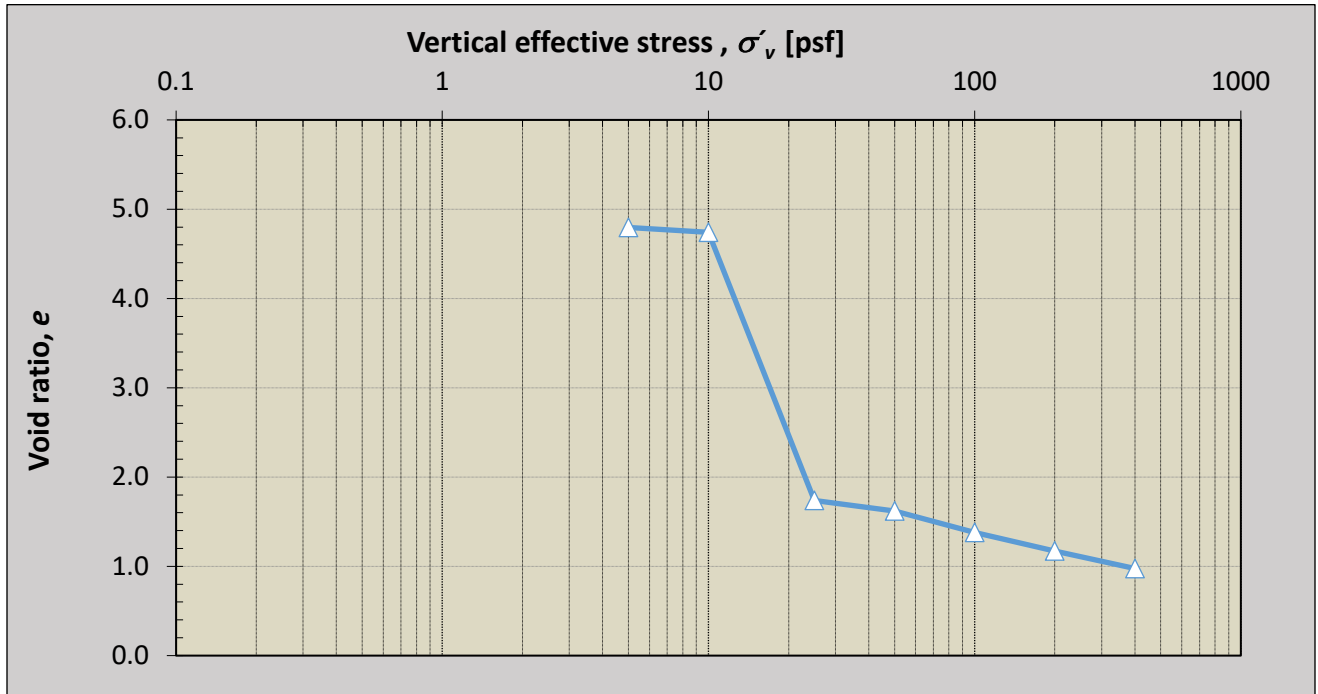
- Ring Volume = 80.4 cm<sup>3</sup>
- Initial Void Ratio (e<sub>o</sub>) of Sample =  $V_v (=V_w) / V_s = 66.9 / 13.51 = 4.95$
- Compression Index (C<sub>c</sub>) =  $(4.95 - 0.975) / \text{LOG}(400 / 5) = 2.01$

**TABLE 4.0: SAMPLE TEST RESULTS**

Applied Pressure(σ') (PSF)	Initial Height (H <sub>i</sub> )	d <sub>100</sub>	Final Height (H <sub>f</sub> )	Drainage Length (H <sub>d</sub> )	T <sub>50</sub>	T <sub>90</sub>	e <sub>100</sub>	Δe <sub>100</sub>
5	1.0000	0.026	0.9717	0.4929	150	420.25	4.79	0.155
10	0.9717	0.035	0.9645	0.4841	200	84.64	4.74	0.208
25	0.9645	0.540	0.4520	0.3541	65	94.09	1.74	3.213
50	0.4520	0.560	0.4330	0.2213	27	100	1.62	3.332
100	0.4330	0.600	0.3990	0.2080	18	14.44	1.38	3.570
200	0.3990	0.635	0.3650	0.1910	6	7.84	1.17	3.778
400	0.3650	0.668	0.3290	0.1735	4	1.56	0.98	3.975

**TABLE 5.0: SAMPLE 1 TEST RESULTS**

Applied Pressure(σ') (PSF)	C <sub>αs</sub>	C <sub>v, Log (t)</sub> (ft <sup>2</sup> / min)	K (ft / min)
5	0.0050	2.22E-06	2.0245E-05
10	0.0181	1.603E-06	1.9522E-06
25	0.0076	2.639E-06	1.3779E-06
50	0.0082	2.480E-06	6.0426E-07
100	0.0024	3.288E-06	4.0054E-07
200	0.0051	8.318E-06	5.0662E-07
400	0.0049	1.029E-05	3.1352E-07



# **APPENDIX K**

## **( Survey Report)**



Client Focused. Technology Driven.



## SURVEY REPORT

**Project:**

Breton Landbridge (West) Geotech  
Project (BS-0038)

Plaquemines Parish, Louisiana

**Prepared for:**



**Mr. Sergio Aviles, P.E., M.ASCE**

**Prepared by:  
Justin Bordelon  
Fenstermaker**

**March 3, 2021**

# **SURVEY REPORT**

Prepared for

## **APS Engineering and Testing**

in Support of Geotechnical Services on

### **Breton Landbridge (West) Geotechnical Investigation (BS-0038)**

### **Boring Stake-Out and Magnetometer Hazard Surveys**

Plaquemines Parish, Louisiana

March 3, 2021

#### **Introduction**

The Louisiana Coastal Protection and Restoration Authority (CPRA) is developing a project that will restore degraded marshes using hydraulically dredged material and bank lines along the south side of Grand Lake using mechanically excavated material from Grand Lake. This project is part of an overall, long-range, restoration goal which would create/nourish 1,000 to 2,000 acres of intermediate marsh across seven (7) miles of the Breton Basin from River aux Chenes to Bayou Terre aux Bouefs.

C.H. Fenstermaker and Associates, L.L.C. (Fenstermaker) is subcontracted to provide survey services to APS Engineering and Testing (APS) for geotechnical services. Tasks performed by Fenstermaker include stake-out of 11 proposed Cone Penetrometer (CPTs) and 14 boring locations and magnetometer surveys to clear each boring location of potential underground hazards.

#### **Location**

The project area is located in and around Grand Lake, approximately 4.5 miles to the southwest of Delacroix, LA.

#### **Pre-Planning and Survey Tasks to be Performed**

Upon receiving a Work Authorization from APS in August 2020, Fenstermaker prepared for mobilization of a field crew by uploading proposed boring locations and reference control in Trimble Business Center (TBC) software to facilitate in accurately performing the static GPS survey and boring stake-out.

BS-0038 Project Scope of Work consisted of the following survey tasks:

- Perform Real-time Kinematic (RTK) topographic surveys to stake-out boring locations.
- Perform Magnetometer Surveys to locate potential hazards at each boring location.

#### **Static GPS Survey at the Reference Control Benchmark**

Prior to the mobilization, all borings and reference monuments were setup in the TBC project file, and then uploaded into the positioning device. On Friday, August 7, 2020, a survey crew was mobilized and traveled from the Lafayette office to the project site to begin the required survey tasks. On February 23, 2021, the crew mobilized again to perform an elevation survey to verify previous boring elevations and to check existing monuments and water gauges.

Upon arriving at the project site, the Fenstermaker established a baseline survey for control using the monument labeled BS32-SM-01 and the CRMSBS-SM-01 ECC, located on an island approximately 7.5 miles north of Pointe a la Hache, LA, along the northerly shore of a lake north of Lake Batola, 4,140 feet east of Bayou Batola, 3,967 feet easterly from a Coastal Monitoring Station RSET, 100 feet westerly from the eastern shoreline of the island, and 2 feet from a fiberglass witness post.

The survey crew installed a GPS base on a two-meter fixed height tripod on both monuments. Once all necessary equipment was installed, the base unit was initialized and a static GPS sessions began. A GPS rover unit was then initialized to receive base corrections using Real-time Kinematic (RTK) for sub-centimeter positioning. The survey crew then navigated to stake-out borings at the project site in and around Grand Lake.

Upon completing the static GPS surveys, GPS log sheets and GPS raw data files were downloaded, then uploaded to Fenstermaker's ftp site. All GPS raw data files were converted to RINEX format then submitted to the NGS Online Positioning User Service (OPUS) Program<sup>1</sup> using the precise ephemeris. The OPUS Solutions for each day were tabulated, then averaged to determine the final positions. The final tabulated OPUS adjustment results can be located Section A of this report.

The published horizontal datum for OPUS is based on the Continuously Operating Reference Stations (CORS) which is NAD83 (2011) 2010.00 Epoch. The vertical datum is North American Vertical Datum of 1988 (NAVD88) using Geoid 12B.

Static GPS survey activities performed are in conformance with CPRA survey standards as specified in “*A Contractor's Guide to the Standards of Practice Required by Louisiana Department of Natural Resources, Coastal Restoration Division for Contractor's Performing GPS Surveys and Establishing GPS Derived Orthometric Heights Within the Louisiana Coastal Zone Primary GPS Network*” dated January 2016.

### **RTK Survey – Borings Stake-Out**

At the commencement of the project, the RTK base unit was initialized at a surface benchmark as described above. The base unit was then activated to begin additional static data collection while simultaneously transmitting DGPS corrections to the RTK rover. The survey crew then navigated by boat to stake-out boring locations using a fixed pole and topo foot with the RTK rover unit attached. Upon completion of the RTK survey, the data logger was downloaded and the information checked and validated.

Over a one-day period, a total of 11 CPTs and 14 borings were staked-out and the locations marked with cane poles with survey flagging and labeled with site info. Elevations were obtained at each location to facilitate in the geotechnical analysis by the APS Team. The boring stake-out was completed on December 16, 2020.

A verification survey on the water bottom elevations at the boring sites was performed on February 23, 2021. The new values have been updated and are shown in report below.

---

<sup>1</sup> The National Geodetic Survey operates the On-line Positioning User Service (OPUS) as a means to provide GPS users easier access to the National Spatial Reference System (NSRS). OPUS allows users to submit their GPS data files to NGS, where the data will be processed to determine a position using NGS computers and software. Each data file that is submitted will be processed with respect to 3 CORS sites.



**BRETON LANDBRIDGE BORINGS STAKEOUT**  
**RTK SURVEY ON FEBRUARY 23, 2021**

POINT NO	LATITUDE	LONGITUDE	ELLIPSOID HGT	NORTHING	EASTING	ELEV	DESCRIPTION	Name
BS32-SM-01	29d45'29.24806"	-89d47'02.06567"	-80.71	460856.73	3772450.53	2.59	CP_MON	BS32-SM-01
CRMSBS-SM-01 ECC	29d41'33.99205"	-89d48'26.72261"	-81.70	436994.56	3765306.08	0.84	CP_MON	CRMSBS-SM-01
220-100	29d41'32.53278"	-89d51'20.31846"	-86.309	436646.515	3749998.8	-3.73	WATERBODY	B6/C11
054-200	29d42'57.84151"	-89d50'58.06960"	-88.88	445288.51	3751849.30	-6.03	WATERBODY	B8
054-202	29d42'49.29731"	-89d50'58.64600"	-88.82	444424.85	3751809.66	-5.99	WATERBODY	B9
054-204	29d42'47.64121"	-89d50'47.06196"	-88.71	444270.81	3752833.20	-5.89	WATERBODY	B7
054-206	29d42'38.09421"	-89d50'51.99294"	-88.56	443300.87	3752410.93	-5.77	WATERBODY	B14
054-208	29d42'38.59337"	-89d51'01.88562"	-88.67	443339.99	3751538.01	-5.87	WATERBODY	B13
054-210	29d42'45.83356"	-89d51'09.30598"	-88.57	444062.83	3750874.28	-5.75	WATERBODY	B10
054-212	29d42'37.96294"	-89d51'14.71684"	-88.57	443261.69	3750407.46	-5.78	WATERBODY	B11
054-214	29d42'29.62791"	-89d51'04.84635"	-88.32	442431.05	3751288.67	-5.55	WATERBODY	B12
054-216	29d41'50.54770"	-89d51'28.32430"	-84.42	438457.02	3749269.32	-1.78	WATERBODY	C10
054-218	29d41'57.33018"	-89d51'01.87680"	-86.08	439172.20	3751592.72	-3.42	WATERBODY	C9
054-220	29d41'55.24568"	-89d50'44.41103"	-86.99	438981.61	3753135.65	-4.34	WATERBODY	B5
054-222	29d41'58.11250"	-89d50'26.10736"	-85.18	439292.17	3754745.96	-2.53	WATERBODY	B4/C8
054-224	29d42'14.16084"	-89d50'20.97732"	-86.82	440919.03	3755177.20	-4.12	WATERBODY	C7
054-226	29d42'09.70795"	-89d49'54.01289"	-85.23	440500.35	3757560.79	-2.55	WATERBODY	C6
054-228	29d42'14.80692"	-89d49'34.67169"	-84.54	441037.77	3759259.53	-1.84	WATERBODY	B3
054-230	29d42'19.18301"	-89d49'29.95286"	-83.34	441485.25	3759669.81	-0.64	WATERBODY	C5
054-232	29d42'49.22987"	-89d49'46.11558"	-86.73	444501.40	3758204.79	-3.91	WATERBODY	B2/C4
054-234	29d42'40.87719"	-89d49'36.65238"	-90.74	443668.70	3759050.25	-7.95	WATERBODY	C3
054-236	29d42'37.67183"	-89d49'12.72292"	-85.74	443372.74	3761164.44	-2.98	WATERBODY	C2
054-238	29d42'57.41631"	-89d49'00.25148"	-83.96	445381.58	3762237.69	-1.13	WATERBODY	B1
054-240	29d42'59.93451"	-89d49'00.17858"	-84.67	445636.01	3762240.75	-1.83	WATERBODY	C1



### **GPS and RTK Survey Equipment**

The equipment used for the static GPS survey consisted of a Trimble® Navigation's dual-frequency R8S GNSS GPS receiver with an internal antenna, also called base stations. A two-meter fixed height tripod was used to eliminate human error that could be introduced by miss-measurement of the GPS antenna heights. The GPS data was downloaded, processed and adjusted using Trimble Business Center (TBC) Software, Version 5.40. The Geoid12B model was used to determine the geoid separation and applied to the ellipsoid heights to determine elevation as specified in the scope.

To perform the RTK survey, a rover consisting of a Trimble® Navigation's dual-frequency R8S GNSS GPS receivers with an internal GPS antenna and a radio link was employed to transmit corrections to the rover from the base setup. A two-meter fixed height rod was used at the rover. The data was collected and stored on a Trimble® TSC3 datalogger and downloaded using TBC, Version 5.40.

### **Magnetometer Hazard Surveys**

The survey crew performed magnetometer surveys to locate hazards and existing pipelines that may exist at each boring location using a Geometrics 858-R Cesium Magnetometer. If a pipeline signal would have been detected within the immediate vicinity of staked boring location, the proposed boring location would be moved to a cleared location to avoid existing hazards. It should be noted that two anomalies were located 12.6 feet (point 11) and 44.5 feet (point 10), respectively, from the C2 staked location.



### **Conclusion**

While reasonable efforts are made to locate any pipelines and magnetic anomalies at the boring locations, the equipment used and the characteristics of pipelines themselves make it impossible to guarantee total success. Accordingly, it is incumbent upon the owners, operators and/or contractors conducting operations to use extreme caution prior to digging and recognize that hazards in addition to those detected and reported by Fenstermaker may exist within the areas of operation in spite of Fenstermaker's most diligent efforts.



The presence of debris can have an adverse impact on the success of construction activities. Louisiana (Louisiana One Call™ www.laonecall.com) maintains an information center and link between those who dig (excavators) and those who own and operate underground facilities (operators). It is advisable, and in most states, law, for the contractor to contact the center for assistance in locating and marking underground utilities.

**FINAL NOTE**

*Please be advised that the data, which was collected during the survey of this project, represents an epoch, a snapshot at the time that the survey was performed. Due to the effects of crustal motion, subsidence, upheaval, drought and other conditions which influence the physical position and stability of surface monuments, topographic features, and other structures within the Louisiana Coastal Zone, it is recommended that GPS monuments used for this project be re-observed and reprocessed on future surveys using the same reference control, if possible, for the purpose of updating the three dimensional position of the reference monuments.*

*The GPS/RTK Survey protocols performed in support of this project were in accordance with the Coastal Protection and Restoration Authority of Louisiana requirements as described in "A Contractor's Guide to the Standards of Practice Required by Louisiana Department of Natural Resources, Coastal Restoration Division for Contractor's Performing GPS Surveys and Establishing GPS Derived Orthometric Heights Within the Louisiana Coastal Zone Primary GPS Network" dated January 2016. All Static GPS were adjusted using Trimble Business Center software to determine the final positions for all reference control monuments.*



**C.H. Fenstermaker & Associates, LLC**

**Ricardo M. Johnson, PLS LA Reg. 4767**  
Director of Coastal Services, Survey & Mapping

**C. H. Fenstermaker & Associates, LLC**

135 Regency Square  
Lafayette, LA 70518  
USA

Phone: 337 237-2200  
<http://fenstermaker.com>

Project File Data		Coordinate System	
Name:	T:\2020\2202397.01\OPUS\BRETON LANDBRIDGE 02232021_STATIC.vce	Name:	United States/State Plane 1983
Size:	128 KB	Datum:	NAD 1983 (Conus)
Modified:	3/2/2021 11:19:04 AM (UTC:-6)	Zone:	Louisiana South 1702
Time zone:	Central Standard Time	Geoid:	GEOID12B (Conus)
Reference number:		Vertical datum:	NAVD88 (2011)
Description:		Calibrated site:	
Comment 1:			
Comment 2:			
Comment 3:			

## Network Adjustment Report

### Adjustment Settings

#### Set-Up Errors

##### GNSS

Error in Height of Antenna: 0.005 ft

Centering Error: 0.005 ft

#### Covariance Display

##### Horizontal:

Propagated Linear Error [E]: U.S.

Constant Term [C]: 0.000 ft

Scale on Linear Error [S]: 1.960

##### Three-Dimensional

Propagated Linear Error [E]: U.S.

Constant Term [C]: 0.000 ft

Scale on Linear Error [S]: 1.960

### Adjustment Statistics

Number of Iterations for Successful Adjustment: 2

Network Reference Factor: 1.01

Chi Square Test (95%): Passed

Precision Confidence Level: 95%

Degrees of Freedom: 105

#### Post Processed Vector Statistics

Reference Factor: 1.01

Redundancy Number: 105.00

A Priori Scalar: 0.49

### Control Coordinate Comparisons

Values shown are control coordinates minus adjusted coordinates.

--	--	--	--

Point ID	$\Delta$ Northing (US survey foot)	$\Delta$ Easting (US survey foot)	$\Delta$ Elevation (US survey foot)	$\Delta$ Height (US survey foot)
<a href="#">DSTR</a>	0.002	-0.014	?	0.052
<a href="#">GRIS</a>	0.011	-0.023	?	-0.086
<a href="#">LMCN</a>	0.006	-0.017	?	?
<a href="#">MARY</a>	0.010	-0.010	?	0.003
<a href="#">MSIN</a>	-0.026	0.006	?	0.112

### Control Point Constraints

Point ID	Type	North $\sigma$ (US survey foot)	East $\sigma$ (US survey foot)	Height $\sigma$ (US survey foot)	Elevation $\sigma$ (US survey foot)
<a href="#">BVHS</a>	Global	Fixed	Fixed	Fixed	
<a href="#">COVG</a>	Global	Fixed	Fixed	Fixed	
<a href="#">LMCN</a>	Global			Fixed	

Fixed = 0.000003(US survey foot)

### Adjusted Grid Coordinates

Point ID	Northing (US survey foot)	Northing Error (US survey foot)	Easting (US survey foot)	Easting Error (US survey foot)	Elevation (US survey foot)	Elevation Error (US survey foot)	Constraint
<a href="#">BS32-SM-01</a>	460856.733	0.005	3772450.526	0.005	2.553	0.022	
<a href="#">BVHS</a>	309482.274	?	3894798.480	?	31.382	?	LLh
<a href="#">COVG</a>	720676.126	?	3670759.090	?	73.010	?	LLh
<a href="#">CRMSBS-SM-01 ECC</a>	436994.555	0.005	3765306.065	0.004	0.843	0.021	
<a href="#">DSTR</a>	533852.055	0.005	3581993.314	0.005	24.547	0.017	
<a href="#">GRIS</a>	281033.465	0.005	3719590.197	0.005	27.176	0.017	
<a href="#">LMCN</a>	275191.077	0.006	3495143.556	0.006	31.494	?	h
<a href="#">MARY</a>	556633.089	0.004	3730298.911	0.004	10.714	0.015	
<a href="#">MSIN</a>	662973.613	0.005	3826393.872	0.004	31.612	0.018	

### Adjusted Geodetic Coordinates

Point ID	Latitude	Longitude	Height (US survey foot)	Height Error (US survey foot)	Constraint
<a href="#">BS32-SM-01</a>	N29°45'29.24806"	W89°47'02.06567"	-80.747	0.022	
<a href="#">BVHS</a>	N29°20'12.48979"	W89°24'23.01019"	-46.909	?	LLh
<a href="#">COVG</a>	N30°28'33.26970"	W90°05'43.92272"	-15.072	?	LLh
<a href="#">CRMSBS-SM-01 ECC</a>	N29°41'33.99197"	W89°48'26.72283"	-81.696	0.021	
<a href="#">DSTR</a>	N29°57'52.39560"	W90°22'56.00635"	-60.990	0.017	
<a href="#">GRIS</a>	N29°15'55.88291"	W89°57'26.26210"	-51.485	0.017	
<a href="#">LMCN</a>	N29°15'17.90411"	W90°39'40.65144"	-48.556	?	h
<a href="#">MARY</a>	N30°01'22.70954"	W89°54'46.80179"	-75.105	0.015	
<a href="#">MSIN</a>	N30°18'42.20586"	W89°36'15.50728"	-56.857	0.018	

### Adjusted ECEF Coordinates

Point ID	X (US survey foot)	X Error (US survey foot)	Y (US survey foot)	Y Error (US survey foot)	Z (US survey foot)	Z Error (US survey foot)	3D Error (US survey foot)	Constraint
<a href="#">BS32-SM-01</a>	68570.215	0.005	-18180911.178	0.019	10325154.601	0.012	0.023	

<a href="#">BVHS</a>	189142.939	?	-18255648.973	?	10191879.226	?	?	LLh
<a href="#">COVG</a>	-30096.458	?	-18050084.731	?	10550998.147	?	?	LLh
<a href="#">CRMSBS-SM-01 ECC</a>	61147.831	0.004	-18192720.919	0.018	10304515.851	0.011	0.022	
<a href="#">DSTR</a>	-121036.794	0.005	-18143274.213	0.015	10390271.318	0.010	0.019	
<a href="#">GRIS</a>	13616.890	0.005	-18269305.359	0.015	10169272.513	0.010	0.019	
<a href="#">LMCN</a>	-210876.326	?	-18269971.160	?	10165927.076	?	?	h
<a href="#">MARY</a>	27533.707	0.004	-18133023.420	0.013	10408665.669	0.009	0.016	
<a href="#">MSIN</a>	124863.916	0.004	-18079855.078	0.016	10499468.374	0.010	0.019	

### Error Ellipse Components

Point ID	Semi-major axis (US survey foot)	Semi-minor axis (US survey foot)	Azimuth
<a href="#">BS32-SM-01</a>	0.006	0.006	1°
<a href="#">CRMSBS-SM-01 ECC</a>	0.006	0.005	144°
<a href="#">DSTR</a>	0.006	0.006	168°
<a href="#">GRIS</a>	0.006	0.006	161°
<a href="#">LMCN</a>	0.007	0.007	44°
<a href="#">MARY</a>	0.005	0.005	169°
<a href="#">MSIN</a>	0.006	0.005	17°

### Adjusted GNSS Observations

#### Transformation Parameters

**Deflection in Latitude:** -0.044 sec (95%) 0.009 sec  
**Deflection in Longitude:** 0.045 sec (95%) 0.008 sec  
**Azimuth Rotation:** -0.006 sec (95%) 0.002 sec  
**Scale Factor:** 1.00000005 (95%) 0.00000001

Observation ID	Observation	A-posteriori Error	Residual	Standardized Residual	
<a href="#">BS32-SM-01 --&gt; CRMSBS-SM-01 ECC (PV2)</a>	Az.	197°26'33.6"	0.038 sec	0.062 sec	1.627
	ΔHt.	-0.956 ft	0.022 ft	0.014 ft	0.716
	Ellip Dist.	24910.332 ft	0.005 ft	-0.015 ft	-3.512
<a href="#">COVG --&gt; BS32-SM-01 (PV25)</a>	Az.	159°14'36.0"	0.004 sec	0.000 sec	0.098
	ΔHt.	-65.709 ft	0.024 ft	-0.001 ft	-0.017
	Ellip Dist.	279029.544 ft	0.006 ft	-0.027 ft	-3.338
<a href="#">DSTR --&gt; BS32-SM-01 (PV12)</a>	Az.	111°26'45.8"	0.005 sec	0.000 sec	-0.055
	ΔHt.	-19.731 ft	0.025 ft	0.005 ft	0.163
	Ellip Dist.	203980.764 ft	0.005 ft	-0.022 ft	-2.659
<a href="#">MARY --&gt; CRMSBS-SM-01 ECC (PV34)</a>	Az.	164°24'01.3"	0.008 sec	0.003 sec	0.267
	ΔHt.	-6.609 ft	0.023 ft	-0.007 ft	-0.192
	Ellip Dist.	124663.736 ft	0.005 ft	0.014 ft	2.491
<a href="#">GRIS --&gt; MARY (PV31)</a>	Az.	2°54'48.1"	0.003 sec	-0.001 sec	-0.319
	ΔHt.	-23.559 ft	0.019 ft	0.004 ft	0.260
	Ellip Dist.	275820.762 ft	0.005 ft	-0.012 ft	-2.287
<a href="#">GRIS --&gt; COVG (PV23)</a>	Az.	354°20'59.4"	0.002 sec	0.000 sec	-0.166
	ΔHt.	36.497 ft	0.020 ft	0.009 ft	0.472
	Ellip Dist.	442369.702 ft	0.005 ft	-0.013 ft	-2.222

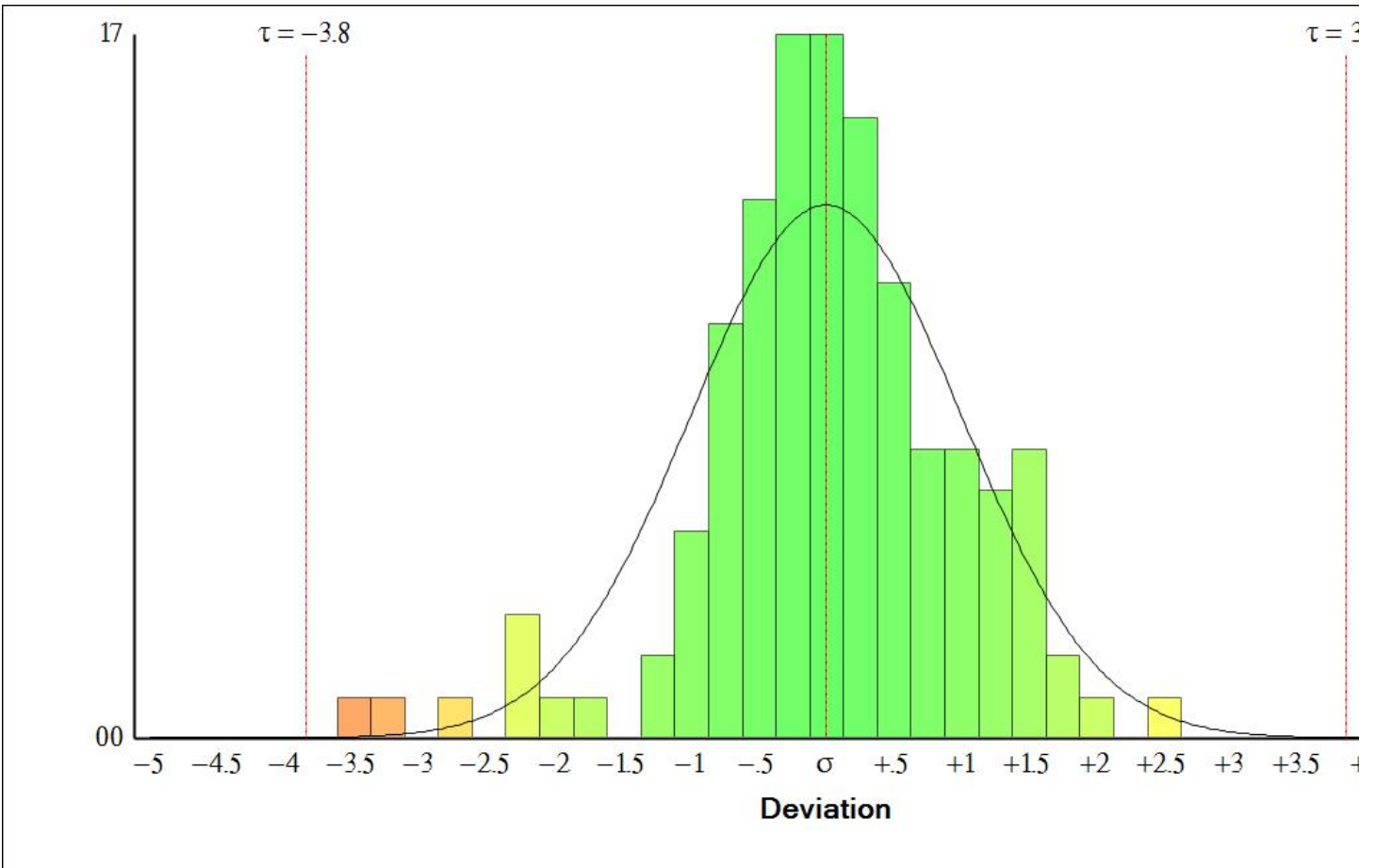
<a href="#">GRIS --&gt; BVHS (PV16)</a>	<b>Az.</b>	81°28'05.9"	0.006 sec	-0.009 sec	-2.133
	<b>ΔHt.</b>	4.620 ft	0.020 ft	-0.007 ft	-0.440
	<b>Ellip Dist.</b>	177502.923 ft	0.005 ft	0.005 ft	0.923
<a href="#">GRIS --&gt; DSTR (PV10)</a>	<b>Az.</b>	332°07'44.8"	0.003 sec	0.002 sec	0.809
	<b>ΔHt.</b>	-9.481 ft	0.020 ft	-0.005 ft	-0.256
	<b>Ellip Dist.</b>	287850.116 ft	0.005 ft	-0.012 ft	-2.103
<a href="#">LMCN --&gt; CRMSBS-SM-01 ECC (PV5)</a>	<b>Az.</b>	59°25'19.3"	0.003 sec	-0.002 sec	-0.405
	<b>ΔHt.</b>	-33.048 ft	0.022 ft	-0.038 ft	-0.982
	<b>Ellip Dist.</b>	314919.150 ft	0.005 ft	0.030 ft	2.085
<a href="#">LMCN --&gt; GRIS (PV6)</a>	<b>Az.</b>	88°50'56.1"	0.004 sec	0.006 sec	1.843
	<b>ΔHt.</b>	-2.880 ft	0.019 ft	0.010 ft	0.559
	<b>Ellip Dist.</b>	224520.730 ft	0.005 ft	-0.001 ft	-0.188
<a href="#">GRIS --&gt; MSIN (PV40)</a>	<b>Az.</b>	16°18'42.8"	0.002 sec	-0.002 sec	-1.032
	<b>ΔHt.</b>	-5.267 ft	0.019 ft	0.016 ft	0.979
	<b>Ellip Dist.</b>	396613.367 ft	0.005 ft	-0.010 ft	-1.814
<a href="#">LMCN --&gt; BVHS (PV17)</a>	<b>Az.</b>	85°26'19.6"	0.002 sec	0.000 sec	-0.105
	<b>ΔHt.</b>	1.740 ft	0.018 ft	-0.010 ft	-0.715
	<b>Ellip Dist.</b>	401123.034 ft	0.005 ft	0.008 ft	1.623
<a href="#">GRIS --&gt; BS32-SM-01 (PV7)</a>	<b>Az.</b>	17°04'11.5"	0.005 sec	-0.002 sec	-0.329
	<b>ΔHt.</b>	-29.212 ft	0.024 ft	-0.005 ft	-0.207
	<b>Ellip Dist.</b>	187438.203 ft	0.006 ft	0.012 ft	1.596
<a href="#">COVG --&gt; CRMSBS-SM-01 ECC (PV26)</a>	<b>Az.</b>	162°11'09.4"	0.003 sec	0.007 sec	1.566
	<b>ΔHt.</b>	-66.665 ft	0.023 ft	0.028 ft	0.667
	<b>Ellip Dist.</b>	299041.903 ft	0.005 ft	0.008 ft	0.812
<a href="#">LMCN --&gt; CRMSBS-SM-01 ECC (PV4)</a>	<b>Az.</b>	59°25'19.3"	0.003 sec	0.004 sec	1.183
	<b>ΔHt.</b>	-33.048 ft	0.022 ft	0.054 ft	1.557
	<b>Ellip Dist.</b>	314919.150 ft	0.005 ft	0.008 ft	0.942
<a href="#">DSTR --&gt; MARY (PV30)</a>	<b>Az.</b>	81°44'33.9"	0.006 sec	0.003 sec	0.570
	<b>ΔHt.</b>	-14.078 ft	0.019 ft	0.000 ft	-0.028
	<b>Ellip Dist.</b>	150056.206 ft	0.005 ft	0.006 ft	1.527
<a href="#">DSTR --&gt; CRMSBS-SM-01 ECC (PV13)</a>	<b>Az.</b>	118°19'36.8"	0.005 sec	0.010 sec	1.461
	<b>ΔHt.</b>	-20.687 ft	0.024 ft	0.005 ft	0.088
	<b>Ellip Dist.</b>	207342.362 ft	0.005 ft	0.013 ft	1.209
<a href="#">BS32-SM-01 --&gt; CRMSBS-SM-01 ECC (PV1)</a>	<b>Az.</b>	197°26'33.6"	0.038 sec	0.043 sec	1.410
	<b>ΔHt.</b>	-0.956 ft	0.022 ft	-0.017 ft	-0.962
	<b>Ellip Dist.</b>	24910.332 ft	0.005 ft	-0.001 ft	-0.188
<a href="#">COVG --&gt; MSIN (PV37)</a>	<b>Az.</b>	110°57'35.7"	0.006 sec	0.006 sec	1.373
	<b>ΔHt.</b>	-41.764 ft	0.018 ft	0.006 ft	0.394
	<b>Ellip Dist.</b>	165995.612 ft	0.005 ft	0.004 ft	0.857
<a href="#">LMCN --&gt; COVG (PV24)</a>	<b>Az.</b>	21°51'08.7"	0.002 sec	-0.002 sec	-1.309
	<b>ΔHt.</b>	33.618 ft	0.018 ft	0.005 ft	0.368
	<b>Ellip Dist.</b>	478875.648 ft	0.005 ft	-0.004 ft	-0.812
<a href="#">MARY --&gt; MSIN (PV36)</a>	<b>Az.</b>	42°48'45.2"	0.006 sec	-0.002 sec	-0.328
	<b>ΔHt.</b>	18.292 ft	0.018 ft	-0.009 ft	-0.659
	<b>Ellip Dist.</b>	143336.602 ft	0.005 ft	0.004 ft	1.217
<a href="#">MSIN --&gt; CRMSBS-SM-01 ECC (PV44)</a>	<b>Az.</b>	195°59'29.9"	0.004 sec	-0.002 sec	-0.303
	<b>ΔHt.</b>	-24.901 ft	0.023 ft	-0.029 ft	-0.578

	<b>Ellip Dist.</b>	234106.511 ft	0.005 ft	-0.019 ft	-1.174
<a href="#">MSIN --&gt; CRMSBS-SM-01 ECC (PV43)</a>	<b>Az.</b>	195°59'29.9"	0.004 sec	-0.003 sec	-0.627
	<b>ΔHt.</b>	-24.901 ft	0.023 ft	-0.001 ft	-0.029
	<b>Ellip Dist.</b>	234106.511 ft	0.005 ft	0.011 ft	1.163
<a href="#">DSTR --&gt; MSIN (PV39)</a>	<b>Az.</b>	62°37'36.3"	0.004 sec	0.001 sec	0.281
	<b>ΔHt.</b>	4.213 ft	0.020 ft	-0.008 ft	-0.437
	<b>Ellip Dist.</b>	276432.049 ft	0.005 ft	0.007 ft	1.133
<a href="#">LMCN --&gt; BS32-SM-01 (PV3)</a>	<b>Az.</b>	56°32'10.8"	0.003 sec	-0.003 sec	-1.109
	<b>ΔHt.</b>	-32.091 ft	0.023 ft	0.012 ft	0.453
	<b>Ellip Dist.</b>	333734.168 ft	0.006 ft	-0.003 ft	-0.423
<a href="#">BVHS --&gt; CRMSBS-SM-01 ECC (PV20)</a>	<b>Az.</b>	315°31'13.4"	0.006 sec	0.009 sec	1.021
	<b>ΔHt.</b>	-34.788 ft	0.024 ft	0.009 ft	0.205
	<b>Ellip Dist.</b>	181741.861 ft	0.005 ft	0.011 ft	0.898
<a href="#">BVHS --&gt; COVG (PV21)</a>	<b>Az.</b>	332°22'41.6"	0.002 sec	0.002 sec	1.008
	<b>ΔHt.</b>	31.877 ft	0.019 ft	0.004 ft	0.260
	<b>Ellip Dist.</b>	468293.506 ft	0.005 ft	0.001 ft	0.251
<a href="#">MARY --&gt; CRMSBS-SM-01 ECC (PV35)</a>	<b>Az.</b>	164°24'01.3"	0.008 sec	0.000 sec	0.035
	<b>ΔHt.</b>	-6.609 ft	0.023 ft	-0.009 ft	-0.213
	<b>Ellip Dist.</b>	124663.736 ft	0.005 ft	0.007 ft	0.989
<a href="#">GRIS --&gt; CRMSBS-SM-01 ECC (PV9)</a>	<b>Az.</b>	17°01'32.9"	0.006 sec	0.000 sec	0.020
	<b>ΔHt.</b>	-30.168 ft	0.024 ft	-0.046 ft	-0.901
	<b>Ellip Dist.</b>	162528.233 ft	0.005 ft	0.002 ft	0.238
<a href="#">LMCN --&gt; MSIN (PV41)</a>	<b>Az.</b>	40°50'37.2"	0.002 sec	-0.001 sec	-0.449
	<b>ΔHt.</b>	-8.147 ft	0.017 ft	-0.004 ft	-0.308
	<b>Ellip Dist.</b>	510029.067 ft	0.005 ft	0.004 ft	0.807
<a href="#">COVG --&gt; CRMSBS-SM-01 ECC (PV27)</a>	<b>Az.</b>	162°11'09.4"	0.003 sec	-0.004 sec	-0.668
	<b>ΔHt.</b>	-66.665 ft	0.023 ft	-0.033 ft	-0.778
	<b>Ellip Dist.</b>	299041.903 ft	0.005 ft	0.002 ft	0.125
<a href="#">MSIN --&gt; BS32-SM-01 (PV42)</a>	<b>Az.</b>	195°48'29.4"	0.005 sec	-0.002 sec	-0.444
	<b>ΔHt.</b>	-23.945 ft	0.024 ft	-0.004 ft	-0.122
	<b>Ellip Dist.</b>	209206.260 ft	0.006 ft	-0.006 ft	-0.743
<a href="#">LMCN --&gt; MARY (PV32)</a>	<b>Az.</b>	40°13'07.8"	0.002 sec	0.000 sec	-0.172
	<b>ΔHt.</b>	-26.438 ft	0.017 ft	-0.009 ft	-0.703
	<b>Ellip Dist.</b>	366770.082 ft	0.005 ft	0.003 ft	0.538
<a href="#">LMCN --&gt; DSTR (PV11)</a>	<b>Az.</b>	18°53'50.8"	0.003 sec	-0.002 sec	-0.696
	<b>ΔHt.</b>	-12.360 ft	0.019 ft	0.000 ft	0.016
	<b>Ellip Dist.</b>	272864.514 ft	0.005 ft	-0.003 ft	-0.481
<a href="#">DSTR --&gt; COVG (PV22)</a>	<b>Az.</b>	25°53'20.7"	0.005 sec	-0.003 sec	-0.682
	<b>ΔHt.</b>	45.978 ft	0.020 ft	-0.006 ft	-0.304
	<b>Ellip Dist.</b>	206852.697 ft	0.005 ft	0.000 ft	-0.023
<a href="#">BVHS --&gt; MARY (PV29)</a>	<b>Az.</b>	327°18'53.0"	0.003 sec	0.002 sec	0.631
	<b>ΔHt.</b>	-28.179 ft	0.018 ft	-0.007 ft	-0.453
	<b>Ellip Dist.</b>	296905.583 ft	0.005 ft	0.001 ft	0.160
<a href="#">BVHS --&gt; MSIN (PV38)</a>	<b>Az.</b>	350°00'39.5"	0.003 sec	0.001 sec	0.597
	<b>ΔHt.</b>	-9.887 ft	0.019 ft	-0.004 ft	-0.241
	<b>Ellip Dist.</b>	360069.754 ft	0.005 ft	0.001 ft	0.290
<a href="#">DSTR --&gt; BVHS (PV15)</a>	<b>Az.</b>	126°07'42.9"	0.003 sec	0.001 sec	0.382

	<b>ΔHt.</b>	14.100 ft	0.020 ft	0.013 ft	0.593
	<b>Ellip Dist.</b>	384972.614 ft	0.005 ft	0.003 ft	0.539
<a href="#">DSTR --&gt; CRMSBS-SM-01 ECC (PV14)</a>	<b>Az.</b>	118°19'36.8"	0.005 sec	0.001 sec	0.109
	<b>ΔHt.</b>	-20.687 ft	0.024 ft	-0.028 ft	-0.584
	<b>Ellip Dist.</b>	207342.362 ft	0.005 ft	0.002 ft	0.145
<a href="#">MARY --&gt; BS32-SM-01 (PV33)</a>	<b>Az.</b>	156°57'20.6"	0.010 sec	-0.006 sec	-0.574
	<b>ΔHt.</b>	-5.653 ft	0.023 ft	-0.003 ft	-0.107
	<b>Ellip Dist.</b>	104649.102 ft	0.005 ft	0.001 ft	0.127
<a href="#">BVHS --&gt; CRMSBS-SM-01 ECC (PV19)</a>	<b>Az.</b>	315°31'13.4"	0.006 sec	-0.004 sec	-0.545
	<b>ΔHt.</b>	-34.788 ft	0.024 ft	-0.011 ft	-0.264
	<b>Ellip Dist.</b>	181741.861 ft	0.005 ft	-0.001 ft	-0.152
<a href="#">GRIS --&gt; CRMSBS-SM-01 ECC (PV8)</a>	<b>Az.</b>	17°01'32.9"	0.006 sec	-0.004 sec	-0.455
	<b>ΔHt.</b>	-30.168 ft	0.024 ft	-0.002 ft	-0.039
	<b>Ellip Dist.</b>	162528.233 ft	0.005 ft	0.003 ft	0.378
<a href="#">COVG --&gt; MARY (PV28)</a>	<b>Az.</b>	160°40'11.9"	0.005 sec	0.001 sec	0.225
	<b>ΔHt.</b>	-60.056 ft	0.018 ft	0.000 ft	0.028
	<b>Ellip Dist.</b>	174524.781 ft	0.005 ft	0.000 ft	0.100

### Histogram of Standardized Residuals

Critical Tau Value: 3.8  
 Observations Failing the Tau Test: 0



## Covariance Terms

From Point	To Point		Components	A-posteriori Error	Horiz. Precision (Ratio)	3D Precision (Ratio)
<a href="#">BS32-SM-01</a>	<a href="#">COVG</a>	Az.	339°23'58.9"	0.004 sec	1 : 54928859	1 : 54901277
		ΔHt.	65.675 ft	0.022 ft		
		ΔElev.	70.457 ft	0.022 ft		
		Ellip Dist.	279029.557 ft	0.005 ft		
<a href="#">BS32-SM-01</a>	<a href="#">DSTR</a>	Az.	291°44'38.2"	0.006 sec	1 : 35132200	1 : 35137631
		ΔHt.	19.756 ft	0.027 ft		
		ΔElev.	21.994 ft	0.027 ft		
		Ellip Dist.	203980.775 ft	0.006 ft		
<a href="#">BS32-SM-01</a>	<a href="#">GRIS</a>	Az.	197°09'19.0"	0.006 sec	1 : 31683739	1 : 31677645
		ΔHt.	29.262 ft	0.025 ft		
		ΔElev.	24.623 ft	0.025 ft		
		Ellip Dist.	187438.212 ft	0.006 ft		
<a href="#">BS32-SM-01</a>	<a href="#">LMCN</a>	Az.	236°58'06.5"	0.004 sec	1 : 49814316	1 : 49840872
		ΔHt.	32.191 ft	0.022 ft		
		ΔElev.	28.941 ft	0.022 ft		
		Ellip Dist.	333734.185 ft	0.007 ft		
<a href="#">BS32-SM-01</a>	<a href="#">MARY</a>	Az.	337°01'12.2"	0.010 sec	1 : 20212025	1 : 20192272
		ΔHt.	5.642 ft	0.024 ft		
		ΔElev.	8.161 ft	0.024 ft		
		Ellip Dist.	104649.107 ft	0.005 ft		
<a href="#">BS32-SM-01</a>	<a href="#">MSIN</a>	Az.	15°43'05.8"	0.005 sec	1 : 34358436	1 : 34341756
		ΔHt.	23.890 ft	0.025 ft		
		ΔElev.	29.059 ft	0.025 ft		
		Ellip Dist.	209206.270 ft	0.006 ft		
<a href="#">BVHS</a>	<a href="#">COVG</a>	Az.	332°22'41.6"	0.000 sec	1 : 0	1 : 0
		ΔHt.	31.837 ft	0.000 ft		
		ΔElev.	41.628 ft	0.000 ft		
		Ellip Dist.	468293.530 ft	0.000 ft		
<a href="#">BVHS</a>	<a href="#">MARY</a>	Az.	327°18'53.0"	0.003 sec	1 : 70615474	1 : 70527857
		ΔHt.	-28.196 ft	0.015 ft		
		ΔElev.	-20.669 ft	0.015 ft		
		Ellip Dist.	296905.597 ft	0.004 ft		
<a href="#">BVHS</a>	<a href="#">MSIN</a>	Az.	350°00'39.5"	0.002 sec	1 : 79466742	1 : 79368482
		ΔHt.	-9.948 ft	0.018 ft		
		ΔElev.	0.229 ft	0.018 ft		
		Ellip Dist.	360069.772 ft	0.005 ft		
<a href="#">COVG</a>	<a href="#">MARY</a>	Az.	160°40'11.9"	0.004 sec	1 : 41019625	1 : 41001406
		ΔHt.	-60.033 ft	0.015 ft		
		ΔElev.	-62.296 ft	0.015 ft		
		Ellip Dist.	174524.790 ft	0.004 ft		
<a href="#">COVG</a>	<a href="#">MSIN</a>	Az.	110°57'35.7"	0.006 sec	1 : 39682914	1 : 39674853
		ΔHt.	-41.785 ft	0.018 ft		
		ΔElev.	-41.398 ft	0.018 ft		
		Ellip Dist.	165995.620 ft	0.004 ft		
<a href="#">CRMSBS-SM-01 ECC</a>	<a href="#">BS32-SM-01</a>	Az.	17°25'51.6"	0.038 sec	1 : 5299557	1 : 5296872
		ΔHt.	0.949 ft	0.022 ft		
		ΔElev.	1.710 ft	0.022 ft		
		Ellip Dist.	24910.333 ft	0.005 ft		



<a href="#">CRMSBS-SM-01 ECC</a>	<a href="#">BVHS</a>	<b>Az.</b>	135°19'22.2"	0.005 sec	1 : 39170242	1 : 39160887
		<b>ΔHt.</b>	34.787 ft	0.021 ft		
		<b>ΔElev.</b>	30.539 ft	0.021 ft		
		<b>Ellip Dist.</b>	181741.870 ft	0.005 ft		
<a href="#">CRMSBS-SM-01 ECC</a>	<a href="#">COVG</a>	<b>Az.</b>	342°19'49.4"	0.003 sec	1 : 64724942	1 : 64755416
		<b>ΔHt.</b>	66.624 ft	0.021 ft		
		<b>ΔElev.</b>	72.167 ft	0.021 ft		
		<b>Ellip Dist.</b>	299041.918 ft	0.005 ft		
<a href="#">CRMSBS-SM-01 ECC</a>	<a href="#">DSTR</a>	<b>Az.</b>	298°36'46.0"	0.005 sec	1 : 37275402	1 : 37281542
		<b>ΔHt.</b>	20.706 ft	0.026 ft		
		<b>ΔElev.</b>	23.704 ft	0.026 ft		
		<b>Ellip Dist.</b>	207342.372 ft	0.006 ft		
<a href="#">CRMSBS-SM-01 ECC</a>	<a href="#">GRIS</a>	<b>Az.</b>	197°05'58.4"	0.006 sec	1 : 30529361	1 : 30520609
		<b>ΔHt.</b>	30.211 ft	0.025 ft		
		<b>ΔElev.</b>	26.333 ft	0.025 ft		
		<b>Ellip Dist.</b>	162528.241 ft	0.005 ft		
<a href="#">CRMSBS-SM-01 ECC</a>	<a href="#">LMCN</a>	<b>Az.</b>	239°50'31.8"	0.004 sec	1 : 50370317	1 : 50380333
		<b>ΔHt.</b>	33.140 ft	0.021 ft		
		<b>ΔElev.</b>	30.651 ft	0.021 ft		
		<b>Ellip Dist.</b>	314919.166 ft	0.006 ft		
<a href="#">CRMSBS-SM-01 ECC</a>	<a href="#">MARY</a>	<b>Az.</b>	344°27'10.6"	0.008 sec	1 : 25925170	1 : 25915695
		<b>ΔHt.</b>	6.591 ft	0.023 ft		
		<b>ΔElev.</b>	9.871 ft	0.023 ft		
		<b>Ellip Dist.</b>	124663.742 ft	0.005 ft		
<a href="#">CRMSBS-SM-01 ECC</a>	<a href="#">MSIN</a>	<b>Az.</b>	15°53'24.2"	0.005 sec	1 : 41041786	1 : 41029817
		<b>ΔHt.</b>	24.839 ft	0.025 ft		
		<b>ΔElev.</b>	30.769 ft	0.025 ft		
		<b>Ellip Dist.</b>	234106.522 ft	0.006 ft		
<a href="#">DSTR</a>	<a href="#">BVHS</a>	<b>Az.</b>	126°07'42.9"	0.003 sec	1 : 79744037	1 : 79690576
		<b>ΔHt.</b>	14.081 ft	0.017 ft		
		<b>ΔElev.</b>	6.835 ft	0.017 ft		
		<b>Ellip Dist.</b>	384972.633 ft	0.005 ft		
<a href="#">DSTR</a>	<a href="#">COVG</a>	<b>Az.</b>	25°53'20.7"	0.005 sec	1 : 42605747	1 : 42632727
		<b>ΔHt.</b>	45.918 ft	0.017 ft		
		<b>ΔElev.</b>	48.463 ft	0.017 ft		
		<b>Ellip Dist.</b>	206852.708 ft	0.005 ft		
<a href="#">DSTR</a>	<a href="#">MARY</a>	<b>Az.</b>	81°44'33.9"	0.007 sec	1 : 31313718	1 : 31320493
		<b>ΔHt.</b>	-14.115 ft	0.020 ft		
		<b>ΔElev.</b>	-13.834 ft	0.020 ft		
		<b>Ellip Dist.</b>	150056.214 ft	0.005 ft		
<a href="#">DSTR</a>	<a href="#">MSIN</a>	<b>Az.</b>	62°37'36.3"	0.004 sec	1 : 48184814	1 : 48204505
		<b>ΔHt.</b>	4.133 ft	0.023 ft		
		<b>ΔElev.</b>	7.064 ft	0.023 ft		
		<b>Ellip Dist.</b>	276432.063 ft	0.006 ft		
<a href="#">GRIS</a>	<a href="#">BVHS</a>	<b>Az.</b>	81°28'05.9"	0.006 sec	1 : 36339926	1 : 36332429
		<b>ΔHt.</b>	4.576 ft	0.017 ft		
		<b>ΔElev.</b>	4.207 ft	0.017 ft		
		<b>Ellip Dist.</b>	177502.932 ft	0.005 ft		
<a href="#">GRIS</a>	<a href="#">COVG</a>	<b>Az.</b>	354°20'59.4"	0.002 sec	1 : 86787828	1 : 86807172
		<b>ΔHt.</b>	36.413 ft	0.017 ft		
		<b>ΔElev.</b>	45.834 ft	0.017 ft		
		<b>Ellip Dist.</b>	442369.724 ft	0.005 ft		

<a href="#">GRIS</a>	<a href="#">DSTR</a>	<b>Az.</b>	332°07'44.8"	0.004 sec	1 : 49244374	1 : 49216898
		<b>ΔHt.</b>	-9.505 ft	0.023 ft		
		<b>ΔElev.</b>	-2.629 ft	0.023 ft		
		<b>Ellip Dist.</b>	287850.131 ft	0.006 ft		
<a href="#">GRIS</a>	<a href="#">MARY</a>	<b>Az.</b>	2°54'48.1"	0.004 sec	1 : 48213298	1 : 48200306
		<b>ΔHt.</b>	-23.620 ft	0.021 ft		
		<b>ΔElev.</b>	-16.462 ft	0.021 ft		
		<b>Ellip Dist.</b>	275820.776 ft	0.006 ft		
<a href="#">GRIS</a>	<a href="#">MSIN</a>	<b>Az.</b>	16°18'42.8"	0.003 sec	1 : 60045993	1 : 60037811
		<b>ΔHt.</b>	-5.372 ft	0.024 ft		
		<b>ΔElev.</b>	4.436 ft	0.024 ft		
		<b>Ellip Dist.</b>	396613.388 ft	0.007 ft		
<a href="#">LMCN</a>	<a href="#">BVHS</a>	<b>Az.</b>	85°26'19.6"	0.003 sec	1 : 70119784	1 : 70136681
		<b>ΔHt.</b>	1.647 ft	0.000 ft		
		<b>ΔElev.</b>	-0.111 ft	0.000 ft		
		<b>Ellip Dist.</b>	401123.054 ft	0.006 ft		
<a href="#">LMCN</a>	<a href="#">COVG</a>	<b>Az.</b>	21°51'08.7"	0.002 sec	1 : 82781128	1 : 82767389
		<b>ΔHt.</b>	33.484 ft	0.000 ft		
		<b>ΔElev.</b>	41.516 ft	0.000 ft		
		<b>Ellip Dist.</b>	478875.672 ft	0.006 ft		
<a href="#">LMCN</a>	<a href="#">DSTR</a>	<b>Az.</b>	18°53'50.8"	0.004 sec	1 : 46697990	1 : 46677182
		<b>ΔHt.</b>	-12.434 ft	0.017 ft		
		<b>ΔElev.</b>	-6.947 ft	0.017 ft		
		<b>Ellip Dist.</b>	272864.528 ft	0.006 ft		
<a href="#">LMCN</a>	<a href="#">GRIS</a>	<b>Az.</b>	88°50'56.1"	0.005 sec	1 : 41682851	1 : 41710040
		<b>ΔHt.</b>	-2.929 ft	0.017 ft		
		<b>ΔElev.</b>	-4.318 ft	0.017 ft		
		<b>Ellip Dist.</b>	224520.741 ft	0.005 ft		
<a href="#">LMCN</a>	<a href="#">MARY</a>	<b>Az.</b>	40°13'07.8"	0.003 sec	1 : 58342505	1 : 58339875
		<b>ΔHt.</b>	-26.549 ft	0.015 ft		
		<b>ΔElev.</b>	-20.780 ft	0.015 ft		
		<b>Ellip Dist.</b>	366770.101 ft	0.006 ft		
<a href="#">LMCN</a>	<a href="#">MSIN</a>	<b>Az.</b>	40°50'37.2"	0.003 sec	1 : 68278358	1 : 68275704
		<b>ΔHt.</b>	-8.301 ft	0.018 ft		
		<b>ΔElev.</b>	0.118 ft	0.018 ft		
		<b>Ellip Dist.</b>	510029.094 ft	0.007 ft		
<a href="#">MARY</a>	<a href="#">MSIN</a>	<b>Az.</b>	42°48'45.2"	0.007 sec	1 : 29480144	1 : 29502273
		<b>ΔHt.</b>	18.248 ft	0.019 ft		
		<b>ΔElev.</b>	20.898 ft	0.019 ft		
		<b>Ellip Dist.</b>	143336.609 ft	0.005 ft		

Date: 3/2/2021 11:24:51 AM

Project: T:\2020\2202397.01\OPUS\BRETON  
LANDBRIDGE 02232021\_STATIC.vce

Trimble Business Center