Professional Service Industries, Inc.
724 Central Avenue
Jefferson, Louisiana 70121
Phone: (504) 733-9411

February 3, 2021

Coastal Protection and Restoration Authority (CPRA)
150 Terrace Avenue
Baton Rouge, Louisiana 70802

Attn: Ms. Renee Bennett, P.M.P.
Email: Renee.S.Bennett@la.gov

Cc: Ms. Morgan Barranco
Email: Morgan.Barranco@la.gov

Re: **Geotechnical Engineering Services Report**
Long Point Bayou Marsh Creation Project (CS-0085)
Cameron Parish, LA
PSI Project No. 02541211-1

Dear Ms. Bennett and Ms. Barranco:

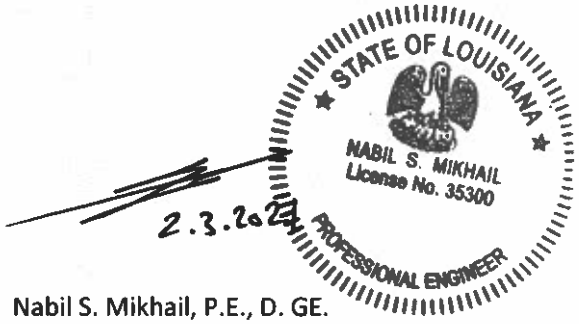
Professional Service Industries, Inc. (PSI), an Intertek company, is pleased to submit our Geotechnical Services Report for the above-referenced project. This report presents the engineering analyses and recommendations for the Long Point Bayou Marsh Creation Project (CS-0085). This report also includes the discussion regarding findings from our geotechnical investigation presented in our Data Report dated September 17, 2020.

If you have any questions pertaining to this report, please contact our office at (504) 733-9411. PSI would be pleased to continue providing geotechnical and construction material testing services throughout the construction of the project, and we look forward to working with you and your organization on this and future projects.

Respectfully submitted,

PROFESSIONAL SERVICE INDUSTRIES, INC.

Prasoon Tiwari, P.E.(TX)
Geotechnical Department Manager



Nabil S. Mikhail, P.E., D. GE.
Chief Engineer

GEOTECHNICAL ENGINEERING SERVICES REPORT

LONG POINT BAYOU MARSH CREATION PROJECT (CS-0085)
CAMERON PARISH, LA

PSI PROJECT NO. 02541211-1

PREPARED FOR

COASTAL PROTECTION AND RESTORATION AUTHORITY (CPRA)
150 TERRACE AVENUE
BATON ROUGE, LA 70802

February 3, 2021

BY

PROFESSIONAL SERVICE INDUSTRIES, INC.
724 CENTRAL AVENUE
JEFFERSON, LOUISIANA 70121
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PROJECT INFORMATION

PROJECT AUTHORIZATION

Professional Service Industries, Inc. (PSI), an Intertek company, has completed the engineering analyses and recommendations portions of a geotechnical investigation for the proposed Long Point Bayou Marsh Creation Project (CS-0085) in Cameron Parish, Louisiana. Our scope of services is outlined in PSI Proposal 0286-298563 Rev. 5, dated April 6, 2020. Our geotechnical services were authorized by Mr. Jerry Carroll, P.E., Lafayette Regional Operations Manager with CPRA, by issuing a Notice to Proceed as Task #2 dated April 6, 2020 under our existing Contract No. 4400015386. A Final Data Report including fieldwork and laboratory test results was submitted on September 17, 2020 and is included in the Appendix attached to this report.

PROJECT DESCRIPTION

Project information was provided to PSI by Ms. Renee Bennett, P.M.P., through an email correspondence dated December 19, 2019. The project information was discussed in detail over a follow up call on January 3, 2020 and a revised scope of services was provided to PSI on January 3, 2020. The project information included scope of services for geotechnical investigation and engineering services for Long Point Bayou Marsh Creation Project (CS-0085) in Cameron Parish, Louisiana.

Based on provided information, PSI understands that approximately 392 acres of marsh will be created using borrow material from the Calcasieu Ship Channel. The fill site will be formed by constructing earthen containment dikes around the boundaries of the marsh creation area where needed. The marsh creation fill site will also be planted with wetland grasses to accelerate plant colonization, stabilize new sediments, and improve habitat. The borrow material for this project site is planned to be dredged from the Calcasieu Ship Channel area between Mile markers 5 and 17.

SITE LOCATION AND DESCRIPTION

The CS-0085 project area is located within CWPPRA Planning Region 4, Calcasieu/Sabine Basin, Cameron Parish. It is situated south of Hackberry, north of Sabine National Wildlife Refuge, east of Highway LA 27 and west of the Calcasieu Ship Channel. The water depth of approximately one (1) to three (3) feet was recorded in the marsh area during our field operations.

Table1: Centerline Coordinates of the CS-0085 Project Area

Geographic	
Latitude (DMS)	**Longitude (DMS)**
29°55’19.6” N	93°21’38.54” W

The approximate site location is shown on the Site Vicinity Map included in the Appendix A, which is based on Appendix B, Proposed Soil Sampling Layout and Permit Drawings of CPRA Scoping document.

Figure.1: Project Site Location

Figure.2: Airboat Mounted Drill rig

Prior to mobilizing the drilling equipment to perform the soil borings/CPT's in the marsh creation area and borrow area, Chustz surveying, LLC performed survey positioning and magnetometer survey at each boring/CPT location in the marsh area and borrow area, as per CPRA guidelines. A detailed report was included in our Final Data Report dated September 17, 2020.

TOPOGRAPHIC SURVEY

The topographic survey information was provided by CPRA to PSI on August 10,2020. Inundation levels and Tidal datum are presented below:

Table 2. Inundation Levels

Inundation Levels	
% inundated	**Marsh Elevation (ft., NAVD88 Geoid 18)**
1%	2.02
10%	1.36
20%	1.11
30%	0.94
40%	0.79
50%	0.66
60%	0.51
65%	0.43
70%	0.35
80%	0.14
90%	-0.15

Table 3. Tidal Datum

Tidal Datum Entire Period of Record 5/31/2015 - 5/31/2020 (ft., NAVD88 Geoid 18)	
	2020
Mean High Water (MHW)	1.05
Mean Low Water (MLW)	0.06

A water sample from the Calcasieu River Ship Channel area was collected to obtain the salinity of the dredging site water. The salinity of dredging site water was calculated about 20 g/l. It is understood that the proposed marsh area has been identified as saline marsh. Optimal marsh inundation ranges are presented in the table below:

Table 4. Optimal Marsh Inundation Ranges within the Louisiana Coastal Zone

Optimal Marsh Inundation Ranges	
Marsh Types	**Optimal Inundation Ranges**
Fresh	10%-90%
Intermediate	10%-90%
Brackish	10%-65%
Saline	20%-80%

Tidal Datum and Inundation levels for 20 years are presented in the figure below:

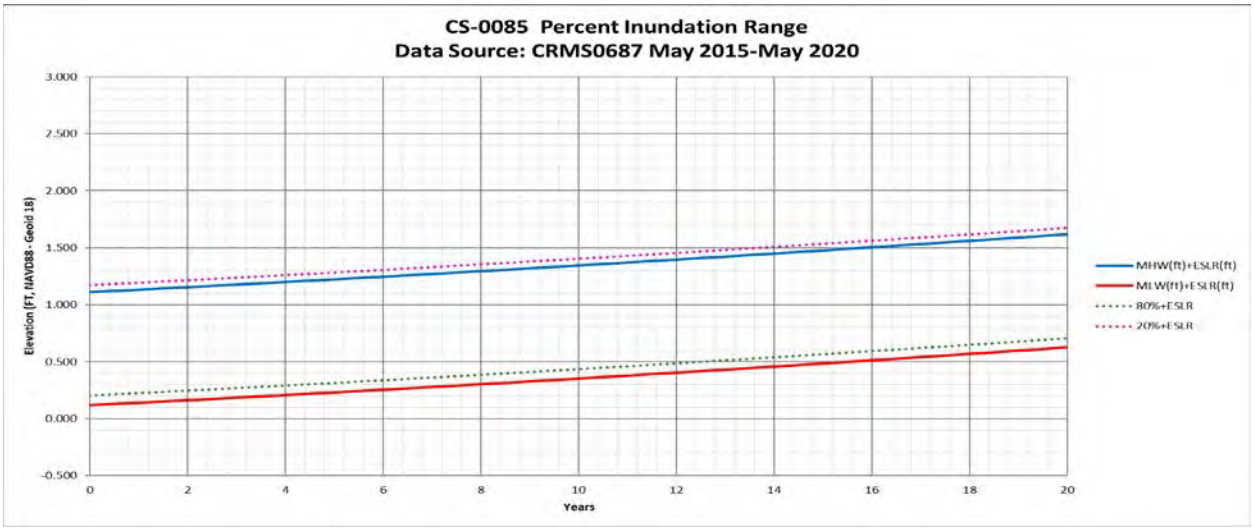


Figure 3: Tidal Datum and Inundation levels for 20 years

Subsidence:

For CS-0085 project, subsidence is estimated at 4.3 mm/yr (Polygon 1), as provided in the 2012 Master Plan that was furnished to us by CPRA (see below).

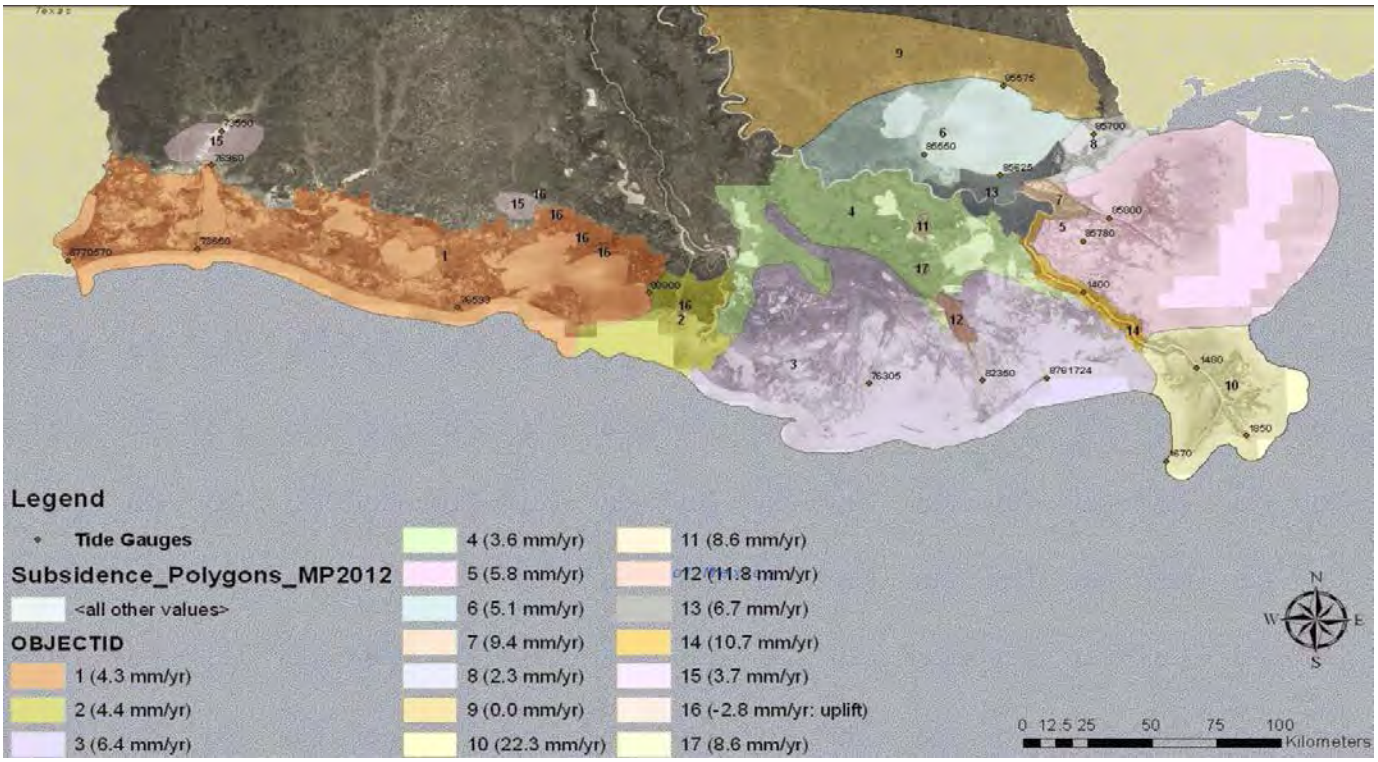


Figure.4: Subsidence Plan

MARSH AREA SUBSURFACE CONDITIONS

Based on the field observations, CPT soundings and results of the geotechnical laboratory testing, the soils were classified and boring logs and CPT sounding plots were developed and presented in our Final Data Report dated September 17, 2020.

General Stratigraphy

Although the subsurface conditions encountered at the boring locations and Cone Penetration test locations in the marsh creation area are generally consistent in terms of geotechnical index properties, stress history and undrained shear strength profiles, the data do exhibit some regional variability within the project area. In general, the soil profile encountered within the project area can be characterized as consisting of 10 to 12 feet of soft clay and organic clay underlain by medium to stiff sandy/silty lean clay (CL), and loose to dense clayey/silty sand (SC) down to about 20 feet. This is typically underlain by clayey sand, sand, silt, sandy silt to about the 30-feet depth. A detailed geotechnical characterization of the site, along with supporting field exploration and laboratory testing results, is documented in the Final Data Report dated September 17, 2020. Individual field and laboratory test results are summarized in Appendix B of the data report.

Survey

The survey information for the soil data in the Final Data Report was based on NAVD88 GEOID12B datum and the topographic survey information provided by CPRA was based on NAVD88 GEOID18 datum. To establish consistency, the survey information based on NAVD88 GEOID12B was converted to NAVD88 GEOID18 in accordance with the following:

0 ft NAVD88 GEOID12B = -0.14 ft NAVD88 GEOID18

Therefore, all elevations mentioned in this report are based on NAVD88 GEOID18 datum only.

SHIP CHANNEL FOR DREDGED MATERIALS

It is our understanding that the borrowed materials will be dredged from the Calcasieu Ship Channel between Mile markers 5 and 17. Based on the soil data obtained from borings in the ship channel area, the borrow material mainly consists of clays to about an elevation of -45 (ft., NAVD88 GEOID18), the maximum depth allowed for dredging in the channel.

ENGINEERING ANALYSES AND RECOMMENDATIONS

GEOTECHNICAL DISCUSSION

As discussed previously, CPRA provided topographic survey information including tidal datum, inundation levels, subsidence and mudline elevations to PSI. It is understood that the target year to begin the marsh creation is assumed to be 2023 with the project life of 20 years. Based on the field and laboratory test results, PSI selected design soil parameters for the different engineering calculations presented in the subsequent sections of this report. The soil parameters selected for the engineering calculations are based on 1) the results of field and laboratory test data; 2) engineering judgment based on experience with similar soils; and 3) published correlations.

Based on the obtained survey and geotechnical information mentioned above, engineering analyses are performed to check the slope stability of dikes, and settlements for both the dikes and marsh creation area.

Marsh Creation Area: As requested, the mudline elevation for the marsh fill area was assumed at El. -1.5 (ft., NAVD88 GEOID18) to perform the engineering calculations. Based on the tidal datum and inundation levels data for 20 years, it is understood that the initial marsh fill elevation should be designed such that at the end of project life (Target Year 20), the average marsh elevation should be at a minimum El. +0.7 (ft., NAVD88 GEOID18). The construction of marsh fill area from dredged fill material was simulated using the USACE computer program "Primary Consolidation Secondary Compression, Desiccation of Dredged Fill" (PSDDF). We understand that the marsh will be created in ramp loading continuously not in lifts; however, for the sake of PSDDF calculation, various one-foot lifts of dredged material were modelled in the PSDDF software.

Based on preliminary calculations, it was calculated that a total of six (6) feet of dredged fill is required to construct the marsh fill area to meet the 20 years elevation requirements. It is understood that the settlement of the dredge fill will occur during the fill construction stage. Based on the settlement results obtained from PSDDF and the provided subsidence information, six (6) feet of dredged fill thickness corresponds to Construction Marsh Fill Elevation (CMFE) of +2.83 feet at the completion of dredging in the marsh area. Therefore, a CMFE of +2.83 feet is recommended to meet the 20 years elevation requirements for this project. Detailed settlement analyses for the marsh fill area are included in the subsequent sections.

Containment Dikes: As requested, the mudline elevation for the dikes was assumed at El. -2 (ft., NAVD88 GEOID18) to perform the engineering calculations. One-foot freeboard was assumed in the cross sections used for slope stability and settlement analyses. In order to maintain one-foot freeboard, the top of dike elevation was assumed at El. +3.83 approximated to +4 (ft., NAVD88 GEOID18) for the engineering calculations with a width of crest of five (5) feet. Detailed slope stability and settlement analyses for the containment dikes are included in the subsequent sections.

Cut and Fill Ratio: For the containment dikes and marsh creation area, cut and fill ratios are also provided in the subsequent sections.

SETTLEMENT ANALYSES: MARSH FILL AREA

This section includes design soil parameters formulated for the settlement analyses and settlement analyses results for the marsh fill area.

Design Soil Parameters

The soil parameters selected for the engineering calculations are based on the results of laboratory test data, engineering judgment based on experience with similar soils, and published correlations. Published data and correlations were used from publications such as "Correlation for Consolidation Characteristics of Silts and Clays (NAVFAC DM 7.01, Fig-4, pg. 7.1-144)" , "Technical Report GL-86-13, the Large Strain Controlled Rate of Strain (LSCRS) Device for Consolidation Testing of Soft Fine-Grained Soils", and "Program Documentation and User's Guide: PSDDF by Timothy D. Stark And Hangseok Choi". The soil parameters used in the settlement analysis for various soil layers are presented in Table 5 below.

Based on the results obtained from the self-weight consolidation tests and correlations used from the publications mentioned in the above paragraph, a relationship was established between void ratio-effective stress-hydraulic conductivity. This relationship was used in the PSDDF computer program to simulate the settlement of the dredged soil material in the marsh fill area. The void ratio-effective stress-hydraulic conductivity relationship is presented in the Appendix B.

Table 5: Soil Parameters for USACE computer program PSDDF input*

Dredged Material	(x) Value
Specific gravity of solids	2.7
Soil Type	Clay soils
Average Liquid Limit/Plastic Limit	90/27
Initial Void Ratio	11
C_α/C_c	0.04
**C_r/C_c	0.15
Number of Sublayers	20
Number of Print times	0,12,24,36,48,60,61,90, 180,365,725,1085,1465,1825, 2555,3000, 3650, 7300 days
Article XI. Print times at which material is added	0 days, 12days, 24 days, 36 days, 48 days, 60 days
Article XII. Time periods after which desiccation starts	60 days
Number of time periods for month	30 days
Month at which desiccation starts	6
Desiccation limit	0.86
Saturation limit	4.3
Degree of saturation at desiccation limit	0.50
Maximum Evaporation efficiency for dredged fill	0.75
Surface drainage efficiency factor of containment area	0.50

INCOMPRESSIBLE FOUNDATION	VALUE
(i) Elevation at Top of Incompressible Foundation	(ii) -12 feet

*Detailed back-up for selection and definition of the soil parameters is provided in Appendix B.
**Two (2) additional consolidation tests were performed after completion of Final Data Report to confirm the Recompression Index (Cr) to be used for settlement calculations.

Settlement Analyses and Results

A settlement analyses for the marsh creation area were performed using the USACE computer program "Primary Consolidation Secondary Compression, Desiccation of Dredged Fill" (PSDDF) for the dredged fill material and Settle3 program by Rocscience for the underlying soils in the containment dike area.

The existing mudline elevation within the marsh creation area is assumed at about El. -1.5 (ft., NAVD88 GEOID18). The parameters including rainfall and evaporation rates were obtained from the National oceanic and Atmospheric Administration (NOAA) Technical Report NWS34. Similarly, average monthly rainfall data for Cameron, Louisiana were obtained from NOAA.

For the purpose of these preliminary analyses, we assumed that the dredging and filling operations for marsh creation would take place over a period of about 72 days, during which time some consolidation will occur (The actual dredging and filling duration will depend on the size of dredged used, filling sequence and other factors).

In order to simulate the construction of marsh fill, various one-foot lifts of dredge material were modelled in the PSDDF software. Based on the assumed mudline elevation, a total height of six (6) feet of construction marsh fill was calculated to meet the 20 years elevation requirements. A Construction sequence of one-foot lift in 12 days was considered in PSDDF for the settlement calculations only as we understand that construction of the marsh will be performed continuously.

The settlement results obtained from the PSDDF include both the dredge fill settlement and the foundation soil settlement. The foundation settlement is very minimal and is about 0.2 inch.

As mentioned previously in the report, subsidence is estimated at 4.3 mm/year for this project. The estimated subsidence is also included in the final settlement calculations.

Based on settlement results obtained from PSDDF and subsidence information, a CMFE of +2.83 feet is recommended at the completion of dredging in the marsh area.

The construction marsh fill simulation was also performed for five and a half (5.5) feet, and six and a half (6.5) feet height of marsh fill and were modeled in PSDDF. Based on settlement results obtained from PSDDF, a CMFE of +2.33 feet and +3.32 feet are recommended for five and a half (5.5) feet, and six and a half (6.5) feet height of marsh fill, respectively, at the completion of dredging in the marsh area.

The recommendations for various CMFE's and their corresponding twenty (20) years marsh fill elevation area presented in the Table 6 below.

Table 6. CMFE and TY20 Elevation for the various cases analyzed

CMFE (feet)	TY20 Elevation (feet)
+2.33	+0.59
+2.83	+0.77
+3.32	+0.97

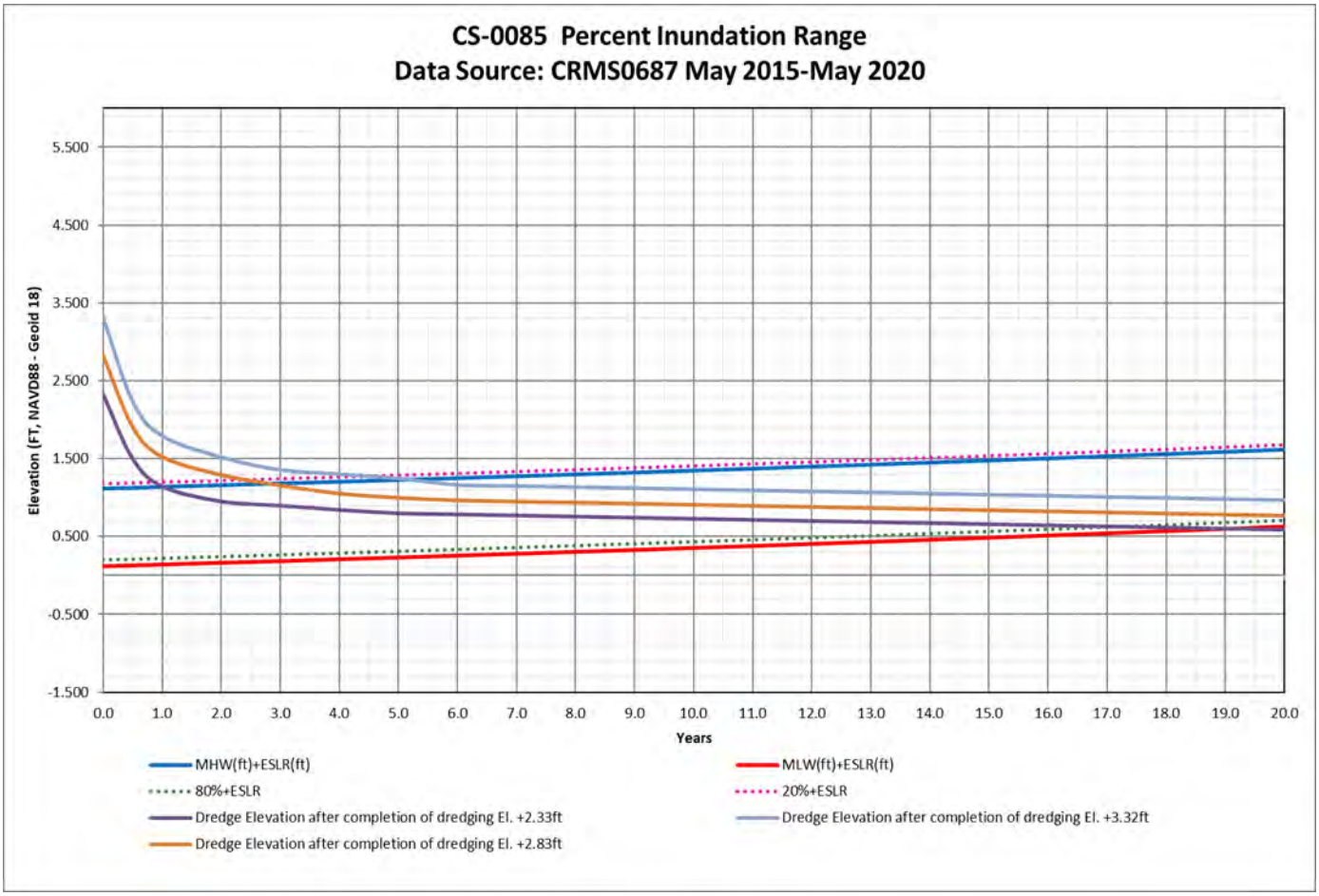


Figure 5: 20 years elevation profile from PSDDF output post dredging of five and a half (5.5) feet, six (6) feet and six and a half (6.5) thickness of construction marsh fill

Based on the PSDDF output, it is understood that the settlement of the dredge fill will occur during the fill construction stage. The plot between Elevation and Time (years) presented above is based on CMFE obtained a day after the addition of the last one-foot lift modelled in PSDDF.

More detailed information about time settlement curve for the marsh fill elevation with inundation levels for the project life (Target Year 20) is presented in Appendix C.

BORROW DREDGED MATERIAL FOR MARSH FILL

The Marsh creation area will be about 392 acres and is on average at about El. -1.5 (ft., NAVD88 GEOID18). Based on preliminary calculations, it was calculated that a the total six (6) feet of construction marsh fill is required to construct the marsh fill area to meet the 20 years elevation requirements. An additional dredged material volume to fill the containment dike excavation in the marsh creation area is also considered in the total dredge volume calculation.

As mentioned previously, the borrow material for this project site is planned to be dredged from the Calcasieu Ship Channel area between Mile markers 5 and 17 to about an elevation of -45 (ft., NAVD88 GEOID18), the maximum dredge elevation allowed. Based on the soil data obtained from borings in the ship channel area, the borrow material mainly consists of clays with average moisture of about 110 percent and specific gravity of about 2.7, this corresponds to a void ratio of about 3.1 for in situ soils.

Dredging duration of approximately 72 days is assumed to construct the required marsh fill area. The design concentration (Cd) defined as the average concentration of the dredged material in the containment area at the end of the disposal activity is estimated from the compression (15-day) settling test. The plot between concentration versus time based on the compression settling test is presented in the Appendix D.

The design concentration (Cd) of about 435g/L was calculated for the average duration of dredging and constructing marsh fill area. Based on TSS at an average dredging time, the void ratio during the fill placement is estimated to be on the order of 5.2. Based on the estimated void ratio at an average dredging time, the volume occupied by dredged material in the containment area immediately after the completion of a particular disposal activity was calculated and presented in the Appendix D.

Based on the PSDDF output, the void ratio of marsh fill area after the 20 years is estimated to be on the order of 3.34. The volumetric ratio of dredged fill soils to the marsh fill soils after the 20 years is approximately 1.

EXCAVATION CUT AND CONTAINMENT DIKE FILL

Based on provided information, a nominal total containment dike length of approximately 30,127 feet is planned to be constructed for the marsh creation area. It is understood that fill material for the containment dike will be excavated from borrow trenches within the marsh creation restoration area, no closer than about 20 ft from the containment dikes.

The estimated thickness of the dredged material at the end of the disposal operation was calculated. Based on estimated thickness of the dredged material at the end of the disposal operation and in order to maintain at least 1 feet of freeboard, the height of the containment dikes was calculated and presented in the Appendix D.

We understand the current plan to construct the containment dikes is to use a clamshell or bucket to excavate the existing material within the marsh area and place the material along the marsh fill perimeter to form the containment dike. This construction method will produce highly variable fill within the dike and variable self-weight consolidation response throughout the dike length. For the uncompacted fill soils to construct the containment dikes, we assumed self-weight consolidation on the order of about 5 percent

of the fill height for the containment dike material (existing marsh area soils). The borrow material will likely be from the upper 8 feet and will be comprised primarily of organic/ fat clays.

For the cut and fill calculation, the excavated borrow material will also need to exceed the design fill quantity in order to compensate for lost soil material due to immediate settlement during construction, material erosion or material sloughing.

A total in place design volume for a containment dike with 5-foot wide crown, 3H:1V side slope, and crest elevation of +4 feet was computed and presented in Table 7 below. The volumetric ratio of required borrow material to constructed fill is approximately 1.20.

Table 7: Estimation of Excavation Cut and Containment Dike Fill Volumes

Crest Elev. (Feet, NAVD88 GEOID18)	Side Slope	Containment Dike length (feet)	Design fill Volume (Cubic yards)	Approximate Required Cut (Cubic yards)
+4	3H:1V	30,127	176,857	212,487

Various factors may influence the ratio between the design fill volume and required cut volume necessary to construct the containment dike. These include method of fill placement, lift sequencing, fill placement's rate and other construction details.

SLOPE STABILITY ANALYSES OF CONTAINMENT DIKES

This section includes design soil parameters formulated for the slope stability analyses, and slope stability analyses results for the containment dikes.

Design Soil Parameters

Detailed fence diagrams, a summary of the consolidation tests and design strength diagrams for the marsh creation area can be found in the Appendix B. The soil strength parameters used in the stability analyses for various soil layers are presented in Table 8 below. The soil parameters for the containment dikes were obtained from CPRA's guidelines for the Marsh Creation and Coastal Restoration Projects.

Table 8: Soil Parameters for Slope Stability Analysis

Soil Type	Elevation (Feet, NAVD88 GEOID18)	Total Unit Weight (pcf)	Undrained Shear Strength (psf)	Angle of Friction (Degrees)
Dike	+5 to -2	80	100	-
Clay	-2 to -5	105	150	-
Clay	-5 to -9	120	500	-
Clay	-9 to -12	110	200	-
Sand	-12 to -20	105	-	30
Sand	-20 to -30	110	-	34

Method of Analyses

Generally, slope failure occurs when the weight of the sliding soil exceeds the resistance derived from the shear strength or frictional resistance of the soil along the sliding surface. Slope stability analysis by limit equilibrium methodology involves the determination of the most likely sliding surface by comparing the developed shearing resistance along a sliding surface with the weight forces associated with the sliding soil. The method of comparison involves the determination of the factor of safety i.e., a ratio of shear resistance along a sliding surface to the weight of the sliding soil. The check for stability involves determination of various values factor of safety along various trial sliding surfaces until a minimum value of factor of safety is reached, for the critical sliding surface. For the slope stability analysis, optimized sliding surfaces were analyzed.

For the present study, the computer program SLIDE, Version 3 of Rocscience was used to implement the methodology described above for the cross section used for analysis.

Containment Dike Sections

Slope stability analyses were performed for the end of the construction for the dike and during the initial phase for the marsh creation area. All the cases considered a 5-foot wide crown, and a 20-foot offset from the toe of the containment dike to the edge of the borrow excavation was maintained. Slope stability analyses are performed for cross-section with side slope 3H:1V. One feet of freeboard was maintained for stability analyses. In order to maintain one-foot freeboard, the top of dike elevation was assumed at El. +4 (ft., NAVD88 GEOID18) for the engineering calculations. As discussed in Geotechnical Discussion section, the mudline elevation for the dikes was assumed at El. -2 (ft., NAVD88 GEOID18).

As requested, additional slope stability analyses were also performed for the containment dikes with the top of dike elevations at El. +3.5, +4.5, +5 and +5.5 (ft., NAVD88 GEOID18) for the recommended CMFE of +2.83.

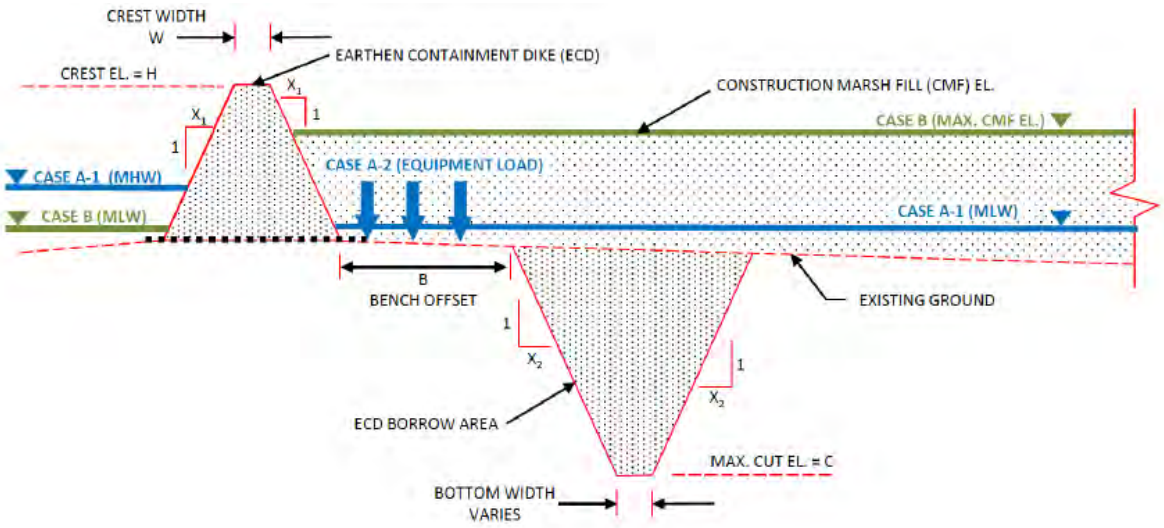


Figure 6 Typical Cross Section of the Dike

Case A-1
Global stability check: During Earthen Containment Dike (ECD) borrow excavation, Mean High Water (MHW)-opposite side of borrow, Mean Low Water (MLW) - borrow side.

Case A-2
Local stability check: During ECD borrow excavation, Distributed load from excavation equipment (260 psf), MLW - borrow side.
Case B
Dredged Material placed to Construction Marsh Fill (CMF) EL.: CMF (max. elevation), MLW - opposite side of borrow.

It was assumed that during construction of the embankment of the containment dike, softening of the borrow area soil would occur due to disturbances caused by excavation process. This softening was assumed to reduce the shear strength. Additionally, consideration was given to the development of a tension crack in the containment dike. The depth of the tension crack was estimated to be equal to twice the cohesion divided by the unit weight of the material (depth = 2Su/y= 2.5 ft.). Furthermore, it was assumed that the tension crack would be filled with water. Results of the analyses for the cases presented above with tension cracks and without tension cracks are provided in the Table 9 and Table 10 respectively below.

Table 9: ECD Geometry Table and Results for 3H:1V side slopes

Case	Outboard Water El. (ft., NAVD88 GEOID18)	Inboard Water El. (ft., NAVD88 GEOID18)	Bench Offset (ft.)	Min. Factor of Safety with Tension Crack				
				Top of Dike Elevation				
				+3.5 ft	+4 ft	+4.5 ft	+5 ft	+5.5 ft
A-1	1.05	0.06	20	2.0	1.8	1.7	1.6	1.5
A-2	1.05	0.06	20	N/A	N/A	N/A	N/A	N/A
B	0.06	2.83	20	2.0	1.8	1.7	1.6	1.5

Table 10: ECD Geometry Table and Results for 3H:1V side slopes

Case	Outboard Water El. (ft., NAVD88 GEOID18)	Inboard Water El. (ft., NAVD88 GEOID18)	Bench Offset (ft.)	Min. Factor of Safety without Tension Crack				
				Top of Dike Elevation				
				+3.5 ft	+4ft	+4.5 ft	+5 ft	+5.5 ft
A-1	1.05	0.06	20	2.3	2.1	1.9	1.8	1.6
A-2	1.05	0.06	20	1.9	1.9	1.9	1.9	1.9
B	0.06	2.83	20	2.3	2.1	1.9	1.8	1.6

Slope stability analysis performed for cross-sections mentioned above are presented in in Appendix D.
Typical industry standards use a factor of safety of 1.3 as the minimum acceptable for short term and 1.5 for long term soil conditions. Slope stability results are also presented in Appendix E of the report.

SETTLEMENT ANALYSES: CONTAINMENT DIKES

This section includes design soil parameters formulated for the settlement analyses, and settlement analyses results for the containment dikes.

Design Soil Parameters

Detailed fence diagrams, a summary of the consolidation tests and design strength diagrams for the marsh creation area can be found in the Appendix B. The soil strength parameters used in the settlement analysis for various soil layers are presented in the Table 11 below.

Table 11: Soil Parameters for Settlement analyses for containment dikes

Soil Type	Elevation (Feet, NAVD88 GEOID18)	Total Unit Weight (pcf)	Compression Index (C_c)	Recompression Index (C_r)*	Pre-consolidation Pressure (P_c) (tsf)	Coefficient of Consolidation (C_v, ft^2/y)	Void ratio
Clay	-2 to -5	105	0.45	0.07	0.25	20	1.5
Clay	-5 to -9	120	0.4	0.06	0.25	50	1.25
Clay	-9 to -12	110	0.25	0.035	0.25	50	1
Sand/Silt	-12 to -20	105	N/A	N/A	N/A	N/A	N/A

*Two (2) additional consolidation tests were performed after completion of the Final Data Report to confirm the Recompression Index ($\mathbf{C_r}$) to be used for settlement calculations. Based on results, approximately $\mathbf{C_r}$ / $\mathbf{C_c}$ =0.15 correlation is used to calculate $\mathbf{C_r}$.

Settlement Analyses and Results

Based on assumed containment dike geometry with a crest width of five (5) feet, crest elevation of +4 feet, and side slope of 3H:1V, settlement analyses were performed for the consolidation of underlying foundation soils using the computer program Settle3 from Rocscience, Inc.

Settlements of the containment dike were estimated based on soil properties mentioned in the previous section and that dike bottom is constructed at Elevation of -2 (ft., NAVD88 GEOID18). As mentioned previously, in order to maintain one-foot freeboard, the top of dike elevation was assumed at El. +4 (ft., NAVD88 GEOID18) for the engineering calculations.

Immediate Settlement: During the construction of the containment dike, immediate settlement could occur due to the volume distortion in the foundation soils. Essentially, this is the rearrangement of grains due to changing stress, resulting in a reduction in void ratio and immediate settlement. It is anticipated that approximately up to 4 to 6 inches of immediate settlement could occur during the construction phase of the containment dike.

Consolidation Settlement: Post construction of the containment dikes, the foundation soils undergo consolidation. Primary consolidation refers to the volume changes in the foundation soil caused by dissipation of stress induced excess pore water pressure. Based on assumed containment dike cross section, consolidation settlements at the center of the dike is estimated about 6-7 inches of post construction during the 20-year project life. It is anticipated that the consolidation settlement will occur in the long-term or several years of service of the dike.

CONCLUSIONS AND RECOMMENDATIONS

Given the need to maintain a freeboard of 1 foot at all time during construction, the crest height of the containment dike will depend on the self-weight consolidation properties of the borrow material as well as the construction practices used. Consolidation settlement analyses for the containment dike will also be undertaken during the marsh filling design analyses to determine if the design crest elevation of the dike needs to be elevated to compensate for settlements. As shown, results indicate that even if a tension crack develops within the containment dike, the side slope and elevations result in favorable factors of safety.

It should be noted that means, methods, and sequence of the proposed construction should be the responsibility of the Contractor, who should be experienced in this type of construction.

It is recommended PSI be retained to provide observation and testing of construction activities involved in this project. PSI cannot accept responsibility for any conditions which deviate from those described in this report, nor for the performance of the foundations if not engaged to also provide construction observation and testing for this project.

In Federal Register, Volume 54, No. 209 (October 1989), the United States Department of Labor, Occupational Safety and Health Administration (OSHA) amended its "Construction Standards for Excavations, 29 CFR, part 1926, Subpart P". This document was issued to better ensure the safety of workmen entering trenches or excavations. It is mandated by this federal regulation that excavations be constructed in accordance with the applicable OSHA guidelines. It is our understanding that these regulations are being strictly enforced, and if they are not closely followed, the Owner and the Contractor could be liable for substantial penalties.

The Contractor is solely responsible for designing and constructing stable, temporary excavations and should shore, slope, or bench the sides of the excavations as required to maintain stability of both the excavation sides and bottom. The Contractor's "responsible person", as defined in 29 CFR Part 1926, should evaluate the soil exposed in the excavations as part of the Contractor's safety procedures. In no case should slope height, slope inclination, or excavation depth, exceed those specified in local, state, and federal safety regulations.

We are providing this information solely as a service to our Client. PSI does not assume responsibility for construction site safety or the Contractor's or other parties' compliance with local, state, and federal safety regulations.

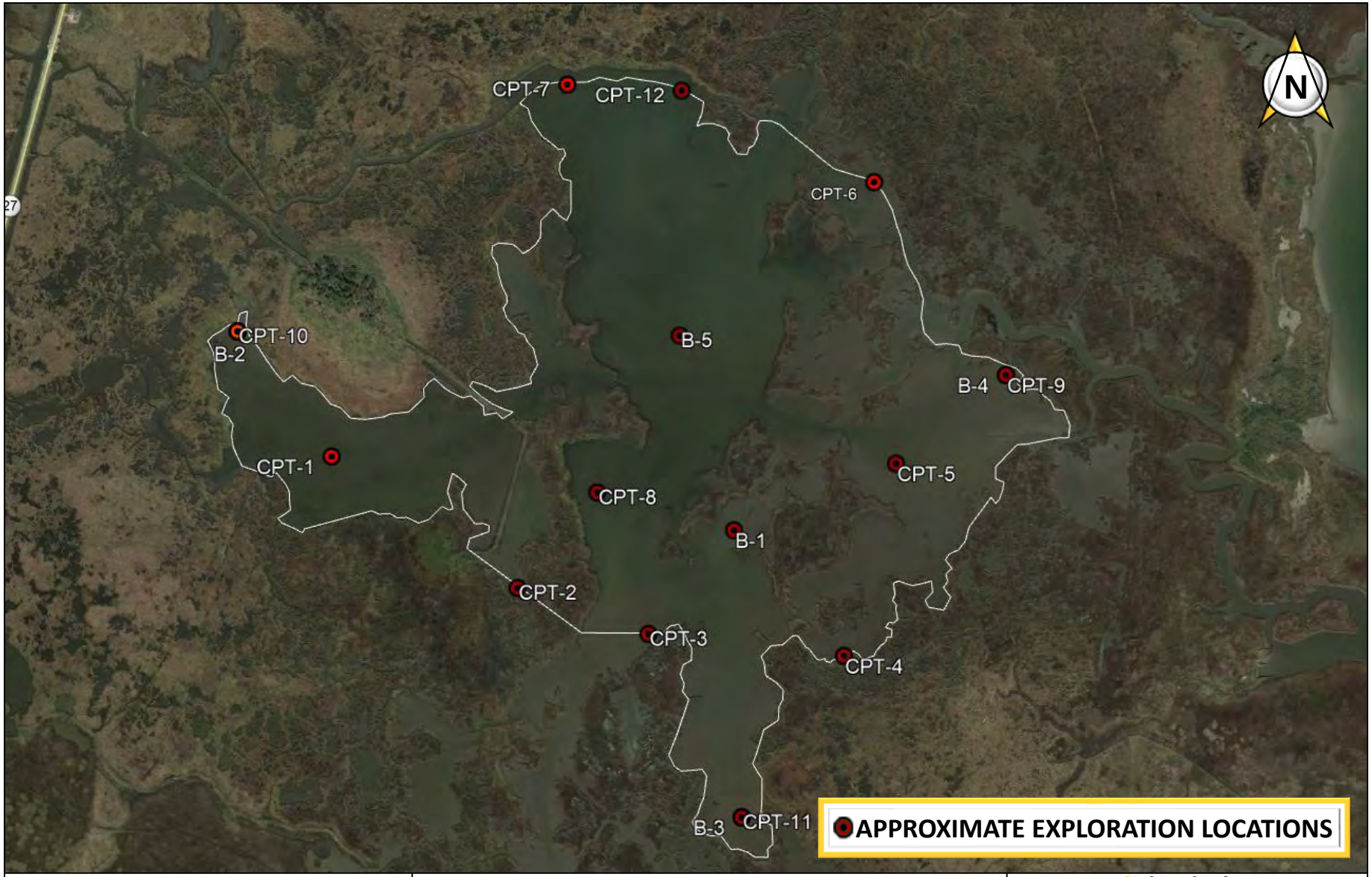
REPORT LIMITATIONS

The recommendations provided in this report are based on the available subsurface information obtained by PSI and design details furnished by the CPRA for the proposed project. If there are any revisions to the plans for this project, or if deviations from the subsurface conditions noted in this report are encountered during construction, PSI should be notified immediately to determine if changes in our recommendations are required. If PSI is not notified of such changes, we will not be responsible for the impact of those changes on the project.

PSI warrants that the findings, recommendations, specifications, or professional advice contained herein have been made in accordance with generally accepted professional geotechnical engineering practices in the local area. No other warranties are implied or expressed.

After the plans and specifications are more complete, PSI should be retained and provided the opportunity to review the final design plans and specifications to check that our engineering recommendations have been properly incorporated into the design documents. At that time, it may be necessary to provide supplementary recommendations. If PSI is not retained to perform these functions, we will not be responsible for the impact of those conditions on the project. This report has been prepared for the exclusive use of CPRA for the proposed marsh creation in Cameron Parish, Louisiana.

APPENDIX A
PROJECT LOCATION PLAN



GEOTECHNICAL ENGINEERING SERVICES

Long Point Bayou Marsh Creation

Cameron, Louisiana

MARSH BORING LOCATION PLAN

PSI PROJECT NO.: 02541211

GOOGLE EARTH IMAGERY DATE: 1/2018

intertek psi

GEOTECHNICAL ENGINEERING SERVICES

Long Point Bayou Marsh Creation

Cameron, Louisiana

CHANNEL BORING LOCATION PLAN

PSI PROJECT NO.: 02541211

GOOGLE EARTH IMAGERY DATE: 1/2018

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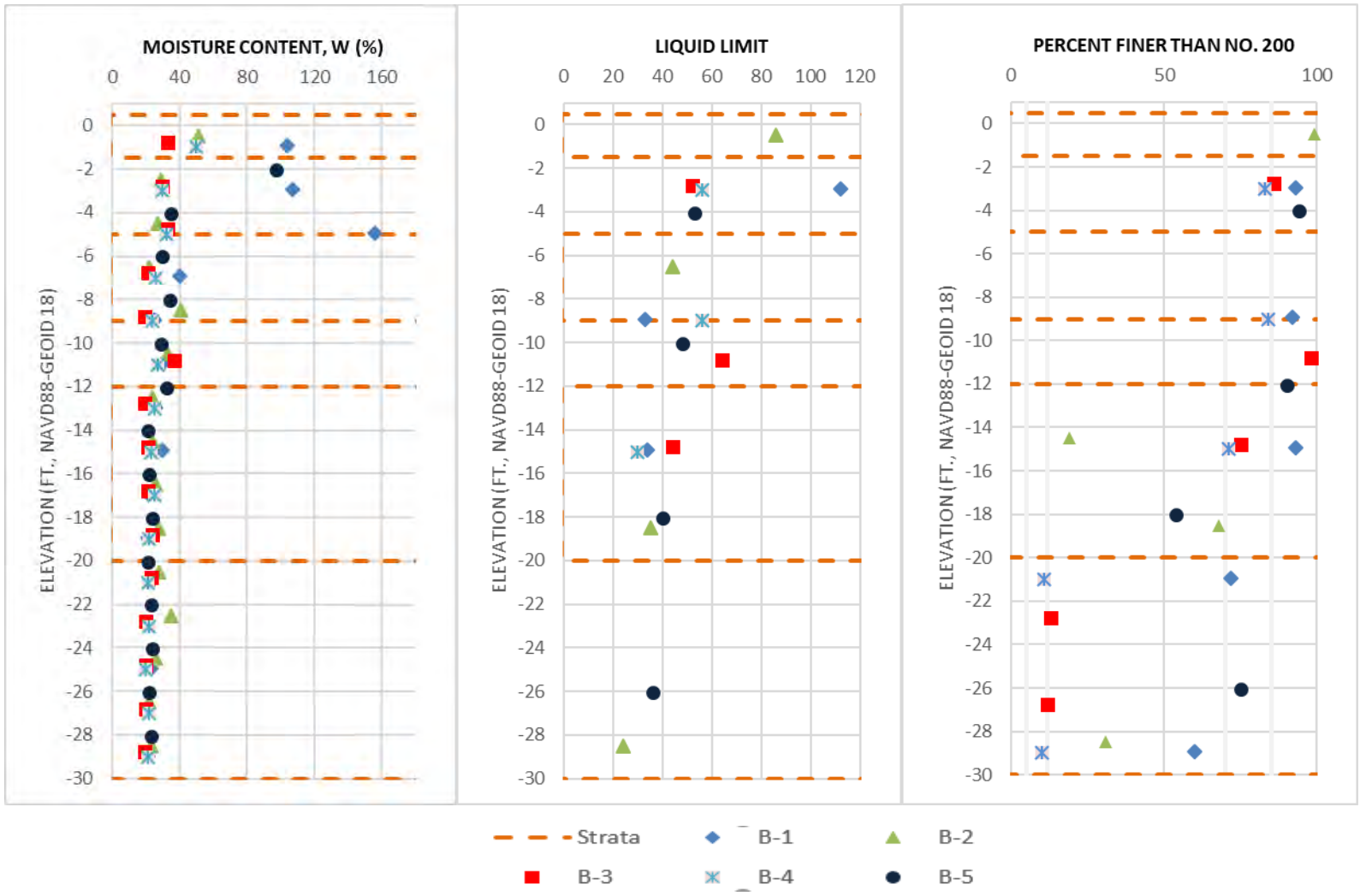
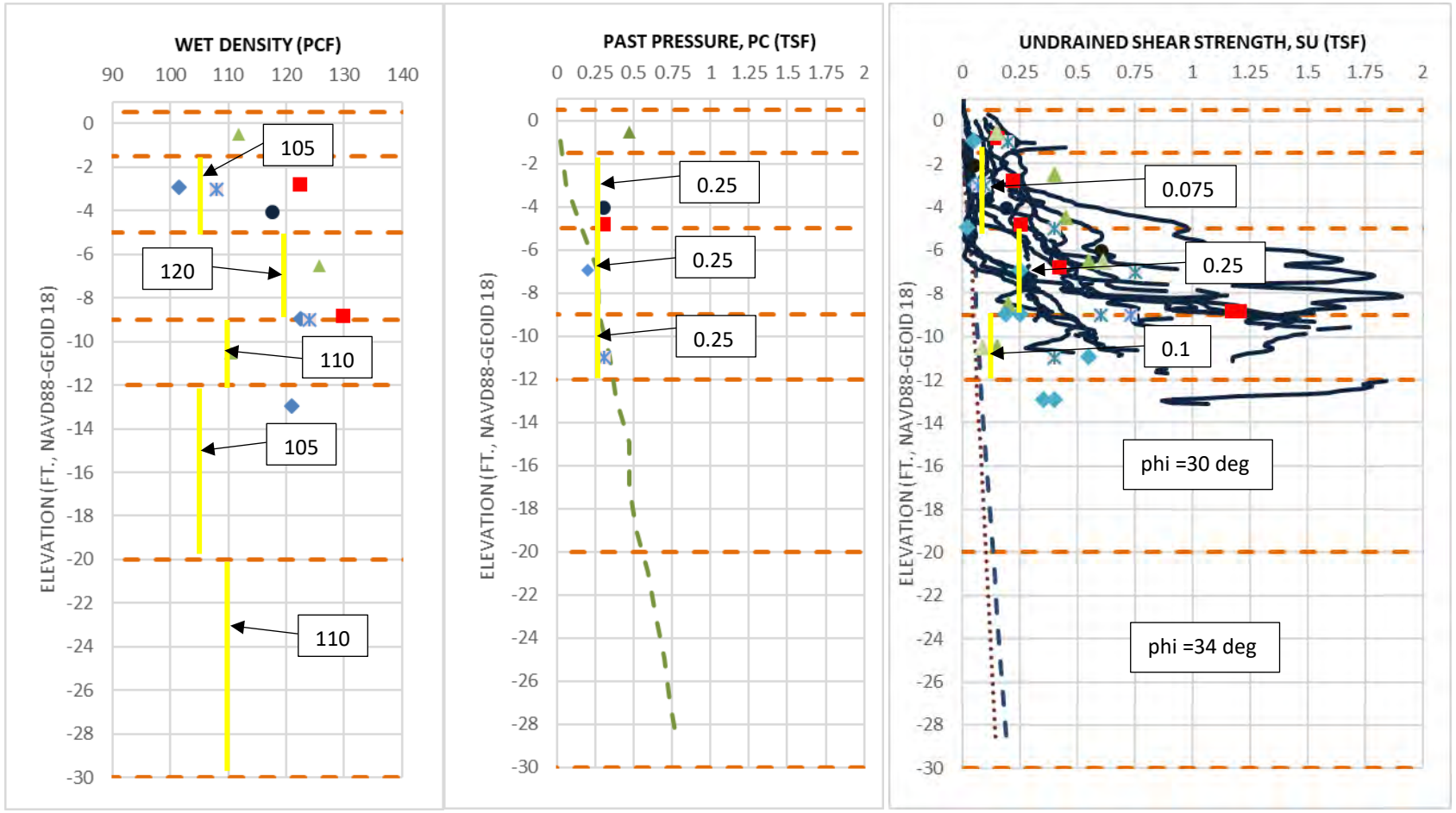
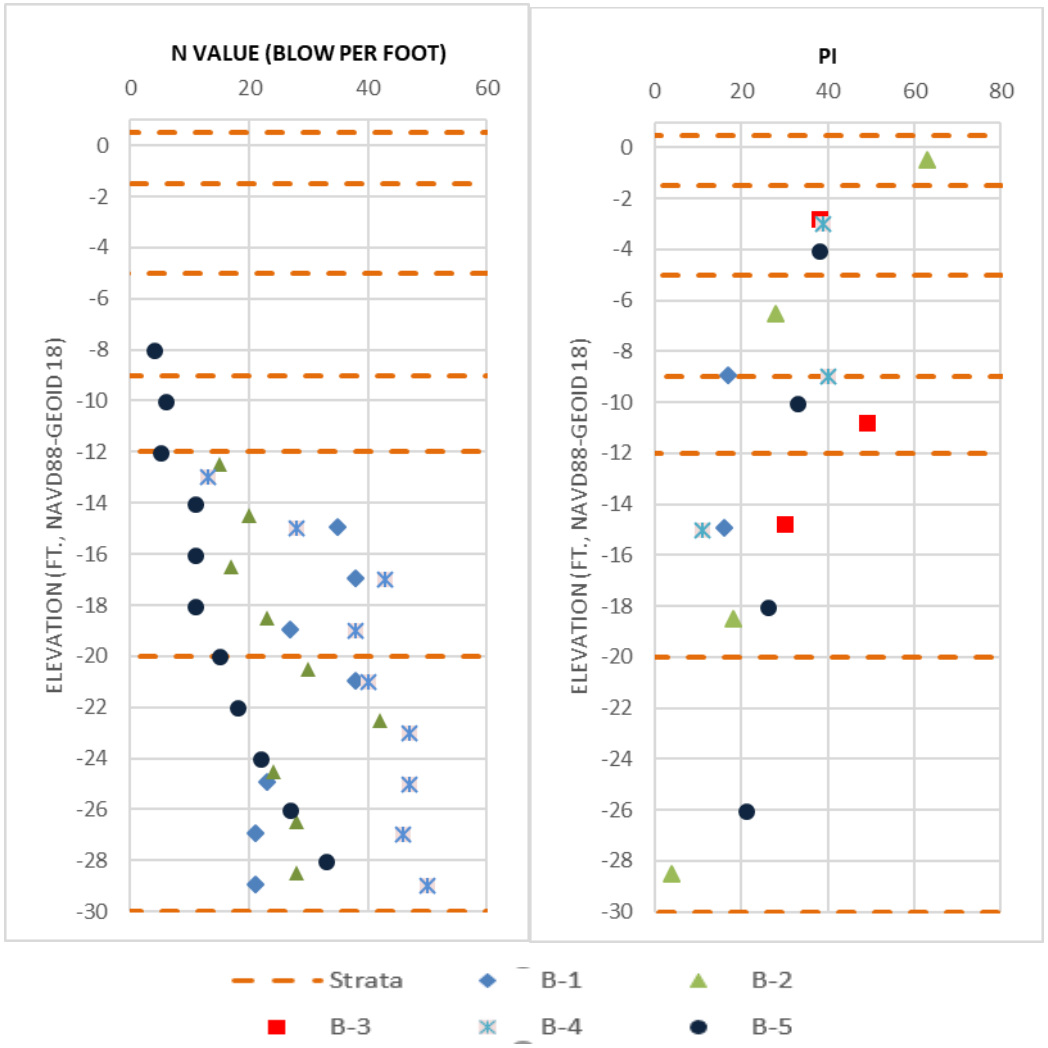
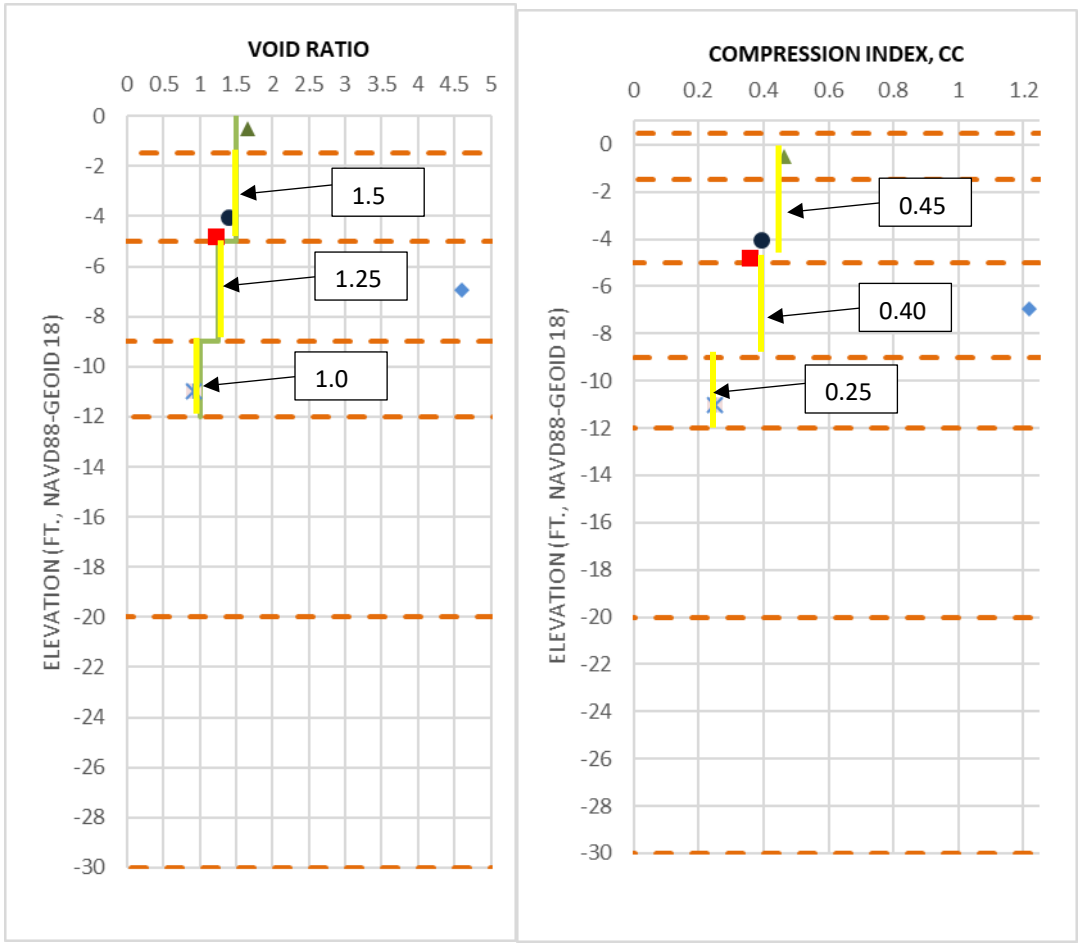
APPENDIX B

MARCH CREATION AREA DESIGN PROFILE

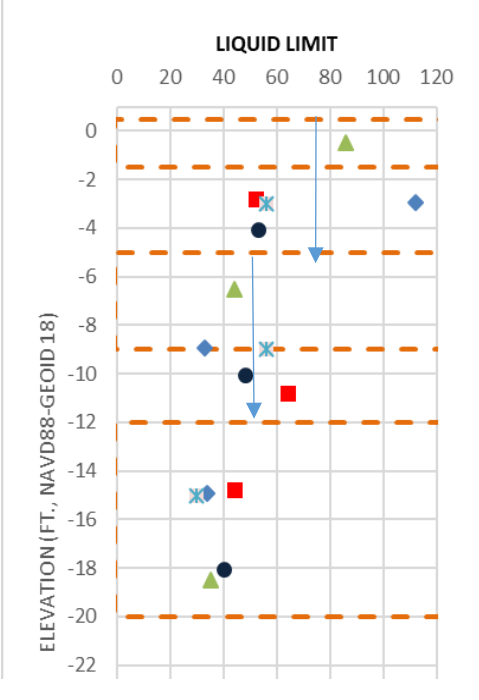

MOISTURE CONTENT, W (%)
0
40
80
120
160
LIQUID LIMIT
0
20
40
60
80
100
120
PERCENT FINER THAN NO. 200
0
50
100
ELEVATION (FT., NAVD88-GEOID 18)
0
-2
-4
-6
-8
-10
-12
-14
-16
-18
-20
-22
-24
-26
-28
-30
Strata
B-1
B-2
B-3
B-4
B-5

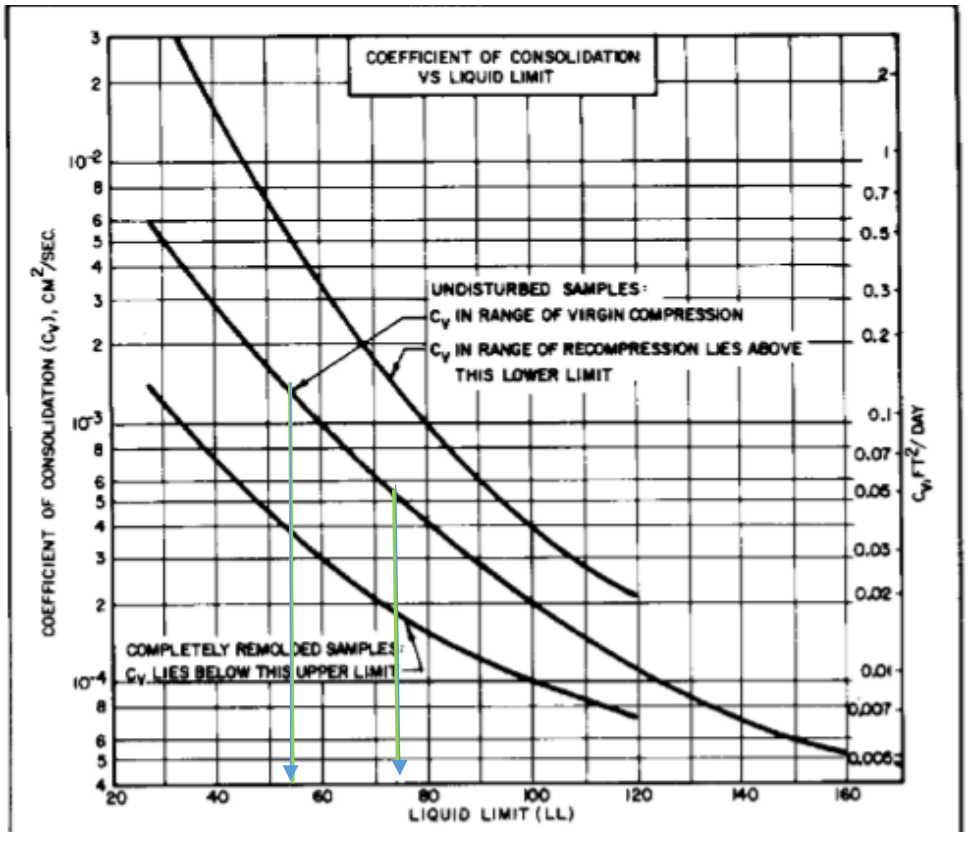

WET DENSITY (PCF)
90 100 110 120 130 140
ELEVATION (FT., NAVD88-GEOID 18)
0 -2 -4 -6 -8 -10 -12 -14 -16 -18 -20 -22 -24 -26 -28 -30
105
120
110
105
110
PAST PRESSURE, PC (TSF)
0 0.25 0.5 0.75 1 1.25 1.5 1.75 2
0.25
0.25
0.25
UNDRAINED SHEAR STRENGTH, SU (TSF)
0 0.25 0.5 0.75 1 1.25 1.5 1.75 2
0.075
0.25
0.1
phi =30 deg
phi =34 deg
Strata
B-1
B-2
B-3
B-4
B-5
Effective Vertical Stress
c/p=0.22
c/p=0.17
CPT
Design Line


N VALUE (BLOW PER FOOT)
0
20
40
60
ELEVATION (FT., NAVD88-GEOID 18)
0
-2
-4
-6
-8
-10
-12
-14
-16
-18
-20
-22
-24
-26
-28
-30
PI
0
20
40
60
80
Strata
B-1
B-2
B-3
B-4
B-5


VOID RATIO
0 0.5 1 1.5 2 2.5 3 3.5 4 4.5 5
0 -2 -4 -6 -8 -10 -12 -14 -16 -18 -20 -22 -24 -26 -28 -30
ELEVATION (FT., NAVD88-GEOID 18)
1.5
1.25
1.0
COMPRESSION INDEX, CC
0 0.2 0.4 0.6 0.8 1 1.2
0 -2 -4 -6 -8 -10 -12 -14 -16 -18 -20 -22 -24 -26 -28 -30
ELEVATION (FT., NAVD88-GEOID 18)
0.45
0.40
0.25
Strata
B-1
B-2
B-3
B-4
B-5
Design Line

Elevation (Feet, NAVD88 GEOID18)	Cv ft2/day	Cv ft2/year	Used Cv ft2/year
-2 to -5	0.05	18.25	20
-5 to -9	0.15	54.75	50
-9 to -12	0.15	54.75	50





Soil Parameters for USACE computer program PSDDF input

C_{α}, Secondary Compression Index

C_{c}, Primary Compression Index

Cr, Recompression Index

DL, Desiccation limit: Desiccation limit of the dredged fill defined as the lowest void ratio the material will attain during second stage drying. An estimate of the moisture content at the desiccation limit is 1.2 times the water content (in decimal form) at the plastic limit of the dredged fill. The corresponding void ratio can be used as the desiccation limit.

SL, Saturation Limit: Saturation limit of the dredged fill defined as the void ratio which separates first-stage desiccation from second-stage desiccation. The moisture content at the saturation limit corresponds to a degree of saturation equal to 100% and can be estimated using 1.8 times the water content (in decimal form) at the liquid limit. The corresponding void ratio can be used as the saturation limit.

The average degree of saturation: It is expressed as a fraction of 1.0, of the dredged fill when dried to the desiccation limit, DL. This value includes the crack network.

Void ratio: Measured void ratios of dredged material layer under effective stresses applied in laboratory consolidation tests and published correlations.

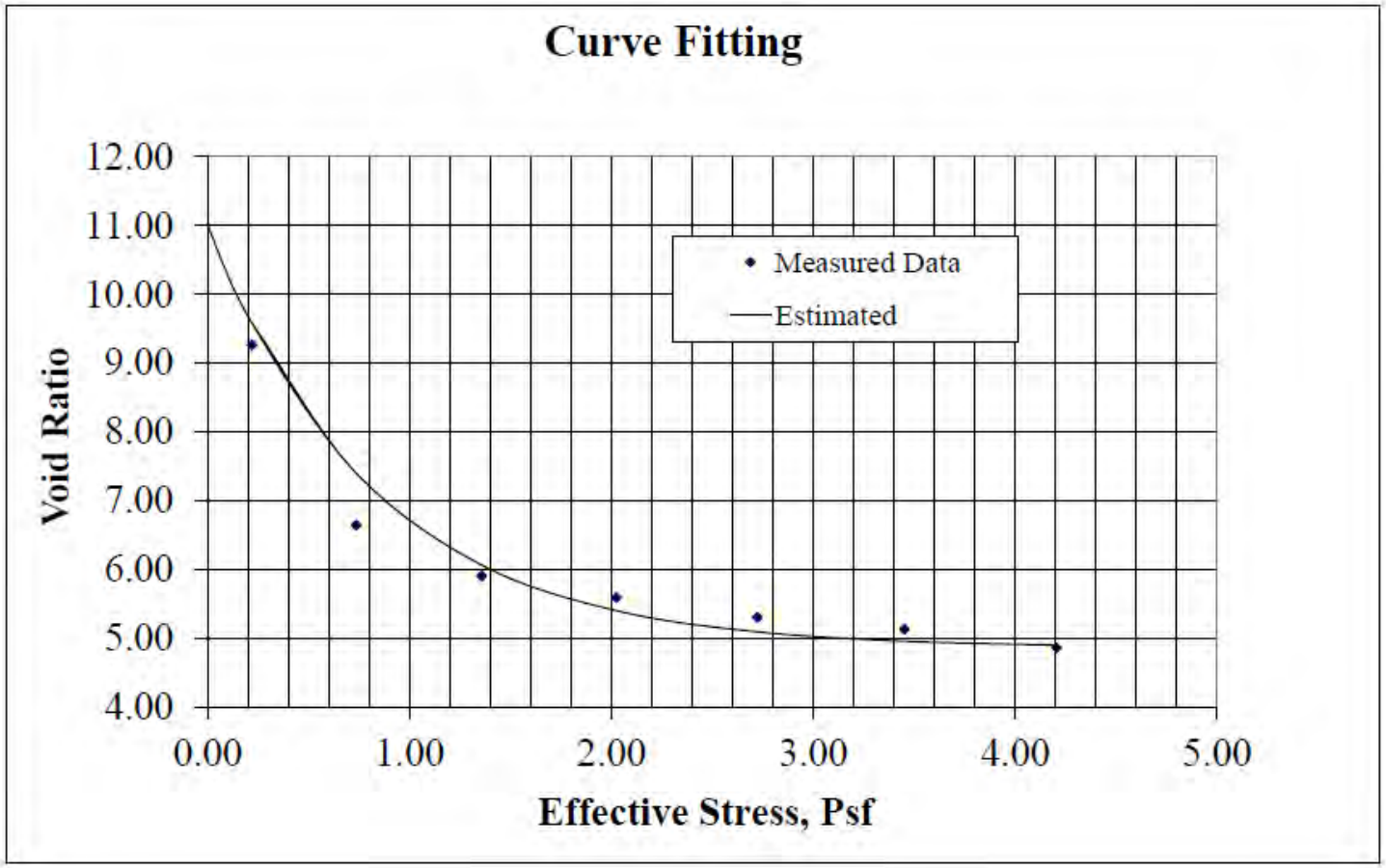
Drainage efficiency factor of the containment area: It is defined as the ratio of the overland runoff volume to the rainfall volume. Values range from 0.0 for areas with no surface drainage, and hence rely only on evaporation for water removal, to 1.0 for areas with rapid removal of rainfall volumes.

Print Times: Times at which the properties of the consolidating layers will be printed and/or a new layer of dredged fill is applied.

Length of vertical drainage path through the incompressible foundation: It is based on the permeability of the incompressible foundation material. Values range from 1 ft (0.3 m) for an incompressible foundation that is free draining to 100 ft (30 m) for a foundation that is impervious. A partially drained foundation has a drainage path length between 1 and 100 ft.

Average monthly rainfall expected at the containment area for each month of the year. January is month number 1.

Void Ratio =11	(Extrapolated from Self weight consolidation tests)



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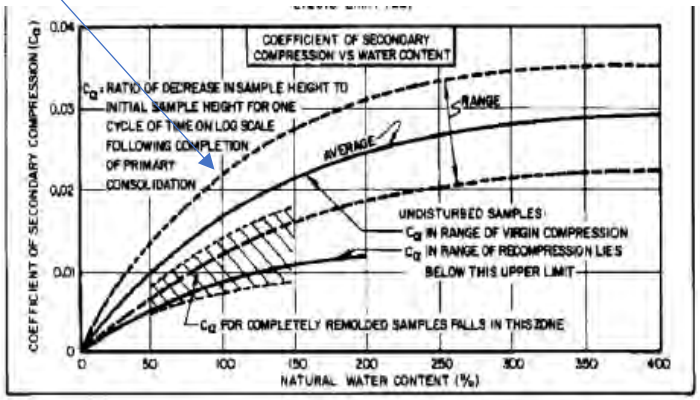
Ratio between secondary compression index, C_α, and Compression index, C_c from standard oedometer tests. Typical values of C_α/C_c range from 0.01 to 0.05.

From Boring B-1 and B-5

Average w%	100
Ca	0.02
Cc	0.45
Ca/Cc	0.04

(approx from consol tests)



e B-4: Correlations for Consolidation Characteristics of Silts and Clays (NAVFAC DM 7.01, Fig-4, pg. 7.1-144).

Based on lab results, avaerage Cr/C ratio is approximately 0.15

Boring No.	Depth ft.	Cc	Cr	Cr/Cc
B-2	2-4	0.43	0.078	0.18
B-2	2-4	0.4	0.076	0.19
B-3	4-6	0.356	0.042	0.12
B-4	10-12	0.299	0.026	0.09

Ratio between recompression index, C_r, and Compression index, C_c from standard oedometer tests. Typical values of C_r/C_c range from 0.1 to 0.3.

Dessication Limit DL

Desiccation limit of the dredged fill defined as the lowest void ratio the material will attain during second-stage drying. An estimate of the moisture content at the desiccation limit is 1.2 times the water content (in decimal form) at the plastic limit of the dredged fill. The corresponding void ratio can be used as the desiccation limit.

	B-6	B-7	B-8	B-9	B-10	B-11	B-12
PL	31	29	30	23	27	25	22

Avg PL for Dredged Fill	27

0.27

water content at DL	0.32

Dessication Limit DL 0.86

Saturation Limit SL

Saturation limit of the dredged fill defined as the void ratio which separates first-stage desiccation from second-stage desiccation. The moisture content at the saturation limit corresponds to a degree of saturation equal to 100% and can be estimated using 1.8 times the water content (in decimal form) at the liquid limit. The corresponding void ratio can be used as the

	B-6	B-7	B-8	B-9	B-10	B-11	B-12
w%	123	92	94	72	100	79	70

avg. w%	90

water content at SL 1.6

Saturation Limit SL	4.3

The average degree of saturation, expressed as a fraction of 1.0, of the dredged fill when dried to the desiccation limit, DL. This value includes the crack network. (Based on field samples; SAT ranges from 40 to 60%.)

Drainage efficiency factor of the containment area which is defined as the ratio of the overland runoff volume to the rainfall volume. Values range from 0.0 for areas with no surface drainage, and hence rely only on evaporation for water removal, to 1.0 for areas with rapid removal of rainfall volumes. In a well managed disposal facility, i.e., weir loads removed after sedimentation and internal trenches excavated, DREFF can be assumed to range from 0.8 to 1.0. DREFF should be reduced to 0.2 - 0.3 if the disposal facility is not managed.

The maximum dredged fill evaporation efficiency for desiccation drying. Observed values range from 0.5 to 1.2, however, the simulation is relatively insensitive to variations in CE between 0.5 and 1.0. Unless data is available, a value of 0.75 is recommended.

Input parameters for PSDDF

Void ratio- Stress (psf)-Hydraulic Conductivity (ft/day) Relationship

Void	Stress (psf)	k (ft/day)
11.00	0.00E+00	2.90E-01
9.00	1.00E-01	5.80E-02
8.00	4.00E-01	4.30E-02
7.50	6.00E-01	2.90E-02
7.00	8.00E-01	1.40E-02
6.00	2.00E+00	7.20E-03
5.50	3.00E+00	4.30E-03
5.00	4.00E+00	3.60E-03
4.50	1.20E+01	2.90E-03
4.00	2.00E+01	1.40E-03
3.50	4.00E+01	1.00E-03
3.00	8.00E+01	4.30E-04
2.50	2.00E+02	2.90E-04
2.00	4.00E+02	1.40E-04

APPENDIX C

SETTLEMENT ANALYSES MARSH FILL AREA

****
Consolidation and desiccation of soft layers---dredged fill
****

Problem LONG POINT BAYOU MARSH CREATION PROJECT

**********Soil data for compressible foundation**********

Material Type	Layer Thickness	Numbers of Sub-layers	Ca/Cc	Cr/Cc	OCR
2	6.50	10	0.040	0.150	1.000
3	4.00	10	0.040	0.150	1.000

Material type : 2 Specific Gravity of Solids: 2.65

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	1.420	0.000E+00	0.100E-02	0.413E-03	0.190E-02	-0.100E+05	-0.413E+01
2	1.410	0.100E+03	0.950E-03	0.394E-03	0.191E-02	-0.100E+05	-0.394E+01
3	1.400	0.200E+03	0.900E-03	0.375E-03	0.255E-02	-0.750E+04	-0.281E+01
4	1.390	0.250E+03	0.820E-03	0.343E-03	0.509E-02	-0.100E+05	-0.343E+01
5	1.380	0.400E+03	0.650E-03	0.273E-03	0.661E-02	-0.125E+05	-0.341E+01
6	1.370	0.500E+03	0.500E-03	0.211E-03	0.333E-02	-0.100E+05	-0.211E+01
7	1.320	0.100E+04	0.170E-03	0.733E-04	0.117E-02	-0.100E+05	-0.733E+00
8	1.220	0.200E+04	0.800E-04	0.360E-04	0.279E-03	-0.136E+05	-0.491E+00
9	1.100	0.400E+04	0.250E-04	0.119E-04	0.126E-03	-0.250E+05	-0.298E+00
10	0.980	0.800E+04	0.115E-04	0.581E-05	0.387E-04	-0.522E+05	-0.303E+00
11	0.870	0.160E+05	0.560E-05	0.299E-05	0.161E-04	-0.109E+06	-0.327E+00
12	0.760	0.320E+05	0.400E-05	0.227E-05	0.656E-05	-0.145E+06	-0.331E+00

Material type : 3 Specific Gravity of Solids: 2.68

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	0.910	0.000E+00	0.200E-02	0.105E-02	0.863E-01	-0.250E+05	-0.262E+02
2	0.900	0.250E+03	0.350E-03	0.184E-03	0.498E-01	-0.250E+05	-0.461E+01
3	0.890	0.500E+03	0.980E-04	0.519E-04	0.400E-02	-0.187E+05	-0.972E+00
4	0.860	0.100E+04	0.450E-04	0.242E-04	0.334E-03	-0.150E+05	-0.363E+00
5	0.790	0.200E+04	0.330E-04	0.184E-04	0.118E-03	-0.200E+05	-0.369E+00
6	0.710	0.400E+04	0.110E-04	0.643E-05	0.999E-04	-0.375E+05	-0.241E+00
7	0.630	0.800E+04	0.400E-05	0.245E-05	0.365E-04	-0.800E+05	-0.196E+00
8	0.560	0.160E+05	0.150E-05	0.962E-06	0.137E-04	-0.171E+06	-0.165E+00
9	0.490	0.320E+05	0.800E-06	0.537E-06	0.607E-05	-0.229E+06	-0.123E+00

**********Soil data for dredged fill**********

Material Type	Specific Gravity	Ca/Cc	Cr/Cc	Saturation Limit	Disication Limit	Max. Crust Depth	Saturation at DL
4	2.700	0.040	0.150	4.300	0.860	0.500	0.500

Material type : 4

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	11.000	0.000E+00	0.290E+00	0.242E-01	0.918E-02	-0.500E-01	-0.121E-02
2	9.000	0.100E+00	0.580E-01	0.580E-02	0.646E-02	-0.133E+00	-0.773E-03
3	8.000	0.400E+00	0.430E-01	0.478E-02	0.159E-02	-0.333E+00	-0.159E-02
4	7.500	0.600E+00	0.290E-01	0.341E-02	0.303E-02	-0.400E+00	-0.136E-02
5	7.000	0.800E+00	0.140E-01	0.175E-02	0.159E-02	-0.933E+00	-0.163E-02
6	6.000	0.200E+01	0.720E-02	0.103E-02	0.726E-03	-0.147E+01	-0.151E-02
7	5.500	0.300E+01	0.430E-02	0.662E-03	0.429E-03	-0.200E+01	-0.132E-02
8	5.000	0.400E+01	0.360E-02	0.600E-03	0.134E-03	-0.900E+01	-0.540E-02
9	4.500	0.120E+02	0.290E-02	0.527E-03	0.320E-03	-0.160E+02	-0.844E-02
10	4.000	0.200E+02	0.140E-02	0.280E-03	0.305E-03	-0.280E+02	-0.784E-02
11	3.500	0.400E+02	0.100E-02	0.222E-03	0.172E-03	-0.600E+02	-0.133E-01
12	3.000	0.800E+02	0.430E-03	0.107E-03	0.139E-03	-0.160E+03	-0.172E-01

```
 13  2.500 0.200E+03 0.290E-03 0.829E-04 0.608E-04-0.320E+03-0.265E-01
 14  2.000 0.400E+03 0.140E-03 0.467E-04 0.724E-04-0.400E+03-0.187E-01
```

Summary of lifts and print detail

Time days	Material Type	Fill Height	# Sub-layers	Void ratio	Start Day	Dessic. Month	Print detail
0.	4	1.0	12	11.00	180.	6	1
12.	4	1.0	12	11.00	180.	6	1
24.	4	1.0	12	11.00	180.	6	1
36.	4	1.0	12	11.00	180.	6	1
48.	4	1.0	12	11.00	180.	6	1
60.	4	1.0	100	11.00	180.	6	1
61.					180.	6	1
90.					180.	6	1
180.					180.	6	1
240.					180.	6	1
365.					180.	6	1
725.					180.	6	1
1085.					180.	6	1
1465.					180.	6	1
1825.					180.	6	1
2555.					180.	6	1
3000.					180.	6	1
3650.					180.	6	1
7300.					180.	6	1

Summary of monthly rainfall and evaporation potential

Month	Rainfall	Evaporation
1	0.210	0.420
2	0.250	0.300
3	0.370	0.320
4	0.450	0.300

	output	
5	0.550	0.370
6	0.560	0.590
7	0.550	0.540
8	0.500	0.400
9	0.460	0.400
10	0.410	0.420
11	0.270	0.370
12	0.210	0.210

**********Calculation data**********

tau	Lower layer Void ratio	Lower layer Permeability	drainage path Length
.809E-03	0.500	0.10000E-01	z = 0.67

Summary of desiccation parameters

Parameter	Value
Surface Drainage Efficiency	0.50
maximum evaporation efficiency	0.75
time to desic. after initial fill	180.00
month of initial desiccation	6
elevation of fixed water table	0.00
elevation of top of incompres. found.	-12.00

**********Initial Conditions in Compressible Foundation**********

***** Coordinates *****

A	XI	Z
10.50	10.50	4.83
10.10	10.10	4.62
9.70	9.70	4.41
9.30	9.30	4.20
8.90	8.90	3.99
8.50	8.50	3.78
8.10	8.10	3.57
7.70	7.70	3.36
7.30	7.30	3.15
6.90	6.90	2.94
6.50	6.50	2.73
6.50	6.50	2.73
5.85	5.85	2.46
5.19	5.19	2.18
4.54	4.54	1.91
3.89	3.89	1.64
3.24	3.24	1.36
2.59	2.59	1.09
1.94	1.94	0.82
1.29	1.29	0.55
0.65	0.65	0.27
0.00	0.00	0.00

***** Void Ratios *****

Einitial	E	Eeop	Material
0.91	0.91	0.91	3
0.91	0.91	0.91	3
0.91	0.91	0.91	3
0.91	0.91	0.91	3
0.91	0.91	0.91	3
0.91	0.91	0.91	3
0.90	0.90	0.90	3
0.90	0.90	0.90	3
0.90	0.90	0.90	3
0.90	0.90	0.90	3
0.90	0.90	0.90	3
1.40	1.40	1.39	2
1.39	1.39	1.39	2
1.39	1.39	1.39	2
1.39	1.39	1.39	2
1.38	1.38	1.38	2
1.38	1.38	1.38	2
1.38	1.38	1.38	2
1.38	1.38	1.38	2
1.38	1.38	1.37	2
1.37	1.37	1.37	2
1.37	1.37	1.37	2

***** Stresses *****

XI	Total	Effective
10.50	102.44	0.00
10.10	149.46	22.00
9.70	196.46	44.01
9.30	243.45	66.01
8.90	290.43	88.02
8.50	337.40	110.02
8.10	384.36	132.03
7.70	431.31	154.03
7.30	478.24	176.04
6.90	525.17	198.04
6.50	572.08	220.05
6.50	572.08	220.05
5.85	640.91	248.14
5.19	709.67	276.23
4.54	778.41	304.32

***** Pore Pressures *****

Total	Static	Excess	Material
102.44	93.60	8.84	3
127.45	118.61	8.84	3
152.45	143.61	8.84	3
177.44	168.60	8.84	3
202.42	193.58	8.84	3
227.38	218.54	8.84	3
252.33	243.49	8.84	3
277.28	268.44	8.84	3
302.21	293.37	8.84	3
327.13	318.29	8.84	3
352.03	343.19	8.84	3
352.03	343.19	8.84	2
392.77	383.93	8.84	2
433.45	424.61	8.84	2
474.09	465.25	8.84	2

3.89	847.11	332.41	514.70	505.86	8.84	2
3.24	915.78	360.50	555.28	546.44	8.84	2
2.59	984.43	388.59	595.83	586.99	8.84	2
1.94	1053.03	416.68	636.34	627.50	8.84	2
1.29	1121.59	444.78	676.81	667.97	8.84	2
0.65	1190.10	472.87	717.23	708.39	8.84	2
0.00	1258.56	500.96	757.60	748.76	8.84	2

Time = 0. Degree of Consolidation = 0.%

Total Settlement = 0.000

Settlement at End of Primary Consolidation = 0.003

Settlement caused by Primary Consolidation at time 0. = 0.000

Settlement caused by Secondary Compression at time 0. = 0.000

**********Initial Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
1.00	1.00	0.08	11.00	11.00	11.00	4
0.92	0.92	0.08	11.00	11.00	7.16	4
0.83	0.83	0.07	11.00	11.00	6.44	4
0.75	0.75	0.06	11.00	11.00	5.89	4
0.67	0.67	0.06	11.00	11.00	5.53	4
0.58	0.58	0.05	11.00	11.00	5.16	4
0.50	0.50	0.04	11.00	11.00	4.97	4
0.42	0.42	0.03	11.00	11.00	4.93	4
0.33	0.33	0.03	11.00	11.00	4.88	4
0.25	0.25	0.02	11.00	11.00	4.84	4
0.17	0.17	0.01	11.00	11.00	4.79	4
0.08	0.08	0.01	11.00	11.00	4.74	4
0.00	0.00	0.00	11.00	11.00	4.70	4

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
1.00	31.20	0.00	31.20	31.20	0.00	4
0.92	37.14	0.00	37.14	36.40	0.74	4

0.83	43.07	0.00	43.07	41.60	1.47	4
0.75	49.01	0.00	49.01	46.80	2.21	4
0.67	54.95	0.00	54.95	52.00	2.95	4
0.58	60.88	0.00	60.88	57.20	3.68	4
0.50	66.82	0.00	66.82	62.40	4.42	4
0.42	72.76	0.00	72.76	67.60	5.16	4
0.33	78.69	0.00	78.69	72.80	5.89	4
0.25	84.63	0.00	84.63	78.00	6.63	4
0.17	90.57	0.00	90.57	83.20	7.37	4
0.08	96.50	0.00	96.50	88.40	8.10	4
0.00	102.44	0.00	102.44	93.60	8.84	4

Time = 0. Degree of Consolidation = 0.%

Total Settlement = 0.000

Settlement at End of Primary Consolidation = 0.454

Settlement caused by Primary Consolidation at time 0. = 0.000

Settlement caused by Secondary Compression at time 0. = 0.000

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
10.50	10.50	4.83	0.91	0.91	0.91	3
10.10	10.10	4.62	0.91	0.91	0.91	3
9.70	9.70	4.41	0.91	0.91	0.91	3
9.30	9.30	4.20	0.91	0.91	0.91	3
8.90	8.90	3.99	0.91	0.91	0.91	3
8.50	8.50	3.78	0.91	0.91	0.91	3
8.10	8.10	3.57	0.90	0.90	0.90	3
7.70	7.70	3.36	0.90	0.90	0.90	3
7.30	7.30	3.15	0.90	0.90	0.90	3
6.90	6.90	2.94	0.90	0.90	0.90	3
6.50	6.50	2.73	0.90	0.90	0.90	3
6.50	6.50	2.73	1.40	1.40	1.39	2
5.85	5.85	2.46	1.39	1.39	1.39	2
5.19	5.19	2.18	1.39	1.39	1.39	2
4.54	4.54	1.91	1.39	1.39	1.39	2
3.89	3.89	1.64	1.38	1.38	1.38	2

3.24	3.24	1.36	1.38	1.38	1.38	2
2.59	2.59	1.09	1.38	1.38	1.38	2
1.94	1.94	0.82	1.38	1.38	1.38	2
1.29	1.29	0.55	1.38	1.38	1.37	2
0.65	0.65	0.27	1.37	1.37	1.37	2
0.00	0.00	0.00	1.37	1.37	1.37	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
10.50	102.51	2.93	99.58	93.67	5.91	3
10.10	149.53	24.15	125.38	118.68	6.69	3
9.70	196.53	45.39	151.15	143.68	7.46	3
9.30	243.52	66.71	176.81	168.67	8.14	3
8.90	290.51	88.22	202.29	193.65	8.64	3
8.50	337.48	110.02	227.45	218.61	8.84	3
8.10	384.43	132.03	252.41	243.57	8.84	3
7.70	431.38	154.03	277.35	268.51	8.84	3
7.30	478.32	176.04	302.28	293.44	8.84	3
6.90	525.24	198.04	327.20	318.36	8.84	3
6.50	572.15	220.05	352.11	343.27	8.84	3
6.50	572.15	220.05	352.11	343.27	8.84	2
5.85	640.98	248.14	392.84	384.00	8.84	2
5.19	709.75	277.75	432.00	424.68	7.32	2
4.54	778.48	309.64	468.84	465.32	3.52	2
3.89	847.17	340.18	506.99	505.92	1.07	2
3.24	915.83	369.34	546.49	546.49	0.00	2
2.59	984.47	397.43	587.03	587.03	0.00	2
1.94	1053.06	423.21	629.85	627.53	2.31	2
1.29	1121.61	449.48	672.13	667.99	4.14	2
0.65	1190.11	477.98	712.13	708.40	3.73	2
0.00	1258.56	509.41	749.15	748.76	0.39	2

Time = 12. Degree of Consolidation = 42.%

Total Settlement = 0.001

Settlement at End of Primary Consolidation = 0.003

Settlement caused by Primary Consolidation at time 12. = 0.001

Settlement caused by Secondary Compression at time 12. = 0.000

output

**********Current Conditions in Dredged Fill**********

***** Coordinates *****

A	XI	Z	Einitial	E	Eeop	Material
1.00	0.69	0.08	11.00	11.00	11.00	4
0.92	0.62	0.08	11.00	8.32	7.16	4
0.83	0.55	0.07	11.00	8.16	6.44	4
0.75	0.49	0.06	11.00	8.00	5.89	4
0.67	0.43	0.06	11.00	7.77	5.53	4
0.58	0.37	0.05	11.00	7.45	5.16	4
0.50	0.31	0.04	11.00	7.19	4.97	4
0.42	0.25	0.03	11.00	6.97	4.93	4
0.33	0.20	0.03	11.00	6.73	4.88	4
0.25	0.15	0.02	11.00	6.47	4.84	4
0.17	0.10	0.01	11.00	6.19	4.79	4
0.08	0.05	0.01	11.00	5.88	4.74	4
0.00	0.00	0.00	11.00	5.53	4.70	4

***** Void Ratios *****

***** Stresses *****

***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
0.69	50.78	0.00	50.78	50.78	0.00	4
0.62	55.96	0.30	55.65	55.22	0.43	4
0.55	60.70	0.35	60.34	59.22	1.12	4
0.49	65.37	0.40	64.97	63.16	1.81	4
0.43	69.96	0.49	69.47	67.01	2.45	4
0.37	74.43	0.62	73.80	70.74	3.06	4
0.31	78.77	0.72	78.04	74.35	3.70	4
0.25	83.00	0.84	82.17	77.85	4.32	4
0.20	87.14	1.13	86.02	81.25	4.77	4
0.15	91.17	1.44	89.73	84.54	5.19	4
0.10	95.08	1.78	93.31	87.72	5.59	4
0.05	98.87	2.24	96.63	90.77	5.87	4
0.00	102.51	2.93	99.58	93.67	5.91	4

Time = 12. Degree of Consolidation = 69.%

Total Settlement = 0.313

Settlement at End of Primary Consolidation = 0.454

Settlement caused by Primary Consolidation at time 12. = 0.313

Settlement caused by Secondary Compression at time 12. = 0.000

Surface Elevation = -0.81

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****

A	XI	Z
10.50	10.50	4.83
10.10	10.10	4.62
9.70	9.70	4.41
9.30	9.29	4.20
8.90	8.89	3.99
8.50	8.49	3.78
8.10	8.09	3.57
7.70	7.69	3.36
7.30	7.30	3.15
6.90	6.90	2.94
6.50	6.50	2.73
6.50	6.50	2.73
5.85	5.84	2.46
5.19	5.19	2.18
4.54	4.54	1.91
3.89	3.89	1.64
3.24	3.24	1.36
2.59	2.59	1.09
1.94	1.94	0.82
1.29	1.29	0.55
0.65	0.65	0.27
0.00	0.00	0.00

***** Void Ratios *****

Einitial	E	Eeop	Material
0.91	0.91	0.91	3
0.91	0.91	0.91	3
0.91	0.91	0.91	3
0.91	0.91	0.91	3
0.91	0.91	0.91	3
0.91	0.91	0.90	3
0.90	0.90	0.90	3
0.90	0.90	0.90	3
0.90	0.90	0.90	3
0.90	0.90	0.90	3
0.90	0.90	0.90	3
1.40	1.40	1.39	2
1.39	1.39	1.39	2
1.39	1.39	1.39	2
1.39	1.39	1.39	2
1.38	1.38	1.38	2
1.38	1.38	1.38	2
1.38	1.38	1.38	2
1.38	1.38	1.38	2
1.38	1.37	1.37	2
1.37	1.37	1.37	2
1.37	1.37	1.37	2

***** Stresses *****

XI	Total	Effective
10.50	111.44	4.51
10.10	158.46	25.50
9.70	205.46	46.48
9.29	252.45	67.52
8.89	299.43	88.71
8.49	346.40	110.16
8.09	393.36	132.03
7.69	440.31	154.03
7.30	487.24	176.04

***** Pore Pressures *****

Total	Static	Excess	Material
106.93	93.76	13.17	3
132.96	118.77	14.19	3
158.98	143.77	15.21	3
184.94	168.76	16.18	3
210.73	193.74	16.99	3
236.25	218.70	17.55	3
261.33	243.65	17.68	3
286.28	268.60	17.68	3
311.21	293.53	17.68	3

6.90	534.17	198.04	336.13	318.45	17.68	3
6.50	581.08	220.05	361.03	343.35	17.68	3
6.50	581.08	220.05	361.03	343.35	17.68	2
5.84	649.91	248.14	401.77	384.09	17.68	2
5.19	718.67	280.10	438.57	424.76	13.81	2
4.54	787.40	314.25	473.15	465.40	7.75	2
3.89	856.09	346.96	509.13	506.00	3.13	2
3.24	924.74	378.18	546.56	546.56	0.00	2
2.59	993.36	406.27	587.09	587.09	0.00	2
1.94	1061.94	431.09	630.85	627.58	3.28	2
1.29	1130.48	457.51	672.97	668.02	4.95	2
0.65	1198.96	486.49	712.47	708.42	4.05	2
0.00	1267.40	518.28	749.12	748.76	0.36	2

Time = 24. Degree of Consolidation = 47.%

Total Settlement = 0.003

Settlement at End of Primary Consolidation = 0.006

Settlement caused by Primary Consolidation at time 24. = 0.003

Settlement caused by Secondary Compression at time 24. = 0.000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
2.00	1.35	0.17	11.00	11.00	11.00	4
1.92	1.28	0.16	11.00	8.42	7.16	4
1.83	1.22	0.15	11.00	8.47	6.44	4
1.75	1.15	0.15	11.00	8.37	5.89	4
1.67	1.09	0.14	11.00	8.30	5.53	4
1.58	1.02	0.13	11.00	8.23	5.16	4
1.50	0.96	0.13	11.00	8.14	4.97	4
1.42	0.89	0.12	11.00	8.04	4.93	4
1.33	0.83	0.11	11.00	7.90	4.88	4
1.25	0.77	0.10	11.00	7.71	4.84	4
1.17	0.71	0.10	11.00	7.50	4.79	4
1.08	0.65	0.09	11.00	7.33	4.74	4
1.00	0.60	0.08	11.00	7.20	4.70	4
1.00	0.60	0.08	11.00	7.20	4.70	4

0.92	0.54	0.08	11.00	7.06	4.65	4
0.83	0.48	0.07	11.00	6.93	4.61	4
0.75	0.43	0.06	11.00	6.79	4.56	4
0.67	0.37	0.06	11.00	6.64	4.51	4
0.58	0.32	0.05	11.00	6.46	4.47	4
0.50	0.27	0.04	11.00	6.26	4.42	4
0.42	0.22	0.03	11.00	6.02	4.38	4
0.33	0.17	0.03	11.00	5.73	4.33	4
0.25	0.13	0.02	11.00	5.42	4.28	4
0.17	0.08	0.01	11.00	5.22	4.24	4
0.08	0.04	0.01	11.00	5.08	4.19	4
0.00	0.00	0.00	11.00	4.97	4.14	4

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
1.35	9.36	0.00	9.36	9.36	0.00	4
1.28	14.54	0.27	14.27	13.81	0.46	4
1.22	19.38	0.26	19.12	17.91	1.21	4
1.15	24.20	0.29	23.91	21.99	1.92	4
1.09	28.98	0.31	28.67	26.03	2.64	4
1.02	33.73	0.33	33.40	30.05	3.35	4
0.96	38.45	0.36	38.09	34.03	4.06	4
0.89	43.12	0.39	42.73	37.97	4.77	4
0.83	47.75	0.44	47.31	41.86	5.45	4
0.77	52.31	0.52	51.79	45.68	6.11	4
0.71	56.77	0.60	56.17	49.40	6.77	4
0.65	61.15	0.67	60.48	53.05	7.44	4
0.60	65.47	0.72	64.75	56.63	8.12	4
0.60	65.47	0.72	64.75	56.63	8.12	4
0.54	69.73	0.77	68.95	60.15	8.80	4
0.48	73.93	0.88	73.05	63.62	9.43	4
0.43	78.08	1.05	77.03	67.03	10.00	4
0.37	82.16	1.23	80.92	70.37	10.55	4
0.32	86.17	1.45	84.72	73.64	11.08	4
0.27	90.09	1.69	88.41	76.83	11.57	4
0.22	93.93	1.97	91.95	79.93	12.02	4
0.17	97.65	2.54	95.11	82.91	12.19	4
0.13	101.22	3.17	98.06	85.75	12.30	4
0.08	104.70	3.56	101.14	88.49	12.65	4
0.04	108.10	3.84	104.26	91.15	13.11	4
0.00	111.44	4.51	106.93	93.76	13.17	4

Time = 24. Degree of Consolidation = 65.%

Total Settlement = 0.647

Settlement at End of Primary Consolidation = 1.002

Settlement caused by Primary Consolidation at time 24. = 0.647

Settlement caused by Secondary Compression at time 24. = 0.000

Surface Elevation = -0.15

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
10.50	10.50	4.83	0.91	0.91	0.91	3
10.10	10.09	4.62	0.91	0.91	0.91	3
9.70	9.69	4.41	0.91	0.91	0.91	3
9.30	9.29	4.20	0.91	0.91	0.91	3
8.90	8.89	3.99	0.91	0.91	0.91	3
8.50	8.49	3.78	0.91	0.91	0.90	3
8.10	8.09	3.57	0.90	0.90	0.90	3
7.70	7.69	3.36	0.90	0.90	0.90	3
7.30	7.29	3.15	0.90	0.90	0.90	3
6.90	6.89	2.94	0.90	0.90	0.90	3
6.50	6.50	2.73	0.90	0.90	0.90	3
6.50	6.50	2.73	1.40	1.40	1.39	2
5.85	5.84	2.46	1.39	1.39	1.39	2
5.19	5.19	2.18	1.39	1.39	1.39	2
4.54	4.54	1.91	1.39	1.39	1.38	2
3.89	3.89	1.64	1.38	1.38	1.38	2
3.24	3.24	1.36	1.38	1.38	1.38	2
2.59	2.59	1.09	1.38	1.38	1.38	2
1.94	1.94	0.82	1.38	1.38	1.38	2
1.29	1.29	0.55	1.38	1.37	1.37	2
0.65	0.65	0.27	1.37	1.37	1.37	2
0.00	0.00	0.00	1.37	1.37	1.37	2

***** Stresses *****			***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
10.50	152.82	4.62	148.20	126.30	21.90	3
10.09	199.83	25.59	174.24	151.31	22.94	3
9.69	246.84	46.56	200.28	176.31	23.97	3

9.29	293.83	67.58	226.25	201.29	24.95	3
8.89	340.81	88.75	252.06	226.27	25.79	3
8.49	387.78	110.18	277.60	251.23	26.36	3
8.09	434.74	132.03	302.71	276.19	26.52	3
7.69	481.68	154.03	327.65	301.13	26.52	3
7.29	528.62	176.04	352.58	326.06	26.52	3
6.89	575.54	198.04	377.50	350.98	26.52	3
6.50	622.45	220.05	402.41	375.89	26.52	3
6.50	622.45	220.05	402.41	375.89	26.52	2
5.84	691.28	248.14	443.14	416.62	26.52	2
5.19	760.05	282.35	477.70	457.30	20.40	2
4.54	828.77	318.70	510.07	497.93	12.14	2
3.89	897.45	353.63	543.83	538.52	5.30	2
3.24	966.10	387.02	579.08	579.08	0.00	2
2.59	1034.70	414.81	619.90	619.59	0.31	2
1.94	1103.27	439.12	664.15	660.06	4.08	2
1.29	1171.79	465.45	706.34	700.49	5.85	2
0.65	1240.27	494.90	745.36	740.88	4.48	2
0.00	1308.69	527.14	781.55	781.21	0.34	2

Time = 36. Degree of Consolidation = 48.%

Total Settlement = 0.004

Settlement at End of Primary Consolidation = 0.008

Settlement caused by Primary Consolidation at time 36. = 0.004

Settlement caused by Secondary Compression at time 36. = 0.000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
3.00	2.02	0.25	11.00	11.00	11.00	4
2.92	1.95	0.24	11.00	8.45	7.16	4
2.83	1.89	0.24	11.00	8.57	6.44	4
2.75	1.82	0.23	11.00	8.47	5.89	4
2.67	1.75	0.22	11.00	8.43	5.53	4
2.58	1.69	0.22	11.00	8.38	5.16	4
2.50	1.62	0.21	11.00	8.33	4.97	4
2.42	1.56	0.20	11.00	8.29	4.93	4

2.33	1.50	0.19	11.00	8.24	4.88	4
2.25	1.43	0.19	11.00	8.18	4.84	4
2.17	1.37	0.18	11.00	8.12	4.79	4
2.08	1.31	0.17	11.00	8.04	4.74	4
2.00	1.24	0.17	11.00	7.94	4.70	4
2.00	1.24	0.17	11.00	7.94	4.70	4
1.92	1.18	0.16	11.00	7.84	4.65	4
1.83	1.12	0.15	11.00	7.68	4.61	4
1.75	1.06	0.15	11.00	7.50	4.56	4
1.67	1.00	0.14	11.00	7.36	4.51	4
1.58	0.94	0.13	11.00	7.26	4.47	4
1.50	0.89	0.13	11.00	7.17	4.42	4
1.42	0.83	0.12	11.00	7.08	4.38	4
1.33	0.77	0.11	11.00	7.00	4.33	4
1.25	0.72	0.10	11.00	6.90	4.28	4
1.17	0.67	0.10	11.00	6.80	4.24	4
1.08	0.61	0.09	11.00	6.70	4.19	4
1.00	0.56	0.08	11.00	6.58	4.14	4
1.00	0.56	0.08	11.00	6.58	4.14	4
0.92	0.51	0.08	11.00	6.47	4.10	4
0.83	0.45	0.07	11.00	6.34	4.05	4
0.75	0.40	0.06	11.00	6.19	4.01	4
0.67	0.35	0.06	11.00	6.04	3.98	4
0.58	0.31	0.05	11.00	5.86	3.97	4
0.50	0.26	0.04	11.00	5.65	3.95	4
0.42	0.21	0.03	11.00	5.44	3.93	4
0.33	0.17	0.03	11.00	5.30	3.91	4
0.25	0.13	0.02	11.00	5.19	3.89	4
0.17	0.08	0.01	11.00	5.11	3.87	4
0.08	0.04	0.01	11.00	5.03	3.86	4
0.00	0.00	0.00	11.00	4.96	3.84	4

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
2.02	0.00	0.00	0.00	0.00	0.00	4
1.95	5.18	0.26	4.91	4.44	0.47	4
1.89	10.05	0.23	9.82	8.58	1.24	4
1.82	14.91	0.26	14.65	12.70	1.95	4
1.75	19.74	0.27	19.47	16.79	2.68	4
1.69	24.55	0.29	24.26	20.87	3.40	4
1.62	29.34	0.30	29.04	24.92	4.12	4
1.56	34.11	0.31	33.80	28.96	4.84	4
1.50	38.86	0.33	38.54	32.97	5.56	4
1.43	43.59	0.34	43.25	36.96	6.29	4
1.37	48.30	0.36	47.93	40.93	7.00	4
1.31	52.97	0.39	52.58	44.87	7.72	4

1.24	57.60	0.43	57.18	48.76	8.41	4
1.24	57.60	0.43	57.18	48.76	8.41	4
1.18	62.19	0.46	61.73	52.62	9.11	4
1.12	66.73	0.53	66.20	56.42	9.79	4
1.06	71.19	0.60	70.59	60.14	10.45	4
1.00	75.58	0.65	74.92	63.79	11.13	4
0.94	79.91	0.70	79.22	67.39	11.83	4
0.89	84.21	0.73	83.48	70.95	12.53	4
0.83	88.47	0.77	87.70	74.47	13.23	4
0.77	92.69	0.81	91.88	77.95	13.93	4
0.72	96.87	0.92	95.95	81.40	14.55	4
0.67	101.01	1.03	99.97	84.80	15.17	4
0.61	105.10	1.16	103.94	88.16	15.78	4
0.56	109.15	1.30	107.85	91.47	16.38	4
0.56	109.15	1.30	107.85	91.47	16.38	4
0.51	113.15	1.44	111.71	94.73	16.98	4
0.45	117.09	1.60	115.50	97.94	17.56	4
0.40	120.98	1.77	119.21	101.09	18.12	4
0.35	124.80	1.96	122.84	104.17	18.67	4
0.31	128.55	2.29	126.26	107.18	19.08	4
0.26	132.21	2.70	129.51	110.11	19.40	4
0.21	135.78	3.12	132.66	112.94	19.72	4
0.17	139.28	3.40	135.87	115.70	20.17	4
0.13	142.72	3.61	139.10	118.41	20.70	4
0.08	146.12	3.79	142.33	121.07	21.26	4
0.04	149.48	3.94	145.54	123.70	21.84	4
0.00	152.82	4.62	148.20	126.30	21.90	4

Time = 36. Degree of Consolidation = 61.%

Total Settlement = 0.976

Settlement at End of Primary Consolidation = 1.589

Settlement caused by Primary Consolidation at time 36. = 0.976

Settlement caused by Secondary Compression at time 36. = 0.000

Surface Elevation = 0.52

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
10.50	10.49	4.83	0.91	0.91	0.91	3
10.10	10.09	4.62	0.91	0.91	0.91	3
9.70	9.69	4.41	0.91	0.91	0.91	3
9.30	9.29	4.20	0.91	0.91	0.91	3
8.90	8.89	3.99	0.91	0.91	0.91	3
8.50	8.49	3.78	0.91	0.91	0.90	3
8.10	8.09	3.57	0.90	0.90	0.90	3
7.70	7.69	3.36	0.90	0.90	0.90	3
7.30	7.29	3.15	0.90	0.90	0.90	3
6.90	6.89	2.94	0.90	0.90	0.90	3
6.50	6.49	2.73	0.90	0.90	0.90	3
6.50	6.49	2.73	1.40	1.40	1.39	2
5.85	5.84	2.46	1.39	1.39	1.39	2
5.19	5.19	2.18	1.39	1.39	1.39	2
4.54	4.54	1.91	1.39	1.39	1.38	2
3.89	3.89	1.64	1.38	1.38	1.38	2
3.24	3.24	1.36	1.38	1.38	1.38	2
2.59	2.59	1.09	1.38	1.38	1.38	2
1.94	1.94	0.82	1.38	1.38	1.37	2
1.29	1.29	0.55	1.38	1.37	1.37	2
0.65	0.65	0.27	1.37	1.37	1.37	2
0.00	0.00	0.00	1.37	1.37	1.37	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
10.49	203.88	4.66	199.22	168.52	30.70	3
10.09	250.90	25.63	225.27	193.53	31.74	3
9.69	297.90	46.59	251.31	218.53	32.78	3
9.29	344.89	67.60	277.29	243.52	33.77	3
8.89	391.87	88.77	303.10	268.49	34.61	3
8.49	438.84	110.19	328.65	293.46	35.19	3
8.09	485.80	132.03	353.77	318.41	35.36	3
7.69	532.75	154.03	378.71	343.35	35.36	3
7.29	579.68	176.04	403.65	368.29	35.36	3
6.89	626.61	198.04	428.56	393.20	35.36	3
6.49	673.52	220.05	453.47	418.11	35.36	3
6.49	673.52	220.05	453.47	418.11	35.36	2
5.84	742.34	248.14	494.21	458.85	35.36	2
5.19	811.11	284.16	526.95	499.52	27.43	2
4.54	879.83	322.27	557.56	540.15	17.41	2
3.89	948.51	358.98	589.53	580.74	8.79	2
3.24	1017.15	394.36	622.78	621.28	1.50	2
2.59	1085.74	419.83	665.91	661.79	4.12	2
1.94	1154.30	444.82	709.48	702.25	7.23	2

1.29	1222.81	472.11	750.70	742.67	8.03	2
0.65	1291.27	502.78	788.49	783.05	5.45	2
0.00	1359.68	535.94	823.74	823.36	0.38	2

Time = 48. Degree of Consolidation = 46.%

Total Settlement = 0.005

Settlement at End of Primary Consolidation = 0.011

Settlement caused by Primary Consolidation at time 48. = 0.005

Settlement caused by Secondary Compression at time 48. = 0.000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
4.00	2.70	0.33	11.00	11.00	11.00	4
3.92	2.63	0.33	11.00	8.47	7.16	4
3.83	2.56	0.32	11.00	8.61	6.44	4
3.75	2.50	0.31	11.00	8.51	5.89	4
3.67	2.43	0.31	11.00	8.48	5.53	4
3.58	2.37	0.30	11.00	8.44	5.16	4
3.50	2.30	0.29	11.00	8.41	4.97	4
3.42	2.23	0.28	11.00	8.38	4.93	4
3.33	2.17	0.28	11.00	8.35	4.88	4
3.25	2.10	0.27	11.00	8.31	4.84	4
3.17	2.04	0.26	11.00	8.28	4.79	4
3.08	1.98	0.26	11.00	8.25	4.74	4
3.00	1.91	0.25	11.00	8.21	4.70	4
3.00	1.91	0.25	11.00	8.21	4.70	4
2.92	1.85	0.24	11.00	8.17	4.65	4
2.83	1.78	0.24	11.00	8.13	4.61	4
2.75	1.72	0.23	11.00	8.08	4.56	4
2.67	1.66	0.22	11.00	8.02	4.51	4
2.58	1.60	0.22	11.00	7.93	4.47	4
2.50	1.53	0.21	11.00	7.81	4.42	4
2.42	1.47	0.20	11.00	7.67	4.38	4
2.33	1.41	0.19	11.00	7.52	4.33	4
2.25	1.36	0.19	11.00	7.40	4.28	4
2.17	1.30	0.18	11.00	7.32	4.24	4

2.08	1.24	0.17	11.00	7.24	4.19	4
2.00	1.18	0.17	11.00	7.18	4.14	4
2.00	1.18	0.17	11.00	7.18	4.14	4
1.92	1.13	0.16	11.00	7.11	4.10	4
1.83	1.07	0.15	11.00	7.05	4.05	4
1.75	1.01	0.15	11.00	6.98	4.01	4
1.67	0.96	0.14	11.00	6.91	3.98	4
1.58	0.90	0.13	11.00	6.84	3.97	4
1.50	0.85	0.13	11.00	6.76	3.95	4
1.42	0.80	0.12	11.00	6.67	3.93	4
1.33	0.74	0.11	11.00	6.59	3.91	4
1.25	0.69	0.10	11.00	6.49	3.89	4
1.17	0.64	0.10	11.00	6.39	3.87	4
1.08	0.59	0.09	11.00	6.29	3.86	4
1.00	0.54	0.08	11.00	6.18	3.84	4
1.00	0.54	0.08	11.00	6.18	3.84	4
0.92	0.49	0.08	11.00	6.06	3.82	4
0.83	0.44	0.07	11.00	5.94	3.80	4
0.75	0.39	0.06	11.00	5.80	3.78	4
0.67	0.35	0.06	11.00	5.65	3.76	4
0.58	0.30	0.05	11.00	5.48	3.74	4
0.50	0.26	0.04	11.00	5.36	3.73	4
0.42	0.21	0.03	11.00	5.27	3.71	4
0.33	0.17	0.03	11.00	5.19	3.69	4
0.25	0.13	0.02	11.00	5.12	3.67	4
0.17	0.08	0.01	11.00	5.06	3.65	4
0.08	0.04	0.01	11.00	5.01	3.63	4
0.00	0.00	0.00	11.00	4.96	3.62	4

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
2.70	0.00	0.00	0.00	0.00	0.00	4
2.63	5.18	0.26	4.92	4.44	0.48	4
2.56	10.06	0.22	9.85	8.59	1.26	4
2.50	14.94	0.25	14.69	12.73	1.96	4
2.43	19.79	0.25	19.53	16.84	2.69	4
2.37	24.63	0.27	24.36	20.94	3.42	4
2.30	29.45	0.28	29.17	25.03	4.14	4
2.23	34.25	0.29	33.97	29.10	4.87	4
2.17	39.05	0.30	38.75	33.15	5.60	4
2.10	43.83	0.31	43.52	37.20	6.32	4
2.04	48.59	0.32	48.28	41.23	7.05	4
1.98	53.34	0.33	53.02	45.24	7.78	4
1.91	58.08	0.34	57.74	49.24	8.50	4
1.91	58.08	0.34	57.74	49.24	8.50	4
1.85	62.80	0.35	62.45	53.22	9.23	4

1.78	67.50	0.36	67.14	57.19	9.95	4
1.72	72.19	0.38	71.81	61.14	10.67	4
1.66	76.85	0.39	76.45	65.06	11.39	4
1.60	81.47	0.43	81.05	68.95	12.10	4
1.53	86.06	0.47	85.58	72.80	12.79	4
1.47	90.58	0.53	90.05	76.58	13.46	4
1.41	95.04	0.59	94.45	80.31	14.14	4
1.36	99.44	0.64	98.80	83.97	14.83	4
1.30	103.80	0.67	103.13	87.59	15.53	4
1.24	108.12	0.70	107.42	91.18	16.24	4
1.18	112.42	0.73	111.69	94.74	16.95	4
1.18	112.42	0.73	111.69	94.74	16.95	4
1.13	116.68	0.76	115.93	98.27	17.66	4
1.07	120.92	0.78	120.14	101.77	18.37	4
1.01	125.13	0.82	124.31	105.24	19.07	4
0.96	129.31	0.91	128.40	108.68	19.72	4
0.90	133.46	0.99	132.46	112.10	20.37	4
0.85	137.58	1.09	136.49	115.48	21.01	4
0.80	141.66	1.19	140.47	118.82	21.65	4
0.74	145.70	1.30	144.40	122.13	22.28	4
0.69	149.70	1.41	148.29	125.39	22.90	4
0.64	153.66	1.53	152.14	128.62	23.52	4
0.59	157.58	1.66	155.93	131.80	24.13	4
0.54	161.45	1.79	159.66	134.93	24.73	4
0.54	161.45	1.79	159.66	134.93	24.73	4
0.49	165.27	1.92	163.35	138.02	25.33	4
0.44	169.05	2.12	166.93	141.05	25.88	4
0.39	172.76	2.39	170.37	144.03	26.34	4
0.35	176.41	2.70	173.72	146.95	26.77	4
0.30	180.00	3.03	176.96	149.79	27.17	4
0.26	183.51	3.28	180.23	152.57	27.66	4
0.21	186.98	3.47	183.52	155.31	28.21	4
0.17	190.42	3.62	186.80	158.01	28.79	4
0.13	193.82	3.75	190.07	160.67	29.40	4
0.08	197.20	3.87	193.33	163.31	30.01	4
0.04	200.55	3.98	196.57	165.93	30.64	4
0.00	203.88	4.66	199.22	168.52	30.70	4

Time = 48. Degree of Consolidation = 59.%

Total Settlement = 1.299

Settlement at End of Primary Consolidation = 2.195

Settlement caused by Primary Consolidation at time 48. = 1.299

Settlement caused by Secondary Compression at time 48. = 0.000

Surface Elevation = 1.20

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****

A	XI	Z
10.50	10.49	4.83
10.10	10.09	4.62
9.70	9.69	4.41
9.30	9.29	4.20
8.90	8.89	3.99
8.50	8.49	3.78
8.10	8.09	3.57
7.70	7.69	3.36
7.30	7.29	3.15
6.90	6.89	2.94
6.50	6.49	2.73
6.50	6.49	2.73
5.85	5.84	2.46
5.19	5.19	2.18
4.54	4.54	1.91
3.89	3.89	1.64
3.24	3.24	1.36
2.59	2.59	1.09
1.94	1.94	0.82
1.29	1.29	0.55
0.65	0.65	0.27
0.00	0.00	0.00

***** Void Ratios *****

Einitial	E	Eeop	Material
0.91	0.91	0.91	3
0.91	0.91	0.91	3
0.91	0.91	0.91	3
0.91	0.91	0.91	3
0.91	0.91	0.90	3
0.91	0.91	0.90	3
0.90	0.90	0.90	3
0.90	0.90	0.90	3
0.90	0.90	0.90	3
0.90	0.90	0.90	3
0.90	0.90	0.90	3
1.40	1.40	1.39	2
1.39	1.39	1.39	2
1.39	1.39	1.39	2
1.39	1.39	1.38	2
1.38	1.38	1.38	2
1.38	1.38	1.38	2
1.38	1.38	1.38	2
1.38	1.38	1.37	2
1.38	1.37	1.37	2
1.37	1.37	1.37	2
1.37	1.37	1.37	2

***** Stresses *****

XI	Total	Effective
10.49	254.85	4.76
10.09	301.86	25.71
9.69	348.87	46.65
9.29	395.86	67.65
8.89	442.84	88.80
8.49	489.81	110.20
8.09	536.77	132.03
7.69	583.71	154.03
7.29	630.65	176.04

***** Pore Pressures *****

Total	Static	Excess	Material
250.09	210.65	39.44	3
276.16	235.66	40.50	3
302.22	260.66	41.56	3
328.21	285.64	42.56	3
354.04	310.62	43.42	3
379.60	335.58	44.02	3
404.74	360.54	44.20	3
429.68	385.48	44.20	3
454.61	410.41	44.20	3

output

6.89	677.57	198.04	479.53	435.33	44.20	3
6.49	724.48	220.05	504.44	460.24	44.20	3
6.49	724.48	220.05	504.44	460.24	44.20	2
5.84	793.31	248.14	545.17	500.97	44.20	2
5.19	862.07	285.56	576.51	541.65	34.87	2
4.54	930.79	324.97	605.82	582.27	23.55	2
3.89	999.47	362.85	636.62	622.86	13.76	2
3.24	1068.10	399.25	668.85	663.40	5.45	2
2.59	1136.69	423.88	712.82	703.90	8.92	2
1.94	1205.24	449.94	755.30	744.35	10.95	2
1.29	1273.74	478.59	795.15	784.76	10.39	2
0.65	1342.19	510.61	831.59	825.12	6.46	2
0.00	1410.58	544.72	865.87	865.43	0.44	2

Time = 60. Degree of Consolidation = 44.%

Total Settlement = 0.006

Settlement at End of Primary Consolidation = 0.014

Settlement caused by Primary Consolidation at time 60. = 0.006

Settlement caused by Secondary Compression at time 60. = 0.000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
5.00	3.38	0.42	11.00	11.00	11.00	4
4.92	3.30	0.41	11.00	8.47	7.16	4
4.83	3.24	0.40	11.00	8.63	6.44	4
4.75	3.17	0.40	11.00	8.53	5.89	4
4.67	3.11	0.39	11.00	8.51	5.53	4
4.58	3.04	0.38	11.00	8.47	5.16	4
4.50	2.97	0.37	11.00	8.45	4.97	4
4.42	2.91	0.37	11.00	8.42	4.93	4
4.33	2.84	0.36	11.00	8.40	4.88	4
4.25	2.78	0.35	11.00	8.38	4.84	4
4.17	2.71	0.35	11.00	8.35	4.79	4
4.08	2.65	0.34	11.00	8.33	4.74	4
4.00	2.58	0.33	11.00	8.30	4.70	4
4.00	2.58	0.33	11.00	8.30	4.70	4

			output			
3.92	2.52	0.33	11.00	8.28	4.65	4
3.83	2.45	0.32	11.00	8.26	4.61	4
3.75	2.39	0.31	11.00	8.23	4.56	4
3.67	2.33	0.31	11.00	8.20	4.51	4
3.58	2.26	0.30	11.00	8.17	4.47	4
3.50	2.20	0.29	11.00	8.13	4.42	4
3.42	2.14	0.28	11.00	8.09	4.38	4
3.33	2.07	0.28	11.00	8.04	4.33	4
3.25	2.01	0.27	11.00	7.98	4.28	4
3.17	1.95	0.26	11.00	7.89	4.24	4
3.08	1.89	0.26	11.00	7.77	4.19	4
3.00	1.83	0.25	11.00	7.65	4.14	4
3.00	1.83	0.25	11.00	7.65	4.14	4
2.92	1.77	0.24	11.00	7.52	4.10	4
2.83	1.71	0.24	11.00	7.42	4.05	4
2.75	1.65	0.23	11.00	7.34	4.01	4
2.67	1.59	0.22	11.00	7.28	3.98	4
2.58	1.53	0.22	11.00	7.22	3.97	4
2.50	1.48	0.21	11.00	7.17	3.95	4
2.42	1.42	0.20	11.00	7.12	3.93	4
2.33	1.36	0.19	11.00	7.07	3.91	4
2.25	1.31	0.19	11.00	7.02	3.89	4
2.17	1.25	0.18	11.00	6.96	3.87	4
2.08	1.20	0.17	11.00	6.91	3.86	4
2.00	1.14	0.17	11.00	6.85	3.84	4
2.00	1.14	0.17	11.00	6.85	3.84	4
1.92	1.09	0.16	11.00	6.79	3.82	4
1.83	1.04	0.15	11.00	6.73	3.80	4
1.75	0.98	0.15	11.00	6.66	3.78	4
1.67	0.93	0.14	11.00	6.59	3.76	4
1.58	0.88	0.13	11.00	6.52	3.74	4
1.50	0.82	0.13	11.00	6.44	3.73	4
1.42	0.77	0.12	11.00	6.35	3.71	4
1.33	0.72	0.11	11.00	6.26	3.69	4
1.25	0.67	0.10	11.00	6.17	3.67	4
1.17	0.62	0.10	11.00	6.07	3.65	4
1.08	0.57	0.09	11.00	5.97	3.63	4
1.00	0.53	0.08	11.00	5.87	3.62	4
1.00	0.53	0.08	11.00	5.87	3.62	4
0.92	0.48	0.08	11.00	5.76	3.60	4
0.83	0.43	0.07	11.00	5.65	3.58	4
0.75	0.39	0.06	11.00	5.52	3.56	4
0.67	0.34	0.06	11.00	5.41	3.54	4
0.58	0.30	0.05	11.00	5.32	3.52	4
0.50	0.25	0.04	11.00	5.25	3.51	4
0.42	0.21	0.03	11.00	5.19	3.49	4
0.33	0.17	0.03	11.00	5.14	3.48	4
0.25	0.13	0.02	11.00	5.09	3.48	4

0.17	0.08	0.01	11.00	5.04	3.47	4
0.08	0.04	0.01	11.00	4.99	3.46	4
0.00	0.00	0.00	11.00	4.95	3.45	4

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
3.38	0.00	0.00	0.00	0.00	0.00	4
3.30	5.18	0.26	4.92	4.44	0.48	4
3.24	10.07	0.21	9.86	8.60	1.26	4
3.17	14.95	0.24	14.71	12.74	1.97	4
3.11	19.81	0.25	19.57	16.87	2.70	4
3.04	24.66	0.26	24.40	20.98	3.43	4
2.97	29.50	0.27	29.23	25.08	4.15	4
2.91	34.32	0.27	34.05	29.17	4.88	4
2.84	39.14	0.28	38.86	33.25	5.61	4
2.78	43.94	0.29	43.66	37.31	6.34	4
2.71	48.74	0.29	48.44	41.37	7.07	4
2.65	53.52	0.30	53.22	45.42	7.80	4
2.58	58.30	0.31	57.99	49.46	8.53	4
2.58	58.30	0.31	57.99	49.46	8.53	4
2.52	63.06	0.32	62.74	53.48	9.26	4
2.45	67.81	0.32	67.49	57.50	9.99	4
2.39	72.55	0.33	72.22	61.50	10.72	4
2.33	77.28	0.34	76.94	65.50	11.45	4
2.26	82.00	0.35	81.65	69.48	12.17	4
2.20	86.70	0.36	86.34	73.44	12.90	4
2.14	91.39	0.37	91.02	77.39	13.62	4
2.07	96.06	0.39	95.67	81.32	14.35	4
2.01	100.70	0.41	100.29	85.23	15.06	4
1.95	105.31	0.44	104.86	89.10	15.76	4
1.89	109.87	0.49	109.38	92.93	16.45	4
1.83	114.38	0.54	113.84	96.70	17.14	4
1.83	114.38	0.54	113.84	96.70	17.14	4
1.77	118.84	0.59	118.25	100.42	17.82	4
1.71	123.24	0.63	122.61	104.09	18.52	4
1.65	127.61	0.66	126.94	107.72	19.23	4
1.59	131.95	0.69	131.26	111.32	19.94	4
1.53	136.26	0.71	135.54	114.89	20.65	4
1.48	140.54	0.73	139.81	118.44	21.37	4
1.42	144.81	0.75	144.05	121.97	22.08	4
1.36	149.05	0.77	148.28	125.48	22.80	4
1.31	153.27	0.79	152.48	128.96	23.52	4
1.25	157.47	0.84	156.63	132.42	24.20	4
1.20	161.65	0.91	160.74	135.86	24.87	4
1.14	165.80	0.98	164.82	139.28	25.54	4
1.14	165.80	0.98	164.82	139.28	25.54	4

1.09	169.93	1.05	168.88	142.67	26.21	4
1.04	174.03	1.12	172.90	146.03	26.87	4
0.98	178.10	1.20	176.90	149.37	27.53	4
0.93	182.14	1.29	180.85	152.67	28.18	4
0.88	186.15	1.38	184.77	155.95	28.82	4
0.82	190.13	1.48	188.65	159.19	29.46	4
0.77	194.07	1.58	192.49	162.39	30.10	4
0.72	197.97	1.68	196.29	165.56	30.73	4
0.67	201.84	1.79	200.04	168.69	31.36	4
0.62	205.66	1.91	203.75	171.78	31.98	4
0.57	209.44	2.05	207.39	174.82	32.57	4
0.53	213.18	2.26	210.92	177.82	33.10	4
0.53	213.18	2.26	210.92	177.82	33.10	4
0.48	216.87	2.47	214.40	180.77	33.62	4
0.43	220.51	2.71	217.81	183.68	34.13	4
0.39	224.10	2.96	221.14	186.53	34.61	4
0.34	227.64	3.19	224.45	189.33	35.12	4
0.30	231.13	3.36	227.78	192.09	35.69	4
0.25	234.59	3.50	231.10	194.81	36.28	4
0.21	238.02	3.62	234.41	197.51	36.90	4
0.17	241.43	3.73	237.70	200.18	37.53	4
0.13	244.82	3.83	240.99	202.83	38.16	4
0.08	248.18	3.92	244.26	205.45	38.80	4
0.04	251.52	4.08	247.44	208.06	39.38	4
0.00	254.85	4.76	250.09	210.65	39.44	4

Time = 60. Degree of Consolidation = 58.%

Total Settlement = 1.624

Settlement at End of Primary Consolidation = 2.819

Settlement caused by Primary Consolidation at time 60. = 1.624

Settlement caused by Secondary Compression at time 60. = 0.000

Surface Elevation = 1.87

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material

10.50	10.49	4.83	0.91	0.91	0.91	3
10.10	10.09	4.62	0.91	0.91	0.91	3
9.70	9.69	4.41	0.91	0.91	0.91	3
9.30	9.29	4.20	0.91	0.91	0.91	3
8.90	8.89	3.99	0.91	0.91	0.90	3
8.50	8.49	3.78	0.91	0.91	0.90	3
8.10	8.09	3.57	0.90	0.90	0.90	3
7.70	7.69	3.36	0.90	0.90	0.90	3
7.30	7.29	3.15	0.90	0.90	0.90	3
6.90	6.89	2.94	0.90	0.90	0.90	3
6.50	6.49	2.73	0.90	0.90	0.90	3
6.50	6.49	2.73	1.40	1.40	1.39	2
5.85	5.84	2.46	1.39	1.39	1.39	2
5.19	5.19	2.18	1.39	1.39	1.38	2
4.54	4.54	1.91	1.39	1.38	1.38	2
3.89	3.89	1.64	1.38	1.38	1.38	2
3.24	3.24	1.36	1.38	1.38	1.38	2
2.59	2.59	1.09	1.38	1.38	1.38	2
1.94	1.94	0.82	1.38	1.37	1.37	2
1.29	1.29	0.55	1.38	1.37	1.37	2
0.65	0.65	0.27	1.37	1.37	1.37	2
0.00	0.00	0.00	1.37	1.36	1.36	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
10.49	323.33	4.80	318.54	270.29	48.24	3
10.09	370.35	25.74	344.61	295.30	49.31	3
9.69	417.35	46.67	370.68	320.30	50.37	3
9.29	464.34	67.67	396.67	345.29	51.38	3
8.89	511.32	88.81	422.51	370.26	52.25	3
8.49	558.29	110.21	448.08	395.23	52.85	3
8.09	605.25	132.03	473.22	420.18	53.04	3
7.69	652.20	154.03	498.16	445.12	53.04	3
7.29	699.13	176.04	523.10	470.06	53.04	3
6.89	746.06	198.04	548.01	494.97	53.04	3
6.49	792.97	220.05	572.92	519.88	53.04	3
6.49	792.97	220.05	572.92	519.88	53.04	2
5.84	861.79	248.14	613.66	560.62	53.04	2
5.19	930.56	285.66	644.89	601.29	43.60	2
4.54	999.28	325.17	674.11	641.92	32.19	2
3.89	1067.95	363.12	704.83	682.50	22.33	2
3.24	1136.58	399.57	737.01	723.04	13.97	2
2.59	1205.17	424.12	781.05	763.54	17.51	2
1.94	1273.72	450.25	823.47	804.00	19.48	2
1.29	1342.22	479.24	862.98	844.41	18.58	2
0.65	1410.67	513.03	897.64	884.76	12.88	2

output

0.00	1479.06	553.11	925.95	925.06	0.89	2

Time = 61. Degree of Consolidation = 38.%

Total Settlement = 0.006

Settlement at End of Primary Consolidation = 0.017

Settlement caused by Primary Consolidation at time 61. = 0.006

Settlement caused by Secondary Compression at time 61. = 0.000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
6.00	4.33	0.50	11.00	11.00	11.00	4
5.99	4.32	0.50	11.00	11.00	9.23	4
5.98	4.31	0.50	11.00	11.00	8.74	4
5.97	4.30	0.50	11.00	11.00	8.45	4
5.96	4.29	0.50	11.00	11.00	8.15	4
5.95	4.28	0.50	11.00	11.00	7.89	4
5.94	4.27	0.50	11.00	11.00	7.67	4
5.93	4.26	0.49	11.00	11.00	7.45	4
5.92	4.25	0.49	11.00	11.00	7.23	4
5.91	4.24	0.49	11.00	11.00	7.01	4
5.90	4.23	0.49	11.00	11.00	6.93	4
5.89	4.22	0.49	11.00	11.00	6.86	4
5.88	4.21	0.49	11.00	11.00	6.78	4
5.87	4.20	0.49	11.00	11.00	6.71	4
5.86	4.19	0.49	11.00	11.00	6.64	4
5.85	4.18	0.49	11.00	11.00	6.56	4
5.84	4.17	0.49	11.00	11.00	6.49	4
5.83	4.16	0.49	11.00	11.00	6.41	4
5.82	4.15	0.49	11.00	11.00	6.34	4
5.81	4.14	0.48	11.00	11.00	6.27	4
5.80	4.13	0.48	11.00	11.00	6.19	4
5.79	4.12	0.48	11.00	11.00	6.12	4
5.78	4.11	0.48	11.00	11.00	6.05	4
5.77	4.10	0.48	11.00	11.00	5.98	4
5.76	4.09	0.48	11.00	11.00	5.94	4
5.75	4.08	0.48	11.00	11.00	5.89	4

output

5.74	4.07	0.48	11.00	11.00	5.85	4
5.73	4.06	0.48	11.00	11.00	5.81	4
5.72	4.05	0.48	11.00	11.00	5.76	4
5.71	4.04	0.48	11.00	11.00	5.72	4
5.70	4.03	0.48	11.00	11.00	5.67	4
5.69	4.02	0.47	11.00	11.00	5.63	4
5.68	4.01	0.47	11.00	11.00	5.59	4
5.67	4.00	0.47	11.00	11.00	5.54	4
5.66	3.99	0.47	11.00	11.00	5.50	4
5.65	3.98	0.47	11.00	11.00	5.45	4
5.64	3.97	0.47	11.00	11.00	5.41	4
5.63	3.96	0.47	11.00	11.00	5.36	4
5.62	3.95	0.47	11.00	11.00	5.32	4
5.61	3.94	0.47	11.00	11.00	5.28	4
5.60	3.93	0.47	11.00	11.00	5.23	4
5.59	3.92	0.47	11.00	11.00	5.19	4
5.58	3.91	0.47	11.00	11.00	5.14	4
5.57	3.90	0.46	11.00	11.00	5.10	4
5.56	3.89	0.46	11.00	11.00	5.06	4
5.55	3.88	0.46	11.00	11.00	5.01	4
5.54	3.87	0.46	11.00	11.00	5.00	4
5.53	3.86	0.46	11.00	11.00	4.99	4
5.52	3.85	0.46	11.00	11.00	4.98	4
5.51	3.84	0.46	11.00	11.00	4.98	4
5.50	3.83	0.46	11.00	11.00	4.97	4
5.49	3.82	0.46	11.00	11.00	4.97	4
5.48	3.81	0.46	11.00	11.00	4.96	4
5.47	3.80	0.46	11.00	11.00	4.96	4
5.46	3.79	0.46	11.00	11.00	4.95	4
5.45	3.78	0.45	11.00	11.00	4.95	4
5.44	3.77	0.45	11.00	11.00	4.94	4
5.43	3.76	0.45	11.00	11.00	4.94	4
5.42	3.75	0.45	11.00	11.00	4.93	4
5.41	3.74	0.45	11.00	11.00	4.92	4
5.40	3.73	0.45	11.00	11.00	4.92	4
5.39	3.72	0.45	11.00	11.00	4.91	4
5.38	3.71	0.45	11.00	10.99	4.91	4
5.37	3.70	0.45	11.00	10.99	4.90	4
5.36	3.69	0.45	11.00	10.99	4.90	4
5.35	3.68	0.45	11.00	10.98	4.89	4
5.34	3.67	0.45	11.00	10.97	4.89	4
5.33	3.66	0.44	11.00	10.96	4.88	4
5.32	3.65	0.44	11.00	10.95	4.87	4
5.31	3.64	0.44	11.00	10.93	4.87	4
5.30	3.63	0.44	11.00	10.91	4.86	4
5.29	3.62	0.44	11.00	10.89	4.86	4
5.28	3.61	0.44	11.00	10.86	4.85	4
5.27	3.60	0.44	11.00	10.83	4.85	4

output

5.26	3.59	0.44	11.00	10.78	4.84	4
5.25	3.58	0.44	11.00	10.74	4.84	4
5.24	3.57	0.44	11.00	10.68	4.83	4
5.23	3.56	0.44	11.00	10.62	4.82	4
5.22	3.55	0.43	11.00	10.55	4.82	4
5.21	3.54	0.43	11.00	10.47	4.81	4
5.20	3.53	0.43	11.00	10.39	4.81	4
5.19	3.52	0.43	11.00	10.30	4.80	4
5.18	3.52	0.43	11.00	10.20	4.80	4
5.17	3.51	0.43	11.00	10.10	4.79	4
5.16	3.50	0.43	11.00	9.99	4.79	4
5.15	3.49	0.43	11.00	9.88	4.78	4
5.14	3.48	0.43	11.00	9.77	4.77	4
5.13	3.47	0.43	11.00	9.66	4.77	4
5.12	3.46	0.43	11.00	9.55	4.76	4
5.11	3.45	0.43	11.00	9.44	4.76	4
5.10	3.44	0.42	11.00	9.34	4.75	4
5.09	3.44	0.42	11.00	9.24	4.75	4
5.08	3.43	0.42	11.00	9.15	4.74	4
5.07	3.42	0.42	11.00	9.07	4.74	4
5.06	3.41	0.42	11.00	9.00	4.73	4
5.05	3.40	0.42	11.00	8.94	4.73	4
5.04	3.39	0.42	11.00	8.89	4.72	4
5.03	3.39	0.42	11.00	8.85	4.71	4
5.02	3.38	0.42	11.00	8.81	4.71	4
5.01	3.37	0.42	11.00	8.77	4.70	4
5.00	3.36	0.42	11.00	8.74	4.70	4
5.00	3.36	0.42	11.00	8.74	4.70	4
4.92	3.29	0.41	11.00	8.47	4.65	4
4.83	3.23	0.40	11.00	8.57	4.61	4
4.75	3.16	0.40	11.00	8.50	4.56	4
4.67	3.10	0.39	11.00	8.48	4.51	4
4.58	3.03	0.38	11.00	8.45	4.47	4
4.50	2.96	0.37	11.00	8.43	4.42	4
4.42	2.90	0.37	11.00	8.40	4.38	4
4.33	2.83	0.36	11.00	8.38	4.33	4
4.25	2.77	0.35	11.00	8.36	4.28	4
4.17	2.70	0.35	11.00	8.33	4.24	4
4.08	2.64	0.34	11.00	8.31	4.19	4
4.00	2.57	0.33	11.00	8.29	4.14	4
4.00	2.57	0.33	11.00	8.29	4.14	4
3.92	2.51	0.33	11.00	8.26	4.10	4
3.83	2.45	0.32	11.00	8.24	4.05	4
3.75	2.38	0.31	11.00	8.21	4.01	4
3.67	2.32	0.31	11.00	8.18	3.98	4
3.58	2.25	0.30	11.00	8.15	3.97	4
3.50	2.19	0.29	11.00	8.11	3.95	4
3.42	2.13	0.28	11.00	8.06	3.93	4

3.33	2.07	0.28	11.00	8.01	3.91	4
3.25	2.00	0.27	11.00	7.93	3.89	4
3.17	1.94	0.26	11.00	7.83	3.87	4
3.08	1.88	0.26	11.00	7.70	3.86	4
3.00	1.82	0.25	11.00	7.58	3.84	4
3.00	1.82	0.25	11.00	7.58	3.84	4
2.92	1.76	0.24	11.00	7.45	3.82	4
2.83	1.70	0.24	11.00	7.37	3.80	4
2.75	1.65	0.23	11.00	7.30	3.78	4
2.67	1.59	0.22	11.00	7.25	3.76	4
2.58	1.53	0.22	11.00	7.19	3.74	4
2.50	1.47	0.21	11.00	7.14	3.73	4
2.42	1.42	0.20	11.00	7.09	3.71	4
2.33	1.36	0.19	11.00	7.04	3.69	4
2.25	1.31	0.19	11.00	6.99	3.67	4
2.17	1.25	0.18	11.00	6.94	3.65	4
2.08	1.20	0.17	11.00	6.89	3.63	4
2.00	1.14	0.17	11.00	6.83	3.62	4
2.00	1.14	0.17	11.00	6.83	3.62	4
1.92	1.09	0.16	11.00	6.77	3.60	4
1.83	1.03	0.15	11.00	6.71	3.58	4
1.75	0.98	0.15	11.00	6.64	3.56	4
1.67	0.93	0.14	11.00	6.57	3.54	4
1.58	0.87	0.13	11.00	6.49	3.52	4
1.50	0.82	0.13	11.00	6.41	3.51	4
1.42	0.77	0.12	11.00	6.33	3.49	4
1.33	0.72	0.11	11.00	6.24	3.48	4
1.25	0.67	0.10	11.00	6.15	3.48	4
1.17	0.62	0.10	11.00	6.05	3.47	4
1.08	0.57	0.09	11.00	5.95	3.46	4
1.00	0.53	0.08	11.00	5.85	3.45	4
1.00	0.53	0.08	11.00	5.85	3.45	4
0.92	0.48	0.08	11.00	5.74	3.44	4
0.83	0.43	0.07	11.00	5.63	3.43	4
0.75	0.39	0.06	11.00	5.50	3.42	4
0.67	0.34	0.06	11.00	5.39	3.41	4
0.58	0.30	0.05	11.00	5.31	3.40	4
0.50	0.25	0.04	11.00	5.25	3.39	4
0.42	0.21	0.03	11.00	5.19	3.38	4
0.33	0.17	0.03	11.00	5.13	3.37	4
0.25	0.13	0.02	11.00	5.08	3.36	4
0.17	0.08	0.01	11.00	5.04	3.36	4
0.08	0.04	0.01	11.00	4.99	3.35	4
0.00	0.00	0.00	11.00	4.95	3.34	4

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	output Total	Static	Excess	Material
4.33	0.00	0.00	0.00	0.00	0.00	4
4.32	0.71	0.00	0.71	0.62	0.09	4
4.31	1.42	0.00	1.42	1.25	0.18	4
4.30	2.14	0.00	2.14	1.87	0.27	4
4.29	2.85	0.00	2.85	2.50	0.35	4
4.28	3.56	0.00	3.56	3.12	0.44	4
4.27	4.27	0.00	4.27	3.74	0.53	4
4.26	4.99	0.00	4.99	4.37	0.62	4
4.25	5.70	0.00	5.70	4.99	0.71	4
4.24	6.41	0.00	6.41	5.62	0.80	4
4.23	7.12	0.00	7.12	6.24	0.88	4
4.22	7.84	0.00	7.84	6.86	0.97	4
4.21	8.55	0.00	8.55	7.49	1.06	4
4.20	9.26	0.00	9.26	8.11	1.15	4
4.19	9.97	0.00	9.97	8.74	1.24	4
4.18	10.69	0.00	10.69	9.36	1.33	4
4.17	11.40	0.00	11.40	9.98	1.41	4
4.16	12.11	0.00	12.11	10.61	1.50	4
4.15	12.82	0.00	12.82	11.23	1.59	4
4.14	13.54	0.00	13.54	11.86	1.68	4
4.13	14.25	0.00	14.25	12.48	1.77	4
4.12	14.96	0.00	14.96	13.10	1.86	4
4.11	15.67	0.00	15.67	13.73	1.94	4
4.10	16.39	0.00	16.39	14.35	2.03	4
4.09	17.10	0.00	17.10	14.98	2.12	4
4.08	17.81	0.00	17.81	15.60	2.21	4
4.07	18.52	0.00	18.52	16.22	2.30	4
4.06	19.23	0.00	19.23	16.85	2.39	4
4.05	19.95	0.00	19.95	17.47	2.48	4
4.04	20.66	0.00	20.66	18.10	2.56	4
4.03	21.37	0.00	21.37	18.72	2.65	4
4.02	22.08	0.00	22.08	19.34	2.74	4
4.01	22.80	0.00	22.80	19.97	2.83	4
4.00	23.51	0.00	23.51	20.59	2.92	4
3.99	24.22	0.00	24.22	21.22	3.01	4
3.98	24.93	0.00	24.93	21.84	3.09	4
3.97	25.65	0.00	25.65	22.46	3.18	4
3.96	26.36	0.00	26.36	23.09	3.27	4
3.95	27.07	0.00	27.07	23.71	3.36	4
3.94	27.78	0.00	27.78	24.34	3.45	4
3.93	28.50	0.00	28.50	24.96	3.54	4
3.92	29.21	0.00	29.21	25.58	3.62	4
3.91	29.92	0.00	29.92	26.21	3.71	4
3.90	30.63	0.00	30.63	26.83	3.80	4
3.89	31.35	0.00	31.35	27.46	3.89	4
3.88	32.06	0.00	32.06	28.08	3.98	4
3.87	32.77	0.00	32.77	28.70	4.07	4

			output			
3.86	33.48	0.00	33.48	29.33	4.15	4
3.85	34.20	0.00	34.20	29.95	4.24	4
3.84	34.91	0.00	34.91	30.58	4.33	4
3.83	35.62	0.00	35.62	31.20	4.42	4
3.82	36.33	0.00	36.33	31.82	4.51	4
3.81	37.04	0.00	37.04	32.45	4.60	4
3.80	37.76	0.00	37.76	33.07	4.69	4
3.79	38.47	0.00	38.47	33.70	4.77	4
3.78	39.18	0.00	39.18	34.32	4.86	4
3.77	39.89	0.00	39.89	34.94	4.95	4
3.76	40.61	0.00	40.61	35.57	5.04	4
3.75	41.32	0.00	41.32	36.19	5.13	4
3.74	42.03	0.00	42.03	36.82	5.22	4
3.73	42.74	0.00	42.74	37.44	5.30	4
3.72	43.46	0.00	43.46	38.06	5.39	4
3.71	44.17	0.00	44.17	38.69	5.48	4
3.70	44.88	0.00	44.88	39.31	5.57	4
3.69	45.59	0.00	45.59	39.93	5.66	4
3.68	46.30	0.00	46.30	40.56	5.75	4
3.67	47.01	0.00	47.01	41.18	5.83	4
3.66	47.73	0.00	47.72	41.80	5.92	4
3.65	48.44	0.00	48.43	42.42	6.01	4
3.64	49.14	0.00	49.14	43.05	6.10	4
3.63	49.85	0.00	49.85	43.67	6.18	4
3.62	50.56	0.01	50.56	44.28	6.27	4
3.61	51.27	0.01	51.26	44.90	6.36	4
3.60	51.97	0.01	51.96	45.52	6.44	4
3.59	52.67	0.01	52.66	46.13	6.53	4
3.58	53.37	0.01	53.36	46.74	6.62	4
3.57	54.07	0.02	54.05	47.35	6.70	4
3.56	54.76	0.02	54.75	47.96	6.79	4
3.55	55.46	0.02	55.43	48.56	6.87	4
3.54	56.14	0.03	56.12	49.16	6.96	4
3.53	56.82	0.03	56.79	49.75	7.04	4
3.52	57.50	0.04	57.47	50.34	7.13	4
3.52	58.18	0.04	58.14	50.93	7.21	4
3.51	58.84	0.05	58.80	51.51	7.29	4
3.50	59.51	0.05	59.46	52.08	7.38	4
3.49	60.16	0.06	60.11	52.65	7.46	4
3.48	60.82	0.06	60.75	53.21	7.54	4
3.47	61.46	0.07	61.39	53.77	7.62	4
3.46	62.10	0.07	62.03	54.32	7.71	4
3.45	62.73	0.08	62.66	54.87	7.79	4
3.44	63.36	0.08	63.28	55.41	7.87	4
3.44	63.99	0.09	63.90	55.94	7.96	4
3.43	64.61	0.09	64.51	56.47	8.04	4
3.42	65.22	0.10	65.12	57.00	8.12	4
3.41	65.83	0.10	65.73	57.52	8.21	4

output

3.40	66.44	0.12	66.32	58.04	8.28	4
3.39	67.04	0.13	66.91	58.55	8.35	4
3.39	67.64	0.15	67.50	59.07	8.43	4
3.38	68.24	0.16	68.08	59.58	8.51	4
3.37	68.84	0.17	68.67	60.09	8.58	4
3.36	69.43	0.18	69.26	60.59	8.66	4
3.36	69.43	0.18	69.26	60.59	8.66	4
3.29	74.30	0.26	74.04	64.72	9.32	4
3.23	79.17	0.23	78.94	68.86	10.09	4
3.16	84.04	0.25	83.78	72.99	10.80	4
3.10	88.88	0.26	88.63	77.10	11.53	4
3.03	93.72	0.26	93.46	81.20	12.26	4
2.96	98.55	0.27	98.28	85.29	12.99	4
2.90	103.37	0.28	103.09	89.37	13.72	4
2.83	108.17	0.29	107.88	93.44	14.45	4
2.77	112.97	0.29	112.67	97.50	15.18	4
2.70	117.75	0.30	117.45	101.55	15.91	4
2.64	122.53	0.31	122.22	105.59	16.64	4
2.57	127.29	0.31	126.98	109.61	17.37	4
2.57	127.29	0.31	126.98	109.61	17.37	4
2.51	132.05	0.32	131.73	113.63	18.10	4
2.45	136.79	0.33	136.47	117.64	18.82	4
2.38	141.53	0.34	141.19	121.64	19.55	4
2.32	146.25	0.35	145.90	125.62	20.28	4
2.25	150.96	0.36	150.60	129.59	21.01	4
2.19	155.65	0.37	155.28	133.55	21.73	4
2.13	160.32	0.38	159.94	137.49	22.46	4
2.07	164.98	0.40	164.58	141.40	23.18	4
2.00	169.60	0.43	169.17	145.29	23.88	4
1.94	174.19	0.47	173.72	149.14	24.58	4
1.88	178.72	0.52	178.20	152.94	25.26	4
1.82	183.20	0.57	182.63	156.68	25.95	4
1.82	183.20	0.57	182.63	156.68	25.95	4
1.76	187.63	0.62	187.01	160.37	26.64	4
1.70	192.01	0.65	191.36	164.01	27.34	4
1.65	196.36	0.68	195.68	167.63	28.05	4
1.59	200.68	0.70	199.98	171.21	28.76	4
1.53	204.98	0.72	204.25	174.77	29.48	4
1.47	209.25	0.74	208.51	178.31	30.20	4
1.42	213.51	0.76	212.74	181.83	30.91	4
1.36	217.74	0.78	216.96	185.33	31.63	4
1.31	221.95	0.81	221.15	188.80	32.34	4
1.25	226.14	0.87	225.27	192.26	33.02	4
1.20	230.31	0.94	229.37	195.69	33.69	4
1.14	234.45	1.01	233.45	199.09	34.35	4
1.14	234.45	1.01	233.45	199.09	34.35	4
1.09	238.57	1.07	237.49	202.47	35.02	4
1.03	242.66	1.15	241.51	205.82	35.68	4

0.98	246.72	1.23	245.49	209.15	36.34	4
0.93	250.75	1.32	249.43	212.45	36.99	4
0.87	254.75	1.41	253.34	215.71	37.63	4
0.82	258.72	1.50	257.21	218.94	38.28	4
0.77	262.65	1.60	261.04	222.13	38.91	4
0.72	266.54	1.71	264.83	225.29	39.54	4
0.67	270.40	1.82	268.58	228.41	40.17	4
0.62	274.21	1.93	272.28	231.49	40.79	4
0.57	277.99	2.09	275.89	234.52	41.37	4
0.53	281.71	2.30	279.41	237.51	41.90	4
0.53	281.71	2.30	279.41	237.51	41.90	4
0.48	285.39	2.51	282.88	240.46	42.43	4
0.43	289.03	2.74	286.29	243.36	42.93	4
0.39	292.61	3.00	289.61	246.20	43.41	4
0.34	296.14	3.21	292.93	248.99	43.93	4
0.30	299.63	3.37	296.25	251.74	44.51	4
0.25	303.09	3.51	299.58	254.47	45.11	4
0.21	306.52	3.63	302.89	257.16	45.73	4
0.17	309.92	3.74	306.19	259.83	46.36	4
0.13	313.30	3.83	309.47	262.47	47.00	4
0.08	316.67	3.93	312.74	265.10	47.64	4
0.04	320.01	4.12	315.89	267.71	48.18	4
0.00	323.33	4.80	318.54	270.29	48.24	4

Time = 61. Degree of Consolidation = 48.%

Total Settlement = 1.668

Settlement at End of Primary Consolidation = 3.455

Settlement caused by Primary Consolidation at time 61. = 1.668

Settlement caused by Secondary Compression at time 61. = 0.000

Surface Elevation = 2.83

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
10.50	10.49	4.83	0.91	0.91	0.91	3
10.10	10.09	4.62	0.91	0.91	0.91	3

9.70	9.69	4.41	0.91	0.91	0.91	3
9.30	9.29	4.20	0.91	0.91	0.91	3
8.90	8.89	3.99	0.91	0.91	0.90	3
8.50	8.49	3.78	0.91	0.91	0.90	3
8.10	8.09	3.57	0.90	0.90	0.90	3
7.70	7.69	3.36	0.90	0.90	0.90	3
7.30	7.29	3.15	0.90	0.90	0.90	3
6.90	6.89	2.94	0.90	0.90	0.90	3
6.50	6.49	2.73	0.90	0.90	0.90	3
6.50	6.49	2.73	1.40	1.40	1.39	2
5.85	5.84	2.46	1.39	1.39	1.39	2
5.19	5.19	2.18	1.39	1.39	1.38	2
4.54	4.54	1.91	1.39	1.38	1.38	2
3.89	3.89	1.64	1.38	1.38	1.38	2
3.24	3.24	1.36	1.38	1.38	1.38	2
2.59	2.59	1.09	1.38	1.38	1.38	2
1.94	1.94	0.82	1.38	1.37	1.37	2
1.29	1.29	0.55	1.38	1.37	1.37	2
0.65	0.65	0.27	1.37	1.37	1.37	2
0.00	0.00	0.00	1.37	1.36	1.36	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
10.49	295.63	6.66	288.97	242.59	46.38	3
10.09	342.64	27.34	315.31	267.60	47.71	3
9.69	389.64	48.00	341.64	292.60	49.05	3
9.29	436.64	68.71	367.93	317.58	50.35	3
8.89	483.62	89.54	394.08	342.56	51.52	3
8.49	530.58	110.60	419.99	367.52	52.47	3
8.09	577.54	132.03	445.52	392.48	53.04	3
7.69	624.49	154.03	470.46	417.42	53.04	3
7.29	671.42	176.04	495.39	442.35	53.04	3
6.89	718.35	198.04	520.31	467.27	53.04	3
6.49	765.26	220.05	545.21	492.17	53.04	3
6.49	765.26	220.05	545.21	492.17	53.04	2
5.84	834.09	248.14	585.95	532.91	53.04	2
5.19	902.85	287.71	615.14	573.58	41.56	2
4.54	971.57	329.06	642.51	614.21	28.30	2
3.89	1040.23	368.57	671.66	654.78	16.88	2
3.24	1108.86	404.36	704.50	695.32	9.18	2
2.59	1177.44	429.86	747.58	735.81	11.77	2
1.94	1245.98	457.06	788.91	776.25	12.66	2
1.29	1314.47	486.93	827.54	816.65	10.89	2
0.65	1382.90	519.66	863.24	857.00	6.24	2
0.00	1451.28	553.58	897.71	897.28	0.42	2

Time = 90. Degree of Consolidation = 45.%

Total Settlement = 0.008

Settlement at End of Primary Consolidation = 0.017

Settlement caused by Primary Consolidation at time 90. = 0.008

Settlement caused by Secondary Compression at time 90. = 0.000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
6.00	3.89	0.50	11.00	11.00	11.00	4
5.99	3.88	0.50	11.00	9.85	9.23	4
5.98	3.87	0.50	11.00	9.16	8.74	4
5.97	3.86	0.50	11.00	8.83	8.45	4
5.96	3.85	0.50	11.00	8.66	8.15	4
5.95	3.85	0.50	11.00	8.57	7.89	4
5.94	3.84	0.50	11.00	8.50	7.67	4
5.93	3.83	0.49	11.00	8.45	7.45	4
5.92	3.82	0.49	11.00	8.42	7.23	4
5.91	3.81	0.49	11.00	8.39	7.01	4
5.90	3.81	0.49	11.00	8.37	6.93	4
5.89	3.80	0.49	11.00	8.36	6.86	4
5.88	3.79	0.49	11.00	8.34	6.78	4
5.87	3.78	0.49	11.00	8.33	6.71	4
5.86	3.77	0.49	11.00	8.32	6.64	4
5.85	3.77	0.49	11.00	8.32	6.56	4
5.84	3.76	0.49	11.00	8.31	6.49	4
5.83	3.75	0.49	11.00	8.30	6.41	4
5.82	3.74	0.49	11.00	8.30	6.34	4
5.81	3.74	0.48	11.00	8.30	6.27	4
5.80	3.73	0.48	11.00	8.29	6.19	4
5.79	3.72	0.48	11.00	8.29	6.12	4
5.78	3.71	0.48	11.00	8.29	6.05	4
5.77	3.70	0.48	11.00	8.28	5.98	4
5.76	3.70	0.48	11.00	8.28	5.94	4
5.75	3.69	0.48	11.00	8.28	5.89	4
5.74	3.68	0.48	11.00	8.28	5.85	4
5.73	3.67	0.48	11.00	8.27	5.81	4

			output			
5.72	3.67	0.48	11.00	8.27	5.76	4
5.71	3.66	0.48	11.00	8.27	5.72	4
5.70	3.65	0.48	11.00	8.27	5.67	4
5.69	3.64	0.47	11.00	8.27	5.63	4
5.68	3.64	0.47	11.00	8.26	5.59	4
5.67	3.63	0.47	11.00	8.26	5.54	4
5.66	3.62	0.47	11.00	8.26	5.50	4
5.65	3.61	0.47	11.00	8.26	5.45	4
5.64	3.60	0.47	11.00	8.26	5.41	4
5.63	3.60	0.47	11.00	8.25	5.36	4
5.62	3.59	0.47	11.00	8.25	5.32	4
5.61	3.58	0.47	11.00	8.25	5.28	4
5.60	3.57	0.47	11.00	8.25	5.23	4
5.59	3.57	0.47	11.00	8.25	5.19	4
5.58	3.56	0.47	11.00	8.24	5.14	4
5.57	3.55	0.46	11.00	8.24	5.10	4
5.56	3.54	0.46	11.00	8.24	5.06	4
5.55	3.53	0.46	11.00	8.24	5.01	4
5.54	3.53	0.46	11.00	8.24	5.00	4
5.53	3.52	0.46	11.00	8.23	4.99	4
5.52	3.51	0.46	11.00	8.23	4.98	4
5.51	3.50	0.46	11.00	8.23	4.98	4
5.50	3.50	0.46	11.00	8.23	4.97	4
5.49	3.49	0.46	11.00	8.23	4.97	4
5.48	3.48	0.46	11.00	8.22	4.96	4
5.47	3.47	0.46	11.00	8.22	4.96	4
5.46	3.47	0.46	11.00	8.22	4.95	4
5.45	3.46	0.45	11.00	8.22	4.95	4
5.44	3.45	0.45	11.00	8.22	4.94	4
5.43	3.44	0.45	11.00	8.21	4.94	4
5.42	3.44	0.45	11.00	8.21	4.93	4
5.41	3.43	0.45	11.00	8.21	4.92	4
5.40	3.42	0.45	11.00	8.21	4.92	4
5.39	3.41	0.45	11.00	8.21	4.91	4
5.38	3.40	0.45	11.00	8.20	4.91	4
5.37	3.40	0.45	11.00	8.20	4.90	4
5.36	3.39	0.45	11.00	8.20	4.90	4
5.35	3.38	0.45	11.00	8.20	4.89	4
5.34	3.37	0.45	11.00	8.20	4.89	4
5.33	3.37	0.44	11.00	8.19	4.88	4
5.32	3.36	0.44	11.00	8.19	4.87	4
5.31	3.35	0.44	11.00	8.19	4.87	4
5.30	3.34	0.44	11.00	8.19	4.86	4
5.29	3.34	0.44	11.00	8.18	4.86	4
5.28	3.33	0.44	11.00	8.18	4.85	4
5.27	3.32	0.44	11.00	8.18	4.85	4
5.26	3.31	0.44	11.00	8.18	4.84	4
5.25	3.30	0.44	11.00	8.17	4.84	4

output

5.24	3.30	0.44	11.00	8.17	4.83	4
5.23	3.29	0.44	11.00	8.17	4.82	4
5.22	3.28	0.43	11.00	8.17	4.82	4
5.21	3.27	0.43	11.00	8.16	4.81	4
5.20	3.27	0.43	11.00	8.16	4.81	4
5.19	3.26	0.43	11.00	8.16	4.80	4
5.18	3.25	0.43	11.00	8.16	4.80	4
5.17	3.24	0.43	11.00	8.15	4.79	4
5.16	3.24	0.43	11.00	8.15	4.79	4
5.15	3.23	0.43	11.00	8.15	4.78	4
5.14	3.22	0.43	11.00	8.15	4.77	4
5.13	3.21	0.43	11.00	8.14	4.77	4
5.12	3.21	0.43	11.00	8.14	4.76	4
5.11	3.20	0.43	11.00	8.14	4.76	4
5.10	3.19	0.42	11.00	8.13	4.75	4
5.09	3.18	0.42	11.00	8.13	4.75	4
5.08	3.18	0.42	11.00	8.13	4.74	4
5.07	3.17	0.42	11.00	8.13	4.74	4
5.06	3.16	0.42	11.00	8.12	4.73	4
5.05	3.15	0.42	11.00	8.12	4.73	4
5.04	3.14	0.42	11.00	8.12	4.72	4
5.03	3.14	0.42	11.00	8.11	4.71	4
5.02	3.13	0.42	11.00	8.11	4.71	4
5.01	3.12	0.42	11.00	8.11	4.70	4
5.00	3.11	0.42	11.00	8.10	4.70	4
5.00	3.11	0.42	11.00	8.10	4.70	4
4.92	3.05	0.41	11.00	8.07	4.65	4
4.83	2.99	0.40	11.00	8.04	4.61	4
4.75	2.93	0.40	11.00	7.99	4.56	4
4.67	2.86	0.39	11.00	7.92	4.51	4
4.58	2.80	0.38	11.00	7.82	4.47	4
4.50	2.74	0.37	11.00	7.71	4.42	4
4.42	2.68	0.37	11.00	7.60	4.38	4
4.33	2.62	0.36	11.00	7.50	4.33	4
4.25	2.56	0.35	11.00	7.42	4.28	4
4.17	2.50	0.35	11.00	7.37	4.24	4
4.08	2.45	0.34	11.00	7.32	4.19	4
4.00	2.39	0.33	11.00	7.28	4.14	4
4.00	2.39	0.33	11.00	7.28	4.14	4
3.92	2.33	0.33	11.00	7.24	4.10	4
3.83	2.27	0.32	11.00	7.20	4.05	4
3.75	2.22	0.31	11.00	7.17	4.01	4
3.67	2.16	0.31	11.00	7.14	3.98	4
3.58	2.10	0.30	11.00	7.11	3.97	4
3.50	2.05	0.29	11.00	7.08	3.95	4
3.42	1.99	0.28	11.00	7.04	3.93	4
3.33	1.94	0.28	11.00	7.01	3.91	4
3.25	1.88	0.27	11.00	6.98	3.89	4

3.17	1.83	0.26	11.00	6.94	3.87	4
3.08	1.77	0.26	11.00	6.91	3.86	4
3.00	1.72	0.25	11.00	6.87	3.84	4
3.00	1.72	0.25	11.00	6.87	3.84	4
2.92	1.66	0.24	11.00	6.83	3.82	4
2.83	1.61	0.24	11.00	6.79	3.80	4
2.75	1.55	0.23	11.00	6.75	3.78	4
2.67	1.50	0.22	11.00	6.70	3.76	4
2.58	1.45	0.22	11.00	6.66	3.74	4
2.50	1.39	0.21	11.00	6.61	3.73	4
2.42	1.34	0.20	11.00	6.56	3.71	4
2.33	1.29	0.19	11.00	6.51	3.69	4
2.25	1.24	0.19	11.00	6.46	3.67	4
2.17	1.18	0.18	11.00	6.40	3.65	4
2.08	1.13	0.17	11.00	6.35	3.63	4
2.00	1.08	0.17	11.00	6.29	3.62	4
2.00	1.08	0.17	11.00	6.29	3.62	4
1.92	1.03	0.16	11.00	6.23	3.60	4
1.83	0.98	0.15	11.00	6.18	3.58	4
1.75	0.93	0.15	11.00	6.11	3.56	4
1.67	0.88	0.14	11.00	6.05	3.54	4
1.58	0.83	0.13	11.00	5.98	3.52	4
1.50	0.79	0.13	11.00	5.92	3.51	4
1.42	0.74	0.12	11.00	5.84	3.49	4
1.33	0.69	0.11	11.00	5.77	3.48	4
1.25	0.64	0.10	11.00	5.69	3.48	4
1.17	0.60	0.10	11.00	5.60	3.47	4
1.08	0.55	0.09	11.00	5.51	3.46	4
1.00	0.51	0.08	11.00	5.43	3.45	4
1.00	0.51	0.08	11.00	5.43	3.45	4
0.92	0.46	0.08	11.00	5.35	3.44	4
0.83	0.42	0.07	11.00	5.29	3.43	4
0.75	0.38	0.06	11.00	5.23	3.42	4
0.67	0.33	0.06	11.00	5.18	3.41	4
0.58	0.29	0.05	11.00	5.13	3.40	4
0.50	0.25	0.04	11.00	5.09	3.39	4
0.42	0.21	0.03	11.00	5.04	3.38	4
0.33	0.16	0.03	11.00	5.00	3.37	4
0.25	0.12	0.02	11.00	4.96	3.36	4
0.17	0.08	0.01	11.00	4.92	3.36	4
0.08	0.04	0.01	11.00	4.88	3.35	4
0.00	0.00	0.00	11.00	4.83	3.34	4

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
3.89	0.00	0.00	0.00	0.00	0.00	4

			output			
3.88	0.68	0.06	0.62	0.59	0.03	4
3.87	1.31	0.09	1.22	1.14	0.08	4
3.86	1.92	0.15	1.77	1.66	0.11	4
3.85	2.52	0.20	2.31	2.16	0.15	4
3.85	3.10	0.23	2.87	2.66	0.21	4
3.84	3.69	0.25	3.44	3.16	0.28	4
3.83	4.27	0.26	4.00	3.65	0.35	4
3.82	4.85	0.27	4.57	4.14	0.43	4
3.81	5.43	0.28	5.14	4.63	0.51	4
3.81	6.00	0.29	5.71	5.12	0.60	4
3.80	6.58	0.29	6.28	5.60	0.68	4
3.79	7.15	0.30	6.85	6.09	0.76	4
3.78	7.73	0.30	7.42	6.58	0.85	4
3.77	8.30	0.30	8.00	7.06	0.93	4
3.77	8.87	0.31	8.57	7.55	1.02	4
3.76	9.44	0.31	9.14	8.03	1.11	4
3.75	10.02	0.31	9.71	8.51	1.19	4
3.74	10.59	0.31	10.28	9.00	1.28	4
3.74	11.16	0.31	10.85	9.48	1.37	4
3.73	11.73	0.31	11.42	9.96	1.46	4
3.72	12.30	0.31	11.99	10.45	1.54	4
3.71	12.87	0.31	12.56	10.93	1.63	4
3.70	13.45	0.32	13.13	11.41	1.72	4
3.70	14.02	0.32	13.70	11.90	1.81	4
3.69	14.59	0.32	14.27	12.38	1.89	4
3.68	15.16	0.32	14.84	12.86	1.98	4
3.67	15.73	0.32	15.41	13.34	2.07	4
3.67	16.30	0.32	15.98	13.82	2.16	4
3.66	16.87	0.32	16.55	14.31	2.24	4
3.65	17.44	0.32	17.12	14.79	2.33	4
3.64	18.01	0.32	17.69	15.27	2.42	4
3.64	18.58	0.32	18.26	15.75	2.51	4
3.63	19.15	0.32	18.83	16.23	2.60	4
3.62	19.72	0.32	19.40	16.72	2.68	4
3.61	20.29	0.32	19.97	17.20	2.77	4
3.60	20.86	0.32	20.54	17.68	2.86	4
3.60	21.43	0.32	21.11	18.16	2.95	4
3.59	22.00	0.32	21.68	18.64	3.03	4
3.58	22.57	0.32	22.24	19.12	3.12	4
3.57	23.14	0.33	22.81	19.60	3.21	4
3.57	23.71	0.33	23.38	20.08	3.30	4
3.56	24.28	0.33	23.95	20.56	3.39	4
3.55	24.85	0.33	24.52	21.05	3.47	4
3.54	25.42	0.33	25.09	21.53	3.56	4
3.53	25.98	0.33	25.66	22.01	3.65	4
3.53	26.55	0.33	26.22	22.49	3.74	4
3.52	27.12	0.33	26.79	22.97	3.83	4
3.51	27.69	0.33	27.36	23.45	3.91	4

			output			
3.50	28.26	0.33	27.93	23.93	4.00	4
3.50	28.83	0.33	28.50	24.41	4.09	4
3.49	29.40	0.33	29.06	24.89	4.18	4
3.48	29.96	0.33	29.63	25.37	4.26	4
3.47	30.53	0.33	30.20	25.85	4.35	4
3.47	31.10	0.33	30.77	26.33	4.44	4
3.46	31.67	0.33	31.33	26.81	4.53	4
3.45	32.23	0.33	31.90	27.28	4.62	4
3.44	32.80	0.34	32.47	27.76	4.70	4
3.44	33.37	0.34	33.03	28.24	4.79	4
3.43	33.94	0.34	33.60	28.72	4.88	4
3.42	34.50	0.34	34.17	29.20	4.97	4
3.41	35.07	0.34	34.73	29.68	5.05	4
3.40	35.64	0.34	35.30	30.16	5.14	4
3.40	36.21	0.34	35.87	30.64	5.23	4
3.39	36.77	0.34	36.43	31.12	5.32	4
3.38	37.34	0.34	37.00	31.59	5.41	4
3.37	37.91	0.34	37.56	32.07	5.49	4
3.37	38.47	0.34	38.13	32.55	5.58	4
3.36	39.04	0.34	38.70	33.03	5.67	4
3.35	39.61	0.34	39.26	33.51	5.76	4
3.34	40.17	0.34	39.83	33.98	5.84	4
3.34	40.74	0.34	40.39	34.46	5.93	4
3.33	41.30	0.35	40.96	34.94	6.02	4
3.32	41.87	0.35	41.52	35.42	6.11	4
3.31	42.43	0.35	42.09	35.89	6.19	4
3.30	43.00	0.35	42.65	36.37	6.28	4
3.30	43.57	0.35	43.22	36.85	6.37	4
3.29	44.13	0.35	43.78	37.32	6.46	4
3.28	44.70	0.35	44.35	37.80	6.55	4
3.27	45.26	0.35	44.91	38.28	6.63	4
3.27	45.83	0.35	45.47	38.75	6.72	4
3.26	46.39	0.35	46.04	39.23	6.81	4
3.25	46.96	0.35	46.60	39.71	6.90	4
3.24	47.52	0.35	47.17	40.18	6.98	4
3.24	48.08	0.35	47.73	40.66	7.07	4
3.23	48.65	0.36	48.29	41.13	7.16	4
3.22	49.21	0.36	48.86	41.61	7.25	4
3.21	49.78	0.36	49.42	42.09	7.33	4
3.21	50.34	0.36	49.98	42.56	7.42	4
3.20	50.90	0.36	50.55	43.04	7.51	4
3.19	51.47	0.36	51.11	43.51	7.60	4
3.18	52.03	0.36	51.67	43.99	7.68	4
3.18	52.59	0.36	52.23	44.46	7.77	4
3.17	53.16	0.36	52.79	44.94	7.86	4
3.16	53.72	0.36	53.36	45.41	7.95	4
3.15	54.28	0.36	53.92	45.88	8.03	4
3.14	54.84	0.37	54.48	46.36	8.12	4

			output			
3.14	55.41	0.37	55.04	46.83	8.21	4
3.13	55.97	0.37	55.60	47.31	8.30	4
3.12	56.53	0.37	56.16	47.78	8.38	4
3.11	57.09	0.37	56.72	48.25	8.47	4
3.11	57.09	0.37	56.72	48.25	8.47	4
3.05	61.77	0.38	61.39	52.19	9.20	4
2.99	66.43	0.39	66.04	56.12	9.92	4
2.93	71.07	0.41	70.66	60.02	10.64	4
2.86	75.69	0.43	75.25	63.90	11.35	4
2.80	80.27	0.47	79.80	67.74	12.05	4
2.74	84.81	0.51	84.29	71.55	12.75	4
2.68	89.29	0.56	88.73	75.30	13.44	4
2.62	93.73	0.60	93.13	79.00	14.13	4
2.56	98.14	0.63	97.50	82.67	14.84	4
2.50	102.51	0.65	101.86	86.30	15.55	4
2.45	106.86	0.67	106.19	89.92	16.27	4
2.39	111.19	0.69	110.51	93.51	16.99	4
2.39	111.19	0.69	110.51	93.51	16.99	4
2.33	115.51	0.70	114.80	97.09	17.71	4
2.27	119.81	0.72	119.09	100.65	18.43	4
2.22	124.09	0.73	123.36	104.20	19.16	4
2.16	128.36	0.74	127.62	107.74	19.88	4
2.10	132.62	0.76	131.86	111.25	20.61	4
2.05	136.86	0.77	136.09	114.76	21.33	4
1.99	141.09	0.78	140.31	118.25	22.05	4
1.94	145.31	0.80	144.51	121.73	22.78	4
1.88	149.51	0.83	148.68	125.20	23.48	4
1.83	153.69	0.87	152.83	128.65	24.18	4
1.77	157.87	0.91	156.95	132.08	24.87	4
1.72	162.02	0.96	161.06	135.50	25.56	4
1.72	162.02	0.96	161.06	135.50	25.56	4
1.66	166.16	1.00	165.16	138.90	26.25	4
1.61	170.28	1.05	169.23	142.29	26.94	4
1.55	174.38	1.10	173.28	145.65	27.63	4
1.50	178.47	1.16	177.31	149.00	28.31	4
1.45	182.53	1.21	181.32	152.33	28.99	4
1.39	186.58	1.27	185.31	155.64	29.67	4
1.34	190.60	1.33	189.27	158.92	30.35	4
1.29	194.60	1.39	193.21	162.19	31.02	4
1.24	198.58	1.45	197.13	165.43	31.70	4
1.18	202.54	1.52	201.02	168.65	32.37	4
1.13	206.47	1.58	204.88	171.84	33.04	4
1.08	210.38	1.65	208.73	175.02	33.71	4
1.08	210.38	1.65	208.73	175.02	33.71	4
1.03	214.26	1.72	212.54	178.16	34.38	4
0.98	218.12	1.79	216.33	181.29	35.04	4
0.93	221.95	1.86	220.09	184.38	35.71	4
0.88	225.76	1.94	223.82	187.45	36.37	4

0.83	229.54	2.03	227.51	190.49	37.01	4
0.79	233.28	2.17	231.12	193.50	37.61	4
0.74	237.00	2.31	234.69	196.49	38.20	4
0.69	240.69	2.47	238.22	199.43	38.79	4
0.64	244.34	2.63	241.71	202.35	39.36	4
0.60	247.95	2.80	245.16	205.23	39.93	4
0.55	251.53	2.98	248.55	208.07	40.48	4
0.51	255.07	3.14	251.93	210.87	41.06	4
0.51	255.07	3.14	251.93	210.87	41.06	4
0.46	258.58	3.30	255.28	213.64	41.64	4
0.42	262.05	3.42	258.63	216.38	42.25	4
0.38	265.50	3.54	261.97	219.09	42.87	4
0.33	268.93	3.64	265.29	221.78	43.51	4
0.29	272.33	3.73	268.60	224.45	44.15	4
0.25	275.72	3.83	271.89	227.10	44.79	4
0.21	279.08	3.91	275.17	229.72	45.44	4
0.16	282.43	4.00	278.43	232.33	46.09	4
0.12	285.76	4.66	281.09	234.93	46.17	4
0.08	289.06	5.33	283.73	237.50	46.23	4
0.04	292.36	6.00	286.36	240.05	46.31	4
0.00	295.63	6.66	288.97	242.59	46.38	4

Time = 90. Degree of Consolidation = 61.%

Total Settlement = 2.112

Settlement at End of Primary Consolidation = 3.455

Settlement caused by Primary Consolidation at time 90. = 2.112

Settlement caused by Secondary Compression at time 90. = 0.000

Surface Elevation = 2.38

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
10.50	10.49	4.83	0.91	0.91	0.91	3
10.10	10.09	4.62	0.91	0.91	0.91	3
9.70	9.69	4.41	0.91	0.91	0.91	3
9.30	9.29	4.20	0.91	0.91	0.91	3

output

8.90	8.89	3.99	0.91	0.91	0.90	3
8.50	8.49	3.78	0.91	0.91	0.90	3
8.10	8.09	3.57	0.90	0.90	0.90	3
7.70	7.69	3.36	0.90	0.90	0.90	3
7.30	7.29	3.15	0.90	0.90	0.90	3
6.90	6.89	2.94	0.90	0.90	0.90	3
6.50	6.49	2.73	0.90	0.90	0.90	3
6.50	6.49	2.73	1.40	1.40	1.39	2
5.85	5.84	2.46	1.39	1.39	1.39	2
5.19	5.19	2.18	1.39	1.39	1.38	2
4.54	4.54	1.91	1.39	1.38	1.38	2
3.89	3.89	1.64	1.38	1.38	1.38	2
3.24	3.24	1.36	1.38	1.38	1.38	2
2.59	2.59	1.09	1.38	1.38	1.38	2
1.94	1.94	0.82	1.38	1.37	1.37	2
1.29	1.29	0.55	1.38	1.37	1.37	2
0.65	0.65	0.27	1.37	1.37	1.37	2
0.00	0.00	0.00	1.37	1.36	1.36	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
10.49	266.50	13.46	253.04	213.46	39.58	3
10.09	313.51	33.42	280.09	238.46	41.63	3
9.69	360.51	53.32	307.19	263.46	43.73	3
9.29	407.50	73.22	334.27	288.44	45.83	3
8.89	454.47	93.19	361.28	313.42	47.87	3
8.49	501.44	113.31	388.14	338.38	49.76	3
8.09	548.40	133.69	414.71	363.33	51.38	3
7.69	595.35	154.51	440.83	388.27	52.56	3
7.29	642.28	176.04	466.24	413.20	53.04	3
6.89	689.20	198.04	491.16	438.12	53.04	3
6.49	736.12	220.05	516.07	463.03	53.04	3
6.49	736.12	220.05	516.07	463.03	53.04	2
5.84	804.94	248.14	556.81	503.77	53.04	2
5.19	873.71	288.06	585.65	544.44	41.21	2
4.54	942.42	329.70	612.72	585.06	27.66	2
3.89	1011.09	369.43	641.66	625.64	16.02	2
3.24	1079.71	405.04	674.67	666.17	8.50	2
2.59	1148.29	430.62	717.67	706.66	11.01	2
1.94	1216.83	457.83	759.00	747.10	11.89	2
1.29	1285.32	487.61	797.71	787.50	10.21	2
0.65	1353.75	520.10	833.65	827.84	5.81	2
0.00	1422.13	553.61	868.52	868.13	0.39	2

Time = 180. Degree of Consolidation = 47.%

Total Settlement = 0.008

Settlement at End of Primary Consolidation = 0.017

Settlement caused by Primary Consolidation at time 180. = 0.008

Settlement caused by Secondary Compression at time 180. = 0.000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
6.00	3.42	0.50	11.00	11.00	11.00	4
5.99	3.41	0.50	11.00	9.62	9.23	4
5.98	3.40	0.50	11.00	8.83	8.74	4
5.97	3.39	0.50	11.00	8.46	8.45	4
5.96	3.39	0.50	11.00	8.23	8.15	4
5.95	3.38	0.50	11.00	8.06	7.89	4
5.94	3.37	0.50	11.00	7.92	7.67	4
5.93	3.36	0.49	11.00	7.78	7.45	4
5.92	3.36	0.49	11.00	7.66	7.23	4
5.91	3.35	0.49	11.00	7.55	7.01	4
5.90	3.34	0.49	11.00	7.46	6.93	4
5.89	3.34	0.49	11.00	7.39	6.86	4
5.88	3.33	0.49	11.00	7.32	6.78	4
5.87	3.32	0.49	11.00	7.27	6.71	4
5.86	3.32	0.49	11.00	7.23	6.64	4
5.85	3.31	0.49	11.00	7.19	6.56	4
5.84	3.30	0.49	11.00	7.16	6.49	4
5.83	3.29	0.49	11.00	7.13	6.41	4
5.82	3.29	0.49	11.00	7.10	6.34	4
5.81	3.28	0.48	11.00	7.08	6.27	4
5.80	3.27	0.48	11.00	7.05	6.19	4
5.79	3.27	0.48	11.00	7.03	6.12	4
5.78	3.26	0.48	11.00	7.02	6.05	4
5.77	3.25	0.48	11.00	7.00	5.98	4
5.76	3.25	0.48	11.00	6.99	5.94	4
5.75	3.24	0.48	11.00	6.97	5.89	4
5.74	3.23	0.48	11.00	6.96	5.85	4
5.73	3.23	0.48	11.00	6.95	5.81	4
5.72	3.22	0.48	11.00	6.93	5.76	4
5.71	3.21	0.48	11.00	6.92	5.72	4

			output			
5.70	3.21	0.48	11.00	6.91	5.67	4
5.69	3.20	0.47	11.00	6.91	5.63	4
5.68	3.20	0.47	11.00	6.90	5.59	4
5.67	3.19	0.47	11.00	6.89	5.54	4
5.66	3.18	0.47	11.00	6.88	5.50	4
5.65	3.18	0.47	11.00	6.87	5.45	4
5.64	3.17	0.47	11.00	6.87	5.41	4
5.63	3.16	0.47	11.00	6.86	5.36	4
5.62	3.16	0.47	11.00	6.85	5.32	4
5.61	3.15	0.47	11.00	6.85	5.28	4
5.60	3.14	0.47	11.00	6.84	5.23	4
5.59	3.14	0.47	11.00	6.84	5.19	4
5.58	3.13	0.47	11.00	6.83	5.14	4
5.57	3.12	0.46	11.00	6.83	5.10	4
5.56	3.12	0.46	11.00	6.82	5.06	4
5.55	3.11	0.46	11.00	6.82	5.01	4
5.54	3.10	0.46	11.00	6.81	5.00	4
5.53	3.10	0.46	11.00	6.81	4.99	4
5.52	3.09	0.46	11.00	6.81	4.98	4
5.51	3.08	0.46	11.00	6.80	4.98	4
5.50	3.08	0.46	11.00	6.80	4.97	4
5.49	3.07	0.46	11.00	6.79	4.97	4
5.48	3.06	0.46	11.00	6.79	4.96	4
5.47	3.06	0.46	11.00	6.79	4.96	4
5.46	3.05	0.46	11.00	6.78	4.95	4
5.45	3.05	0.45	11.00	6.78	4.95	4
5.44	3.04	0.45	11.00	6.78	4.94	4
5.43	3.03	0.45	11.00	6.77	4.94	4
5.42	3.03	0.45	11.00	6.77	4.93	4
5.41	3.02	0.45	11.00	6.77	4.92	4
5.40	3.01	0.45	11.00	6.76	4.92	4
5.39	3.01	0.45	11.00	6.76	4.91	4
5.38	3.00	0.45	11.00	6.76	4.91	4
5.37	2.99	0.45	11.00	6.75	4.90	4
5.36	2.99	0.45	11.00	6.75	4.90	4
5.35	2.98	0.45	11.00	6.75	4.89	4
5.34	2.97	0.45	11.00	6.74	4.89	4
5.33	2.97	0.44	11.00	6.74	4.88	4
5.32	2.96	0.44	11.00	6.74	4.87	4
5.31	2.95	0.44	11.00	6.74	4.87	4
5.30	2.95	0.44	11.00	6.73	4.86	4
5.29	2.94	0.44	11.00	6.73	4.86	4
5.28	2.94	0.44	11.00	6.73	4.85	4
5.27	2.93	0.44	11.00	6.72	4.85	4
5.26	2.92	0.44	11.00	6.72	4.84	4
5.25	2.92	0.44	11.00	6.72	4.84	4
5.24	2.91	0.44	11.00	6.72	4.83	4
5.23	2.90	0.44	11.00	6.71	4.82	4

			output			
5.22	2.90	0.43	11.00	6.71	4.82	4
5.21	2.89	0.43	11.00	6.71	4.81	4
5.20	2.88	0.43	11.00	6.70	4.81	4
5.19	2.88	0.43	11.00	6.70	4.80	4
5.18	2.87	0.43	11.00	6.70	4.80	4
5.17	2.86	0.43	11.00	6.69	4.79	4
5.16	2.86	0.43	11.00	6.69	4.79	4
5.15	2.85	0.43	11.00	6.69	4.78	4
5.14	2.85	0.43	11.00	6.69	4.77	4
5.13	2.84	0.43	11.00	6.68	4.77	4
5.12	2.83	0.43	11.00	6.68	4.76	4
5.11	2.83	0.43	11.00	6.68	4.76	4
5.10	2.82	0.42	11.00	6.67	4.75	4
5.09	2.81	0.42	11.00	6.67	4.75	4
5.08	2.81	0.42	11.00	6.67	4.74	4
5.07	2.80	0.42	11.00	6.67	4.74	4
5.06	2.79	0.42	11.00	6.66	4.73	4
5.05	2.79	0.42	11.00	6.66	4.73	4
5.04	2.78	0.42	11.00	6.66	4.72	4
5.03	2.77	0.42	11.00	6.65	4.71	4
5.02	2.77	0.42	11.00	6.65	4.71	4
5.01	2.76	0.42	11.00	6.65	4.70	4
5.00	2.76	0.42	11.00	6.65	4.70	4
5.00	2.76	0.42	11.00	6.65	4.70	4
4.92	2.70	0.41	11.00	6.62	4.65	4
4.83	2.65	0.40	11.00	6.60	4.61	4
4.75	2.60	0.40	11.00	6.57	4.56	4
4.67	2.54	0.39	11.00	6.55	4.51	4
4.58	2.49	0.38	11.00	6.52	4.47	4
4.50	2.44	0.37	11.00	6.50	4.42	4
4.42	2.39	0.37	11.00	6.47	4.38	4
4.33	2.34	0.36	11.00	6.44	4.33	4
4.25	2.28	0.35	11.00	6.42	4.28	4
4.17	2.23	0.35	11.00	6.39	4.24	4
4.08	2.18	0.34	11.00	6.36	4.19	4
4.00	2.13	0.33	11.00	6.34	4.14	4
4.00	2.13	0.33	11.00	6.34	4.14	4
3.92	2.08	0.33	11.00	6.31	4.10	4
3.83	2.03	0.32	11.00	6.28	4.05	4
3.75	1.98	0.31	11.00	6.25	4.01	4
3.67	1.93	0.31	11.00	6.22	3.98	4
3.58	1.88	0.30	11.00	6.19	3.97	4
3.50	1.83	0.29	11.00	6.16	3.95	4
3.42	1.78	0.28	11.00	6.13	3.93	4
3.33	1.73	0.28	11.00	6.09	3.91	4
3.25	1.68	0.27	11.00	6.06	3.89	4
3.17	1.63	0.26	11.00	6.03	3.87	4
3.08	1.58	0.26	11.00	5.99	3.86	4

3.00	1.54	0.25	11.00	5.96	3.84	4
3.00	1.54	0.25	11.00	5.96	3.84	4
2.92	1.49	0.24	11.00	5.92	3.82	4
2.83	1.44	0.24	11.00	5.88	3.80	4
2.75	1.39	0.23	11.00	5.84	3.78	4
2.67	1.34	0.22	11.00	5.80	3.76	4
2.58	1.30	0.22	11.00	5.76	3.74	4
2.50	1.25	0.21	11.00	5.71	3.73	4
2.42	1.20	0.20	11.00	5.65	3.71	4
2.33	1.16	0.19	11.00	5.60	3.69	4
2.25	1.11	0.19	11.00	5.53	3.67	4
2.17	1.07	0.18	11.00	5.47	3.65	4
2.08	1.02	0.17	11.00	5.41	3.63	4
2.00	0.98	0.17	11.00	5.36	3.62	4
2.00	0.98	0.17	11.00	5.36	3.62	4
1.92	0.93	0.16	11.00	5.31	3.60	4
1.83	0.89	0.15	11.00	5.26	3.58	4
1.75	0.85	0.15	11.00	5.22	3.56	4
1.67	0.80	0.14	11.00	5.18	3.54	4
1.58	0.76	0.13	11.00	5.14	3.52	4
1.50	0.72	0.13	11.00	5.10	3.51	4
1.42	0.68	0.12	11.00	5.06	3.49	4
1.33	0.63	0.11	11.00	5.02	3.48	4
1.25	0.59	0.10	11.00	4.98	3.48	4
1.17	0.55	0.10	11.00	4.94	3.47	4
1.08	0.51	0.09	11.00	4.90	3.46	4
1.00	0.47	0.08	11.00	4.86	3.45	4
1.00	0.47	0.08	11.00	4.86	3.45	4
0.92	0.43	0.08	11.00	4.82	3.44	4
0.83	0.39	0.07	11.00	4.78	3.43	4
0.75	0.35	0.06	11.00	4.75	3.42	4
0.67	0.31	0.06	11.00	4.71	3.41	4
0.58	0.27	0.05	11.00	4.67	3.40	4
0.50	0.23	0.04	11.00	4.63	3.39	4
0.42	0.19	0.03	11.00	4.59	3.38	4
0.33	0.15	0.03	11.00	4.56	3.37	4
0.25	0.11	0.02	11.00	4.52	3.36	4
0.17	0.08	0.01	11.00	4.48	3.36	4
0.08	0.04	0.01	11.00	4.45	3.35	4
0.00	0.00	0.00	11.00	4.41	3.34	4

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
3.42	0.00	0.00	0.00	0.00	0.00	4
3.41	0.67	0.07	0.60	0.59	0.02	4
3.40	1.29	0.15	1.14	1.11	0.03	4

output

3.39	1.88	0.26	1.62	1.62	0.00	4
3.39	2.45	0.33	2.12	2.10	0.02	4
3.38	3.02	0.38	2.64	2.58	0.06	4
3.37	3.57	0.43	3.14	3.04	0.10	4
3.36	4.12	0.49	3.64	3.50	0.13	4
3.36	4.66	0.54	4.13	3.96	0.17	4
3.35	5.20	0.58	4.62	4.40	0.22	4
3.34	5.73	0.62	5.12	4.85	0.27	4
3.34	6.26	0.65	5.61	5.29	0.33	4
3.33	6.78	0.67	6.11	5.72	0.39	4
3.32	7.30	0.69	6.61	6.15	0.46	4
3.32	7.82	0.71	7.11	6.58	0.53	4
3.31	8.33	0.72	7.61	7.01	0.60	4
3.30	8.85	0.74	8.11	7.43	0.68	4
3.29	9.36	0.75	8.61	7.86	0.75	4
3.29	9.87	0.76	9.11	8.28	0.83	4
3.28	10.38	0.77	9.61	8.70	0.91	4
3.27	10.88	0.78	10.11	9.12	0.99	4
3.27	11.39	0.79	10.61	9.54	1.07	4
3.26	11.90	0.79	11.10	9.95	1.15	4
3.25	12.40	0.80	11.60	10.37	1.23	4
3.25	12.91	0.82	12.09	10.78	1.30	4
3.24	13.41	0.83	12.57	11.20	1.38	4
3.23	13.91	0.85	13.06	11.61	1.45	4
3.23	14.41	0.86	13.55	12.03	1.52	4
3.22	14.92	0.88	14.04	12.44	1.60	4
3.21	15.42	0.89	14.52	12.85	1.67	4
3.21	15.92	0.90	15.01	13.26	1.75	4
3.20	16.42	0.91	15.50	13.68	1.83	4
3.20	16.91	0.92	15.99	14.09	1.90	4
3.19	17.41	0.93	16.48	14.50	1.98	4
3.18	17.91	0.94	16.97	14.91	2.06	4
3.18	18.41	0.95	17.46	15.32	2.14	4
3.17	18.91	0.96	17.95	15.73	2.22	4
3.16	19.41	0.97	18.44	16.13	2.30	4
3.16	19.90	0.98	18.93	16.54	2.38	4
3.15	20.40	0.98	19.42	16.95	2.47	4
3.14	20.90	0.99	19.91	17.36	2.55	4
3.14	21.39	1.00	20.40	17.77	2.63	4
3.13	21.89	1.00	20.89	18.17	2.71	4
3.12	22.38	1.01	21.38	18.58	2.79	4
3.12	22.88	1.01	21.86	18.99	2.88	4
3.11	23.37	1.02	22.35	19.39	2.96	4
3.10	23.87	1.02	22.84	19.80	3.04	4
3.10	24.36	1.03	23.33	20.21	3.13	4
3.09	24.86	1.03	23.82	20.61	3.21	4
3.08	25.35	1.04	24.31	21.02	3.29	4
3.08	25.84	1.04	24.80	21.42	3.38	4

			output			
3.07	26.34	1.05	25.29	21.83	3.46	4
3.06	26.83	1.05	25.78	22.24	3.54	4
3.06	27.33	1.06	26.27	22.64	3.63	4
3.05	27.82	1.06	26.76	23.05	3.71	4
3.05	28.31	1.06	27.25	23.45	3.80	4
3.04	28.80	1.07	27.74	23.85	3.88	4
3.03	29.30	1.07	28.22	24.26	3.97	4
3.03	29.79	1.08	28.71	24.66	4.05	4
3.02	30.28	1.08	29.20	25.07	4.13	4
3.01	30.77	1.08	29.69	25.47	4.22	4
3.01	31.27	1.09	30.18	25.87	4.30	4
3.00	31.76	1.09	30.67	26.28	4.39	4
2.99	32.25	1.10	31.15	26.68	4.47	4
2.99	32.74	1.10	31.64	27.08	4.56	4
2.98	33.23	1.10	32.13	27.49	4.64	4
2.97	33.72	1.11	32.62	27.89	4.73	4
2.97	34.21	1.11	33.10	28.29	4.81	4
2.96	34.71	1.11	33.59	28.69	4.90	4
2.95	35.20	1.12	34.08	29.10	4.98	4
2.95	35.69	1.12	34.57	29.50	5.07	4
2.94	36.18	1.12	35.05	29.90	5.15	4
2.94	36.67	1.13	35.54	30.30	5.24	4
2.93	37.16	1.13	36.03	30.70	5.32	4
2.92	37.65	1.14	36.51	31.11	5.41	4
2.92	38.14	1.14	37.00	31.51	5.49	4
2.91	38.63	1.14	37.48	31.91	5.58	4
2.90	39.12	1.15	37.97	32.31	5.66	4
2.90	39.61	1.15	38.46	32.71	5.75	4
2.89	40.09	1.15	38.94	33.11	5.83	4
2.88	40.58	1.16	39.43	33.51	5.92	4
2.88	41.07	1.16	39.91	33.91	6.00	4
2.87	41.56	1.16	40.40	34.31	6.09	4
2.86	42.05	1.17	40.88	34.71	6.17	4
2.86	42.54	1.17	41.37	35.11	6.26	4
2.85	43.03	1.17	41.85	35.51	6.34	4
2.85	43.52	1.18	42.34	35.91	6.43	4
2.84	44.00	1.18	42.82	36.31	6.51	4
2.83	44.49	1.18	43.31	36.71	6.60	4
2.83	44.98	1.19	43.79	37.11	6.68	4
2.82	45.47	1.19	44.28	37.51	6.77	4
2.81	45.95	1.19	44.76	37.91	6.85	4
2.81	46.44	1.20	45.24	38.31	6.94	4
2.80	46.93	1.20	45.73	38.71	7.02	4
2.79	47.42	1.20	46.21	39.11	7.11	4
2.79	47.90	1.21	46.69	39.50	7.19	4
2.78	48.39	1.21	47.18	39.90	7.28	4
2.77	48.88	1.21	47.66	40.30	7.36	4
2.77	49.36	1.22	48.14	40.70	7.45	4

			output			
2.76	49.85	1.22	48.63	41.10	7.53	4
2.76	50.33	1.22	49.11	41.49	7.62	4
2.76	50.33	1.22	49.11	41.49	7.62	4
2.70	54.38	1.25	53.13	44.80	8.32	4
2.65	58.41	1.28	57.13	48.10	9.03	4
2.60	62.44	1.31	61.12	51.39	9.74	4
2.54	66.45	1.34	65.11	54.66	10.44	4
2.49	70.45	1.37	69.08	57.93	11.15	4
2.44	74.44	1.40	73.04	61.18	11.86	4
2.39	78.42	1.44	76.99	64.43	12.56	4
2.34	82.39	1.47	80.92	67.66	13.27	4
2.28	86.35	1.50	84.85	70.88	13.97	4
2.23	90.29	1.53	88.76	74.09	14.68	4
2.18	94.23	1.56	92.66	77.28	15.38	4
2.13	98.15	1.60	96.55	80.47	16.08	4
2.13	98.15	1.60	96.55	80.47	16.08	4
2.08	102.06	1.63	100.43	83.64	16.79	4
2.03	105.95	1.66	104.29	86.80	17.49	4
1.98	109.84	1.70	108.14	89.95	18.19	4
1.93	113.71	1.73	111.98	93.09	18.89	4
1.88	117.57	1.77	115.80	96.21	19.59	4
1.83	121.42	1.81	119.61	99.32	20.29	4
1.78	125.25	1.85	123.40	102.41	20.99	4
1.73	129.07	1.89	127.18	105.49	21.69	4
1.68	132.87	1.93	130.94	108.56	22.38	4
1.63	136.66	1.97	134.69	111.61	23.08	4
1.58	140.43	2.02	138.42	114.65	23.77	4
1.54	144.19	2.09	142.10	117.67	24.43	4
1.54	144.19	2.09	142.10	117.67	24.43	4
1.49	147.94	2.16	145.78	120.68	25.10	4
1.44	151.66	2.23	149.43	123.67	25.76	4
1.39	155.37	2.31	153.06	126.64	26.42	4
1.34	159.07	2.40	156.67	129.60	27.07	4
1.30	162.74	2.49	160.25	132.54	27.71	4
1.25	166.39	2.59	163.81	135.45	28.35	4
1.20	170.03	2.69	167.34	138.35	28.99	4
1.16	173.63	2.80	170.83	141.22	29.61	4
1.11	177.22	2.93	174.29	144.07	30.22	4
1.07	180.77	3.06	177.71	146.88	30.83	4
1.02	184.30	3.18	181.12	149.68	31.45	4
0.98	187.80	3.28	184.52	152.44	32.08	4
0.98	187.80	3.28	184.52	152.44	32.08	4
0.93	191.28	3.38	187.91	155.19	32.72	4
0.89	194.75	3.47	191.27	157.91	33.36	4
0.85	198.19	3.56	194.63	160.62	34.01	4
0.80	201.61	3.65	197.96	163.30	34.66	4
0.76	205.01	3.73	201.29	165.97	35.32	4
0.72	208.40	3.81	204.59	168.62	35.97	4

0.68	211.77	3.89	207.89	171.25	36.63	4
0.63	215.12	3.96	211.16	173.87	37.29	4
0.59	218.46	4.32	214.14	176.47	37.67	4
0.55	221.78	4.94	216.84	179.05	37.78	4
0.51	225.08	5.57	219.51	181.62	37.90	4
0.47	228.37	6.19	222.18	184.17	38.01	4
0.47	228.37	6.19	222.18	184.17	38.01	4
0.43	231.64	6.82	224.82	186.70	38.12	4
0.39	234.89	7.44	227.45	189.22	38.23	4
0.35	238.12	8.06	230.06	191.71	38.35	4
0.31	241.34	8.68	232.66	194.20	38.46	4
0.27	244.54	9.30	235.25	196.66	38.59	4
0.23	247.73	9.90	237.83	199.11	38.72	4
0.19	250.90	10.51	240.39	201.54	38.85	4
0.15	254.05	11.10	242.95	203.96	38.99	4
0.11	257.19	11.69	245.50	206.36	39.14	4
0.08	260.31	12.27	248.04	208.74	39.30	4
0.04	263.41	12.86	250.55	211.11	39.44	4
0.00	266.50	13.46	253.04	213.46	39.58	4

Time = 180. Degree of Consolidation = 75.%

Total Settlement = 2.579

Settlement at End of Primary Consolidation = 3.455

Settlement caused by Primary Consolidation at time 180. = 2.579

Settlement caused by Secondary Compression at time 180. = 0.000

Settlement Due to Desiccation = 0.000

Surface Elevation = 1.91

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
10.50	10.49	4.83	0.91	0.91	0.91	3
10.10	10.09	4.62	0.91	0.91	0.91	3
9.70	9.69	4.41	0.91	0.91	0.91	3
9.30	9.29	4.20	0.91	0.91	0.91	3

8.90	8.89	3.99	0.91	0.91	0.90	3
8.50	8.49	3.78	0.91	0.91	0.90	3
8.10	8.09	3.57	0.90	0.90	0.90	3
7.70	7.69	3.36	0.90	0.90	0.90	3
7.30	7.29	3.15	0.90	0.90	0.90	3
6.90	6.89	2.94	0.90	0.90	0.90	3
6.50	6.49	2.73	0.90	0.90	0.90	3
6.50	6.49	2.73	1.40	1.40	1.39	2
5.85	5.84	2.46	1.39	1.39	1.39	2
5.19	5.19	2.18	1.39	1.39	1.38	2
4.54	4.54	1.91	1.39	1.38	1.38	2
3.89	3.89	1.64	1.38	1.38	1.38	2
3.24	3.24	1.36	1.38	1.38	1.38	2
2.59	2.59	1.09	1.38	1.38	1.38	2
1.94	1.94	0.82	1.38	1.37	1.37	2
1.29	1.29	0.55	1.38	1.37	1.37	2
0.65	0.65	0.27	1.37	1.37	1.37	2
0.00	0.00	0.00	1.37	1.36	1.36	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
10.49	256.22	16.43	239.79	203.18	36.61	3
10.09	303.23	36.12	267.11	228.18	38.93	3
9.69	350.22	55.73	294.49	253.17	41.32	3
9.29	397.21	75.32	321.89	278.16	43.73	3
8.89	444.19	94.96	349.23	303.13	46.10	3
8.49	491.15	114.71	376.45	328.09	48.36	3
8.09	538.11	134.69	403.42	353.04	50.38	3
7.69	585.06	155.05	430.00	377.98	52.02	3
7.29	631.99	176.04	455.95	402.91	53.04	3
6.89	678.91	198.04	480.87	427.83	53.04	3
6.49	725.83	220.05	505.78	452.74	53.04	3
6.49	725.83	220.05	505.78	452.74	53.04	2
5.84	794.65	248.14	546.52	493.48	53.04	2
5.19	863.42	288.06	575.36	534.15	41.21	2
4.54	932.13	329.70	602.43	574.77	27.66	2
3.89	1000.80	369.43	631.37	615.35	16.02	2
3.24	1069.42	405.04	664.38	655.88	8.50	2
2.59	1138.00	430.62	707.38	696.37	11.01	2
1.94	1206.54	457.83	748.71	736.81	11.89	2
1.29	1275.03	487.61	787.42	777.21	10.20	2
0.65	1343.46	520.10	823.36	817.55	5.81	2
0.00	1411.84	553.61	858.23	857.84	0.39	2

Time = 240. Degree of Consolidation = 48.%

Total Settlement = 0.008

Settlement at End of Primary Consolidation = 0.017

Settlement caused by Primary Consolidation at time 240. = 0.008

Settlement caused by Secondary Compression at time 240. = 0.000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
6.00	3.26	0.50	11.00	11.00	11.00	4
5.99	3.25	0.50	11.00	9.61	9.23	4
5.98	3.24	0.50	11.00	8.82	8.74	4
5.97	3.23	0.50	11.00	8.45	8.45	4
5.96	3.22	0.50	11.00	8.20	8.15	4
5.95	3.21	0.50	11.00	8.01	7.89	4
5.94	3.21	0.50	11.00	7.84	7.67	4
5.93	3.20	0.49	11.00	7.68	7.45	4
5.92	3.19	0.49	11.00	7.54	7.23	4
5.91	3.19	0.49	11.00	7.42	7.01	4
5.90	3.18	0.49	11.00	7.32	6.93	4
5.89	3.17	0.49	11.00	7.24	6.86	4
5.88	3.17	0.49	11.00	7.17	6.78	4
5.87	3.16	0.49	11.00	7.12	6.71	4
5.86	3.15	0.49	11.00	7.06	6.64	4
5.85	3.14	0.49	11.00	7.02	6.56	4
5.84	3.14	0.49	11.00	6.97	6.49	4
5.83	3.13	0.49	11.00	6.93	6.41	4
5.82	3.13	0.49	11.00	6.90	6.34	4
5.81	3.12	0.48	11.00	6.87	6.27	4
5.80	3.11	0.48	11.00	6.83	6.19	4
5.79	3.11	0.48	11.00	6.81	6.12	4
5.78	3.10	0.48	11.00	6.78	6.05	4
5.77	3.09	0.48	11.00	6.75	5.98	4
5.76	3.09	0.48	11.00	6.73	5.94	4
5.75	3.08	0.48	11.00	6.71	5.89	4
5.74	3.07	0.48	11.00	6.69	5.85	4
5.73	3.07	0.48	11.00	6.67	5.81	4
5.72	3.06	0.48	11.00	6.65	5.76	4
5.71	3.05	0.48	11.00	6.64	5.72	4

			output			
5.70	3.05	0.48	11.00	6.62	5.67	4
5.69	3.04	0.47	11.00	6.61	5.63	4
5.68	3.03	0.47	11.00	6.59	5.59	4
5.67	3.03	0.47	11.00	6.58	5.54	4
5.66	3.02	0.47	11.00	6.57	5.50	4
5.65	3.02	0.47	11.00	6.55	5.45	4
5.64	3.01	0.47	11.00	6.54	5.41	4
5.63	3.00	0.47	11.00	6.53	5.36	4
5.62	3.00	0.47	11.00	6.52	5.32	4
5.61	2.99	0.47	11.00	6.51	5.28	4
5.60	2.98	0.47	11.00	6.51	5.23	4
5.59	2.98	0.47	11.00	6.50	5.19	4
5.58	2.97	0.47	11.00	6.49	5.14	4
5.57	2.97	0.46	11.00	6.48	5.10	4
5.56	2.96	0.46	11.00	6.47	5.06	4
5.55	2.95	0.46	11.00	6.47	5.01	4
5.54	2.95	0.46	11.00	6.46	5.00	4
5.53	2.94	0.46	11.00	6.45	4.99	4
5.52	2.93	0.46	11.00	6.45	4.98	4
5.51	2.93	0.46	11.00	6.44	4.98	4
5.50	2.92	0.46	11.00	6.44	4.97	4
5.49	2.92	0.46	11.00	6.43	4.97	4
5.48	2.91	0.46	11.00	6.43	4.96	4
5.47	2.90	0.46	11.00	6.42	4.96	4
5.46	2.90	0.46	11.00	6.42	4.95	4
5.45	2.89	0.45	11.00	6.41	4.95	4
5.44	2.89	0.45	11.00	6.41	4.94	4
5.43	2.88	0.45	11.00	6.40	4.94	4
5.42	2.87	0.45	11.00	6.40	4.93	4
5.41	2.87	0.45	11.00	6.39	4.92	4
5.40	2.86	0.45	11.00	6.39	4.92	4
5.39	2.85	0.45	11.00	6.39	4.91	4
5.38	2.85	0.45	11.00	6.38	4.91	4
5.37	2.84	0.45	11.00	6.38	4.90	4
5.36	2.84	0.45	11.00	6.38	4.90	4
5.35	2.83	0.45	11.00	6.37	4.89	4
5.34	2.82	0.45	11.00	6.37	4.89	4
5.33	2.82	0.44	11.00	6.36	4.88	4
5.32	2.81	0.44	11.00	6.36	4.87	4
5.31	2.81	0.44	11.00	6.36	4.87	4
5.30	2.80	0.44	11.00	6.35	4.86	4
5.29	2.79	0.44	11.00	6.35	4.86	4
5.28	2.79	0.44	11.00	6.35	4.85	4
5.27	2.78	0.44	11.00	6.35	4.85	4
5.26	2.77	0.44	11.00	6.34	4.84	4
5.25	2.77	0.44	11.00	6.34	4.84	4
5.24	2.76	0.44	11.00	6.34	4.83	4
5.23	2.76	0.44	11.00	6.33	4.82	4

			output			
5.22	2.75	0.43	11.00	6.33	4.82	4
5.21	2.74	0.43	11.00	6.33	4.81	4
5.20	2.74	0.43	11.00	6.32	4.81	4
5.19	2.73	0.43	11.00	6.32	4.80	4
5.18	2.73	0.43	11.00	6.32	4.80	4
5.17	2.72	0.43	11.00	6.32	4.79	4
5.16	2.71	0.43	11.00	6.31	4.79	4
5.15	2.71	0.43	11.00	6.31	4.78	4
5.14	2.70	0.43	11.00	6.31	4.77	4
5.13	2.70	0.43	11.00	6.30	4.77	4
5.12	2.69	0.43	11.00	6.30	4.76	4
5.11	2.68	0.43	11.00	6.30	4.76	4
5.10	2.68	0.42	11.00	6.30	4.75	4
5.09	2.67	0.42	11.00	6.29	4.75	4
5.08	2.66	0.42	11.00	6.29	4.74	4
5.07	2.66	0.42	11.00	6.29	4.74	4
5.06	2.65	0.42	11.00	6.28	4.73	4
5.05	2.65	0.42	11.00	6.28	4.73	4
5.04	2.64	0.42	11.00	6.28	4.72	4
5.03	2.63	0.42	11.00	6.28	4.71	4
5.02	2.63	0.42	11.00	6.27	4.71	4
5.01	2.62	0.42	11.00	6.27	4.70	4
5.00	2.62	0.42	11.00	6.27	4.70	4
5.00	2.62	0.42	11.00	6.27	4.70	4
4.92	2.57	0.41	11.00	6.25	4.65	4
4.83	2.52	0.40	11.00	6.22	4.61	4
4.75	2.47	0.40	11.00	6.20	4.56	4
4.67	2.42	0.39	11.00	6.18	4.51	4
4.58	2.37	0.38	11.00	6.15	4.47	4
4.50	2.32	0.37	11.00	6.13	4.42	4
4.42	2.27	0.37	11.00	6.10	4.38	4
4.33	2.22	0.36	11.00	6.08	4.33	4
4.25	2.17	0.35	11.00	6.05	4.28	4
4.17	2.12	0.35	11.00	6.02	4.24	4
4.08	2.07	0.34	11.00	6.00	4.19	4
4.00	2.02	0.33	11.00	5.97	4.14	4
4.00	2.02	0.33	11.00	5.97	4.14	4
3.92	1.97	0.33	11.00	5.94	4.10	4
3.83	1.93	0.32	11.00	5.92	4.05	4
3.75	1.88	0.31	11.00	5.89	4.01	4
3.67	1.83	0.31	11.00	5.85	3.98	4
3.58	1.78	0.30	11.00	5.82	3.97	4
3.50	1.74	0.29	11.00	5.79	3.95	4
3.42	1.69	0.28	11.00	5.75	3.93	4
3.33	1.64	0.28	11.00	5.71	3.91	4
3.25	1.60	0.27	11.00	5.66	3.89	4
3.17	1.55	0.26	11.00	5.62	3.87	4
3.08	1.50	0.26	11.00	5.56	3.86	4

3.00	1.46	0.25	11.00	5.51	3.84	4
3.00	1.46	0.25	11.00	5.51	3.84	4
2.92	1.41	0.24	11.00	5.45	3.82	4
2.83	1.37	0.24	11.00	5.41	3.80	4
2.75	1.32	0.23	11.00	5.36	3.78	4
2.67	1.28	0.22	11.00	5.32	3.76	4
2.58	1.24	0.22	11.00	5.28	3.74	4
2.50	1.19	0.21	11.00	5.25	3.73	4
2.42	1.15	0.20	11.00	5.21	3.71	4
2.33	1.11	0.19	11.00	5.17	3.69	4
2.25	1.06	0.19	11.00	5.14	3.67	4
2.17	1.02	0.18	11.00	5.10	3.65	4
2.08	0.98	0.17	11.00	5.07	3.63	4
2.00	0.94	0.17	11.00	5.03	3.62	4
2.00	0.94	0.17	11.00	5.03	3.62	4
1.92	0.90	0.16	11.00	5.00	3.60	4
1.83	0.85	0.15	11.00	4.97	3.58	4
1.75	0.81	0.15	11.00	4.93	3.56	4
1.67	0.77	0.14	11.00	4.90	3.54	4
1.58	0.73	0.13	11.00	4.86	3.52	4
1.50	0.69	0.13	11.00	4.83	3.51	4
1.42	0.65	0.12	11.00	4.79	3.49	4
1.33	0.61	0.11	11.00	4.76	3.48	4
1.25	0.57	0.10	11.00	4.72	3.48	4
1.17	0.53	0.10	11.00	4.69	3.47	4
1.08	0.49	0.09	11.00	4.65	3.46	4
1.00	0.45	0.08	11.00	4.62	3.45	4
1.00	0.45	0.08	11.00	4.62	3.45	4
0.92	0.41	0.08	11.00	4.59	3.44	4
0.83	0.37	0.07	11.00	4.55	3.43	4
0.75	0.34	0.06	11.00	4.52	3.42	4
0.67	0.30	0.06	11.00	4.49	3.41	4
0.58	0.26	0.05	11.00	4.46	3.40	4
0.50	0.22	0.04	11.00	4.42	3.39	4
0.42	0.18	0.03	11.00	4.39	3.38	4
0.33	0.15	0.03	11.00	4.36	3.37	4
0.25	0.11	0.02	11.00	4.32	3.36	4
0.17	0.07	0.01	11.00	4.29	3.36	4
0.08	0.04	0.01	11.00	4.26	3.35	4
0.00	0.00	0.00	11.00	4.22	3.34	4

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
3.26	0.00	0.00	0.00	0.00	0.00	4
3.25	0.67	0.07	0.60	0.59	0.02	4
3.24	1.29	0.15	1.14	1.11	0.02	4

			output			
3.23	1.88	0.27	1.61	1.61	0.00	4
3.22	2.45	0.34	2.11	2.10	0.01	4
3.21	3.01	0.40	2.62	2.57	0.04	4
3.21	3.57	0.46	3.10	3.04	0.07	4
3.20	4.11	0.53	3.58	3.49	0.09	4
3.19	4.65	0.58	4.06	3.94	0.12	4
3.19	5.18	0.63	4.54	4.38	0.16	4
3.18	5.70	0.67	5.03	4.82	0.21	4
3.17	6.22	0.70	5.52	5.25	0.27	4
3.17	6.73	0.73	6.00	5.67	0.33	4
3.16	7.25	0.75	6.49	6.10	0.40	4
3.15	7.75	0.77	6.98	6.52	0.46	4
3.14	8.26	0.79	7.47	6.93	0.53	4
3.14	8.76	0.83	7.93	7.35	0.58	4
3.13	9.27	0.88	8.39	7.76	0.62	4
3.13	9.77	0.92	8.85	8.18	0.67	4
3.12	10.27	0.96	9.30	8.59	0.72	4
3.11	10.76	1.00	9.76	8.99	0.77	4
3.11	11.26	1.03	10.22	9.40	0.82	4
3.10	11.75	1.07	10.68	9.81	0.88	4
3.09	12.24	1.10	11.15	10.21	0.94	4
3.09	12.73	1.12	11.61	10.61	1.00	4
3.08	13.22	1.15	12.07	11.01	1.06	4
3.07	13.71	1.17	12.54	11.41	1.13	4
3.07	14.20	1.20	13.00	11.81	1.19	4
3.06	14.69	1.22	13.47	12.21	1.26	4
3.05	15.17	1.24	13.94	12.61	1.33	4
3.05	15.66	1.26	14.40	13.01	1.40	4
3.04	16.14	1.27	14.87	13.40	1.47	4
3.03	16.63	1.29	15.34	13.80	1.54	4
3.03	17.11	1.31	15.80	14.19	1.61	4
3.02	17.59	1.32	16.27	14.58	1.69	4
3.02	18.07	1.33	16.74	14.98	1.76	4
3.01	18.55	1.35	17.21	15.37	1.84	4
3.00	19.03	1.36	17.67	15.76	1.91	4
3.00	19.51	1.37	18.14	16.15	1.99	4
2.99	19.99	1.38	18.61	16.55	2.07	4
2.98	20.47	1.39	19.08	16.94	2.14	4
2.98	20.95	1.40	19.55	17.33	2.22	4
2.97	21.43	1.41	20.02	17.72	2.30	4
2.97	21.91	1.42	20.48	18.10	2.38	4
2.96	22.38	1.43	20.95	18.49	2.46	4
2.95	22.86	1.44	21.42	18.88	2.54	4
2.95	23.34	1.45	21.89	19.27	2.62	4
2.94	23.81	1.45	22.36	19.66	2.70	4
2.93	24.29	1.46	22.83	20.05	2.78	4
2.93	24.76	1.47	23.30	20.43	2.86	4
2.92	25.24	1.48	23.76	20.82	2.94	4

			output			
2.92	25.71	1.48	24.23	21.21	3.03	4
2.91	26.19	1.49	24.70	21.59	3.11	4
2.90	26.66	1.49	25.17	21.98	3.19	4
2.90	27.14	1.50	25.64	22.36	3.27	4
2.89	27.61	1.51	26.11	22.75	3.36	4
2.89	28.09	1.51	26.57	23.14	3.44	4
2.88	28.56	1.52	27.04	23.52	3.52	4
2.87	29.03	1.52	27.51	23.91	3.61	4
2.87	29.51	1.53	27.98	24.29	3.69	4
2.86	29.98	1.53	28.45	24.67	3.77	4
2.85	30.45	1.54	28.91	25.06	3.86	4
2.85	30.92	1.54	29.38	25.44	3.94	4
2.84	31.40	1.55	29.85	25.83	4.02	4
2.84	31.87	1.55	30.32	26.21	4.11	4
2.83	32.34	1.55	30.79	26.59	4.19	4
2.82	32.81	1.56	31.25	26.98	4.28	4
2.82	33.28	1.56	31.72	27.36	4.36	4
2.81	33.75	1.57	32.19	27.74	4.44	4
2.81	34.22	1.57	32.65	28.13	4.53	4
2.80	34.70	1.57	33.12	28.51	4.61	4
2.79	35.17	1.58	33.59	28.89	4.70	4
2.79	35.64	1.58	34.05	29.27	4.78	4
2.78	36.11	1.59	34.52	29.65	4.87	4
2.77	36.58	1.59	34.99	30.04	4.95	4
2.77	37.05	1.59	35.45	30.42	5.04	4
2.76	37.52	1.60	35.92	30.80	5.12	4
2.76	37.99	1.60	36.39	31.18	5.21	4
2.75	38.46	1.60	36.85	31.56	5.29	4
2.74	38.93	1.61	37.32	31.94	5.38	4
2.74	39.40	1.61	37.78	32.32	5.46	4
2.73	39.87	1.61	38.25	32.70	5.55	4
2.73	40.33	1.62	38.72	33.09	5.63	4
2.72	40.80	1.62	39.18	33.47	5.72	4
2.71	41.27	1.63	39.65	33.85	5.80	4
2.71	41.74	1.63	40.11	34.23	5.89	4
2.70	42.21	1.63	40.58	34.61	5.97	4
2.70	42.68	1.64	41.04	34.99	6.06	4
2.69	43.15	1.64	41.51	35.37	6.14	4
2.68	43.61	1.64	41.97	35.75	6.23	4
2.68	44.08	1.65	42.44	36.12	6.31	4
2.67	44.55	1.65	42.90	36.50	6.40	4
2.66	45.02	1.65	43.36	36.88	6.48	4
2.66	45.48	1.66	43.83	37.26	6.57	4
2.65	45.95	1.66	44.29	37.64	6.65	4
2.65	46.42	1.66	44.76	38.02	6.74	4
2.64	46.88	1.67	45.22	38.40	6.82	4
2.63	47.35	1.67	45.68	38.78	6.91	4
2.63	47.82	1.67	46.15	39.16	6.99	4

output

2.62	48.28	1.68	46.61	39.53	7.08	4
2.62	48.75	1.68	47.07	39.91	7.16	4
2.62	48.75	1.68	47.07	39.91	7.16	4
2.57	52.63	1.71	50.93	43.06	7.87	4
2.52	56.50	1.73	54.77	46.19	8.58	4
2.47	60.37	1.76	58.61	49.32	9.29	4
2.42	64.22	1.79	62.43	52.43	10.00	4
2.37	68.06	1.82	66.24	55.54	10.71	4
2.32	71.89	1.85	70.05	58.63	11.41	4
2.27	75.71	1.87	73.84	61.71	12.12	4
2.22	79.52	1.91	77.61	64.79	12.83	4
2.17	83.32	1.94	81.38	67.85	13.53	4
2.12	87.11	1.97	85.14	70.90	14.24	4
2.07	90.88	2.00	88.88	73.94	14.94	4
2.02	94.64	2.06	92.59	76.96	15.62	4
2.02	94.64	2.06	92.59	76.96	15.62	4
1.97	98.40	2.11	96.28	79.98	16.30	4
1.93	102.13	2.17	99.97	82.98	16.99	4
1.88	105.86	2.23	103.63	85.97	17.66	4
1.83	109.58	2.29	107.29	88.95	18.34	4
1.78	113.28	2.36	110.92	91.91	19.01	4
1.74	116.96	2.43	114.53	94.86	19.67	4
1.69	120.63	2.51	118.12	97.79	20.33	4
1.64	124.28	2.59	121.69	100.71	20.99	4
1.60	127.91	2.67	125.24	103.60	21.64	4
1.55	131.53	2.77	128.76	106.48	22.28	4
1.50	135.12	2.87	132.25	109.34	22.91	4
1.46	138.69	2.98	135.71	112.17	23.54	4
1.46	138.69	2.98	135.71	112.17	23.54	4
1.41	142.24	3.09	139.15	114.98	24.17	4
1.37	145.76	3.19	142.57	117.77	24.81	4
1.32	149.26	3.27	145.99	120.53	25.46	4
1.28	152.75	3.35	149.39	123.28	26.11	4
1.24	156.22	3.43	152.78	126.01	26.77	4
1.19	159.67	3.51	156.16	128.73	27.43	4
1.15	163.10	3.58	159.52	131.43	28.10	4
1.11	166.52	3.65	162.87	134.11	28.76	4
1.06	169.93	3.72	166.21	136.78	29.43	4
1.02	173.32	3.79	169.52	139.43	30.09	4
0.98	176.69	3.86	172.83	142.07	30.76	4
0.94	180.05	3.93	176.12	144.69	31.43	4
0.94	180.05	3.93	176.12	144.69	31.43	4
0.90	183.39	4.00	179.39	147.30	32.10	4
0.85	186.72	4.55	182.17	149.89	32.28	4
0.81	190.04	5.11	184.93	152.47	32.46	4
0.77	193.34	5.67	187.66	155.03	32.63	4
0.73	196.62	6.24	190.38	157.58	32.81	4
0.69	199.89	6.80	193.09	160.11	32.98	4

0.65	203.14	7.36	195.78	162.63	33.16	4
0.61	206.38	7.92	198.46	165.13	33.34	4
0.57	209.60	8.47	201.13	167.61	33.52	4
0.53	212.81	9.02	203.79	170.08	33.71	4
0.49	216.00	9.56	206.44	172.54	33.90	4
0.45	219.18	10.10	209.08	174.98	34.10	4
0.45	219.18	10.10	209.08	174.98	34.10	4
0.41	222.35	10.64	211.71	177.41	34.30	4
0.37	225.50	11.17	214.33	179.82	34.51	4
0.34	228.63	11.69	216.95	182.22	34.72	4
0.30	231.75	12.20	219.56	184.61	34.95	4
0.26	234.86	12.71	222.15	186.98	35.17	4
0.22	237.96	13.23	224.72	189.34	35.39	4
0.18	241.04	13.76	227.28	191.68	35.60	4
0.15	244.10	14.28	229.82	194.01	35.81	4
0.11	247.15	14.82	232.34	196.32	36.01	4
0.07	250.19	15.35	234.84	198.62	36.22	4
0.04	253.21	15.89	237.32	200.91	36.41	4
0.00	256.22	16.43	239.79	203.18	36.61	4

Time = 240. Degree of Consolidation = 79.%

Total Settlement = 2.744

Settlement at End of Primary Consolidation = 3.455

Settlement caused by Primary Consolidation at time 240. = 2.744

Settlement caused by Secondary Compression at time 240. = 0.000

Settlement Due to Desiccation = 0.000

Surface Elevation = 1.75

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
10.50	10.49	4.83	0.91	0.91	0.91	3
10.10	10.09	4.62	0.91	0.91	0.91	3
9.70	9.69	4.41	0.91	0.91	0.91	3
9.30	9.29	4.20	0.91	0.91	0.91	3

output

8.90	8.89	3.99	0.91	0.91	0.90	3
8.50	8.49	3.78	0.91	0.91	0.90	3
8.10	8.09	3.57	0.90	0.90	0.90	3
7.70	7.69	3.36	0.90	0.90	0.90	3
7.30	7.29	3.15	0.90	0.90	0.90	3
6.90	6.89	2.94	0.90	0.90	0.90	3
6.50	6.49	2.73	0.90	0.90	0.90	3
6.50	6.49	2.73	1.40	1.40	1.39	2
5.85	5.84	2.46	1.39	1.39	1.39	2
5.19	5.19	2.18	1.39	1.39	1.38	2
4.54	4.54	1.91	1.39	1.38	1.38	2
3.89	3.89	1.64	1.38	1.38	1.38	2
3.24	3.24	1.36	1.38	1.38	1.38	2
2.59	2.59	1.09	1.38	1.38	1.38	2
1.94	1.94	0.82	1.38	1.37	1.37	2
1.29	1.29	0.55	1.38	1.37	1.37	2
0.65	0.65	0.27	1.37	1.37	1.37	2
0.00	0.00	0.00	1.37	1.36	1.36	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
10.49	241.63	20.11	221.52	188.59	32.93	3
10.09	288.63	39.51	249.13	213.59	35.54	3
9.69	335.63	58.82	276.81	238.58	38.23	3
9.29	382.62	78.09	304.52	263.56	40.96	3
8.89	429.59	97.38	332.21	288.53	43.67	3
8.49	476.56	116.76	359.79	313.49	46.30	3
8.09	523.51	136.33	387.18	338.45	48.73	3
7.69	570.46	156.24	414.22	363.39	50.84	3
7.29	617.39	176.69	440.71	388.32	52.39	3
6.89	664.32	198.04	466.27	413.23	53.04	3
6.49	711.23	220.05	491.18	438.14	53.04	3
6.49	711.23	220.05	491.18	438.14	53.04	2
5.84	780.06	248.14	531.92	478.88	53.04	2
5.19	848.82	288.06	560.76	519.55	41.21	2
4.54	917.53	329.70	587.83	560.17	27.66	2
3.89	986.20	369.43	616.77	600.75	16.02	2
3.24	1054.82	405.04	649.78	641.28	8.50	2
2.59	1123.41	430.62	692.79	681.77	11.01	2
1.94	1191.94	457.83	734.11	722.22	11.89	2
1.29	1260.43	487.61	772.82	762.61	10.20	2
0.65	1328.86	520.10	808.76	802.96	5.81	2
0.00	1397.24	553.61	843.63	843.24	0.39	2

Time = 365. Degree of Consolidation = 49.%

Total Settlement = 0.008

Settlement at End of Primary Consolidation = 0.017

Settlement caused by Primary Consolidation at time 365. = 0.008

Settlement caused by Secondary Compression at time 365. = 0.000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
6.00	3.02	0.50	11.00	11.00	11.00	4
5.99	3.01	0.50	11.00	9.61	9.23	4
5.98	3.00	0.50	11.00	8.82	8.74	4
5.97	3.00	0.50	11.00	8.45	8.45	4
5.96	2.99	0.50	11.00	8.17	8.15	4
5.95	2.98	0.50	11.00	7.95	7.89	4
5.94	2.97	0.50	11.00	7.76	7.67	4
5.93	2.97	0.49	11.00	7.58	7.45	4
5.92	2.96	0.49	11.00	7.43	7.23	4
5.91	2.95	0.49	11.00	7.30	7.01	4
5.90	2.95	0.49	11.00	7.20	6.93	4
5.89	2.94	0.49	11.00	7.11	6.86	4
5.88	2.93	0.49	11.00	7.03	6.78	4
5.87	2.93	0.49	11.00	6.96	6.71	4
5.86	2.92	0.49	11.00	6.90	6.64	4
5.85	2.91	0.49	11.00	6.84	6.56	4
5.84	2.91	0.49	11.00	6.79	6.49	4
5.83	2.90	0.49	11.00	6.73	6.41	4
5.82	2.89	0.49	11.00	6.69	6.34	4
5.81	2.89	0.48	11.00	6.64	6.27	4
5.80	2.88	0.48	11.00	6.60	6.19	4
5.79	2.87	0.48	11.00	6.56	6.12	4
5.78	2.87	0.48	11.00	6.53	6.05	4
5.77	2.86	0.48	11.00	6.49	5.98	4
5.76	2.85	0.48	11.00	6.46	5.94	4
5.75	2.85	0.48	11.00	6.43	5.89	4
5.74	2.84	0.48	11.00	6.40	5.85	4
5.73	2.84	0.48	11.00	6.37	5.81	4
5.72	2.83	0.48	11.00	6.35	5.76	4
5.71	2.82	0.48	11.00	6.32	5.72	4

			output			
5.70	2.82	0.48	11.00	6.30	5.67	4
5.69	2.81	0.47	11.00	6.28	5.63	4
5.68	2.81	0.47	11.00	6.26	5.59	4
5.67	2.80	0.47	11.00	6.24	5.54	4
5.66	2.79	0.47	11.00	6.22	5.50	4
5.65	2.79	0.47	11.00	6.20	5.45	4
5.64	2.78	0.47	11.00	6.19	5.41	4
5.63	2.78	0.47	11.00	6.17	5.36	4
5.62	2.77	0.47	11.00	6.15	5.32	4
5.61	2.76	0.47	11.00	6.14	5.28	4
5.60	2.76	0.47	11.00	6.12	5.23	4
5.59	2.75	0.47	11.00	6.11	5.19	4
5.58	2.75	0.47	11.00	6.10	5.14	4
5.57	2.74	0.46	11.00	6.08	5.10	4
5.56	2.73	0.46	11.00	6.07	5.06	4
5.55	2.73	0.46	11.00	6.06	5.01	4
5.54	2.72	0.46	11.00	6.05	5.00	4
5.53	2.72	0.46	11.00	6.04	4.99	4
5.52	2.71	0.46	11.00	6.03	4.98	4
5.51	2.71	0.46	11.00	6.02	4.98	4
5.50	2.70	0.46	11.00	6.01	4.97	4
5.49	2.69	0.46	11.00	6.00	4.97	4
5.48	2.69	0.46	11.00	5.99	4.96	4
5.47	2.68	0.46	11.00	5.98	4.96	4
5.46	2.68	0.46	11.00	5.97	4.95	4
5.45	2.67	0.45	11.00	5.96	4.95	4
5.44	2.66	0.45	11.00	5.96	4.94	4
5.43	2.66	0.45	11.00	5.95	4.94	4
5.42	2.65	0.45	11.00	5.94	4.93	4
5.41	2.65	0.45	11.00	5.93	4.92	4
5.40	2.64	0.45	11.00	5.93	4.92	4
5.39	2.64	0.45	11.00	5.92	4.91	4
5.38	2.63	0.45	11.00	5.91	4.91	4
5.37	2.62	0.45	11.00	5.91	4.90	4
5.36	2.62	0.45	11.00	5.90	4.90	4
5.35	2.61	0.45	11.00	5.89	4.89	4
5.34	2.61	0.45	11.00	5.89	4.89	4
5.33	2.60	0.44	11.00	5.88	4.88	4
5.32	2.60	0.44	11.00	5.87	4.87	4
5.31	2.59	0.44	11.00	5.87	4.87	4
5.30	2.58	0.44	11.00	5.86	4.86	4
5.29	2.58	0.44	11.00	5.86	4.86	4
5.28	2.57	0.44	11.00	5.85	4.85	4
5.27	2.57	0.44	11.00	5.85	4.85	4
5.26	2.56	0.44	11.00	5.84	4.84	4
5.25	2.56	0.44	11.00	5.84	4.84	4
5.24	2.55	0.44	11.00	5.83	4.83	4
5.23	2.54	0.44	11.00	5.83	4.82	4

			output			
5.22	2.54	0.43	11.00	5.82	4.82	4
5.21	2.53	0.43	11.00	5.82	4.81	4
5.20	2.53	0.43	11.00	5.81	4.81	4
5.19	2.52	0.43	11.00	5.81	4.80	4
5.18	2.52	0.43	11.00	5.80	4.80	4
5.17	2.51	0.43	11.00	5.80	4.79	4
5.16	2.50	0.43	11.00	5.79	4.79	4
5.15	2.50	0.43	11.00	5.79	4.78	4
5.14	2.49	0.43	11.00	5.78	4.77	4
5.13	2.49	0.43	11.00	5.78	4.77	4
5.12	2.48	0.43	11.00	5.77	4.76	4
5.11	2.48	0.43	11.00	5.77	4.76	4
5.10	2.47	0.42	11.00	5.76	4.75	4
5.09	2.46	0.42	11.00	5.76	4.75	4
5.08	2.46	0.42	11.00	5.76	4.74	4
5.07	2.45	0.42	11.00	5.75	4.74	4
5.06	2.45	0.42	11.00	5.75	4.73	4
5.05	2.44	0.42	11.00	5.74	4.73	4
5.04	2.44	0.42	11.00	5.74	4.72	4
5.03	2.43	0.42	11.00	5.73	4.71	4
5.02	2.43	0.42	11.00	5.73	4.71	4
5.01	2.42	0.42	11.00	5.73	4.70	4
5.00	2.41	0.42	11.00	5.72	4.70	4
5.00	2.41	0.42	11.00	5.72	4.70	4
4.92	2.37	0.41	11.00	5.69	4.65	4
4.83	2.32	0.40	11.00	5.65	4.61	4
4.75	2.28	0.40	11.00	5.61	4.56	4
4.67	2.23	0.39	11.00	5.58	4.51	4
4.58	2.18	0.38	11.00	5.53	4.47	4
4.50	2.14	0.37	11.00	5.49	4.42	4
4.42	2.09	0.37	11.00	5.45	4.38	4
4.33	2.05	0.36	11.00	5.41	4.33	4
4.25	2.00	0.35	11.00	5.38	4.28	4
4.17	1.96	0.35	11.00	5.34	4.24	4
4.08	1.92	0.34	11.00	5.31	4.19	4
4.00	1.87	0.33	11.00	5.28	4.14	4
4.00	1.87	0.33	11.00	5.28	4.14	4
3.92	1.83	0.33	11.00	5.25	4.10	4
3.83	1.79	0.32	11.00	5.22	4.05	4
3.75	1.74	0.31	11.00	5.19	4.01	4
3.67	1.70	0.31	11.00	5.16	3.98	4
3.58	1.66	0.30	11.00	5.13	3.97	4
3.50	1.61	0.29	11.00	5.10	3.95	4
3.42	1.57	0.28	11.00	5.08	3.93	4
3.33	1.53	0.28	11.00	5.05	3.91	4
3.25	1.49	0.27	11.00	5.02	3.89	4
3.17	1.45	0.26	11.00	4.99	3.87	4
3.08	1.41	0.26	11.00	4.97	3.86	4

3.00	1.36	0.25	11.00	4.94	3.84	4
3.00	1.36	0.25	11.00	4.94	3.84	4
2.92	1.32	0.24	11.00	4.91	3.82	4
2.83	1.28	0.24	11.00	4.88	3.80	4
2.75	1.24	0.23	11.00	4.85	3.78	4
2.67	1.20	0.22	11.00	4.83	3.76	4
2.58	1.16	0.22	11.00	4.80	3.74	4
2.50	1.12	0.21	11.00	4.77	3.73	4
2.42	1.08	0.20	11.00	4.74	3.71	4
2.33	1.04	0.19	11.00	4.71	3.69	4
2.25	1.00	0.19	11.00	4.69	3.67	4
2.17	0.96	0.18	11.00	4.66	3.65	4
2.08	0.92	0.17	11.00	4.63	3.63	4
2.00	0.88	0.17	11.00	4.61	3.62	4
2.00	0.88	0.17	11.00	4.61	3.62	4
1.92	0.84	0.16	11.00	4.58	3.60	4
1.83	0.81	0.15	11.00	4.55	3.58	4
1.75	0.77	0.15	11.00	4.53	3.56	4
1.67	0.73	0.14	11.00	4.50	3.54	4
1.58	0.69	0.13	11.00	4.48	3.52	4
1.50	0.65	0.13	11.00	4.45	3.51	4
1.42	0.61	0.12	11.00	4.43	3.49	4
1.33	0.58	0.11	11.00	4.40	3.48	4
1.25	0.54	0.10	11.00	4.37	3.48	4
1.17	0.50	0.10	11.00	4.35	3.47	4
1.08	0.47	0.09	11.00	4.32	3.46	4
1.00	0.43	0.08	11.00	4.30	3.45	4
1.00	0.43	0.08	11.00	4.30	3.45	4
0.92	0.39	0.08	11.00	4.27	3.44	4
0.83	0.36	0.07	11.00	4.25	3.43	4
0.75	0.32	0.06	11.00	4.22	3.42	4
0.67	0.28	0.06	11.00	4.19	3.41	4
0.58	0.25	0.05	11.00	4.17	3.40	4
0.50	0.21	0.04	11.00	4.14	3.39	4
0.42	0.18	0.03	11.00	4.12	3.38	4
0.33	0.14	0.03	11.00	4.09	3.37	4
0.25	0.10	0.02	11.00	4.07	3.36	4
0.17	0.07	0.01	11.00	4.04	3.36	4
0.08	0.03	0.01	11.00	4.02	3.35	4
0.00	0.00	0.00	11.00	4.00	3.34	4

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
3.02	0.00	0.00	0.00	0.00	0.00	4
3.01	0.67	0.07	0.60	0.59	0.02	4
3.00	1.29	0.15	1.14	1.11	0.02	4

output

3.00	1.88	0.27	1.61	1.61	0.00	4
2.99	2.45	0.35	2.10	2.10	0.00	4
2.98	3.01	0.42	2.59	2.57	0.02	4
2.97	3.56	0.50	3.06	3.03	0.03	4
2.97	4.10	0.57	3.53	3.48	0.05	4
2.96	4.63	0.63	4.00	3.92	0.08	4
2.95	5.15	0.68	4.47	4.36	0.12	4
2.95	5.67	0.72	4.95	4.79	0.16	4
2.94	6.18	0.76	5.43	5.21	0.22	4
2.93	6.69	0.79	5.90	5.63	0.27	4
2.93	7.20	0.84	6.35	6.05	0.31	4
2.92	7.70	0.92	6.78	6.46	0.32	4
2.91	8.19	0.99	7.20	6.87	0.33	4
2.91	8.69	1.06	7.63	7.27	0.36	4
2.90	9.18	1.12	8.06	7.68	0.38	4
2.89	9.67	1.18	8.49	8.08	0.42	4
2.89	10.16	1.23	8.93	8.48	0.45	4
2.88	10.64	1.28	9.36	8.87	0.49	4
2.87	11.12	1.32	9.80	9.27	0.53	4
2.87	11.60	1.37	10.24	9.66	0.58	4
2.86	12.08	1.41	10.67	10.05	0.62	4
2.85	12.56	1.45	11.11	10.44	0.67	4
2.85	13.04	1.48	11.55	10.83	0.73	4
2.84	13.51	1.52	11.99	11.21	0.78	4
2.84	13.98	1.55	12.43	11.60	0.84	4
2.83	14.45	1.58	12.87	11.98	0.89	4
2.82	14.92	1.61	13.31	12.36	0.95	4
2.82	15.39	1.64	13.75	12.74	1.01	4
2.81	15.86	1.66	14.20	13.12	1.08	4
2.81	16.33	1.69	14.64	13.50	1.14	4
2.80	16.79	1.71	15.08	13.87	1.20	4
2.79	17.26	1.74	15.52	14.25	1.27	4
2.79	17.72	1.76	15.96	14.63	1.34	4
2.78	18.18	1.78	16.40	15.00	1.40	4
2.78	18.64	1.80	16.85	15.37	1.47	4
2.77	19.10	1.82	17.29	15.75	1.54	4
2.76	19.56	1.83	17.73	16.12	1.61	4
2.76	20.02	1.85	18.17	16.49	1.68	4
2.75	20.48	1.87	18.61	16.86	1.76	4
2.75	20.94	1.88	19.06	17.23	1.83	4
2.74	21.40	1.90	19.50	17.60	1.90	4
2.73	21.85	1.91	19.94	17.96	1.98	4
2.73	22.31	1.93	20.38	18.33	2.05	4
2.72	22.76	1.94	20.82	18.70	2.13	4
2.72	23.22	1.95	21.27	19.06	2.20	4
2.71	23.67	1.97	21.71	19.43	2.28	4
2.71	24.13	1.98	22.15	19.80	2.35	4
2.70	24.58	1.99	22.59	20.16	2.43	4

			output			
2.69	25.03	2.00	23.03	20.52	2.51	4
2.69	25.48	2.02	23.47	20.89	2.58	4
2.68	25.94	2.04	23.90	21.25	2.65	4
2.68	26.39	2.05	24.33	21.61	2.72	4
2.67	26.84	2.07	24.77	21.98	2.79	4
2.66	27.29	2.09	25.20	22.34	2.86	4
2.66	27.74	2.10	25.64	22.70	2.94	4
2.65	28.19	2.12	26.07	23.06	3.01	4
2.65	28.64	2.13	26.50	23.42	3.08	4
2.64	29.09	2.15	26.94	23.78	3.16	4
2.64	29.53	2.16	27.37	24.14	3.23	4
2.63	29.98	2.18	27.81	24.50	3.31	4
2.62	30.43	2.19	28.24	24.86	3.38	4
2.62	30.88	2.20	28.68	25.22	3.46	4
2.61	31.32	2.21	29.11	25.58	3.53	4
2.61	31.77	2.23	29.54	25.94	3.61	4
2.60	32.22	2.24	29.98	26.29	3.68	4
2.60	32.66	2.25	30.41	26.65	3.76	4
2.59	33.11	2.26	30.85	27.01	3.84	4
2.58	33.55	2.27	31.28	27.37	3.91	4
2.58	34.00	2.29	31.71	27.72	3.99	4
2.57	34.44	2.30	32.15	28.08	4.07	4
2.57	34.89	2.31	32.58	28.44	4.15	4
2.56	35.33	2.32	33.01	28.79	4.22	4
2.56	35.78	2.33	33.45	29.15	4.30	4
2.55	36.22	2.34	33.88	29.50	4.38	4
2.54	36.66	2.35	34.31	29.86	4.46	4
2.54	37.11	2.36	34.75	30.21	4.54	4
2.53	37.55	2.37	35.18	30.57	4.61	4
2.53	37.99	2.38	35.61	30.92	4.69	4
2.52	38.44	2.39	36.05	31.28	4.77	4
2.52	38.88	2.40	36.48	31.63	4.85	4
2.51	39.32	2.41	36.91	31.98	4.93	4
2.50	39.76	2.42	37.34	32.34	5.01	4
2.50	40.20	2.43	37.78	32.69	5.09	4
2.49	40.64	2.44	38.21	33.04	5.17	4
2.49	41.08	2.45	38.64	33.39	5.25	4
2.48	41.53	2.45	39.07	33.75	5.33	4
2.48	41.97	2.46	39.50	34.10	5.40	4
2.47	42.41	2.47	39.93	34.45	5.48	4
2.46	42.85	2.48	40.37	34.80	5.56	4
2.46	43.29	2.49	40.80	35.15	5.64	4
2.45	43.73	2.50	41.23	35.50	5.72	4
2.45	44.17	2.51	41.66	35.86	5.80	4
2.44	44.60	2.52	42.09	36.21	5.88	4
2.44	45.04	2.52	42.52	36.56	5.96	4
2.43	45.48	2.53	42.95	36.91	6.04	4
2.43	45.92	2.54	43.38	37.26	6.12	4

			output			
2.42	46.36	2.55	43.81	37.61	6.20	4
2.41	46.80	2.56	44.24	37.96	6.28	4
2.41	46.80	2.56	44.24	37.96	6.28	4
2.37	50.44	2.63	47.81	40.86	6.95	4
2.32	54.06	2.70	51.36	43.75	7.61	4
2.28	57.67	2.77	54.90	46.62	8.28	4
2.23	61.27	2.85	58.42	49.48	8.94	4
2.18	64.85	2.93	61.91	52.32	9.59	4
2.14	68.40	3.02	65.39	55.14	10.24	4
2.09	71.94	3.10	68.84	57.95	10.89	4
2.05	75.47	3.18	72.29	60.73	11.56	4
2.00	78.97	3.25	75.73	63.50	12.22	4
1.96	82.47	3.31	79.16	66.26	12.89	4
1.92	85.95	3.38	82.57	69.00	13.57	4
1.87	89.41	3.44	85.97	71.73	14.24	4
1.87	89.41	3.44	85.97	71.73	14.24	4
1.83	92.86	3.50	89.36	74.45	14.92	4
1.79	96.30	3.56	92.74	77.15	15.59	4
1.74	99.73	3.62	96.11	79.84	16.27	4
1.70	103.14	3.68	99.46	82.51	16.95	4
1.66	106.54	3.73	102.81	85.18	17.63	4
1.61	109.93	3.79	106.14	87.83	18.31	4
1.57	113.30	3.85	109.46	90.47	18.99	4
1.53	116.67	3.90	112.76	93.10	19.67	4
1.49	120.02	3.96	116.06	95.71	20.35	4
1.45	123.36	4.11	119.25	98.31	20.93	4
1.41	126.69	4.56	122.13	100.90	21.23	4
1.36	130.00	5.00	125.00	103.48	21.52	4
1.36	130.00	5.00	125.00	103.48	21.52	4
1.32	133.31	5.45	127.86	106.05	21.81	4
1.28	136.60	5.90	130.70	108.60	22.10	4
1.24	139.88	6.35	133.53	111.15	22.38	4
1.20	143.14	6.79	136.35	113.68	22.68	4
1.16	146.40	7.24	139.16	116.20	22.97	4
1.12	149.64	7.68	141.96	118.70	23.26	4
1.08	152.87	8.12	144.75	121.20	23.55	4
1.04	156.09	8.56	147.53	123.68	23.85	4
1.00	159.30	9.00	150.30	126.15	24.15	4
0.96	162.49	9.43	153.06	128.61	24.46	4
0.92	165.68	9.86	155.82	131.05	24.76	4
0.88	168.85	10.28	158.57	133.49	25.08	4
0.88	168.85	10.28	158.57	133.49	25.08	4
0.84	172.01	10.71	161.30	135.91	25.39	4
0.81	175.16	11.13	164.03	138.33	25.70	4
0.77	178.30	11.54	166.75	140.73	26.03	4
0.73	181.43	11.95	169.47	143.12	26.35	4
0.69	184.54	12.36	172.18	145.50	26.68	4
0.65	187.65	12.77	174.88	147.87	27.01	4

0.61	190.74	13.18	177.56	150.22	27.34	4
0.58	193.82	13.59	180.23	152.57	27.66	4
0.54	196.89	14.00	182.89	154.90	27.99	4
0.50	199.95	14.42	185.54	157.23	28.31	4
0.47	203.00	14.83	188.17	159.54	28.63	4
0.43	206.04	15.25	190.79	161.84	28.95	4
0.43	206.04	15.25	190.79	161.84	28.95	4
0.39	209.07	15.66	193.40	164.13	29.27	4
0.36	212.08	16.08	196.00	166.41	29.59	4
0.32	215.09	16.49	198.59	168.68	29.92	4
0.28	218.08	16.91	201.17	170.93	30.24	4
0.25	221.06	17.31	203.75	173.18	30.57	4
0.21	224.03	17.72	206.31	175.41	30.90	4
0.18	226.99	18.12	208.87	177.63	31.23	4
0.14	229.94	18.52	211.42	179.85	31.57	4
0.10	232.88	18.91	213.97	182.05	31.92	4
0.07	235.80	19.30	216.51	184.24	32.27	4
0.03	238.72	19.67	219.05	186.42	32.63	4
0.00	241.63	20.11	221.52	188.59	32.93	4

Time = 365. Degree of Consolidation = 86.%

Total Settlement = 2.978

Settlement at End of Primary Consolidation = 3.455

Settlement caused by Primary Consolidation at time 365. = 2.978

Settlement caused by Secondary Compression at time 365. = 0.000

Settlement Due to Desiccation = 0.000

Surface Elevation = 1.51

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
10.50	10.49	4.83	0.91	0.91	0.91	3
10.10	10.09	4.62	0.91	0.91	0.91	3
9.70	9.69	4.41	0.91	0.91	0.91	3
9.30	9.29	4.20	0.91	0.91	0.91	3

8.90	8.89	3.99	0.91	0.91	0.90	3
8.50	8.49	3.78	0.91	0.91	0.90	3
8.10	8.09	3.57	0.90	0.90	0.90	3
7.70	7.69	3.36	0.90	0.90	0.90	3
7.30	7.29	3.15	0.90	0.90	0.90	3
6.90	6.89	2.94	0.90	0.90	0.90	3
6.50	6.49	2.73	0.90	0.90	0.90	3
6.50	6.49	2.73	1.40	1.40	1.39	2
5.85	5.84	2.46	1.39	1.39	1.39	2
5.19	5.19	2.18	1.39	1.39	1.38	2
4.54	4.54	1.91	1.39	1.38	1.38	2
3.89	3.89	1.64	1.38	1.38	1.38	2
3.24	3.24	1.36	1.38	1.38	1.38	2
2.59	2.59	1.09	1.38	1.38	1.38	2
1.94	1.94	0.82	1.38	1.37	1.37	2
1.29	1.29	0.55	1.38	1.37	1.37	2
0.65	0.65	0.27	1.37	1.37	1.37	2
0.00	0.00	0.00	1.37	1.36	1.36	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
10.49	228.09	22.15	205.95	175.05	30.89	3
10.09	275.10	41.38	233.72	200.05	33.67	3
9.69	322.09	60.51	261.58	225.04	36.53	3
9.29	369.08	79.60	289.47	250.02	39.45	3
8.89	416.05	98.70	317.35	275.00	42.36	3
8.49	463.02	117.87	345.15	299.96	45.19	3
8.09	509.97	137.22	372.76	324.91	47.85	3
7.69	556.92	156.87	400.05	349.85	50.20	3
7.29	603.85	177.03	426.82	374.78	52.04	3
6.89	650.78	198.04	452.73	399.69	53.04	3
6.49	697.69	220.05	477.64	424.60	53.04	3
6.49	697.69	220.05	477.64	424.60	53.04	2
5.84	766.52	248.14	518.38	465.34	53.04	2
5.19	835.28	288.06	547.22	506.01	41.21	2
4.54	903.99	329.70	574.29	546.63	27.66	2
3.89	972.66	369.43	603.23	587.21	16.02	2
3.24	1041.28	405.04	636.24	627.74	8.50	2
2.59	1109.86	430.62	679.25	668.23	11.01	2
1.94	1178.40	457.83	720.57	708.68	11.89	2
1.29	1246.89	487.61	759.28	749.07	10.20	2
0.65	1315.32	520.10	795.22	789.42	5.81	2
0.00	1383.70	553.61	830.09	829.70	0.39	2

Time = 725. Degree of Consolidation = 49.%

Total Settlement = 0.008

Settlement at End of Primary Consolidation = 0.017

Settlement caused by Primary Consolidation at time 725. = 0.008

Settlement caused by Secondary Compression at time 725. = 0.000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
6.00	2.81	0.50	11.00	11.00	11.00	4
5.99	2.80	0.50	11.00	9.61	9.23	4
5.98	2.79	0.50	11.00	8.82	8.74	4
5.97	2.78	0.50	11.00	8.45	8.45	4
5.96	2.77	0.50	11.00	8.15	8.15	4
5.95	2.76	0.50	11.00	7.91	7.89	4
5.94	2.76	0.50	11.00	7.68	7.67	4
5.93	2.75	0.49	11.00	7.48	7.45	4
5.92	2.74	0.49	11.00	7.31	7.23	4
5.91	2.74	0.49	11.00	7.18	7.01	4
5.90	2.73	0.49	11.00	7.06	6.93	4
5.89	2.72	0.49	11.00	6.96	6.86	4
5.88	2.72	0.49	11.00	6.87	6.78	4
5.87	2.71	0.49	11.00	6.78	6.71	4
5.86	2.70	0.49	11.00	6.70	6.64	4
5.85	2.70	0.49	11.00	6.62	6.56	4
5.84	2.69	0.49	11.00	6.55	6.49	4
5.83	2.68	0.49	11.00	6.49	6.41	4
5.82	2.68	0.49	11.00	6.42	6.34	4
5.81	2.67	0.48	11.00	6.37	6.27	4
5.80	2.67	0.48	11.00	6.31	6.19	4
5.79	2.66	0.48	11.00	6.26	6.12	4
5.78	2.65	0.48	11.00	6.21	6.05	4
5.77	2.65	0.48	11.00	6.16	5.98	4
5.76	2.64	0.48	11.00	6.11	5.94	4
5.75	2.64	0.48	11.00	6.07	5.89	4
5.74	2.63	0.48	11.00	6.02	5.85	4
5.73	2.62	0.48	11.00	5.98	5.81	4
5.72	2.62	0.48	11.00	5.94	5.76	4
5.71	2.61	0.48	11.00	5.91	5.72	4

			output			
5.70	2.61	0.48	11.00	5.87	5.67	4
5.69	2.60	0.47	11.00	5.83	5.63	4
5.68	2.60	0.47	11.00	5.80	5.59	4
5.67	2.59	0.47	11.00	5.76	5.54	4
5.66	2.58	0.47	11.00	5.73	5.50	4
5.65	2.58	0.47	11.00	5.70	5.45	4
5.64	2.57	0.47	11.00	5.67	5.41	4
5.63	2.57	0.47	11.00	5.63	5.36	4
5.62	2.56	0.47	11.00	5.60	5.32	4
5.61	2.56	0.47	11.00	5.57	5.28	4
5.60	2.55	0.47	11.00	5.55	5.23	4
5.59	2.55	0.47	11.00	5.52	5.19	4
5.58	2.54	0.47	11.00	5.49	5.14	4
5.57	2.53	0.46	11.00	5.47	5.10	4
5.56	2.53	0.46	11.00	5.44	5.06	4
5.55	2.52	0.46	11.00	5.43	5.01	4
5.54	2.52	0.46	11.00	5.41	5.00	4
5.53	2.51	0.46	11.00	5.39	4.99	4
5.52	2.51	0.46	11.00	5.38	4.98	4
5.51	2.50	0.46	11.00	5.36	4.98	4
5.50	2.50	0.46	11.00	5.35	4.97	4
5.49	2.49	0.46	11.00	5.34	4.97	4
5.48	2.49	0.46	11.00	5.33	4.96	4
5.47	2.48	0.46	11.00	5.32	4.96	4
5.46	2.48	0.46	11.00	5.30	4.95	4
5.45	2.47	0.45	11.00	5.29	4.95	4
5.44	2.47	0.45	11.00	5.28	4.94	4
5.43	2.46	0.45	11.00	5.27	4.94	4
5.42	2.45	0.45	11.00	5.26	4.93	4
5.41	2.45	0.45	11.00	5.26	4.92	4
5.40	2.44	0.45	11.00	5.25	4.92	4
5.39	2.44	0.45	11.00	5.24	4.91	4
5.38	2.43	0.45	11.00	5.23	4.91	4
5.37	2.43	0.45	11.00	5.22	4.90	4
5.36	2.42	0.45	11.00	5.21	4.90	4
5.35	2.42	0.45	11.00	5.20	4.89	4
5.34	2.41	0.45	11.00	5.20	4.89	4
5.33	2.41	0.44	11.00	5.19	4.88	4
5.32	2.40	0.44	11.00	5.18	4.87	4
5.31	2.40	0.44	11.00	5.18	4.87	4
5.30	2.39	0.44	11.00	5.17	4.86	4
5.29	2.39	0.44	11.00	5.16	4.86	4
5.28	2.38	0.44	11.00	5.15	4.85	4
5.27	2.38	0.44	11.00	5.15	4.85	4
5.26	2.37	0.44	11.00	5.14	4.84	4
5.25	2.37	0.44	11.00	5.13	4.84	4
5.24	2.36	0.44	11.00	5.13	4.83	4
5.23	2.36	0.44	11.00	5.12	4.82	4

			output			
5.22	2.35	0.43	11.00	5.12	4.82	4
5.21	2.35	0.43	11.00	5.11	4.81	4
5.20	2.34	0.43	11.00	5.10	4.81	4
5.19	2.34	0.43	11.00	5.10	4.80	4
5.18	2.33	0.43	11.00	5.09	4.80	4
5.17	2.33	0.43	11.00	5.09	4.79	4
5.16	2.32	0.43	11.00	5.08	4.79	4
5.15	2.32	0.43	11.00	5.07	4.78	4
5.14	2.31	0.43	11.00	5.07	4.77	4
5.13	2.31	0.43	11.00	5.06	4.77	4
5.12	2.30	0.43	11.00	5.06	4.76	4
5.11	2.30	0.43	11.00	5.05	4.76	4
5.10	2.29	0.42	11.00	5.05	4.75	4
5.09	2.29	0.42	11.00	5.04	4.75	4
5.08	2.28	0.42	11.00	5.04	4.74	4
5.07	2.28	0.42	11.00	5.03	4.74	4
5.06	2.27	0.42	11.00	5.03	4.73	4
5.05	2.27	0.42	11.00	5.02	4.73	4
5.04	2.26	0.42	11.00	5.02	4.72	4
5.03	2.26	0.42	11.00	5.01	4.71	4
5.02	2.25	0.42	11.00	5.01	4.71	4
5.01	2.25	0.42	11.00	5.00	4.70	4
5.00	2.24	0.42	11.00	5.00	4.70	4
5.00	2.24	0.42	11.00	5.00	4.70	4
4.92	2.20	0.41	11.00	4.96	4.65	4
4.83	2.16	0.40	11.00	4.93	4.61	4
4.75	2.12	0.40	11.00	4.90	4.56	4
4.67	2.08	0.39	11.00	4.87	4.51	4
4.58	2.04	0.38	11.00	4.84	4.47	4
4.50	1.99	0.37	11.00	4.82	4.42	4
4.42	1.95	0.37	11.00	4.79	4.38	4
4.33	1.91	0.36	11.00	4.77	4.33	4
4.25	1.87	0.35	11.00	4.74	4.28	4
4.17	1.83	0.35	11.00	4.72	4.24	4
4.08	1.80	0.34	11.00	4.69	4.19	4
4.00	1.76	0.33	11.00	4.67	4.14	4
4.00	1.76	0.33	11.00	4.67	4.14	4
3.92	1.72	0.33	11.00	4.65	4.10	4
3.83	1.68	0.32	11.00	4.63	4.05	4
3.75	1.64	0.31	11.00	4.61	4.01	4
3.67	1.60	0.31	11.00	4.59	3.98	4
3.58	1.56	0.30	11.00	4.57	3.97	4
3.50	1.52	0.29	11.00	4.55	3.95	4
3.42	1.48	0.28	11.00	4.53	3.93	4
3.33	1.45	0.28	11.00	4.51	3.91	4
3.25	1.41	0.27	11.00	4.49	3.89	4
3.17	1.37	0.26	11.00	4.47	3.87	4
3.08	1.33	0.26	11.00	4.46	3.86	4

3.00	1.29	0.25	11.00	4.44	3.84	4
3.00	1.29	0.25	11.00	4.44	3.84	4
2.92	1.26	0.24	11.00	4.42	3.82	4
2.83	1.22	0.24	11.00	4.40	3.80	4
2.75	1.18	0.23	11.00	4.39	3.78	4
2.67	1.14	0.22	11.00	4.37	3.76	4
2.58	1.11	0.22	11.00	4.36	3.74	4
2.50	1.07	0.21	11.00	4.34	3.73	4
2.42	1.03	0.20	11.00	4.32	3.71	4
2.33	0.99	0.19	11.00	4.31	3.69	4
2.25	0.96	0.19	11.00	4.29	3.67	4
2.17	0.92	0.18	11.00	4.28	3.65	4
2.08	0.88	0.17	11.00	4.26	3.63	4
2.00	0.85	0.17	11.00	4.25	3.62	4
2.00	0.85	0.17	11.00	4.25	3.62	4
1.92	0.81	0.16	11.00	4.23	3.60	4
1.83	0.78	0.15	11.00	4.22	3.58	4
1.75	0.74	0.15	11.00	4.21	3.56	4
1.67	0.70	0.14	11.00	4.19	3.54	4
1.58	0.67	0.13	11.00	4.18	3.52	4
1.50	0.63	0.13	11.00	4.16	3.51	4
1.42	0.60	0.12	11.00	4.15	3.49	4
1.33	0.56	0.11	11.00	4.14	3.48	4
1.25	0.52	0.10	11.00	4.12	3.48	4
1.17	0.49	0.10	11.00	4.11	3.47	4
1.08	0.45	0.09	11.00	4.10	3.46	4
1.00	0.42	0.08	11.00	4.09	3.45	4
1.00	0.42	0.08	11.00	4.09	3.45	4
0.92	0.38	0.08	11.00	4.07	3.44	4
0.83	0.35	0.07	11.00	4.06	3.43	4
0.75	0.31	0.06	11.00	4.05	3.42	4
0.67	0.28	0.06	11.00	4.04	3.41	4
0.58	0.24	0.05	11.00	4.02	3.40	4
0.50	0.21	0.04	11.00	4.01	3.39	4
0.42	0.17	0.03	11.00	4.00	3.38	4
0.33	0.14	0.03	11.00	3.99	3.37	4
0.25	0.10	0.02	11.00	3.98	3.36	4
0.17	0.07	0.01	11.00	3.97	3.36	4
0.08	0.03	0.01	11.00	3.96	3.35	4
0.00	0.00	0.00	11.00	3.95	3.34	4

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
2.81	0.00	0.00	0.00	0.00	0.00	4
2.80	0.67	0.07	0.60	0.59	0.02	4
2.79	1.29	0.15	1.14	1.11	0.02	4

output

2.78	1.88	0.27	1.61	1.61	0.00	4
2.77	2.45	0.35	2.10	2.10	0.00	4
2.76	3.01	0.44	2.57	2.57	0.01	4
2.76	3.56	0.53	3.03	3.02	0.00	4
2.75	4.09	0.61	3.48	3.47	0.01	4
2.74	4.61	0.67	3.94	3.91	0.03	4
2.74	5.13	0.73	4.40	4.34	0.07	4
2.73	5.64	0.78	4.87	4.76	0.11	4
2.72	6.15	0.85	5.30	5.17	0.12	4
2.72	6.65	0.96	5.69	5.59	0.10	4
2.71	7.14	1.06	6.08	5.99	0.09	4
2.70	7.63	1.16	6.47	6.40	0.08	4
2.70	8.12	1.25	6.87	6.79	0.08	4
2.69	8.60	1.34	7.27	7.19	0.08	4
2.68	9.08	1.42	7.67	7.58	0.09	4
2.68	9.56	1.49	8.07	7.97	0.10	4
2.67	10.03	1.56	8.47	8.35	0.12	4
2.67	10.50	1.63	8.87	8.73	0.14	4
2.66	10.97	1.69	9.28	9.11	0.16	4
2.65	11.43	1.75	9.68	9.49	0.19	4
2.65	11.89	1.81	10.08	9.86	0.22	4
2.64	12.35	1.87	10.49	10.23	0.26	4
2.64	12.81	1.92	10.89	10.60	0.29	4
2.63	13.27	1.97	11.30	10.97	0.33	4
2.62	13.72	2.03	11.69	11.33	0.35	4
2.62	14.17	2.11	12.06	11.69	0.36	4
2.61	14.62	2.19	12.43	12.05	0.38	4
2.61	15.06	2.26	12.80	12.41	0.39	4
2.60	15.51	2.34	13.17	12.77	0.41	4
2.60	15.95	2.41	13.55	13.12	0.42	4
2.59	16.39	2.47	13.92	13.48	0.44	4
2.58	16.83	2.54	14.29	13.83	0.46	4
2.58	17.27	2.61	14.66	14.18	0.49	4
2.57	17.70	2.67	15.04	14.52	0.51	4
2.57	18.14	2.73	15.41	14.87	0.54	4
2.56	18.57	2.79	15.78	15.21	0.57	4
2.56	19.00	2.85	16.15	15.56	0.60	4
2.55	19.43	2.91	16.52	15.90	0.63	4
2.55	19.86	2.97	16.89	16.24	0.66	4
2.54	20.29	3.02	17.27	16.57	0.69	4
2.53	20.71	3.07	17.64	16.91	0.73	4
2.53	21.14	3.11	18.02	17.25	0.78	4
2.52	21.56	3.15	18.41	17.58	0.83	4
2.52	21.98	3.18	18.80	17.91	0.88	4
2.51	22.40	3.21	19.19	18.25	0.94	4
2.51	22.82	3.24	19.58	18.58	1.00	4
2.50	23.24	3.27	19.97	18.91	1.06	4
2.50	23.66	3.30	20.36	19.24	1.12	4

output

2.49	24.08	3.32	20.76	19.57	1.19	4
2.49	24.50	3.35	21.15	19.90	1.25	4
2.48	24.91	3.37	21.55	20.23	1.32	4
2.48	25.33	3.39	21.94	20.56	1.38	4
2.47	25.75	3.41	22.33	20.89	1.45	4
2.47	26.16	3.43	22.73	21.21	1.52	4
2.46	26.58	3.45	23.13	21.54	1.59	4
2.45	26.99	3.47	23.52	21.86	1.66	4
2.45	27.41	3.49	23.92	22.19	1.73	4
2.44	27.82	3.51	24.31	22.52	1.80	4
2.44	28.23	3.52	24.71	22.84	1.87	4
2.43	28.64	3.54	25.10	23.16	1.94	4
2.43	29.06	3.56	25.50	23.49	2.01	4
2.42	29.47	3.57	25.89	23.81	2.08	4
2.42	29.88	3.59	26.29	24.13	2.16	4
2.41	30.29	3.61	26.69	24.46	2.23	4
2.41	30.70	3.62	27.08	24.78	2.30	4
2.40	31.11	3.64	27.48	25.10	2.38	4
2.40	31.52	3.65	27.87	25.42	2.45	4
2.39	31.93	3.66	28.27	25.74	2.52	4
2.39	32.34	3.68	28.66	26.06	2.60	4
2.38	32.75	3.69	29.06	26.38	2.67	4
2.38	33.16	3.71	29.45	26.70	2.75	4
2.37	33.56	3.72	29.85	27.02	2.82	4
2.37	33.97	3.73	30.24	27.34	2.90	4
2.36	34.38	3.74	30.63	27.66	2.97	4
2.36	34.79	3.76	31.03	27.98	3.05	4
2.35	35.19	3.77	31.42	28.30	3.13	4
2.35	35.60	3.78	31.82	28.61	3.20	4
2.34	36.00	3.79	32.21	28.93	3.28	4
2.34	36.41	3.81	32.60	29.25	3.35	4
2.33	36.81	3.82	33.00	29.57	3.43	4
2.33	37.22	3.83	33.39	29.88	3.51	4
2.32	37.62	3.84	33.78	30.20	3.58	4
2.32	38.03	3.85	34.18	30.52	3.66	4
2.31	38.43	3.86	34.57	30.83	3.74	4
2.31	38.84	3.87	34.96	31.15	3.82	4
2.30	39.24	3.89	35.36	31.46	3.89	4
2.30	39.64	3.90	35.75	31.78	3.97	4
2.29	40.05	3.91	36.14	32.09	4.05	4
2.29	40.45	3.92	36.53	32.40	4.13	4
2.28	40.85	3.93	36.92	32.72	4.20	4
2.28	41.25	3.94	37.32	33.03	4.28	4
2.27	41.66	3.95	37.71	33.35	4.36	4
2.27	42.06	3.96	38.10	33.66	4.44	4
2.26	42.46	3.97	38.49	33.97	4.52	4
2.26	42.86	3.98	38.88	34.29	4.60	4
2.25	43.26	3.99	39.27	34.60	4.67	4

output

2.25	43.66	4.00	39.66	34.91	4.75	4
2.24	44.06	4.06	40.00	35.22	4.78	4
2.24	44.06	4.06	40.00	35.22	4.78	4
2.20	47.39	4.59	42.80	37.81	4.99	4
2.16	50.70	5.09	45.61	40.39	5.22	4
2.12	54.00	5.58	48.43	42.95	5.47	4
2.08	57.29	6.04	51.25	45.50	5.75	4
2.04	60.57	6.48	54.08	48.04	6.04	4
1.99	63.83	6.92	56.92	50.57	6.34	4
1.95	67.08	7.33	59.75	53.09	6.66	4
1.91	70.32	7.74	62.59	55.59	7.00	4
1.87	73.55	8.13	65.42	58.08	7.34	4
1.83	76.77	8.51	68.26	60.57	7.69	4
1.80	79.98	8.89	71.10	63.04	8.06	4
1.76	83.18	9.25	73.93	65.50	8.43	4
1.76	83.18	9.25	73.93	65.50	8.43	4
1.72	86.37	9.61	76.76	67.95	8.81	4
1.68	89.55	9.96	79.59	70.40	9.19	4
1.64	92.72	10.30	82.42	72.83	9.59	4
1.60	95.88	10.63	85.25	75.26	9.99	4
1.56	99.04	10.96	88.08	77.67	10.41	4
1.52	102.18	11.27	90.91	80.08	10.83	4
1.48	105.32	11.57	93.74	82.48	11.27	4
1.45	108.44	11.87	96.58	84.87	11.71	4
1.41	111.56	12.15	99.41	87.25	12.16	4
1.37	114.67	12.43	102.24	89.63	12.61	4
1.33	117.78	12.71	105.07	92.00	13.07	4
1.29	120.88	12.99	107.89	94.36	13.53	4
1.29	120.88	12.99	107.89	94.36	13.53	4
1.26	123.97	13.26	110.71	96.71	14.00	4
1.22	127.05	13.53	113.52	99.05	14.46	4
1.18	130.12	13.80	116.33	101.39	14.93	4
1.14	133.19	14.06	119.13	103.72	15.41	4
1.11	136.25	14.32	121.93	106.05	15.89	4
1.07	139.31	14.57	124.73	108.37	16.37	4
1.03	142.35	14.82	127.53	110.68	16.85	4
0.99	145.39	15.07	130.32	112.98	17.34	4
0.96	148.43	15.31	133.11	115.28	17.84	4
0.92	151.45	15.55	135.90	117.57	18.33	4
0.88	154.47	15.79	138.68	119.85	18.83	4
0.85	157.49	16.03	141.46	122.13	19.33	4
0.85	157.49	16.03	141.46	122.13	19.33	4
0.81	160.50	16.26	144.24	124.40	19.84	4
0.78	163.50	16.49	147.01	126.66	20.34	4
0.74	166.49	16.72	149.77	128.92	20.85	4
0.70	169.48	16.94	152.54	131.17	21.36	4
0.67	172.46	17.16	155.30	133.42	21.88	4
0.63	175.44	17.38	158.06	135.66	22.40	4

0.60	178.41	17.60	160.82	137.90	22.92	4
0.56	181.38	17.81	163.57	140.13	23.44	4
0.52	184.34	18.02	166.32	142.35	23.97	4
0.49	187.29	18.23	169.07	144.57	24.50	4
0.45	190.24	18.43	171.81	146.78	25.03	4
0.42	193.18	18.63	174.55	148.98	25.57	4
0.42	193.18	18.63	174.55	148.98	25.57	4
0.38	196.12	18.83	177.29	151.19	26.10	4
0.35	199.05	19.03	180.02	153.38	26.64	4
0.31	201.98	19.23	182.75	155.57	27.18	4
0.28	204.90	19.42	185.48	157.76	27.72	4
0.24	207.82	19.62	188.20	159.94	28.27	4
0.21	210.73	19.80	190.93	162.11	28.82	4
0.17	213.64	19.99	193.64	164.28	29.37	4
0.14	216.54	20.44	196.10	166.44	29.66	4
0.10	219.43	20.88	198.55	168.60	29.95	4
0.07	222.32	21.31	201.01	170.76	30.25	4
0.03	225.21	21.74	203.48	172.91	30.57	4
0.00	228.09	22.15	205.95	175.05	30.89	4

Time = 725. Degree of Consolidation = 92.%

Total Settlement = 3.195

Settlement at End of Primary Consolidation = 3.455

Settlement caused by Primary Consolidation at time 725. = 3.195

Settlement caused by Secondary Compression at time 725. = 0.000

Settlement Due to Desiccation = 0.000

Surface Elevation = 1.30

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
10.50	10.49	4.83	0.91	0.91	0.91	3
10.10	10.09	4.62	0.91	0.91	0.91	3
9.70	9.69	4.41	0.91	0.91	0.91	3
9.30	9.29	4.20	0.91	0.91	0.91	3

8.90	8.89	3.99	0.91	0.91	0.90	3
8.50	8.49	3.78	0.91	0.91	0.90	3
8.10	8.09	3.57	0.90	0.90	0.90	3
7.70	7.69	3.36	0.90	0.90	0.90	3
7.30	7.29	3.15	0.90	0.90	0.90	3
6.90	6.89	2.94	0.90	0.90	0.90	3
6.50	6.49	2.73	0.90	0.90	0.90	3
6.50	6.49	2.73	1.40	1.40	1.39	2
5.85	5.84	2.46	1.39	1.39	1.39	2
5.19	5.19	2.18	1.39	1.39	1.38	2
4.54	4.54	1.91	1.39	1.38	1.38	2
3.89	3.89	1.64	1.38	1.38	1.38	2
3.24	3.24	1.36	1.38	1.38	1.38	2
2.59	2.59	1.09	1.38	1.38	1.38	2
1.94	1.94	0.82	1.38	1.37	1.37	2
1.29	1.29	0.55	1.38	1.37	1.37	2
0.65	0.65	0.27	1.37	1.37	1.37	2
0.00	0.00	0.00	1.37	1.36	1.36	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
10.49	222.33	27.52	194.81	169.29	25.52	3
10.09	269.33	46.38	222.95	194.29	28.66	3
9.69	316.32	65.13	251.19	219.28	31.92	3
9.29	363.31	83.82	279.49	244.25	35.24	3
8.89	410.28	102.49	307.79	269.22	38.57	3
8.49	457.24	121.20	336.04	294.18	41.86	3
8.09	504.20	140.05	364.14	319.13	45.01	3
7.69	551.14	159.16	391.98	344.07	47.91	3
7.29	598.07	178.71	419.37	369.00	50.37	3
6.89	645.00	198.98	446.01	393.91	52.10	3
6.49	691.91	220.52	471.39	418.82	52.56	3
6.49	691.91	220.52	471.39	418.82	52.56	2
5.84	760.73	248.14	512.60	459.56	53.04	2
5.19	829.50	288.06	541.44	500.23	41.21	2
4.54	898.21	329.70	568.51	540.85	27.66	2
3.89	966.88	369.43	597.45	581.43	16.02	2
3.24	1035.50	405.04	630.46	621.96	8.50	2
2.59	1104.08	430.62	673.46	662.45	11.01	2
1.94	1172.62	457.83	714.79	702.89	11.89	2
1.29	1241.11	487.61	753.50	743.29	10.20	2
0.65	1309.54	520.10	789.44	783.63	5.81	2
0.00	1377.92	553.61	824.31	823.92	0.39	2

Time = 1085. Degree of Consolidation = 51.%

Total Settlement = 0.009

Settlement at End of Primary Consolidation = 0.017

Settlement caused by Primary Consolidation at time 1085. = 0.009

Settlement caused by Secondary Compression at time 1085. = 0.000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
6.00	2.71	0.50	11.00	11.00	11.00	4
5.99	2.70	0.50	11.00	9.23	9.23	4
5.98	2.70	0.50	11.00	8.74	8.74	4
5.97	2.69	0.50	11.00	8.45	8.45	4
5.96	2.68	0.50	11.00	8.15	8.15	4
5.95	2.67	0.50	11.00	7.89	7.89	4
5.94	2.66	0.50	11.00	7.67	7.67	4
5.93	2.66	0.49	11.00	7.45	7.45	4
5.92	2.65	0.49	11.00	7.23	7.23	4
5.91	2.64	0.49	11.00	7.01	7.01	4
5.90	2.64	0.49	11.00	6.93	6.93	4
5.89	2.63	0.49	11.00	6.85	6.86	4
5.88	2.62	0.49	11.00	6.78	6.78	4
5.87	2.62	0.49	11.00	6.71	6.71	4
5.86	2.61	0.49	11.00	6.63	6.64	4
5.85	2.61	0.49	11.00	6.56	6.56	4
5.84	2.60	0.49	11.00	6.49	6.49	4
5.83	2.59	0.49	11.00	6.41	6.41	4
5.82	2.59	0.49	11.00	6.34	6.34	4
5.81	2.58	0.48	11.00	6.27	6.27	4
5.80	2.57	0.48	11.00	6.19	6.19	4
5.79	2.57	0.48	11.00	6.12	6.12	4
5.78	2.56	0.48	11.00	6.04	6.05	4
5.77	2.56	0.48	11.00	5.98	5.98	4
5.76	2.55	0.48	11.00	5.94	5.94	4
5.75	2.55	0.48	11.00	5.89	5.89	4
5.74	2.54	0.48	11.00	5.85	5.85	4
5.73	2.53	0.48	11.00	5.81	5.81	4
5.72	2.53	0.48	11.00	5.76	5.76	4
5.71	2.52	0.48	11.00	5.72	5.72	4

			output			
5.70	2.52	0.48	11.00	5.67	5.67	4
5.69	2.51	0.47	11.00	5.63	5.63	4
5.68	2.51	0.47	11.00	5.58	5.59	4
5.67	2.50	0.47	11.00	5.54	5.54	4
5.66	2.50	0.47	11.00	5.50	5.50	4
5.65	2.49	0.47	11.00	5.45	5.45	4
5.64	2.48	0.47	11.00	5.41	5.41	4
5.63	2.48	0.47	11.00	5.36	5.36	4
5.62	2.47	0.47	11.00	5.32	5.32	4
5.61	2.47	0.47	11.00	5.27	5.28	4
5.60	2.46	0.47	11.00	5.23	5.23	4
5.59	2.46	0.47	11.00	5.19	5.19	4
5.58	2.45	0.47	11.00	5.14	5.14	4
5.57	2.45	0.46	11.00	5.10	5.10	4
5.56	2.44	0.46	11.00	5.05	5.06	4
5.55	2.44	0.46	11.00	5.01	5.01	4
5.54	2.43	0.46	11.00	5.00	5.00	4
5.53	2.43	0.46	11.00	4.99	4.99	4
5.52	2.42	0.46	11.00	4.98	4.98	4
5.51	2.42	0.46	11.00	4.98	4.98	4
5.50	2.41	0.46	11.00	4.97	4.97	4
5.49	2.41	0.46	11.00	4.97	4.97	4
5.48	2.40	0.46	11.00	4.96	4.96	4
5.47	2.40	0.46	11.00	4.96	4.96	4
5.46	2.39	0.46	11.00	4.95	4.95	4
5.45	2.39	0.45	11.00	4.95	4.95	4
5.44	2.38	0.45	11.00	4.94	4.94	4
5.43	2.38	0.45	11.00	4.93	4.94	4
5.42	2.37	0.45	11.00	4.93	4.93	4
5.41	2.37	0.45	11.00	4.92	4.92	4
5.40	2.36	0.45	11.00	4.92	4.92	4
5.39	2.36	0.45	11.00	4.91	4.91	4
5.38	2.35	0.45	11.00	4.91	4.91	4
5.37	2.35	0.45	11.00	4.90	4.90	4
5.36	2.34	0.45	11.00	4.90	4.90	4
5.35	2.34	0.45	11.00	4.89	4.89	4
5.34	2.33	0.45	11.00	4.88	4.89	4
5.33	2.33	0.44	11.00	4.88	4.88	4
5.32	2.32	0.44	11.00	4.87	4.87	4
5.31	2.32	0.44	11.00	4.87	4.87	4
5.30	2.31	0.44	11.00	4.86	4.86	4
5.29	2.31	0.44	11.00	4.86	4.86	4
5.28	2.30	0.44	11.00	4.85	4.85	4
5.27	2.30	0.44	11.00	4.85	4.85	4
5.26	2.29	0.44	11.00	4.84	4.84	4
5.25	2.29	0.44	11.00	4.83	4.84	4
5.24	2.28	0.44	11.00	4.83	4.83	4
5.23	2.28	0.44	11.00	4.82	4.82	4

			output			
5.22	2.28	0.43	11.00	4.82	4.82	4
5.21	2.27	0.43	11.00	4.81	4.81	4
5.20	2.27	0.43	11.00	4.81	4.81	4
5.19	2.26	0.43	11.00	4.80	4.80	4
5.18	2.26	0.43	11.00	4.80	4.80	4
5.17	2.25	0.43	11.00	4.79	4.79	4
5.16	2.25	0.43	11.00	4.79	4.79	4
5.15	2.24	0.43	11.00	4.78	4.78	4
5.14	2.24	0.43	11.00	4.77	4.77	4
5.13	2.23	0.43	11.00	4.77	4.77	4
5.12	2.23	0.43	11.00	4.76	4.76	4
5.11	2.22	0.43	11.00	4.76	4.76	4
5.10	2.22	0.42	11.00	4.75	4.75	4
5.09	2.21	0.42	11.00	4.75	4.75	4
5.08	2.21	0.42	11.00	4.74	4.74	4
5.07	2.20	0.42	11.00	4.74	4.74	4
5.06	2.20	0.42	11.00	4.73	4.73	4
5.05	2.19	0.42	11.00	4.72	4.73	4
5.04	2.19	0.42	11.00	4.72	4.72	4
5.03	2.18	0.42	11.00	4.71	4.71	4
5.02	2.18	0.42	11.00	4.71	4.71	4
5.01	2.17	0.42	11.00	4.70	4.70	4
5.00	2.17	0.42	11.00	4.70	4.70	4
5.00	2.17	0.42	11.00	4.70	4.70	4
4.92	2.13	0.41	11.00	4.68	4.65	4
4.83	2.09	0.40	11.00	4.66	4.61	4
4.75	2.05	0.40	11.00	4.64	4.56	4
4.67	2.01	0.39	11.00	4.62	4.51	4
4.58	1.97	0.38	11.00	4.60	4.47	4
4.50	1.93	0.37	11.00	4.58	4.42	4
4.42	1.90	0.37	11.00	4.57	4.38	4
4.33	1.86	0.36	11.00	4.55	4.33	4
4.25	1.82	0.35	11.00	4.53	4.28	4
4.17	1.78	0.35	11.00	4.52	4.24	4
4.08	1.74	0.34	11.00	4.50	4.19	4
4.00	1.70	0.33	11.00	4.48	4.14	4
4.00	1.70	0.33	11.00	4.48	4.14	4
3.92	1.67	0.33	11.00	4.47	4.10	4
3.83	1.63	0.32	11.00	4.45	4.05	4
3.75	1.59	0.31	11.00	4.43	4.01	4
3.67	1.55	0.31	11.00	4.42	3.98	4
3.58	1.52	0.30	11.00	4.40	3.97	4
3.50	1.48	0.29	11.00	4.38	3.95	4
3.42	1.44	0.28	11.00	4.37	3.93	4
3.33	1.40	0.28	11.00	4.35	3.91	4
3.25	1.37	0.27	11.00	4.33	3.89	4
3.17	1.33	0.26	11.00	4.32	3.87	4
3.08	1.29	0.26	11.00	4.30	3.86	4

3.00	1.26	0.25	11.00	4.28	3.84	4
3.00	1.26	0.25	11.00	4.28	3.84	4
2.92	1.22	0.24	11.00	4.27	3.82	4
2.83	1.18	0.24	11.00	4.25	3.80	4
2.75	1.15	0.23	11.00	4.23	3.78	4
2.67	1.11	0.22	11.00	4.22	3.76	4
2.58	1.07	0.22	11.00	4.20	3.74	4
2.50	1.04	0.21	11.00	4.19	3.73	4
2.42	1.00	0.20	11.00	4.17	3.71	4
2.33	0.97	0.19	11.00	4.15	3.69	4
2.25	0.93	0.19	11.00	4.14	3.67	4
2.17	0.89	0.18	11.00	4.12	3.65	4
2.08	0.86	0.17	11.00	4.11	3.63	4
2.00	0.82	0.17	11.00	4.09	3.62	4
2.00	0.82	0.17	11.00	4.09	3.62	4
1.92	0.79	0.16	11.00	4.08	3.60	4
1.83	0.75	0.15	11.00	4.06	3.58	4
1.75	0.72	0.15	11.00	4.05	3.56	4
1.67	0.68	0.14	11.00	4.04	3.54	4
1.58	0.65	0.13	11.00	4.02	3.52	4
1.50	0.61	0.13	11.00	4.01	3.51	4
1.42	0.58	0.12	11.00	3.99	3.49	4
1.33	0.54	0.11	11.00	3.98	3.48	4
1.25	0.51	0.10	11.00	3.97	3.48	4
1.17	0.47	0.10	11.00	3.96	3.47	4
1.08	0.44	0.09	11.00	3.94	3.46	4
1.00	0.41	0.08	11.00	3.93	3.45	4
1.00	0.41	0.08	11.00	3.93	3.45	4
0.92	0.37	0.08	11.00	3.92	3.44	4
0.83	0.34	0.07	11.00	3.91	3.43	4
0.75	0.30	0.06	11.00	3.90	3.42	4
0.67	0.27	0.06	11.00	3.89	3.41	4
0.58	0.24	0.05	11.00	3.88	3.40	4
0.50	0.20	0.04	11.00	3.87	3.39	4
0.42	0.17	0.03	11.00	3.86	3.38	4
0.33	0.13	0.03	11.00	3.85	3.37	4
0.25	0.10	0.02	11.00	3.84	3.36	4
0.17	0.07	0.01	11.00	3.83	3.36	4
0.08	0.03	0.01	11.00	3.82	3.35	4
0.00	0.00	0.00	11.00	3.81	3.34	4

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
2.71	0.00	0.00	0.00	0.00	0.00	4
2.70	0.66	0.09	0.57	0.57	0.00	4
2.70	1.26	0.18	1.09	1.09	0.00	4

output

2.69	1.85	0.27	1.59	1.59	0.00	4
2.68	2.42	0.35	2.07	2.07	0.00	4
2.67	2.98	0.44	2.54	2.54	0.00	4
2.66	3.52	0.53	2.99	2.99	0.00	4
2.66	4.06	0.62	3.44	3.44	0.00	4
2.65	4.58	0.71	3.87	3.87	0.00	4
2.64	5.09	0.80	4.29	4.29	0.00	4
2.64	5.59	0.88	4.71	4.71	0.00	4
2.63	6.09	0.97	5.12	5.12	0.00	4
2.62	6.59	1.06	5.53	5.53	0.00	4
2.62	7.08	1.15	5.93	5.93	0.00	4
2.61	7.57	1.24	6.33	6.33	0.00	4
2.61	8.05	1.33	6.72	6.72	0.00	4
2.60	8.53	1.41	7.11	7.11	0.00	4
2.59	9.00	1.50	7.50	7.50	0.00	4
2.59	9.48	1.59	7.88	7.88	0.00	4
2.58	9.94	1.68	8.26	8.26	0.00	4
2.57	10.41	1.77	8.64	8.64	0.00	4
2.57	10.87	1.86	9.01	9.01	0.00	4
2.56	11.33	1.94	9.38	9.38	0.00	4
2.56	11.78	2.03	9.75	9.75	0.00	4
2.55	12.23	2.12	10.11	10.11	0.00	4
2.55	12.68	2.21	10.47	10.47	0.00	4
2.54	13.12	2.30	10.82	10.82	0.00	4
2.53	13.57	2.39	11.18	11.18	0.00	4
2.53	14.01	2.48	11.53	11.53	0.00	4
2.52	14.45	2.56	11.88	11.88	0.00	4
2.52	14.88	2.65	12.23	12.23	0.00	4
2.51	15.32	2.74	12.58	12.58	0.00	4
2.51	15.75	2.83	12.92	12.92	0.00	4
2.50	16.18	2.92	13.26	13.26	0.00	4
2.50	16.61	3.01	13.60	13.60	0.00	4
2.49	17.03	3.09	13.94	13.94	0.00	4
2.48	17.45	3.18	14.27	14.27	0.00	4
2.48	17.87	3.27	14.60	14.60	0.00	4
2.47	18.29	3.36	14.93	14.93	0.00	4
2.47	18.71	3.45	15.26	15.26	0.00	4
2.46	19.12	3.54	15.59	15.59	0.00	4
2.46	19.53	3.62	15.91	15.91	0.00	4
2.45	19.94	3.71	16.23	16.23	0.00	4
2.45	20.35	3.80	16.55	16.55	0.00	4
2.44	20.75	3.89	16.86	16.86	0.00	4
2.44	21.15	3.98	17.18	17.18	0.00	4
2.43	21.55	4.07	17.49	17.49	0.00	4
2.43	21.95	4.15	17.80	17.80	0.00	4
2.42	22.35	4.24	18.11	18.11	0.00	4
2.42	22.75	4.33	18.42	18.42	0.00	4
2.41	23.15	4.42	18.73	18.73	0.00	4

			output			
2.41	23.55	4.51	19.04	19.04	0.00	4
2.40	23.95	4.60	19.35	19.35	0.00	4
2.40	24.35	4.69	19.66	19.66	0.00	4
2.39	24.75	4.77	19.97	19.97	0.00	4
2.39	25.14	4.86	20.28	20.28	0.00	4
2.38	25.54	4.95	20.59	20.59	0.00	4
2.38	25.94	5.04	20.90	20.90	0.00	4
2.37	26.34	5.13	21.21	21.21	0.00	4
2.37	26.73	5.22	21.52	21.52	0.00	4
2.36	27.13	5.30	21.82	21.82	0.00	4
2.36	27.52	5.39	22.13	22.13	0.00	4
2.35	27.92	5.48	22.44	22.44	0.00	4
2.35	28.32	5.57	22.75	22.75	0.00	4
2.34	28.71	5.66	23.05	23.05	0.00	4
2.34	29.11	5.75	23.36	23.36	0.00	4
2.33	29.50	5.83	23.67	23.67	0.00	4
2.33	29.89	5.92	23.97	23.97	0.00	4
2.32	30.29	6.01	24.28	24.28	0.00	4
2.32	30.68	6.10	24.58	24.58	0.00	4
2.31	31.08	6.19	24.89	24.89	0.00	4
2.31	31.47	6.28	25.19	25.19	0.00	4
2.30	31.86	6.36	25.50	25.50	0.00	4
2.30	32.25	6.45	25.80	25.80	0.00	4
2.29	32.65	6.54	26.10	26.10	0.00	4
2.29	33.04	6.63	26.41	26.41	0.00	4
2.28	33.43	6.72	26.71	26.71	0.00	4
2.28	33.82	6.81	27.01	27.01	0.00	4
2.28	34.21	6.90	27.32	27.32	0.00	4
2.27	34.60	6.98	27.62	27.62	0.00	4
2.27	34.99	7.07	27.92	27.92	0.00	4
2.26	35.38	7.16	28.22	28.22	0.00	4
2.26	35.77	7.25	28.52	28.52	0.00	4
2.25	36.16	7.34	28.83	28.83	0.00	4
2.25	36.55	7.43	29.13	29.13	0.00	4
2.24	36.94	7.51	29.43	29.43	0.00	4
2.24	37.33	7.60	29.73	29.73	0.00	4
2.23	37.72	7.69	30.03	30.03	0.00	4
2.23	38.11	7.78	30.33	30.33	0.00	4
2.22	38.50	7.87	30.63	30.63	0.00	4
2.22	38.88	7.96	30.93	30.93	0.00	4
2.21	39.27	8.04	31.23	31.23	0.00	4
2.21	39.66	8.13	31.52	31.52	0.00	4
2.20	40.04	8.22	31.82	31.82	0.00	4
2.20	40.43	8.31	32.12	32.12	0.00	4
2.19	40.82	8.40	32.42	32.42	0.00	4
2.19	41.20	8.49	32.72	32.72	0.00	4
2.18	41.59	8.57	33.01	33.01	0.00	4
2.18	41.97	8.66	33.31	33.31	0.00	4

output

2.17	42.36	8.75	33.61	33.61	0.00	4
2.17	42.74	8.84	33.90	33.90	0.00	4
2.17	42.74	8.84	33.90	33.90	0.00	4
2.13	45.94	9.17	36.78	36.37	0.41	4
2.09	49.14	9.48	39.65	38.82	0.83	4
2.05	52.32	9.79	42.53	41.27	1.26	4
2.01	55.50	10.08	45.41	43.71	1.70	4
1.97	58.67	10.37	48.29	46.14	2.15	4
1.93	61.83	10.66	51.17	48.57	2.60	4
1.90	64.98	10.93	54.04	50.98	3.06	4
1.86	68.12	11.21	56.92	53.39	3.53	4
1.82	71.26	11.48	59.79	55.79	3.99	4
1.78	74.39	11.74	62.65	58.18	4.47	4
1.74	77.51	12.00	65.51	60.57	4.94	4
1.70	80.63	12.27	68.37	62.95	5.41	4
1.70	80.63	12.27	68.37	62.95	5.41	4
1.67	83.74	12.53	71.21	65.32	5.89	4
1.63	86.84	12.79	74.05	67.69	6.36	4
1.59	89.94	13.05	76.88	70.05	6.84	4
1.55	93.03	13.32	79.71	72.40	7.31	4
1.52	96.11	13.59	82.52	74.74	7.78	4
1.48	99.18	13.85	85.33	77.08	8.25	4
1.44	102.25	14.12	88.13	79.41	8.72	4
1.40	105.30	14.39	90.92	81.73	9.19	4
1.37	108.36	14.65	93.70	84.05	9.66	4
1.33	111.40	14.92	96.48	86.35	10.13	4
1.29	114.44	15.19	99.25	88.66	10.60	4
1.26	117.47	15.45	102.02	90.95	11.07	4
1.26	117.47	15.45	102.02	90.95	11.07	4
1.22	120.49	15.72	104.77	93.23	11.54	4
1.18	123.51	15.98	107.52	95.51	12.01	4
1.15	126.52	16.25	110.27	97.79	12.48	4
1.11	129.52	16.51	113.01	100.05	12.96	4
1.07	132.51	16.77	115.75	102.31	13.44	4
1.04	135.50	17.02	118.48	104.56	13.92	4
1.00	138.48	17.28	121.20	106.80	14.40	4
0.97	141.45	17.53	123.93	109.04	14.89	4
0.93	144.42	17.78	126.64	111.27	15.37	4
0.89	147.38	18.02	129.36	113.49	15.87	4
0.86	150.33	18.26	132.07	115.71	16.36	4
0.82	153.28	18.50	134.78	117.92	16.86	4
0.82	153.28	18.50	134.78	117.92	16.86	4
0.79	156.22	18.74	137.48	120.13	17.36	4
0.75	159.16	18.97	140.18	122.32	17.86	4
0.72	162.08	19.21	142.88	124.51	18.36	4
0.68	165.01	19.43	145.57	126.70	18.87	4
0.65	167.92	19.66	148.26	128.88	19.38	4
0.61	170.83	19.88	150.95	131.05	19.90	4

0.58	173.73	20.24	153.49	133.22	20.27	4
0.54	176.63	20.77	155.86	135.38	20.48	4
0.51	179.52	21.28	158.25	137.53	20.71	4
0.47	182.41	21.77	160.64	139.68	20.96	4
0.44	185.29	22.24	163.05	141.83	21.22	4
0.41	188.17	22.70	165.47	143.97	21.50	4
0.41	188.17	22.70	165.47	143.97	21.50	4
0.37	191.04	23.17	167.88	146.10	21.77	4
0.34	193.91	23.61	170.29	148.23	22.06	4
0.30	196.77	24.05	172.72	150.36	22.36	4
0.27	199.63	24.47	175.15	152.48	22.67	4
0.24	202.48	24.89	177.59	154.60	23.00	4
0.20	205.33	25.29	180.04	156.71	23.33	4
0.17	208.17	25.68	182.49	158.81	23.67	4
0.13	211.01	26.07	184.94	160.92	24.03	4
0.10	213.85	26.44	187.40	163.02	24.39	4
0.07	216.68	26.81	189.87	165.11	24.76	4
0.03	219.51	27.17	192.34	167.20	25.13	4
0.00	222.33	27.52	194.81	169.29	25.52	4

Time = 1085. Degree of Consolidation = 95.%

Total Settlement = 3.287

Settlement at End of Primary Consolidation = 3.455

Settlement caused by Primary Consolidation at time 1085. = 3.287

Settlement caused by Secondary Compression at time 1085. = 0.000

Settlement Due to Desiccation = 0.000

Surface Elevation = 1.20

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
10.50	10.49	4.83	0.91	0.91	0.91	3
10.10	10.09	4.62	0.91	0.91	0.91	3
9.70	9.69	4.41	0.91	0.91	0.91	3
9.30	9.29	4.20	0.91	0.91	0.91	3

output

8.90	8.89	3.99	0.91	0.91	0.90	3
8.50	8.49	3.78	0.91	0.90	0.90	3
8.10	8.09	3.57	0.90	0.90	0.90	3
7.70	7.69	3.36	0.90	0.90	0.90	3
7.30	7.29	3.15	0.90	0.90	0.90	3
6.90	6.89	2.94	0.90	0.90	0.90	3
6.50	6.49	2.73	0.90	0.90	0.90	3
6.50	6.49	2.73	1.40	1.40	1.39	2
5.85	5.84	2.46	1.39	1.39	1.39	2
5.19	5.19	2.18	1.39	1.39	1.38	2
4.54	4.54	1.91	1.39	1.38	1.38	2
3.89	3.89	1.64	1.38	1.38	1.38	2
3.24	3.24	1.36	1.38	1.38	1.38	2
2.59	2.59	1.09	1.38	1.38	1.38	2
1.94	1.94	0.82	1.38	1.37	1.37	2
1.29	1.29	0.55	1.38	1.37	1.37	2
0.65	0.65	0.27	1.37	1.37	1.37	2
0.00	0.00	0.00	1.37	1.36	1.36	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
10.49	216.20	33.98	182.22	163.16	19.06	3
10.09	263.20	52.43	210.77	188.16	22.61	3
9.69	310.19	70.77	239.42	213.14	26.28	3
9.29	357.17	89.02	268.15	238.12	30.03	3
8.89	404.14	107.23	296.91	263.08	33.82	3
8.49	451.10	125.47	325.63	288.04	37.59	3
8.09	498.05	143.81	354.25	312.98	41.26	3
7.69	544.99	162.35	382.64	337.92	44.72	3
7.29	591.92	181.26	410.66	362.85	47.81	3
6.89	638.85	200.81	438.04	387.76	50.27	3
6.49	685.76	221.44	464.32	412.67	51.65	3
6.49	685.76	221.44	464.32	412.67	51.65	2
5.84	754.58	248.14	506.45	453.41	53.04	2
5.19	823.35	288.06	535.29	494.08	41.21	2
4.54	892.06	329.70	562.36	534.70	27.66	2
3.89	960.73	369.43	591.30	575.28	16.02	2
3.24	1029.35	405.04	624.31	615.81	8.50	2
2.59	1097.93	430.62	667.31	656.30	11.01	2
1.94	1166.47	457.83	708.63	696.74	11.89	2
1.29	1234.96	487.61	747.34	737.14	10.20	2
0.65	1303.39	520.10	783.29	777.48	5.81	2
0.00	1371.77	553.61	818.16	817.77	0.39	2

Time = 1465. Degree of Consolidation = 53.%

Total Settlement = 0.009

Settlement at End of Primary Consolidation = 0.017

Settlement caused by Primary Consolidation at time 1465. = 0.009

Settlement caused by Secondary Compression at time 1465. = 0.000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
6.00	2.61	0.50	11.00	11.00	11.00	4
5.99	2.61	0.50	11.00	9.23	9.23	4
5.98	2.60	0.50	11.00	8.74	8.74	4
5.97	2.59	0.50	11.00	8.45	8.45	4
5.96	2.58	0.50	11.00	8.15	8.15	4
5.95	2.57	0.50	11.00	7.89	7.89	4
5.94	2.57	0.50	11.00	7.67	7.67	4
5.93	2.56	0.49	11.00	7.45	7.45	4
5.92	2.55	0.49	11.00	7.23	7.23	4
5.91	2.55	0.49	11.00	7.01	7.01	4
5.90	2.54	0.49	11.00	6.93	6.93	4
5.89	2.53	0.49	11.00	6.85	6.86	4
5.88	2.53	0.49	11.00	6.78	6.78	4
5.87	2.52	0.49	11.00	6.71	6.71	4
5.86	2.51	0.49	11.00	6.63	6.64	4
5.85	2.51	0.49	11.00	6.56	6.56	4
5.84	2.50	0.49	11.00	6.49	6.49	4
5.83	2.49	0.49	11.00	6.41	6.41	4
5.82	2.49	0.49	11.00	6.34	6.34	4
5.81	2.48	0.48	11.00	6.27	6.27	4
5.80	2.48	0.48	11.00	6.19	6.19	4
5.79	2.47	0.48	11.00	6.12	6.12	4
5.78	2.46	0.48	11.00	6.04	6.05	4
5.77	2.46	0.48	11.00	5.98	5.98	4
5.76	2.45	0.48	11.00	5.94	5.94	4
5.75	2.45	0.48	11.00	5.89	5.89	4
5.74	2.44	0.48	11.00	5.85	5.85	4
5.73	2.44	0.48	11.00	5.81	5.81	4
5.72	2.43	0.48	11.00	5.76	5.76	4
5.71	2.42	0.48	11.00	5.72	5.72	4

			output			
5.70	2.42	0.48	11.00	5.67	5.67	4
5.69	2.41	0.47	11.00	5.63	5.63	4
5.68	2.41	0.47	11.00	5.58	5.59	4
5.67	2.40	0.47	11.00	5.54	5.54	4
5.66	2.40	0.47	11.00	5.50	5.50	4
5.65	2.39	0.47	11.00	5.45	5.45	4
5.64	2.39	0.47	11.00	5.41	5.41	4
5.63	2.38	0.47	11.00	5.36	5.36	4
5.62	2.38	0.47	11.00	5.32	5.32	4
5.61	2.37	0.47	11.00	5.27	5.28	4
5.60	2.36	0.47	11.00	5.23	5.23	4
5.59	2.36	0.47	11.00	5.19	5.19	4
5.58	2.35	0.47	11.00	5.14	5.14	4
5.57	2.35	0.46	11.00	5.10	5.10	4
5.56	2.34	0.46	11.00	5.05	5.06	4
5.55	2.34	0.46	11.00	5.01	5.01	4
5.54	2.33	0.46	11.00	5.00	5.00	4
5.53	2.33	0.46	11.00	4.99	4.99	4
5.52	2.32	0.46	11.00	4.98	4.98	4
5.51	2.32	0.46	11.00	4.98	4.98	4
5.50	2.31	0.46	11.00	4.97	4.97	4
5.49	2.31	0.46	11.00	4.97	4.97	4
5.48	2.30	0.46	11.00	4.96	4.96	4
5.47	2.30	0.46	11.00	4.96	4.96	4
5.46	2.29	0.46	11.00	4.95	4.95	4
5.45	2.29	0.45	11.00	4.95	4.95	4
5.44	2.28	0.45	11.00	4.94	4.94	4
5.43	2.28	0.45	11.00	4.93	4.94	4
5.42	2.27	0.45	11.00	4.93	4.93	4
5.41	2.27	0.45	11.00	4.92	4.92	4
5.40	2.27	0.45	11.00	4.92	4.92	4
5.39	2.26	0.45	11.00	4.91	4.91	4
5.38	2.26	0.45	11.00	4.91	4.91	4
5.37	2.25	0.45	11.00	4.90	4.90	4
5.36	2.25	0.45	11.00	4.90	4.90	4
5.35	2.24	0.45	11.00	4.89	4.89	4
5.34	2.24	0.45	11.00	4.88	4.89	4
5.33	2.23	0.44	11.00	4.88	4.88	4
5.32	2.23	0.44	11.00	4.87	4.87	4
5.31	2.22	0.44	11.00	4.87	4.87	4
5.30	2.22	0.44	11.00	4.86	4.86	4
5.29	2.21	0.44	11.00	4.86	4.86	4
5.28	2.21	0.44	11.00	4.85	4.85	4
5.27	2.20	0.44	11.00	4.85	4.85	4
5.26	2.20	0.44	11.00	4.84	4.84	4
5.25	2.19	0.44	11.00	4.83	4.84	4
5.24	2.19	0.44	11.00	4.83	4.83	4
5.23	2.18	0.44	11.00	4.82	4.82	4

			output			
5.22	2.18	0.43	11.00	4.82	4.82	4
5.21	2.17	0.43	11.00	4.81	4.81	4
5.20	2.17	0.43	11.00	4.81	4.81	4
5.19	2.16	0.43	11.00	4.80	4.80	4
5.18	2.16	0.43	11.00	4.80	4.80	4
5.17	2.15	0.43	11.00	4.79	4.79	4
5.16	2.15	0.43	11.00	4.79	4.79	4
5.15	2.14	0.43	11.00	4.78	4.78	4
5.14	2.14	0.43	11.00	4.77	4.77	4
5.13	2.13	0.43	11.00	4.77	4.77	4
5.12	2.13	0.43	11.00	4.76	4.76	4
5.11	2.12	0.43	11.00	4.76	4.76	4
5.10	2.12	0.42	11.00	4.75	4.75	4
5.09	2.11	0.42	11.00	4.75	4.75	4
5.08	2.11	0.42	11.00	4.74	4.74	4
5.07	2.10	0.42	11.00	4.74	4.74	4
5.06	2.10	0.42	11.00	4.73	4.73	4
5.05	2.10	0.42	11.00	4.72	4.73	4
5.04	2.09	0.42	11.00	4.72	4.72	4
5.03	2.09	0.42	11.00	4.71	4.71	4
5.02	2.08	0.42	11.00	4.71	4.71	4
5.01	2.08	0.42	11.00	4.70	4.70	4
5.00	2.07	0.42	11.00	4.70	4.70	4
5.00	2.07	0.42	11.00	4.70	4.70	4
4.92	2.03	0.41	11.00	4.65	4.65	4
4.83	1.99	0.40	11.00	4.60	4.61	4
4.75	1.95	0.40	11.00	4.56	4.56	4
4.67	1.92	0.39	11.00	4.51	4.51	4
4.58	1.88	0.38	11.00	4.47	4.47	4
4.50	1.84	0.37	11.00	4.42	4.42	4
4.42	1.80	0.37	11.00	4.37	4.38	4
4.33	1.77	0.36	11.00	4.33	4.33	4
4.25	1.73	0.35	11.00	4.28	4.28	4
4.17	1.69	0.35	11.00	4.24	4.24	4
4.08	1.66	0.34	11.00	4.19	4.19	4
4.00	1.62	0.33	11.00	4.14	4.14	4
4.00	1.62	0.33	11.00	4.14	4.14	4
3.92	1.58	0.33	11.00	4.13	4.10	4
3.83	1.55	0.32	11.00	4.11	4.05	4
3.75	1.51	0.31	11.00	4.10	4.01	4
3.67	1.48	0.31	11.00	4.08	3.98	4
3.58	1.44	0.30	11.00	4.07	3.97	4
3.50	1.41	0.29	11.00	4.05	3.95	4
3.42	1.37	0.28	11.00	4.04	3.93	4
3.33	1.34	0.28	11.00	4.02	3.91	4
3.25	1.30	0.27	11.00	4.01	3.89	4
3.17	1.27	0.26	11.00	3.99	3.87	4
3.08	1.23	0.26	11.00	3.98	3.86	4

3.00	1.20	0.25	11.00	3.97	3.84	4
3.00	1.20	0.25	11.00	3.97	3.84	4
2.92	1.16	0.24	11.00	3.96	3.82	4
2.83	1.13	0.24	11.00	3.94	3.80	4
2.75	1.10	0.23	11.00	3.93	3.78	4
2.67	1.06	0.22	11.00	3.92	3.76	4
2.58	1.03	0.22	11.00	3.91	3.74	4
2.50	0.99	0.21	11.00	3.90	3.73	4
2.42	0.96	0.20	11.00	3.89	3.71	4
2.33	0.93	0.19	11.00	3.88	3.69	4
2.25	0.89	0.19	11.00	3.87	3.67	4
2.17	0.86	0.18	11.00	3.86	3.65	4
2.08	0.82	0.17	11.00	3.85	3.63	4
2.00	0.79	0.17	11.00	3.84	3.62	4
2.00	0.79	0.17	11.00	3.84	3.62	4
1.92	0.76	0.16	11.00	3.83	3.60	4
1.83	0.72	0.15	11.00	3.82	3.58	4
1.75	0.69	0.15	11.00	3.81	3.56	4
1.67	0.66	0.14	11.00	3.80	3.54	4
1.58	0.62	0.13	11.00	3.80	3.52	4
1.50	0.59	0.13	11.00	3.79	3.51	4
1.42	0.56	0.12	11.00	3.78	3.49	4
1.33	0.52	0.11	11.00	3.77	3.48	4
1.25	0.49	0.10	11.00	3.76	3.48	4
1.17	0.46	0.10	11.00	3.75	3.47	4
1.08	0.42	0.09	11.00	3.75	3.46	4
1.00	0.39	0.08	11.00	3.74	3.45	4
1.00	0.39	0.08	11.00	3.74	3.45	4
0.92	0.36	0.08	11.00	3.73	3.44	4
0.83	0.33	0.07	11.00	3.72	3.43	4
0.75	0.29	0.06	11.00	3.72	3.42	4
0.67	0.26	0.06	11.00	3.71	3.41	4
0.58	0.23	0.05	11.00	3.70	3.40	4
0.50	0.19	0.04	11.00	3.69	3.39	4
0.42	0.16	0.03	11.00	3.69	3.38	4
0.33	0.13	0.03	11.00	3.68	3.37	4
0.25	0.10	0.02	11.00	3.67	3.36	4
0.17	0.06	0.01	11.00	3.66	3.36	4
0.08	0.03	0.01	11.00	3.66	3.35	4
0.00	0.00	0.00	11.00	3.65	3.34	4

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
2.61	0.00	0.00	0.00	0.00	0.00	4
2.61	0.66	0.09	0.57	0.57	0.00	4
2.60	1.26	0.18	1.09	1.09	0.00	4

output

2.59	1.85	0.27	1.59	1.59	0.00	4
2.58	2.42	0.35	2.07	2.07	0.00	4
2.57	2.98	0.44	2.54	2.54	0.00	4
2.57	3.52	0.53	2.99	2.99	0.00	4
2.56	4.06	0.62	3.44	3.44	0.00	4
2.55	4.58	0.71	3.87	3.87	0.00	4
2.55	5.09	0.80	4.29	4.29	0.00	4
2.54	5.59	0.88	4.71	4.71	0.00	4
2.53	6.09	0.97	5.12	5.12	0.00	4
2.53	6.59	1.06	5.53	5.53	0.00	4
2.52	7.08	1.15	5.93	5.93	0.00	4
2.51	7.57	1.24	6.33	6.33	0.00	4
2.51	8.05	1.33	6.72	6.72	0.00	4
2.50	8.53	1.41	7.11	7.11	0.00	4
2.49	9.00	1.50	7.50	7.50	0.00	4
2.49	9.48	1.59	7.88	7.88	0.00	4
2.48	9.94	1.68	8.26	8.26	0.00	4
2.48	10.41	1.77	8.64	8.64	0.00	4
2.47	10.87	1.86	9.01	9.01	0.00	4
2.46	11.33	1.94	9.38	9.38	0.00	4
2.46	11.78	2.03	9.75	9.75	0.00	4
2.45	12.23	2.12	10.11	10.11	0.00	4
2.45	12.68	2.21	10.47	10.47	0.00	4
2.44	13.12	2.30	10.82	10.82	0.00	4
2.44	13.57	2.39	11.18	11.18	0.00	4
2.43	14.01	2.48	11.53	11.53	0.00	4
2.42	14.45	2.56	11.88	11.88	0.00	4
2.42	14.88	2.65	12.23	12.23	0.00	4
2.41	15.32	2.74	12.58	12.58	0.00	4
2.41	15.75	2.83	12.92	12.92	0.00	4
2.40	16.18	2.92	13.26	13.26	0.00	4
2.40	16.61	3.01	13.60	13.60	0.00	4
2.39	17.03	3.09	13.94	13.94	0.00	4
2.39	17.45	3.18	14.27	14.27	0.00	4
2.38	17.87	3.27	14.60	14.60	0.00	4
2.38	18.29	3.36	14.93	14.93	0.00	4
2.37	18.71	3.45	15.26	15.26	0.00	4
2.36	19.12	3.54	15.59	15.59	0.00	4
2.36	19.53	3.62	15.91	15.91	0.00	4
2.35	19.94	3.71	16.23	16.23	0.00	4
2.35	20.35	3.80	16.55	16.55	0.00	4
2.34	20.75	3.89	16.86	16.86	0.00	4
2.34	21.15	3.98	17.18	17.18	0.00	4
2.33	21.55	4.07	17.49	17.49	0.00	4
2.33	21.95	4.15	17.80	17.80	0.00	4
2.32	22.35	4.24	18.11	18.11	0.00	4
2.32	22.75	4.33	18.42	18.42	0.00	4
2.31	23.15	4.42	18.73	18.73	0.00	4

			output			
2.31	23.55	4.51	19.04	19.04	0.00	4
2.30	23.95	4.60	19.35	19.35	0.00	4
2.30	24.35	4.69	19.66	19.66	0.00	4
2.29	24.75	4.77	19.97	19.97	0.00	4
2.29	25.14	4.86	20.28	20.28	0.00	4
2.28	25.54	4.95	20.59	20.59	0.00	4
2.28	25.94	5.04	20.90	20.90	0.00	4
2.27	26.34	5.13	21.21	21.21	0.00	4
2.27	26.73	5.22	21.52	21.52	0.00	4
2.27	27.13	5.30	21.82	21.82	0.00	4
2.26	27.52	5.39	22.13	22.13	0.00	4
2.26	27.92	5.48	22.44	22.44	0.00	4
2.25	28.32	5.57	22.75	22.75	0.00	4
2.25	28.71	5.66	23.05	23.05	0.00	4
2.24	29.11	5.75	23.36	23.36	0.00	4
2.24	29.50	5.83	23.67	23.67	0.00	4
2.23	29.89	5.92	23.97	23.97	0.00	4
2.23	30.29	6.01	24.28	24.28	0.00	4
2.22	30.68	6.10	24.58	24.58	0.00	4
2.22	31.08	6.19	24.89	24.89	0.00	4
2.21	31.47	6.28	25.19	25.19	0.00	4
2.21	31.86	6.36	25.50	25.50	0.00	4
2.20	32.25	6.45	25.80	25.80	0.00	4
2.20	32.65	6.54	26.10	26.10	0.00	4
2.19	33.04	6.63	26.41	26.41	0.00	4
2.19	33.43	6.72	26.71	26.71	0.00	4
2.18	33.82	6.81	27.01	27.01	0.00	4
2.18	34.21	6.90	27.32	27.32	0.00	4
2.17	34.60	6.98	27.62	27.62	0.00	4
2.17	34.99	7.07	27.92	27.92	0.00	4
2.16	35.38	7.16	28.22	28.22	0.00	4
2.16	35.77	7.25	28.52	28.52	0.00	4
2.15	36.16	7.34	28.83	28.83	0.00	4
2.15	36.55	7.43	29.13	29.13	0.00	4
2.14	36.94	7.51	29.43	29.43	0.00	4
2.14	37.33	7.60	29.73	29.73	0.00	4
2.13	37.72	7.69	30.03	30.03	0.00	4
2.13	38.11	7.78	30.33	30.33	0.00	4
2.12	38.50	7.87	30.63	30.63	0.00	4
2.12	38.88	7.96	30.93	30.93	0.00	4
2.11	39.27	8.04	31.23	31.23	0.00	4
2.11	39.66	8.13	31.52	31.52	0.00	4
2.10	40.04	8.22	31.82	31.82	0.00	4
2.10	40.43	8.31	32.12	32.12	0.00	4
2.10	40.82	8.40	32.42	32.42	0.00	4
2.09	41.20	8.49	32.72	32.72	0.00	4
2.09	41.59	8.57	33.01	33.01	0.00	4
2.08	41.97	8.66	33.31	33.31	0.00	4

output

2.08	42.36	8.75	33.61	33.61	0.00	4
2.07	42.74	8.84	33.90	33.90	0.00	4
2.07	42.74	8.84	33.90	33.90	0.00	4
2.03	45.94	9.58	36.36	36.36	0.00	4
1.99	49.11	10.31	38.80	38.80	0.00	4
1.95	52.27	11.05	41.22	41.22	0.00	4
1.92	55.41	11.79	43.62	43.62	0.00	4
1.88	58.52	12.52	46.00	46.00	0.00	4
1.84	61.62	13.26	48.36	48.36	0.00	4
1.80	64.69	14.00	50.70	50.70	0.00	4
1.77	67.75	14.73	53.01	53.01	0.00	4
1.73	70.78	15.47	55.31	55.31	0.00	4
1.69	73.80	16.21	57.59	57.59	0.00	4
1.66	76.79	16.94	59.85	59.85	0.00	4
1.62	79.77	17.68	62.09	62.09	0.00	4
1.62	79.77	17.68	62.09	62.09	0.00	4
1.58	82.73	17.95	64.79	64.32	0.47	4
1.55	85.69	18.21	67.48	66.54	0.94	4
1.51	88.64	18.46	70.17	68.75	1.43	4
1.48	91.58	18.71	72.87	70.95	1.91	4
1.44	94.51	18.95	75.56	73.15	2.41	4
1.41	97.44	19.19	78.25	75.34	2.91	4
1.37	100.36	19.42	80.94	77.53	3.41	4
1.34	103.28	19.65	83.63	79.71	3.92	4
1.30	106.19	19.87	86.32	81.88	4.44	4
1.27	109.09	20.22	88.88	84.05	4.83	4
1.23	111.99	20.74	91.26	86.21	5.05	4
1.20	114.88	21.24	93.65	88.36	5.28	4
1.20	114.88	21.24	93.65	88.36	5.28	4
1.16	117.77	21.74	96.03	90.51	5.52	4
1.13	120.65	22.22	98.43	92.66	5.77	4
1.10	123.53	22.69	100.84	94.80	6.04	4
1.06	126.40	23.14	103.26	96.94	6.32	4
1.03	129.27	23.58	105.68	99.07	6.62	4
0.99	132.13	24.01	108.12	101.19	6.93	4
0.96	134.99	24.43	110.56	103.31	7.25	4
0.93	137.84	24.83	113.01	105.43	7.58	4
0.89	140.69	25.23	115.46	107.54	7.92	4
0.86	143.54	25.62	117.92	109.65	8.27	4
0.82	146.38	25.99	120.38	111.75	8.63	4
0.79	149.21	26.37	122.85	113.85	8.99	4
0.79	149.21	26.37	122.85	113.85	8.99	4
0.76	152.04	26.74	125.31	115.95	9.36	4
0.72	154.87	27.10	127.77	118.04	9.73	4
0.69	157.70	27.46	130.24	120.13	10.11	4
0.66	160.52	27.81	132.71	122.21	10.50	4
0.62	163.33	28.15	135.18	124.29	10.89	4
0.59	166.15	28.49	137.66	126.37	11.29	4

0.56	168.96	28.83	140.13	128.44	11.69	4
0.52	171.76	29.16	142.61	130.51	12.10	4
0.49	174.57	29.48	145.08	132.58	12.51	4
0.46	177.36	29.80	147.56	134.64	12.93	4
0.42	180.16	30.12	150.04	136.70	13.35	4
0.39	182.95	30.43	152.52	138.75	13.77	4
0.39	182.95	30.43	152.52	138.75	13.77	4
0.36	185.74	30.74	155.00	140.80	14.19	4
0.33	188.53	31.05	157.47	142.85	14.62	4
0.29	191.31	31.36	159.95	144.90	15.05	4
0.26	194.09	31.66	162.43	146.94	15.49	4
0.23	196.86	31.96	164.90	148.98	15.92	4
0.19	199.63	32.26	167.38	151.01	16.36	4
0.16	202.40	32.55	169.85	153.05	16.81	4
0.13	205.17	32.84	172.33	155.08	17.25	4
0.10	207.93	33.13	174.80	157.10	17.70	4
0.06	210.69	33.41	177.28	159.12	18.15	4
0.03	213.45	33.70	179.75	161.14	18.61	4
0.00	216.20	33.98	182.22	163.16	19.06	4

Time = 1465. Degree of Consolidation = 98.%

Total Settlement = 3.385

Settlement at End of Primary Consolidation = 3.455

Settlement caused by Primary Consolidation at time 1465. = 3.384

Settlement caused by Secondary Compression at time 1465. = 0.001

Settlement Due to Desiccation = 0.000

Surface Elevation = 1.11

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
10.50	10.49	4.83	0.91	0.91	0.91	3
10.10	10.09	4.62	0.91	0.91	0.91	3
9.70	9.69	4.41	0.91	0.91	0.91	3
9.30	9.29	4.20	0.91	0.91	0.91	3

output

8.90	8.89	3.99	0.91	0.91	0.90	3
8.50	8.49	3.78	0.91	0.90	0.90	3
8.10	8.09	3.57	0.90	0.90	0.90	3
7.70	7.69	3.36	0.90	0.90	0.90	3
7.30	7.29	3.15	0.90	0.90	0.90	3
6.90	6.89	2.94	0.90	0.90	0.90	3
6.50	6.49	2.73	0.90	0.90	0.90	3
6.50	6.49	2.73	1.40	1.40	1.39	2
5.85	5.84	2.46	1.39	1.39	1.39	2
5.19	5.19	2.18	1.39	1.39	1.38	2
4.54	4.54	1.91	1.39	1.38	1.38	2
3.89	3.89	1.64	1.38	1.38	1.38	2
3.24	3.24	1.36	1.38	1.38	1.38	2
2.59	2.59	1.09	1.38	1.38	1.38	2
1.94	1.94	0.82	1.38	1.37	1.37	2
1.29	1.29	0.55	1.38	1.37	1.37	2
0.65	0.65	0.27	1.37	1.37	1.37	2
0.00	0.00	0.00	1.37	1.36	1.36	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
10.49	213.51	37.53	175.98	160.47	15.51	3
10.09	260.51	55.77	204.74	185.46	19.28	3
9.69	307.50	73.88	233.62	210.45	23.17	3
9.29	354.47	91.89	262.58	235.42	27.16	3
8.89	401.44	109.86	291.59	260.38	31.20	3
8.49	448.40	127.83	320.58	285.34	35.24	3
8.09	495.35	145.88	349.48	310.29	39.19	3
7.69	542.29	164.11	378.18	335.22	42.96	3
7.29	589.22	182.67	406.55	360.15	46.40	3
6.89	636.14	201.81	434.33	385.06	49.27	3
6.49	683.06	221.94	461.11	409.97	51.14	3
6.49	683.06	221.94	461.11	409.97	51.14	2
5.84	751.88	248.14	503.74	450.70	53.04	2
5.19	820.64	288.06	532.59	491.38	41.21	2
4.54	889.36	329.70	559.66	532.00	27.66	2
3.89	958.03	369.43	588.60	572.57	16.02	2
3.24	1026.65	405.04	621.61	613.11	8.50	2
2.59	1095.23	430.62	664.61	653.60	11.01	2
1.94	1163.77	457.83	705.93	694.04	11.89	2
1.29	1232.25	487.61	744.64	734.44	10.20	2
0.65	1300.69	520.10	780.59	774.78	5.81	2
0.00	1369.07	553.61	815.46	815.07	0.39	2

Time = 1825. Degree of Consolidation = 54.%

Total Settlement = 0.009

Settlement at End of Primary Consolidation = 0.017

Settlement caused by Primary Consolidation at time 1825. = 0.009

Settlement caused by Secondary Compression at time 1825. = 0.000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
6.00	2.57	0.50	11.00	11.00	11.00	4
5.99	2.56	0.50	11.00	9.23	9.23	4
5.98	2.55	0.50	11.00	8.74	8.74	4
5.97	2.55	0.50	11.00	8.45	8.45	4
5.96	2.54	0.50	11.00	8.15	8.15	4
5.95	2.53	0.50	11.00	7.89	7.89	4
5.94	2.52	0.50	11.00	7.67	7.67	4
5.93	2.52	0.49	11.00	7.45	7.45	4
5.92	2.51	0.49	11.00	7.23	7.23	4
5.91	2.50	0.49	11.00	7.01	7.01	4
5.90	2.50	0.49	11.00	6.93	6.93	4
5.89	2.49	0.49	11.00	6.85	6.86	4
5.88	2.48	0.49	11.00	6.78	6.78	4
5.87	2.48	0.49	11.00	6.71	6.71	4
5.86	2.47	0.49	11.00	6.63	6.64	4
5.85	2.46	0.49	11.00	6.56	6.56	4
5.84	2.46	0.49	11.00	6.49	6.49	4
5.83	2.45	0.49	11.00	6.41	6.41	4
5.82	2.45	0.49	11.00	6.34	6.34	4
5.81	2.44	0.48	11.00	6.27	6.27	4
5.80	2.43	0.48	11.00	6.19	6.19	4
5.79	2.43	0.48	11.00	6.12	6.12	4
5.78	2.42	0.48	11.00	6.04	6.05	4
5.77	2.42	0.48	11.00	5.98	5.98	4
5.76	2.41	0.48	11.00	5.94	5.94	4
5.75	2.40	0.48	11.00	5.89	5.89	4
5.74	2.40	0.48	11.00	5.85	5.85	4
5.73	2.39	0.48	11.00	5.81	5.81	4
5.72	2.39	0.48	11.00	5.76	5.76	4
5.71	2.38	0.48	11.00	5.72	5.72	4

			output			
5.70	2.38	0.48	11.00	5.67	5.67	4
5.69	2.37	0.47	11.00	5.63	5.63	4
5.68	2.36	0.47	11.00	5.58	5.59	4
5.67	2.36	0.47	11.00	5.54	5.54	4
5.66	2.35	0.47	11.00	5.50	5.50	4
5.65	2.35	0.47	11.00	5.45	5.45	4
5.64	2.34	0.47	11.00	5.41	5.41	4
5.63	2.34	0.47	11.00	5.36	5.36	4
5.62	2.33	0.47	11.00	5.32	5.32	4
5.61	2.33	0.47	11.00	5.27	5.28	4
5.60	2.32	0.47	11.00	5.23	5.23	4
5.59	2.32	0.47	11.00	5.19	5.19	4
5.58	2.31	0.47	11.00	5.14	5.14	4
5.57	2.31	0.46	11.00	5.10	5.10	4
5.56	2.30	0.46	11.00	5.05	5.06	4
5.55	2.30	0.46	11.00	5.01	5.01	4
5.54	2.29	0.46	11.00	5.00	5.00	4
5.53	2.29	0.46	11.00	4.99	4.99	4
5.52	2.28	0.46	11.00	4.98	4.98	4
5.51	2.28	0.46	11.00	4.98	4.98	4
5.50	2.27	0.46	11.00	4.97	4.97	4
5.49	2.27	0.46	11.00	4.97	4.97	4
5.48	2.26	0.46	11.00	4.96	4.96	4
5.47	2.26	0.46	11.00	4.96	4.96	4
5.46	2.25	0.46	11.00	4.95	4.95	4
5.45	2.25	0.45	11.00	4.95	4.95	4
5.44	2.24	0.45	11.00	4.94	4.94	4
5.43	2.24	0.45	11.00	4.93	4.94	4
5.42	2.23	0.45	11.00	4.93	4.93	4
5.41	2.23	0.45	11.00	4.92	4.92	4
5.40	2.22	0.45	11.00	4.92	4.92	4
5.39	2.22	0.45	11.00	4.91	4.91	4
5.38	2.21	0.45	11.00	4.91	4.91	4
5.37	2.21	0.45	11.00	4.90	4.90	4
5.36	2.20	0.45	11.00	4.90	4.90	4
5.35	2.20	0.45	11.00	4.89	4.89	4
5.34	2.19	0.45	11.00	4.88	4.89	4
5.33	2.19	0.44	11.00	4.88	4.88	4
5.32	2.18	0.44	11.00	4.87	4.87	4
5.31	2.18	0.44	11.00	4.87	4.87	4
5.30	2.17	0.44	11.00	4.86	4.86	4
5.29	2.17	0.44	11.00	4.86	4.86	4
5.28	2.16	0.44	11.00	4.85	4.85	4
5.27	2.16	0.44	11.00	4.85	4.85	4
5.26	2.15	0.44	11.00	4.84	4.84	4
5.25	2.15	0.44	11.00	4.83	4.84	4
5.24	2.14	0.44	11.00	4.83	4.83	4
5.23	2.14	0.44	11.00	4.82	4.82	4

			output			
5.22	2.13	0.43	11.00	4.82	4.82	4
5.21	2.13	0.43	11.00	4.81	4.81	4
5.20	2.12	0.43	11.00	4.81	4.81	4
5.19	2.12	0.43	11.00	4.80	4.80	4
5.18	2.11	0.43	11.00	4.80	4.80	4
5.17	2.11	0.43	11.00	4.79	4.79	4
5.16	2.10	0.43	11.00	4.79	4.79	4
5.15	2.10	0.43	11.00	4.78	4.78	4
5.14	2.10	0.43	11.00	4.77	4.77	4
5.13	2.09	0.43	11.00	4.77	4.77	4
5.12	2.09	0.43	11.00	4.76	4.76	4
5.11	2.08	0.43	11.00	4.76	4.76	4
5.10	2.08	0.42	11.00	4.75	4.75	4
5.09	2.07	0.42	11.00	4.75	4.75	4
5.08	2.07	0.42	11.00	4.74	4.74	4
5.07	2.06	0.42	11.00	4.74	4.74	4
5.06	2.06	0.42	11.00	4.73	4.73	4
5.05	2.05	0.42	11.00	4.72	4.73	4
5.04	2.05	0.42	11.00	4.72	4.72	4
5.03	2.04	0.42	11.00	4.71	4.71	4
5.02	2.04	0.42	11.00	4.71	4.71	4
5.01	2.03	0.42	11.00	4.70	4.70	4
5.00	2.03	0.42	11.00	4.70	4.70	4
5.00	2.03	0.42	11.00	4.70	4.70	4
4.92	1.99	0.41	11.00	4.65	4.65	4
4.83	1.95	0.40	11.00	4.60	4.61	4
4.75	1.91	0.40	11.00	4.56	4.56	4
4.67	1.87	0.39	11.00	4.51	4.51	4
4.58	1.83	0.38	11.00	4.47	4.47	4
4.50	1.80	0.37	11.00	4.42	4.42	4
4.42	1.76	0.37	11.00	4.37	4.38	4
4.33	1.72	0.36	11.00	4.33	4.33	4
4.25	1.69	0.35	11.00	4.28	4.28	4
4.17	1.65	0.35	11.00	4.24	4.24	4
4.08	1.61	0.34	11.00	4.19	4.19	4
4.00	1.58	0.33	11.00	4.14	4.14	4
4.00	1.58	0.33	11.00	4.14	4.14	4
3.92	1.54	0.33	11.00	4.10	4.10	4
3.83	1.51	0.32	11.00	4.05	4.05	4
3.75	1.47	0.31	11.00	4.01	4.01	4
3.67	1.44	0.31	11.00	3.98	3.98	4
3.58	1.40	0.30	11.00	3.97	3.97	4
3.50	1.37	0.29	11.00	3.95	3.95	4
3.42	1.33	0.28	11.00	3.93	3.93	4
3.33	1.30	0.28	11.00	3.91	3.91	4
3.25	1.26	0.27	11.00	3.89	3.89	4
3.17	1.23	0.26	11.00	3.87	3.87	4
3.08	1.20	0.26	11.00	3.85	3.86	4

3.00	1.16	0.25	11.00	3.84	3.84	4
3.00	1.16	0.25	11.00	3.84	3.84	4
2.92	1.13	0.24	11.00	3.82	3.82	4
2.83	1.10	0.24	11.00	3.80	3.80	4
2.75	1.06	0.23	11.00	3.78	3.78	4
2.67	1.03	0.22	11.00	3.76	3.76	4
2.58	1.00	0.22	11.00	3.74	3.74	4
2.50	0.96	0.21	11.00	3.73	3.73	4
2.42	0.93	0.20	11.00	3.71	3.71	4
2.33	0.90	0.19	11.00	3.69	3.69	4
2.25	0.87	0.19	11.00	3.67	3.67	4
2.17	0.83	0.18	11.00	3.65	3.65	4
2.08	0.80	0.17	11.00	3.63	3.63	4
2.00	0.77	0.17	11.00	3.62	3.62	4
2.00	0.77	0.17	11.00	3.62	3.62	4
1.92	0.74	0.16	11.00	3.62	3.60	4
1.83	0.71	0.15	11.00	3.63	3.58	4
1.75	0.67	0.15	11.00	3.63	3.56	4
1.67	0.64	0.14	11.00	3.64	3.54	4
1.58	0.61	0.13	11.00	3.64	3.52	4
1.50	0.58	0.13	11.00	3.64	3.51	4
1.42	0.54	0.12	11.00	3.65	3.49	4
1.33	0.51	0.11	11.00	3.64	3.48	4
1.25	0.48	0.10	11.00	3.64	3.48	4
1.17	0.45	0.10	11.00	3.64	3.47	4
1.08	0.42	0.09	11.00	3.64	3.46	4
1.00	0.38	0.08	11.00	3.63	3.45	4
1.00	0.38	0.08	11.00	3.63	3.45	4
0.92	0.35	0.08	11.00	3.63	3.44	4
0.83	0.32	0.07	11.00	3.62	3.43	4
0.75	0.29	0.06	11.00	3.62	3.42	4
0.67	0.25	0.06	11.00	3.61	3.41	4
0.58	0.22	0.05	11.00	3.60	3.40	4
0.50	0.19	0.04	11.00	3.60	3.39	4
0.42	0.16	0.03	11.00	3.59	3.38	4
0.33	0.13	0.03	11.00	3.59	3.37	4
0.25	0.10	0.02	11.00	3.58	3.36	4
0.17	0.06	0.01	11.00	3.57	3.36	4
0.08	0.03	0.01	11.00	3.57	3.35	4
0.00	0.00	0.00	11.00	3.56	3.34	4

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
2.57	0.00	0.00	0.00	0.00	0.00	4
2.56	0.66	0.09	0.57	0.57	0.00	4
2.55	1.26	0.18	1.09	1.09	0.00	4

output

2.55	1.85	0.27	1.59	1.59	0.00	4
2.54	2.42	0.35	2.07	2.07	0.00	4
2.53	2.98	0.44	2.54	2.54	0.00	4
2.52	3.52	0.53	2.99	2.99	0.00	4
2.52	4.06	0.62	3.44	3.44	0.00	4
2.51	4.58	0.71	3.87	3.87	0.00	4
2.50	5.09	0.80	4.29	4.29	0.00	4
2.50	5.59	0.88	4.71	4.71	0.00	4
2.49	6.09	0.97	5.12	5.12	0.00	4
2.48	6.59	1.06	5.53	5.53	0.00	4
2.48	7.08	1.15	5.93	5.93	0.00	4
2.47	7.57	1.24	6.33	6.33	0.00	4
2.46	8.05	1.33	6.72	6.72	0.00	4
2.46	8.53	1.41	7.11	7.11	0.00	4
2.45	9.00	1.50	7.50	7.50	0.00	4
2.45	9.48	1.59	7.88	7.88	0.00	4
2.44	9.94	1.68	8.26	8.26	0.00	4
2.43	10.41	1.77	8.64	8.64	0.00	4
2.43	10.87	1.86	9.01	9.01	0.00	4
2.42	11.33	1.94	9.38	9.38	0.00	4
2.42	11.78	2.03	9.75	9.75	0.00	4
2.41	12.23	2.12	10.11	10.11	0.00	4
2.40	12.68	2.21	10.47	10.47	0.00	4
2.40	13.12	2.30	10.82	10.82	0.00	4
2.39	13.57	2.39	11.18	11.18	0.00	4
2.39	14.01	2.48	11.53	11.53	0.00	4
2.38	14.45	2.56	11.88	11.88	0.00	4
2.38	14.88	2.65	12.23	12.23	0.00	4
2.37	15.32	2.74	12.58	12.58	0.00	4
2.36	15.75	2.83	12.92	12.92	0.00	4
2.36	16.18	2.92	13.26	13.26	0.00	4
2.35	16.61	3.01	13.60	13.60	0.00	4
2.35	17.03	3.09	13.94	13.94	0.00	4
2.34	17.45	3.18	14.27	14.27	0.00	4
2.34	17.87	3.27	14.60	14.60	0.00	4
2.33	18.29	3.36	14.93	14.93	0.00	4
2.33	18.71	3.45	15.26	15.26	0.00	4
2.32	19.12	3.54	15.59	15.59	0.00	4
2.32	19.53	3.62	15.91	15.91	0.00	4
2.31	19.94	3.71	16.23	16.23	0.00	4
2.31	20.35	3.80	16.55	16.55	0.00	4
2.30	20.75	3.89	16.86	16.86	0.00	4
2.30	21.15	3.98	17.18	17.18	0.00	4
2.29	21.55	4.07	17.49	17.49	0.00	4
2.29	21.95	4.15	17.80	17.80	0.00	4
2.28	22.35	4.24	18.11	18.11	0.00	4
2.28	22.75	4.33	18.42	18.42	0.00	4
2.27	23.15	4.42	18.73	18.73	0.00	4

			output			
2.27	23.55	4.51	19.04	19.04	0.00	4
2.26	23.95	4.60	19.35	19.35	0.00	4
2.26	24.35	4.69	19.66	19.66	0.00	4
2.25	24.75	4.77	19.97	19.97	0.00	4
2.25	25.14	4.86	20.28	20.28	0.00	4
2.24	25.54	4.95	20.59	20.59	0.00	4
2.24	25.94	5.04	20.90	20.90	0.00	4
2.23	26.34	5.13	21.21	21.21	0.00	4
2.23	26.73	5.22	21.52	21.52	0.00	4
2.22	27.13	5.30	21.82	21.82	0.00	4
2.22	27.52	5.39	22.13	22.13	0.00	4
2.21	27.92	5.48	22.44	22.44	0.00	4
2.21	28.32	5.57	22.75	22.75	0.00	4
2.20	28.71	5.66	23.05	23.05	0.00	4
2.20	29.11	5.75	23.36	23.36	0.00	4
2.19	29.50	5.83	23.67	23.67	0.00	4
2.19	29.89	5.92	23.97	23.97	0.00	4
2.18	30.29	6.01	24.28	24.28	0.00	4
2.18	30.68	6.10	24.58	24.58	0.00	4
2.17	31.08	6.19	24.89	24.89	0.00	4
2.17	31.47	6.28	25.19	25.19	0.00	4
2.16	31.86	6.36	25.50	25.50	0.00	4
2.16	32.25	6.45	25.80	25.80	0.00	4
2.15	32.65	6.54	26.10	26.10	0.00	4
2.15	33.04	6.63	26.41	26.41	0.00	4
2.14	33.43	6.72	26.71	26.71	0.00	4
2.14	33.82	6.81	27.01	27.01	0.00	4
2.13	34.21	6.90	27.32	27.32	0.00	4
2.13	34.60	6.98	27.62	27.62	0.00	4
2.12	34.99	7.07	27.92	27.92	0.00	4
2.12	35.38	7.16	28.22	28.22	0.00	4
2.11	35.77	7.25	28.52	28.52	0.00	4
2.11	36.16	7.34	28.83	28.83	0.00	4
2.10	36.55	7.43	29.13	29.13	0.00	4
2.10	36.94	7.51	29.43	29.43	0.00	4
2.10	37.33	7.60	29.73	29.73	0.00	4
2.09	37.72	7.69	30.03	30.03	0.00	4
2.09	38.11	7.78	30.33	30.33	0.00	4
2.08	38.50	7.87	30.63	30.63	0.00	4
2.08	38.88	7.96	30.93	30.93	0.00	4
2.07	39.27	8.04	31.23	31.23	0.00	4
2.07	39.66	8.13	31.52	31.52	0.00	4
2.06	40.04	8.22	31.82	31.82	0.00	4
2.06	40.43	8.31	32.12	32.12	0.00	4
2.05	40.82	8.40	32.42	32.42	0.00	4
2.05	41.20	8.49	32.72	32.72	0.00	4
2.04	41.59	8.57	33.01	33.01	0.00	4
2.04	41.97	8.66	33.31	33.31	0.00	4

output

2.03	42.36	8.75	33.61	33.61	0.00	4
2.03	42.74	8.84	33.90	33.90	0.00	4
2.03	42.74	8.84	33.90	33.90	0.00	4
1.99	45.94	9.58	36.36	36.36	0.00	4
1.95	49.11	10.31	38.80	38.80	0.00	4
1.91	52.27	11.05	41.22	41.22	0.00	4
1.87	55.41	11.79	43.62	43.62	0.00	4
1.83	58.52	12.52	46.00	46.00	0.00	4
1.80	61.62	13.26	48.36	48.36	0.00	4
1.76	64.69	14.00	50.70	50.70	0.00	4
1.72	67.75	14.73	53.01	53.01	0.00	4
1.69	70.78	15.47	55.31	55.31	0.00	4
1.65	73.80	16.21	57.59	57.59	0.00	4
1.61	76.79	16.94	59.85	59.85	0.00	4
1.58	79.77	17.68	62.09	62.09	0.00	4
1.58	79.77	17.68	62.09	62.09	0.00	4
1.54	82.73	18.42	64.31	64.31	0.00	4
1.51	85.66	19.15	66.51	66.51	0.00	4
1.47	88.58	19.89	68.69	68.69	0.00	4
1.44	91.48	20.63	70.85	70.85	0.00	4
1.40	94.37	21.36	73.01	73.01	0.00	4
1.37	97.25	22.10	75.15	75.15	0.00	4
1.33	100.13	22.84	77.29	77.29	0.00	4
1.30	103.00	23.57	79.43	79.43	0.00	4
1.26	105.86	24.31	81.55	81.55	0.00	4
1.23	108.71	25.05	83.67	83.67	0.00	4
1.20	111.56	25.78	85.77	85.77	0.00	4
1.16	114.39	26.52	87.87	87.87	0.00	4
1.16	114.39	26.52	87.87	87.87	0.00	4
1.13	117.22	27.26	89.96	89.96	0.00	4
1.10	120.04	27.99	92.05	92.05	0.00	4
1.06	122.86	28.73	94.13	94.13	0.00	4
1.03	125.66	29.47	96.19	96.19	0.00	4
1.00	128.46	30.20	98.25	98.25	0.00	4
0.96	131.25	30.94	100.31	100.31	0.00	4
0.93	134.03	31.68	102.35	102.35	0.00	4
0.90	136.80	32.41	104.39	104.39	0.00	4
0.87	139.56	33.15	106.41	106.41	0.00	4
0.83	142.32	33.89	108.43	108.43	0.00	4
0.80	145.07	34.62	110.45	110.45	0.00	4
0.77	147.81	35.36	112.45	112.45	0.00	4
0.77	147.81	35.36	112.45	112.45	0.00	4
0.74	150.55	35.09	115.46	114.45	1.01	4
0.71	153.29	34.83	118.46	116.46	2.00	4
0.67	156.03	34.61	121.43	118.46	2.96	4
0.64	158.78	34.42	124.36	120.47	3.88	4
0.61	161.53	34.29	127.24	122.48	4.76	4
0.58	164.28	34.20	130.07	124.50	5.58	4

output

0.54	167.03	34.18	132.85	126.51	6.34	4
0.51	169.78	34.20	135.57	128.52	7.05	4
0.48	172.53	34.28	138.25	130.54	7.71	4
0.45	175.27	34.40	140.87	132.55	8.33	4
0.42	178.02	34.56	143.46	134.56	8.90	4
0.38	180.76	34.75	146.01	136.56	9.45	4
0.38	180.76	34.75	146.01	136.56	9.45	4
0.35	183.51	34.94	148.57	138.57	10.00	4
0.32	186.25	35.15	151.10	140.57	10.52	4
0.29	188.99	35.37	153.61	142.58	11.04	4
0.25	191.72	35.61	156.11	144.57	11.54	4
0.22	194.45	35.84	158.61	146.57	12.04	4
0.19	197.18	36.09	161.10	148.56	12.53	4
0.16	199.91	36.33	163.58	150.56	13.03	4
0.13	202.64	36.57	166.06	152.54	13.52	4
0.10	205.36	36.82	168.54	154.53	14.01	4
0.06	208.08	37.06	171.02	156.51	14.51	4
0.03	210.80	37.30	173.50	158.49	15.01	4
0.00	213.51	37.53	175.98	160.47	15.51	4

Time = 1825. Degree of Consolidation = 99.%

Total Settlement = 3.428

Settlement at End of Primary Consolidation = 3.455

Settlement caused by Primary Consolidation at time 1825. = 3.425

Settlement caused by Secondary Compression at time 1825. = 0.003

Settlement Due to Desiccation = 0.000

Surface Elevation = 1.06

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
10.50	10.49	4.83	0.91	0.91	0.91	3
10.10	10.09	4.62	0.91	0.91	0.91	3
9.70	9.69	4.41	0.91	0.91	0.91	3
9.30	9.29	4.20	0.91	0.91	0.91	3

8.90	8.89	3.99	0.91	0.91	0.90	3
8.50	8.49	3.78	0.91	0.90	0.90	3
8.10	8.09	3.57	0.90	0.90	0.90	3
7.70	7.69	3.36	0.90	0.90	0.90	3
7.30	7.29	3.15	0.90	0.90	0.90	3
6.90	6.89	2.94	0.90	0.90	0.90	3
6.50	6.49	2.73	0.90	0.90	0.90	3
6.50	6.49	2.73	1.40	1.40	1.39	2
5.85	5.84	2.46	1.39	1.39	1.39	2
5.19	5.19	2.18	1.39	1.39	1.38	2
4.54	4.54	1.91	1.39	1.38	1.38	2
3.89	3.89	1.64	1.38	1.38	1.38	2
3.24	3.24	1.36	1.38	1.38	1.38	2
2.59	2.59	1.09	1.38	1.38	1.38	2
1.94	1.94	0.82	1.38	1.37	1.37	2
1.29	1.29	0.55	1.38	1.37	1.37	2
0.65	0.65	0.27	1.37	1.37	1.37	2
0.00	0.00	0.00	1.37	1.36	1.36	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
10.49	212.85	40.08	172.77	159.81	12.96	3
10.09	259.85	58.16	201.69	184.80	16.89	3
9.69	306.83	76.10	230.73	209.79	20.95	3
9.29	353.81	93.95	259.86	234.76	25.11	3
8.89	400.78	111.73	289.05	259.72	29.32	3
8.49	447.74	129.51	318.22	284.67	33.55	3
8.09	494.69	147.36	347.33	309.62	37.71	3
7.69	541.63	165.37	376.26	334.55	41.70	3
7.29	588.56	183.68	404.88	359.48	45.40	3
6.89	635.48	202.52	432.95	384.40	48.56	3
6.49	682.39	222.30	460.09	409.30	50.79	3
6.49	682.39	222.30	460.09	409.30	50.79	2
5.84	751.21	248.14	503.08	450.04	53.04	2
5.19	819.98	288.06	531.92	490.71	41.21	2
4.54	888.69	329.70	558.99	531.33	27.66	2
3.89	957.36	369.43	587.93	571.91	16.02	2
3.24	1025.98	405.04	620.94	612.44	8.50	2
2.59	1094.56	430.62	663.94	652.93	11.01	2
1.94	1163.10	457.83	705.26	693.37	11.89	2
1.29	1231.59	487.61	743.97	733.77	10.20	2
0.65	1300.02	520.10	779.92	774.11	5.81	2
0.00	1368.40	553.61	814.79	814.40	0.39	2

Time = 2555. Degree of Consolidation = 55.%

Total Settlement = 0.009

Settlement at End of Primary Consolidation = 0.017

Settlement caused by Primary Consolidation at time 2555. = 0.009

Settlement caused by Secondary Compression at time 2555. = 0.000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
6.00	2.56	0.50	11.00	11.00	11.00	4
5.99	2.55	0.50	11.00	9.23	9.23	4
5.98	2.54	0.50	11.00	8.74	8.74	4
5.97	2.54	0.50	11.00	8.45	8.45	4
5.96	2.53	0.50	11.00	8.15	8.15	4
5.95	2.52	0.50	11.00	7.89	7.89	4
5.94	2.51	0.50	11.00	7.67	7.67	4
5.93	2.51	0.49	11.00	7.45	7.45	4
5.92	2.50	0.49	11.00	7.23	7.23	4
5.91	2.49	0.49	11.00	7.01	7.01	4
5.90	2.49	0.49	11.00	6.93	6.93	4
5.89	2.48	0.49	11.00	6.85	6.86	4
5.88	2.47	0.49	11.00	6.78	6.78	4
5.87	2.47	0.49	11.00	6.71	6.71	4
5.86	2.46	0.49	11.00	6.63	6.64	4
5.85	2.45	0.49	11.00	6.56	6.56	4
5.84	2.45	0.49	11.00	6.49	6.49	4
5.83	2.44	0.49	11.00	6.41	6.41	4
5.82	2.43	0.49	11.00	6.34	6.34	4
5.81	2.43	0.48	11.00	6.27	6.27	4
5.80	2.42	0.48	11.00	6.19	6.19	4
5.79	2.42	0.48	11.00	6.12	6.12	4
5.78	2.41	0.48	11.00	6.04	6.05	4
5.77	2.40	0.48	11.00	5.98	5.98	4
5.76	2.40	0.48	11.00	5.94	5.94	4
5.75	2.39	0.48	11.00	5.89	5.89	4
5.74	2.39	0.48	11.00	5.85	5.85	4
5.73	2.38	0.48	11.00	5.81	5.81	4
5.72	2.38	0.48	11.00	5.76	5.76	4
5.71	2.37	0.48	11.00	5.72	5.72	4

			output			
5.70	2.37	0.48	11.00	5.67	5.67	4
5.69	2.36	0.47	11.00	5.63	5.63	4
5.68	2.35	0.47	11.00	5.58	5.59	4
5.67	2.35	0.47	11.00	5.54	5.54	4
5.66	2.34	0.47	11.00	5.50	5.50	4
5.65	2.34	0.47	11.00	5.45	5.45	4
5.64	2.33	0.47	11.00	5.41	5.41	4
5.63	2.33	0.47	11.00	5.36	5.36	4
5.62	2.32	0.47	11.00	5.32	5.32	4
5.61	2.32	0.47	11.00	5.27	5.28	4
5.60	2.31	0.47	11.00	5.23	5.23	4
5.59	2.31	0.47	11.00	5.19	5.19	4
5.58	2.30	0.47	11.00	5.14	5.14	4
5.57	2.30	0.46	11.00	5.10	5.10	4
5.56	2.29	0.46	11.00	5.05	5.06	4
5.55	2.29	0.46	11.00	5.01	5.01	4
5.54	2.28	0.46	11.00	5.00	5.00	4
5.53	2.28	0.46	11.00	4.99	4.99	4
5.52	2.27	0.46	11.00	4.98	4.98	4
5.51	2.27	0.46	11.00	4.98	4.98	4
5.50	2.26	0.46	11.00	4.97	4.97	4
5.49	2.26	0.46	11.00	4.97	4.97	4
5.48	2.25	0.46	11.00	4.96	4.96	4
5.47	2.25	0.46	11.00	4.96	4.96	4
5.46	2.24	0.46	11.00	4.95	4.95	4
5.45	2.24	0.45	11.00	4.95	4.95	4
5.44	2.23	0.45	11.00	4.94	4.94	4
5.43	2.23	0.45	11.00	4.93	4.94	4
5.42	2.22	0.45	11.00	4.93	4.93	4
5.41	2.22	0.45	11.00	4.92	4.92	4
5.40	2.21	0.45	11.00	4.92	4.92	4
5.39	2.21	0.45	11.00	4.91	4.91	4
5.38	2.20	0.45	11.00	4.91	4.91	4
5.37	2.20	0.45	11.00	4.90	4.90	4
5.36	2.19	0.45	11.00	4.90	4.90	4
5.35	2.19	0.45	11.00	4.89	4.89	4
5.34	2.18	0.45	11.00	4.88	4.89	4
5.33	2.18	0.44	11.00	4.88	4.88	4
5.32	2.17	0.44	11.00	4.87	4.87	4
5.31	2.17	0.44	11.00	4.87	4.87	4
5.30	2.16	0.44	11.00	4.86	4.86	4
5.29	2.16	0.44	11.00	4.86	4.86	4
5.28	2.15	0.44	11.00	4.85	4.85	4
5.27	2.15	0.44	11.00	4.85	4.85	4
5.26	2.14	0.44	11.00	4.84	4.84	4
5.25	2.14	0.44	11.00	4.83	4.84	4
5.24	2.13	0.44	11.00	4.83	4.83	4
5.23	2.13	0.44	11.00	4.82	4.82	4

			output			
5.22	2.12	0.43	11.00	4.82	4.82	4
5.21	2.12	0.43	11.00	4.81	4.81	4
5.20	2.11	0.43	11.00	4.81	4.81	4
5.19	2.11	0.43	11.00	4.80	4.80	4
5.18	2.10	0.43	11.00	4.80	4.80	4
5.17	2.10	0.43	11.00	4.79	4.79	4
5.16	2.09	0.43	11.00	4.79	4.79	4
5.15	2.09	0.43	11.00	4.78	4.78	4
5.14	2.08	0.43	11.00	4.77	4.77	4
5.13	2.08	0.43	11.00	4.77	4.77	4
5.12	2.08	0.43	11.00	4.76	4.76	4
5.11	2.07	0.43	11.00	4.76	4.76	4
5.10	2.07	0.42	11.00	4.75	4.75	4
5.09	2.06	0.42	11.00	4.75	4.75	4
5.08	2.06	0.42	11.00	4.74	4.74	4
5.07	2.05	0.42	11.00	4.74	4.74	4
5.06	2.05	0.42	11.00	4.73	4.73	4
5.05	2.04	0.42	11.00	4.72	4.73	4
5.04	2.04	0.42	11.00	4.72	4.72	4
5.03	2.03	0.42	11.00	4.71	4.71	4
5.02	2.03	0.42	11.00	4.71	4.71	4
5.01	2.02	0.42	11.00	4.70	4.70	4
5.00	2.02	0.42	11.00	4.70	4.70	4
5.00	2.02	0.42	11.00	4.70	4.70	4
4.92	1.98	0.41	11.00	4.65	4.65	4
4.83	1.94	0.40	11.00	4.60	4.61	4
4.75	1.90	0.40	11.00	4.56	4.56	4
4.67	1.86	0.39	11.00	4.51	4.51	4
4.58	1.82	0.38	11.00	4.47	4.47	4
4.50	1.79	0.37	11.00	4.42	4.42	4
4.42	1.75	0.37	11.00	4.37	4.38	4
4.33	1.71	0.36	11.00	4.33	4.33	4
4.25	1.67	0.35	11.00	4.28	4.28	4
4.17	1.64	0.35	11.00	4.24	4.24	4
4.08	1.60	0.34	11.00	4.19	4.19	4
4.00	1.57	0.33	11.00	4.14	4.14	4
4.00	1.57	0.33	11.00	4.14	4.14	4
3.92	1.53	0.33	11.00	4.10	4.10	4
3.83	1.50	0.32	11.00	4.05	4.05	4
3.75	1.46	0.31	11.00	4.01	4.01	4
3.67	1.43	0.31	11.00	3.98	3.98	4
3.58	1.39	0.30	11.00	3.97	3.97	4
3.50	1.36	0.29	11.00	3.95	3.95	4
3.42	1.32	0.28	11.00	3.93	3.93	4
3.33	1.29	0.28	11.00	3.91	3.91	4
3.25	1.25	0.27	11.00	3.89	3.89	4
3.17	1.22	0.26	11.00	3.87	3.87	4
3.08	1.19	0.26	11.00	3.85	3.86	4

3.00	1.15	0.25	11.00	3.84	3.84	4
3.00	1.15	0.25	11.00	3.84	3.84	4
2.92	1.12	0.24	11.00	3.82	3.82	4
2.83	1.09	0.24	11.00	3.80	3.80	4
2.75	1.05	0.23	11.00	3.78	3.78	4
2.67	1.02	0.22	11.00	3.76	3.76	4
2.58	0.99	0.22	11.00	3.74	3.74	4
2.50	0.95	0.21	11.00	3.73	3.73	4
2.42	0.92	0.20	11.00	3.71	3.71	4
2.33	0.89	0.19	11.00	3.69	3.69	4
2.25	0.86	0.19	11.00	3.67	3.67	4
2.17	0.82	0.18	11.00	3.65	3.65	4
2.08	0.79	0.17	11.00	3.63	3.63	4
2.00	0.76	0.17	11.00	3.62	3.62	4
2.00	0.76	0.17	11.00	3.62	3.62	4
1.92	0.73	0.16	11.00	3.61	3.60	4
1.83	0.70	0.15	11.00	3.60	3.58	4
1.75	0.66	0.15	11.00	3.60	3.56	4
1.67	0.63	0.14	11.00	3.59	3.54	4
1.58	0.60	0.13	11.00	3.59	3.52	4
1.50	0.57	0.13	11.00	3.58	3.51	4
1.42	0.54	0.12	11.00	3.58	3.49	4
1.33	0.50	0.11	11.00	3.57	3.48	4
1.25	0.47	0.10	11.00	3.57	3.48	4
1.17	0.44	0.10	11.00	3.56	3.47	4
1.08	0.41	0.09	11.00	3.56	3.46	4
1.00	0.38	0.08	11.00	3.55	3.45	4
1.00	0.38	0.08	11.00	3.55	3.45	4
0.92	0.35	0.08	11.00	3.55	3.44	4
0.83	0.31	0.07	11.00	3.54	3.43	4
0.75	0.28	0.06	11.00	3.54	3.42	4
0.67	0.25	0.06	11.00	3.53	3.41	4
0.58	0.22	0.05	11.00	3.53	3.40	4
0.50	0.19	0.04	11.00	3.52	3.39	4
0.42	0.16	0.03	11.00	3.52	3.38	4
0.33	0.13	0.03	11.00	3.52	3.37	4
0.25	0.09	0.02	11.00	3.51	3.36	4
0.17	0.06	0.01	11.00	3.51	3.36	4
0.08	0.03	0.01	11.00	3.50	3.35	4
0.00	0.00	0.00	11.00	3.50	3.34	4

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
2.56	0.00	0.00	0.00	0.00	0.00	4
2.55	0.66	0.09	0.57	0.57	0.00	4
2.54	1.26	0.18	1.09	1.09	0.00	4

output

2.54	1.85	0.27	1.59	1.59	0.00	4
2.53	2.42	0.35	2.07	2.07	0.00	4
2.52	2.98	0.44	2.54	2.54	0.00	4
2.51	3.52	0.53	2.99	2.99	0.00	4
2.51	4.06	0.62	3.44	3.44	0.00	4
2.50	4.58	0.71	3.87	3.87	0.00	4
2.49	5.09	0.80	4.29	4.29	0.00	4
2.49	5.59	0.88	4.71	4.71	0.00	4
2.48	6.09	0.97	5.12	5.12	0.00	4
2.47	6.59	1.06	5.53	5.53	0.00	4
2.47	7.08	1.15	5.93	5.93	0.00	4
2.46	7.57	1.24	6.33	6.33	0.00	4
2.45	8.05	1.33	6.72	6.72	0.00	4
2.45	8.53	1.41	7.11	7.11	0.00	4
2.44	9.00	1.50	7.50	7.50	0.00	4
2.43	9.48	1.59	7.88	7.88	0.00	4
2.43	9.94	1.68	8.26	8.26	0.00	4
2.42	10.41	1.77	8.64	8.64	0.00	4
2.42	10.87	1.86	9.01	9.01	0.00	4
2.41	11.33	1.94	9.38	9.38	0.00	4
2.40	11.78	2.03	9.75	9.75	0.00	4
2.40	12.23	2.12	10.11	10.11	0.00	4
2.39	12.68	2.21	10.47	10.47	0.00	4
2.39	13.12	2.30	10.82	10.82	0.00	4
2.38	13.57	2.39	11.18	11.18	0.00	4
2.38	14.01	2.48	11.53	11.53	0.00	4
2.37	14.45	2.56	11.88	11.88	0.00	4
2.37	14.88	2.65	12.23	12.23	0.00	4
2.36	15.32	2.74	12.58	12.58	0.00	4
2.35	15.75	2.83	12.92	12.92	0.00	4
2.35	16.18	2.92	13.26	13.26	0.00	4
2.34	16.61	3.01	13.60	13.60	0.00	4
2.34	17.03	3.09	13.94	13.94	0.00	4
2.33	17.45	3.18	14.27	14.27	0.00	4
2.33	17.87	3.27	14.60	14.60	0.00	4
2.32	18.29	3.36	14.93	14.93	0.00	4
2.32	18.71	3.45	15.26	15.26	0.00	4
2.31	19.12	3.54	15.59	15.59	0.00	4
2.31	19.53	3.62	15.91	15.91	0.00	4
2.30	19.94	3.71	16.23	16.23	0.00	4
2.30	20.35	3.80	16.55	16.55	0.00	4
2.29	20.75	3.89	16.86	16.86	0.00	4
2.29	21.15	3.98	17.18	17.18	0.00	4
2.28	21.55	4.07	17.49	17.49	0.00	4
2.28	21.95	4.15	17.80	17.80	0.00	4
2.27	22.35	4.24	18.11	18.11	0.00	4
2.27	22.75	4.33	18.42	18.42	0.00	4
2.26	23.15	4.42	18.73	18.73	0.00	4

			output			
2.26	23.55	4.51	19.04	19.04	0.00	4
2.25	23.95	4.60	19.35	19.35	0.00	4
2.25	24.35	4.69	19.66	19.66	0.00	4
2.24	24.75	4.77	19.97	19.97	0.00	4
2.24	25.14	4.86	20.28	20.28	0.00	4
2.23	25.54	4.95	20.59	20.59	0.00	4
2.23	25.94	5.04	20.90	20.90	0.00	4
2.22	26.34	5.13	21.21	21.21	0.00	4
2.22	26.73	5.22	21.52	21.52	0.00	4
2.21	27.13	5.30	21.82	21.82	0.00	4
2.21	27.52	5.39	22.13	22.13	0.00	4
2.20	27.92	5.48	22.44	22.44	0.00	4
2.20	28.32	5.57	22.75	22.75	0.00	4
2.19	28.71	5.66	23.05	23.05	0.00	4
2.19	29.11	5.75	23.36	23.36	0.00	4
2.18	29.50	5.83	23.67	23.67	0.00	4
2.18	29.89	5.92	23.97	23.97	0.00	4
2.17	30.29	6.01	24.28	24.28	0.00	4
2.17	30.68	6.10	24.58	24.58	0.00	4
2.16	31.08	6.19	24.89	24.89	0.00	4
2.16	31.47	6.28	25.19	25.19	0.00	4
2.15	31.86	6.36	25.50	25.50	0.00	4
2.15	32.25	6.45	25.80	25.80	0.00	4
2.14	32.65	6.54	26.10	26.10	0.00	4
2.14	33.04	6.63	26.41	26.41	0.00	4
2.13	33.43	6.72	26.71	26.71	0.00	4
2.13	33.82	6.81	27.01	27.01	0.00	4
2.12	34.21	6.90	27.32	27.32	0.00	4
2.12	34.60	6.98	27.62	27.62	0.00	4
2.11	34.99	7.07	27.92	27.92	0.00	4
2.11	35.38	7.16	28.22	28.22	0.00	4
2.10	35.77	7.25	28.52	28.52	0.00	4
2.10	36.16	7.34	28.83	28.83	0.00	4
2.09	36.55	7.43	29.13	29.13	0.00	4
2.09	36.94	7.51	29.43	29.43	0.00	4
2.08	37.33	7.60	29.73	29.73	0.00	4
2.08	37.72	7.69	30.03	30.03	0.00	4
2.08	38.11	7.78	30.33	30.33	0.00	4
2.07	38.50	7.87	30.63	30.63	0.00	4
2.07	38.88	7.96	30.93	30.93	0.00	4
2.06	39.27	8.04	31.23	31.23	0.00	4
2.06	39.66	8.13	31.52	31.52	0.00	4
2.05	40.04	8.22	31.82	31.82	0.00	4
2.05	40.43	8.31	32.12	32.12	0.00	4
2.04	40.82	8.40	32.42	32.42	0.00	4
2.04	41.20	8.49	32.72	32.72	0.00	4
2.03	41.59	8.57	33.01	33.01	0.00	4
2.03	41.97	8.66	33.31	33.31	0.00	4

output

2.02	42.36	8.75	33.61	33.61	0.00	4
2.02	42.74	8.84	33.90	33.90	0.00	4
2.02	42.74	8.84	33.90	33.90	0.00	4
1.98	45.94	9.58	36.36	36.36	0.00	4
1.94	49.11	10.31	38.80	38.80	0.00	4
1.90	52.27	11.05	41.22	41.22	0.00	4
1.86	55.41	11.79	43.62	43.62	0.00	4
1.82	58.52	12.52	46.00	46.00	0.00	4
1.79	61.62	13.26	48.36	48.36	0.00	4
1.75	64.69	14.00	50.70	50.70	0.00	4
1.71	67.75	14.73	53.01	53.01	0.00	4
1.67	70.78	15.47	55.31	55.31	0.00	4
1.64	73.80	16.21	57.59	57.59	0.00	4
1.60	76.79	16.94	59.85	59.85	0.00	4
1.57	79.77	17.68	62.09	62.09	0.00	4
1.57	79.77	17.68	62.09	62.09	0.00	4
1.53	82.73	18.42	64.31	64.31	0.00	4
1.50	85.66	19.15	66.51	66.51	0.00	4
1.46	88.58	19.89	68.69	68.69	0.00	4
1.43	91.48	20.63	70.85	70.85	0.00	4
1.39	94.37	21.36	73.01	73.01	0.00	4
1.36	97.25	22.10	75.15	75.15	0.00	4
1.32	100.13	22.84	77.29	77.29	0.00	4
1.29	103.00	23.57	79.43	79.43	0.00	4
1.25	105.86	24.31	81.55	81.55	0.00	4
1.22	108.71	25.05	83.67	83.67	0.00	4
1.19	111.56	25.78	85.77	85.77	0.00	4
1.15	114.39	26.52	87.87	87.87	0.00	4
1.15	114.39	26.52	87.87	87.87	0.00	4
1.12	117.22	27.26	89.96	89.96	0.00	4
1.09	120.04	27.99	92.05	92.05	0.00	4
1.05	122.85	28.73	94.12	94.12	0.00	4
1.02	125.66	29.47	96.19	96.19	0.00	4
0.99	128.46	30.20	98.25	98.25	0.00	4
0.95	131.24	30.94	100.30	100.30	0.00	4
0.92	134.02	31.68	102.35	102.35	0.00	4
0.89	136.80	32.41	104.38	104.38	0.00	4
0.86	139.56	33.15	106.41	106.41	0.00	4
0.82	142.32	33.89	108.43	108.43	0.00	4
0.79	145.07	34.62	110.44	110.44	0.00	4
0.76	147.81	35.36	112.45	112.45	0.00	4
0.76	147.81	35.36	112.45	112.45	0.00	4
0.73	150.54	35.59	114.95	114.45	0.51	4
0.70	153.28	35.82	117.46	116.44	1.02	4
0.66	156.01	36.04	119.97	118.44	1.53	4
0.63	158.74	36.26	122.48	120.43	2.05	4
0.60	161.46	36.48	124.99	122.42	2.57	4
0.57	164.19	36.69	127.50	124.41	3.09	4

0.54	166.91	36.90	130.01	126.39	3.62	4
0.50	169.63	37.10	132.52	128.37	4.15	4
0.47	172.34	37.30	135.04	130.35	4.69	4
0.44	175.06	37.50	137.55	132.33	5.22	4
0.41	177.77	37.70	140.07	134.31	5.76	4
0.38	180.48	37.89	142.59	136.28	6.31	4
0.38	180.48	37.89	142.59	136.28	6.31	4
0.35	183.19	38.09	145.10	138.25	6.85	4
0.31	185.90	38.28	147.62	140.22	7.40	4
0.28	188.60	38.46	150.14	142.19	7.95	4
0.25	191.30	38.65	152.65	144.16	8.50	4
0.22	194.00	38.83	155.17	146.12	9.05	4
0.19	196.70	39.01	157.69	148.08	9.61	4
0.16	199.40	39.19	160.21	150.04	10.17	4
0.13	202.09	39.36	162.73	152.00	10.73	4
0.09	204.79	39.54	165.25	153.96	11.29	4
0.06	207.48	39.71	167.77	155.91	11.86	4
0.03	210.16	39.87	170.29	157.86	12.43	4
0.00	212.85	40.08	172.77	159.81	12.96	4

Time = 2555. Degree of Consolidation = 99.%

Total Settlement = 3.439

Settlement at End of Primary Consolidation = 3.455

Settlement caused by Primary Consolidation at time 2555. = 3.432

Settlement caused by Secondary Compression at time 2555. = 0.006

Settlement Due to Desiccation = 0.000

Surface Elevation = 1.05

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
10.50	10.49	4.83	0.91	0.91	0.91	3
10.10	10.09	4.62	0.91	0.91	0.91	3
9.70	9.69	4.41	0.91	0.91	0.91	3
9.30	9.29	4.20	0.91	0.91	0.91	3

8.90	8.89	3.99	0.91	0.91	0.90	3
8.50	8.49	3.78	0.91	0.90	0.90	3
8.10	8.09	3.57	0.90	0.90	0.90	3
7.70	7.69	3.36	0.90	0.90	0.90	3
7.30	7.29	3.15	0.90	0.90	0.90	3
6.90	6.89	2.94	0.90	0.90	0.90	3
6.50	6.49	2.73	0.90	0.90	0.90	3
6.50	6.49	2.73	1.40	1.40	1.39	2
5.85	5.84	2.46	1.39	1.39	1.39	2
5.19	5.19	2.18	1.39	1.39	1.38	2
4.54	4.54	1.91	1.39	1.38	1.38	2
3.89	3.89	1.64	1.38	1.38	1.38	2
3.24	3.24	1.36	1.38	1.38	1.38	2
2.59	2.59	1.09	1.38	1.38	1.38	2
1.94	1.94	0.82	1.38	1.37	1.37	2
1.29	1.29	0.55	1.38	1.37	1.37	2
0.65	0.65	0.27	1.37	1.37	1.37	2
0.00	0.00	0.00	1.37	1.36	1.36	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
10.49	212.85	40.08	172.77	159.81	12.96	3
10.09	259.85	58.16	201.69	184.80	16.89	3
9.69	306.83	76.10	230.73	209.79	20.95	3
9.29	353.81	93.95	259.86	234.76	25.11	3
8.89	400.78	111.73	289.05	259.72	29.32	3
8.49	447.74	129.51	318.22	284.67	33.55	3
8.09	494.69	147.36	347.33	309.62	37.71	3
7.69	541.63	165.37	376.26	334.55	41.70	3
7.29	588.56	183.68	404.88	359.48	45.40	3
6.89	635.48	202.52	432.95	384.40	48.56	3
6.49	682.39	222.30	460.09	409.30	50.79	3
6.49	682.39	222.30	460.09	409.30	50.79	2
5.84	751.21	248.14	503.08	450.04	53.04	2
5.19	819.98	288.06	531.92	490.71	41.21	2
4.54	888.69	329.70	558.99	531.33	27.66	2
3.89	957.36	369.43	587.93	571.91	16.02	2
3.24	1025.98	405.04	620.94	612.44	8.50	2
2.59	1094.56	430.62	663.94	652.93	11.01	2
1.94	1163.10	457.83	705.26	693.37	11.89	2
1.29	1231.59	487.61	743.97	733.77	10.20	2
0.65	1300.02	520.10	779.92	774.11	5.81	2
0.00	1368.40	553.61	814.79	814.40	0.39	2

Time = 3000. Degree of Consolidation = 55.%

Total Settlement = 0.009

Settlement at End of Primary Consolidation = 0.017

Settlement caused by Primary Consolidation at time 3000. = 0.009

Settlement caused by Secondary Compression at time 3000. = 0.000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
6.00	2.56	0.50	11.00	11.00	11.00	4
5.99	2.55	0.50	11.00	9.23	9.23	4
5.98	2.54	0.50	11.00	8.74	8.74	4
5.97	2.54	0.50	11.00	8.45	8.45	4
5.96	2.53	0.50	11.00	8.15	8.15	4
5.95	2.52	0.50	11.00	7.89	7.89	4
5.94	2.51	0.50	11.00	7.67	7.67	4
5.93	2.51	0.49	11.00	7.45	7.45	4
5.92	2.50	0.49	11.00	7.23	7.23	4
5.91	2.49	0.49	11.00	7.01	7.01	4
5.90	2.49	0.49	11.00	6.93	6.93	4
5.89	2.48	0.49	11.00	6.85	6.86	4
5.88	2.47	0.49	11.00	6.78	6.78	4
5.87	2.47	0.49	11.00	6.71	6.71	4
5.86	2.46	0.49	11.00	6.63	6.64	4
5.85	2.45	0.49	11.00	6.56	6.56	4
5.84	2.45	0.49	11.00	6.49	6.49	4
5.83	2.44	0.49	11.00	6.41	6.41	4
5.82	2.43	0.49	11.00	6.34	6.34	4
5.81	2.43	0.48	11.00	6.27	6.27	4
5.80	2.42	0.48	11.00	6.19	6.19	4
5.79	2.42	0.48	11.00	6.12	6.12	4
5.78	2.41	0.48	11.00	6.04	6.05	4
5.77	2.40	0.48	11.00	5.98	5.98	4
5.76	2.40	0.48	11.00	5.94	5.94	4
5.75	2.39	0.48	11.00	5.89	5.89	4
5.74	2.39	0.48	11.00	5.85	5.85	4
5.73	2.38	0.48	11.00	5.81	5.81	4
5.72	2.38	0.48	11.00	5.76	5.76	4
5.71	2.37	0.48	11.00	5.72	5.72	4

			output			
5.70	2.37	0.48	11.00	5.67	5.67	4
5.69	2.36	0.47	11.00	5.63	5.63	4
5.68	2.35	0.47	11.00	5.58	5.59	4
5.67	2.35	0.47	11.00	5.54	5.54	4
5.66	2.34	0.47	11.00	5.50	5.50	4
5.65	2.34	0.47	11.00	5.45	5.45	4
5.64	2.33	0.47	11.00	5.41	5.41	4
5.63	2.33	0.47	11.00	5.36	5.36	4
5.62	2.32	0.47	11.00	5.32	5.32	4
5.61	2.32	0.47	11.00	5.27	5.28	4
5.60	2.31	0.47	11.00	5.23	5.23	4
5.59	2.31	0.47	11.00	5.19	5.19	4
5.58	2.30	0.47	11.00	5.14	5.14	4
5.57	2.30	0.46	11.00	5.10	5.10	4
5.56	2.29	0.46	11.00	5.05	5.06	4
5.55	2.29	0.46	11.00	5.01	5.01	4
5.54	2.28	0.46	11.00	5.00	5.00	4
5.53	2.28	0.46	11.00	4.99	4.99	4
5.52	2.27	0.46	11.00	4.98	4.98	4
5.51	2.27	0.46	11.00	4.98	4.98	4
5.50	2.26	0.46	11.00	4.97	4.97	4
5.49	2.26	0.46	11.00	4.97	4.97	4
5.48	2.25	0.46	11.00	4.96	4.96	4
5.47	2.25	0.46	11.00	4.96	4.96	4
5.46	2.24	0.46	11.00	4.95	4.95	4
5.45	2.24	0.45	11.00	4.95	4.95	4
5.44	2.23	0.45	11.00	4.94	4.94	4
5.43	2.23	0.45	11.00	4.93	4.94	4
5.42	2.22	0.45	11.00	4.93	4.93	4
5.41	2.22	0.45	11.00	4.92	4.92	4
5.40	2.21	0.45	11.00	4.92	4.92	4
5.39	2.21	0.45	11.00	4.91	4.91	4
5.38	2.20	0.45	11.00	4.91	4.91	4
5.37	2.20	0.45	11.00	4.90	4.90	4
5.36	2.19	0.45	11.00	4.90	4.90	4
5.35	2.19	0.45	11.00	4.89	4.89	4
5.34	2.18	0.45	11.00	4.88	4.89	4
5.33	2.18	0.44	11.00	4.88	4.88	4
5.32	2.17	0.44	11.00	4.87	4.87	4
5.31	2.17	0.44	11.00	4.87	4.87	4
5.30	2.16	0.44	11.00	4.86	4.86	4
5.29	2.16	0.44	11.00	4.86	4.86	4
5.28	2.15	0.44	11.00	4.85	4.85	4
5.27	2.15	0.44	11.00	4.85	4.85	4
5.26	2.14	0.44	11.00	4.84	4.84	4
5.25	2.14	0.44	11.00	4.83	4.84	4
5.24	2.13	0.44	11.00	4.83	4.83	4
5.23	2.13	0.44	11.00	4.82	4.82	4

			output			
5.22	2.12	0.43	11.00	4.82	4.82	4
5.21	2.12	0.43	11.00	4.81	4.81	4
5.20	2.11	0.43	11.00	4.81	4.81	4
5.19	2.11	0.43	11.00	4.80	4.80	4
5.18	2.10	0.43	11.00	4.80	4.80	4
5.17	2.10	0.43	11.00	4.79	4.79	4
5.16	2.09	0.43	11.00	4.79	4.79	4
5.15	2.09	0.43	11.00	4.78	4.78	4
5.14	2.08	0.43	11.00	4.77	4.77	4
5.13	2.08	0.43	11.00	4.77	4.77	4
5.12	2.08	0.43	11.00	4.76	4.76	4
5.11	2.07	0.43	11.00	4.76	4.76	4
5.10	2.07	0.42	11.00	4.75	4.75	4
5.09	2.06	0.42	11.00	4.75	4.75	4
5.08	2.06	0.42	11.00	4.74	4.74	4
5.07	2.05	0.42	11.00	4.74	4.74	4
5.06	2.05	0.42	11.00	4.73	4.73	4
5.05	2.04	0.42	11.00	4.72	4.73	4
5.04	2.04	0.42	11.00	4.72	4.72	4
5.03	2.03	0.42	11.00	4.71	4.71	4
5.02	2.03	0.42	11.00	4.71	4.71	4
5.01	2.02	0.42	11.00	4.70	4.70	4
5.00	2.02	0.42	11.00	4.70	4.70	4
5.00	2.02	0.42	11.00	4.70	4.70	4
4.92	1.98	0.41	11.00	4.65	4.65	4
4.83	1.94	0.40	11.00	4.60	4.61	4
4.75	1.90	0.40	11.00	4.56	4.56	4
4.67	1.86	0.39	11.00	4.51	4.51	4
4.58	1.82	0.38	11.00	4.47	4.47	4
4.50	1.79	0.37	11.00	4.42	4.42	4
4.42	1.75	0.37	11.00	4.37	4.38	4
4.33	1.71	0.36	11.00	4.33	4.33	4
4.25	1.67	0.35	11.00	4.28	4.28	4
4.17	1.64	0.35	11.00	4.24	4.24	4
4.08	1.60	0.34	11.00	4.19	4.19	4
4.00	1.57	0.33	11.00	4.14	4.14	4
4.00	1.57	0.33	11.00	4.14	4.14	4
3.92	1.53	0.33	11.00	4.10	4.10	4
3.83	1.50	0.32	11.00	4.05	4.05	4
3.75	1.46	0.31	11.00	4.01	4.01	4
3.67	1.43	0.31	11.00	3.98	3.98	4
3.58	1.39	0.30	11.00	3.97	3.97	4
3.50	1.36	0.29	11.00	3.95	3.95	4
3.42	1.32	0.28	11.00	3.93	3.93	4
3.33	1.29	0.28	11.00	3.91	3.91	4
3.25	1.25	0.27	11.00	3.89	3.89	4
3.17	1.22	0.26	11.00	3.87	3.87	4
3.08	1.19	0.26	11.00	3.85	3.86	4

3.00	1.15	0.25	11.00	3.84	3.84	4
3.00	1.15	0.25	11.00	3.84	3.84	4
2.92	1.12	0.24	11.00	3.82	3.82	4
2.83	1.09	0.24	11.00	3.80	3.80	4
2.75	1.05	0.23	11.00	3.78	3.78	4
2.67	1.02	0.22	11.00	3.76	3.76	4
2.58	0.99	0.22	11.00	3.74	3.74	4
2.50	0.95	0.21	11.00	3.73	3.73	4
2.42	0.92	0.20	11.00	3.71	3.71	4
2.33	0.89	0.19	11.00	3.69	3.69	4
2.25	0.86	0.19	11.00	3.67	3.67	4
2.17	0.82	0.18	11.00	3.65	3.65	4
2.08	0.79	0.17	11.00	3.63	3.63	4
2.00	0.76	0.17	11.00	3.62	3.62	4
2.00	0.76	0.17	11.00	3.62	3.62	4
1.92	0.73	0.16	11.00	3.61	3.60	4
1.83	0.70	0.15	11.00	3.60	3.58	4
1.75	0.66	0.15	11.00	3.60	3.56	4
1.67	0.63	0.14	11.00	3.59	3.54	4
1.58	0.60	0.13	11.00	3.59	3.52	4
1.50	0.57	0.13	11.00	3.58	3.51	4
1.42	0.54	0.12	11.00	3.58	3.49	4
1.33	0.50	0.11	11.00	3.57	3.48	4
1.25	0.47	0.10	11.00	3.57	3.48	4
1.17	0.44	0.10	11.00	3.56	3.47	4
1.08	0.41	0.09	11.00	3.56	3.46	4
1.00	0.38	0.08	11.00	3.55	3.45	4
1.00	0.38	0.08	11.00	3.55	3.45	4
0.92	0.35	0.08	11.00	3.55	3.44	4
0.83	0.31	0.07	11.00	3.54	3.43	4
0.75	0.28	0.06	11.00	3.54	3.42	4
0.67	0.25	0.06	11.00	3.53	3.41	4
0.58	0.22	0.05	11.00	3.53	3.40	4
0.50	0.19	0.04	11.00	3.52	3.39	4
0.42	0.16	0.03	11.00	3.52	3.38	4
0.33	0.13	0.03	11.00	3.52	3.37	4
0.25	0.09	0.02	11.00	3.51	3.36	4
0.17	0.06	0.01	11.00	3.51	3.36	4
0.08	0.03	0.01	11.00	3.50	3.35	4
0.00	0.00	0.00	11.00	3.50	3.34	4

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
2.56	0.00	0.00	0.00	0.00	0.00	4
2.55	0.66	0.09	0.57	0.57	0.00	4
2.54	1.26	0.18	1.09	1.09	0.00	4

output

2.54	1.85	0.27	1.59	1.59	0.00	4
2.53	2.42	0.35	2.07	2.07	0.00	4
2.52	2.98	0.44	2.54	2.54	0.00	4
2.51	3.52	0.53	2.99	2.99	0.00	4
2.51	4.06	0.62	3.44	3.44	0.00	4
2.50	4.58	0.71	3.87	3.87	0.00	4
2.49	5.09	0.80	4.29	4.29	0.00	4
2.49	5.59	0.88	4.71	4.71	0.00	4
2.48	6.09	0.97	5.12	5.12	0.00	4
2.47	6.59	1.06	5.53	5.53	0.00	4
2.47	7.08	1.15	5.93	5.93	0.00	4
2.46	7.57	1.24	6.33	6.33	0.00	4
2.45	8.05	1.33	6.72	6.72	0.00	4
2.45	8.53	1.41	7.11	7.11	0.00	4
2.44	9.00	1.50	7.50	7.50	0.00	4
2.43	9.48	1.59	7.88	7.88	0.00	4
2.43	9.94	1.68	8.26	8.26	0.00	4
2.42	10.41	1.77	8.64	8.64	0.00	4
2.42	10.87	1.86	9.01	9.01	0.00	4
2.41	11.33	1.94	9.38	9.38	0.00	4
2.40	11.78	2.03	9.75	9.75	0.00	4
2.40	12.23	2.12	10.11	10.11	0.00	4
2.39	12.68	2.21	10.47	10.47	0.00	4
2.39	13.12	2.30	10.82	10.82	0.00	4
2.38	13.57	2.39	11.18	11.18	0.00	4
2.38	14.01	2.48	11.53	11.53	0.00	4
2.37	14.45	2.56	11.88	11.88	0.00	4
2.37	14.88	2.65	12.23	12.23	0.00	4
2.36	15.32	2.74	12.58	12.58	0.00	4
2.35	15.75	2.83	12.92	12.92	0.00	4
2.35	16.18	2.92	13.26	13.26	0.00	4
2.34	16.61	3.01	13.60	13.60	0.00	4
2.34	17.03	3.09	13.94	13.94	0.00	4
2.33	17.45	3.18	14.27	14.27	0.00	4
2.33	17.87	3.27	14.60	14.60	0.00	4
2.32	18.29	3.36	14.93	14.93	0.00	4
2.32	18.71	3.45	15.26	15.26	0.00	4
2.31	19.12	3.54	15.59	15.59	0.00	4
2.31	19.53	3.62	15.91	15.91	0.00	4
2.30	19.94	3.71	16.23	16.23	0.00	4
2.30	20.35	3.80	16.55	16.55	0.00	4
2.29	20.75	3.89	16.86	16.86	0.00	4
2.29	21.15	3.98	17.18	17.18	0.00	4
2.28	21.55	4.07	17.49	17.49	0.00	4
2.28	21.95	4.15	17.80	17.80	0.00	4
2.27	22.35	4.24	18.11	18.11	0.00	4
2.27	22.75	4.33	18.42	18.42	0.00	4
2.26	23.15	4.42	18.73	18.73	0.00	4

			output			
2.26	23.55	4.51	19.04	19.04	0.00	4
2.25	23.95	4.60	19.35	19.35	0.00	4
2.25	24.35	4.69	19.66	19.66	0.00	4
2.24	24.75	4.77	19.97	19.97	0.00	4
2.24	25.14	4.86	20.28	20.28	0.00	4
2.23	25.54	4.95	20.59	20.59	0.00	4
2.23	25.94	5.04	20.90	20.90	0.00	4
2.22	26.34	5.13	21.21	21.21	0.00	4
2.22	26.73	5.22	21.52	21.52	0.00	4
2.21	27.13	5.30	21.82	21.82	0.00	4
2.21	27.52	5.39	22.13	22.13	0.00	4
2.20	27.92	5.48	22.44	22.44	0.00	4
2.20	28.32	5.57	22.75	22.75	0.00	4
2.19	28.71	5.66	23.05	23.05	0.00	4
2.19	29.11	5.75	23.36	23.36	0.00	4
2.18	29.50	5.83	23.67	23.67	0.00	4
2.18	29.89	5.92	23.97	23.97	0.00	4
2.17	30.29	6.01	24.28	24.28	0.00	4
2.17	30.68	6.10	24.58	24.58	0.00	4
2.16	31.08	6.19	24.89	24.89	0.00	4
2.16	31.47	6.28	25.19	25.19	0.00	4
2.15	31.86	6.36	25.50	25.50	0.00	4
2.15	32.25	6.45	25.80	25.80	0.00	4
2.14	32.65	6.54	26.10	26.10	0.00	4
2.14	33.04	6.63	26.41	26.41	0.00	4
2.13	33.43	6.72	26.71	26.71	0.00	4
2.13	33.82	6.81	27.01	27.01	0.00	4
2.12	34.21	6.90	27.32	27.32	0.00	4
2.12	34.60	6.98	27.62	27.62	0.00	4
2.11	34.99	7.07	27.92	27.92	0.00	4
2.11	35.38	7.16	28.22	28.22	0.00	4
2.10	35.77	7.25	28.52	28.52	0.00	4
2.10	36.16	7.34	28.83	28.83	0.00	4
2.09	36.55	7.43	29.13	29.13	0.00	4
2.09	36.94	7.51	29.43	29.43	0.00	4
2.08	37.33	7.60	29.73	29.73	0.00	4
2.08	37.72	7.69	30.03	30.03	0.00	4
2.08	38.11	7.78	30.33	30.33	0.00	4
2.07	38.50	7.87	30.63	30.63	0.00	4
2.07	38.88	7.96	30.93	30.93	0.00	4
2.06	39.27	8.04	31.23	31.23	0.00	4
2.06	39.66	8.13	31.52	31.52	0.00	4
2.05	40.04	8.22	31.82	31.82	0.00	4
2.05	40.43	8.31	32.12	32.12	0.00	4
2.04	40.82	8.40	32.42	32.42	0.00	4
2.04	41.20	8.49	32.72	32.72	0.00	4
2.03	41.59	8.57	33.01	33.01	0.00	4
2.03	41.97	8.66	33.31	33.31	0.00	4

output

2.02	42.36	8.75	33.61	33.61	0.00	4
2.02	42.74	8.84	33.90	33.90	0.00	4
2.02	42.74	8.84	33.90	33.90	0.00	4
1.98	45.94	9.58	36.36	36.36	0.00	4
1.94	49.11	10.31	38.80	38.80	0.00	4
1.90	52.27	11.05	41.22	41.22	0.00	4
1.86	55.41	11.79	43.62	43.62	0.00	4
1.82	58.52	12.52	46.00	46.00	0.00	4
1.79	61.62	13.26	48.36	48.36	0.00	4
1.75	64.69	14.00	50.70	50.70	0.00	4
1.71	67.75	14.73	53.01	53.01	0.00	4
1.67	70.78	15.47	55.31	55.31	0.00	4
1.64	73.80	16.21	57.59	57.59	0.00	4
1.60	76.79	16.94	59.85	59.85	0.00	4
1.57	79.77	17.68	62.09	62.09	0.00	4
1.57	79.77	17.68	62.09	62.09	0.00	4
1.53	82.73	18.42	64.31	64.31	0.00	4
1.50	85.66	19.15	66.51	66.51	0.00	4
1.46	88.58	19.89	68.69	68.69	0.00	4
1.43	91.48	20.63	70.85	70.85	0.00	4
1.39	94.37	21.36	73.01	73.01	0.00	4
1.36	97.25	22.10	75.15	75.15	0.00	4
1.32	100.13	22.84	77.29	77.29	0.00	4
1.29	103.00	23.57	79.43	79.43	0.00	4
1.25	105.86	24.31	81.55	81.55	0.00	4
1.22	108.71	25.05	83.67	83.67	0.00	4
1.19	111.56	25.78	85.77	85.77	0.00	4
1.15	114.39	26.52	87.87	87.87	0.00	4
1.15	114.39	26.52	87.87	87.87	0.00	4
1.12	117.22	27.26	89.96	89.96	0.00	4
1.09	120.04	27.99	92.05	92.05	0.00	4
1.05	122.85	28.73	94.12	94.12	0.00	4
1.02	125.66	29.47	96.19	96.19	0.00	4
0.99	128.46	30.20	98.25	98.25	0.00	4
0.95	131.24	30.94	100.30	100.30	0.00	4
0.92	134.02	31.68	102.35	102.35	0.00	4
0.89	136.80	32.41	104.38	104.38	0.00	4
0.86	139.56	33.15	106.41	106.41	0.00	4
0.82	142.32	33.89	108.43	108.43	0.00	4
0.79	145.07	34.62	110.44	110.44	0.00	4
0.76	147.81	35.36	112.45	112.45	0.00	4
0.76	147.81	35.36	112.45	112.45	0.00	4
0.73	150.54	35.59	114.95	114.45	0.51	4
0.70	153.28	35.82	117.46	116.44	1.02	4
0.66	156.01	36.04	119.97	118.44	1.53	4
0.63	158.74	36.26	122.48	120.43	2.05	4
0.60	161.46	36.48	124.99	122.42	2.57	4
0.57	164.19	36.69	127.50	124.41	3.09	4

0.54	166.91	36.90	130.01	126.39	3.62	4
0.50	169.63	37.10	132.52	128.37	4.15	4
0.47	172.34	37.30	135.04	130.35	4.69	4
0.44	175.06	37.50	137.55	132.33	5.22	4
0.41	177.77	37.70	140.07	134.31	5.76	4
0.38	180.48	37.89	142.59	136.28	6.31	4
0.38	180.48	37.89	142.59	136.28	6.31	4
0.35	183.19	38.09	145.10	138.25	6.85	4
0.31	185.90	38.28	147.62	140.22	7.40	4
0.28	188.60	38.46	150.14	142.19	7.95	4
0.25	191.30	38.65	152.65	144.16	8.50	4
0.22	194.00	38.83	155.17	146.12	9.05	4
0.19	196.70	39.01	157.69	148.08	9.61	4
0.16	199.40	39.19	160.21	150.04	10.17	4
0.13	202.09	39.36	162.73	152.00	10.73	4
0.09	204.79	39.54	165.25	153.96	11.29	4
0.06	207.48	39.71	167.77	155.91	11.86	4
0.03	210.16	39.87	170.29	157.86	12.43	4
0.00	212.85	40.08	172.77	159.81	12.96	4

Time = 3000. Degree of Consolidation = 99.%

Total Settlement = 3.439

Settlement at End of Primary Consolidation = 3.455

Settlement caused by Primary Consolidation at time 3000. = 3.431

Settlement caused by Secondary Compression at time 3000. = 0.008

Settlement Due to Desiccation = 0.000

Surface Elevation = 1.05

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
10.50	10.49	4.83	0.91	0.91	0.91	3
10.10	10.09	4.62	0.91	0.91	0.91	3
9.70	9.69	4.41	0.91	0.91	0.91	3
9.30	9.29	4.20	0.91	0.91	0.91	3

output

8.90	8.89	3.99	0.91	0.91	0.90	3
8.50	8.49	3.78	0.91	0.90	0.90	3
8.10	8.09	3.57	0.90	0.90	0.90	3
7.70	7.69	3.36	0.90	0.90	0.90	3
7.30	7.29	3.15	0.90	0.90	0.90	3
6.90	6.89	2.94	0.90	0.90	0.90	3
6.50	6.49	2.73	0.90	0.90	0.90	3
6.50	6.49	2.73	1.40	1.40	1.39	2
5.85	5.84	2.46	1.39	1.39	1.39	2
5.19	5.19	2.18	1.39	1.39	1.38	2
4.54	4.54	1.91	1.39	1.38	1.38	2
3.89	3.89	1.64	1.38	1.38	1.38	2
3.24	3.24	1.36	1.38	1.38	1.38	2
2.59	2.59	1.09	1.38	1.38	1.38	2
1.94	1.94	0.82	1.38	1.37	1.37	2
1.29	1.29	0.55	1.38	1.37	1.37	2
0.65	0.65	0.27	1.37	1.37	1.37	2
0.00	0.00	0.00	1.37	1.36	1.36	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
10.49	212.85	40.08	172.77	159.81	12.96	3
10.09	259.85	58.16	201.69	184.80	16.89	3
9.69	306.83	76.10	230.73	209.79	20.95	3
9.29	353.81	93.95	259.86	234.76	25.11	3
8.89	400.78	111.73	289.05	259.72	29.32	3
8.49	447.74	129.51	318.22	284.67	33.55	3
8.09	494.69	147.36	347.33	309.62	37.71	3
7.69	541.63	165.37	376.26	334.55	41.70	3
7.29	588.56	183.68	404.88	359.48	45.40	3
6.89	635.48	202.52	432.95	384.40	48.56	3
6.49	682.39	222.30	460.09	409.30	50.79	3
6.49	682.39	222.30	460.09	409.30	50.79	2
5.84	751.21	248.14	503.08	450.04	53.04	2
5.19	819.98	288.06	531.92	490.71	41.21	2
4.54	888.69	329.70	558.99	531.33	27.66	2
3.89	957.36	369.43	587.93	571.91	16.02	2
3.24	1025.98	405.04	620.94	612.44	8.50	2
2.59	1094.56	430.62	663.94	652.93	11.01	2
1.94	1163.10	457.83	705.26	693.37	11.89	2
1.29	1231.59	487.61	743.97	733.77	10.20	2
0.65	1300.02	520.10	779.92	774.11	5.81	2
0.00	1368.40	553.61	814.79	814.40	0.39	2

Time = 3650. Degree of Consolidation = 55.%

Total Settlement = 0.009

Settlement at End of Primary Consolidation = 0.017

Settlement caused by Primary Consolidation at time 3650. = 0.009

Settlement caused by Secondary Compression at time 3650. = 0.000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
6.00	2.56	0.50	11.00	11.00	11.00	4
5.99	2.55	0.50	11.00	9.23	9.23	4
5.98	2.54	0.50	11.00	8.74	8.74	4
5.97	2.54	0.50	11.00	8.45	8.45	4
5.96	2.53	0.50	11.00	8.15	8.15	4
5.95	2.52	0.50	11.00	7.89	7.89	4
5.94	2.51	0.50	11.00	7.67	7.67	4
5.93	2.51	0.49	11.00	7.45	7.45	4
5.92	2.50	0.49	11.00	7.23	7.23	4
5.91	2.49	0.49	11.00	7.01	7.01	4
5.90	2.49	0.49	11.00	6.93	6.93	4
5.89	2.48	0.49	11.00	6.85	6.86	4
5.88	2.47	0.49	11.00	6.78	6.78	4
5.87	2.47	0.49	11.00	6.71	6.71	4
5.86	2.46	0.49	11.00	6.63	6.64	4
5.85	2.45	0.49	11.00	6.56	6.56	4
5.84	2.45	0.49	11.00	6.49	6.49	4
5.83	2.44	0.49	11.00	6.41	6.41	4
5.82	2.43	0.49	11.00	6.34	6.34	4
5.81	2.43	0.48	11.00	6.27	6.27	4
5.80	2.42	0.48	11.00	6.19	6.19	4
5.79	2.42	0.48	11.00	6.12	6.12	4
5.78	2.41	0.48	11.00	6.04	6.05	4
5.77	2.40	0.48	11.00	5.98	5.98	4
5.76	2.40	0.48	11.00	5.94	5.94	4
5.75	2.39	0.48	11.00	5.89	5.89	4
5.74	2.39	0.48	11.00	5.85	5.85	4
5.73	2.38	0.48	11.00	5.81	5.81	4
5.72	2.38	0.48	11.00	5.76	5.76	4
5.71	2.37	0.48	11.00	5.72	5.72	4

			output			
5.70	2.37	0.48	11.00	5.67	5.67	4
5.69	2.36	0.47	11.00	5.63	5.63	4
5.68	2.35	0.47	11.00	5.58	5.59	4
5.67	2.35	0.47	11.00	5.54	5.54	4
5.66	2.34	0.47	11.00	5.50	5.50	4
5.65	2.34	0.47	11.00	5.45	5.45	4
5.64	2.33	0.47	11.00	5.41	5.41	4
5.63	2.33	0.47	11.00	5.36	5.36	4
5.62	2.32	0.47	11.00	5.32	5.32	4
5.61	2.32	0.47	11.00	5.27	5.28	4
5.60	2.31	0.47	11.00	5.23	5.23	4
5.59	2.31	0.47	11.00	5.19	5.19	4
5.58	2.30	0.47	11.00	5.14	5.14	4
5.57	2.30	0.46	11.00	5.10	5.10	4
5.56	2.29	0.46	11.00	5.05	5.06	4
5.55	2.29	0.46	11.00	5.01	5.01	4
5.54	2.28	0.46	11.00	5.00	5.00	4
5.53	2.28	0.46	11.00	4.99	4.99	4
5.52	2.27	0.46	11.00	4.98	4.98	4
5.51	2.27	0.46	11.00	4.98	4.98	4
5.50	2.26	0.46	11.00	4.97	4.97	4
5.49	2.26	0.46	11.00	4.97	4.97	4
5.48	2.25	0.46	11.00	4.96	4.96	4
5.47	2.25	0.46	11.00	4.96	4.96	4
5.46	2.24	0.46	11.00	4.95	4.95	4
5.45	2.24	0.45	11.00	4.95	4.95	4
5.44	2.23	0.45	11.00	4.94	4.94	4
5.43	2.23	0.45	11.00	4.93	4.94	4
5.42	2.22	0.45	11.00	4.93	4.93	4
5.41	2.22	0.45	11.00	4.92	4.92	4
5.40	2.21	0.45	11.00	4.92	4.92	4
5.39	2.21	0.45	11.00	4.91	4.91	4
5.38	2.20	0.45	11.00	4.91	4.91	4
5.37	2.20	0.45	11.00	4.90	4.90	4
5.36	2.19	0.45	11.00	4.90	4.90	4
5.35	2.19	0.45	11.00	4.89	4.89	4
5.34	2.18	0.45	11.00	4.88	4.89	4
5.33	2.18	0.44	11.00	4.88	4.88	4
5.32	2.17	0.44	11.00	4.87	4.87	4
5.31	2.17	0.44	11.00	4.87	4.87	4
5.30	2.16	0.44	11.00	4.86	4.86	4
5.29	2.16	0.44	11.00	4.86	4.86	4
5.28	2.15	0.44	11.00	4.85	4.85	4
5.27	2.15	0.44	11.00	4.85	4.85	4
5.26	2.14	0.44	11.00	4.84	4.84	4
5.25	2.14	0.44	11.00	4.83	4.84	4
5.24	2.13	0.44	11.00	4.83	4.83	4
5.23	2.13	0.44	11.00	4.82	4.82	4

			output			
5.22	2.12	0.43	11.00	4.82	4.82	4
5.21	2.12	0.43	11.00	4.81	4.81	4
5.20	2.11	0.43	11.00	4.81	4.81	4
5.19	2.11	0.43	11.00	4.80	4.80	4
5.18	2.10	0.43	11.00	4.80	4.80	4
5.17	2.10	0.43	11.00	4.79	4.79	4
5.16	2.09	0.43	11.00	4.79	4.79	4
5.15	2.09	0.43	11.00	4.78	4.78	4
5.14	2.08	0.43	11.00	4.77	4.77	4
5.13	2.08	0.43	11.00	4.77	4.77	4
5.12	2.08	0.43	11.00	4.76	4.76	4
5.11	2.07	0.43	11.00	4.76	4.76	4
5.10	2.07	0.42	11.00	4.75	4.75	4
5.09	2.06	0.42	11.00	4.75	4.75	4
5.08	2.06	0.42	11.00	4.74	4.74	4
5.07	2.05	0.42	11.00	4.74	4.74	4
5.06	2.05	0.42	11.00	4.73	4.73	4
5.05	2.04	0.42	11.00	4.72	4.73	4
5.04	2.04	0.42	11.00	4.72	4.72	4
5.03	2.03	0.42	11.00	4.71	4.71	4
5.02	2.03	0.42	11.00	4.71	4.71	4
5.01	2.02	0.42	11.00	4.70	4.70	4
5.00	2.02	0.42	11.00	4.70	4.70	4
5.00	2.02	0.42	11.00	4.70	4.70	4
4.92	1.98	0.41	11.00	4.65	4.65	4
4.83	1.94	0.40	11.00	4.60	4.61	4
4.75	1.90	0.40	11.00	4.56	4.56	4
4.67	1.86	0.39	11.00	4.51	4.51	4
4.58	1.82	0.38	11.00	4.47	4.47	4
4.50	1.79	0.37	11.00	4.42	4.42	4
4.42	1.75	0.37	11.00	4.37	4.38	4
4.33	1.71	0.36	11.00	4.33	4.33	4
4.25	1.67	0.35	11.00	4.28	4.28	4
4.17	1.64	0.35	11.00	4.24	4.24	4
4.08	1.60	0.34	11.00	4.19	4.19	4
4.00	1.57	0.33	11.00	4.14	4.14	4
4.00	1.57	0.33	11.00	4.14	4.14	4
3.92	1.53	0.33	11.00	4.10	4.10	4
3.83	1.50	0.32	11.00	4.05	4.05	4
3.75	1.46	0.31	11.00	4.01	4.01	4
3.67	1.43	0.31	11.00	3.98	3.98	4
3.58	1.39	0.30	11.00	3.97	3.97	4
3.50	1.36	0.29	11.00	3.95	3.95	4
3.42	1.32	0.28	11.00	3.93	3.93	4
3.33	1.29	0.28	11.00	3.91	3.91	4
3.25	1.25	0.27	11.00	3.89	3.89	4
3.17	1.22	0.26	11.00	3.87	3.87	4
3.08	1.19	0.26	11.00	3.85	3.86	4

3.00	1.15	0.25	11.00	3.84	3.84	4
3.00	1.15	0.25	11.00	3.84	3.84	4
2.92	1.12	0.24	11.00	3.82	3.82	4
2.83	1.09	0.24	11.00	3.80	3.80	4
2.75	1.05	0.23	11.00	3.78	3.78	4
2.67	1.02	0.22	11.00	3.76	3.76	4
2.58	0.99	0.22	11.00	3.74	3.74	4
2.50	0.95	0.21	11.00	3.73	3.73	4
2.42	0.92	0.20	11.00	3.71	3.71	4
2.33	0.89	0.19	11.00	3.69	3.69	4
2.25	0.86	0.19	11.00	3.67	3.67	4
2.17	0.82	0.18	11.00	3.65	3.65	4
2.08	0.79	0.17	11.00	3.63	3.63	4
2.00	0.76	0.17	11.00	3.62	3.62	4
2.00	0.76	0.17	11.00	3.62	3.62	4
1.92	0.73	0.16	11.00	3.61	3.60	4
1.83	0.70	0.15	11.00	3.60	3.58	4
1.75	0.66	0.15	11.00	3.60	3.56	4
1.67	0.63	0.14	11.00	3.59	3.54	4
1.58	0.60	0.13	11.00	3.59	3.52	4
1.50	0.57	0.13	11.00	3.58	3.51	4
1.42	0.54	0.12	11.00	3.58	3.49	4
1.33	0.50	0.11	11.00	3.57	3.48	4
1.25	0.47	0.10	11.00	3.57	3.48	4
1.17	0.44	0.10	11.00	3.56	3.47	4
1.08	0.41	0.09	11.00	3.56	3.46	4
1.00	0.38	0.08	11.00	3.55	3.45	4
1.00	0.38	0.08	11.00	3.55	3.45	4
0.92	0.35	0.08	11.00	3.55	3.44	4
0.83	0.31	0.07	11.00	3.54	3.43	4
0.75	0.28	0.06	11.00	3.54	3.42	4
0.67	0.25	0.06	11.00	3.53	3.41	4
0.58	0.22	0.05	11.00	3.53	3.40	4
0.50	0.19	0.04	11.00	3.52	3.39	4
0.42	0.16	0.03	11.00	3.52	3.38	4
0.33	0.13	0.03	11.00	3.52	3.37	4
0.25	0.09	0.02	11.00	3.51	3.36	4
0.17	0.06	0.01	11.00	3.51	3.36	4
0.08	0.03	0.01	11.00	3.50	3.35	4
0.00	0.00	0.00	11.00	3.50	3.34	4

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
2.56	0.00	0.00	0.00	0.00	0.00	4
2.55	0.66	0.09	0.57	0.57	0.00	4
2.54	1.26	0.18	1.09	1.09	0.00	4

output

2.54	1.85	0.27	1.59	1.59	0.00	4
2.53	2.42	0.35	2.07	2.07	0.00	4
2.52	2.98	0.44	2.54	2.54	0.00	4
2.51	3.52	0.53	2.99	2.99	0.00	4
2.51	4.06	0.62	3.44	3.44	0.00	4
2.50	4.58	0.71	3.87	3.87	0.00	4
2.49	5.09	0.80	4.29	4.29	0.00	4
2.49	5.59	0.88	4.71	4.71	0.00	4
2.48	6.09	0.97	5.12	5.12	0.00	4
2.47	6.59	1.06	5.53	5.53	0.00	4
2.47	7.08	1.15	5.93	5.93	0.00	4
2.46	7.57	1.24	6.33	6.33	0.00	4
2.45	8.05	1.33	6.72	6.72	0.00	4
2.45	8.53	1.41	7.11	7.11	0.00	4
2.44	9.00	1.50	7.50	7.50	0.00	4
2.43	9.48	1.59	7.88	7.88	0.00	4
2.43	9.94	1.68	8.26	8.26	0.00	4
2.42	10.41	1.77	8.64	8.64	0.00	4
2.42	10.87	1.86	9.01	9.01	0.00	4
2.41	11.33	1.94	9.38	9.38	0.00	4
2.40	11.78	2.03	9.75	9.75	0.00	4
2.40	12.23	2.12	10.11	10.11	0.00	4
2.39	12.68	2.21	10.47	10.47	0.00	4
2.39	13.12	2.30	10.82	10.82	0.00	4
2.38	13.57	2.39	11.18	11.18	0.00	4
2.38	14.01	2.48	11.53	11.53	0.00	4
2.37	14.45	2.56	11.88	11.88	0.00	4
2.37	14.88	2.65	12.23	12.23	0.00	4
2.36	15.32	2.74	12.58	12.58	0.00	4
2.35	15.75	2.83	12.92	12.92	0.00	4
2.35	16.18	2.92	13.26	13.26	0.00	4
2.34	16.61	3.01	13.60	13.60	0.00	4
2.34	17.03	3.09	13.94	13.94	0.00	4
2.33	17.45	3.18	14.27	14.27	0.00	4
2.33	17.87	3.27	14.60	14.60	0.00	4
2.32	18.29	3.36	14.93	14.93	0.00	4
2.32	18.71	3.45	15.26	15.26	0.00	4
2.31	19.12	3.54	15.59	15.59	0.00	4
2.31	19.53	3.62	15.91	15.91	0.00	4
2.30	19.94	3.71	16.23	16.23	0.00	4
2.30	20.35	3.80	16.55	16.55	0.00	4
2.29	20.75	3.89	16.86	16.86	0.00	4
2.29	21.15	3.98	17.18	17.18	0.00	4
2.28	21.55	4.07	17.49	17.49	0.00	4
2.28	21.95	4.15	17.80	17.80	0.00	4
2.27	22.35	4.24	18.11	18.11	0.00	4
2.27	22.75	4.33	18.42	18.42	0.00	4
2.26	23.15	4.42	18.73	18.73	0.00	4

			output			
2.26	23.55	4.51	19.04	19.04	0.00	4
2.25	23.95	4.60	19.35	19.35	0.00	4
2.25	24.35	4.69	19.66	19.66	0.00	4
2.24	24.75	4.77	19.97	19.97	0.00	4
2.24	25.14	4.86	20.28	20.28	0.00	4
2.23	25.54	4.95	20.59	20.59	0.00	4
2.23	25.94	5.04	20.90	20.90	0.00	4
2.22	26.34	5.13	21.21	21.21	0.00	4
2.22	26.73	5.22	21.52	21.52	0.00	4
2.21	27.13	5.30	21.82	21.82	0.00	4
2.21	27.52	5.39	22.13	22.13	0.00	4
2.20	27.92	5.48	22.44	22.44	0.00	4
2.20	28.32	5.57	22.75	22.75	0.00	4
2.19	28.71	5.66	23.05	23.05	0.00	4
2.19	29.11	5.75	23.36	23.36	0.00	4
2.18	29.50	5.83	23.67	23.67	0.00	4
2.18	29.89	5.92	23.97	23.97	0.00	4
2.17	30.29	6.01	24.28	24.28	0.00	4
2.17	30.68	6.10	24.58	24.58	0.00	4
2.16	31.08	6.19	24.89	24.89	0.00	4
2.16	31.47	6.28	25.19	25.19	0.00	4
2.15	31.86	6.36	25.50	25.50	0.00	4
2.15	32.25	6.45	25.80	25.80	0.00	4
2.14	32.65	6.54	26.10	26.10	0.00	4
2.14	33.04	6.63	26.41	26.41	0.00	4
2.13	33.43	6.72	26.71	26.71	0.00	4
2.13	33.82	6.81	27.01	27.01	0.00	4
2.12	34.21	6.90	27.32	27.32	0.00	4
2.12	34.60	6.98	27.62	27.62	0.00	4
2.11	34.99	7.07	27.92	27.92	0.00	4
2.11	35.38	7.16	28.22	28.22	0.00	4
2.10	35.77	7.25	28.52	28.52	0.00	4
2.10	36.16	7.34	28.83	28.83	0.00	4
2.09	36.55	7.43	29.13	29.13	0.00	4
2.09	36.94	7.51	29.43	29.43	0.00	4
2.08	37.33	7.60	29.73	29.73	0.00	4
2.08	37.72	7.69	30.03	30.03	0.00	4
2.08	38.11	7.78	30.33	30.33	0.00	4
2.07	38.50	7.87	30.63	30.63	0.00	4
2.07	38.88	7.96	30.93	30.93	0.00	4
2.06	39.27	8.04	31.23	31.23	0.00	4
2.06	39.66	8.13	31.52	31.52	0.00	4
2.05	40.04	8.22	31.82	31.82	0.00	4
2.05	40.43	8.31	32.12	32.12	0.00	4
2.04	40.82	8.40	32.42	32.42	0.00	4
2.04	41.20	8.49	32.72	32.72	0.00	4
2.03	41.59	8.57	33.01	33.01	0.00	4
2.03	41.97	8.66	33.31	33.31	0.00	4

output

2.02	42.36	8.75	33.61	33.61	0.00	4
2.02	42.74	8.84	33.90	33.90	0.00	4
2.02	42.74	8.84	33.90	33.90	0.00	4
1.98	45.94	9.58	36.36	36.36	0.00	4
1.94	49.11	10.31	38.80	38.80	0.00	4
1.90	52.27	11.05	41.22	41.22	0.00	4
1.86	55.41	11.79	43.62	43.62	0.00	4
1.82	58.52	12.52	46.00	46.00	0.00	4
1.79	61.62	13.26	48.36	48.36	0.00	4
1.75	64.69	14.00	50.70	50.70	0.00	4
1.71	67.75	14.73	53.01	53.01	0.00	4
1.67	70.78	15.47	55.31	55.31	0.00	4
1.64	73.80	16.21	57.59	57.59	0.00	4
1.60	76.79	16.94	59.85	59.85	0.00	4
1.57	79.77	17.68	62.09	62.09	0.00	4
1.57	79.77	17.68	62.09	62.09	0.00	4
1.53	82.73	18.42	64.31	64.31	0.00	4
1.50	85.66	19.15	66.51	66.51	0.00	4
1.46	88.58	19.89	68.69	68.69	0.00	4
1.43	91.48	20.63	70.85	70.85	0.00	4
1.39	94.37	21.36	73.01	73.01	0.00	4
1.36	97.25	22.10	75.15	75.15	0.00	4
1.32	100.13	22.84	77.29	77.29	0.00	4
1.29	103.00	23.57	79.43	79.43	0.00	4
1.25	105.86	24.31	81.55	81.55	0.00	4
1.22	108.71	25.05	83.67	83.67	0.00	4
1.19	111.56	25.78	85.77	85.77	0.00	4
1.15	114.39	26.52	87.87	87.87	0.00	4
1.15	114.39	26.52	87.87	87.87	0.00	4
1.12	117.22	27.26	89.96	89.96	0.00	4
1.09	120.04	27.99	92.05	92.05	0.00	4
1.05	122.85	28.73	94.12	94.12	0.00	4
1.02	125.66	29.47	96.19	96.19	0.00	4
0.99	128.46	30.20	98.25	98.25	0.00	4
0.95	131.24	30.94	100.30	100.30	0.00	4
0.92	134.02	31.68	102.35	102.35	0.00	4
0.89	136.80	32.41	104.38	104.38	0.00	4
0.86	139.56	33.15	106.41	106.41	0.00	4
0.82	142.32	33.89	108.43	108.43	0.00	4
0.79	145.07	34.62	110.44	110.44	0.00	4
0.76	147.81	35.36	112.45	112.45	0.00	4
0.76	147.81	35.36	112.45	112.45	0.00	4
0.73	150.54	35.59	114.95	114.45	0.51	4
0.70	153.28	35.82	117.46	116.44	1.02	4
0.66	156.01	36.04	119.97	118.44	1.53	4
0.63	158.74	36.26	122.48	120.43	2.05	4
0.60	161.46	36.48	124.99	122.42	2.57	4
0.57	164.19	36.69	127.50	124.41	3.09	4

0.54	166.91	36.90	130.01	126.39	3.62	4
0.50	169.63	37.10	132.52	128.37	4.15	4
0.47	172.34	37.30	135.04	130.35	4.69	4
0.44	175.06	37.50	137.55	132.33	5.22	4
0.41	177.77	37.70	140.07	134.31	5.76	4
0.38	180.48	37.89	142.59	136.28	6.31	4
0.38	180.48	37.89	142.59	136.28	6.31	4
0.35	183.19	38.09	145.10	138.25	6.85	4
0.31	185.90	38.28	147.62	140.22	7.40	4
0.28	188.60	38.46	150.14	142.19	7.95	4
0.25	191.30	38.65	152.65	144.16	8.50	4
0.22	194.00	38.83	155.17	146.12	9.05	4
0.19	196.70	39.01	157.69	148.08	9.61	4
0.16	199.40	39.19	160.21	150.04	10.17	4
0.13	202.09	39.36	162.73	152.00	10.73	4
0.09	204.79	39.54	165.25	153.96	11.29	4
0.06	207.48	39.71	167.77	155.91	11.86	4
0.03	210.16	39.87	170.29	157.86	12.43	4
0.00	212.85	40.08	172.77	159.81	12.96	4

Time = 3650. Degree of Consolidation = 99.%

Total Settlement = 3.439

Settlement at End of Primary Consolidation = 3.455

Settlement caused by Primary Consolidation at time 3650. = 3.429

Settlement caused by Secondary Compression at time 3650. = 0.010

Settlement Due to Desiccation = 0.000

Surface Elevation = 1.05

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
10.50	10.49	4.83	0.91	0.91	0.91	3
10.10	10.09	4.62	0.91	0.91	0.91	3
9.70	9.69	4.41	0.91	0.91	0.91	3
9.30	9.29	4.20	0.91	0.91	0.91	3

8.90	8.89	3.99	0.91	0.91	0.90	3
8.50	8.49	3.78	0.91	0.90	0.90	3
8.10	8.09	3.57	0.90	0.90	0.90	3
7.70	7.69	3.36	0.90	0.90	0.90	3
7.30	7.29	3.15	0.90	0.90	0.90	3
6.90	6.89	2.94	0.90	0.90	0.90	3
6.50	6.49	2.73	0.90	0.90	0.90	3
6.50	6.49	2.73	1.40	1.40	1.39	2
5.85	5.84	2.46	1.39	1.39	1.39	2
5.19	5.19	2.18	1.39	1.39	1.38	2
4.54	4.54	1.91	1.39	1.38	1.38	2
3.89	3.89	1.64	1.38	1.38	1.38	2
3.24	3.24	1.36	1.38	1.38	1.38	2
2.59	2.59	1.09	1.38	1.38	1.38	2
1.94	1.94	0.82	1.38	1.37	1.37	2
1.29	1.29	0.55	1.38	1.37	1.37	2
0.65	0.65	0.27	1.37	1.37	1.37	2
0.00	0.00	0.00	1.37	1.36	1.36	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
10.49	212.85	40.08	172.77	159.81	12.96	3
10.09	259.85	58.16	201.69	184.80	16.89	3
9.69	306.83	76.10	230.73	209.79	20.95	3
9.29	353.81	93.95	259.86	234.76	25.11	3
8.89	400.78	111.73	289.05	259.72	29.32	3
8.49	447.74	129.51	318.22	284.67	33.55	3
8.09	494.69	147.36	347.33	309.62	37.71	3
7.69	541.63	165.37	376.26	334.55	41.70	3
7.29	588.56	183.68	404.88	359.48	45.40	3
6.89	635.48	202.52	432.95	384.40	48.56	3
6.49	682.39	222.30	460.09	409.30	50.79	3
6.49	682.39	222.30	460.09	409.30	50.79	2
5.84	751.21	248.14	503.08	450.04	53.04	2
5.19	819.98	288.06	531.92	490.71	41.21	2
4.54	888.69	329.70	558.99	531.33	27.66	2
3.89	957.36	369.43	587.93	571.91	16.02	2
3.24	1025.98	405.04	620.94	612.44	8.50	2
2.59	1094.56	430.62	663.94	652.93	11.01	2
1.94	1163.10	457.83	705.26	693.37	11.89	2
1.29	1231.59	487.61	743.97	733.77	10.20	2
0.65	1300.02	520.10	779.92	774.11	5.81	2
0.00	1368.40	553.61	814.79	814.40	0.39	2

Time = 7300. Degree of Consolidation = 55.%

Total Settlement = 0.009

Settlement at End of Primary Consolidation = 0.017

Settlement caused by Primary Consolidation at time 7300. = 0.009

Settlement caused by Secondary Compression at time 7300. = 0.000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
6.00	2.56	0.50	11.00	11.00	11.00	4
5.99	2.55	0.50	11.00	9.23	9.23	4
5.98	2.54	0.50	11.00	8.74	8.74	4
5.97	2.54	0.50	11.00	8.45	8.45	4
5.96	2.53	0.50	11.00	8.15	8.15	4
5.95	2.52	0.50	11.00	7.89	7.89	4
5.94	2.51	0.50	11.00	7.67	7.67	4
5.93	2.51	0.49	11.00	7.45	7.45	4
5.92	2.50	0.49	11.00	7.23	7.23	4
5.91	2.49	0.49	11.00	7.01	7.01	4
5.90	2.49	0.49	11.00	6.93	6.93	4
5.89	2.48	0.49	11.00	6.85	6.86	4
5.88	2.47	0.49	11.00	6.78	6.78	4
5.87	2.47	0.49	11.00	6.71	6.71	4
5.86	2.46	0.49	11.00	6.63	6.64	4
5.85	2.45	0.49	11.00	6.56	6.56	4
5.84	2.45	0.49	11.00	6.49	6.49	4
5.83	2.44	0.49	11.00	6.41	6.41	4
5.82	2.43	0.49	11.00	6.34	6.34	4
5.81	2.43	0.48	11.00	6.27	6.27	4
5.80	2.42	0.48	11.00	6.19	6.19	4
5.79	2.42	0.48	11.00	6.12	6.12	4
5.78	2.41	0.48	11.00	6.04	6.05	4
5.77	2.40	0.48	11.00	5.98	5.98	4
5.76	2.40	0.48	11.00	5.94	5.94	4
5.75	2.39	0.48	11.00	5.89	5.89	4
5.74	2.39	0.48	11.00	5.85	5.85	4
5.73	2.38	0.48	11.00	5.81	5.81	4
5.72	2.38	0.48	11.00	5.76	5.76	4
5.71	2.37	0.48	11.00	5.72	5.72	4

output

5.70	2.37	0.48	11.00	5.67	5.67	4
5.69	2.36	0.47	11.00	5.63	5.63	4
5.68	2.35	0.47	11.00	5.58	5.59	4
5.67	2.35	0.47	11.00	5.54	5.54	4
5.66	2.34	0.47	11.00	5.50	5.50	4
5.65	2.34	0.47	11.00	5.45	5.45	4
5.64	2.33	0.47	11.00	5.41	5.41	4
5.63	2.33	0.47	11.00	5.36	5.36	4
5.62	2.32	0.47	11.00	5.32	5.32	4
5.61	2.32	0.47	11.00	5.27	5.28	4
5.60	2.31	0.47	11.00	5.23	5.23	4
5.59	2.31	0.47	11.00	5.19	5.19	4
5.58	2.30	0.47	11.00	5.14	5.14	4
5.57	2.30	0.46	11.00	5.10	5.10	4
5.56	2.29	0.46	11.00	5.05	5.06	4
5.55	2.29	0.46	11.00	5.01	5.01	4
5.54	2.28	0.46	11.00	5.00	5.00	4
5.53	2.28	0.46	11.00	4.99	4.99	4
5.52	2.27	0.46	11.00	4.98	4.98	4
5.51	2.27	0.46	11.00	4.98	4.98	4
5.50	2.26	0.46	11.00	4.97	4.97	4
5.49	2.26	0.46	11.00	4.97	4.97	4
5.48	2.25	0.46	11.00	4.96	4.96	4
5.47	2.25	0.46	11.00	4.96	4.96	4
5.46	2.24	0.46	11.00	4.95	4.95	4
5.45	2.24	0.45	11.00	4.95	4.95	4
5.44	2.23	0.45	11.00	4.94	4.94	4
5.43	2.23	0.45	11.00	4.93	4.94	4
5.42	2.22	0.45	11.00	4.93	4.93	4
5.41	2.22	0.45	11.00	4.92	4.92	4
5.40	2.21	0.45	11.00	4.92	4.92	4
5.39	2.21	0.45	11.00	4.91	4.91	4
5.38	2.20	0.45	11.00	4.91	4.91	4
5.37	2.20	0.45	11.00	4.90	4.90	4
5.36	2.19	0.45	11.00	4.90	4.90	4
5.35	2.19	0.45	11.00	4.89	4.89	4
5.34	2.18	0.45	11.00	4.88	4.89	4
5.33	2.18	0.44	11.00	4.88	4.88	4
5.32	2.17	0.44	11.00	4.87	4.87	4
5.31	2.17	0.44	11.00	4.87	4.87	4
5.30	2.16	0.44	11.00	4.86	4.86	4
5.29	2.16	0.44	11.00	4.86	4.86	4
5.28	2.15	0.44	11.00	4.85	4.85	4
5.27	2.15	0.44	11.00	4.85	4.85	4
5.26	2.14	0.44	11.00	4.84	4.84	4
5.25	2.14	0.44	11.00	4.83	4.84	4
5.24	2.13	0.44	11.00	4.83	4.83	4
5.23	2.13	0.44	11.00	4.82	4.82	4

			output			
5.22	2.12	0.43	11.00	4.82	4.82	4
5.21	2.12	0.43	11.00	4.81	4.81	4
5.20	2.11	0.43	11.00	4.81	4.81	4
5.19	2.11	0.43	11.00	4.80	4.80	4
5.18	2.10	0.43	11.00	4.80	4.80	4
5.17	2.10	0.43	11.00	4.79	4.79	4
5.16	2.09	0.43	11.00	4.79	4.79	4
5.15	2.09	0.43	11.00	4.78	4.78	4
5.14	2.08	0.43	11.00	4.77	4.77	4
5.13	2.08	0.43	11.00	4.77	4.77	4
5.12	2.08	0.43	11.00	4.76	4.76	4
5.11	2.07	0.43	11.00	4.76	4.76	4
5.10	2.07	0.42	11.00	4.75	4.75	4
5.09	2.06	0.42	11.00	4.75	4.75	4
5.08	2.06	0.42	11.00	4.74	4.74	4
5.07	2.05	0.42	11.00	4.74	4.74	4
5.06	2.05	0.42	11.00	4.73	4.73	4
5.05	2.04	0.42	11.00	4.72	4.73	4
5.04	2.04	0.42	11.00	4.72	4.72	4
5.03	2.03	0.42	11.00	4.71	4.71	4
5.02	2.03	0.42	11.00	4.71	4.71	4
5.01	2.02	0.42	11.00	4.70	4.70	4
5.00	2.02	0.42	11.00	4.70	4.70	4
5.00	2.02	0.42	11.00	4.70	4.70	4
4.92	1.98	0.41	11.00	4.65	4.65	4
4.83	1.94	0.40	11.00	4.60	4.61	4
4.75	1.90	0.40	11.00	4.56	4.56	4
4.67	1.86	0.39	11.00	4.51	4.51	4
4.58	1.82	0.38	11.00	4.47	4.47	4
4.50	1.79	0.37	11.00	4.42	4.42	4
4.42	1.75	0.37	11.00	4.37	4.38	4
4.33	1.71	0.36	11.00	4.33	4.33	4
4.25	1.67	0.35	11.00	4.28	4.28	4
4.17	1.64	0.35	11.00	4.24	4.24	4
4.08	1.60	0.34	11.00	4.19	4.19	4
4.00	1.57	0.33	11.00	4.14	4.14	4
4.00	1.57	0.33	11.00	4.14	4.14	4
3.92	1.53	0.33	11.00	4.10	4.10	4
3.83	1.50	0.32	11.00	4.05	4.05	4
3.75	1.46	0.31	11.00	4.01	4.01	4
3.67	1.43	0.31	11.00	3.98	3.98	4
3.58	1.39	0.30	11.00	3.97	3.97	4
3.50	1.36	0.29	11.00	3.95	3.95	4
3.42	1.32	0.28	11.00	3.93	3.93	4
3.33	1.29	0.28	11.00	3.91	3.91	4
3.25	1.25	0.27	11.00	3.89	3.89	4
3.17	1.22	0.26	11.00	3.87	3.87	4
3.08	1.19	0.26	11.00	3.85	3.86	4

3.00	1.15	0.25	11.00	3.84	3.84	4
3.00	1.15	0.25	11.00	3.84	3.84	4
2.92	1.12	0.24	11.00	3.82	3.82	4
2.83	1.09	0.24	11.00	3.80	3.80	4
2.75	1.05	0.23	11.00	3.78	3.78	4
2.67	1.02	0.22	11.00	3.76	3.76	4
2.58	0.99	0.22	11.00	3.74	3.74	4
2.50	0.95	0.21	11.00	3.73	3.73	4
2.42	0.92	0.20	11.00	3.71	3.71	4
2.33	0.89	0.19	11.00	3.69	3.69	4
2.25	0.86	0.19	11.00	3.67	3.67	4
2.17	0.82	0.18	11.00	3.65	3.65	4
2.08	0.79	0.17	11.00	3.63	3.63	4
2.00	0.76	0.17	11.00	3.62	3.62	4
2.00	0.76	0.17	11.00	3.62	3.62	4
1.92	0.73	0.16	11.00	3.61	3.60	4
1.83	0.70	0.15	11.00	3.60	3.58	4
1.75	0.66	0.15	11.00	3.60	3.56	4
1.67	0.63	0.14	11.00	3.59	3.54	4
1.58	0.60	0.13	11.00	3.59	3.52	4
1.50	0.57	0.13	11.00	3.58	3.51	4
1.42	0.54	0.12	11.00	3.58	3.49	4
1.33	0.50	0.11	11.00	3.57	3.48	4
1.25	0.47	0.10	11.00	3.57	3.48	4
1.17	0.44	0.10	11.00	3.56	3.47	4
1.08	0.41	0.09	11.00	3.56	3.46	4
1.00	0.38	0.08	11.00	3.55	3.45	4
1.00	0.38	0.08	11.00	3.55	3.45	4
0.92	0.35	0.08	11.00	3.55	3.44	4
0.83	0.31	0.07	11.00	3.54	3.43	4
0.75	0.28	0.06	11.00	3.54	3.42	4
0.67	0.25	0.06	11.00	3.53	3.41	4
0.58	0.22	0.05	11.00	3.53	3.40	4
0.50	0.19	0.04	11.00	3.52	3.39	4
0.42	0.16	0.03	11.00	3.52	3.38	4
0.33	0.13	0.03	11.00	3.52	3.37	4
0.25	0.09	0.02	11.00	3.51	3.36	4
0.17	0.06	0.01	11.00	3.51	3.36	4
0.08	0.03	0.01	11.00	3.50	3.35	4
0.00	0.00	0.00	11.00	3.50	3.34	4

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
2.56	0.00	0.00	0.00	0.00	0.00	4
2.55	0.66	0.09	0.57	0.57	0.00	4
2.54	1.26	0.18	1.09	1.09	0.00	4

output

2.54	1.85	0.27	1.59	1.59	0.00	4
2.53	2.42	0.35	2.07	2.07	0.00	4
2.52	2.98	0.44	2.54	2.54	0.00	4
2.51	3.52	0.53	2.99	2.99	0.00	4
2.51	4.06	0.62	3.44	3.44	0.00	4
2.50	4.58	0.71	3.87	3.87	0.00	4
2.49	5.09	0.80	4.29	4.29	0.00	4
2.49	5.59	0.88	4.71	4.71	0.00	4
2.48	6.09	0.97	5.12	5.12	0.00	4
2.47	6.59	1.06	5.53	5.53	0.00	4
2.47	7.08	1.15	5.93	5.93	0.00	4
2.46	7.57	1.24	6.33	6.33	0.00	4
2.45	8.05	1.33	6.72	6.72	0.00	4
2.45	8.53	1.41	7.11	7.11	0.00	4
2.44	9.00	1.50	7.50	7.50	0.00	4
2.43	9.48	1.59	7.88	7.88	0.00	4
2.43	9.94	1.68	8.26	8.26	0.00	4
2.42	10.41	1.77	8.64	8.64	0.00	4
2.42	10.87	1.86	9.01	9.01	0.00	4
2.41	11.33	1.94	9.38	9.38	0.00	4
2.40	11.78	2.03	9.75	9.75	0.00	4
2.40	12.23	2.12	10.11	10.11	0.00	4
2.39	12.68	2.21	10.47	10.47	0.00	4
2.39	13.12	2.30	10.82	10.82	0.00	4
2.38	13.57	2.39	11.18	11.18	0.00	4
2.38	14.01	2.48	11.53	11.53	0.00	4
2.37	14.45	2.56	11.88	11.88	0.00	4
2.37	14.88	2.65	12.23	12.23	0.00	4
2.36	15.32	2.74	12.58	12.58	0.00	4
2.35	15.75	2.83	12.92	12.92	0.00	4
2.35	16.18	2.92	13.26	13.26	0.00	4
2.34	16.61	3.01	13.60	13.60	0.00	4
2.34	17.03	3.09	13.94	13.94	0.00	4
2.33	17.45	3.18	14.27	14.27	0.00	4
2.33	17.87	3.27	14.60	14.60	0.00	4
2.32	18.29	3.36	14.93	14.93	0.00	4
2.32	18.71	3.45	15.26	15.26	0.00	4
2.31	19.12	3.54	15.59	15.59	0.00	4
2.31	19.53	3.62	15.91	15.91	0.00	4
2.30	19.94	3.71	16.23	16.23	0.00	4
2.30	20.35	3.80	16.55	16.55	0.00	4
2.29	20.75	3.89	16.86	16.86	0.00	4
2.29	21.15	3.98	17.18	17.18	0.00	4
2.28	21.55	4.07	17.49	17.49	0.00	4
2.28	21.95	4.15	17.80	17.80	0.00	4
2.27	22.35	4.24	18.11	18.11	0.00	4
2.27	22.75	4.33	18.42	18.42	0.00	4
2.26	23.15	4.42	18.73	18.73	0.00	4

			output			
2.26	23.55	4.51	19.04	19.04	0.00	4
2.25	23.95	4.60	19.35	19.35	0.00	4
2.25	24.35	4.69	19.66	19.66	0.00	4
2.24	24.75	4.77	19.97	19.97	0.00	4
2.24	25.14	4.86	20.28	20.28	0.00	4
2.23	25.54	4.95	20.59	20.59	0.00	4
2.23	25.94	5.04	20.90	20.90	0.00	4
2.22	26.34	5.13	21.21	21.21	0.00	4
2.22	26.73	5.22	21.52	21.52	0.00	4
2.21	27.13	5.30	21.82	21.82	0.00	4
2.21	27.52	5.39	22.13	22.13	0.00	4
2.20	27.92	5.48	22.44	22.44	0.00	4
2.20	28.32	5.57	22.75	22.75	0.00	4
2.19	28.71	5.66	23.05	23.05	0.00	4
2.19	29.11	5.75	23.36	23.36	0.00	4
2.18	29.50	5.83	23.67	23.67	0.00	4
2.18	29.89	5.92	23.97	23.97	0.00	4
2.17	30.29	6.01	24.28	24.28	0.00	4
2.17	30.68	6.10	24.58	24.58	0.00	4
2.16	31.08	6.19	24.89	24.89	0.00	4
2.16	31.47	6.28	25.19	25.19	0.00	4
2.15	31.86	6.36	25.50	25.50	0.00	4
2.15	32.25	6.45	25.80	25.80	0.00	4
2.14	32.65	6.54	26.10	26.10	0.00	4
2.14	33.04	6.63	26.41	26.41	0.00	4
2.13	33.43	6.72	26.71	26.71	0.00	4
2.13	33.82	6.81	27.01	27.01	0.00	4
2.12	34.21	6.90	27.32	27.32	0.00	4
2.12	34.60	6.98	27.62	27.62	0.00	4
2.11	34.99	7.07	27.92	27.92	0.00	4
2.11	35.38	7.16	28.22	28.22	0.00	4
2.10	35.77	7.25	28.52	28.52	0.00	4
2.10	36.16	7.34	28.83	28.83	0.00	4
2.09	36.55	7.43	29.13	29.13	0.00	4
2.09	36.94	7.51	29.43	29.43	0.00	4
2.08	37.33	7.60	29.73	29.73	0.00	4
2.08	37.72	7.69	30.03	30.03	0.00	4
2.08	38.11	7.78	30.33	30.33	0.00	4
2.07	38.50	7.87	30.63	30.63	0.00	4
2.07	38.88	7.96	30.93	30.93	0.00	4
2.06	39.27	8.04	31.23	31.23	0.00	4
2.06	39.66	8.13	31.52	31.52	0.00	4
2.05	40.04	8.22	31.82	31.82	0.00	4
2.05	40.43	8.31	32.12	32.12	0.00	4
2.04	40.82	8.40	32.42	32.42	0.00	4
2.04	41.20	8.49	32.72	32.72	0.00	4
2.03	41.59	8.57	33.01	33.01	0.00	4
2.03	41.97	8.66	33.31	33.31	0.00	4

output

2.02	42.36	8.75	33.61	33.61	0.00	4
2.02	42.74	8.84	33.90	33.90	0.00	4
2.02	42.74	8.84	33.90	33.90	0.00	4
1.98	45.94	9.58	36.36	36.36	0.00	4
1.94	49.11	10.31	38.80	38.80	0.00	4
1.90	52.27	11.05	41.22	41.22	0.00	4
1.86	55.41	11.79	43.62	43.62	0.00	4
1.82	58.52	12.52	46.00	46.00	0.00	4
1.79	61.62	13.26	48.36	48.36	0.00	4
1.75	64.69	14.00	50.70	50.70	0.00	4
1.71	67.75	14.73	53.01	53.01	0.00	4
1.67	70.78	15.47	55.31	55.31	0.00	4
1.64	73.80	16.21	57.59	57.59	0.00	4
1.60	76.79	16.94	59.85	59.85	0.00	4
1.57	79.77	17.68	62.09	62.09	0.00	4
1.57	79.77	17.68	62.09	62.09	0.00	4
1.53	82.73	18.42	64.31	64.31	0.00	4
1.50	85.66	19.15	66.51	66.51	0.00	4
1.46	88.58	19.89	68.69	68.69	0.00	4
1.43	91.48	20.63	70.85	70.85	0.00	4
1.39	94.37	21.36	73.01	73.01	0.00	4
1.36	97.25	22.10	75.15	75.15	0.00	4
1.32	100.13	22.84	77.29	77.29	0.00	4
1.29	103.00	23.57	79.43	79.43	0.00	4
1.25	105.86	24.31	81.55	81.55	0.00	4
1.22	108.71	25.05	83.67	83.67	0.00	4
1.19	111.56	25.78	85.77	85.77	0.00	4
1.15	114.39	26.52	87.87	87.87	0.00	4
1.15	114.39	26.52	87.87	87.87	0.00	4
1.12	117.22	27.26	89.96	89.96	0.00	4
1.09	120.04	27.99	92.05	92.05	0.00	4
1.05	122.85	28.73	94.12	94.12	0.00	4
1.02	125.66	29.47	96.19	96.19	0.00	4
0.99	128.46	30.20	98.25	98.25	0.00	4
0.95	131.24	30.94	100.30	100.30	0.00	4
0.92	134.02	31.68	102.35	102.35	0.00	4
0.89	136.80	32.41	104.38	104.38	0.00	4
0.86	139.56	33.15	106.41	106.41	0.00	4
0.82	142.32	33.89	108.43	108.43	0.00	4
0.79	145.07	34.62	110.44	110.44	0.00	4
0.76	147.81	35.36	112.45	112.45	0.00	4
0.76	147.81	35.36	112.45	112.45	0.00	4
0.73	150.54	35.59	114.95	114.45	0.51	4
0.70	153.28	35.82	117.46	116.44	1.02	4
0.66	156.01	36.04	119.97	118.44	1.53	4
0.63	158.74	36.26	122.48	120.43	2.05	4
0.60	161.46	36.48	124.99	122.42	2.57	4
0.57	164.19	36.69	127.50	124.41	3.09	4

output

0.54	166.91	36.90	130.01	126.39	3.62	4
0.50	169.63	37.10	132.52	128.37	4.15	4
0.47	172.34	37.30	135.04	130.35	4.69	4
0.44	175.06	37.50	137.55	132.33	5.22	4
0.41	177.77	37.70	140.07	134.31	5.76	4
0.38	180.48	37.89	142.59	136.28	6.31	4
0.38	180.48	37.89	142.59	136.28	6.31	4
0.35	183.19	38.09	145.10	138.25	6.85	4
0.31	185.90	38.28	147.62	140.22	7.40	4
0.28	188.60	38.46	150.14	142.19	7.95	4
0.25	191.30	38.65	152.65	144.16	8.50	4
0.22	194.00	38.83	155.17	146.12	9.05	4
0.19	196.70	39.01	157.69	148.08	9.61	4
0.16	199.40	39.19	160.21	150.04	10.17	4
0.13	202.09	39.36	162.73	152.00	10.73	4
0.09	204.79	39.54	165.25	153.96	11.29	4
0.06	207.48	39.71	167.77	155.91	11.86	4
0.03	210.16	39.87	170.29	157.86	12.43	4
0.00	212.85	40.08	172.77	159.81	12.96	4

Time = 7300. Degree of Consolidation = 99.%

Total Settlement = 3.439

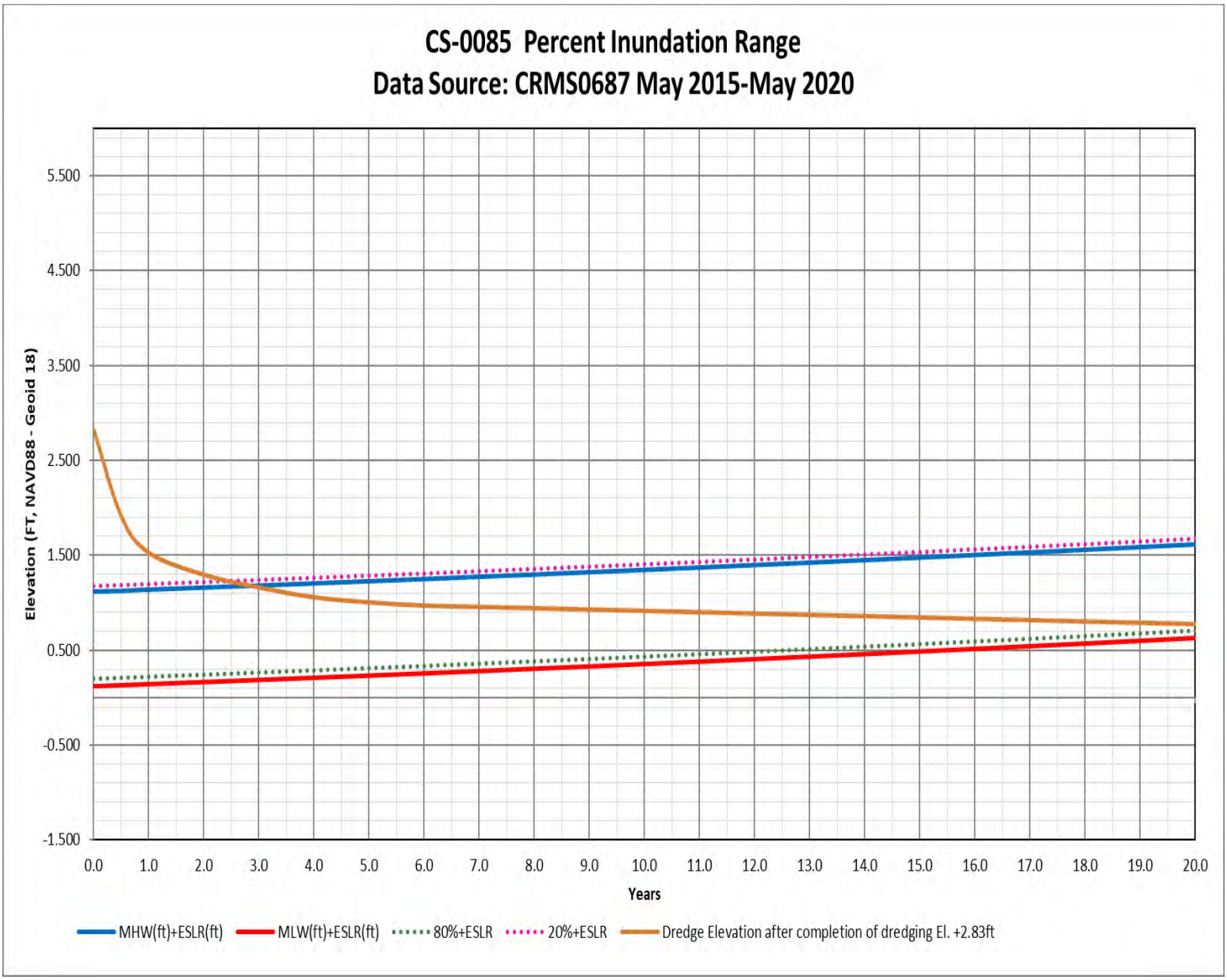
Settlement at End of Primary Consolidation = 3.455

Settlement caused by Primary Consolidation at time 7300. = 3.421

Settlement caused by Secondary Compression at time 7300. = 0.017

Settlement Due to Desiccation = 0.000

Surface Elevation = 1.05


CS-0085 Percent Inundation Range
Data Source: CRMS0687 May 2015-May 2020
Elevation (FT, NAVD88 - Geoid 18)
5.500
4.500
3.500
2.500
1.500
0.500
-0.500
-1.500
0.0
1.0
2.0
3.0
4.0
5.0
6.0
7.0
8.0
9.0
10.0
11.0
12.0
13.0
14.0
15.0
16.0
17.0
18.0
19.0
20.0
Years
MHW(ft)+ESLR(ft)
MLW(ft)+ESLR(ft)
80%+ESLR
20%+ESLR
Dredge Elevation after completion of dredging El. +2.83ft

APPENDIX D

VOLUMETRIC CUT AND FILL RATIO

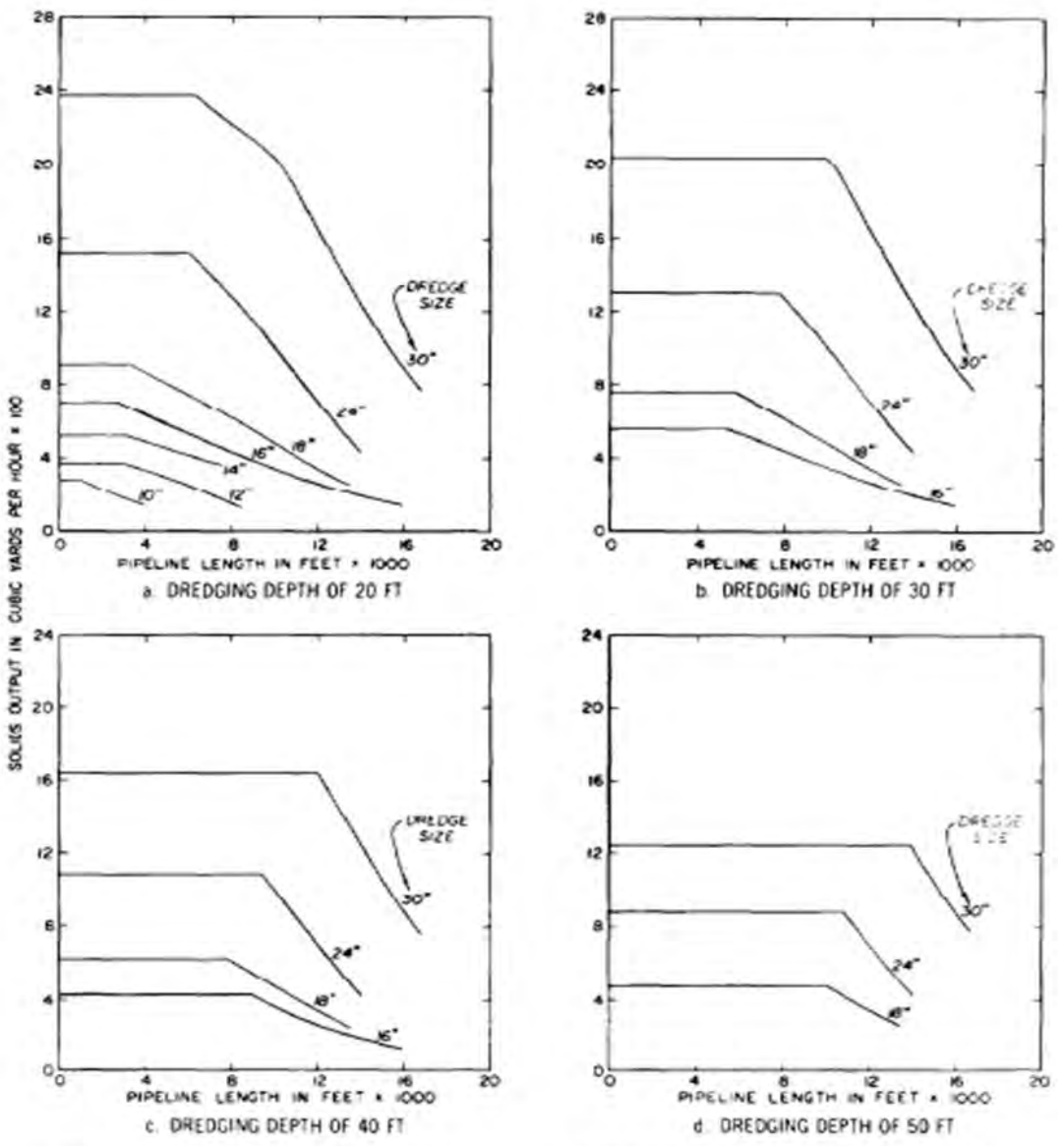


Figure 4-2. Relationships among solids output, dredge size, and pipeline length for various dredging depths

1) General Design Data:

Wn =	114	(%)	Moisture Content
Gs =	2.7	(#)	Specific Gravity
+ #200 Sieve =	5	(%)	Percent Coarse Sample by Weight
Dredge Size =	30	(in)	

Work Hours / day =	15	(hr. / day)		
Production Rate =	1,650	(cu. yd / hr	24750	(cu. yd / day.)
Volume to be Dredged =	1,825,175	(cu. yd.)	49,279,728	(ft.^3)

Estimate the time of dredging

Time =	1106.2	(hr.)	Time = Volume / Production Rate
Work days =	73.7	(day)	Work Days = Time / Work Hours

Average time for initial dredged material consolidation

t50 =	37	(day)	t50 = Work days / 2

Intertek PSI

Cut-to-Fill Calculations - Containment Dike

Project No. 2541211
Project Name: Long Point

1) Compute Total Volume of Embankment

Marsh Creation Area: Dikes

Ground Surface:	-2	ft.	Assumed			
Crown Width:	5		Assumed			
Side Slopes	3	H:1V	Assumed			
Top of Crown:	4		Assumed			
Area:	138.0	ft.^2				
Length:	30,127	ft.	From Google Outline			
			Volume:	4,157,526	ft.^3	153,982 cu.yd.

Marsh Creation Area: Immediate Settlement beneath dikes

Immediate Settlement:	6	in	0.500	ft.		
Equivalent Base Width (ft.):	41	ft.				
Length of Dike:	30,127	ft.				
			Volume:	617,604	ft.^3	22,874 cu.yd.
			Vc =	4,775,130	ft. ^3	176,857 cu. Yd.
					use:	176,857 cu. Yd.

2) Compute the Weight of the Solids

γc dry:	61.5	pcf.	Dry Weight of Cut Material
Mcv:	30.0	(%)	Moisture Content of Cut and compact
γc:	80.0	pcf.	Wet Weight of Cut Material

Ws = 293,854,123 lbs.

3) Calculate the required volume of borrow material

γb dry:	51.2	pcf.	Dry weight of Borrow Material
Mcb:	105.0	(%)	Moisture Content of borrow material
γb:	105.0	pcf.	wet weight of borrow

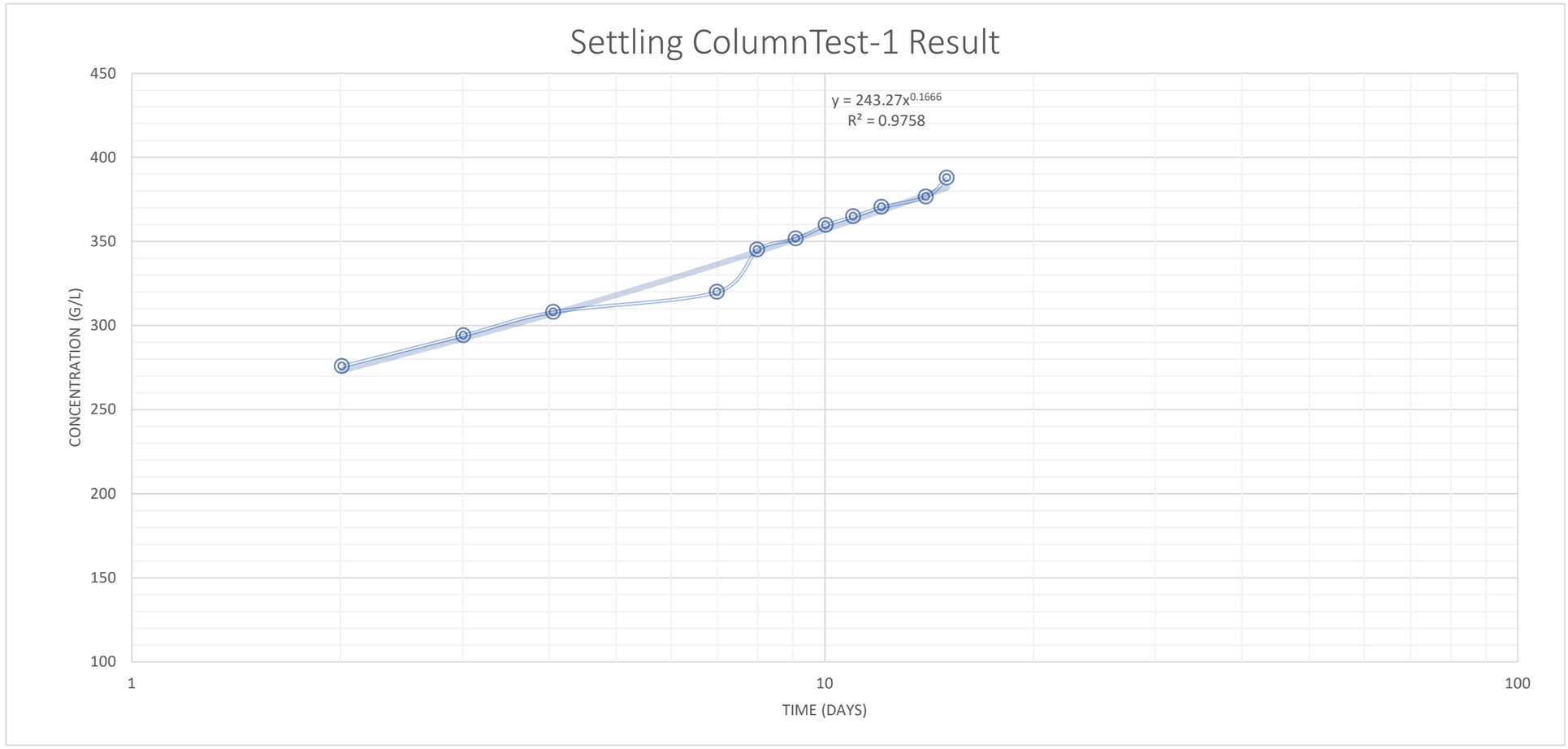
Vb =	5,737,152	ft. ^3	212,487	cu. Yd.
		use:	212,487	cu. Yd.

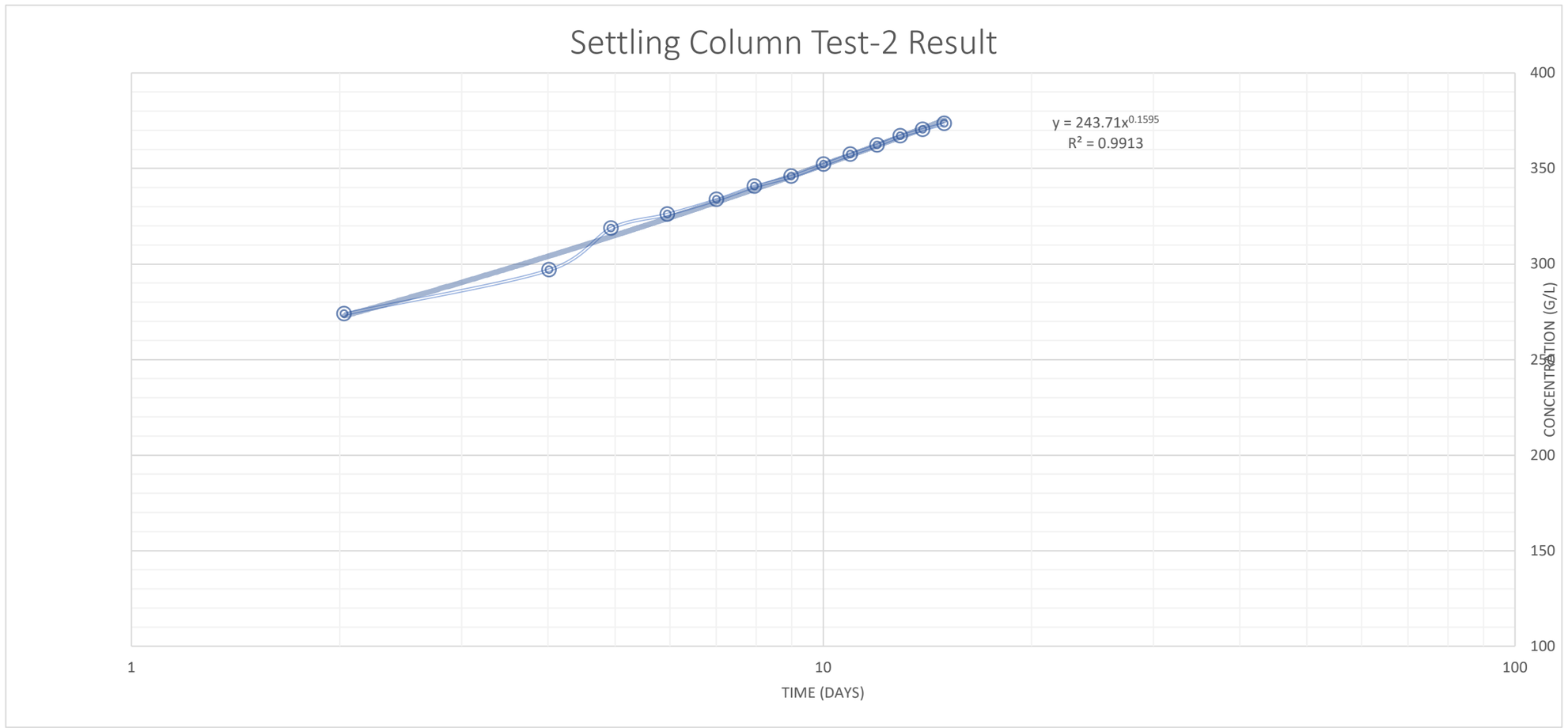
4) Determine % Shrink

% Shrink = 16.8

5) Determine Cut-to-Fill Ratio

Cut-to-Fill = 1.20





Average void ratio of the in situ sediments $e_i = \frac{G_s \cdot w}{1}$

Boring	B6	B7	B8	B9	B10	B11	B12	Ave	ei
w	1.85	1.55	1.28	0.86	1.02	0.66	0.75	1.14	3.11

Average void ratio of the sediments after dredge disposal

Void ratio, e0: $e_0 = \frac{G_s \cdot \gamma_w}{C_d} - 1$

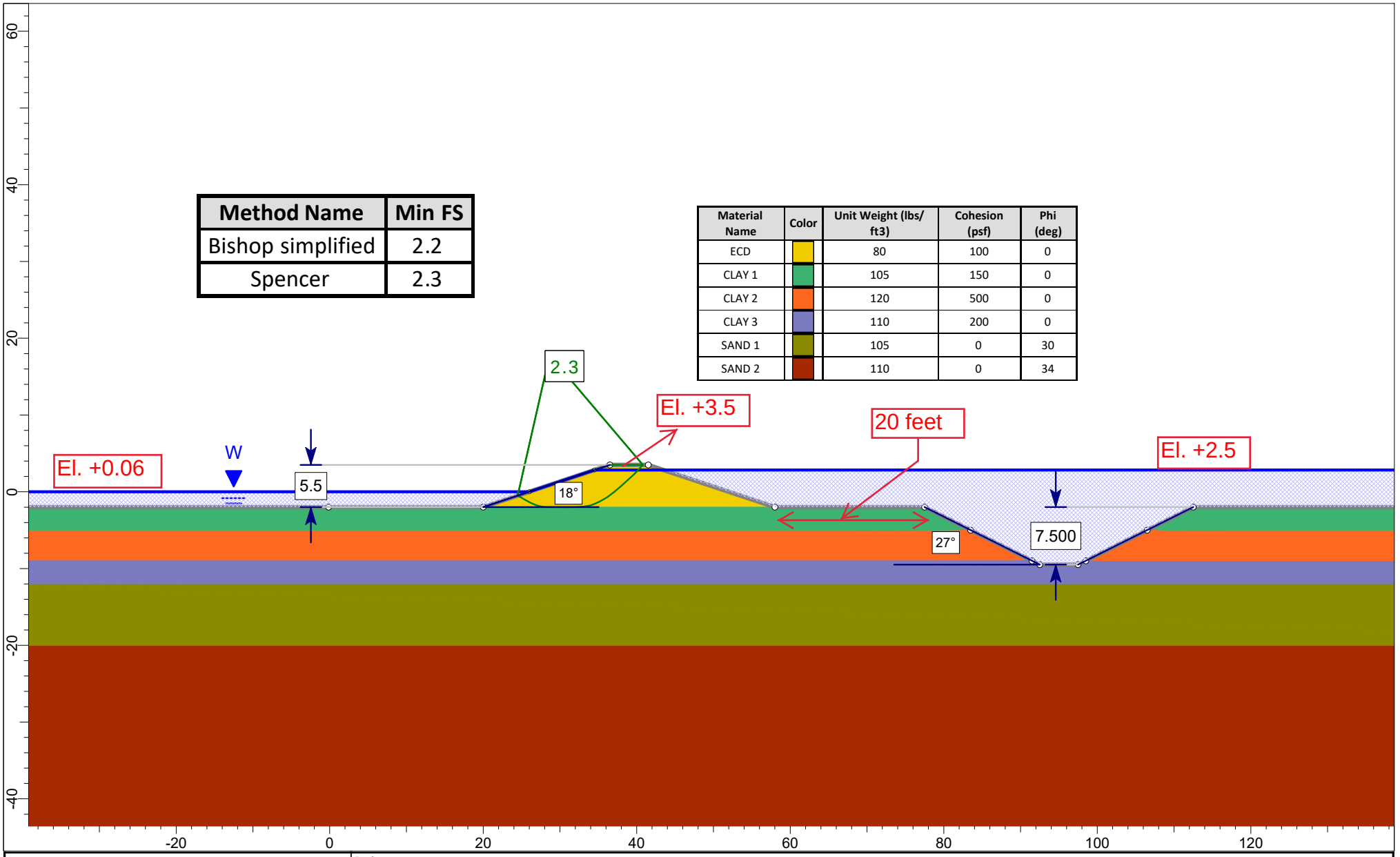
$C_d = 243.27 \cdot (80days)^{0.1666} = 441.94\ {}^{g}/_{L}$

$C_d = (243.71) \cdot (80days)^{0.1595} = 431.622\ {}^{g}/_{L}$

				Initial TSS Con	Cd	e0
Specific gravity,	2.74	(measured, PSI)				
Unit weight of water	1000	g/L				
Dredging Duration	72	Day	Composit A	146.67	441.9453	5.19
Average Time	36	Day	Composit B	150.22	431.622	5.34

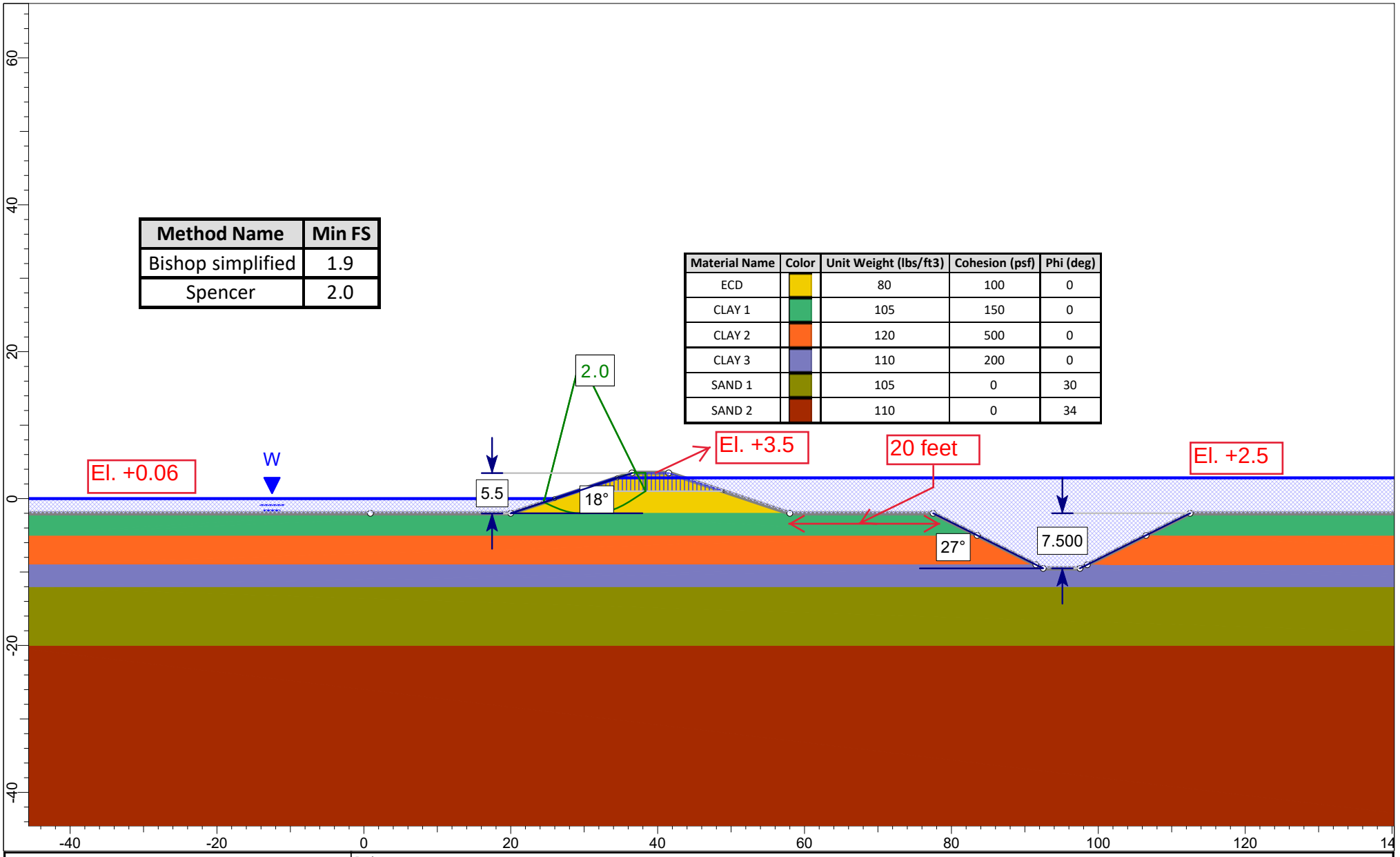
APPENDIX E
SLOPE STABILITY ANALYSES

Top of Dike Elevation +3.5 feet (NAVD88-Geoid 18)



rocscience	Project	PSI Report No. : 02541211-, Long point Bayou Marsh Creation Project	
	Group	Case B	Scenario: Master Scenario
	Drawn By		Company: Intertek PSI
	Date		File Name: ECD Slope-Case B (C=100 psf) 3H 1V.slmd

SLIDEINTERPRET 9.008



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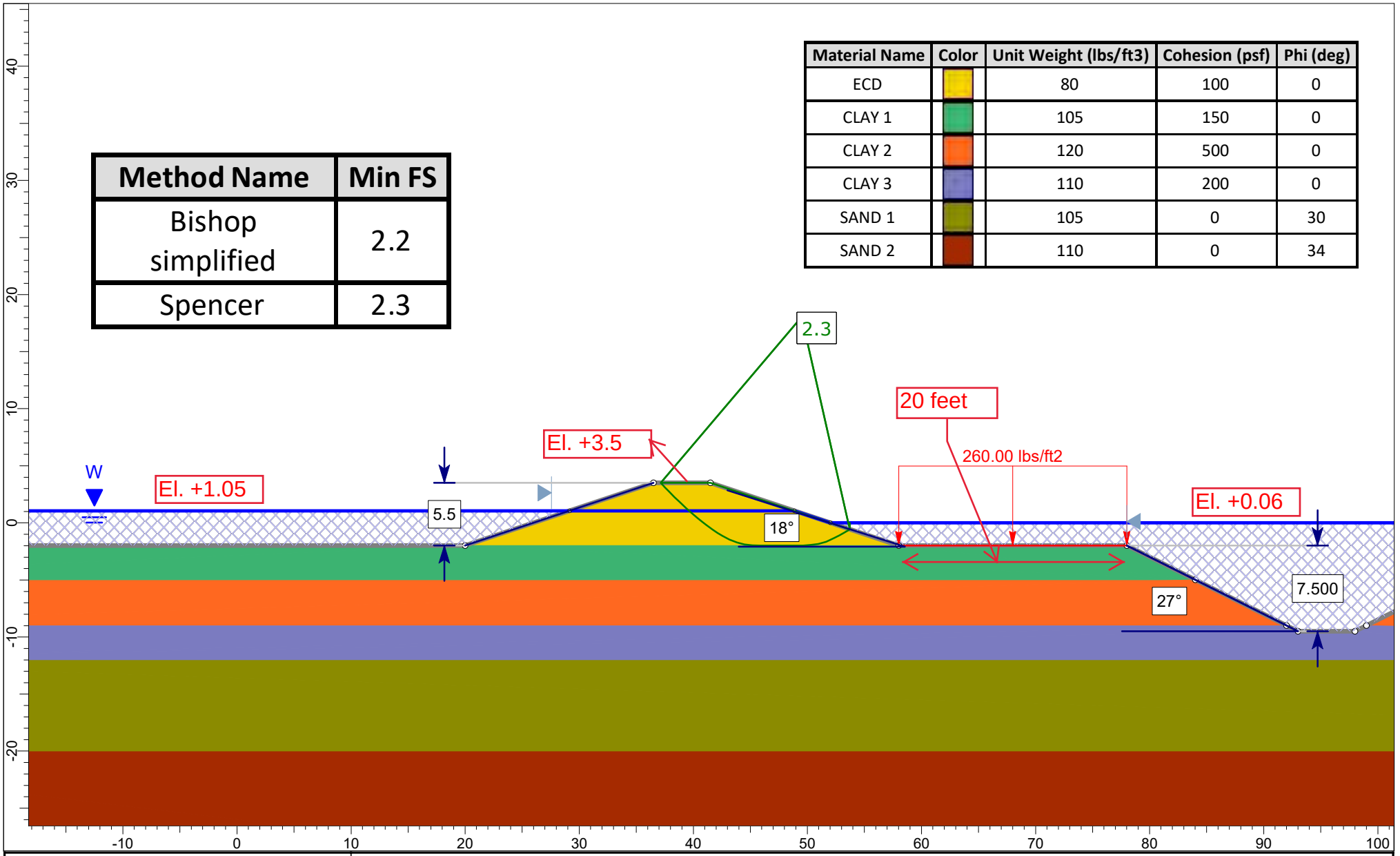
SLIDEINTERPRET 9.008

Project	PSI Report No. : 02541211-, Long point Bayou Marsh Creation Project		
Group	Case B- Tension Crack	*Scenario*	Master Scenario
Drawn By		*Company*	Intertek PSI
Date		*File Name*	ECD Slope-Case B (C=100 psf) 3H 1V.slmd

Method Name	Min FS
Bishop simplified	2.2
Spencer	2.3

Material Name	Color	Unit Weight (lbs/ft3)	Cohesion (psf)	Phi (deg)
ECD		80	100	0
CLAY 1		105	150	0
CLAY 2		120	500	0
CLAY 3		110	200	0
SAND 1		105	0	30
SAND 2		110	0	34



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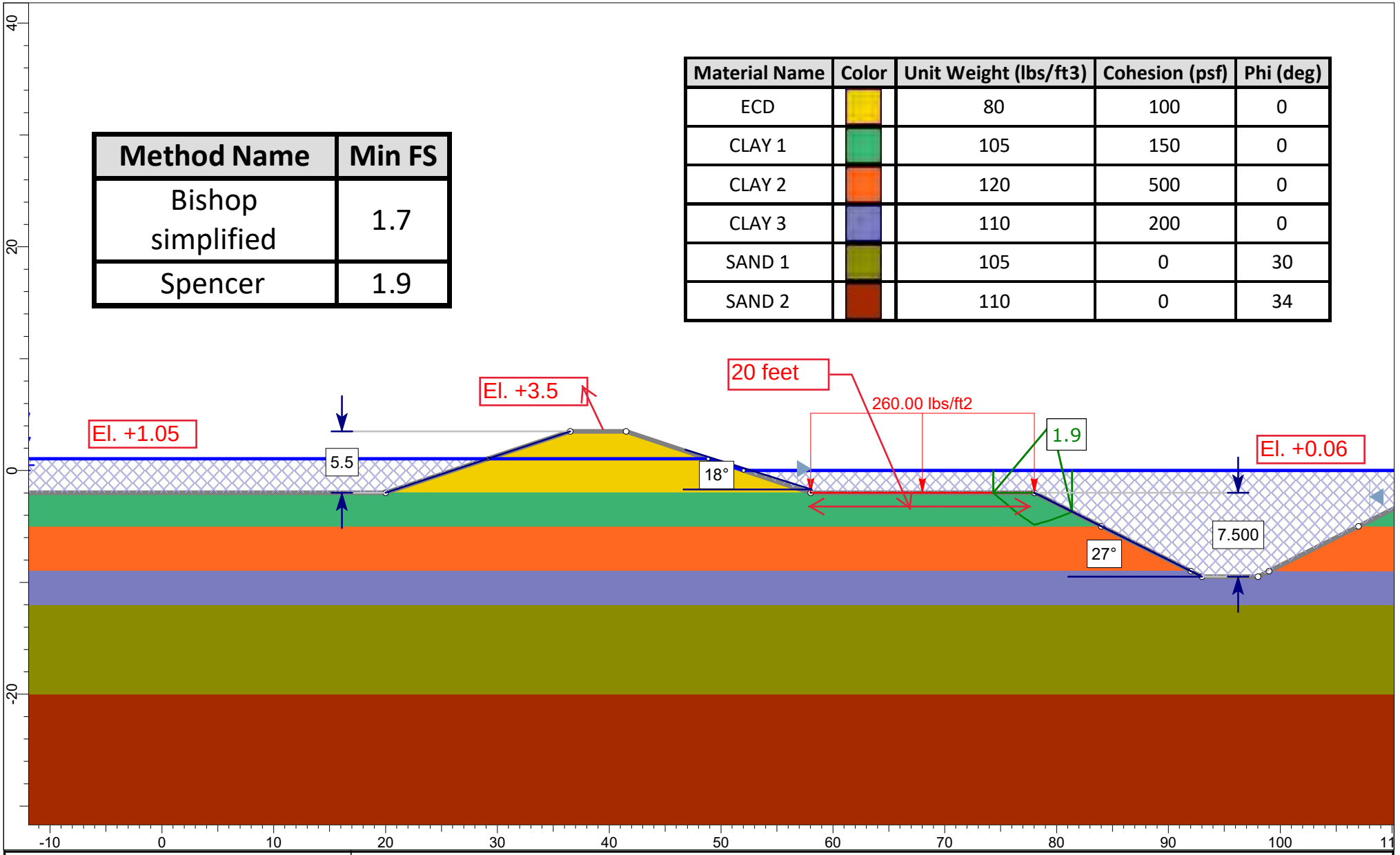
Project	PSI Report No. : 02541211, Long point Bayou Marsh Creation Project		
Group	A-1 GLobal	Scenario	Master Scenario
Drawn By	Intertek PSI	Company	
Date		File Name	ECD Slope-Case A-1 GLobal 3H 1V.slmd

Method Name	Min FS
Bishop simplified	1.7
Spencer	1.9

Material Name	Color	Unit Weight (lbs/ft3)	Cohesion (psf)	Phi (deg)
ECD		80	100	0
CLAY 1		105	150	0
CLAY 2		120	500	0
CLAY 3		110	200	0
SAND 1		105	0	30
SAND 2		110	0	34



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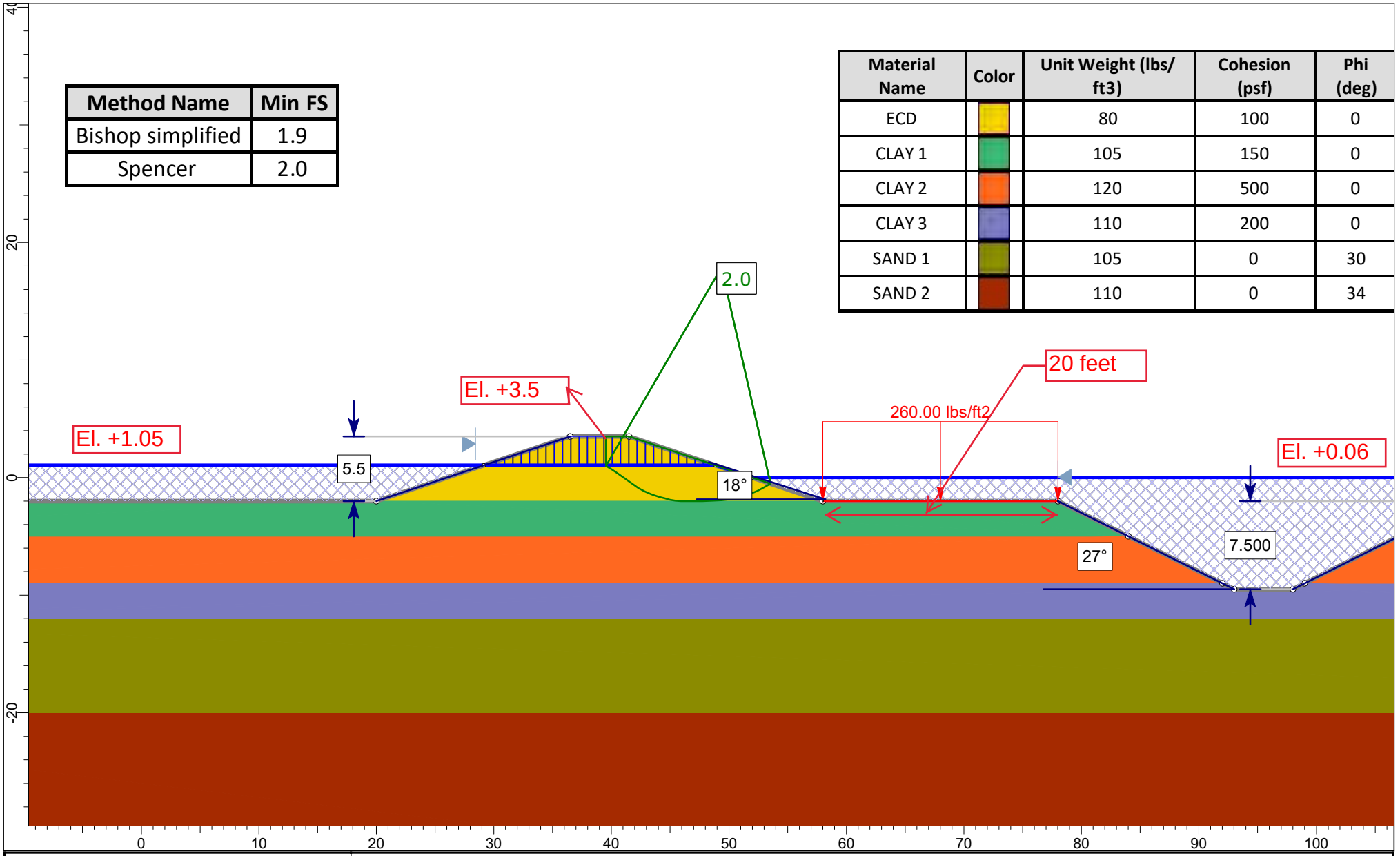
SLIDEINTERPRET 9.008

Project	PSI Report No. : 02541211, Long point Bayou Marsh Creation Project		
Group	A-2 Local	Scenario	Master Scenario
Drawn By	Intertek PSI	Company	
Date		File Name	ECD Slope-Case A-2 Local 3H 1V.slmd

Method Name	Min FS
Bishop simplified	1.9
Spencer	2.0

Material Name	Color	Unit Weight (lbs/ ft3)	Cohesion (psf)	Phi (deg)
ECD		80	100	0
CLAY 1		105	150	0
CLAY 2		120	500	0
CLAY 3		110	200	0
SAND 1		105	0	30
SAND 2		110	0	34



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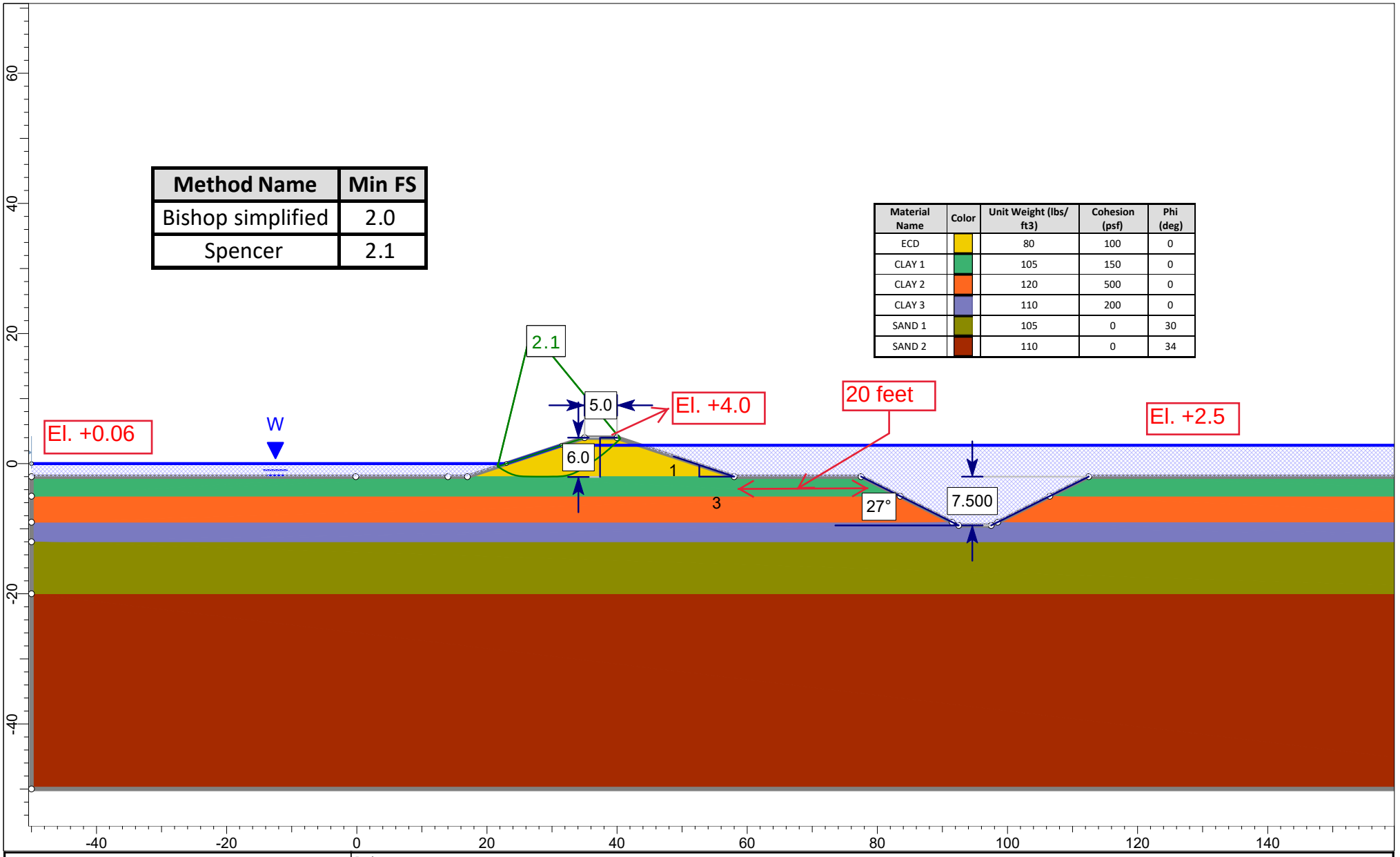
Project	PSI Report No. : 02541211, Long point Bayou Marsh Creation Project		
Group	A-1 Global-Tension Crack	Scenario	Master Scenario
Drawn By	Intertek PSI	Company	
Date		File Name	ECD Slope-Cases A-1 Global-Tension Crack 3H 1V.slmd

Top of Dike Elevation +4.0 feet (NAVD88-Geoid 18)



Material Name	Color	Unit Weight (lbs/ft3)	Cohesion (psf)	Phi (deg)
ECD		80	100	0
CLAY 1		105	150	0
CLAY 2		120	500	0
CLAY 3		110	200	0
SAND 1		105	0	30
SAND 2		110	0	34

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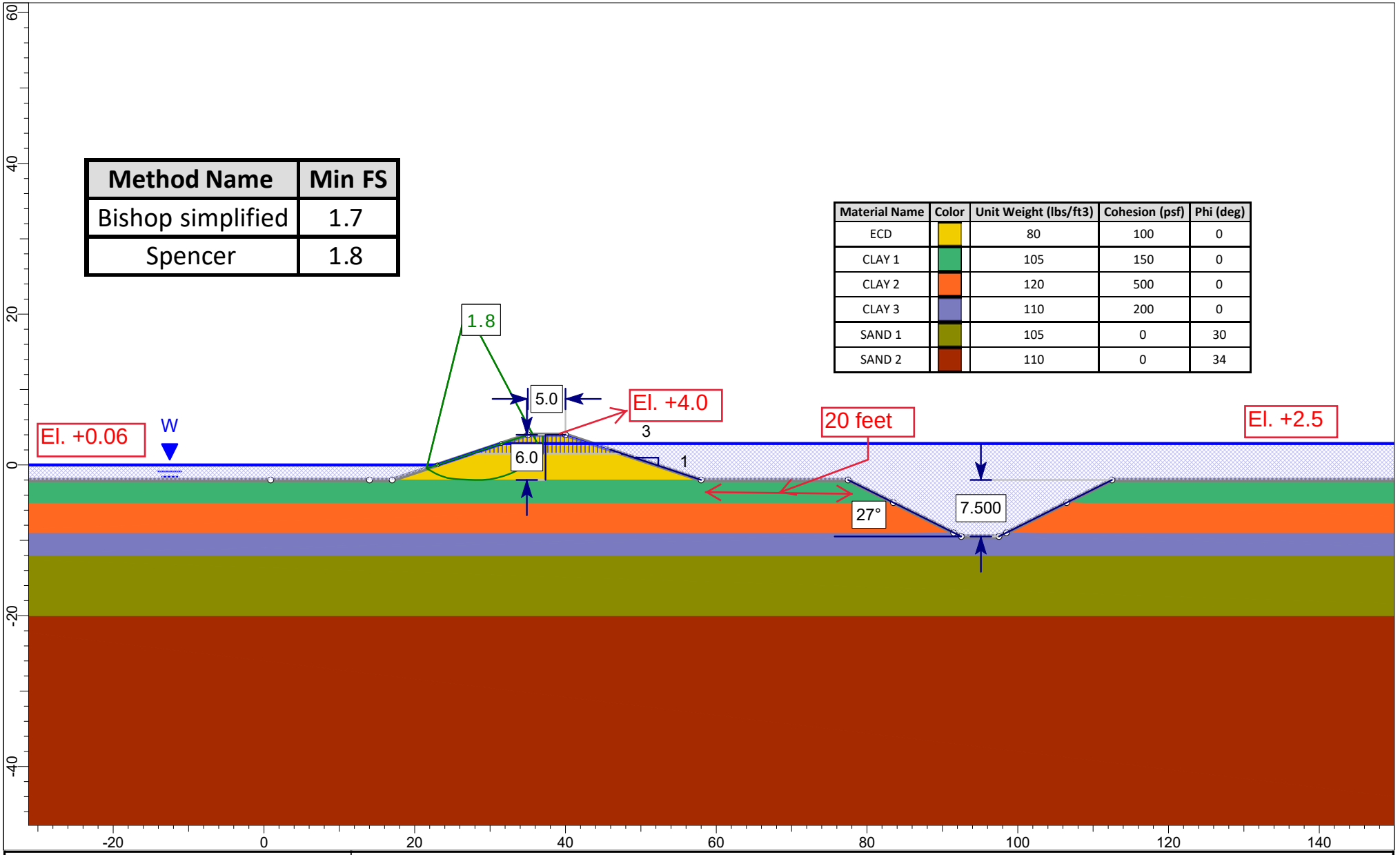
SLIDEINTERPRET 9.008

Project	PSI Report No. : 02541211-, Long point Bayou Marsh Creation Project		
Group	Case B	*Scenario*	Master Scenario
Drawn By		*Company*	Intertek PSI
Date		*File Name*	ECD Slope-Case B (C=100 psf) 3H 1V.slmd

Method Name	Min FS
Bishop simplified	1.7
Spencer	1.8

Material Name	Color	Unit Weight (lbs/ft3)	Cohesion (psf)	Phi (deg)
ECD		80	100	0
CLAY 1		105	150	0
CLAY 2		120	500	0
CLAY 3		110	200	0
SAND 1		105	0	30
SAND 2		110	0	34



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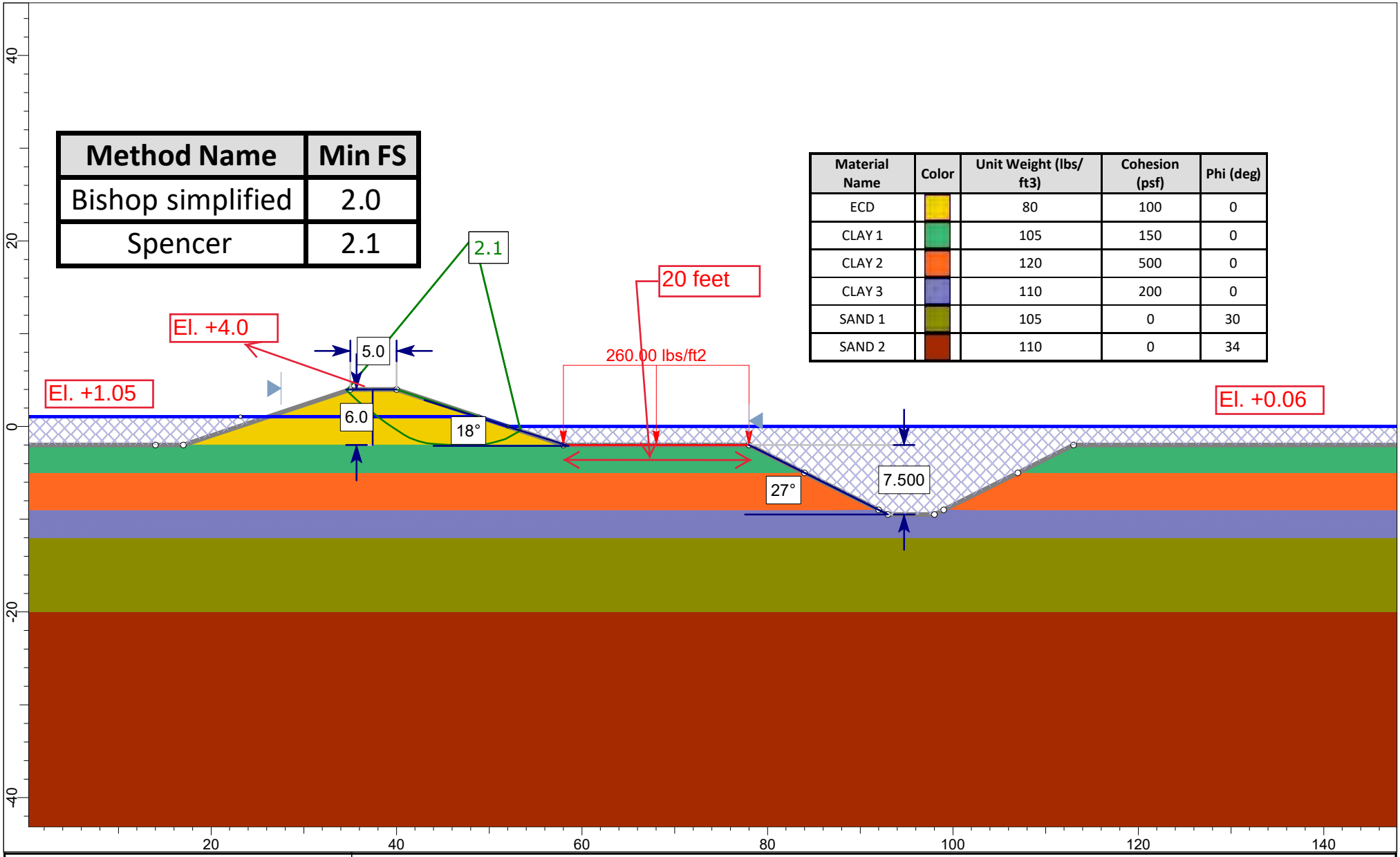
SLIDEINTERPRET 9.008

Project	PSI Report No. : 02541211-, Long point Bayou Marsh Creation Project		
Group	Case B- Tension Crack	Scenario	Master Scenario
Drawn By		Company	Intertek PSI
Date		File Name	ECD Slope-Case B (C=100 psf) 3H 1V.slmd

Method Name	Min FS
Bishop simplified	2.0
Spencer	2.1

Material Name	Color	Unit Weight (lbs/ft3)	Cohesion (psf)	Phi (deg)
ECD		80	100	0
CLAY 1		105	150	0
CLAY 2		120	500	0
CLAY 3		110	200	0
SAND 1		105	0	30
SAND 2		110	0	34



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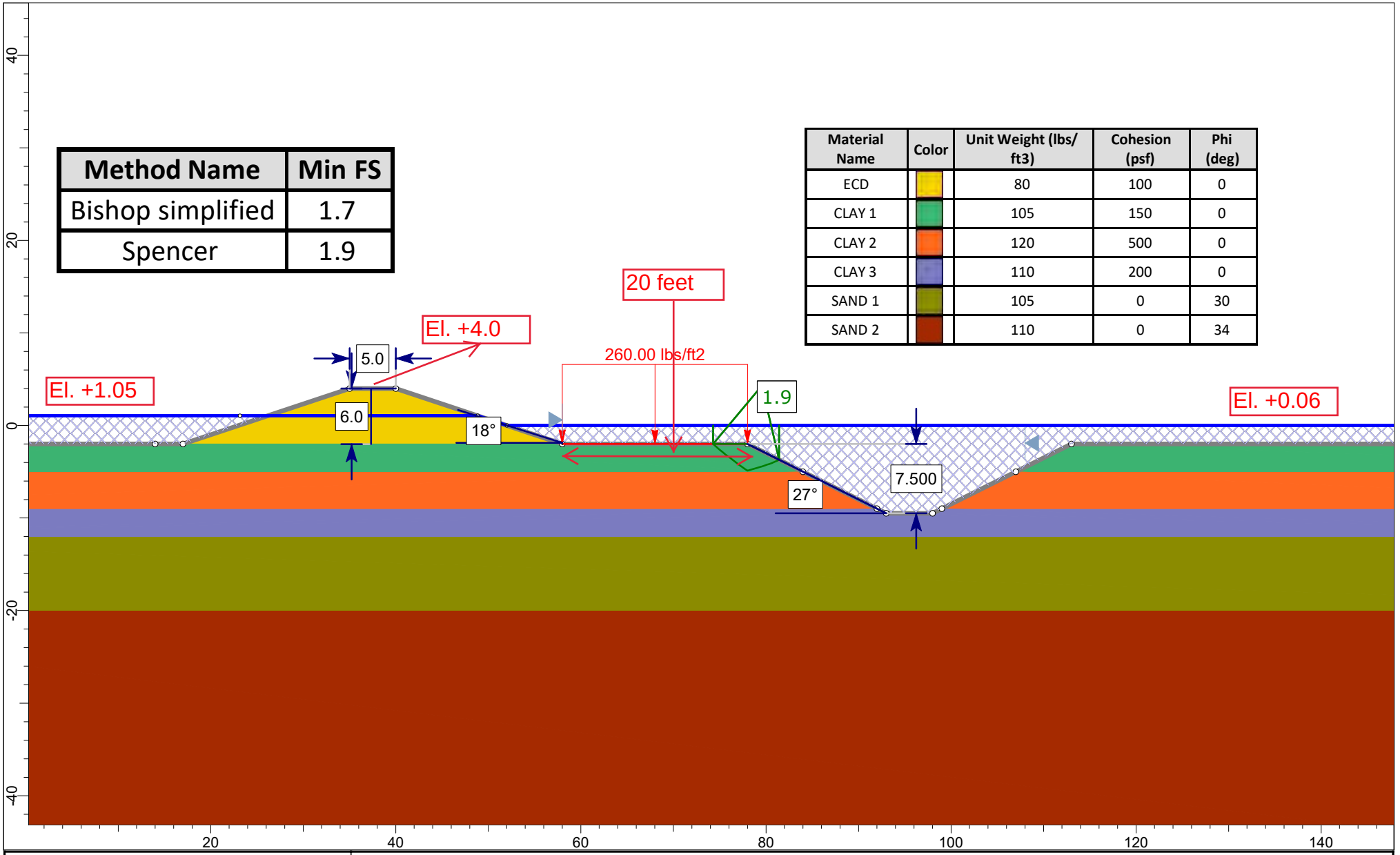
SLIDEINTERPRET 9.007

Project	PSI Report No. : 02541211, Long point Bayou Marsh Creation Project		
Group	A-1 GLobal	Scenario	Master Scenario
Drawn By	Intertek PSI	Company	
Date		File Name	ECD Slope-Cases A1 and A2 (C=100 psf) 3H 1V.slmd

Method Name	Min FS
Bishop simplified	1.7
Spencer	1.9

Material Name	Color	Unit Weight (lbs/ ft3)	Cohesion (psf)	Phi (deg)
ECD		80	100	0
CLAY 1		105	150	0
CLAY 2		120	500	0
CLAY 3		110	200	0
SAND 1		105	0	30
SAND 2		110	0	34



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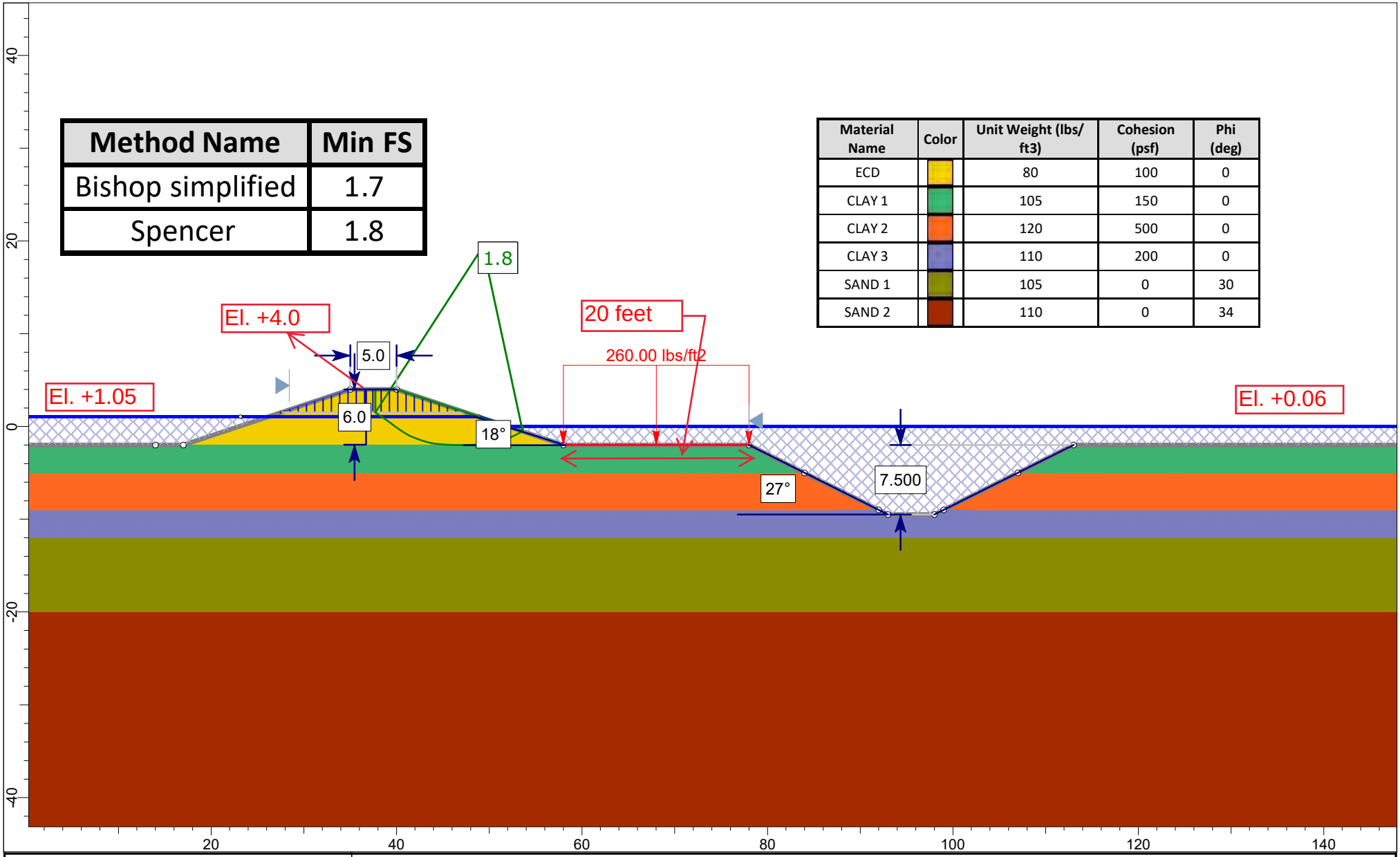
SLIDEINTERPRET 9.007

Project	PSI Report No. : 02541211, Long point Bayou Marsh Creation Project		
Group	A-2 Local	Scenario	Master Scenario
Drawn By	Intertek PSI	Company	
Date		File Name	ECD Slope-Cases A1 and A2 (C=100 psf) 3H 1V.slmd

Method Name	Min FS
Bishop simplified	1.7
Spencer	1.8

Material Name	Color	Unit Weight (lbs/ft3)	Cohesion (psf)	Phi (deg)
ECD		80	100	0
CLAY 1		105	150	0
CLAY 2		120	500	0
CLAY 3		110	200	0
SAND 1		105	0	30
SAND 2		110	0	34



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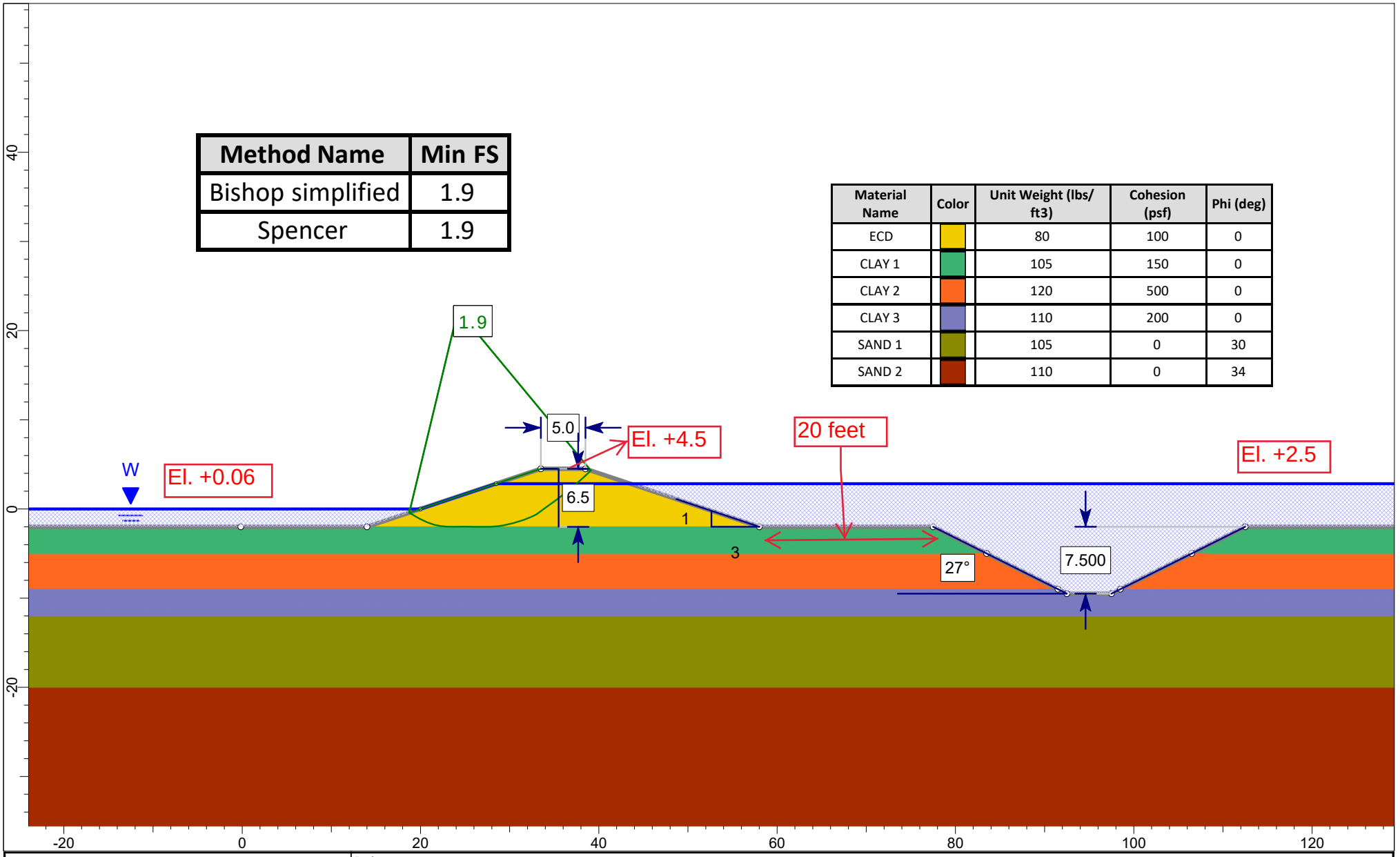
SLIDEINTERPRET 9.007

Project	PSI Report No. : 02541211, Long point Bayou Marsh Creation Project		
Group	A-1 Global-Tension Crack	Scenario	Master Scenario
Drawn By	Intertek PSI	Company	
Date		File Name	ECD Slope-Cases A1 and A2 (C=100 psf) 3H 1V.slmd

Top of Dike Elevation +4.5 feet (NAVD88-Geoid 18)

Method Name	Min FS
Bishop simplified	1.9
Spencer	1.9

Material Name	Color	Unit Weight (lbs/ ft3)	Cohesion (psf)	Phi (deg)
ECD		80	100	0
CLAY 1		105	150	0
CLAY 2		120	500	0
CLAY 3		110	200	0
SAND 1		105	0	30
SAND 2		110	0	34



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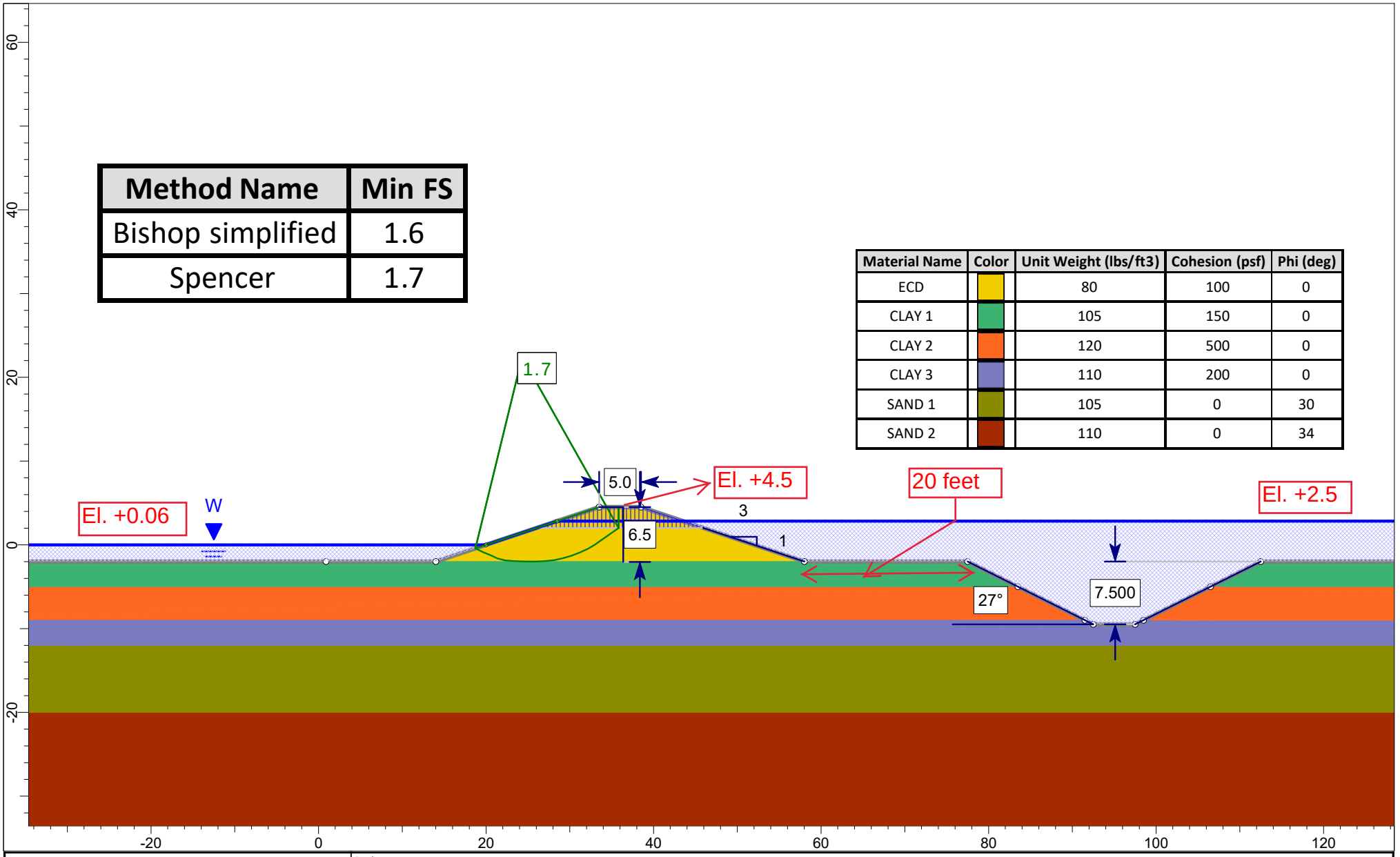
SLIDEINTERPRET 9.008

Project	PSI Report No. : 02541211-, Long point Bayou Marsh Creation Project		
Group	Case B	Scenario	Master Scenario
Drawn By		Company	Intertek PSI
Date		File Name	ECD Slope-Case B (C=100 psf) 3H 1V.slmd

Method Name	Min FS
Bishop simplified	1.6
Spencer	1.7

Material Name	Color	Unit Weight (lbs/ft3)	Cohesion (psf)	Phi (deg)
ECD		80	100	0
CLAY 1		105	150	0
CLAY 2		120	500	0
CLAY 3		110	200	0
SAND 1		105	0	30
SAND 2		110	0	34



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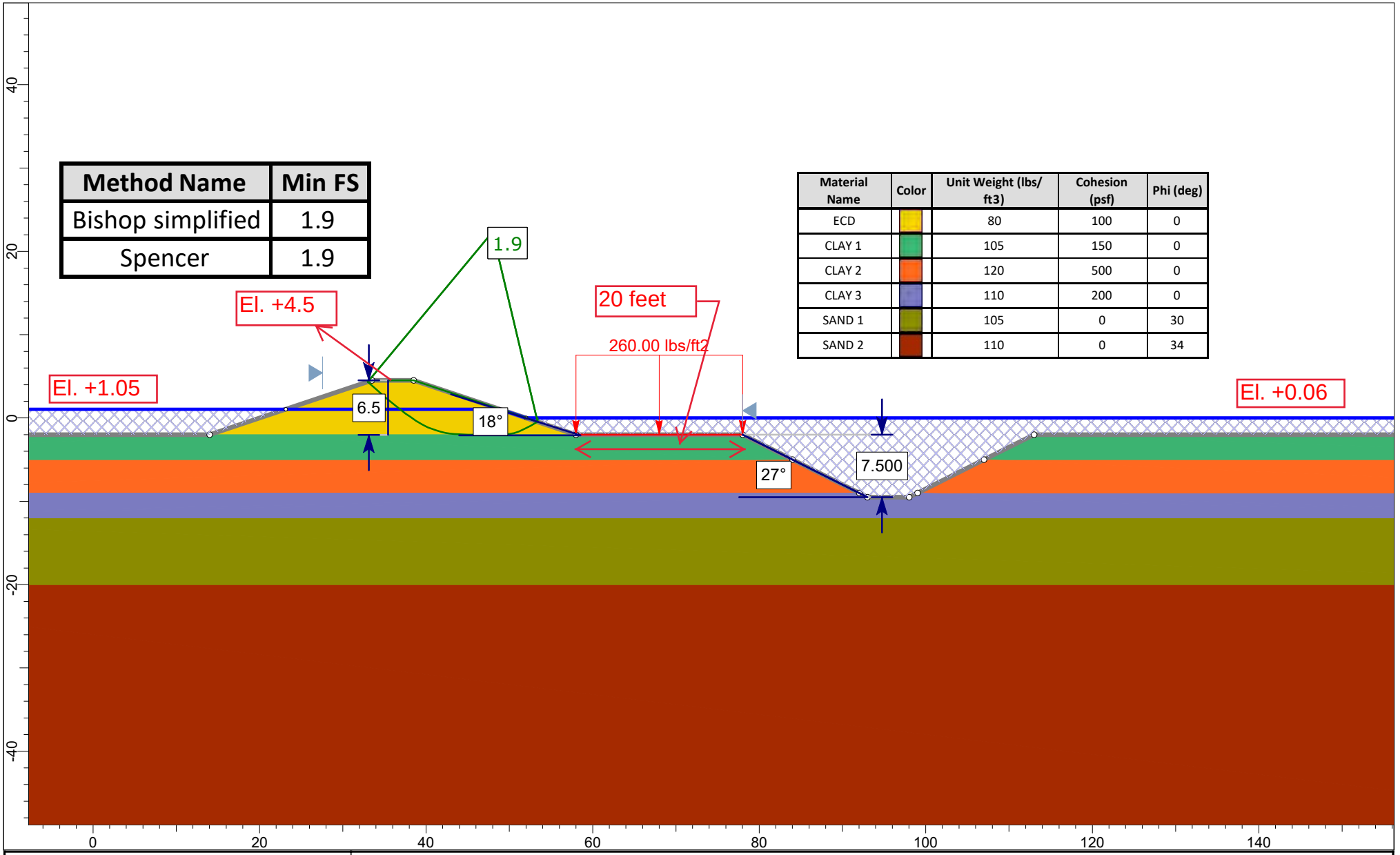
SLIDEINTERPRET 9.008

Project	PSI Report No. : 02541211-, Long point Bayou Marsh Creation Project		
Group	Case B- Tension Crack	Scenario	Master Scenario
Drawn By		Company	Intertek PSI
Date		File Name	ECD Slope-Case B (C=100 psf) 3H 1V.slmd



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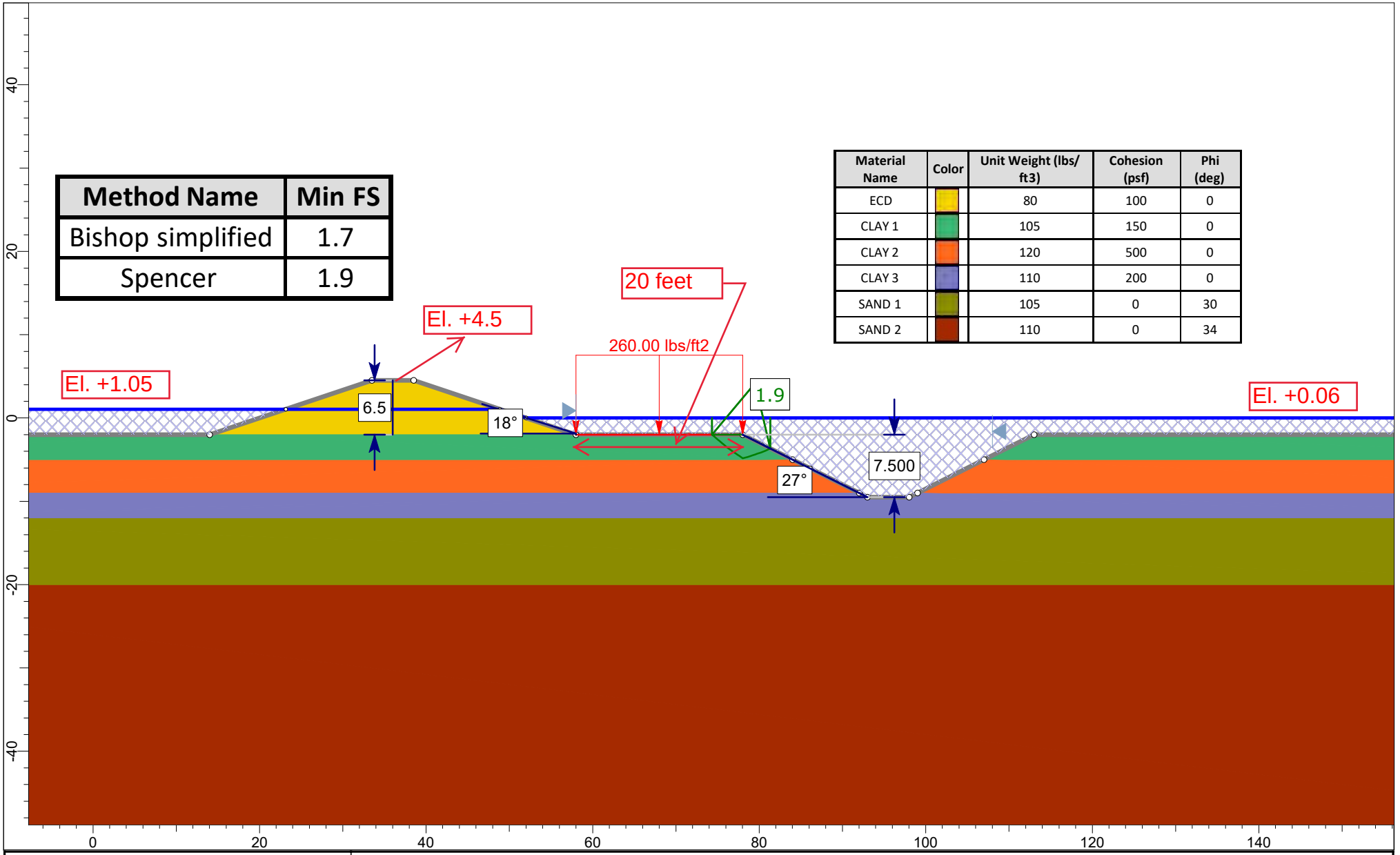
SLIDEINTERPRET 9.007

Project	PSI Report No. : 02541211, Long point Bayou Marsh Creation Project		
Group	A-1 GLobal	*Scenario*	Master Scenario
Drawn By	Intertek PSI	*Company*	
Date		*File Name*	ECD Slope-Cases A1 and A2 (C=100 psf) 3H 1V.slmd



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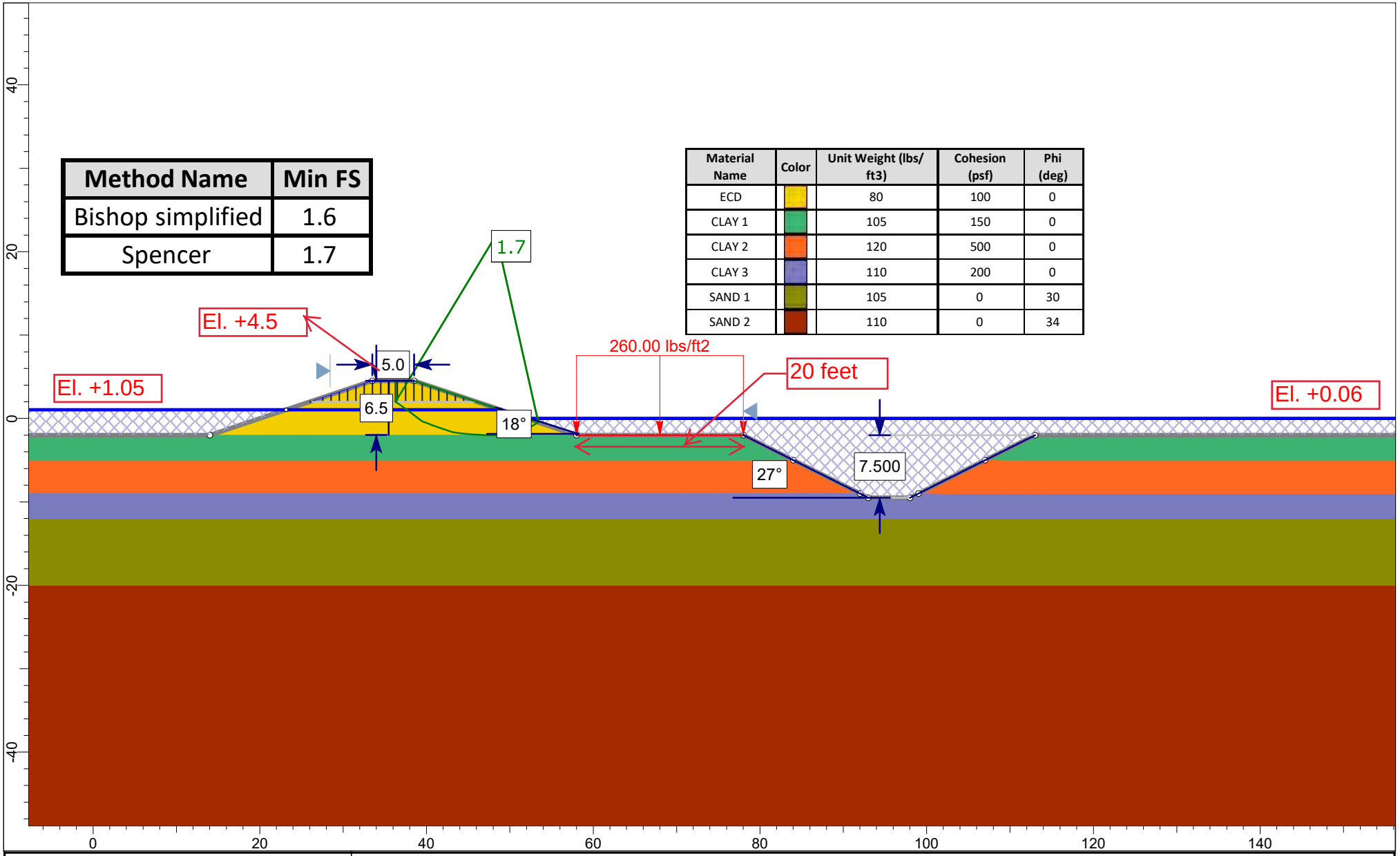
SLIDEINTERPRET 9.007

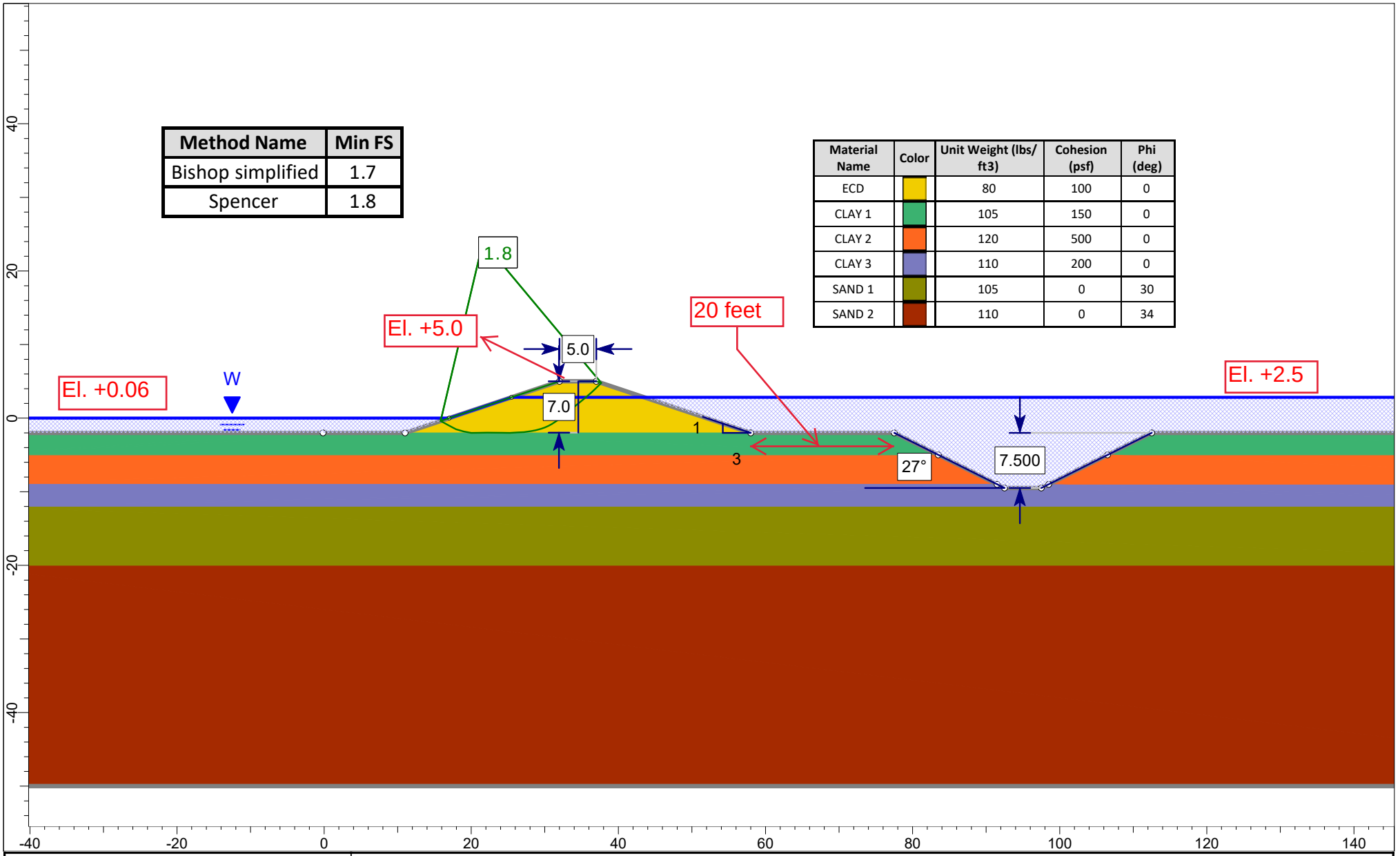
Project	PSI Report No. : 02541211, Long point Bayou Marsh Creation Project		
Group	A-2 Local	Scenario	Master Scenario
Drawn By	Intertek PSI	Company	
Date		File Name	ECD Slope-Cases A1 and A2 (C=100 psf) 3H 1V.slmd



rocscience	Project	PSI Report No. : 02541211, Long point Bayou Marsh Creation Project	
	Group	A-1 Global-Tension Crack	Scenario: Master Scenario
	Drawn By	Intertek PSI	Company
	Date		File Name: ECD Slope-Cases A1 and A2 (C=100 psf) 3H 1V.slmd

SLIDEINTERPRET 9.007

Top of Dike Elevation +5.0 feet (NAVD88-Geoid 18)



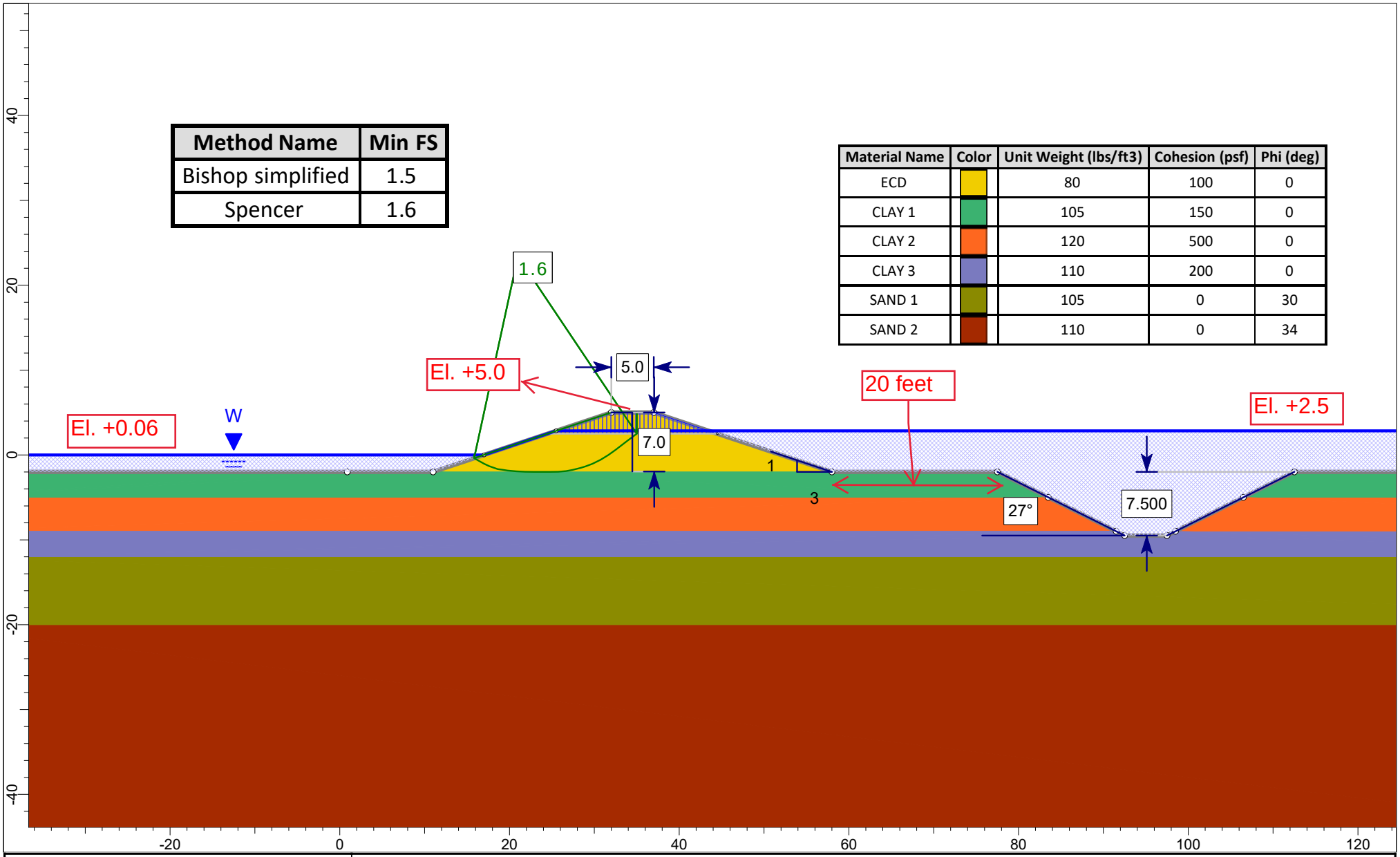
rocscience

SLIDEINTERPRET 9.008

Project	PSI Report No. : 02541211-, Long point Bayou Marsh Creation Project		
Group	Case B	*Scenario*	Master Scenario
Drawn By		*Company*	Intertek PSI
Date		*File Name*	ECD Slope-Case B (C=100 psf) 3H 1V.slmd

Method Name	Min FS
Bishop simplified	1.5
Spencer	1.6

Material Name	Color	Unit Weight (lbs/ft3)	Cohesion (psf)	Phi (deg)
ECD		80	100	0
CLAY 1		105	150	0
CLAY 2		120	500	0
CLAY 3		110	200	0
SAND 1		105	0	30
SAND 2		110	0	34



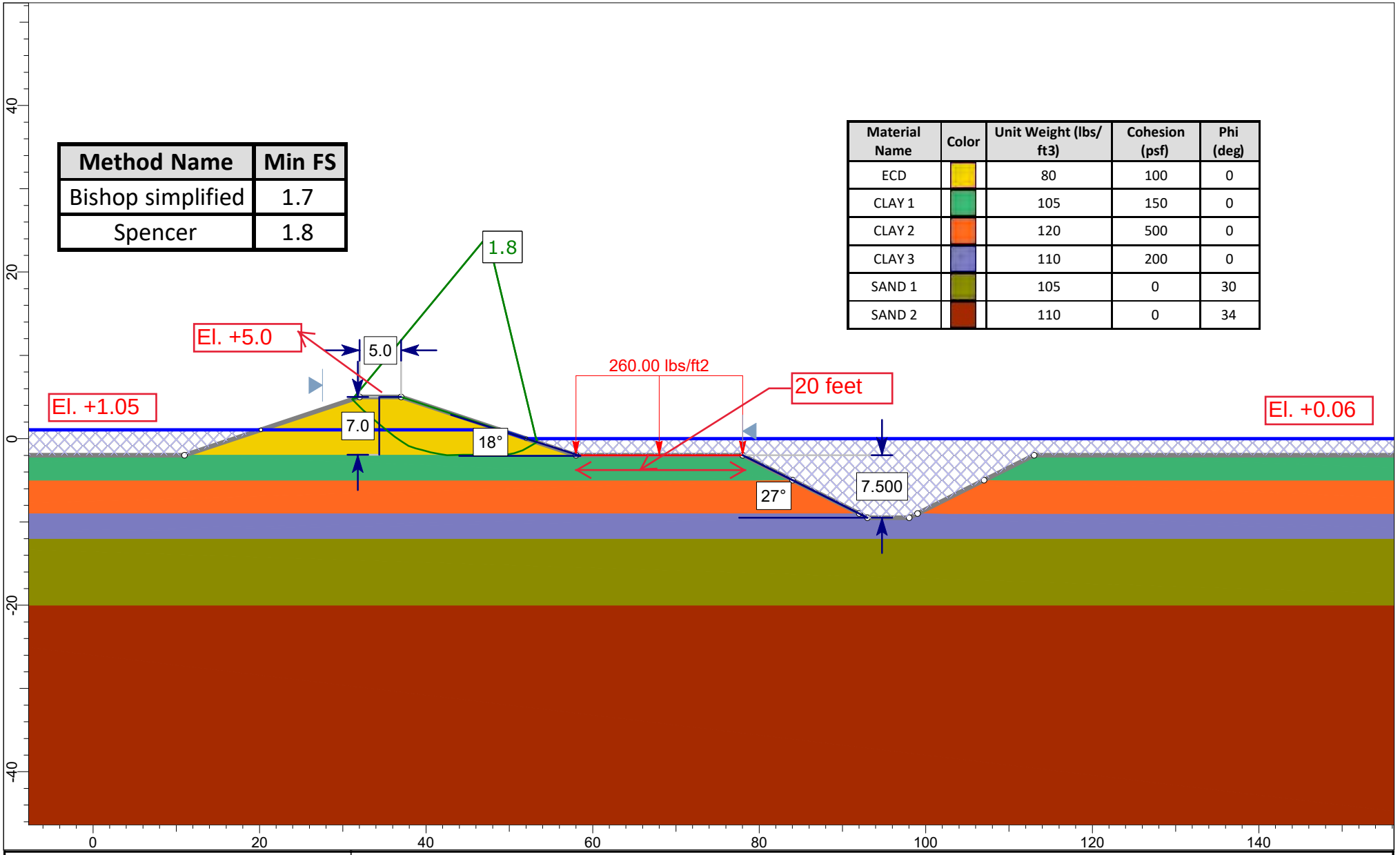
rocscience

SLIDEINTERPRET 9.008

Project	PSI Report No. : 02541211-, Long point Bayou Marsh Creation Project		
Group	Case B- Tension Crack	Scenario	Master Scenario
Drawn By		Company	Intertek PSI
Date		File Name	ECD Slope-Case B (C=100 psf) 3H 1V.slmd

Method Name	Min FS
Bishop simplified	1.7
Spencer	1.8

Material Name	Color	Unit Weight (lbs/ft3)	Cohesion (psf)	Phi (deg)
ECD		80	100	0
CLAY 1		105	150	0
CLAY 2		120	500	0
CLAY 3		110	200	0
SAND 1		105	0	30
SAND 2		110	0	34



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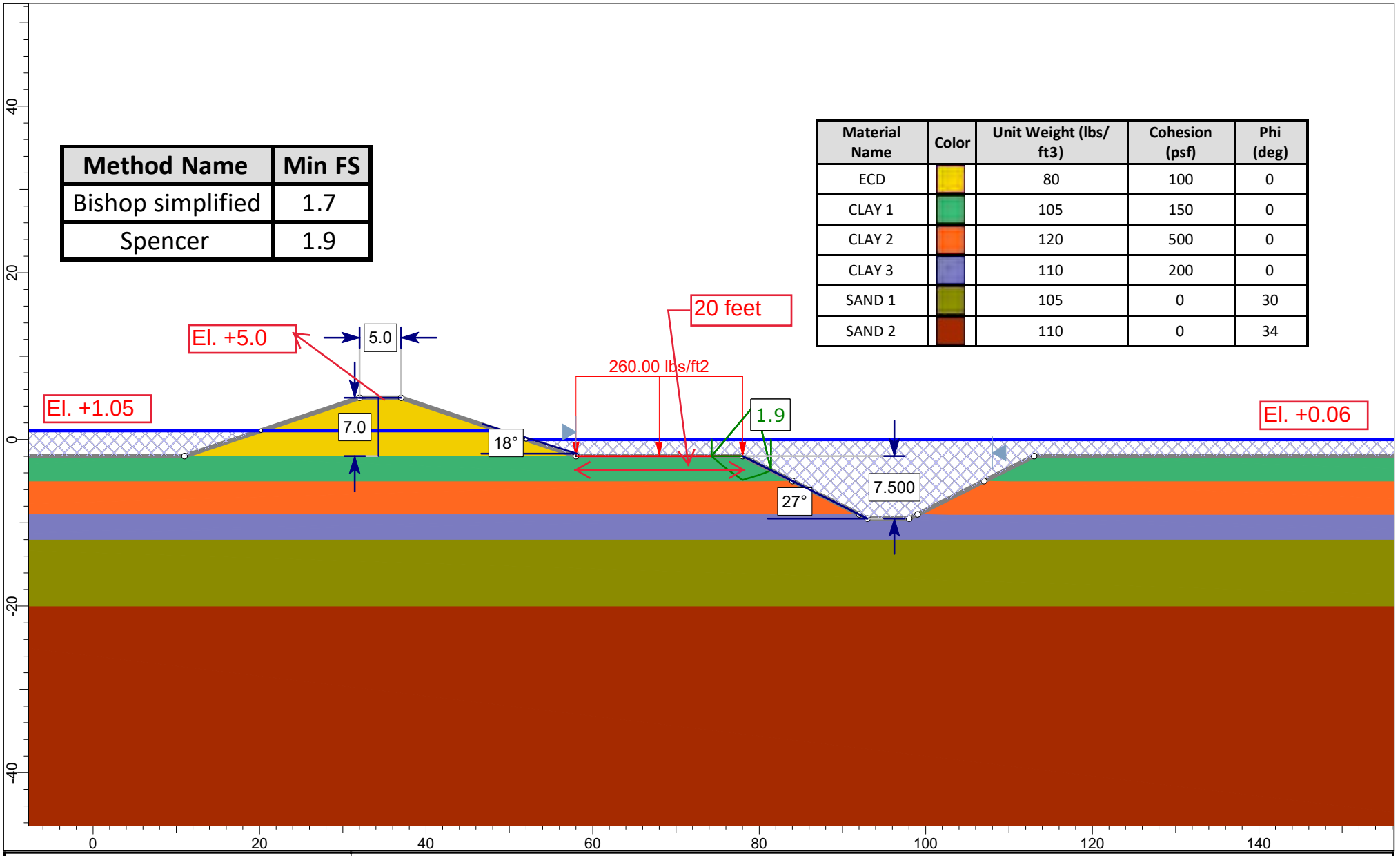
SLIDEINTERPRET 9.007

Project	PSI Report No. : 02541211, Long point Bayou Marsh Creation Project		
Group	A-1 GLobal	Scenario	Master Scenario
Drawn By	Intertek PSI	Company	
Date		File Name	ECD Slope-Cases A1 and A2 (C=100 psf) 3H 1V.slmd

Method Name	Min FS
Bishop simplified	1.7
Spencer	1.9

Material Name	Color	Unit Weight (lbs/ft3)	Cohesion (psf)	Phi (deg)
ECD		80	100	0
CLAY 1		105	150	0
CLAY 2		120	500	0
CLAY 3		110	200	0
SAND 1		105	0	30
SAND 2		110	0	34



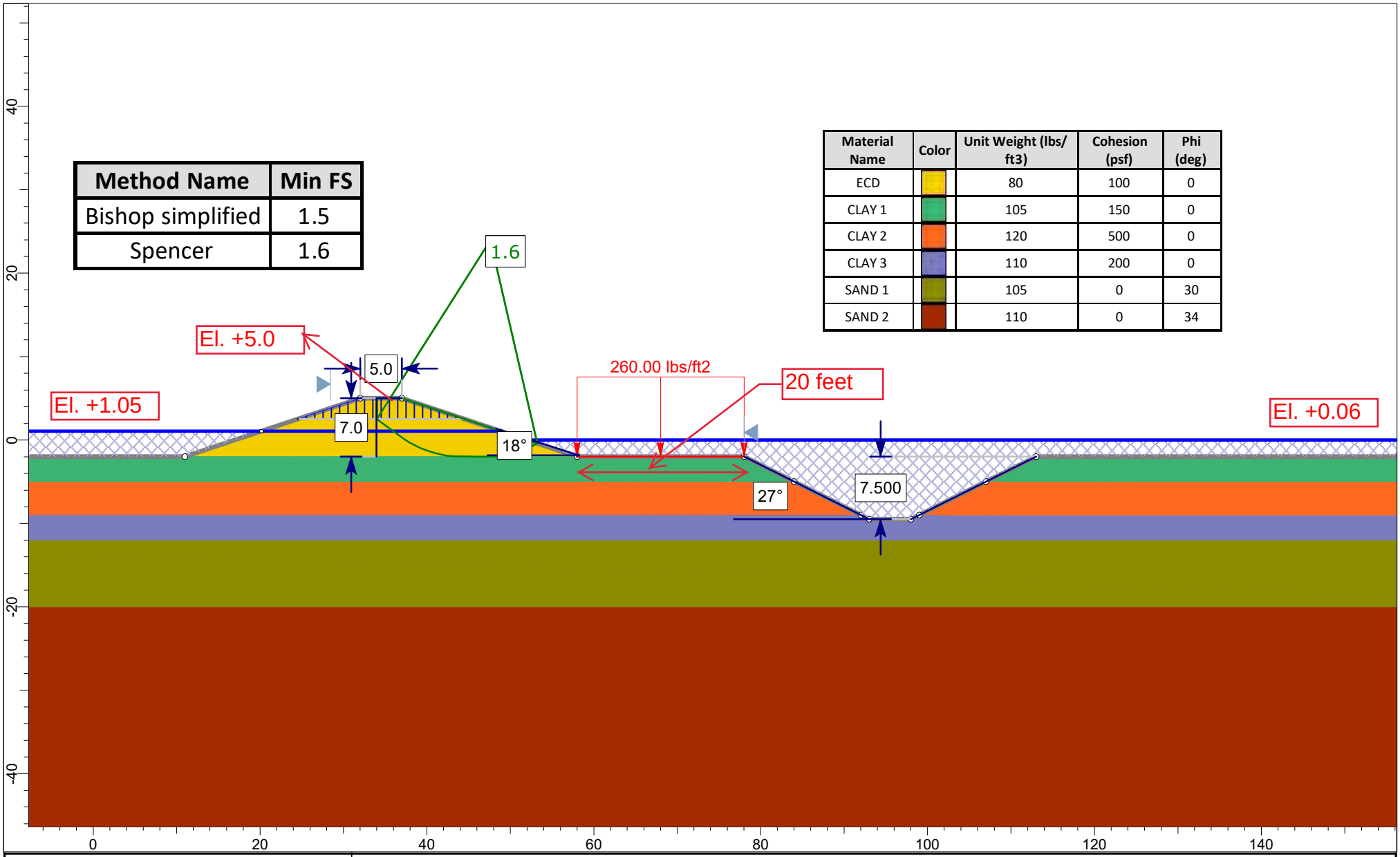
rocscience

SLIDEINTERPRET 9.007

Project	PSI Report No. : 02541211, Long point Bayou Marsh Creation Project		
Group	A-2 Local	Scenario	Master Scenario
Drawn By	Intertek PSI	Company	
Date		File Name	ECD Slope-Cases A1 and A2 (C=100 psf) 3H 1V.slmd

Method Name	Min FS
Bishop simplified	1.5
Spencer	1.6

Material Name	Color	Unit Weight (lbs/ft3)	Cohesion (psf)	Phi (deg)
ECD		80	100	0
CLAY 1		105	150	0
CLAY 2		120	500	0
CLAY 3		110	200	0
SAND 1		105	0	30
SAND 2		110	0	34



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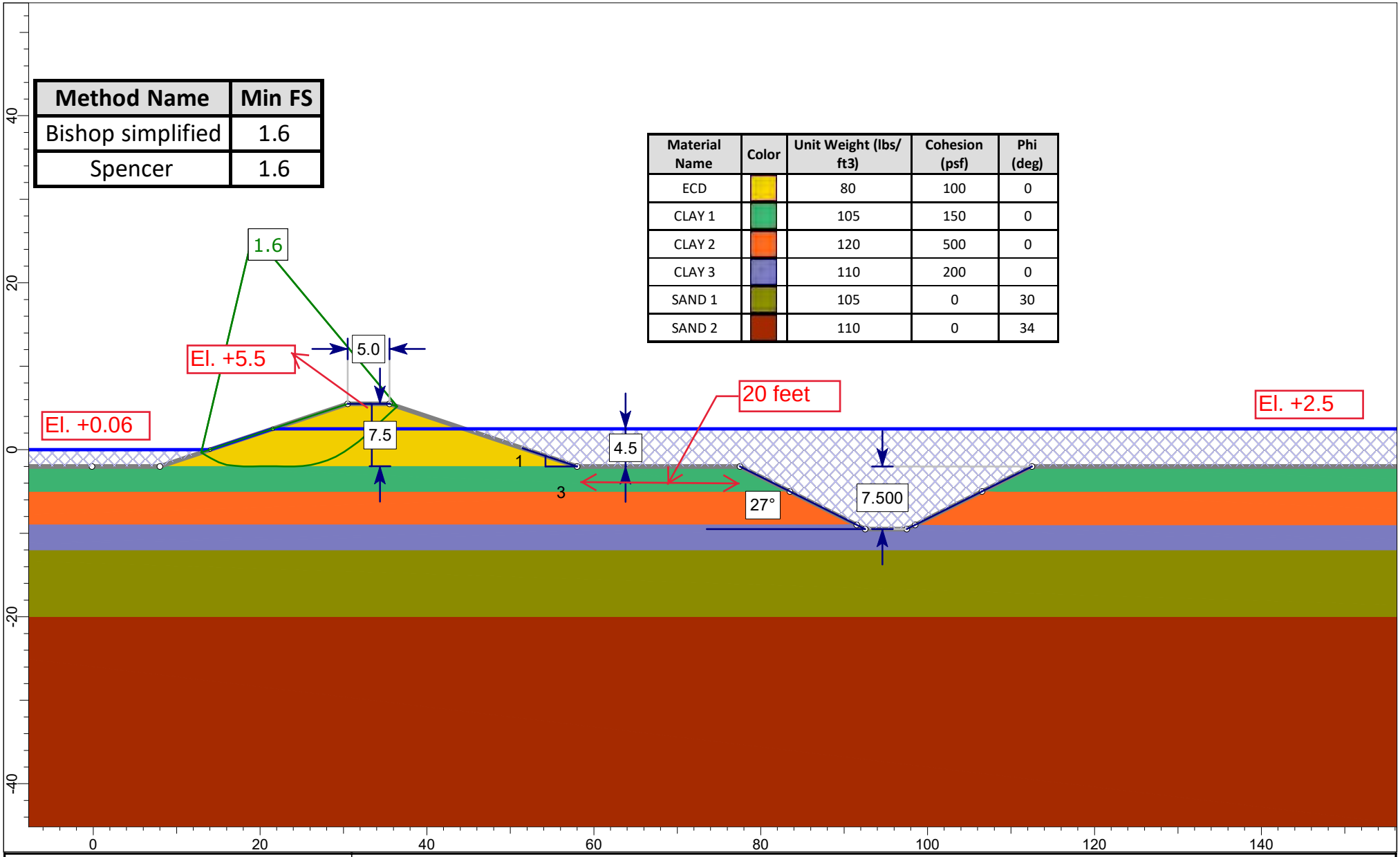
SLIDEINTERPRET 9.007

Project	PSI Report No. : 02541211, Long point Bayou Marsh Creation Project		
Group	A-1 Global-Tension Crack	Scenario	Master Scenario
Drawn By	Intertek PSI	Company	
Date		File Name	ECD Slope-Cases A1 and A2 (C=100 psf) 3H 1V.slmd

Top of Dike Elevation +5.5 feet (NAVD88-Geoid 18)

Method Name	Min FS
Bishop simplified	1.6
Spencer	1.6

Material Name	Color	Unit Weight (lbs/ft3)	Cohesion (psf)	Phi (deg)
ECD		80	100	0
CLAY 1		105	150	0
CLAY 2		120	500	0
CLAY 3		110	200	0
SAND 1		105	0	30
SAND 2		110	0	34



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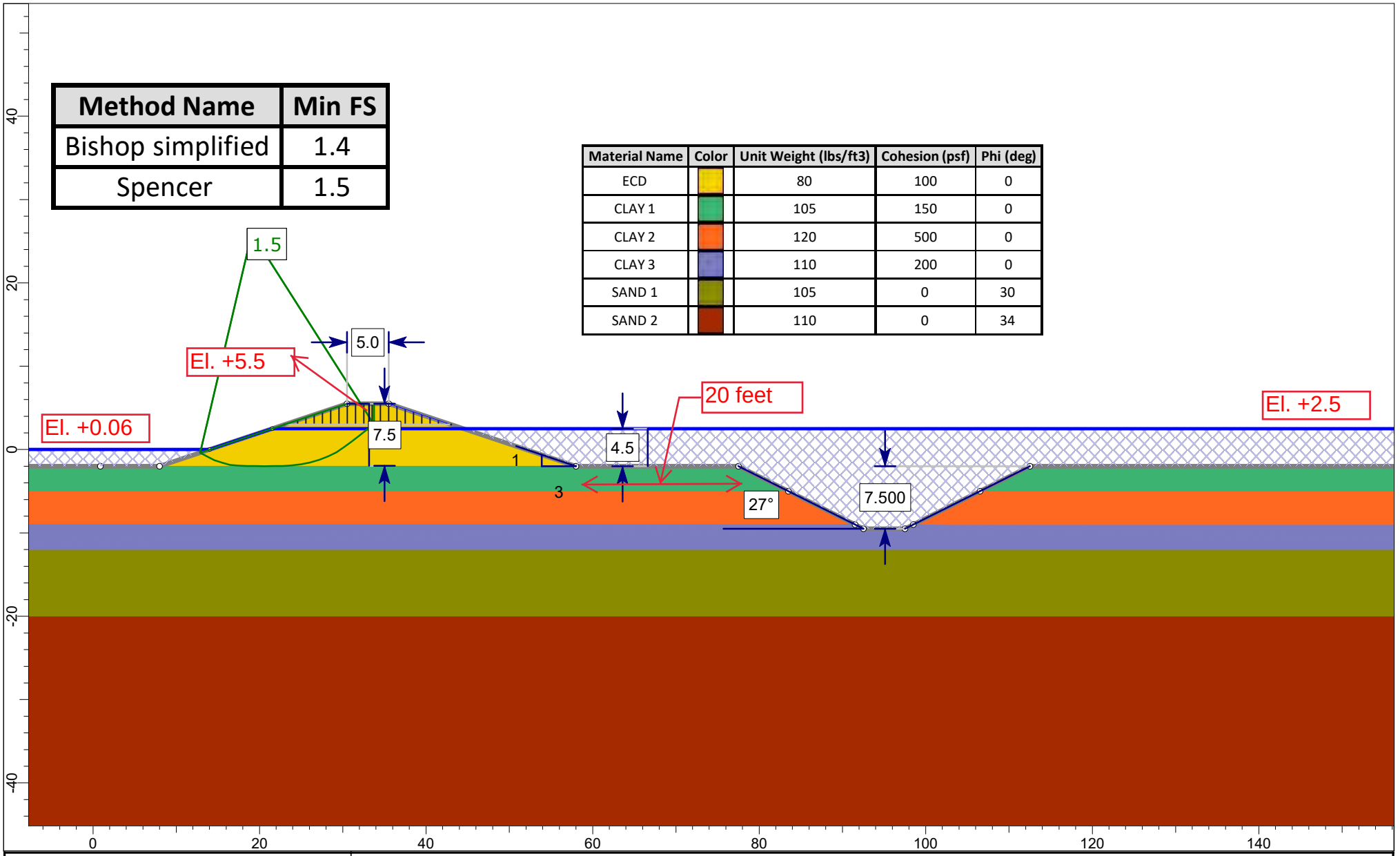
SLIDEINTERPRET 9.007

Project	PSI Report No. : 02541211-, Long point Bayou Marsh Creation Project		
Group	Case B	Scenario	Master Scenario
Drawn By		Company	Intertek PSI
Date		File Name	ECD Slope-Case B (C=100 psf) 3H 1V.slmd

Method Name	Min FS
Bishop simplified	1.4
Spencer	1.5

Material Name	Color	Unit Weight (lbs/ft3)	Cohesion (psf)	Phi (deg)
ECD		80	100	0
CLAY 1		105	150	0
CLAY 2		120	500	0
CLAY 3		110	200	0
SAND 1		105	0	30
SAND 2		110	0	34



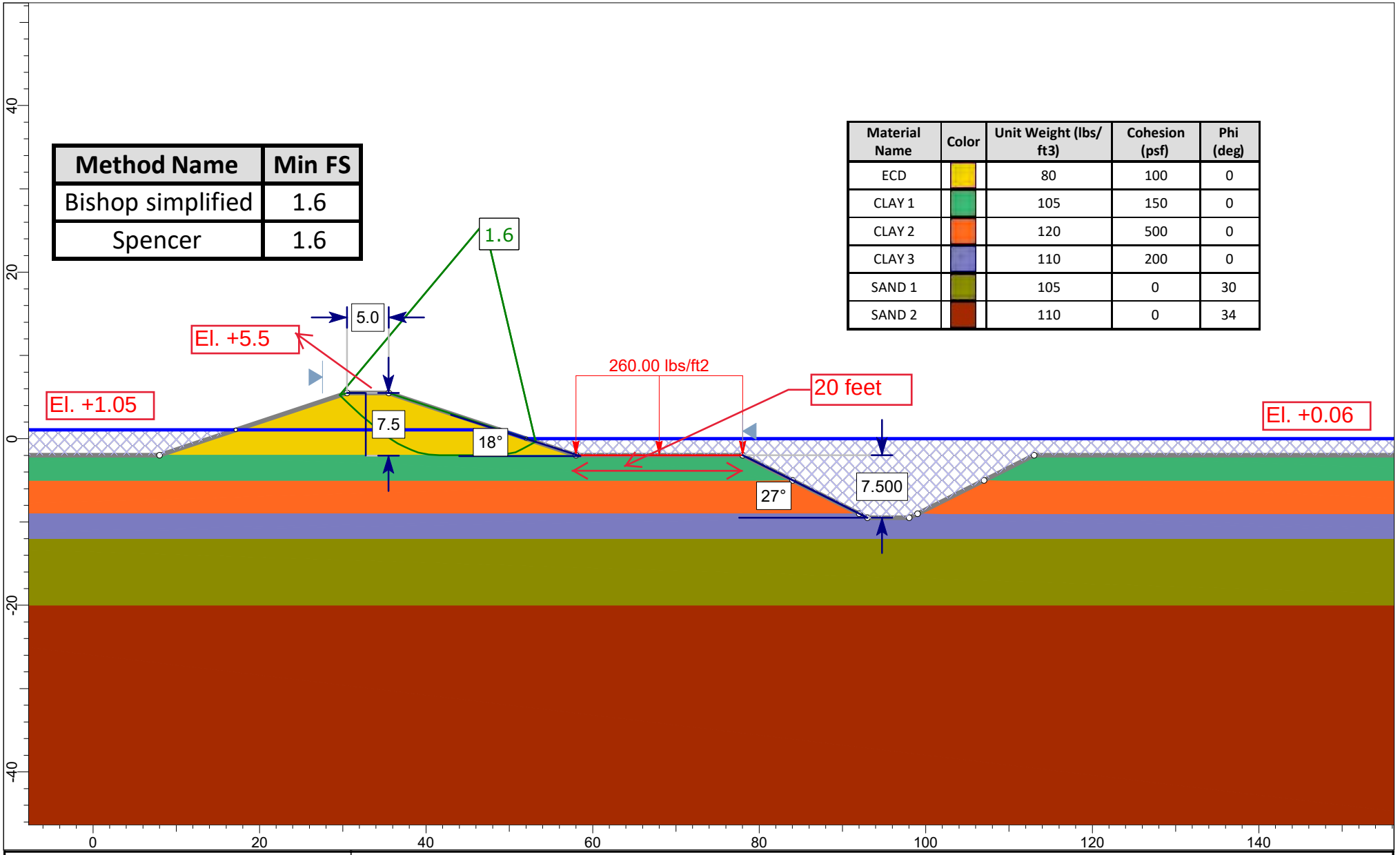
rocscience

SLIDEINTERPRET 9.007

Project	PSI Report No. : 02541211-, Long point Bayou Marsh Creation Project		
Group	Case B- Tension Crack	Scenario	Master Scenario
Drawn By		Company	Intertek PSI
Date		File Name	ECD Slope-Case B (C=100 psf) 3H 1V.slmd

Method Name	Min FS
Bishop simplified	1.6
Spencer	1.6

Material Name	Color	Unit Weight (lbs/ft3)	Cohesion (psf)	Phi (deg)
ECD		80	100	0
CLAY 1		105	150	0
CLAY 2		120	500	0
CLAY 3		110	200	0
SAND 1		105	0	30
SAND 2		110	0	34



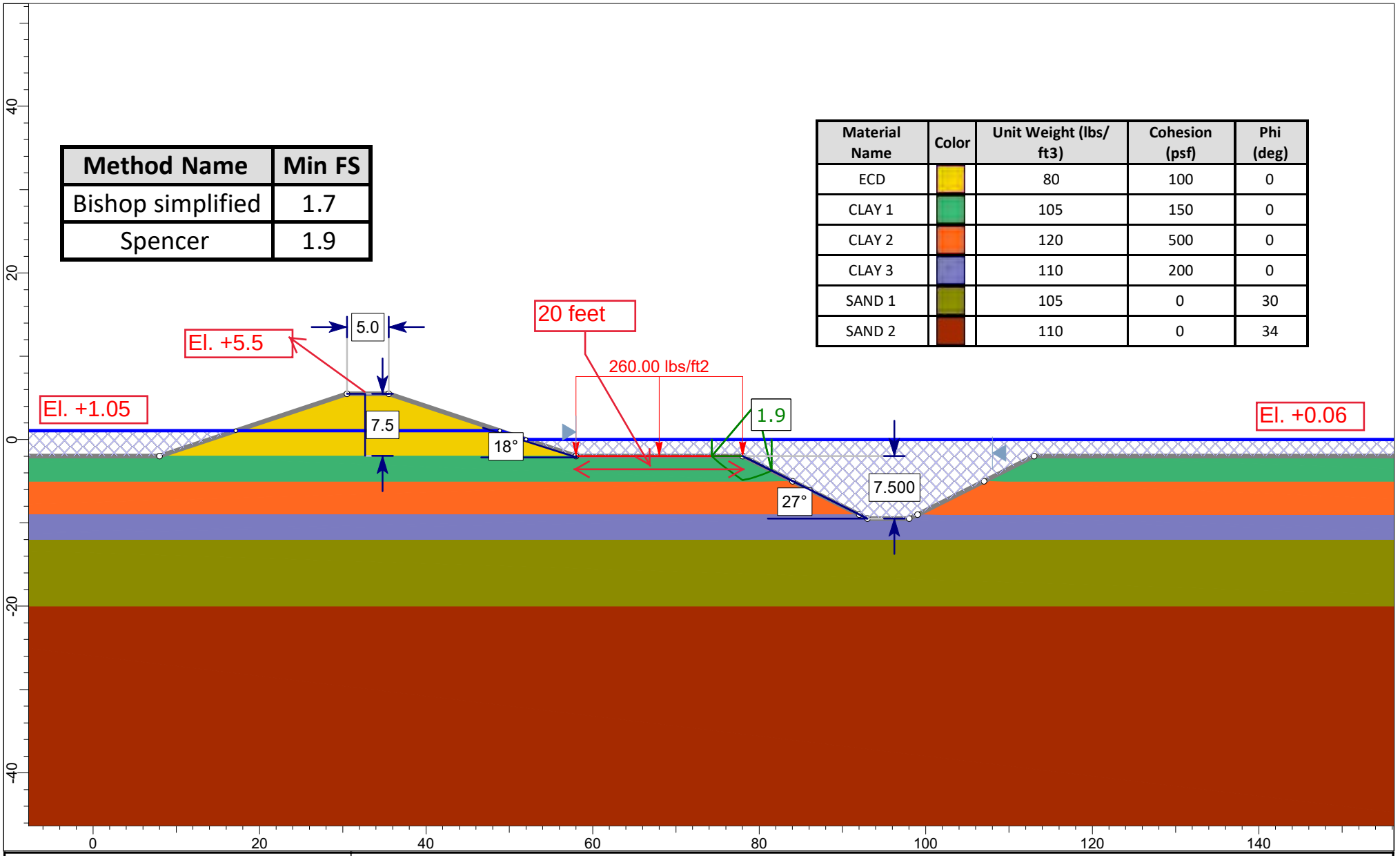
rocscience

SLIDEINTERPRET 9.007

Project	PSI Report No. : 02541211, Long point Bayou Marsh Creation Project		
Group	A-1 GLobal	Scenario	Master Scenario
Drawn By	Intertek PSI	Company	
Date		File Name	ECD Slope-Cases A1 and A2 (C=100 psf) 3H 1V.slmd

Method Name	Min FS
Bishop simplified	1.7
Spencer	1.9

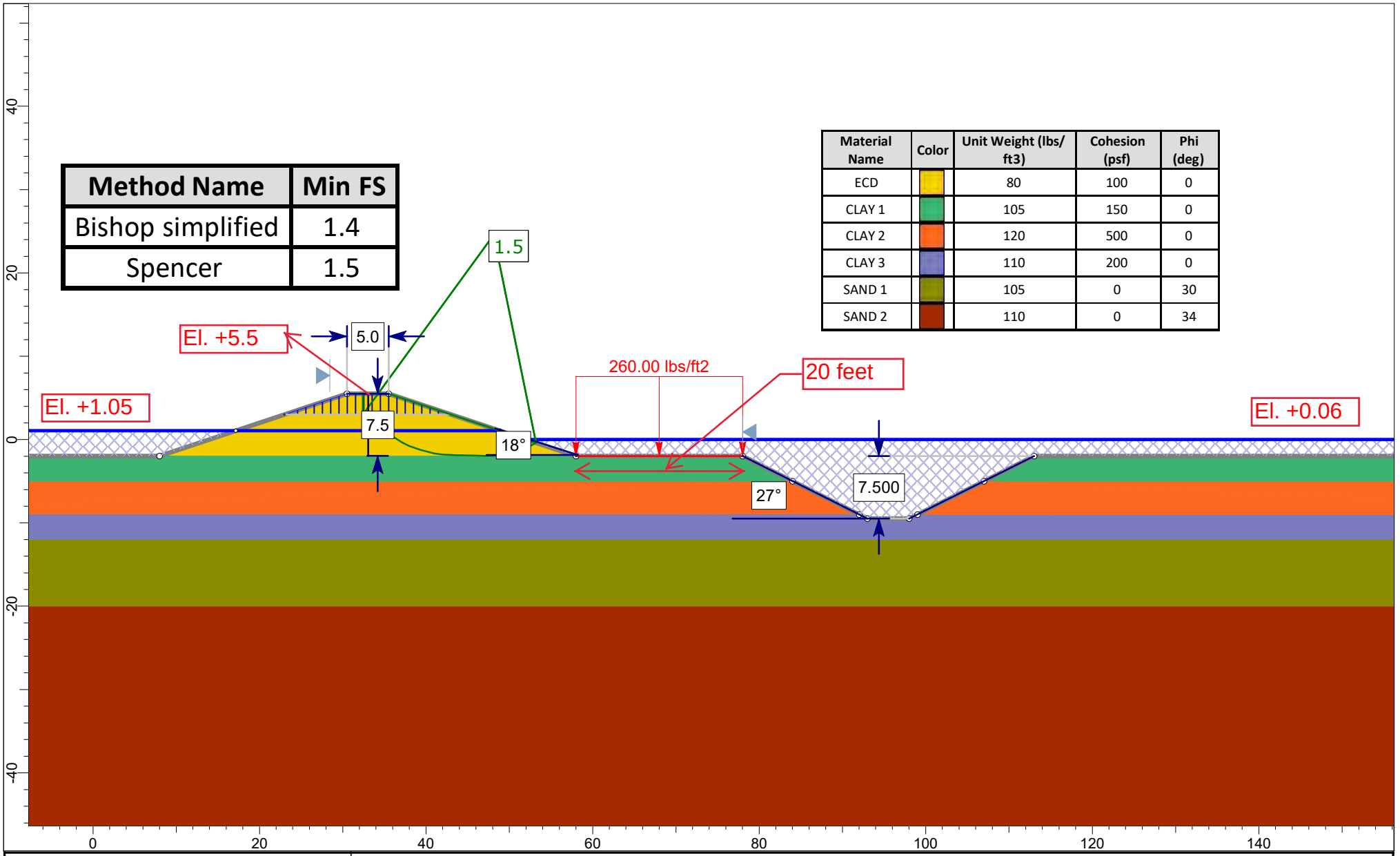
Material Name	Color	Unit Weight (lbs/ft3)	Cohesion (psf)	Phi (deg)
ECD		80	100	0
CLAY 1		105	150	0
CLAY 2		120	500	0
CLAY 3		110	200	0
SAND 1		105	0	30
SAND 2		110	0	34



rocscience

SLIDEINTERPRET 9.007

Project	PSI Report No. : 02541211, Long point Bayou Marsh Creation Project		
Group	A-2 Local	Scenario	Master Scenario
Drawn By	Intertek PSI	Company	
Date		File Name	ECD Slope-Cases A1 and A2 (C=100 psf) 3H 1V.slmd



rocscience	Project	PSI Report No. : 02541211, Long point Bayou Marsh Creation Project	
	Group	A-1 Global-Tension Crack	Scenario: Master Scenario
	Drawn By	Intertek PSI	Company
	Date		File Name: ECD Slope-Cases A1 and A2 (C=100 psf) 3H 1V.slmd

SLIDEINTERPRET 9.007

APPENDIX F

SETTLEMENT ANALYSES CONTAINMENT DIKES

Settle3 Analysis Information
Long point Bayou Marsh

Project Settings

Document Name	ECD Embankment 3H 1V , Dike height 6 ft
Project Title	Long point Bayou Marsh
Analysis	ECD Settlement
Company	Intertek PSI
Stress Computation Method	Boussinesq
Time-dependent Consolidation Analysis	
Time Units	days
Permeability Units	feet/year
Minimum settlement ratio for subgrade modulus	0.9

Use average properties to calculate layered stresses

Improve consolidation accuracy

Ignore negative effective stresses in settlement calculations

Stage Settings

Stage #	Name	Time [days]
1	Stage 1	0
2	Stage 2	30
3	Stage 3	7200

Results

Time taken to compute: 0.155556 seconds

Stage: Stage 1 = 0 d

Data Type	Minimum	Maximum
Total Settlement [in]	0	2.30772
Total Consolidation Settlement [in]	0	2.02699
Virgin Consolidation Settlement [in]	0	1.3903
Recompression Consolidation Settlement [in]	0	0.636688
Immediate Settlement [in]	0	0.281431
Secondary Settlement [in]	0	0
Loading Stress ZZ [ksf]	0.383322	0.877503
Loading Stress XX [ksf]	0.00322815	0.568533
Loading Stress YY [ksf]	0.140306	0.886597
Effective Stress ZZ [ksf]	0.1278	1.353
Effective Stress XX [ksf]	0.334617	1.85308
Effective Stress YY [ksf]	0.28207	2.12753
Total Stress ZZ [ksf]	0.440491	3.65597
Total Stress XX [ksf]	0.334617	4.1084
Total Stress YY [ksf]	0.28207	4.38286
Modulus of Subgrade Reaction (Total) [ksf/ft]	0	3.67017
Modulus of Subgrade Reaction (Immediate) [ksf/ft]	0	17.4803
Modulus of Subgrade Reaction (Consolidation) [ksf/ft]	0	4.6717
Total Strain	0	0.0824879
Pore Water Pressure [ksf]	0	2.30297
Excess Pore Water Pressure [ksf]	0	0.67373
Degree of Consolidation [%]	0	32.9458
Pre-consolidation Stress [ksf]	0.5	1.35257
Over-consolidation Ratio	1	3.76162
Void Ratio	0	1.4442
Permeability [ft/y]	0	6.20124
Coefficient of Consolidation [ft^2/y]	0	50
Hydroconsolidation Settlement [in]	0	0
Average Degree of Consolidation [%]	0	0
Undrained Shear Strength	-2.77556e-017	0.0658725

Stage: Stage 2 = 30 d

Data Type	Minimum	Maximum
Total Settlement [in]	0	5.33884
Total Consolidation Settlement [in]	0	5.05811
Virgin Consolidation Settlement [in]	0	3.95616
Recompression Consolidation Settlement [in]	0	1.10195
Immediate Settlement [in]	0	0.281431
Secondary Settlement [in]	0	0
Loading Stress ZZ [ksf]	0.383322	0.877503
Loading Stress XX [ksf]	0.00322815	0.568533
Loading Stress YY [ksf]	0.140306	0.886597
Effective Stress ZZ [ksf]	0.440491	1.78397
Effective Stress XX [ksf]	0.334617	2.2364
Effective Stress YY [ksf]	0.28207	2.51086
Total Stress ZZ [ksf]	0.440491	3.65597
Total Stress XX [ksf]	0.334617	4.1084
Total Stress YY [ksf]	0.28207	4.38286
Modulus of Subgrade Reaction (Total) [ksf/ft]	0	1.5994
Modulus of Subgrade Reaction (Immediate) [ksf/ft]	0	17.4803
Modulus of Subgrade Reaction (Consolidation) [ksf/ft]	0	1.76422
Total Strain	0.000958473	0.0824879
Pore Water Pressure [ksf]	0	1.872
Excess Pore Water Pressure [ksf]	0	0.26871
Degree of Consolidation [%]	0	97.5571
Pre-consolidation Stress [ksf]	0.5	1.7836
Over-consolidation Ratio	1	1.09587
Void Ratio	0	1.43184
Permeability [ft/y]	0	6.20124
Coefficient of Consolidation [ft^2/y]	0	50
Hydroconsolidation Settlement [in]	0	0
Average Degree of Consolidation [%]	0	71.0462
Undrained Shear Strength	0	0.0658725

Stage: Stage 3 = 7200 d

Data Type	Minimum	Maximum
Total Settlement [in]	0	6.43322
Total Consolidation Settlement [in]	0	6.15249
Virgin Consolidation Settlement [in]	0	5.05054
Recompression Consolidation Settlement [in]	0	1.10195
Immediate Settlement [in]	0	0.281431
Secondary Settlement [in]	0	0
Loading Stress ZZ [ksf]	0.383322	0.877503
Loading Stress XX [ksf]	0.00322815	0.568533
Loading Stress YY [ksf]	0.140306	0.886597
Effective Stress ZZ [ksf]	0.440491	1.78397
Effective Stress XX [ksf]	0.334617	2.2364
Effective Stress YY [ksf]	0.28207	2.51086
Total Stress ZZ [ksf]	0.440491	3.65597
Total Stress XX [ksf]	0.334617	4.1084
Total Stress YY [ksf]	0.28207	4.38286
Modulus of Subgrade Reaction (Total) [ksf/ft]	0	1.19475
Modulus of Subgrade Reaction (Immediate) [ksf/ft]	0	17.4803
Modulus of Subgrade Reaction (Consolidation) [ksf/ft]	0	1.28439
Total Strain	0.000958473	0.0824879
Pore Water Pressure [ksf]	0	1.872
Excess Pore Water Pressure [ksf]	-3.43829e-006	9.70612e-006
Degree of Consolidation [%]	0	100
Pre-consolidation Stress [ksf]	0.5	1.7836
Over-consolidation Ratio	1	1.09587
Void Ratio	0	1.43184
Permeability [ft/y]	0	6.20124
Coefficient of Consolidation [ft^2/y]	0	50
Hydroconsolidation Settlement [in]	0	0
Average Degree of Consolidation [%]	0	100
Undrained Shear Strength	0	0.0658725

Loads

1. Fill Load: "Fill Load 1"

Label	Fill Load 1
Load Type	Flexible
Area of Load	13893.6 ft^2
Load	0.4015 ksf
Depth	0 ft
Installation Stage	Stage 1 = 0 d

Coordinates

X [ft]	Y [ft]
99.8885	99.829
99.8885	-0.171
238.825	-0.171
238.825	99.829

Embankments

1. Embankment: "Embankment Load 1"

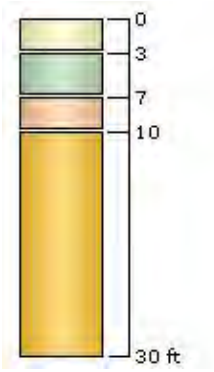
Label	Embankment Load 1
Center Line	(100, 0) to (100, 100)
Near End Angle	90 degrees
Far End Angle	90 degrees
Number of Layers	1
Base Width	41

Layer	Stage	Left Bench Width (ft)	Left Angle (deg)	Height (ft)	Unit Weight (kips/ft^3)	Right Angle (deg)	Right Bench Width (ft)
1	Stage 1 = 0 d	0	18	6	0.08	18	0

Soil Layers

Ground Surface Drained: Yes

Layer #	Type	Thickness [ft]	Depth [ft]	Drained at Bottom
1	CLAY 1	3	0	No
2	CLAY 2	4	3	No
3	CLAY 3	3	7	Yes
4	SAND 1	20	10	No



Soil Properties

Property	CLAY 1	CLAY 2	CLAY 3	SAND 1
Color				
Unit Weight [kips/ft^3]	0.105	0.12	0.11	0.105
Saturated Unit Weight [kips/ft^3]	0.105	0.12	0.11	0.105
K0	1	1	1	1
Immediate Settlement	Disabled	Disabled	Disabled	Enabled
Es [ksf]	-	-	-	400
Esur [ksf]	-	-	-	400
Primary Consolidation	Enabled	Enabled	Enabled	Disabled
Material Type	Non-Linear	Non-Linear	Non-Linear	
Cc	0.45	0.4	0.25	-
Cr	0.07	0.06	0.035	-
e0	1.5	1.25	1	-
Pc [ksf]	0.5	0.5	0.5	-
Cv [ft^2/y]	20	50	50	-
Cvr [ft^2/y]	20	50	50	-
B-bar	1	1	1	-
Undrained Su A [kips/ft2]	0	0	0	0
Undrained Su S	0.2	0.2	0.2	0.2
Undrained Su m	0.8	0.8	0.8	0.8
Piezo Line ID	0	1	1	1

Groundwater

Groundwater method	Piezometric Lines
Water Unit Weight	0.0624 kips/ft^3

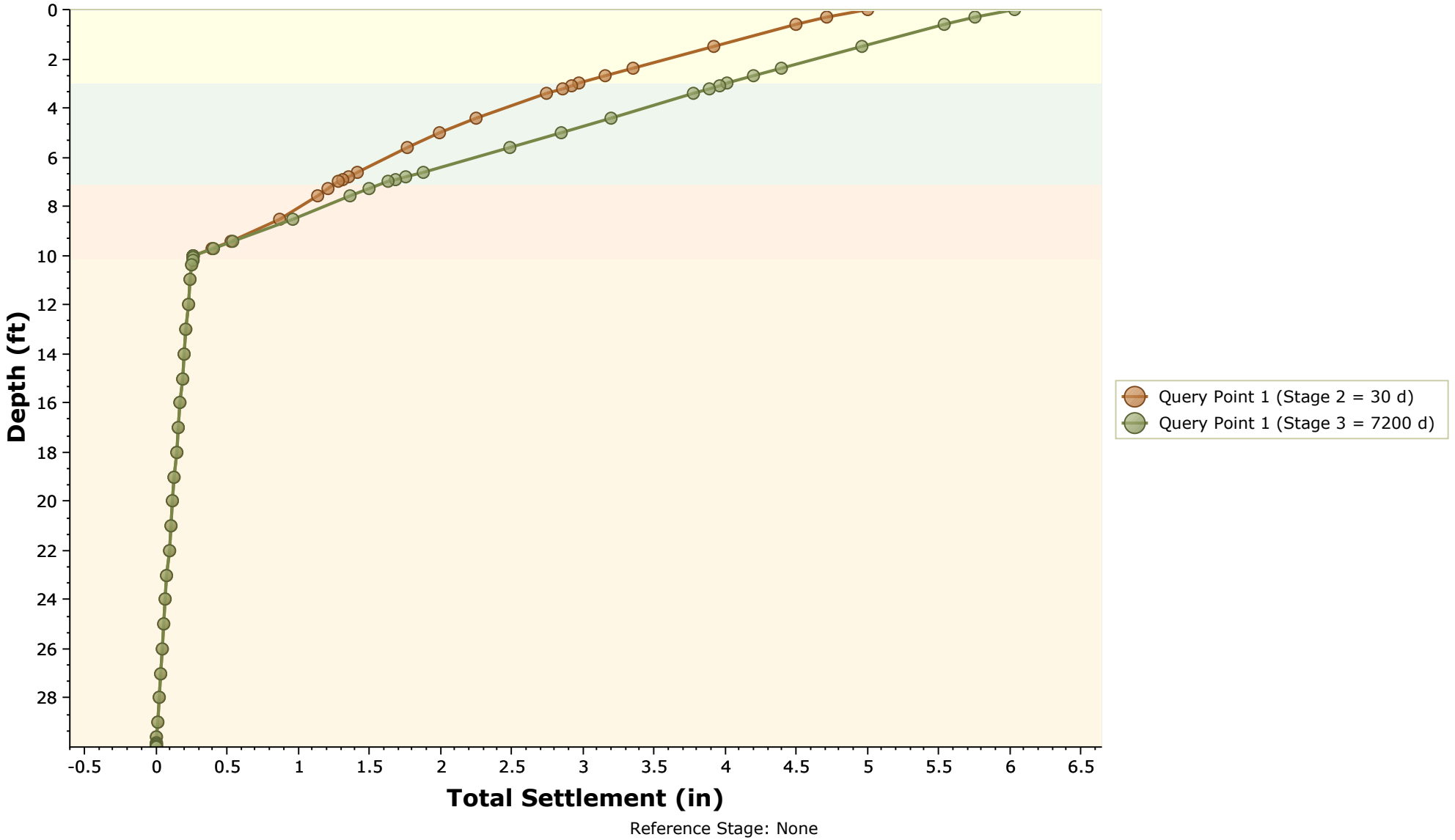
Piezometric Line Entities

ID	Depth (ft)
1	0 ft

Query Points

Point #	Query Point Name	(X,Y) Location	Number of Divisions
1	Query Point 1	100, 50	Auto: 53
3	Query Point 3	119, 49.0881	Auto: 53

Total Settlement vs. Depth



Reference Stage: None

rocscience	Project	Long point Bayou Marsh	
	Analysis Description	ECD Settlement	
	Drawn By	Company	Intertek PSI
	Date	File Name	ECD Embankment 3H 1V , Dike height 5.5 ft.s3z

SETTLE3 5.001

APPENDIX G
FINAL DATA REPORT

Professional Service Industries, Inc.
724 Central Avenue
Jefferson, Louisiana 70121
Phone: (504) 733-9411

September 17, 2020

Coastal Protection and Restoration Authority (CPRA)
150 Terrace Avenue
Baton Rouge, Louisiana 70802

Attn: Ms. Renee Bennett, P.M.P.
Email: Renee.S.Bennett@la.gov

Cc: Ms. Morgan Barranco
Email: Morgan.Barranco@LA.GOV

Re: **Geotechnical Engineering Services Data Report**
Long Point Bayou Marsh Creation Project (CS-0085)
Cameron Parish, LA
PSI Project No. 02541211-1

Dear Ms. Bennett:

Professional Service Industries, Inc. (PSI), an Intertek company, is pleased to submit our Geotechnical Data Report for the above-referenced project. This report presents the results of our field exploration and laboratory testing performed for the proposed construction. A final geotechnical report will be submitted once the engineering analyses are performed.

If you have any questions pertaining to this report, please contact our office at (504) 733-9411. PSI would be pleased to continue providing geotechnical and construction material testing services throughout the construction of the project, and we look forward to working with you and your organization on this and future projects.

Respectfully submitted,

PROFESSIONAL SERVICE INDUSTRIES, INC.

Prasoon Tiwari, P.E.(TX)
Geotechnical Department Manager

STATE OF LOUISIANA
NABIL S. MIKHAIL
License No. 35300
9.17.2020
PROFESSIONAL ENGINEER

Nabil S. Mikhail, P.E., D.GE
Chief Engineer

GEOTECHNICAL ENGINEERING SERVICES DATA REPORT

LONG POINT BAYOU MARSH CREATION PROJECT (CS-0085)
CAMERON PARISH, LA

PSI PROJECT NO. 02541211-1

PREPARED FOR

COASTAL PROTECTION AND RESTORATION AUTHORITY (CPRA)
150 TERRACE AVENUE
BATON ROUGE, LA 70802

September 17, 2020

BY

PROFESSIONAL SERVICE INDUSTRIES, INC.
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PROJECT INFORMATION

PROJECT AUTHORIZATION

Professional Service Industries, Inc. (PSI), an Intertek company, has completed the field and laboratory portions of a geotechnical investigation for the proposed Long Point Bayou Marsh Creation Project (CS-0085) in Cameron Parish, Louisiana. Our scope of services is outlined in PSI Proposal 0286-298563 Rev 5, dated April 6, 2020. Our geotechnical services were authorized by Mr. Jerry Carroll, P.E., Lafayette Regional Operations Manager with CPRA, by issuing a Notice to Proceed as Task #2 dated April 6, 2020 under our existing Contract No. 4400015386. A final geotechnical report will be submitted once the engineering analyses are performed.

PROJECT DESCRIPTION

Project information was provided to PSI by Ms. Renee Bennett, P.M.P. with CPRA, by an email correspondence dated December 19, 2019. The project information was discussed in detail over a follow up call on January 3, 2020 and a revised scope of services was provided to PSI on January 3, 2020. The project information included scope of services for geotechnical investigation and engineering services for Long Point Bayou Marsh Creation Project (CS-0085) in Cameron Parish, Louisiana.

Based on provided information, PSI understands that approximately 392 acres of marsh will be created using borrow material from the Calcasieu Ship Channel. The fill site will be formed by constructing earthen dikes around the boundaries of the marsh creation area where needed. The marsh creation fill site will also be planted with wetland grasses to accelerate plant colonization, stabilize new sediments, and improve habitat. The borrow material for this project site is planned to be dredged from the Calcasieu Ship Channel area between Mile markers 5 and 17.

SITE LOCATION AND DESCRIPTION

The CS-0085 project area is located in CWPPRA Planning Region 4, Calcasieu/Sabine Basin, Cameron Parish, south of Hackberry, north of Sabine National Wildlife Refuge, east of Highway LA 27 and west of the Calcasieu Ship Channel. The water depth of approximately one (1) to three (3) feet was recorded at boring locations in the Marsh area during our field operations.

Table1: Centerline Coordinates of the CS-0085 Project Area

Geographic	
Latitude (DMS)	**Longitude (DMS)**
29* 55’19.6” N	93*21’38.54” W

The approximate site location is shown on the Site Vicinity Map included in the Appendix A, which is based on Appendix B, Proposed Soil Sampling Layout and Permit Drawings of CPRA Scoping document.

FIELD AND LABORATORY PROCEDURES

FIELD EXPLORATION

PERMIT ACCESS

Prior to mobilizing for the field work to survey the boring locations and conduct site reconnaissance, PSI coordinated and acquired documented access permission to conduct any work at the subject site. Special Use Permit for Sabine National Wildlife Refuge, Coastal Use Authorization from Office of Coastal Management and USACE's permit were secured prior to mobilizing to the project site. Additionally, notification to the coast guard was provided prior to mobilizing the barge mounted drill rig in the ship channel area.

SURVEY POSITIONING AND MAGNETOMETER SURVEY

Prior to mobilizing the drilling equipment to perform the soil borings/CPT's, Chustz surveying, LLC performed survey positioning and magnetometer survey at each boring/CPT location in the marsh area and borrow area, as per CPRA guidelines. The horizontal and vertical control for survey positioning was performed in accordance with secondary monument and data sheets presented in Appendix D of the attached Scope Document. The magnetometer survey at each boring/CPT location in the marsh and borrow area was performed to ensure there are no pipelines or obstructions in the area. The locations in the marsh area were staked in the field by the survey crew. Based on information obtained from the survey work, soil boring and CPT details are presented in the Table 2. The survey report is presented in Appendix A.

Table 2. Soil Boring and CPT Sounding details (Datum: NAVD88 GEOID12B)

Boring Location	Northing	Easting	Mudline Elevation (ft)	Water Surface Elevation (ft)	Project Area*
B-1	521980.25	2638800.9	0.2	2.3	Marsh
B-2	523622.39	2634883.9	0.64	2.4	Marsh
B-3	519709.77	2638822.9	0.36	2.4	Marsh
B-4	523168.5	2640982.6	0.14	2.4	Marsh
B-5	523526.97	2638396.7	-0.89	2.3	Marsh
B-6	502413.49	2643251.4	-43.54	1.4	Borrow
B-7	506467.17	2643634.3	-42.24	1.5	Borrow
B-8	514945.17	2644470.5	-38.90	1.5	Borrow
B-9	520923.85	2644779.5	-40.17	1.6	Borrow
B-10	525073.53	2645165.5	-40.60	1.6	Borrow
B-11	529408.86	2645624.2	-41.76	1.7	Borrow
B-12	536575.47	2646292.5	-40.49	1.7	Borrow
CPT 1	522619.72	2635614.8	-0.09	2.5	Marsh
CPT 2	521553.61	2637072.8	0.44	2.5	Marsh
CPT 3	521172	2638106.8	0.03	2.5	Marsh

CPT 4	520971.77	2639657.2	1.82	2.5	Marsh
CPT 5	522485.73	2640096.9	-0.11	2.5	Marsh
CPT 6	524712.54	2639962.3	0.02	2.4	Marsh
CPT 7	525528.58	2637537.9	-0.51	2.5	Marsh
CPT 8	522298.03	2637720.2	-0.16	2.4	Marsh
CPT 9	523168.5	2640982.6	0.14	2.4	Marsh
CPT 10	523622.39	2634883.9	0.64	2.4	Marsh
CPT 11	519709.77	2638822.9	0.36	2.4	Marsh
CPT 12	525466.65	2638444.9	-0.72	2.3	Marsh

* A water depth of approximately 39 to 45 feet was recorded at boring locations in the Ship Channel area during our field operations.

SOIL BORINGS

Based on provided information and discussion with CPRA, soil borings and CPT soundings locations were finalized. Boring Location Plans for marsh area and borrow area are attached in the Appendix B.

A total of seventeen (17) soil borings and CPT soundings were performed for the Containment Dike and Marsh Creation area. As discussed with CPRA, the soil borings and CPT soundings were explored using an airboat mounted drilling equipment. All the borings and CPT soundings were performed between June 24 to June 30. Detailed description mentioned below:

- Five (5), 3-inch diameter borings to a depth of 30 feet below mudline sampled continuously. Three (3) of these borings (B-2, B-3 and B-4) were co-located next to CPTs (CPT-9, CPT-10 and CPT-11) for comparison. Drilling, and sampling were performed in accordance with applicable ASTM Standards and the furnished Scope of Services Document. The proposed soil borings were advanced with a 4-inch diameter rotary wash drilling method.

  Undisturbed samples of cohesive soils were obtained by using three-inch diameter thin-wall tube samplers (Shelby Tube) in general accordance with the procedures for “Thin-Walled Tube Geotechnical Sampling of Soils” (ASTM D1587). For cohesionless soils and semi-cohesive soils, Standard Penetration Test (SPT) was performed to obtain standard penetration values of the soil. The standard penetration value (N) is defined as the number of blows of a 140-pound hammer falling 30 inches that is required to advance the split-barrel sampler one (1) ft. into the soil. The number of blows is recorded for each of three (3) successive increments of six (6) inches penetration. The “N” value is obtained by adding the second and third incremental numbers. The results of the standard penetration test indicate the relative density of cohesionless soils and thereby provide a basis for estimating the relative strength of the soil profile components. Samples of granular soils were obtained utilizing a two (2) inch O.D. split-barrel sampler in general accordance with procedures for “Penetration Test and Split-Barrel Sampling of Soils” (ASTM D1586). The boreholes were grouted upon their completion per LDEQ and LA DOTD regulations.

- Twelve (12), Cone Penetration tests to the refusal depth varying from 10 feet to 15 feet.

Our CPT utilizes a 60° apex cone, 1.4-inch diameter, Type 2 electric cone penetrometer that meets ASTM D5778 specification. The soil information obtained from CPT soundings are presented in the Appendix B. The CPT was advanced to the shallow refusal depth due to the presence of the Pleistocene. Refusal prior to the depth specified occurs due to achieving maximum tip resistance, a high frictional resistance of the sleeve, or excessive tilt angle of the CPT probe. To prevent damage to the CPT, no attempt was made to advance beyond refusal depth. Due to low penetration depths for CPT soundings, a cut off value of 1.7 was used for overburden correction factors for estimating normalized soil behavior type. For cohesive soils, Shear strength (Su) was estimated using the total cone resistance (q_t) and cone factor (N_{kt}).

$$s_u = \frac{q_t - \sigma_v}{N_{kt}}$$

- N_{kt} =16, used for marsh area CPT's.

A total of seven (7) soil borings were performed for the borrow area. The borings were performed between May 26 to May 29. Detailed description mentioned below:

- Seven (7), bulk sample collection continuously to the maximum depth of the dredging in the Channel (approximately Elev. -45 MLLW in the center of channel). The bulk samples were collected utilizing 5-inch diameter and 5 feet long piston sampler.

GEOTECHNICAL LABORATORY TESTING

During the field work, the samples were identified according to boring number and depth and were transported to PSI's laboratory for classification and testing. A geotechnical laboratory testing program was developed after reviewing the field logs. The laboratory testing program was provided to CPRA for review and approval prior to testing. After approval, laboratory tests were performed in general accordance with applicable ASTM procedures and the furnished Scope Document. Laboratory testing of the obtained samples has been performed to evaluate the classification, strength and other engineering characteristics of the subsurface materials.

The Shelby tube samples were removed from the sampling tubes in the laboratory using a specially fabricated hydraulic piston-type extruder. The tube samples were extruded, classified and subjected to index and compressive strength tests. Additional estimates of shear strength were obtained through the use of a hand penetrometer (HP) and torvane (TV), respectively. The results of the laboratory tests are presented in the Boring Logs given in the Appendix B. A key to the terms and symbols used on the boring logs is also presented in Appendix B.

An overview of the scope of the laboratory testing phase for both the marsh area borings and borrow area borings are tabulated in Table 3 and Table 4 respectively below. A detailed discussion on laboratory test results is presented in subsequent sections of the data report.

Table 3. Laboratory Testing Summary for Marsh area borings

Test Method	ASTM Reference	No. of Tests performed
Moisture Content	(ASTM D2216)	74
Visual Classification	(ASTM D2488)	74
Organic Content	(ASTM D2974)	5
Atterberg limits	(ASTM D4318)	20
Percent Passing #200 sieve	(ASTM D1140)	19
Hydrometer Analysis	(ASTM D7928)	4
Specific Gravity	(ASTM D854)	5
Total Unit Weight Determination	(ASTM D2937)	11
Unconsolidated Undrained Triaxial Test	(ASTM D2850)	11
Consolidation Test	(ASTM D2435)	5

Table 4. Laboratory Testing Summary for Borrow area borings

Test Method	ASTM Reference	No. of Tests performed
Moisture Content	(ASTM D2216)	7
Visual Classification	(ASTM D2488)	7
Organic Content	(ASTM D2974)	7
Atterberg limits	(ASTM D4318)	7
Percent Passing #200 sieve	(ASTM D1140)	7
Hydrometer Analysis	(ASTM D7928)	7
Column Settling Test	USACE 1110-2-5027	2
Low Stress Consolidation Test	ASTM D2345 (mod.)	2

CLASSIFICATION AND INDEX TESTS

To determine the soil classification and geotechnical index properties, various classification and index tests were performed. The following classification and index tests for the marsh and borrow area were performed:

- Visual Classification (ASTM D2488)
- Moisture Content (ASTM D2216)
- Atterberg Limits (ASTM D4318)
- Percent Passing #200 sieve (ASTM D1140)
- Particle-Size Analysis and Hydrometer (ASTM D7928)
- Specific Gravity (ASTM D854)
- Organic Content (ASTM D2974)
- Total Unit Weight Determination (ASTM D2937)

1. Visual Classification
   Visual classification was performed based on ASTM D2488 and incorporated into the soil boring logs in Appendix B. It includes the description of soil color, consistency and type, and identification of variations (organics, layers, seams, etc.).

2. Moisture Content
   More than eighty (80) moisture content determinations (ASTM D2216) were performed in conjunction with the sample extrusion process and preparation of test specimens. Moisture content determinations were made for each extruded sample, and total densities were computed for each sample. Moisture content for each sample are included on the soil boring logs in Appendix B.

3. Atterberg Limits
   A total of twenty-seven (27) Atterberg limit determinations (ASTMD4318) were performed on selected samples to assist in soil classification and to enable correlation to pertinent clay behavior properties. The Atterberg limit data consist of measured liquid limit (LL) and plastic limit (PL) values from which the plasticity index (PI = LL - PL) is derived. The individual test data are included on the boring logs in Appendix B.

4. Percent Passing #200 sieve and Hydrometer Analysis
   A total of eleven (11) hydrometer particle size analysis tests (ASTM D7928) and 26 fines content determinations (ASTM D 1140) were performed on selected samples. The test results, in terms of percent fines (i.e., percent by dry weight finer than the U.S. No. 200 sieve size, 0.074 mm, or combined silt and clay fraction) are included on the soil boring logs in Appendix B. The hydrometer test results are included in Appendix C.

5. Specific Gravity
   A total of five (5) specific gravity tests based on ASTM D854 were performed on selected samples and results are included in Appendix C.

6. Organic Content
   A total of twelve (12) organic tests based on ASTM D2974 were performed on selected samples. The organic content results are included in Appendix C.

7. Total Unit Weight Determination
   Total unit weights of the tube samples were computed based on (ASTM D2937) sample volume and weight measurements taken after exclusion of any materials that appeared to have been disturbed during the sampling or extrusion process.

STRENGTH TESTS

To determine the strength characteristics of the marsh area soil deposits, various compression tests and index strength tests were performed. The following tests for the selected marsh area soil samples were performed:

1. Unconsolidated-Undrained Triaxial Compression Tests
   Unconsolidated-undrained (UU) triaxial compression tests (ASTM D2850) were performed on specimens trimmed from selected samples. Results of these strength tests are included on the soil boring logs in Appendix B. Individual UU test stress-strain curves are included in Appendix D.

2. Hand penetrometer and Torvane Index Strength Tests
   Hand-operated Torvane (TV) and hand penetrometer index strength tests were performed in conjunction with the sample extrusion process and are included in soil boring logs. These test results are considered to be index strengths in that the absolute value of the measured undrained shear strength is generally not considered adequately reliable for use in design. The test results, however, are useful in identifying soil strength variability and trends with respect to depth, material type, etc.

CONSOLIDATION TESTS

To determine the stress history, stress deformation, and time rate settlement characteristics of the marsh area soil deposits, consolidation tests were performed on selected clay samples from marsh area soil borings. A total of 5 tests were performed.

Additionally, to determine the settlement criteria for the dredged soil from the borrow area, settling column tests and low stress consolidation tests were performed. A total of 2 tests each were performed.

1. Consolidation Test (ASTM D2435)
   Incremental consolidation tests (ASTM D 2435) were included in the laboratory testing program to enable assessment of stress history and determination of stress history, stress deformation, and time rate settlement characteristics of the marsh clay deposits that will dictate post-construction settlement of the marsh creation area. One consolidation test for each marsh area boring was performed and a total of five (5) tests were conducted.

   During each load increment, the accumulation of vertical displacement with time is measured. In general, each load increment was sustained for a period of 12 to 36 hours. The vertical displacement versus time data was evaluated using the conventional log-time and square-root time curve fitting techniques to determine the end of primary consolidation (i.e., the point in time at which dissipation of load-induced excess pore water pressures in the sample had dissipated and drained creep ensued for each load increment). The individual test results, in terms of coefficient of consolidation versus effective vertical stress and void ratio versus effective vertical stress are presented in Appendix E.

2. Settling Column Test
   Two representative composite samples were prepared using samples obtained from the seven (7) sampling locations performed within the proposed borrow area. Laboratory settling tests were performed in a 20-cm diameter graduated plexi-glass settling columns.

   A water sample from the Calcasieu River Ship Channel area was collected to obtain the salinity of the dredging site water. Salinity test was performed by gravimetric method and was also further confirmed by a digital salinity meter. The salinity of dredging site water was calculated about 20 g/l. The composite test samples were mixed with synthesized water having a salinity, in terms of total dissolved solids, of 20 g/l. The initial solids content of the settling test samples was about 13 percent, with a corresponding initial total suspended solids concentration of about 150 g/l. The slurry was mixed with a hand-held stirrer to provide a homogeneous sample and remove any segregation of particles which may have occurred during placement of the slurry into the column.

A 7-foot settling column was prepared to run the tests on composite samples. The settling column tests simulate the sedimentation of a dredged material in a quiescent environment. This test provides information regarding two types of settling regimes which occur; zone settling, and compression settling. The settling tests consist of measuring the fall of the liquid-solid interface over time. These data are plotted in terms of height of the interface over time in Appendix E.

3. Low Stress Consolidation Test (Modified ASTM D2435)
One-dimensional incremental slurry consolidation tests were performed on two (2) composite samples prepared from the dredge borrow area. The change in specimen height with time under each load is monitored and evaluated to characterize the one-dimensional compressibility, consolidation and drained creep properties of the sediment. A comparison graph depicting the void ratio versus vertical effective stress relationships from both the settling column and self-weight consolidation tests are plotted and presented in the Appendix E.

   It should be noted that some differences were observed in the void ratio versus vertical effective stress relationship between the settling column and the slurry consolidation test as can be seen by the variance in void ratio for a similar vertical effective stress. This difference may be due in part to the difference in diameter of the testing equipment, which may lead to arching effects. Another possible reason for the observed discrepancy may be due in part to the salinity of the settling column. The addition of salt into the water may cause dispersion and or swelling of the clay particles, which would result in a change in void ratio.

DISCUSSION ON SUBSURFACE CONDITIONS

MARSH FILL AREA SUBSURFACE CONDITIONS

Based on the field observations, CPT soundings and results of the geotechnical laboratory testing, the soils were classified, and boring logs and CPT sounding plots were developed. A generalized subsurface profile is presented in Table 5.

Table 5: Generalized Soil Profile

Approximate Elevation Range (Datum: NAVD88 GEOID12B, feet)*	Consistency/Relative Density	Material Description
0 – 8	Very Soft to Soft	Fat Clay (CH), Organic Clay (OH)
8 - 12	Very Soft to Stiff	Lean clay (CL), Fat Clay (CH)
12 - 22	Firm to Hard / Dense to Very Dense	Lean clay (CL), Sandy Lean clay (CL), Clayey Sand (SC), Poorly Graded Sand with Silt (SP-SM)
22 - 30	Very Stiff to Hard / Medium Dense to Very Dense	Sandy Lean clay (CL), Silty Sand (SM), Silty Clayey Sand (SC-SM), Poorly Graded Sand with Silt (SP-SM)

**Referenced from existing mudline elevation at the boring locations at the time of drilling activities.*

The above soil profile is of generalized nature to highlight the major subsurface stratification features and material characteristics of the marsh creation area. The boring logs and CPT sounding plots included in the Appendix A should be reviewed for specific information at individual locations. These records include soil descriptions, stratification, locations of the samples, and laboratory test data. The stratification shown on the boring logs represent the conditions only at the actual boring locations. Variations may occur and should be expected between and away from boring locations. The stratification represents the approximate boundary between subsurface materials and the actual transition may be more distinct or gradual.

TOP OF PLEISTOCENE

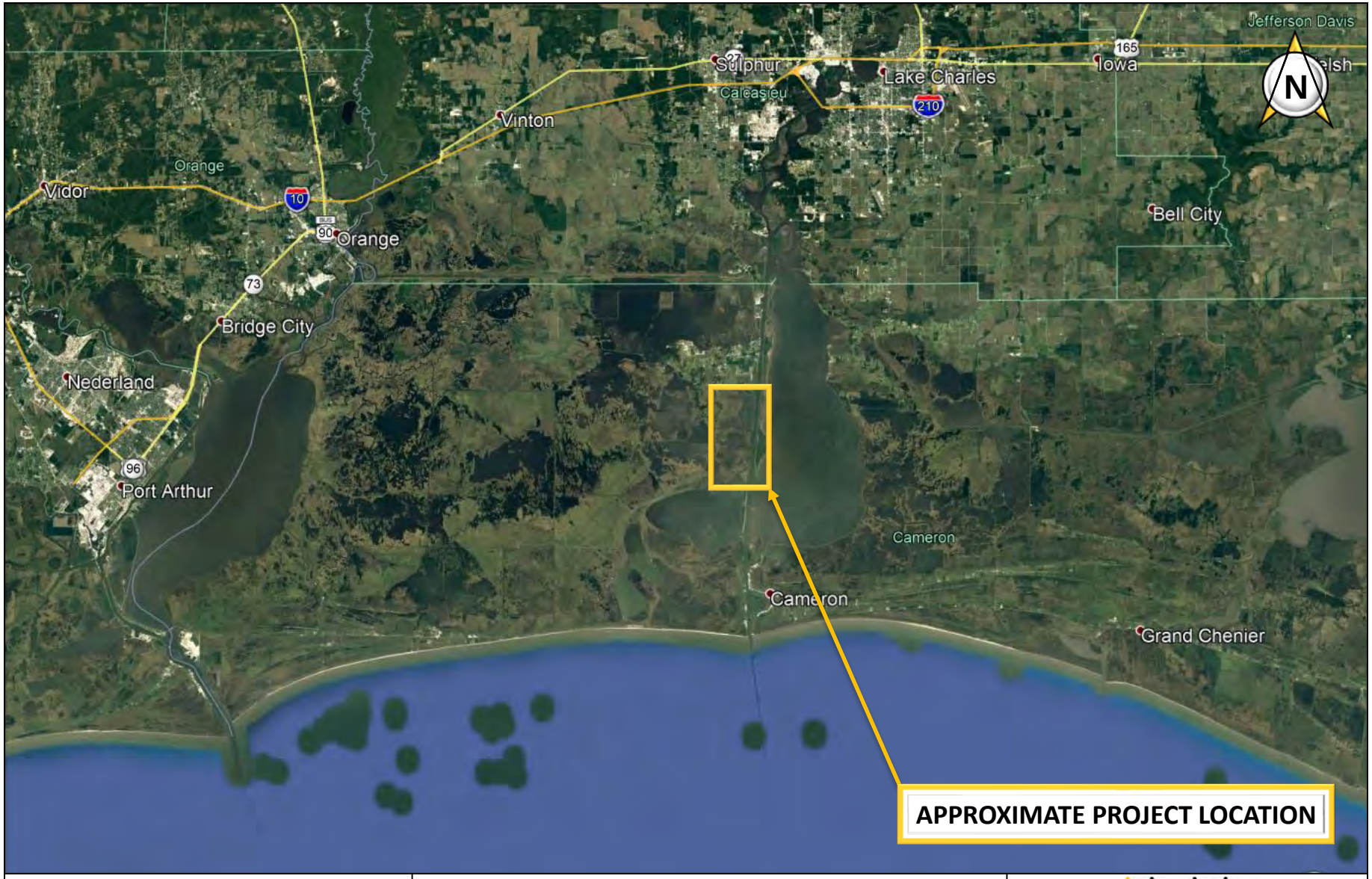
Based on information obtained from soil borings and CPT soundings, the top of Pleistocene may be established at about -10 to -15 feet elevation in the marsh creation area.

FUTURE DESIGN REPORT

Based on furnished data from field work and Laboratory test results, soil properties will be established for the design of the proposed project and will be included in the final report.

APPENDIX A

SITE VICINITY MAP
SURVEY REPORT



GEOTECHNICAL ENGINEERING SERVICES

Long Point Bayou Marsh Creation

Cameron, Louisiana

SITE VICINITY MAP

PSI PROJECT NO.: 02541211

GOOGLE EARTH IMAGERY DATE: 1/2018

intertek psi

Survey Report

Long Point Bayou Boring Sites Survey
Cameron Parish, Louisiana

Prepared for Intertek-PSI
724 Central Ave.
Jefferson, LA 70121

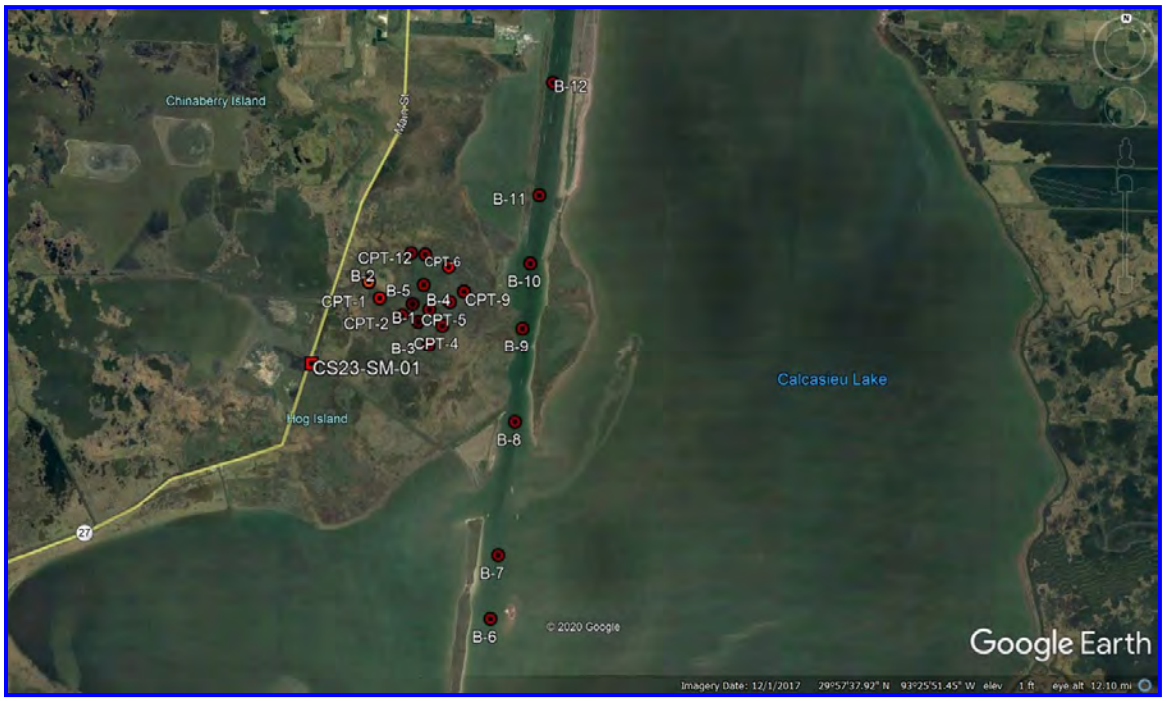
Chustz Surveying, LLC
211 Richy Street
New Roads, LA 70760
225-638-5949

May 2020

Section 1
General Project Description

In April of 2020, Chustz Surveying was tasked by Intertek-PSI to conduct location and magnetometer surveys at 21 boring sites in Cameron Parish. The surveys consisted of locating the sites utilizing RTK and multibeam hydrographic methods from the provided project benchmark (CS23-SM-01 “HOGG RESET”).

Vicinity Map



Section 2
Data Collection

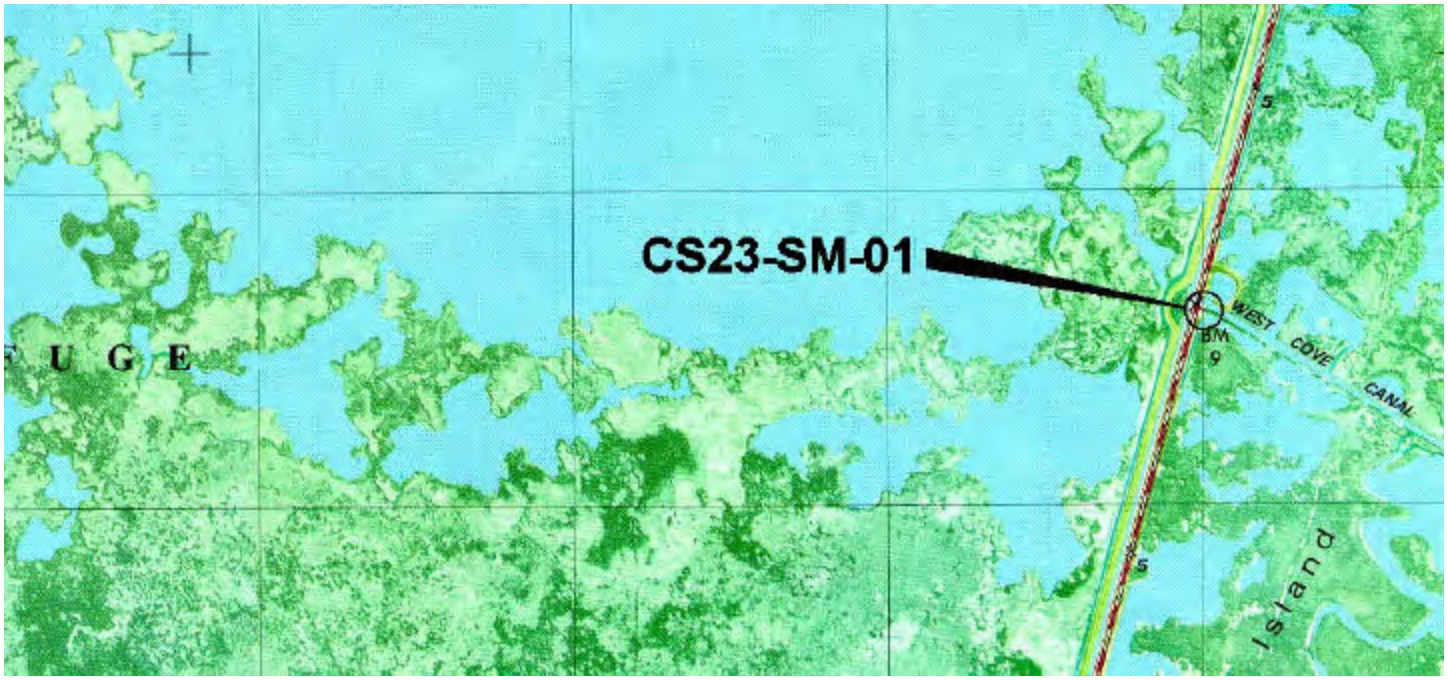
On April 27, 2020, Chustz Surveying deployed a three person crew to the site to begin the survey. Utilizing two Trimble R8 GPS receivers, the crew set the base up on CS23-SM-01 and set two iron rods on site to establish temporary control points for the survey. They then moved the base to one of the iron rods and made an RTK tie to the other to confirm the temporary control points. The crew then began locating the boring sites in the marsh area and drove pvc pipe with pink flagging into the ground at each location. The crew then established temporary gauges upstream and downstream of the sites for the hydrographic survey in the Calcasieu Ship Channel. The crew returned the next day with a fourth person and a Geometrics G882 cesium magnetometer. In Hypack, they set up a grid around each location to cover a 25 ft. radius. They then conducted the magnetometer surveys at each bore site in the marsh area. The crew returned on May 1, 2020, to conduct the required surveys in the Calcasieu Ship Channel. The gauges were read before and after the survey to ensure a quality data set. The survey was completed that day.

Section 3
Data Processing

The data was transferred to our office for initial processing once the surveys were complete. The RTK data files were loaded into Trimble Business Center where they were processed and checked for correct rod and instrument heights. All RTK ties were checked to ensure they were within the allowed accuracies. The hydrographic and magnetometer data was processed in Hypack utilizing prorated gauges for each location.

Section 6
Project Summary and Conclusion

The field effort was completed ahead of schedule on Friday, May 1, 2020, and all data was processed and deliverables were completed for Monday, May 11, 2020. No safety incidents occurred as part of this work effort.



VICINITY MAP Scale: 1" = 2000' Reproduced from USC&GS "BROWNS LAKE" Quadrangle

Station Name: CS23-SM-01

Monument Location: From St. Peters Catholic Church in the town of Hackberry, Louisiana, proceed south on La. Highway 27 for approximately 5.4 miles to a bridge crossing West Cove Canal at Hogg Island Gulley and the monument at left on east side of highway in a parking area.

Monument Description: 2" aluminum cap set on a 9/16" stainless steel rod driven to refusal and set in a 6" PVC sleeve filled with concrete.

Stamping: "HOGG RESET"

Date: October 2000

Monument Established By: John Chance Land Surveys, Inc

For: *Louisiana Department of Natural Resources, CRD*

Adjusted NAD 83 (1992) Geodetic Position
Lat. 29° 54' 33.164186" N
Long. 93° 23' 00.168705" W

Adjusted NAD 1983 Datum LSZ (1702) Feet
N= 518,286.36
E= 2,631,372.09

Adjusted NAVD88 Height
Elevation = 1.92 feet / 0.586m

Ellipsoid Height = -26.413m
Geoid99 Height = -26.999m

Note: Reset, Re-Surveyed and Re-Adjusted in February 2002

Long Point Bayou Survey Locations, Datum: NAVD88 GEOID12B

Site	Northing	Easting	Elevation	Water Surface	Depth
B-1	521980.25	2638800.90	0.20	2.3	2.1
B-5	523526.97	2638396.70	-0.89	2.3	3.2
B-6	502413.49	2643251.37	-43.54	1.4	44.9
B-7	506467.17	2643634.25	-42.24	1.5	43.7
B-8	514945.17	2644470.50	-38.90	1.5	40.4
B-9	520923.85	2644779.52	-40.17	1.6	41.8
B-10	525073.53	2645165.53	-40.60	1.6	42.2
B-11	529408.86	2645624.22	-41.76	1.7	43.5
B-12	536575.47	2646292.47	-40.49	1.7	42.2
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CPT 3	521172.00	2638106.80	0.03	2.5	2.5
CPT 4	520971.77	2639657.18	1.82	2.5	0.7
CPT 5	522485.73	2640096.92	-0.11	2.5	2.6
CPT 6	524712.54	2639962.32	0.02	2.4	2.4
CPT 7	525528.58	2637537.87	-0.51	2.5	3.0
CPT 8	522298.03	2637720.15	-0.16	2.4	2.6
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CPT 11	519709.77	2638822.85	0.36	2.4	2.0
CPT 12	525466.65	2638444.90	-0.72	2.3	3.0

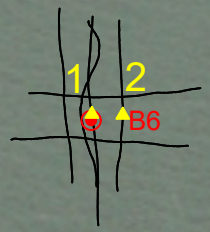
Long Point Bayou Magnetometer Findings

Ref. #	Easting	Northing	Gamma Mean	Gamma Max	Gamma Min	Amplitude	Type	Begin DBL	End DBL	Duration	Location Notes:
1	2643252.03	502419.11	46830.19	46836.48		6.3	M	70.62	-34.64	105.26	B6
2	2643279.87	502418.30	46842.90	46848.36		5.5	M	-7.83	65.00	72.83	B6
3	2638104.01	521197.77	46841.52	46841.50	46823.00	18.5	D	4363.25	4369.24	5.99	CPT3
4	2639675.73	520985.35	46833.44	46841.29		7.8	M	1965.20	1999.40	34.20	CPT4
5	2635635.94	522624.05	46837.84	46844.04		6.2	M	2923.55	2915.28	8.27	CPT1

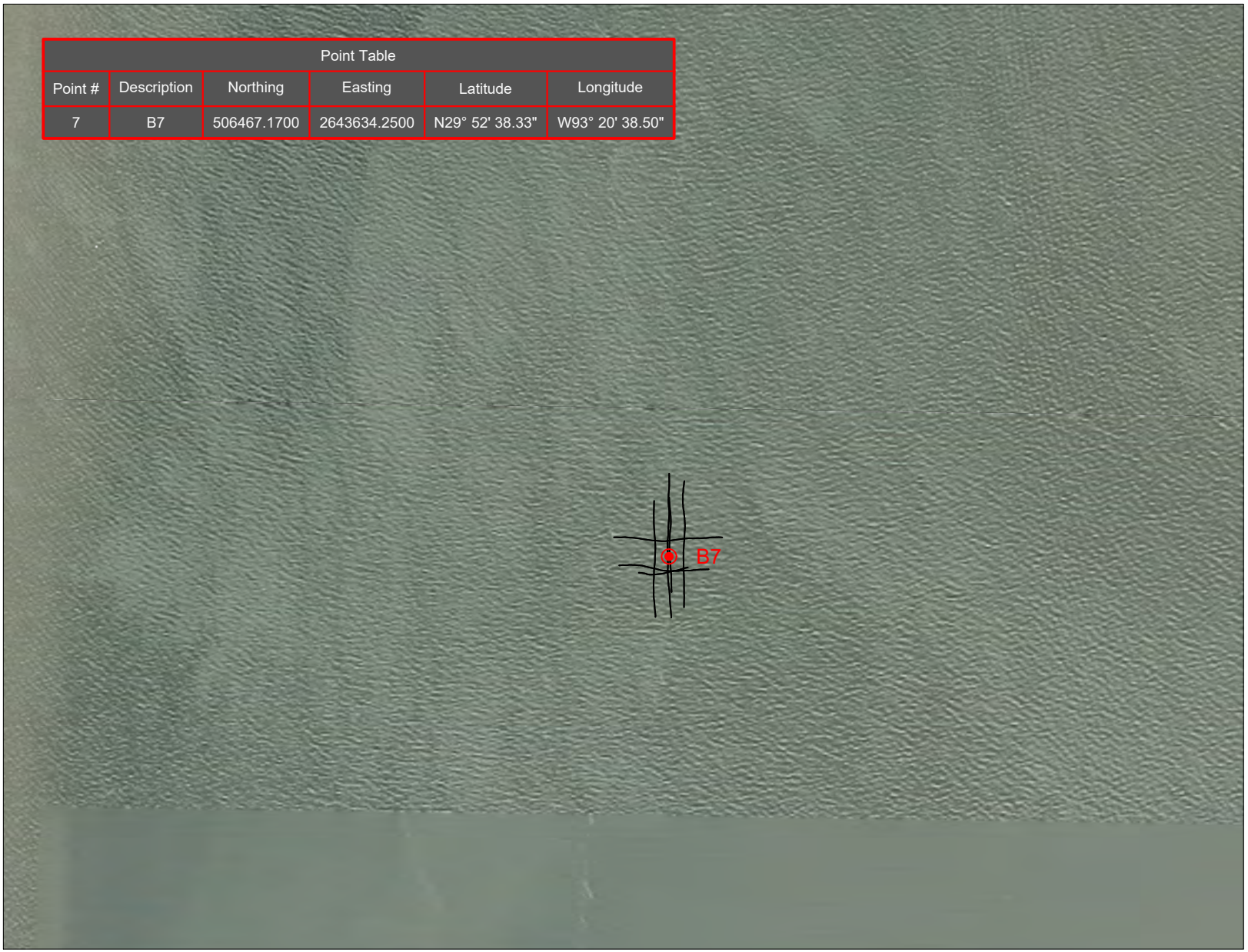
Point Table					
Point #	Description	Northing	Easting	Latitude	Longitude
1	B1	521980.8400	2638801.0400	N29° 55' 11.04"	W93° 21' 36.51"

Point Table					
Point #	Description	Northing	Easting	Latitude	Longitude
5	B5	523527.7100	2638396.2900	N29° 55' 26.28"	W93° 21' 41.42"

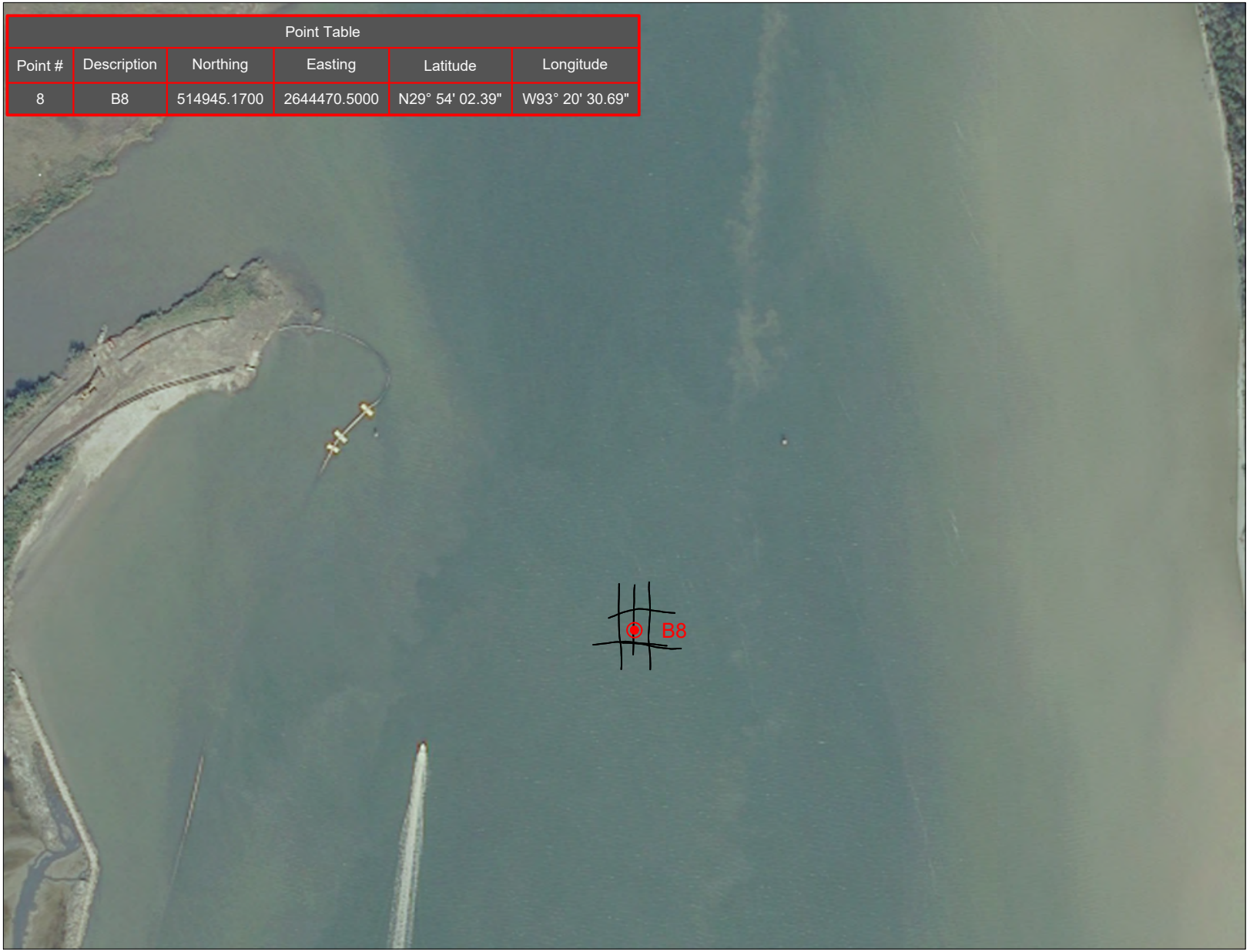
Point Table					
Point #	Description	Northing	Easting	Latitude	Longitude
6	B6	502413.4900	2643251.3700	N29° 51' 58.14"	W93° 20' 42.04"



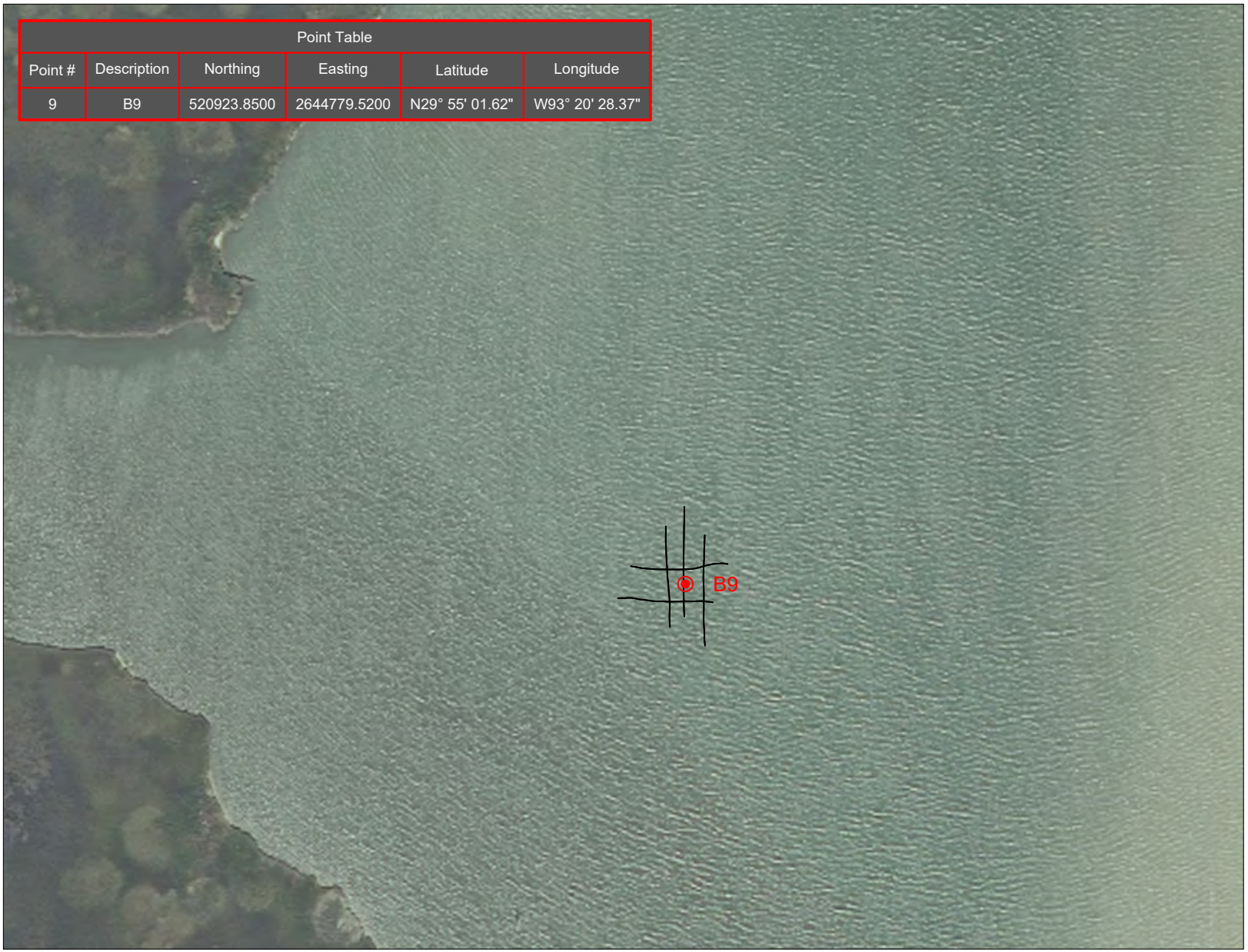
Point Table					
Point #	Description	Northing	Easting	Latitude	Longitude
7	B7	506467.1700	2643634.2500	N29° 52' 38.33"	W93° 20' 38.50"



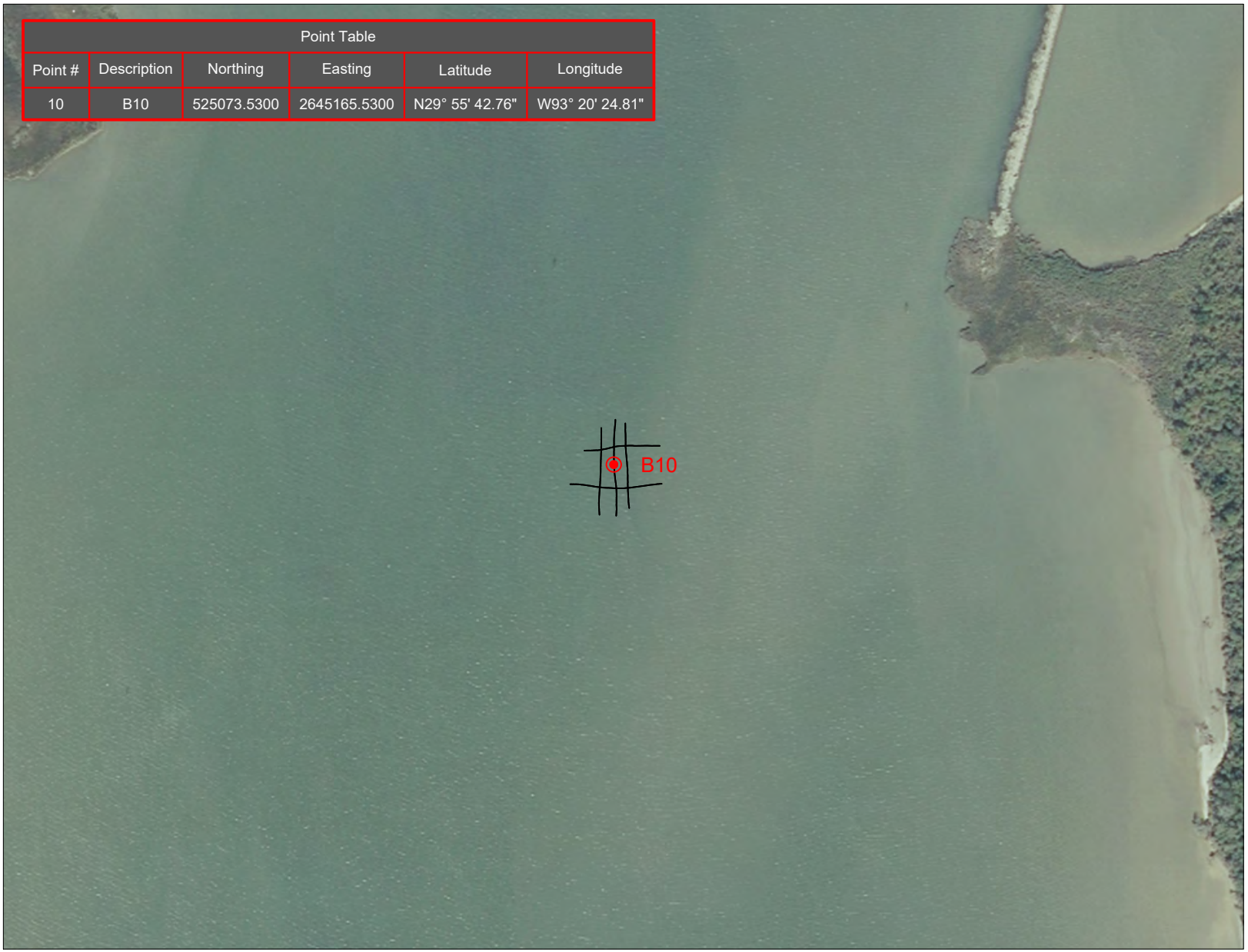
Point Table					
Point #	Description	Northing	Easting	Latitude	Longitude
8	B8	514945.1700	2644470.5000	N29° 54' 02.39"	W93° 20' 30.69"



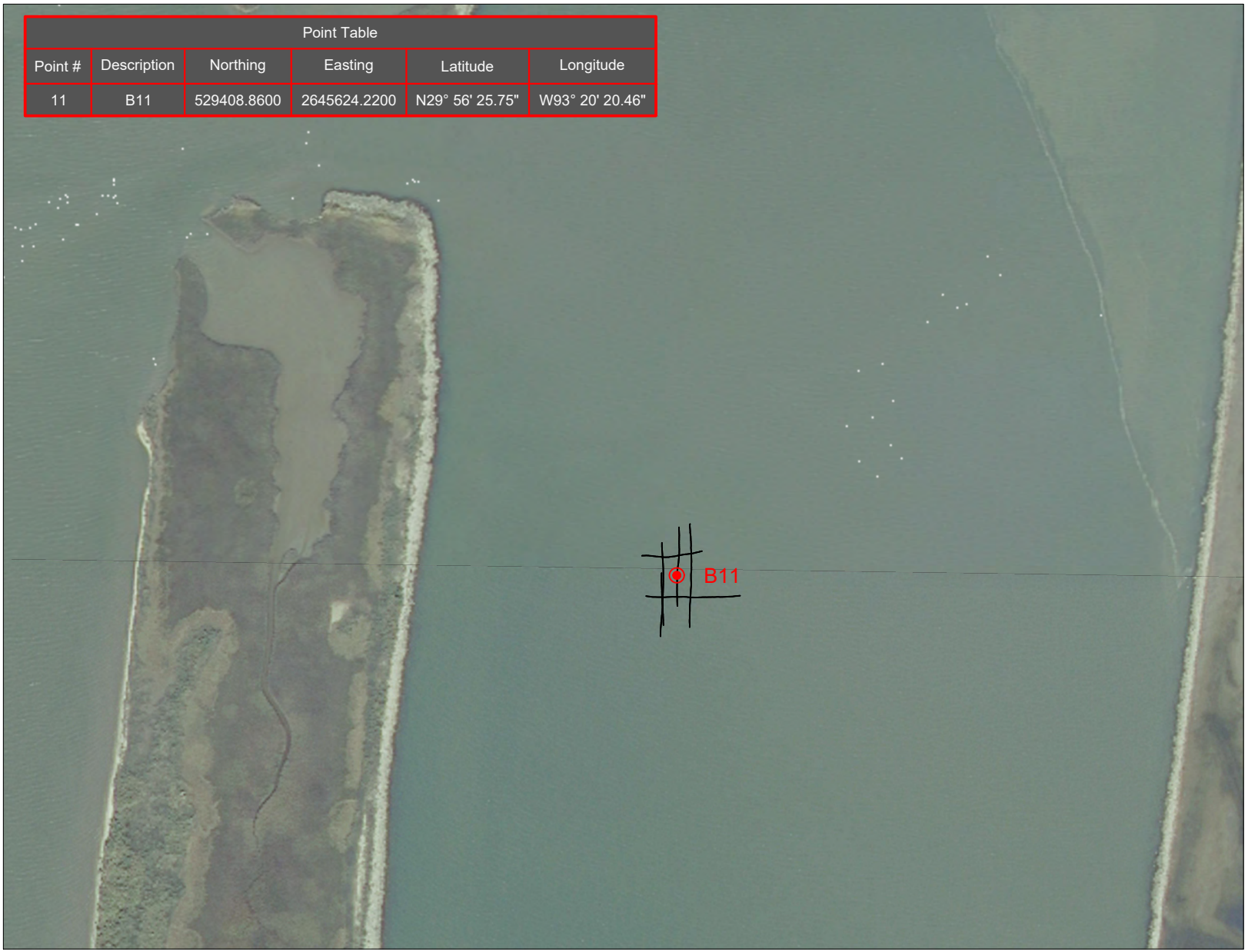
Point Table					
Point #	Description	Northing	Easting	Latitude	Longitude
9	B9	520923.8500	2644779.5200	N29° 55' 01.62"	W93° 20' 28.37"



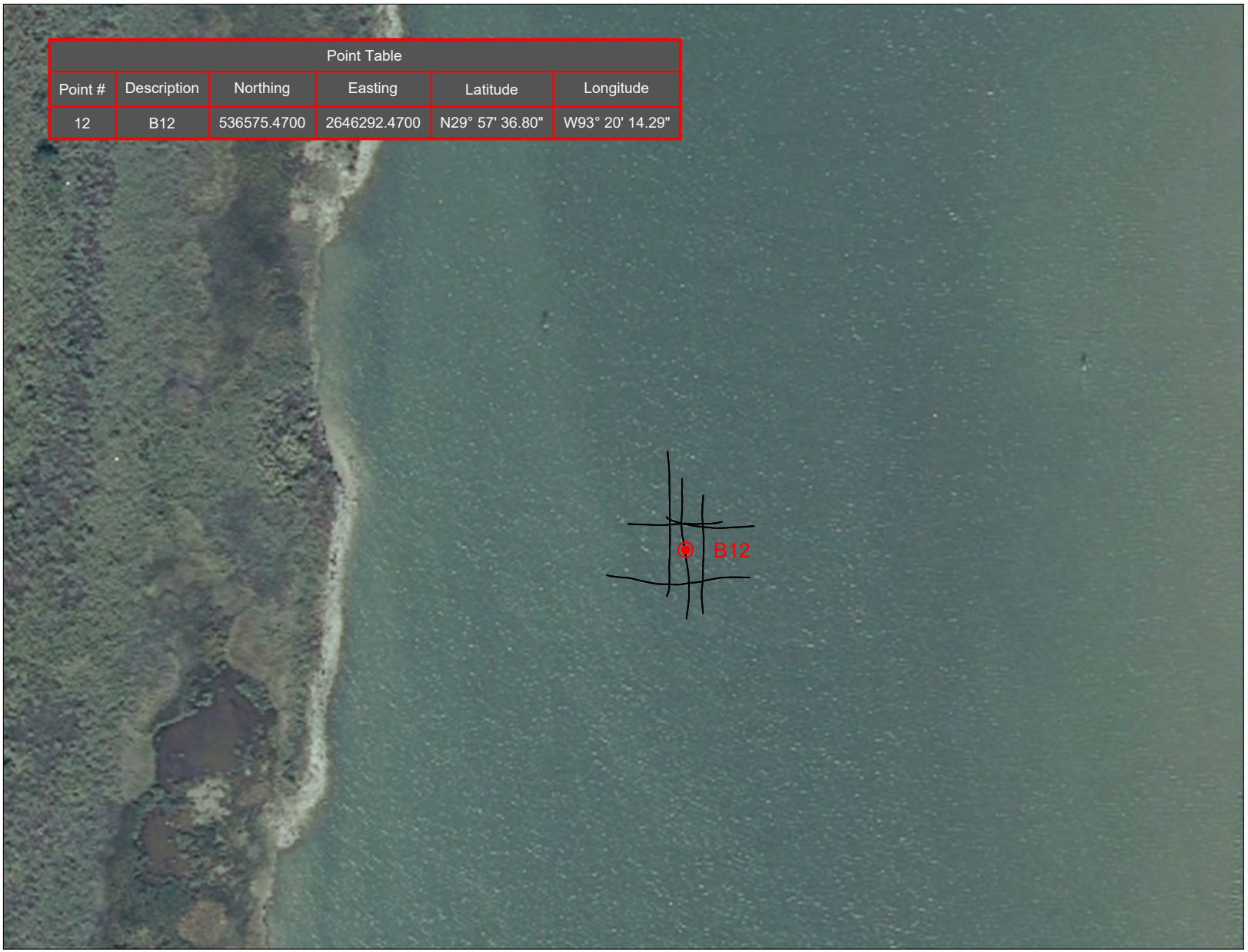
Point Table					
Point #	Description	Northing	Easting	Latitude	Longitude
10	B10	525073.5300	2645165.5300	N29° 55' 42.76"	W93° 20' 24.81"



Point Table					
Point #	Description	Northing	Easting	Latitude	Longitude
11	B11	529408.8600	2645624.2200	N29° 56' 25.75"	W93° 20' 20.46"

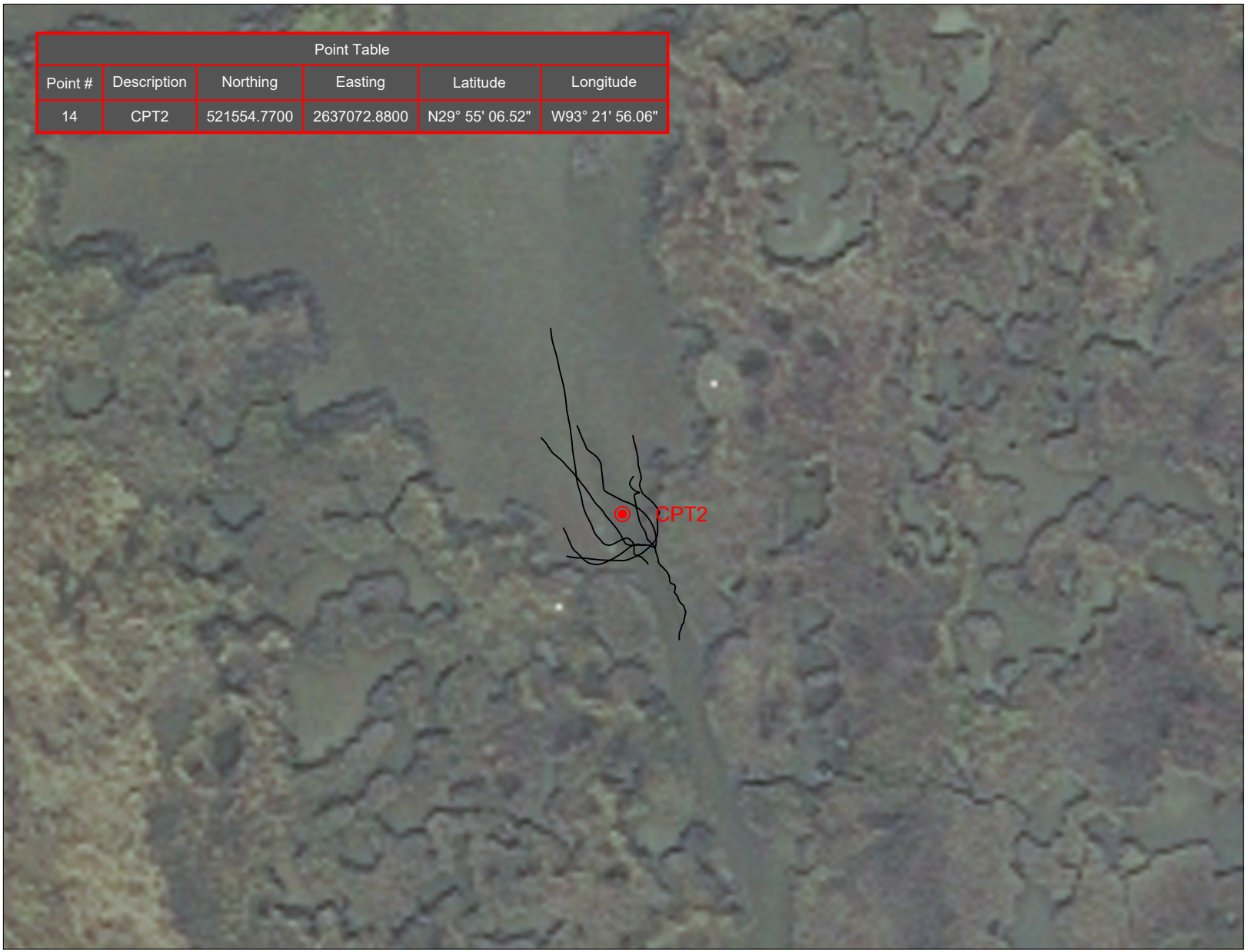


Point Table					
Point #	Description	Northing	Easting	Latitude	Longitude
12	B12	536575.4700	2646292.4700	N29° 57' 36.80"	W93° 20' 14.29"



Point Table					
Point #	Description	Northing	Easting	Latitude	Longitude
13	CPT1	522619.3100	2635613.2300	N29° 55' 16.80"	W93° 22' 12.86"

Point Table					
Point #	Description	Northing	Easting	Latitude	Longitude
14	CPT2	521554.7700	2637072.8800	N29° 55' 06.52"	W93° 21' 56.06"



Point Table					
Point #	Description	Northing	Easting	Latitude	Longitude
15	CPT3	521171.7600	2638106.4100	N29° 55' 02.91"	W93° 21' 44.24"

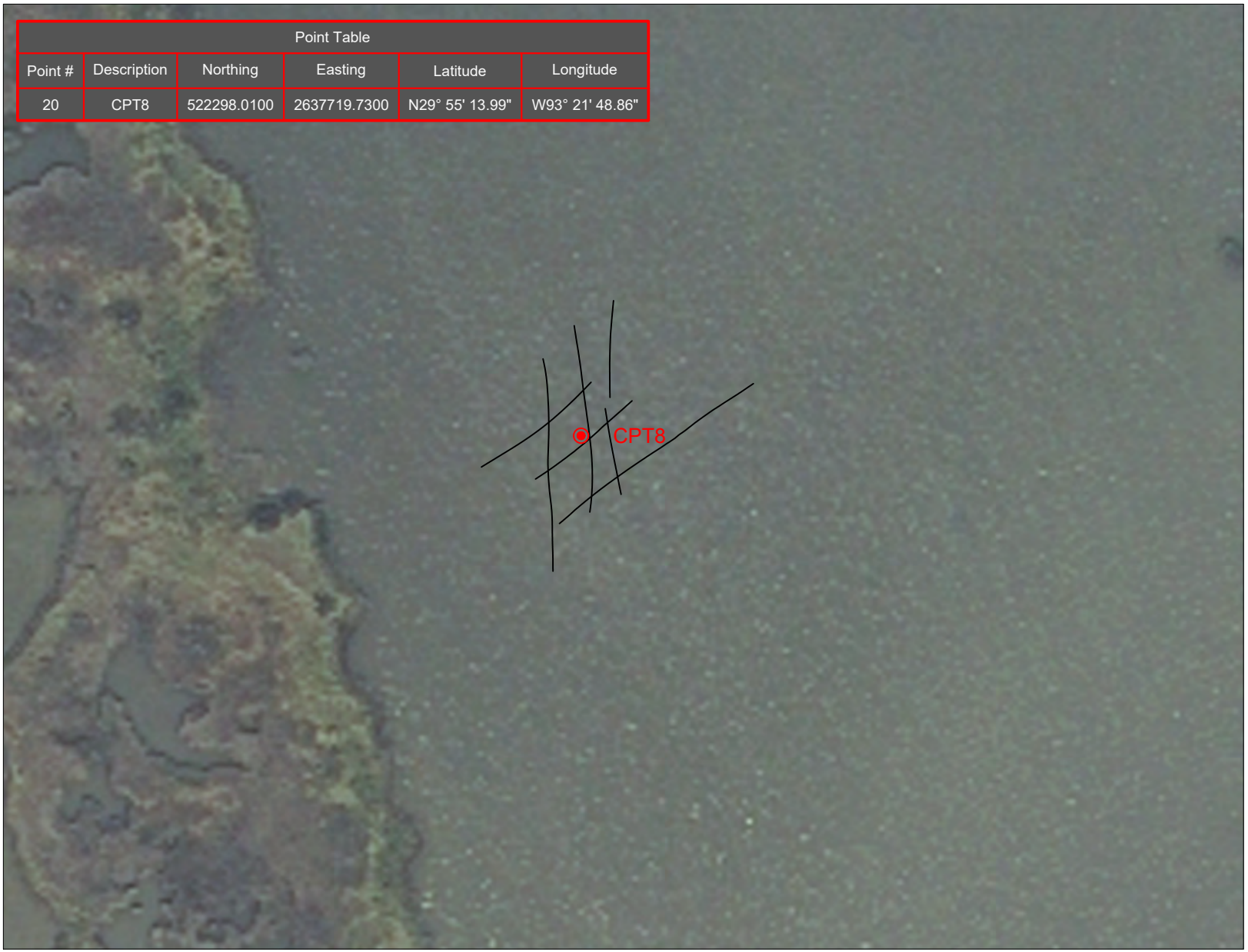
Point Table					
Point #	Description	Northing	Easting	Latitude	Longitude
16	CPT4	520971.5700	2639657.1400	N29° 55' 01.20"	W93° 21' 26.58"

Point Table					
Point #	Description	Northing	Easting	Latitude	Longitude
17	CPT5	522485.3100	2640097.5400	N29° 55' 16.26"	W93° 21' 21.88"

Point Table					
Point #	Description	Northing	Easting	Latitude	Longitude
18	CPT6	524713.4100	2639962.6300	N29° 55' 38.29"	W93° 21' 23.86"

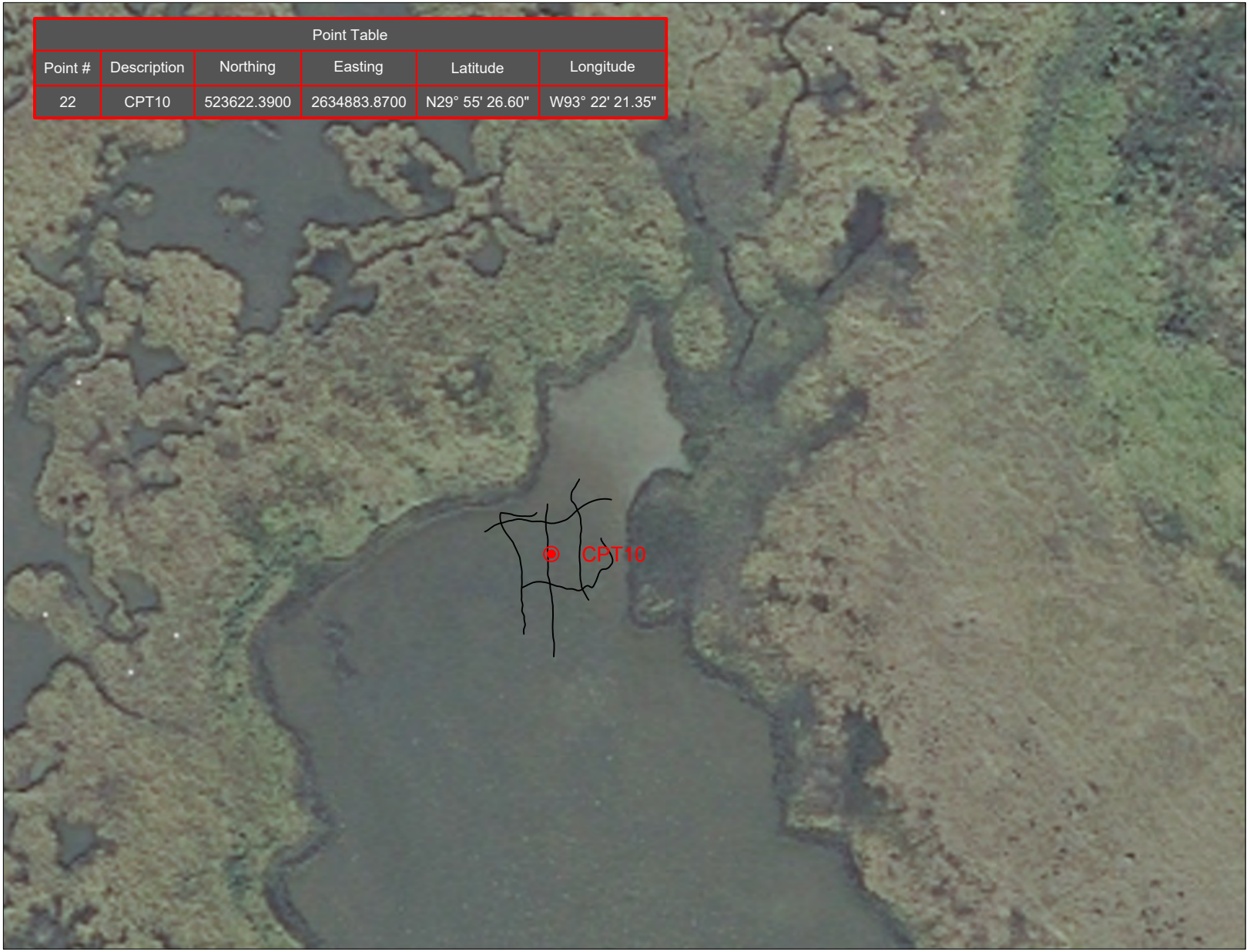

Point Table
Point # | Description | Northing | Easting | Latitude | Longitude
19 | CPT7 | 525528.2100 | 2637538.5000 | N29° 55' 45.93" | W93° 21' 51.57"
CPT7

Point Table					
Point #	Description	Northing	Easting	Latitude	Longitude
20	CPT8	522298.0100	2637719.7300	N29° 55' 13.99"	W93° 21' 48.86"



Point Table					
Point #	Description	Northing	Easting	Latitude	Longitude
21	CPT9	523169.8300	2640983.5200	N29° 55' 23.19"	W93° 21' 11.95"

Point Table					
Point #	Description	Northing	Easting	Latitude	Longitude
22	CPT10	523622.3900	2634883.8700	N29° 55' 26.60"	W93° 22' 21.35"

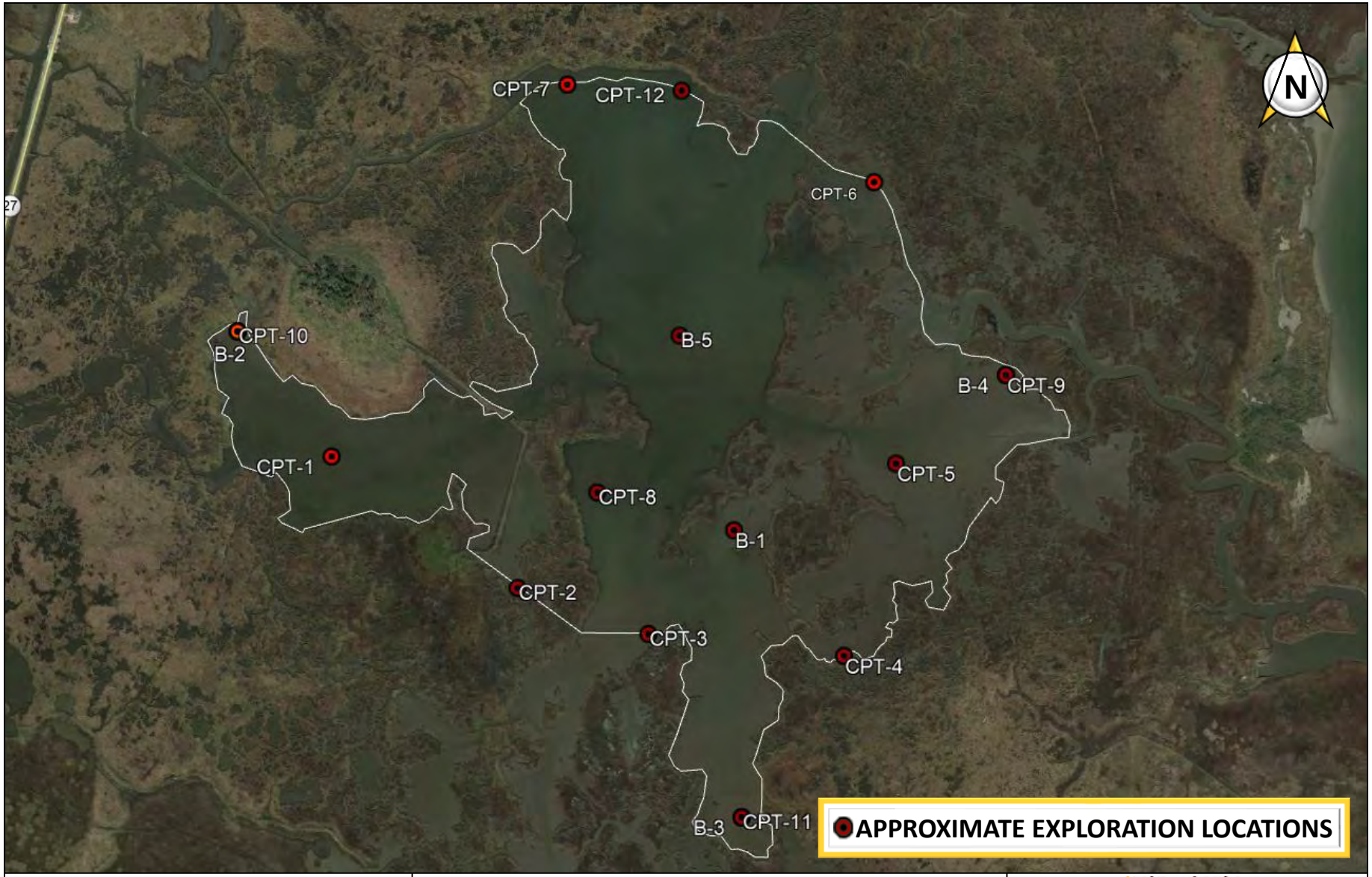


Point Table					
Point #	Description	Northing	Easting	Latitude	Longitude
23	CPT11	519709.2500	2638822.4600	N29° 54' 48.56"	W93° 21' 35.81"


Point Table
Point # | Description | Northing | Easting | Latitude | Longitude
24 | CPT12 | 525464.6400 | 2638445.5300 | N29° 55' 45.46" | W93° 21' 41.25"
CPT12

APPENDIX B

BORING LOCATION PLAN
BORING LOGS BORING LOGS AND CPT SOUNDING PLOTS
KEY TO TERMS AND SYMBOLS USED ON BORING LOGS



GEOTECHNICAL ENGINEERING SERVICES

Long Point Bayou Marsh Creation

Cameron, Louisiana

MARSH BORING LOCATION PLAN

PSI PROJECT NO.: 02541211

GOOGLE EARTH IMAGERY DATE: 1/2018

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GEOTECHNICAL ENGINEERING SERVICES

Long Point Bayou Marsh Creation

Cameron, Louisiana

CHANNEL BORING LOCATION PLAN

PSI PROJECT NO.: 02541211

GOOGLE EARTH IMAGERY DATE: 1/2018

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LOG OF BORING B-1

LONG POINT BAYOU MARSH CREATION
CAMERON PARISH, LOUISIANA

TYPE OF BORING: ROTARY WASH | LOCATION: MARSH AREA | PSI Project No.: 02541211

DEPTH, FT.	SOIL TYPE	USCS SYMBOL	SAMPLES	SOIL DESCRIPTION	N-BLOWS/FT.	MOISTURE CONTENT (%)	LIQUID LIMIT (LL)	PLASTIC LIMIT (PL)	PLASTICITY INDEX (PI)	% PASSING No. 200 SIEVE	SHEAR STRENGTH (tsf) HP	SHEAR STRENGTH (tsf) UC	SHEAR STRENGTH (tsf) TV	SHEAR STRENGTH (tsf) MV	SHEAR STRENGTH (tsf) UU	DRY UNIT WEIGHT (pcf)
0.0		OH		Very soft dark gray **ORGANIC CLAY**												
				- with roots, 0 to 2 feet		104							0.05			
2.5						107	112	31	81	93			0.10		0.06	49
5.0						156							0.02			
7.5		CL		Soft gray **LEAN CLAY**, with organics and silt partings		40	33	16	17	92			0.20		0.19	98
				- Peat layer, 8 feet to 8.5 feet		25							0.25			
10.0		CL		Firm to stiff gray **LEAN CLAY**, with silt												
				- Peat layer, 10 feet to 10.5 feet		30							0.55			
12.5						26							0.40		0.35	96
15.0		CL		Very stiff to hard gray **LEAN CLAY**	10-20-15											
				- 6.64% sand, 93.36% fines (23.17% clay), 14 to 16 feet	35	30	34	18	16	93						
17.5		CL		Very stiff to hard gray **LEAN CLAY WITH SAND**	12-16-22											
					38	22										
					9-12-15											
20.0					27	21										
					11-18-20											
22.5					38	23				72						
25.0		CL		Hard gray **SANDY LEAN CLAY**	10-16-20											
					36	23										
					12-18-22											
27.5					40	21										
					14-19-25											
30.0					44	21				60						
				BORING TERMINATED AT 30 FEET												

SHEAR STRENGTH (tsf): ○ HP ● UC △ TV ◆ MV ▲ UU; 0.0 0.5 1.0 1.5

DEPTH OF BORING: 30 FEET
DATE DRILLED: 6/28/20
NOTE:

▽ GROUNDWATER DURING DRILLING: N / A
▼ GROUNDWATER UPON COMPLETION: N / A
▼ DELAYED GROUNDWATER: N / A .

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LOG OF BORING B-2

LONG POINT BAYOU MARSH CREATION
CAMERON PARISH, LOUISIANA

TYPE OF BORING: ROTARY WASH | LOCATION: MARSH AREA | PSI Project No.: 02541211

DEPTH, FT.	SOIL TYPE	USCS SYMBOL	SAMPLES	SOIL DESCRIPTION	N-BLOWS/FT.	MOISTURE CONTENT (%)	LIQUID LIMIT (LL)	PLASTIC LIMIT (PL)	PLASTICITY INDEX (PI)	% PASSING No. 200 SIEVE	SHEAR STRENGTH (tsf) HP	SHEAR STRENGTH (tsf) UC	SHEAR STRENGTH (tsf) TV	SHEAR STRENGTH (tsf) MV	SHEAR STRENGTH (tsf) UU	DRY UNIT WEIGHT (pcf)
		OH		Dark gray **ORGANIC CLAY**												
		CH		Soft gray/brown **FAT CLAY**, with organics		51	86	23	63	99			0.15		0.15	74
2.5		CL		Firm to stiff gray/brown **LEAN CLAY**, trace organics		29							0.40			
5.0						27							0.45			
7.5						22	44	16	28				0.55		0.61	103
		CH		Very soft to soft gray **FAT CLAY**, with sand		41							0.20			
10.0				- with silt, 8 to 10 feet		33							0.15		0.09	83
12.5		SC		Medium dense brown **CLAYEY SAND**	4-6-9 15	24										
15.0					5-9-11 20	24				19						
17.5					10-9-8 17	26										
		CL		Very stiff brown **SANDY LEAN CLAY**	9-11-12 23	28	35	17	18	68						
20.0		SP		Dense brown **POORLY GRADED SAND**, with clay pockets	10-11-19 30	28										
22.5		CL		Very stiff to hard brown **SANDY LEAN CLAY**, trace sand and silt	12-19-23 42	35										
25.0					9-11-13 24	26										
		SC-SM		Medium dense brown **SILTY, CLAYEY SAND**	9-14-14 28	22										
27.5					10-14-14 28	23	24	20	4	31						
30.0				BORING TERMINATED AT 30 FEET												

DEPTH OF BORING: 30 FEET
DATE DRILLED: 6/30/20
NOTE:

▽ GROUNDWATER DURING DRILLING: N / A
▼ GROUNDWATER UPON COMPLETION: N / A
▼ DELAYED GROUNDWATER: N / A .

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LOG OF BORING B-3

LONG POINT BAYOU MARSH CREATION
CAMERON PARISH, LOUISIANA

TYPE OF BORING: ROTARY WASH | LOCATION: MARSH AREA | PSI Project No.: 02541211

DEPTH, FT.	SOIL TYPE	USCS SYMBOL	SAMPLES	SOIL DESCRIPTION	N-BLOWS/FT.	MOISTURE CONTENT (%)	LIQUID LIMIT (LL)	PLASTIC LIMIT (PL)	PLASTICITY INDEX (PI)	% PASSING No. 200 SIEVE	SHEAR STRENGTH (tsf) HP	SHEAR STRENGTH (tsf) UC	SHEAR STRENGTH (tsf) TV	SHEAR STRENGTH (tsf) MV	SHEAR STRENGTH (tsf) UU	DRY UNIT WEIGHT (pcf)
0.0		CH		Soft to firm gray **FAT CLAY**, intermittent organic soil layers and trace sand		33							0.15			
2.5						30	52	14	38	86			0.17		0.22	94
5.0						33					0.25					
7.5						21					0.42					
		CL		Very stiff gray **LEAN CLAY**, with trace sand		19					1.17				1.20	109
10.0		CH		Firm gray **FAT CLAY** - 2.25% sand, 97.75% fines (42.98% clay), 10 to 12 feet	3-4-3 7	37	64	15	49	98						
12.5		CL		Stiff to very stiff gray **LEAN CLAY WITH SAND**	6-7-9 16	19										
15.0					7-7-8 15	21	44	14	30	75						
17.5					7-8-9 17	21										
20.0					4-5-5 10	24										
		CL		Gray/brown **SANDY LEAN CLAY**	6-6-12 18	23										
22.5		SM		Medium dense to dense brown **SILTY SAND**	10-12-17 29	20				13						
25.0					8-15-13 28	20										
27.5					10-14-14 28	20				12						
30.0					10-15-18 33	19										
				BORING TERMINATED AT 30 FEET												

SHEAR STRENGTH (tsf): ○ HP ● UC △ TV ◆ MV ▲ UU — 0.0 0.5 1.0 1.5

DEPTH OF BORING: 30 FEET
DATE DRILLED: 6/29/20
NOTE:

▽ GROUNDWATER DURING DRILLING: N / A
▼ GROUNDWATER UPON COMPLETION: N / A
▼ DELAYED GROUNDWATER: N / A .

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LOG OF BORING B-4

LONG POINT BAYOU MARSH CREATION
CAMERON PARISH, LOUISIANA

TYPE OF BORING: ROTARY WASH | LOCATION: MARSH AREA | PSI Project No.: 02541211

DEPTH, FT.	SOIL TYPE	USCS SYMBOL	SAMPLES	SOIL DESCRIPTION	N-BLOWS/FT.	MOISTURE CONTENT (%)	LIQUID LIMIT (LL)	PLASTIC LIMIT (PL)	PLASTICITY INDEX (PI)	% PASSING No. 200 SIEVE	SHEAR STRENGTH (tsf) HP	SHEAR STRENGTH (tsf) UC	SHEAR STRENGTH (tsf) TV	SHEAR STRENGTH (tsf) MV	SHEAR STRENGTH (tsf) UU	DRY UNIT WEIGHT (pcf)
		CH		Very soft to soft gray **FAT CLAY WITH SAND**, with organics		50							0.20			
2.5						30	56	17	39	83			0.10		0.07	83
		CH		Firm to stiff gray **FAT CLAY WITH SAND**, with silt		32							0.40			
5.0				- with organics, 4 to 6 feet												
						26							0.75			
7.5				- trace organics, 8 to 10 feet												
						24	56	16	40	84			0.60		0.73	100
10.0																
						27							0.40			
12.5		CL		Stiff to very stiff tan **LEAN CLAY WITH SAND**	4-5-8											
					13	25										
				- 29.17% sand, 70.83% fines (20.24% clay), 14 to 16 feet	6-13-15											
15.0					28	23	30	19	11	71						
		SP-SM		Dense brown **POORLY GRADED SAND WITH SILT**	6-17-26											
					43	25										
17.5					12-14-24											
					38	22										
20.0					7-14-26											
					40	21				11						
22.5					9-19-28											
					47	22										
25.0					9-18-29											
					47	20										
					9-17-29											
27.5					46	22										
					8-19-31											
					50	21				10						
30.0				BORING TERMINATED AT 30 FEET												

SHEAR STRENGTH (tsf): ○ HP ● UC △ TV ◆ MV ▲ UU — 0.0 0.5 1.0 1.5

DEPTH OF BORING: 30 FEET
DATE DRILLED: 6/24/20
NOTE:

▽ GROUNDWATER DURING DRILLING: N / A
▼ GROUNDWATER UPON COMPLETION: N / A
▼ DELAYED GROUNDWATER: N / A .

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LOG OF BORING B-5

LONG POINT BAYOU MARSH CREATION
CAMERON PARISH, LOUISIANA

TYPE OF BORING: ROTARY WASH | LOCATION: MARSH AREA | PSI Project No.: 02541211

DEPTH, FT.	SOIL TYPE	USCS SYMBOL	SAMPLES	SOIL DESCRIPTION	N-BLOWS/FT.	MOISTURE CONTENT (%)	LIQUID LIMIT (LL)	PLASTIC LIMIT (PL)	PLASTICITY INDEX (PI)	% PASSING No. 200 SIEVE	SHEAR STRENGTH (tsf) ○ HP ● UC △ TV ◆ MV ▲ UU 0.0 0.5 1.0 1.5	SHEAR STRENGTH (tsf) HP	UC	TV	MV	UU	DRY UNIT WEIGHT (pcf)
		OH		Very soft dark gray **ORGANIC CLAY**		97					△			0.05			
2.5		CH		Soft dark gray/gray **FAT CLAY**, with organics and trace sand		35	53	15	38	94	▲					0.19	87
5.0		CH		Stiff gray **FAT CLAY**, trace organics - with silt, 4 to 6 feet		30					△			0.60			
7.5		CL		Soft to firm gray **LEAN CLAY**, trace sand	1-2-2 4	34											
10.0				- 9.96% sand, 90.04% fines (41.71% clay), 10 to 12 feet	3-3-3 6 2-2-3 5	29 32	48	15	33	90							
12.5		CL		Stiff light gray **SANDY LEAN CLAY**	5-5-6 11	21											
15.0					4-5-6 11	22											
17.5					4-5-6 11	24	40	14	26	54							
20.0		CL		Stiff to very stiff light gray **LEAN CLAY WITH SAND**	5-6-9 15	21											
22.5					7-8-10 18 8-10-12 22	23 24											
25.0					10-12-15 27	22	36	15	21	75							
27.5		CL		Hard light gray **LEAN CLAY WITH SAND**	12-14-19 33	23											
30.0					13-18-22 40	20											
				BORING TERMINATED AT 30 FEET													

DEPTH OF BORING: 30 FEET
DATE DRILLED: 6/27/20
NOTE:

▽ GROUNDWATER DURING DRILLING: N / A
▼ GROUNDWATER UPON COMPLETION: N / A
▼ DELAYED GROUNDWATER: N / A .

JEFFERSON - FULL SPT AND MINIVANE V2 - PSIHOUSTON.GDT - 9/16/20 13:21 - 0254

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LOG OF BORING B-6

LONG POINT BAYOU MARSH CREATION
CAMERON PARISH, LOUISIANA

TYPE OF BORING: PISTON SAMPLER | LOCATION: CALCASIEU SHIP CHANNEL | PSI Project No.: 02541211

DEPTH, FT.	SOIL TYPE	USCS SYMBOL	SAMPLES	SOIL DESCRIPTION	N-BLOWS/FT.	MOISTURE CONTENT (%)	LIQUID LIMIT (LL)	PLASTIC LIMIT (PL)	PLASTICITY INDEX (PI)	% PASSING No. 200 SIEVE	SHEAR STRENGTH (tsf) ○ HP ● UC △ TV ◆ MV ▲ UU 0.0 0.5 1.0 1.5	SHEAR STRENGTH (tsf) HP	UC	TV	MV	UU	DRY UNIT WEIGHT (pcf)
		CH		Gray **FAT CLAY**, with silt pockets													
2.5				-2.5% sand, 97.5% fines (49.67% clay), 0 to 5 feet		185	123	31	92	98							
5.0				BORING TERMINATED AT APPROXIMATE EL. -48.54 FEET													
7.5																	
10.0																	

DEPTH OF BORING: 5 FEET
DATE DRILLED: 5/26/20
NOTE: N / A = NOT AVAILABLE

▽ GROUNDWATER DURING DRILLING: N / A
▼ GROUNDWATER UPON COMPLETION: N / A
▼ DELAYED GROUNDWATER: N / A .

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LOG OF BORING B-7

LONG POINT BAYOU MARSH CREATION
CAMERON PARISH, LOUISIANA

TYPE OF BORING: PISTON SAMPLER | LOCATION: CALCASIEU SHIP CHANNEL | PSI Project No.: 02541211

DEPTH, FT.	SOIL TYPE	USCS SYMBOL	SAMPLES	SOIL DESCRIPTION	N-BLOWS/FT.	MOISTURE CONTENT (%)	LIQUID LIMIT LL	PLASTIC LIMIT PL	PLASTICITY INDEX PI	% PASSING No. 200 SIEVE	SHEAR STRENGTH (tsf) ○ HP ● UC △ TV ◆ MV ▲ UU 0.0 0.5 1.0 1.5	SHEAR STRENGTH (tsf) HP	UC	TV	MV	UU	DRY UNIT WEIGHT (pcf)
		CH		Gray **FAT CLAY**, with silt pockets													
2.5				-2.5% sand, 97.5% fines (49.74% clay), 0 to 5 feet		155	92	29	63	98							
5.0				BORING TERMINATED AT APPROXIMATE EL. -47.24 FEET													
7.5																	
10.0																	

DEPTH OF BORING: 5 FEET
DATE DRILLED: 5/27/20
NOTE: N / A = NOT AVAILABLE

▽ GROUNDWATER DURING DRILLING: N / A
▼ GROUNDWATER UPON COMPLETION: N / A
▼ DELAYED GROUNDWATER: N / A .

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LOG OF BORING B-8

LONG POINT BAYOU MARSH CREATION
CAMERON PARISH, LOUISIANA

TYPE OF BORING: PISTON SAMPLER | LOCATION: CALCASIEU SHIP CHANNEL | PSI Project No.: 02541211

DEPTH, FT.	SOIL TYPE	USCS SYMBOL	SAMPLES	SOIL DESCRIPTION	N-BLOWS/FT.	MOISTURE CONTENT (%)	LIQUID LIMIT (LL)	PLASTIC LIMIT (PL)	PLASTICITY INDEX (PI)	% PASSING No. 200 SIEVE	SHEAR STRENGTH (tsf) ○ HP ● UC △ TV ◆ MV ▲ UU 0.0 0.5 1.0 1.5	SHEAR STRENGTH (tsf) HP	UC	TV	MV	UU	DRY UNIT WEIGHT (pcf)
		CH		Gray **FAT CLAY**, with silt pockets													
2.5				-3.16% sand, 96.84% fines (49.75% clay), 0 to 5 feet		128	94	30	64	97							
5.0				BORING TERMINATED AT APPROXIMATE EL. -43.9 FEET													
7.5																	
10.0																	

DEPTH OF BORING: 5 FEET
DATE DRILLED: 5/27/20
NOTE: N / A = NOT AVAILABLE

▽ GROUNDWATER DURING DRILLING: N / A
▼ GROUNDWATER UPON COMPLETION: N / A
▼ DELAYED GROUNDWATER: N / A .

JEFFERSON - FULL SPT AND MINIVANE V2 - PSIHOUSTON.GDT - 8/11/20 14:32 - 0254

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LOG OF BORING B-9

LONG POINT BAYOU MARSH CREATION
CAMERON PARISH, LOUISIANA

TYPE OF BORING: PISTON SAMPLER | LOCATION: CALCASIEU SHIP CHANNEL | PSI Project No.: 02541211

DEPTH, FT.	SOIL TYPE	USCS SYMBOL	SAMPLES	SOIL DESCRIPTION	N-BLOWS/FT.	MOISTURE CONTENT (%)	LIQUID LIMIT (LL)	PLASTIC LIMIT (PL)	PLASTICITY INDEX (PI)	% PASSING No. 200 SIEVE	SHEAR STRENGTH (tsf) ○ HP ● UC △ TV ◆ MV ▲ UU 0.0 0.5 1.0 1.5	SHEAR STRENGTH (tsf) HP	UC	TV	MV	UU	DRY UNIT WEIGHT (pcf)
		CH		Gray **FAT CLAY**, with silt pockets													
2.5				-1.02% sand, 98.98% fines (52.53% clay), 0 to 5 feet		86	72	23	49	99							
5.0				BORING TERMINATED AT APPROXIMATE EL. -45.17 FEET													
7.5																	
10.0																	

DEPTH OF BORING: 5 FEET
DATE DRILLED: 5/28/20
NOTE: N / A = NOT AVAILABLE

▽ GROUNDWATER DURING DRILLING: N / A
▼ GROUNDWATER UPON COMPLETION: N / A
▼ DELAYED GROUNDWATER: N / A .

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(504) 733-9411

LOG OF BORING B-10

LONG POINT BAYOU MARSH CREATION
CAMERON PARISH, LOUISIANA

TYPE OF BORING: PISTON SAMPLER | LOCATION: CALCASIEU SHIP CHANNEL | PSI Project No.: 02541211

DEPTH, FT.	SOIL TYPE	USCS SYMBOL	SAMPLES	SOIL DESCRIPTION	N-BLOWS/FT.	MOISTURE CONTENT (%)	LIQUID LIMIT (LL)	PLASTIC LIMIT (PL)	PLASTICITY INDEX (PI)	% PASSING No. 200 SIEVE	SHEAR STRENGTH (tsf) ○ HP ● UC △ TV ◆ MV ▲ UU 0.0 0.5 1.0 1.5	SHEAR STRENGTH (tsf) HP	UC	TV	MV	UU	DRY UNIT WEIGHT (pcf)
		CH		Gray **FAT CLAY**, with silt pockets													
2.5				-6.53% sand, 93.47% fines (50.43% clay), 0 to 5 feet		102	100	27	73	93							
5.0				BORING TERMINATED AT APPROXIMATE EL. -45.6 FEET													
7.5																	
10.0																	

DEPTH OF BORING: 5 FEET
DATE DRILLED: 5/28/20
NOTE: N / A = NOT AVAILABLE

▽ GROUNDWATER DURING DRILLING: N / A
▼ GROUNDWATER UPON COMPLETION: N / A
▼ DELAYED GROUNDWATER: N / A .

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LOG OF BORING B-11

LONG POINT BAYOU MARSH CREATION
CAMERON PARISH, LOUISIANA

TYPE OF BORING: PISTON SAMPLER | LOCATION: CALCASIEU SHIP CHANNEL | PSI Project No.: 02541211

DEPTH, FT.	SOIL TYPE	USCS SYMBOL	SAMPLES	SOIL DESCRIPTION	N-BLOWS/FT.	MOISTURE CONTENT (%)	LIQUID LIMIT (LL)	PLASTIC LIMIT (PL)	PLASTICITY INDEX (PI)	% PASSING No. 200 SIEVE	SHEAR STRENGTH (tsf) ○ HP ● UC △ TV ◆ MV ▲ UU 0.0 0.5 1.0 1.5	SHEAR STRENGTH (tsf) HP	UC	TV	MV	UU	DRY UNIT WEIGHT (pcf)
		CH		Gray **FAT CLAY**, with silt pockets													
2.5				-5.77% sand, 94.23% fines (57.01% clay), 0 to 5 feet		66	79	25	54	94							
5.0				BORING TERMINATED AT APPROXIMATE EL. -46.76 FEET													
7.5																	
10.0																	

DEPTH OF BORING: 5 FEET
DATE DRILLED: 5/29/20
NOTE: N / A = NOT AVAILABLE

▽ GROUNDWATER DURING DRILLING: N / A
▼ GROUNDWATER UPON COMPLETION: N / A
▼ DELAYED GROUNDWATER: N / A .

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LOG OF BORING B-12

LONG POINT BAYOU MARSH CREATION
CAMERON PARISH, LOUISIANA

TYPE OF BORING: PISTON SAMPLER | LOCATION: CALCASIEU SHIP CHANNEL | PSI Project No.: 02541211

DEPTH, FT.	SOIL TYPE	USCS SYMBOL	SAMPLES	SOIL DESCRIPTION	N-BLOWS/FT.	MOISTURE CONTENT (%)	LIQUID LIMIT (LL)	PLASTIC LIMIT (PL)	PLASTICITY INDEX (PI)	% PASSING No. 200 SIEVE	SHEAR STRENGTH (tsf) ○ HP ● UC △ TV ◆ MV ▲ UU 0.0 0.5 1.0 1.5	SHEAR STRENGTH (tsf) HP	UC	TV	MV	UU	DRY UNIT WEIGHT (pcf)
		CH		Gray **FAT CLAY WITH SAND**, with silt pockets													
2.5				-15.95% sand, 84.05% fines (42.35% clay), 0 to 5 feet		75	70	22	48	84							
5.0				BORING TERMINATED AT APPROXIMATE EL. -45.49 FEET													
7.5																	
10.0																	

DEPTH OF BORING: 5 FEET
DATE DRILLED: 5/29/20
NOTE: N / A = NOT AVAILABLE

▽ GROUNDWATER DURING DRILLING: N / A
▼ GROUNDWATER UPON COMPLETION: N / A
▼ DELAYED GROUNDWATER: N / A .

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CPT: CPT-01

Total depth: 13.98 ft, Date: 6/29/2020

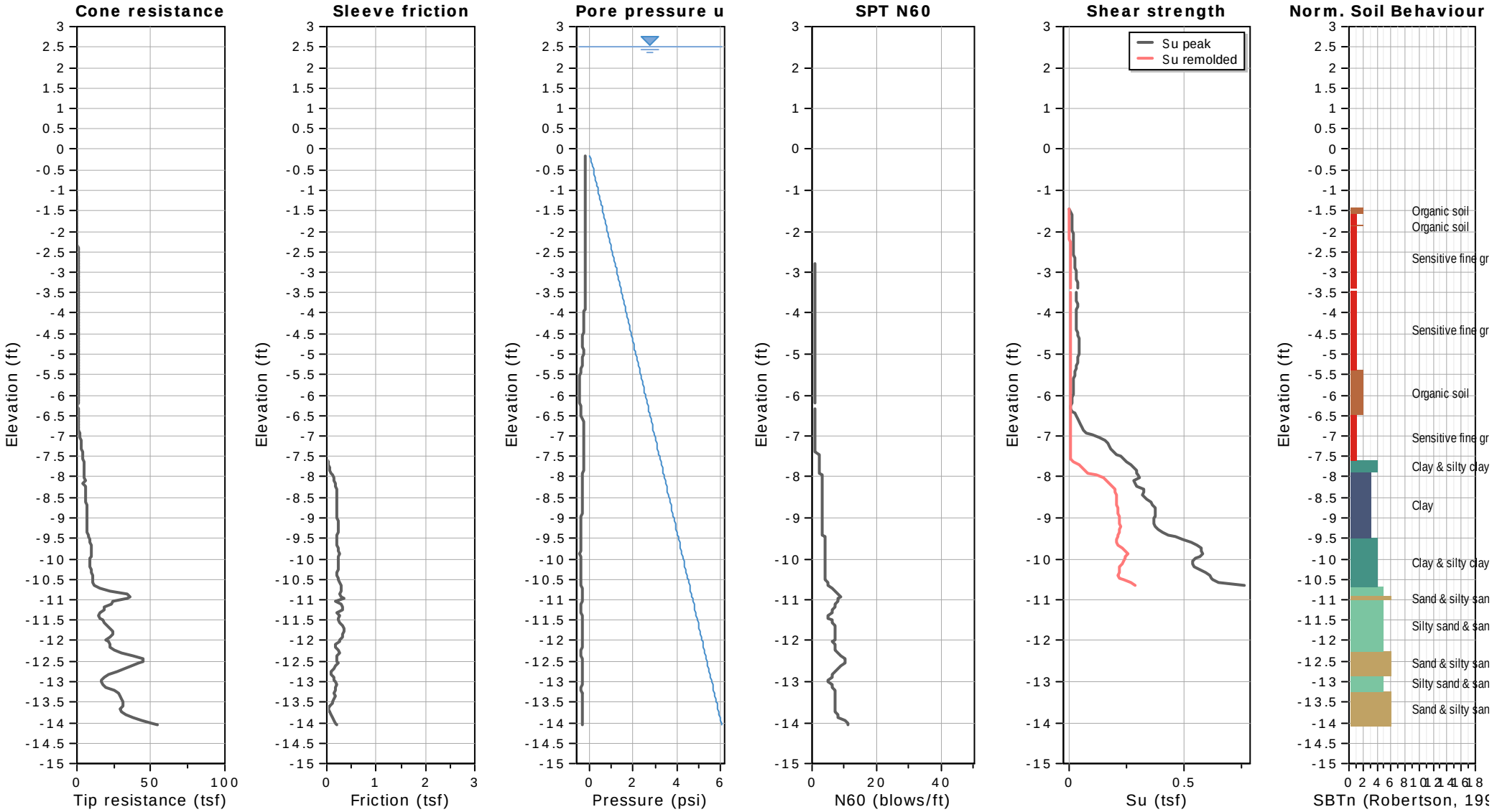
Mudline Elevation: -0.09 ft

Cone Type: 60° 1.4" Diam. Type 2 Electric Cone Penetrometer

Cone Operator: Charley Baker

Project: 02541211 - Long Point Marsh Creation

Location: Hackberry, Louisiana



CPT: CPT-02

Total depth: 13.58 ft, Date: 6/29/2020

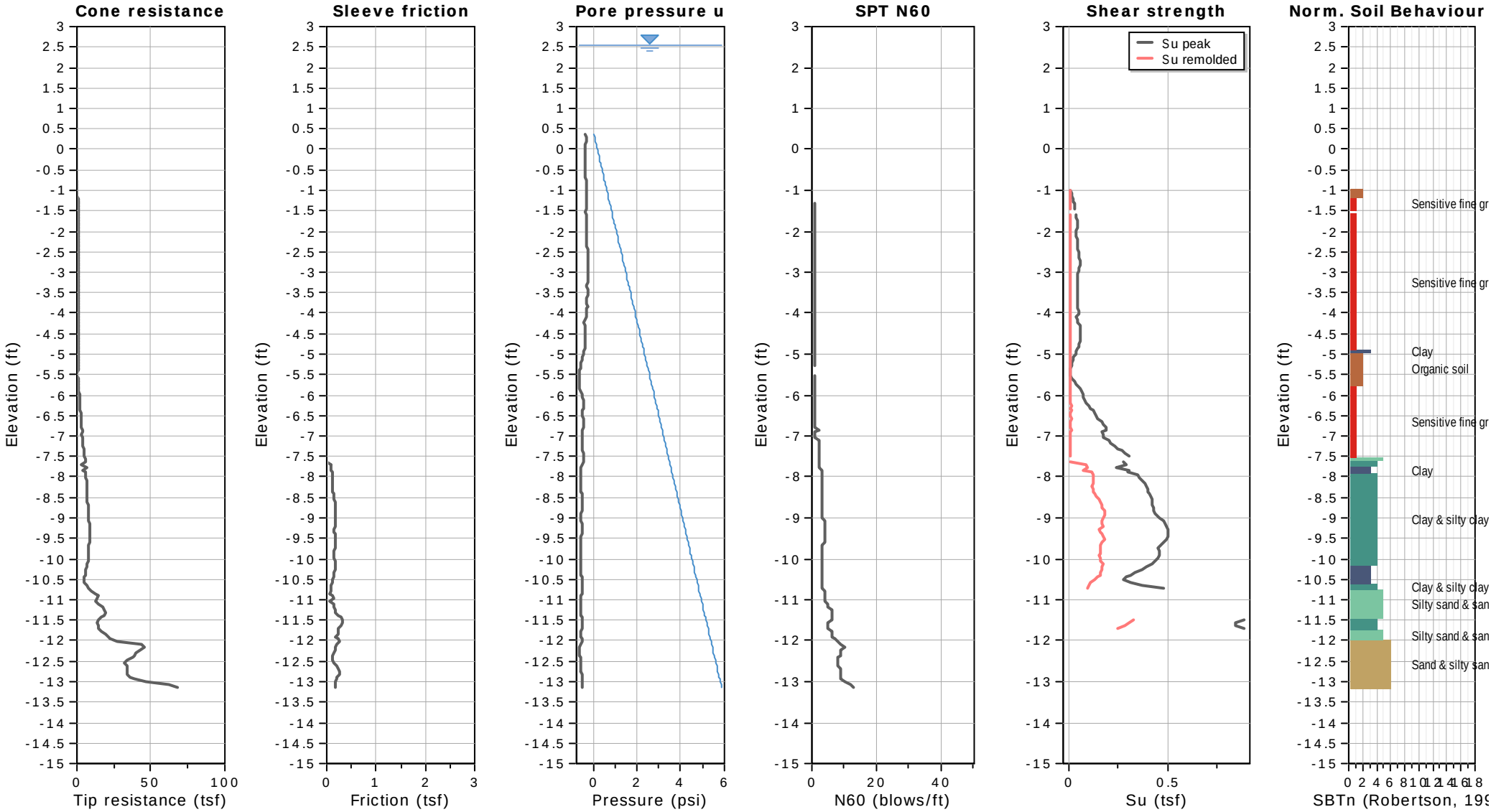
Mudline Elevation: 0.44 ft

Cone Type: 60° 1.4" Diam. Type 2 Electric Cone Penetrometer

Cone Operator: Charley Baker

Project: 02541211 - Long Point Marsh Creation

Location: Hackberry, Louisiana



CPT: CPT-03

Total depth: 13.12 ft, Date: 6/29/2020

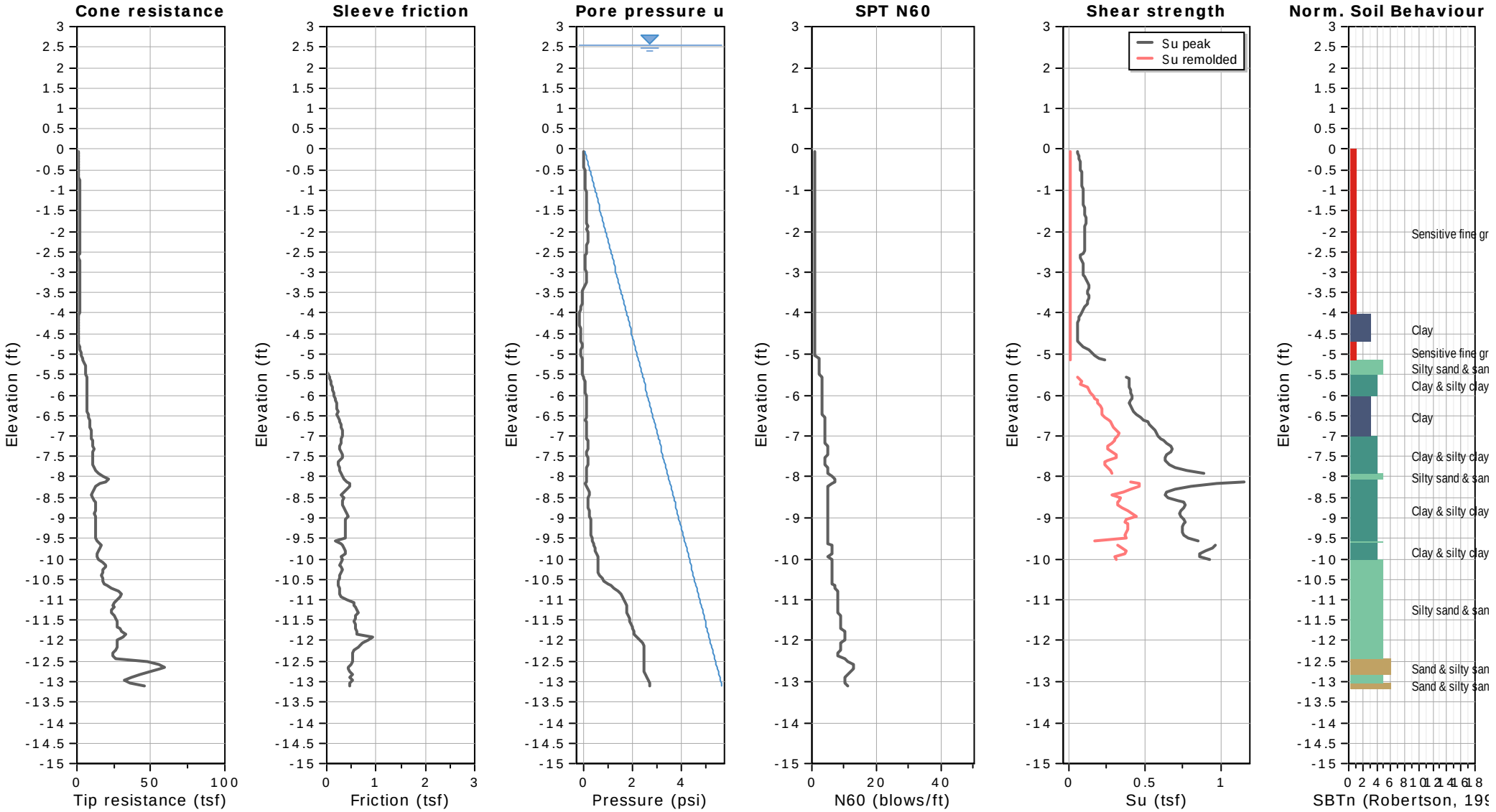
Mudline Elevation: 0.03 ft

Cone Type: 60° 1.4" Diam. Type 2 Electric Cone Penetrometer

Cone Operator: Charley Baker

Project: 02541211 - Long Point Marsh Creation

Location: Hackberry, Louisiana



CPT: CPT-04

Total depth: 12.47 ft, Date: 6/29/2020

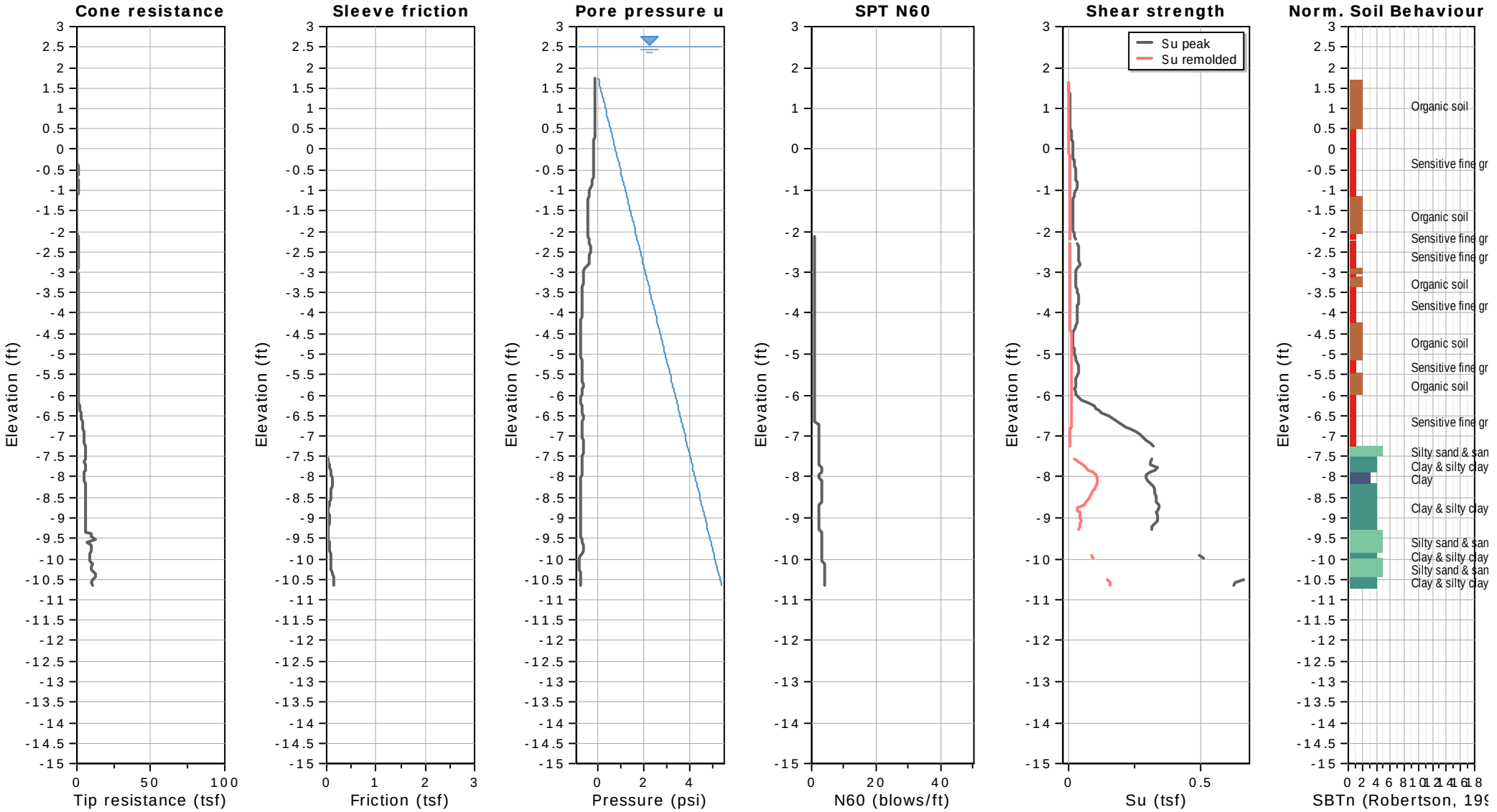
Mudline Elevation: 1.82 ft

Cone Type: 60° 1.4" Diam. Type 2 Electric Cone Penetrometer

Cone Operator: Charley Baker

Project: 02541211 - Long Point Marsh Creation

Location: Hackberry, Louisiana



CPT: CPT-05

Total depth: 11.15 ft, Date: 6/26/2020

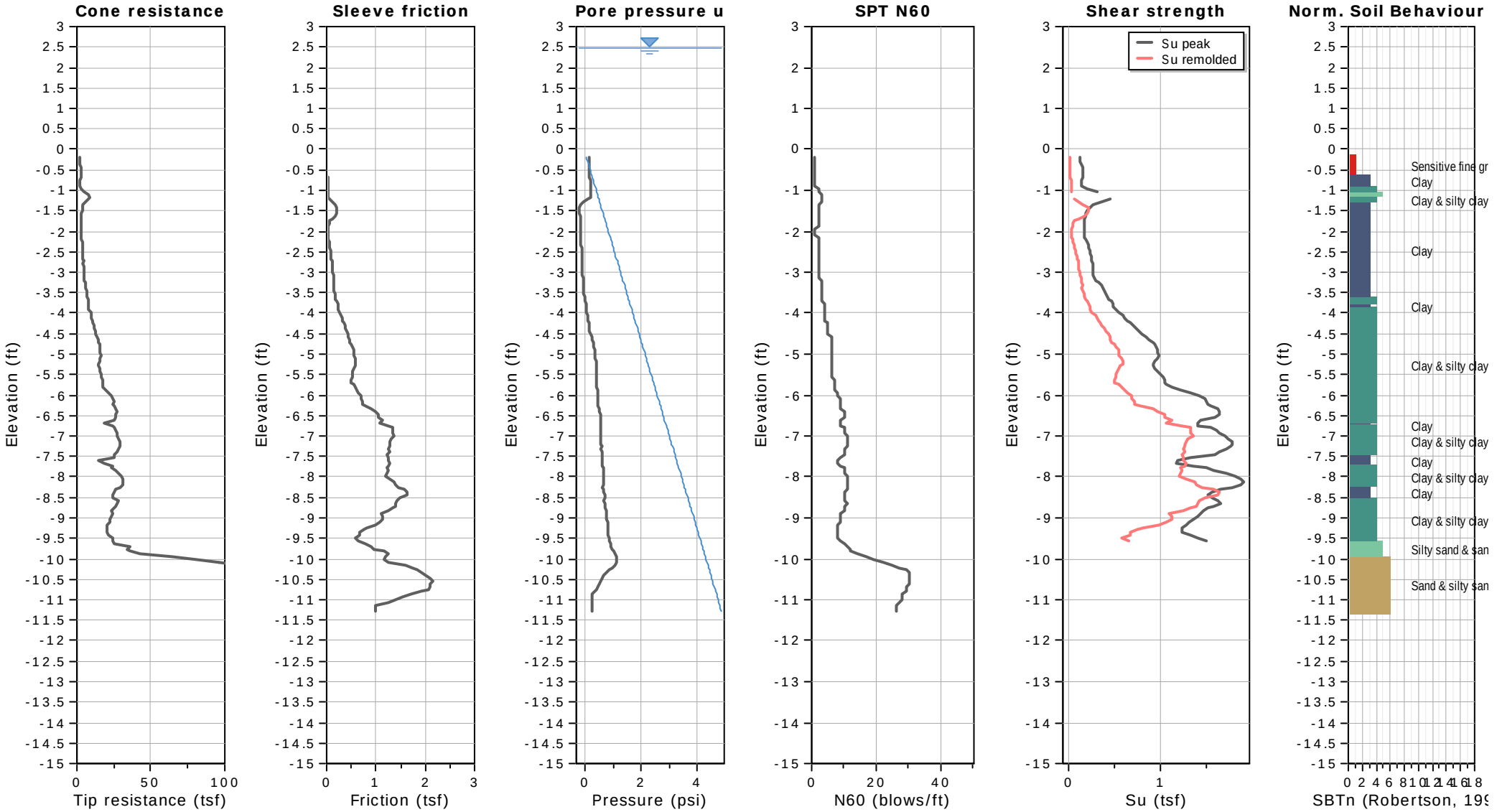
Mudline Elevation: -0.11 ft

Cone Type: 60° 1.4" Diam. Type 2 Electric Cone Penetrometer

Cone Operator: Charley Baker

Project: 02541211 - Long Point Marsh Creation

Location: Hackberry, Louisiana



CPT: CPT-06

Total depth: 9.32 ft, Date: 6/29/2020

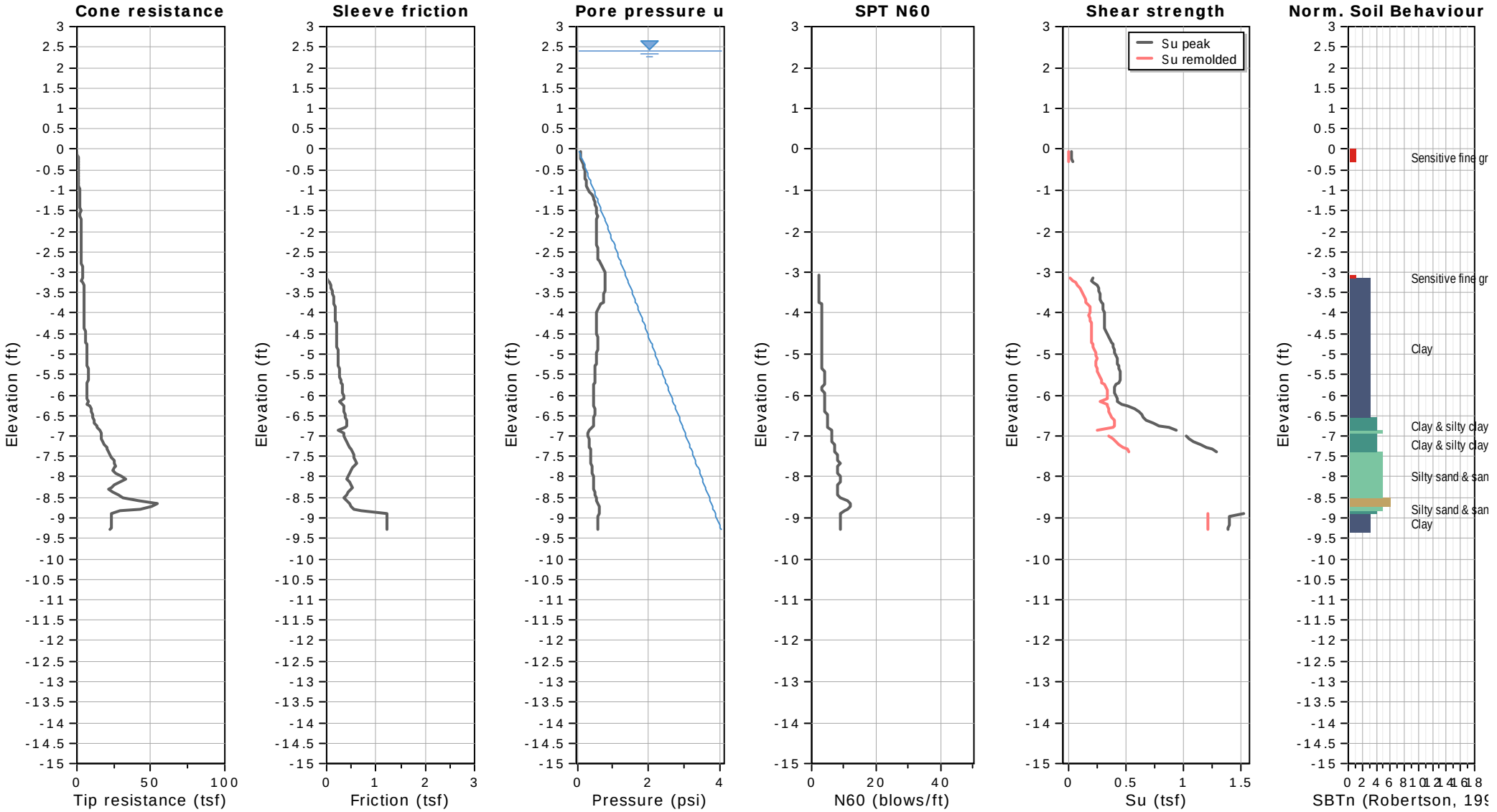
Mudline Elevation: 0.02 ft

Cone Type: 60° 1.4" Diam. Type 2 Electric Cone Penetrometer

Cone Operator: Charley Baker

Project: 02541211 - Long Point Marsh Creation

Location: Hackberry, Louisiana



CPT: CPT-07

Total depth: 8.79 ft, Date: 6/29/2020

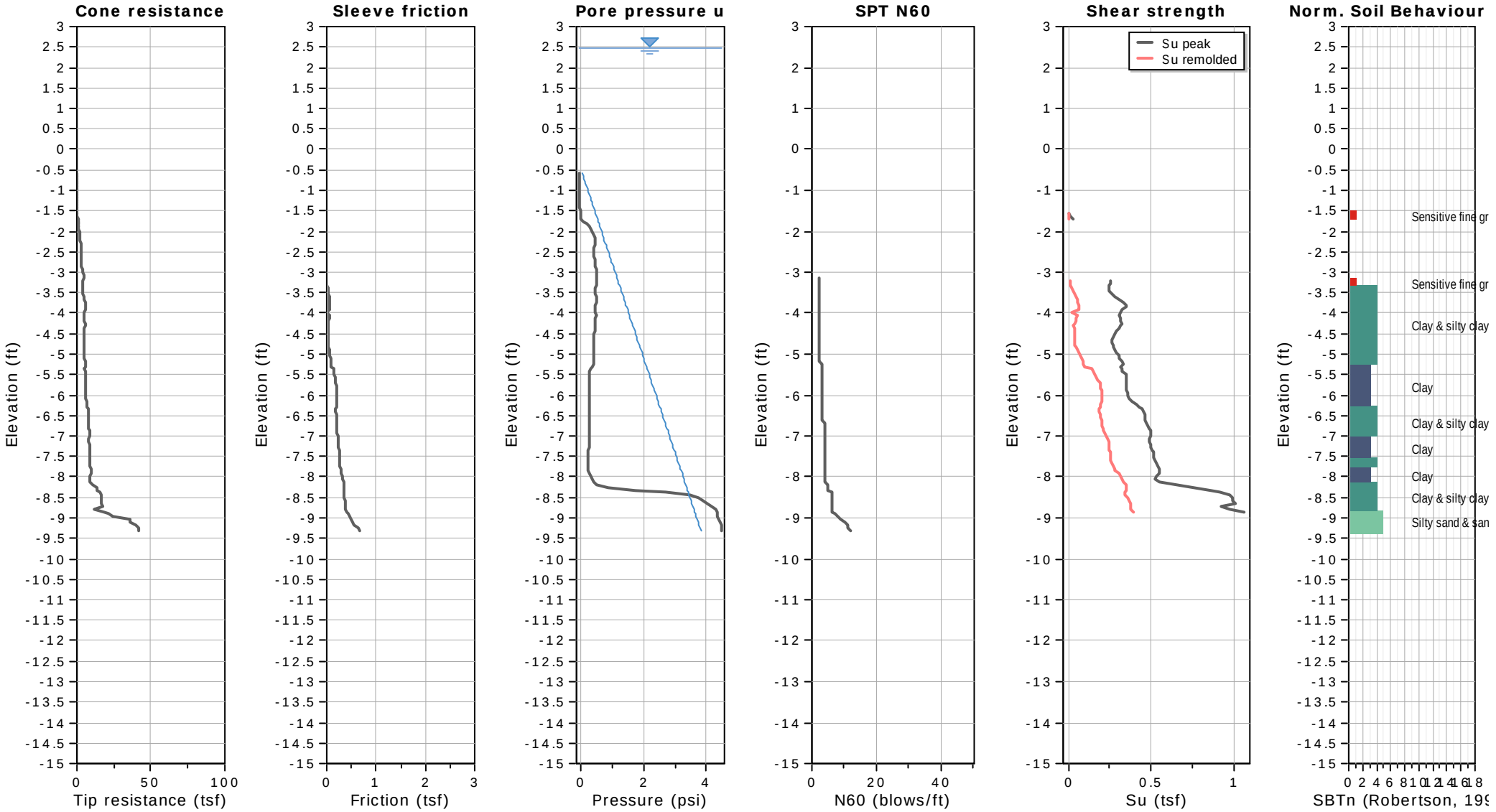
Mudline Elevation: -0.51 ft

Cone Type: 60° 1.4" Diam. Type 2 Electric Cone Penetrometer

Cone Operator: Charley Baker

Project: 02541211 - Long Point Marsh Creation

Location: Hackberry, Louisiana



CPT: CPT-08

Total depth: 9.38 ft, Date: 6/29/2020

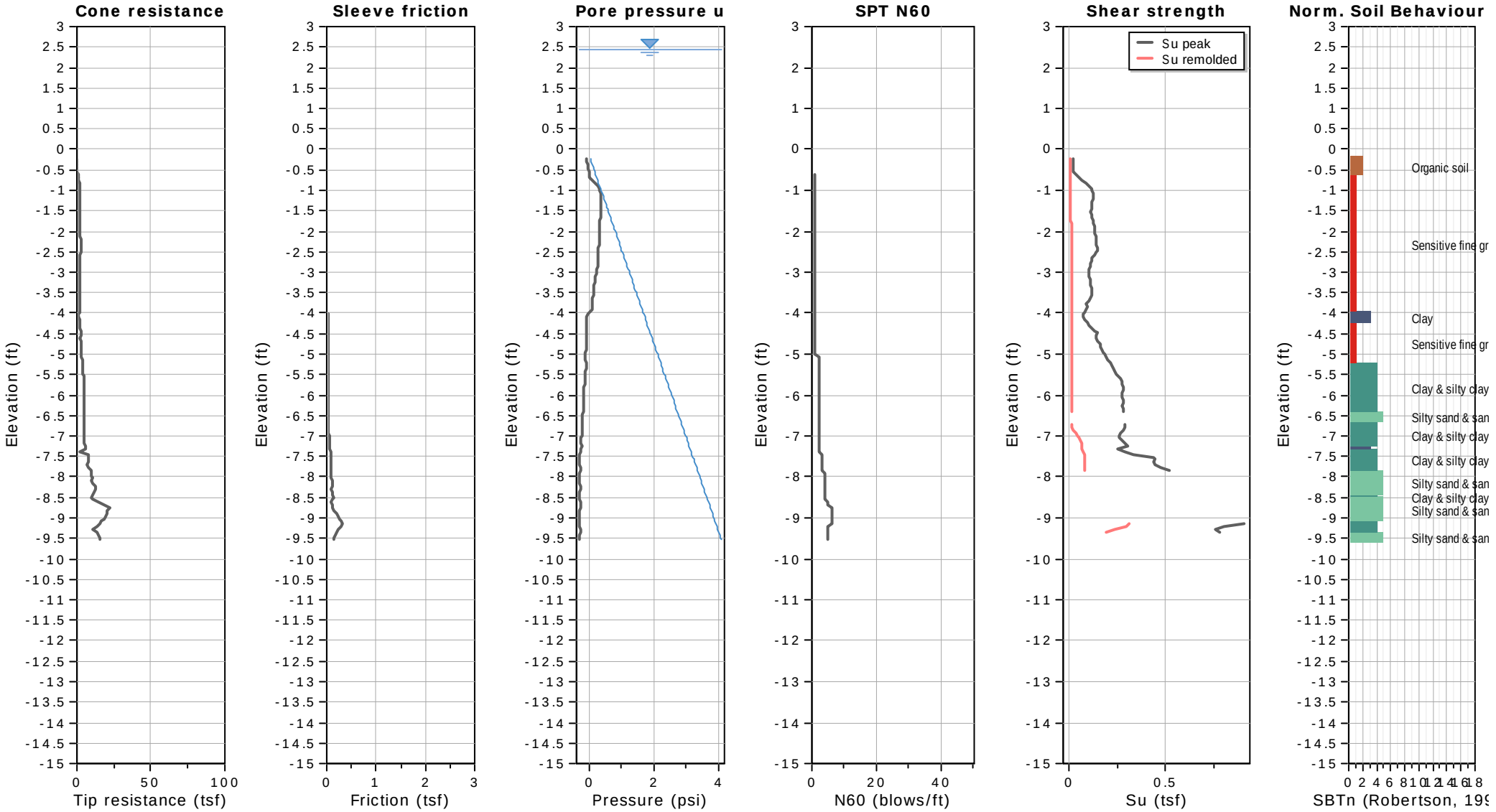
Mudline Elevation: -0.16 ft

Cone Type: 60° 1.4" Diam. Type 2 Electric Cone Penetrometer

Cone Operator: Charley Baker

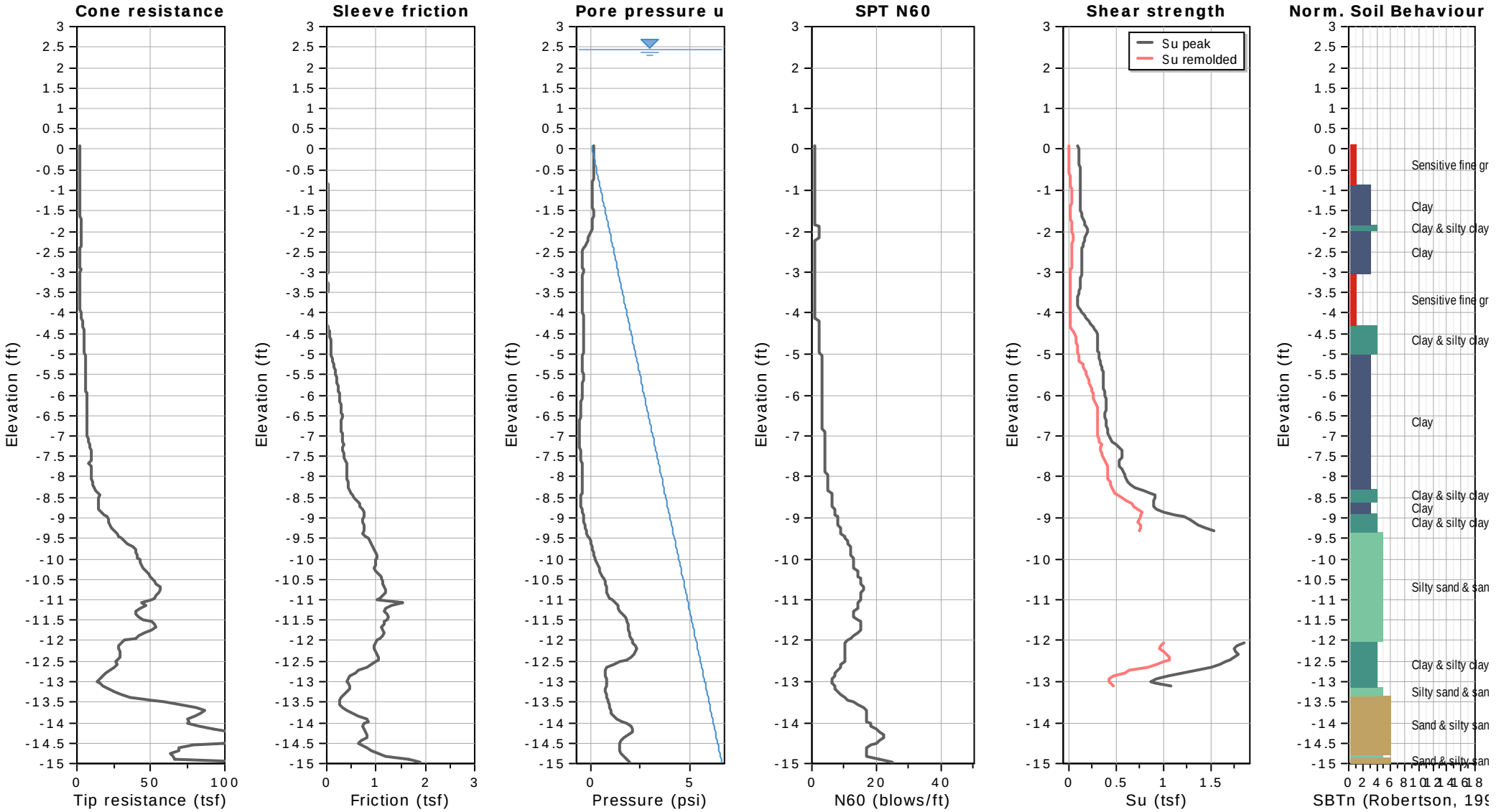
Project: 02541211 - Long Point Marsh Creation

Location: Hackberry, Louisiana



Project: 02541211 - Long Point Marsh Creation
Location: Hackberry, Louisiana

CPT: CPT-09
Total depth: 15.09 ft, Date: 6/25/2020
Mudline Elevation: 0.14 ft
Cone Type: 60° 1.4" Diam. Type 2 Electric Cone Penetrometer
Cone Operator: Charley Baker



CPT: CPT-10

Total depth: 14.30 ft, Date: 6/29/2020

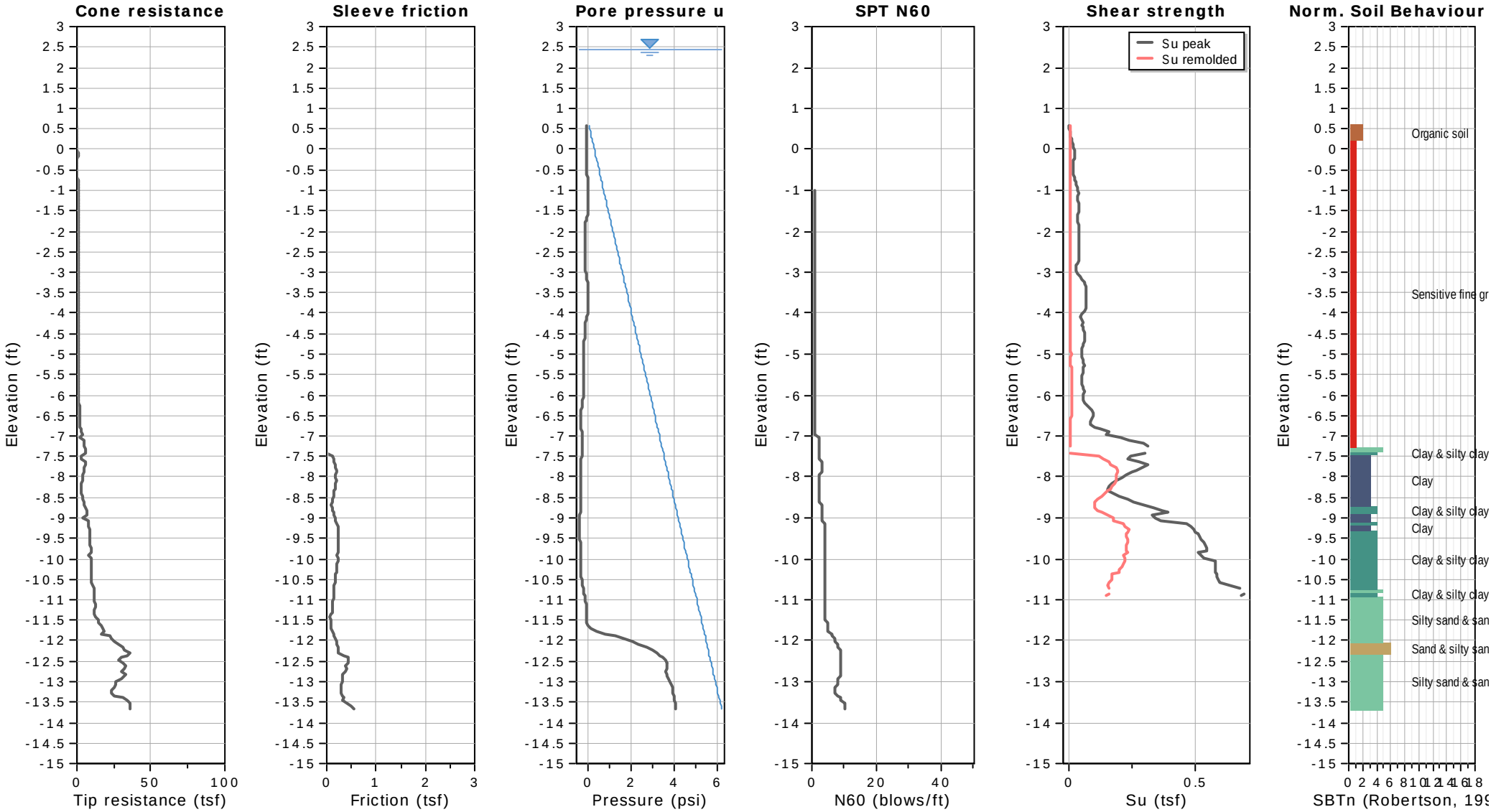
Mudline Elevation: 0.64 ft

Cone Type: 60° 1.4" Diam. Type 2 Electric Cone Penetrometer

Cone Operator: Charley Baker

Project: 02541211 - Long Point Marsh Creation

Location: Hackberry, Louisiana



CPT: CPT-11

Total depth: 11.48 ft, Date: 6/29/2020

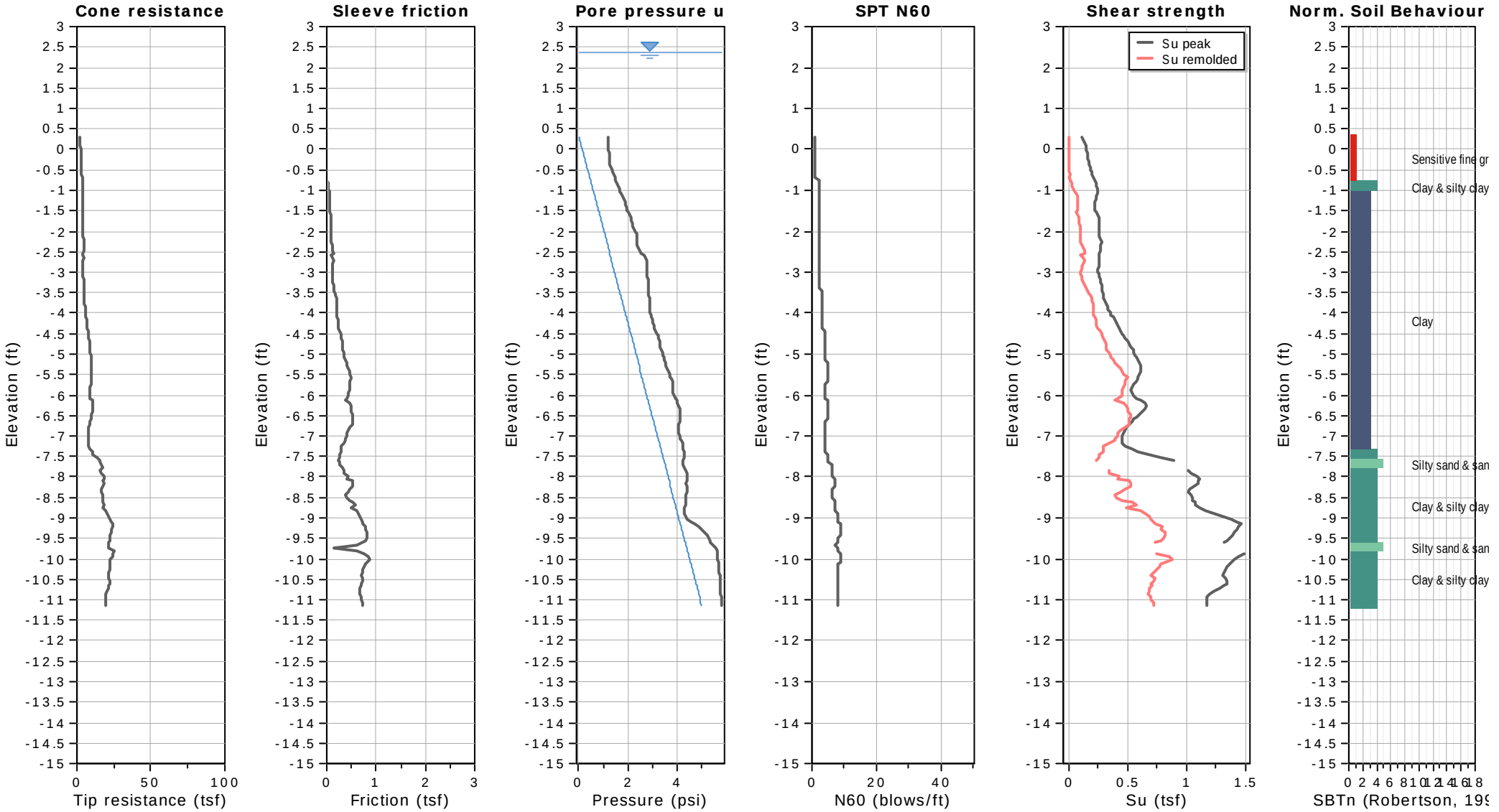
Mudline Elevation: 0.36 ft

Cone Type: 60° 1.4" Diam. Type 2 Electric Cone Penetrometer

Cone Operator: Charley Baker

Project: 02541211 - Long Point Marsh Creation

Location: Hackberry, Louisiana



CPT: CPT-12

Total depth: 9.71 ft, Date: 6/29/2020

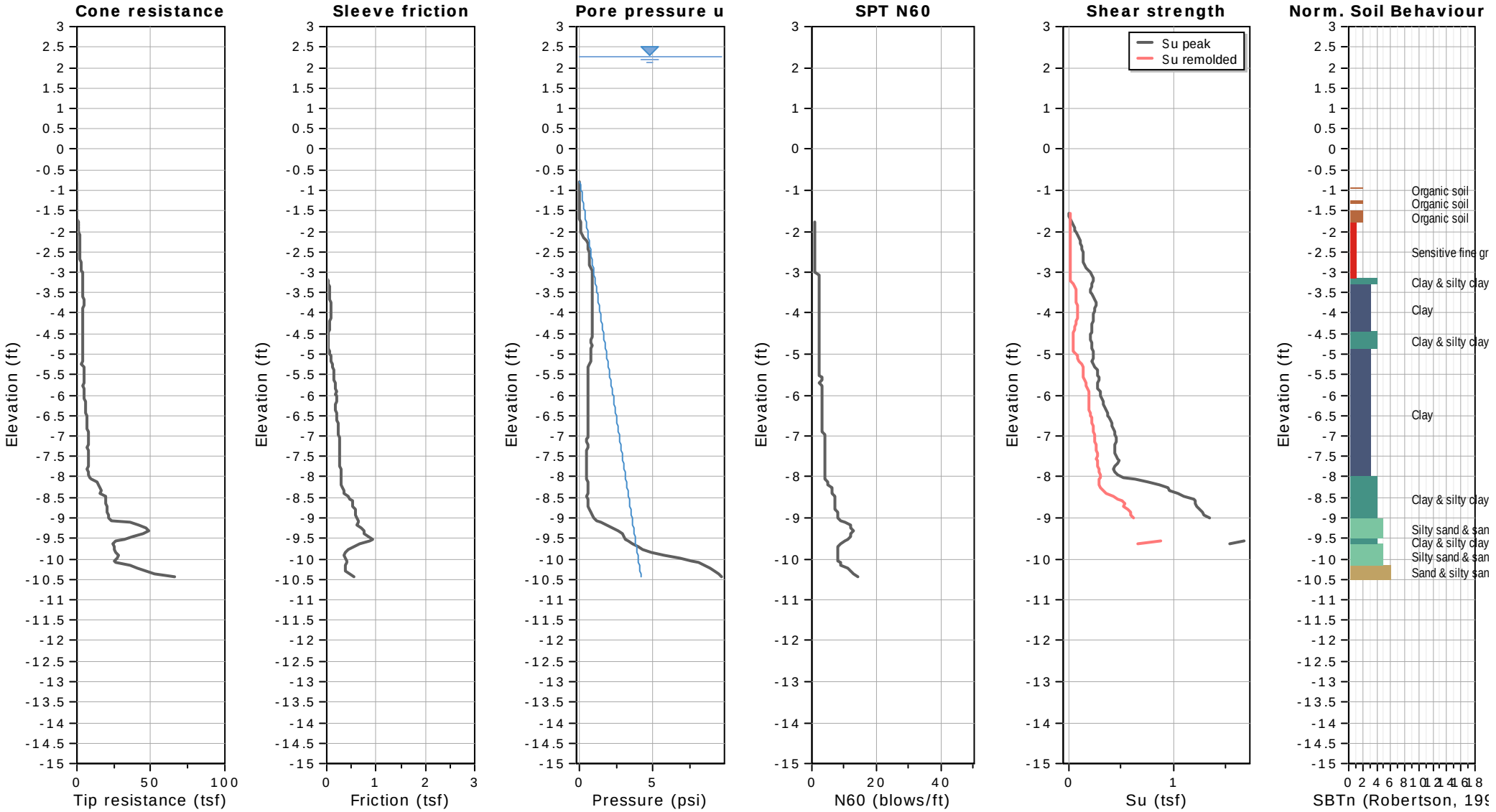
Mudline Elevation: -0.72 ft

Cone Type: 60° 1.4" Diam. Type 2 Electric Cone Penetrometer

Cone Operator: Charley Baker

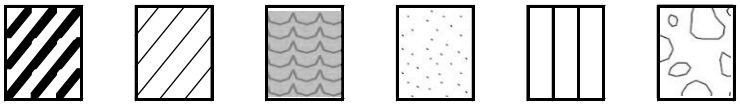
Project: 02541211 - Long Point Marsh Creation

Location: Hackberry, Louisiana



KEY TO TERMS AND SYMBOLS USED ON LOGS

SOIL TYPE

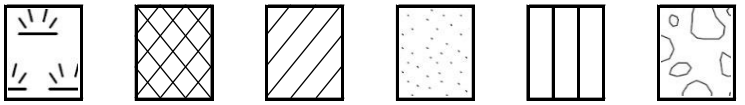


FAT CLAY | LEAN CLAY | ORGANIC CLAY | SAND | SILT | GRAVEL

SAMPLER TYPE

NO RECOVERY | AUGER SAMPLE | SHELBY TUBE | SPLIT SPOON

SOIL TYPE / MODIFIERS



TOPSOIL | FILL | CLAYEY | SANDY | SILTY | GRAVELY

GROUNDWATER DURING DRILLING

GROUNDWATER UPON COMPLETION

UNIFIED SOIL CLASSIFICATION SYSTEM - ASTM D 2487 (1980)

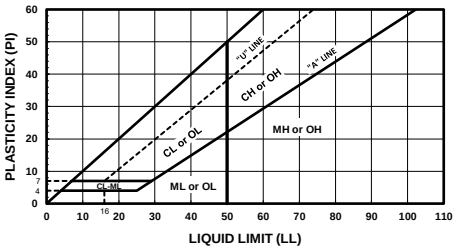
MAJOR DIVISIONS			LETTER SYMBOL	TYPICAL DESCRIPTIONS
COARSE-GRAINED SOILS LESS THAN 50% PASSING NO. 200 SIEVE	GRAVEL & GRAVELLY SOILS LESS THAN 50% PASSING NO. 4 SIEVE	CLEAN GRAVEL (LITTLE OR NO FINES)	GW	WELL-GRADED GRAVEL, GRAVEL-SAND MIXTURES WITH LITTLE OR NO FINES
			GP	POORLY GRADED GRAVEL, GRAVEL-SAND MIXTURES WITH LITTLE OR NO FINES
		WITH APPRECIABLE FINES	GM	SILTY GRAVEL, GRAVEL-SAND-SILT MIXTURES
			GC	CLAYEY GRAVELS, GRAVEL-SAND-CLAY MIXTURES
	SANDS MORE THAN 50% PASSING NO. 4 SIEVE	CLEAN SANDS (LITTLE OR NO FINES)	SW	WELL-GRADED SAND
			SP	POORLY-GRADED SANDS
		WITH APPRECIABLE FINES	SM	SILTY SANDS
			SC	CLAYEY SANDS
FINE-GRAINED SOILS MORE THAN 50% PASSING NO. 200 SIEVE	SILTS AND CLAYS LIQUID LIMIT < 50		ML	INORGANIC SILTS & VERY FINE SANDS, CLAYEY SILT W/ LOW PLASTICITY INDEX
			CL	INORGANIC LEAN CLAYS GRAVELLY, SANDY, OR SILTY LEAN CLAYS
			OL	ORGANIC SILTS & ORGANIC SILTY CLAYS W/LOW PLASTICITY INDEX
	SILTS AND CLAYS LIQUID LIMIT ≥ 50		MH	INORGANIC SILTS W/ HIGH PLASTICITY INDEX, ELASTIC SILTS
			CH	INORGANIC FAT CLAYS GRAVELLY, SANDY, OR SILTY FAT CLAYS
			OH	ORGANIC CLAYS OF MED TO HIGH PLASTICITY, ORGANIC SILTS
HIGHLY ORGANIC SOIL			PT	PEAT AND OTHER HIGHLY ORGANIC SOILS
UNCLASSIFIED FILL MATERIALS			ARTIFICIALLY DEPOSITED AND OTHER UNCLASSIFIED SOILS AND MAN-MADE SOIL MIXTURES	

CONSISTENCY - COHESIVE SOILS

CONSISTENCY	SHEAR STRENGTH IN TONS/FT^2
VERY SOFT	0 TO 0.125
SOFT	0.125 TO 0.25
FIRM	0.25 TO .50
STIFF	0.50 TO 1.00
VERY STIFF	1.00 TO 2.00
HARD	> 2.00 OR 2.00+

RELATIVE DENSITY - GRANULAR SOILS

DENSITY	N-VALUE (BLOWS/FT)
VERY LOOSE	0-4
LOOSE	4-9
MEDIUM DENSE	10-29
DENSE	30-49
VERY DENSE	> 50 OR 50+



ABBREVIATIONS

HP - HAND PENETROMETER

TV - MINIATURE TORVANE

UC - UNCONFINED COMPRESSION TEST

UU - UNCONSOLIDATED UNDRAINED TRAIXIAL

NOTE: BORING LOGS INDICATE SHEAR STRENGTH AS OBTAINED BY ABOVE TESTS

CLASSIFICATION OF GRANULAR SOILS

U.S. STANDARD SIEVE SIZE(S)

12"	3"	3/4"	4	10	40	200	
BOULDERS	COBBLES	GRAVEL		SAND			SILT OR CLAY / CLAY
		COARSE	FINE	COARSE	MEDIUM	FINE	
300	75	19	4.75	2.0	0.42	0.075	0.005

GRAIN SIZE IN MM

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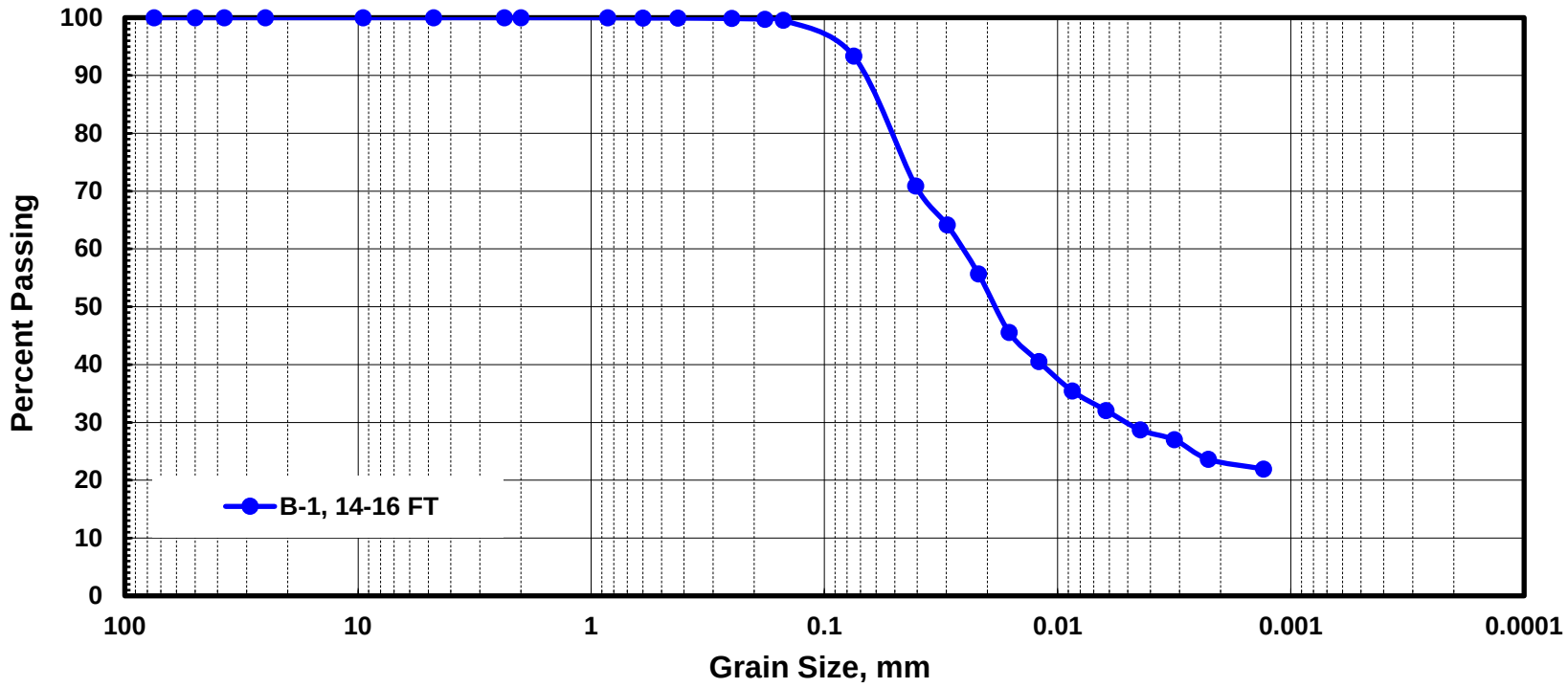
724 Central Avenue
Jefferson, Louisiana 70121
Phone: (504) 733-9411

APPENDIX C

HYDROMETER TEST RESULTS
SPECIFIC GRAVITY TEST RESULTS
ORGANIC CONTENT RESULTS

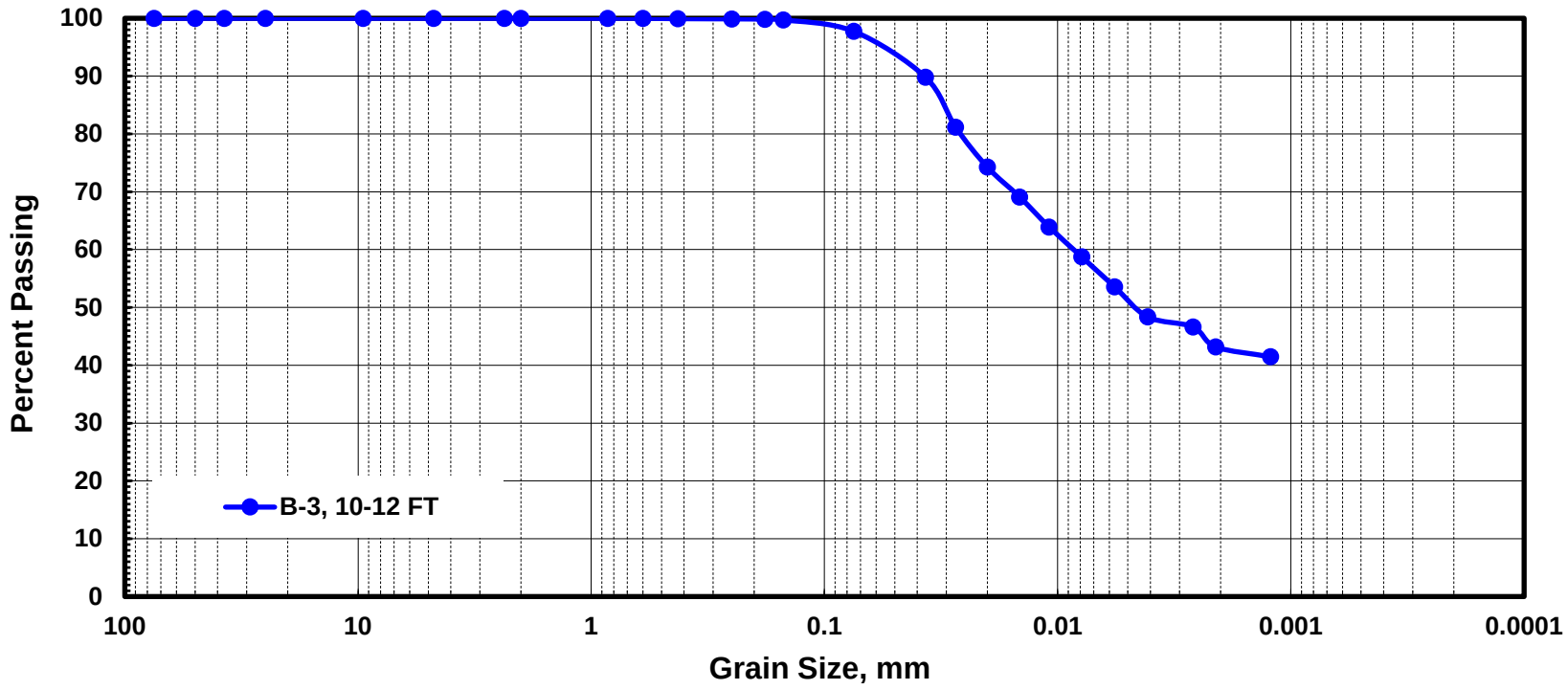


US STANDARD SIEVE SIZE

	6"	3"	3/4"	#4	#10	#40	#200		
BOULDERS	COBBLES	GRAVEL		SAND				SILT OR CLAY	CLAY
		COARSE	FINE	COARSE	MEDIUM	FINE			
	152	75	19	4.75	2.0	0.425	0.075		0.002

PARTICLE SIZE IN MM

GRADATION INFORMATION	D_{10} mm	D_{30} mm	D_{50} mm	D_{60} mm	C_u (D_{60}/D_{10})	C_c $D_{30}^2/(D_{60}*D_{10})$	%Gravel Ret. #4	%Sand <#4 & >#200	%Fines Pass #200	%Clay < 0.002 mm
B-1, 14-16 FT	NA	0.0050	0.0184	0.0256	NA	NA	0.0%	6.64	93.36	23.17
Lean Clay (CL), Gray										

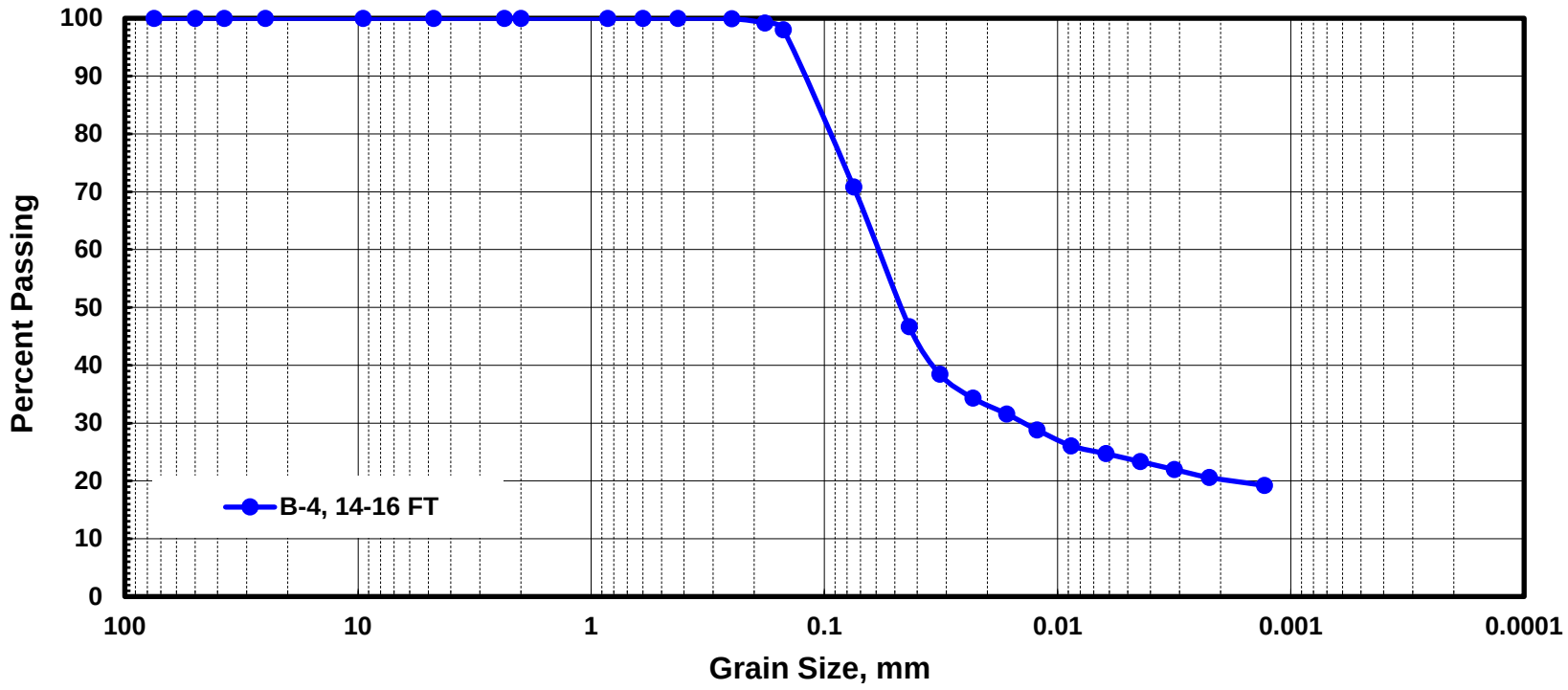


US STANDARD SIEVE SIZE

	6"	3"	3/4"	#4	#10	#40	#200	
BOULDERS	COBBLES	GRAVEL		SAND			SILT OR CLAY	CLAY
		COARSE	FINE	COARSE	MEDIUM	FINE		
	152	75	19	4.75	2.0	0.425	0.075	0.002

PARTICLE SIZE IN MM

GRADATION INFORMATION	D_{10} mm	D_{30} mm	D_{50} mm	D_{60} mm	C_u (D_{60}/D_{10})	C_c $D_{30}^2/(D_{60}*D_{10})$	%Gravel Ret. #4	%Sand <#4 & >#200	%Fines Pass #200	%Clay < 0.002 mm
B-3, 10-12 FT	NA	NA	0.0046	0.0085	NA	NA	0.0%	2.25	97.75	42.98
Lean Clay (CL), Gray										



US STANDARD SIEVE SIZE

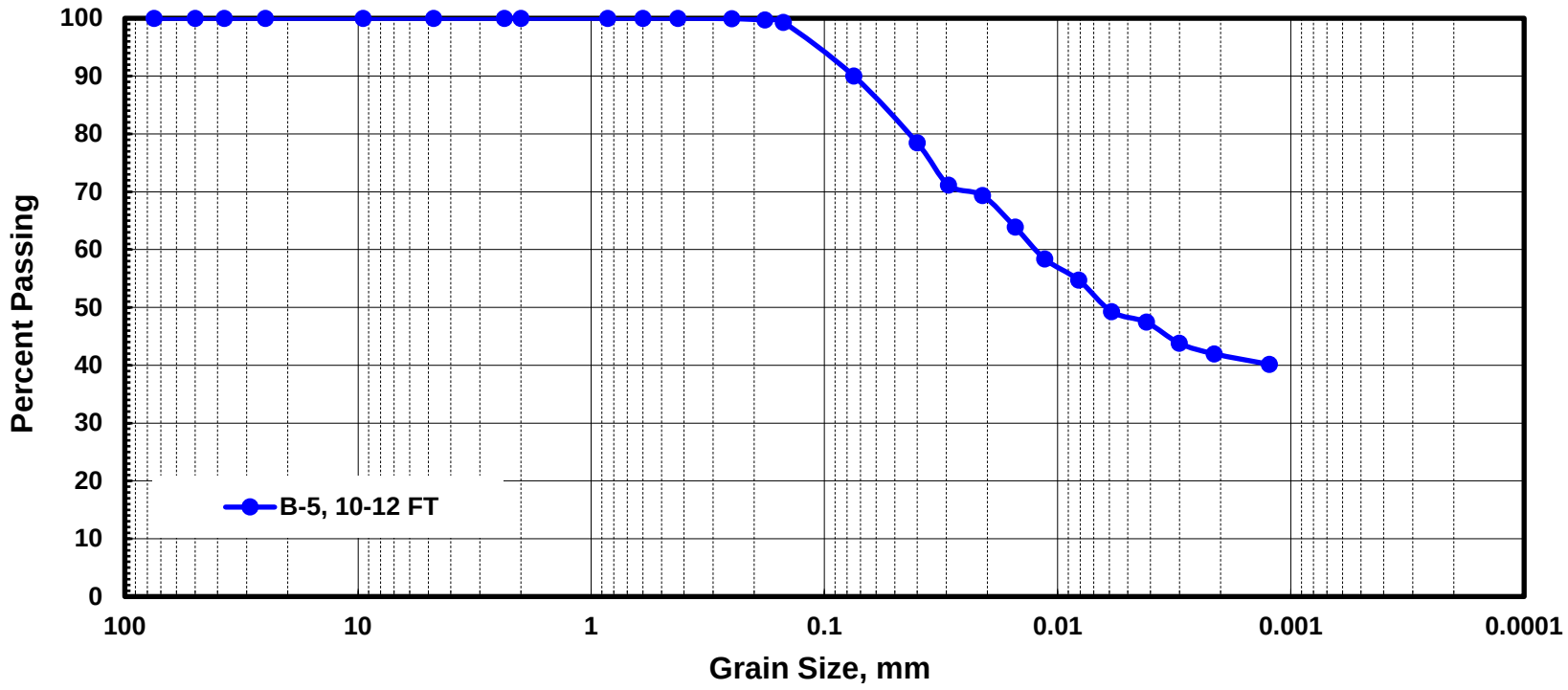
6"	3"	3/4"	#4	#10	#40	#200

BOULDERS	COBBLES	GRAVEL		SAND			SILT OR CLAY	CLAY
		COARSE	FINE	COARSE	MEDIUM	FINE		

152	75	19	4.75	2.0	0.425	0.075	0.002

PARTICLE SIZE IN MM

GRADATION INFORMATION	D_{10} mm	D_{30} mm	D_{50} mm	D_{60} mm	C_u (D_{60}/D_{10})	C_c $D_{30}^2/(D_{60}*D_{10})$	%Gravel Ret. #4	%Sand <#4 & >#200	%Fines Pass #200	%Clay < 0.002 mm
B-4, 14-16 FT	NA	0.0139	0.0467	0.0586	NA	NA	0.0%	29.17	70.83	20.24
Lean Clay with Sand (CL), Tan										



US STANDARD SIEVE SIZE

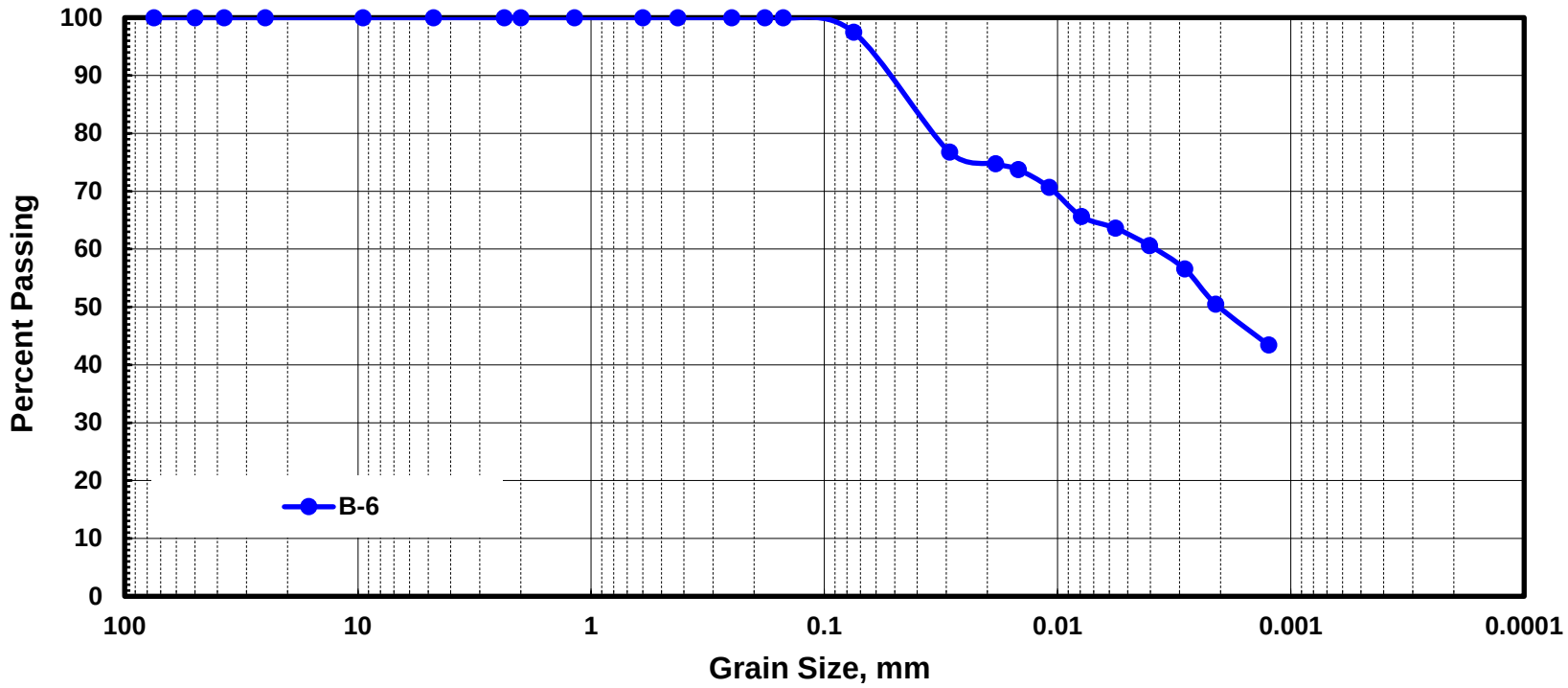
6"	3"	3/4"	#4	#10	#40	#200

BOULDERS	COBBLES	GRAVEL		SAND			SILT OR CLAY	CLAY
		COARSE	FINE	COARSE	MEDIUM	FINE		

152	75	19	4.75	2.0	0.425	0.075	0.002

PARTICLE SIZE IN MM

GRADATION INFORMATION	D_{10} mm	D_{30} mm	D_{50} mm	D_{60} mm	C_u (D_{60}/D_{10})	C_c $D_{30}^2/(D_{60}*D_{10})$	%Gravel Ret. #4	%Sand <#4 & >#200	%Fines Pass #200	%Clay < 0.002 mm
B-5, 10-12 FT	NA	NA	0.0061	0.0124	NA	NA	0.0%	9.96	90.04	41.71
Lean Clay (CL), Gray										

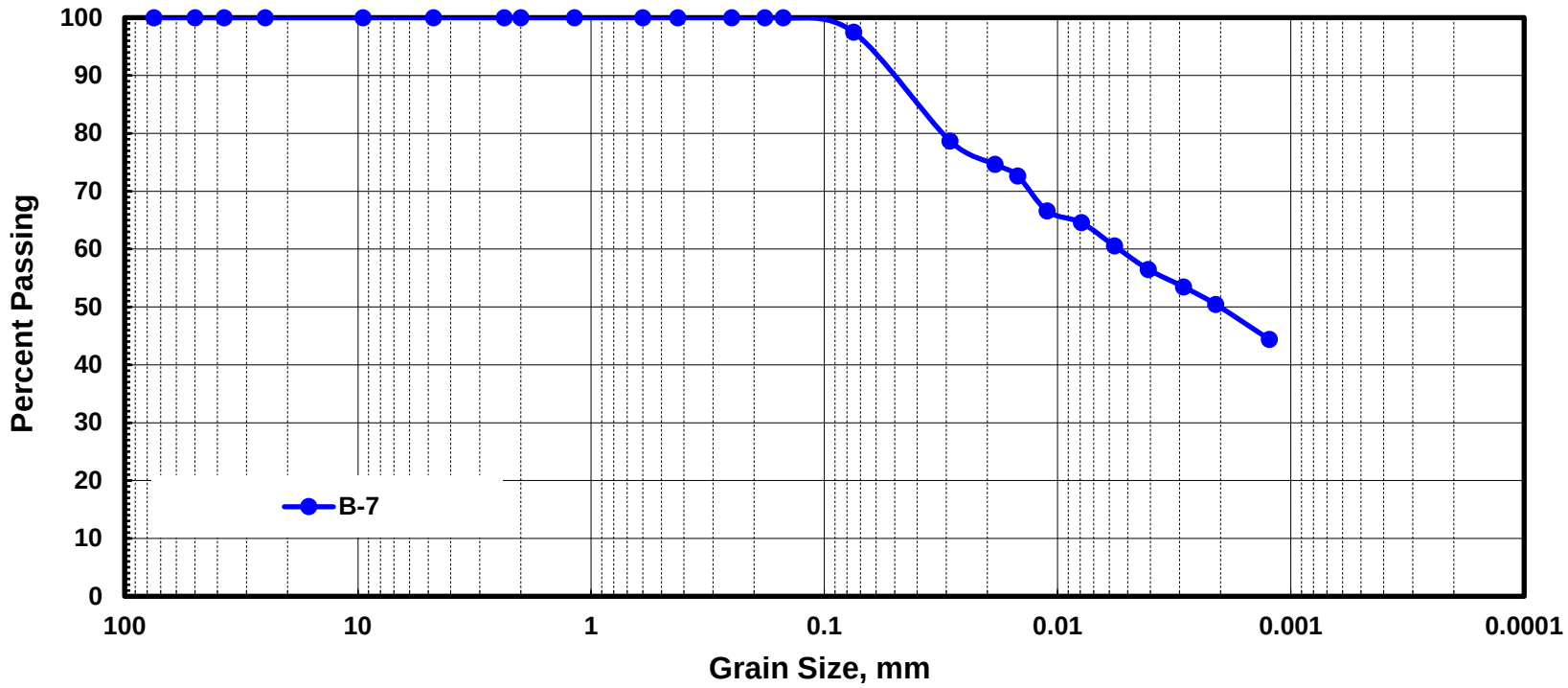


US STANDARD SIEVE SIZE

	6"	3"	3/4"	#4	#10	#40	#200		
BOULDERS	COBBLES	GRAVEL		SAND			SILT OR CLAY	CLAY	
		COARSE	FINE	COARSE	MEDIUM	FINE			
	152	75	19	4.75	2.0	0.425	0.075	0.002	

PARTICLE SIZE IN MM

GRADATION INFORMATION	D_{10} mm	D_{30} mm	D_{50} mm	D_{60} mm	C_u (D_{60}/D_{10})	C_c $D_{30}^2/(D_{60}*D_{10})$	%Gravel Ret. #4	%Sand <#4 & >#200	%Fines Pass #200	%Clay < 0.002 mm
B-6	NA	NA	0.0020	0.0038	NA	NA	0.0%	2.5	97.5	49.67



US STANDARD SIEVE SIZE

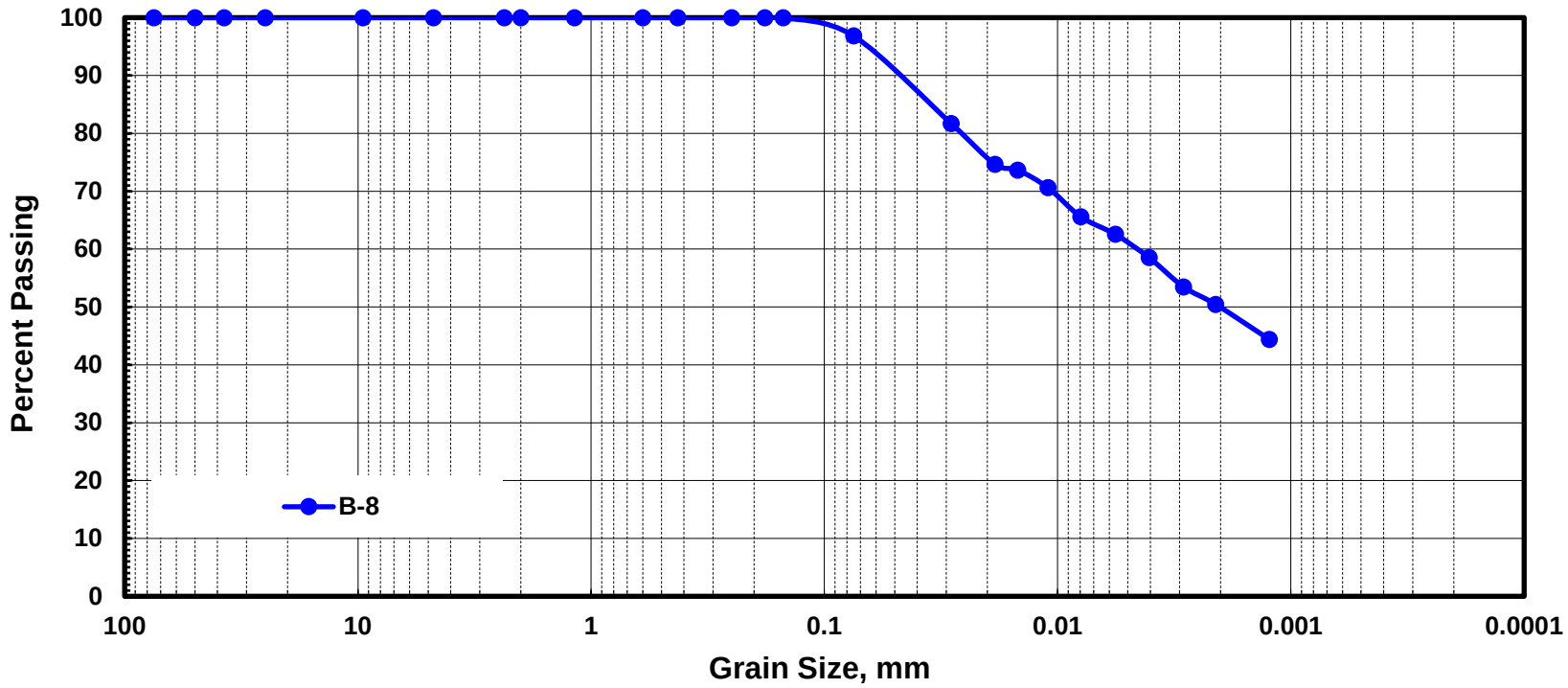
6"	3"	3/4"	#4	#10	#40	#200

BOULDERS	COBBLES	GRAVEL		SAND			SILT OR CLAY	CLAY
		COARSE	FINE	COARSE	MEDIUM	FINE		

152	75	19	4.75	2.0	0.425	0.075	0.002

PARTICLE SIZE IN MM

GRADATION INFORMATION	D_{10} mm	D_{30} mm	D_{50} mm	D_{60} mm	C_u (D_{60}/D_{10})	C_c $D_{30}^2/(D_{60}*D_{10})$	%Gravel Ret. #4	%Sand <#4 & >#200	%Fines Pass #200	%Clay < 0.002 mm
B-7	NA	NA	0.0020	0.0055	NA	NA	0.0%	2.5	97.5	49.74

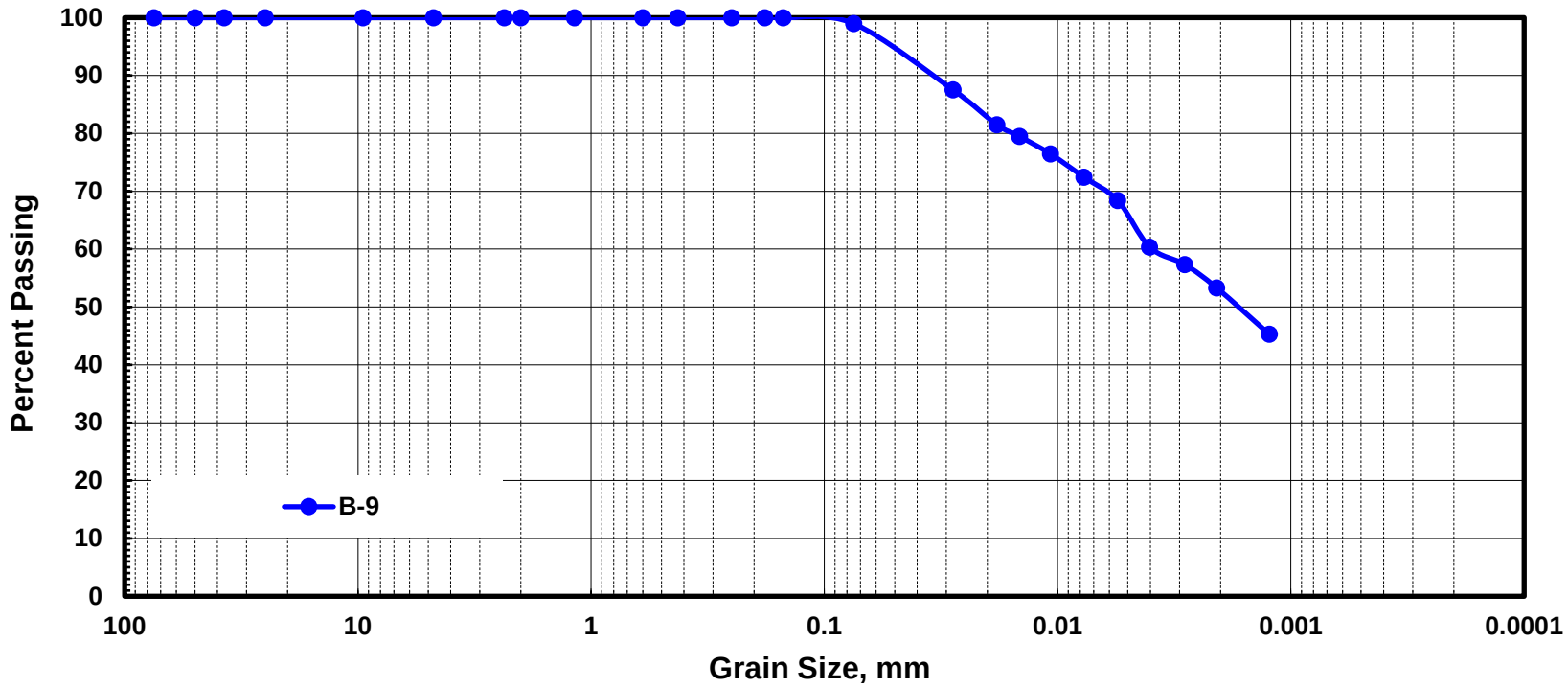


US STANDARD SIEVE SIZE

	6"	3"	3/4"	#4	#10	#40	#200		
BOULDERS	COBBLES	GRAVEL		SAND			SILT OR CLAY	CLAY	
		COARSE	FINE	COARSE	MEDIUM	FINE			
	152	75	19	4.75	2.0	0.425	0.075	0.002	

PARTICLE SIZE IN MM

GRADATION INFORMATION	D_{10} mm	D_{30} mm	D_{50} mm	D_{60} mm	C_u (D_{60}/D_{10})	C_c $D_{30}^2/(D_{60}*D_{10})$	%Gravel Ret. #4	%Sand <#4 & >#200	%Fines Pass #200	%Clay < 0.002 mm
B-8	NA	NA	0.0020	0.0046	NA	NA	0.0%	3.16	96.84	49.75

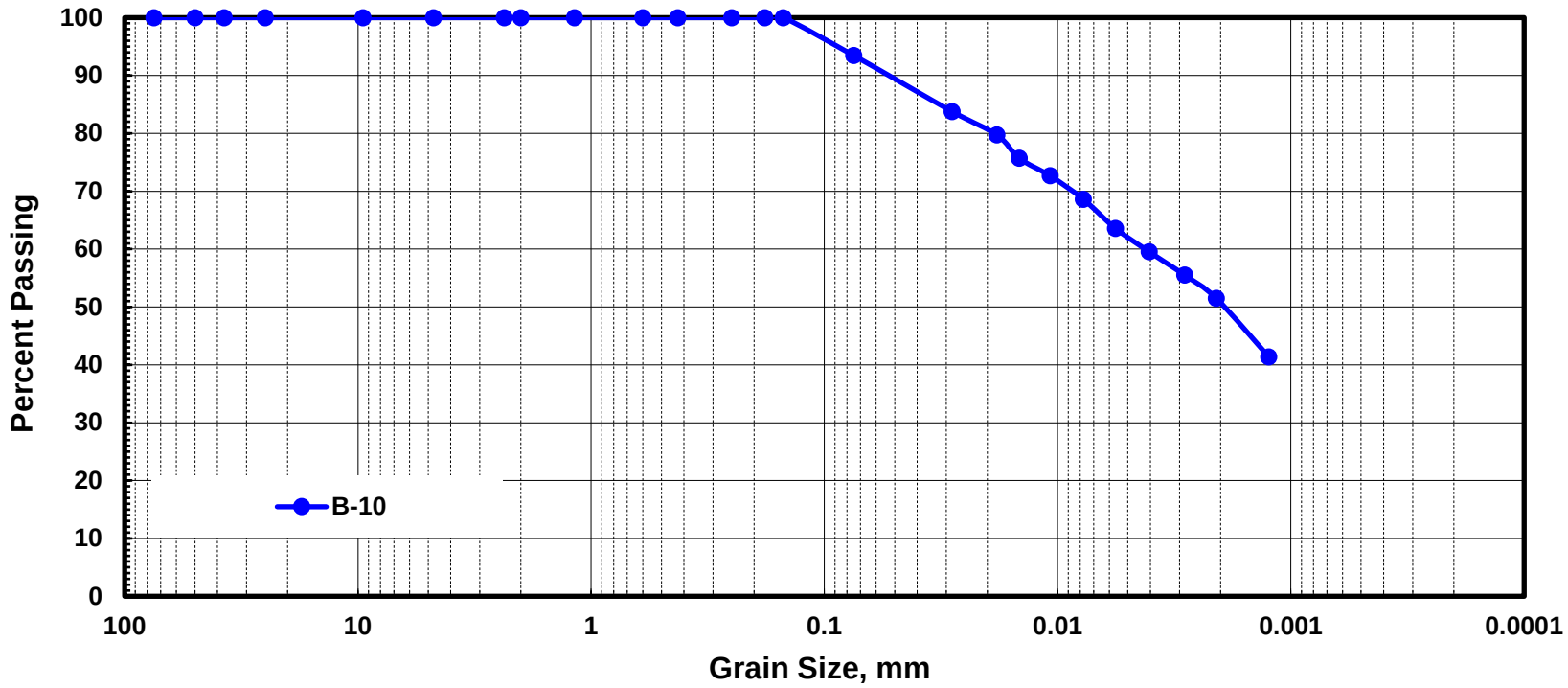


US STANDARD SIEVE SIZE

	6"	3"	3/4"	#4	#10	#40	#200		
BOULDERS	COBBLES	GRAVEL		SAND			SILT OR CLAY	CLAY	
		COARSE	FINE	COARSE	MEDIUM	FINE			
	152	75	19	4.75	2.0	0.425	0.075	0.002	

PARTICLE SIZE IN MM

GRADATION INFORMATION	D_{10} mm	D_{30} mm	D_{50} mm	D_{60} mm	C_u (D_{60}/D_{10})	C_c $D_{30}^2/(D_{60}*D_{10})$	%Gravel Ret. #4	%Sand <#4 & >#200	%Fines Pass #200	%Clay < 0.002 mm
B-9	NA	NA	0.0017	0.0039	NA	NA	0.0%	1.02	98.98	52.53

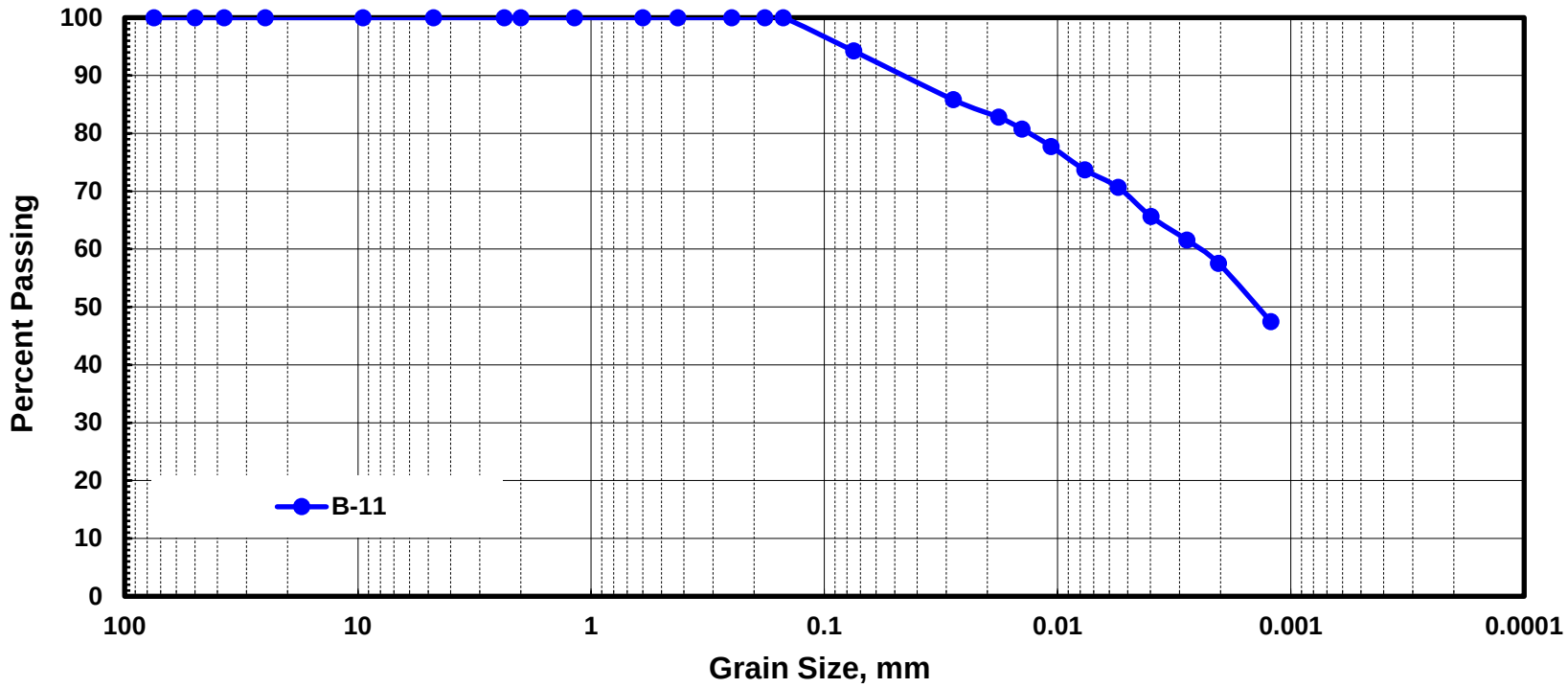


US STANDARD SIEVE SIZE

6"	3"	3/4"	#4	#10	#40	#200	
BOULDERS	COBBLES	GRAVEL		SAND			SILT OR CLAY / CLAY
		COARSE	FINE	COARSE	MEDIUM	FINE	
152	75	19		4.75	2.0	0.425	0.075 / 0.002

PARTICLE SIZE IN MM

GRADATION INFORMATION	D_{10} mm	D_{30} mm	D_{50} mm	D_{60} mm	C_u (D_{60}/D_{10})	C_c $D_{30}^2/(D_{60}*D_{10})$	%Gravel Ret. #4	%Sand <#4 & >#200	%Fines Pass #200	%Clay < 0.002 mm
B-10	NA	NA	0.0019	0.0042	NA	NA	0.0%	6.53	93.47	50.43

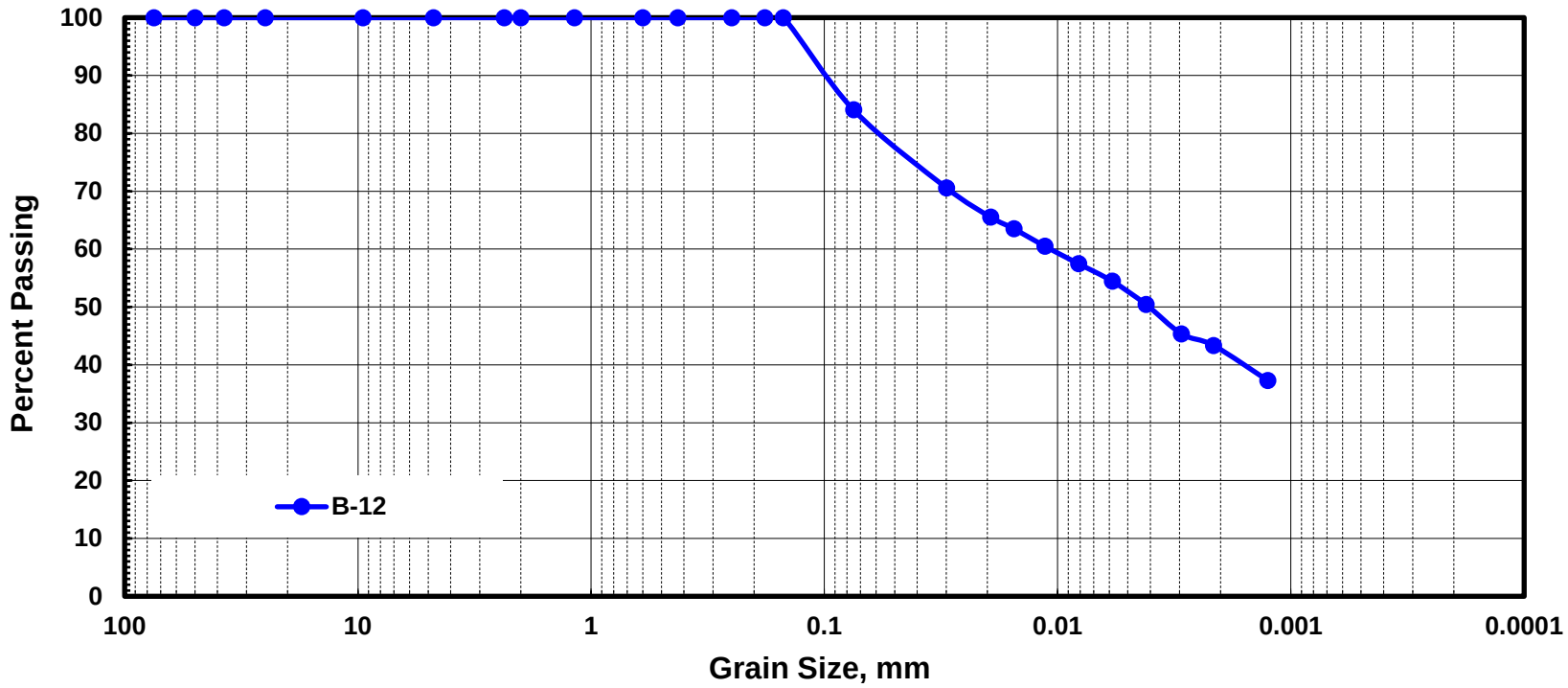


US STANDARD SIEVE SIZE

	6"	3"	3/4"	#4	#10	#40	#200		
BOULDERS	COBBLES	GRAVEL		SAND			SILT OR CLAY	CLAY	
		COARSE	FINE	COARSE	MEDIUM	FINE			
	152	75	19	4.75	2.0	0.425	0.075	0.002	

PARTICLE SIZE IN MM

GRADATION INFORMATION	D_{10} mm	D_{30} mm	D_{50} mm	D_{60} mm	C_u (D_{60}/D_{10})	C_c $D_{30}^2/(D_{60}*D_{10})$	%Gravel Ret. #4	%Sand <#4 & >#200	%Fines Pass #200	%Clay < 0.002 mm
B-11	NA	NA	0.0014	0.0025	NA	NA	0.0%	5.77	94.23	57.01



US STANDARD SIEVE SIZE

6"	3"	3/4"	#4	#10	#40	#200	
BOULDERS	COBBLES	GRAVEL		SAND			SILT OR CLAY / CLAY
		COARSE	FINE	COARSE	MEDIUM	FINE	
152	75	19	4.75	2.0	0.425	0.075	0.002

PARTICLE SIZE IN MM

GRADATION INFORMATION	D_{10} mm	D_{30} mm	D_{50} mm	D_{60} mm	C_u (D_{60}/D_{10})	C_c $D_{30}^2/(D_{60}*D_{10})$	%Gravel Ret. #4	%Sand <#4 & >#200	%Fines Pass #200	%Clay < 0.002 mm
B-12	NA	NA	0.0041	0.0107	NA	NA	0.0%	15.95	84.05	42.35

intertek psi	Specific Gravity ASTM (D 854)			
Project Name: Long Point Bayou Marsh Creation	Checked By:		Computed By: RR	
Project No: 254-1211	Date tested: 7/29/2020			
Prepared: AC Date: 7/20/20	Scales Control Number:		AE444189, AE44431, AE9V2283	
Tested by: EG Date: 7/28/20	Oven Control Number:		286-9908419, B33ER01048	
Boring Number :	B-1			
Sample Number:	5			
Depth, feet:	8-10			
Description of Material:	Lean Clay (CL), Gray			
Pyconmeter Calibration Information				
Flask ID.	5E			
Calibrated Mass of Flask (Mpc), gms:	218.110			
Calibrated Volume of the Flask (Vpc), mL:	500.000			
Check for Pyconmeter Calibration				
Mass of Flask, gms(Mp):	218.11	Is Mp within 0.06g of Mpc (Y/N):		N
Mass of Flask + Water, (Mpw,t), gms:	716.74			
Temperature of Water (Ct), deg. C:	23.5	(Temprature of Water After Cooling)		
Density of Water at Tt, (pw,ct), g/mL:	0.99742	(From Table 1 of ASTM D 854)		
Volume of the Flask (Vp), mL:	499.918	Vp = (Mpwct - Mp)/pw,ct		
Test Data				
Mass of Flask + Water at Test (Mpw, t), gms:	716.835	(Mpw = Mp + (Vp * pw,t)		
Mass of Dry Soil (Ms), gms:	52.52			
Mass of Flask + Water + Soil, (Mpws, t), gms:	749.19			
Temperature of Water (Tt), deg. C:	22.7	(Temprature of Water+Soil After Cooling)		
Density of Water at Tt, (pw,t), g/mL:	0.99761	(From Table 1 of ASTM D 854)		
Specific gravity of Water at T, (Gt):	2.605	Gt = Ms /{Mpw,t - (Mpwst - Ms)}		
Temperature Coefficient, K:	0.99941	(From Table 1 of ASTM D 854)		
Specific gravity of soil, Gs (20 deg. C):	*2.603*	Gs (20C) = Gt * K		
Remarks:				

intertek psi	Specific Gravity ASTM (D 854)			
Project Name: Long Point Bayou Marsh Creation	Checked By:		Computed By: RR	
Project No: 254-1211	Date tested: 7/29/2020			
Prepared: AC Date: 7/20/20	Scales Control Number:		AE444189, AE44431, AE9V2283	
Tested by: EG Date: 7/28/20	Oven Control Number:		286-9908419, B33ER01048	
Boring Number :	B-2			
Sample Number:	4			
Depth, feet:	6-8			
Description of Material:	Lean Clay (CL), Gray			
Pyconmeter Calibration Information				
Flask ID.	2A			
Calibrated Mass of Flask (Mpc), gms:	94.840			
Calibrated Volume of the Flask (Vpc), mL:	250.000			
Check for Pyconmeter Calibration				
Mass of Flask, gms(Mp):	94.85	Is Mp within 0.06g of Mpc (Y/N):		N
Mass of Flask + Water, (Mpw,t), gms:	343.96			
Temperature of Water (Ct), deg. C:	23.7	(Temprature of Water After Cooling)		
Density of Water at Tt, (pw,ct), g/mL:	0.99738	(From Table 1 of ASTM D 854)		
Volume of the Flask (Vp), mL:	249.765	Vp = (Mpwct - Mp)/pw,ct		
Test Data				
Mass of Flask + Water at Test (Mpw, t), gms:	343.984	(Mpw = Mp + (Vp * pw,t)		
Mass of Dry Soil (Ms), gms:	38.75			
Mass of Flask + Water + Soil, (Mpws, t), gms:	368.07			
Temperature of Water (Tt), deg. C:	23.3	(Temprature of Water+Soil After Cooling)		
Density of Water at Tt, (pw,t), g/mL:	0.99747	(From Table 1 of ASTM D 854)		
Specific gravity of Water at T, (Gt):	2.643	Gt = Ms /{Mpw,t - (Mpwst - Ms)}		
Temperature Coefficient, K:	0.99926	(From Table 1 of ASTM D 854)		
Specific gravity of soil, Gs (20 deg. C):	*2.641*	Gs (20C) = Gt * K		
Remarks:				

intertek psi	Specific Gravity ASTM (D 854)			
Project Name: Long Point Bayou Marsh Creation	Checked By:		Computed By: RR	
Project No: 254-1211	Date tested: 7/29/2020			
Prepared: AC Date: 7/20/20	Scales Control Number:		AE444189, AE44431, AE9V2283	
Tested by: EG Date: 7/28/20	Oven Control Number:		286-9908419, B33ER01048	
Boring Number :	B-3			
Sample Number:	2			
Depth, feet:	2-4			
Description of Material:	Fat Clay (CH), Gray			
Pyconmeter Calibration Information				
Flask ID.	4D			
Calibrated Mass of Flask (Mpc), gms:	165.800			
Calibrated Volume of the Flask (Vpc), mL:	500.000			
Check for Pyconmeter Calibration				
Mass of Flask, gms(Mp):	165.80	Is Mp within 0.06g of Mpc (Y/N):		N
Mass of Flask + Water, (Mpw,t), gms:	664.33			
Temperature of Water (Ct), deg. C:	23.5	(Temprature of Water After Cooling)		
Density of Water at Tt, (pw,ct), g/mL:	0.99742	(From Table 1 of ASTM D 854)		
Volume of the Flask (Vp), mL:	499.817	Vp = (Mpwct - Mp)/pw,ct		
Test Data				
Mass of Flask + Water at Test (Mpw, t), gms:	664.425	(Mpw = Mp + (Vp * pw,t)		
Mass of Dry Soil (Ms), gms:	51.32			
Mass of Flask + Water + Soil, (Mpws, t), gms:	696.22			
Temperature of Water (Tt), deg. C:	22.7	(Temprature of Water+Soil After Cooling)		
Density of Water at Tt, (pw,t), g/mL:	0.99761	(From Table 1 of ASTM D 854)		
Specific gravity of Water at T, (Gt):	2.628	Gt = Ms /{Mpw,t - (Mpwst - Ms)}		
Temperature Coefficient, K:	0.99941	(From Table 1 of ASTM D 854)		
Specific gravity of soil, Gs (20 deg. C):	*2.627*	Gs (20C) = Gt * K		
Remarks:				

intertek psi	Specific Gravity ASTM (D 854)			
Project Name: Long Point Bayou Marsh Creation	Checked By:		Computed By: RR	
Project No: 254-1211	Date tested: 7/29/2020			
Prepared: AC Date: 7/20/20	Scales Control Number:		AE444189, AE44431, AE9V2283	
Tested by: EG Date: 7/28/20	Oven Control Number:		286-9908419, B33ER01048	
Boring Number :	B-4			
Sample Number:	5			
Depth, feet:	8-10			
Description of Material:	Fat Clay with Sand (CH), Gray			
Pyconmeter Calibration Information				
Flask ID.	3C			
Calibrated Mass of Flask (Mpc), gms:	156.000			
Calibrated Volume of the Flask (Vpc), mL:	500.000			
Check for Pyconmeter Calibration				
Mass of Flask, gms(Mp):	156.00	Is Mp within 0.06g of Mpc (Y/N):		N
Mass of Flask + Water, (Mpw,t), gms:	654.41			
Temperature of Water (Ct), deg. C:	22.8	(Temprature of Water After Cooling)		
Density of Water at Tt, (pw,ct), g/mL:	0.99759	(From Table 1 of ASTM D 854)		
Volume of the Flask (Vp), mL:	499.614	Vp = (Mpwct - Mp)/pw,ct		
Test Data				
Mass of Flask + Water at Test (Mpw, t), gms:	654.279	(Mpw = Mp + (Vp * pw,t)		
Mass of Dry Soil (Ms), gms:	52.68			
Mass of Flask + Water + Soil, (Mpws, t), gms:	687.76			
Temperature of Water (Tt), deg. C:	23.9	(Temprature of Water+Soil After Cooling)		
Density of Water at Tt, (pw,t), g/mL:	0.99733	(From Table 1 of ASTM D 854)		
Specific gravity of Water at T, (Gt):	2.744	Gt = Ms /{Mpw,t - (Mpwst - Ms)}		
Temperature Coefficient, K:	0.99912	(From Table 1 of ASTM D 854)		
Specific gravity of soil, Gs (20 deg. C):	*2.742*	Gs (20C) = Gt * K		
Remarks:				

intertek psi	Specific Gravity ASTM (D 854)			
Project Name: Long Point Bayou Marsh Creation	Checked By:		Computed By: RR	
Project No: 254-1211	Date tested: 7/29/2020			
Prepared: AC Date: 7/20/20	Scales Control Number:		AE444189, AE44431, AE9V2283	
Tested by: EG Date: 7/28/20	Oven Control Number:		286-9908419, B33ER01048	
Boring Number :	B-5			
Sample Number:	2			
Depth, feet:	2-4			
Description of Material:	Fat Clay (CH), Gray			
Pyconmeter Calibration Information				
Flask ID.	6F			
Calibrated Mass of Flask (Mpc), gms:	170.450			
Calibrated Volume of the Flask (Vpc), mL:	500.000			
Check for Pyconmeter Calibration				
Mass of Flask, gms(Mp):	170.45	Is Mp within 0.06g of Mpc (Y/N):		N
Mass of Flask + Water, (Mpw,t), gms:	668.97			
Temperature of Water (Ct), deg. C:	22.3	(Temprature of Water After Cooling)		
Density of Water at Tt, (pw,ct), g/mL:	0.99771	(From Table 1 of ASTM D 854)		
Volume of the Flask (Vp), mL:	499.666	Vp = (Mpwct - Mp)/pw,ct		
Test Data				
Mass of Flask + Water at Test (Mpw, t), gms:	668.592	(Mpw = Mp + (Vp * pw,t)		
Mass of Dry Soil (Ms), gms:	50.66			
Mass of Flask + Water + Soil, (Mpws, t), gms:	700.46			
Temperature of Water (Tt), deg. C:	25.4	(Temprature of Water+Soil After Cooling)		
Density of Water at Tt, (pw,t), g/mL:	0.99695	(From Table 1 of ASTM D 854)		
Specific gravity of Water at T, (Gt):	2.696	Gt = Ms /{Mpw,t - (Mpwst - Ms)}		
Temperature Coefficient, K:	0.99874	(From Table 1 of ASTM D 854)		
Specific gravity of soil, Gs (20 deg. C):	*2.692*	Gs (20C) = Gt * K		
Remarks:				

ORGANIC CONTENT

Boring No.	Depth (feet)	Organic Content (%)
B-1	2-4	2.4
B-2	6-8	0.6
B-3	0-2	3.3
B-4	2-4	1.1
B-5	0-2	11.5
B-6	0-5	2.9
B-7	0-5	3.4
B-8	0-5	3.3
B-9	0-5	1.9
B-10	0-5	3.6
B-11	0-5	2.3
B-12	0-5	1.7

APPENDIX D

UNCONSOLIDATED UNDRAINED TRIAXIAL COMPRESSION TEST RESULTS

UNCONSOLIDATED UNDRAINED TRIAXIAL TEST
ASTM D 2850

Project Name:	Long Point Bayou Marsh Creation Proj.	**Date Tested:**	7/14/2020
Project No.:	02541211	**Scale:**	03ES254
Boring No.:	B-1	**Calipers:**	01CAL254
Samp. and Spec. No.:	S-2	**Oven:**	10OV251
Sample Depth:	2-4'	**GeoJac Station No.:**	02GJ254
Qp / Torvane (tsf):	TV = 0.075	**Loadcell:**	16COM254
Sample Description:	DK GR CH W/ ORGANICS	**Air Pressure (psi):**	1.2

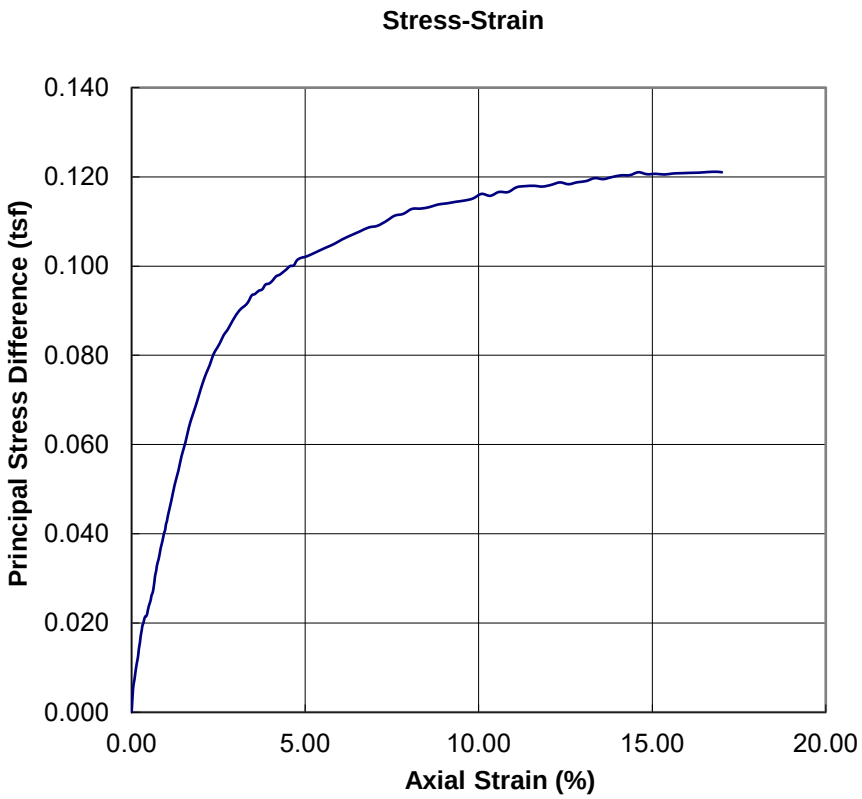
Sample Data:	1	2	3	Average	Height / Diameter Ratio (2 to 2.5)
Diameter (in)	2.757	2.626	2.696	2.693	2.15
Height (in)	5.778	5.782	5.771	5.777	
	Area, ft²:	0.040	Volume, ft³:	0.019	

	Moisture Content (%)		**Unit Weight**
Can Number:	246-16	Wet Weight of Sample (g):	785.01
Wt. of Can (g):	30.06	Dry Weight of Sample (g):	426.14
Wt. of Wet Soil + Can (g):	80.35	Wet Unit Weight (pcf):	**90.9**
Wt. of Dry Soil + Can (g):	57.36	Dry Unit Weight (pcf):	**49.3**
Wt. of Dry Soil (g):	27.30		
Wt. of Water (g):	22.99		
Moisture Content (%):	**84.2**		

	Max Strain (≤ 15%)	Compressive Strength, tsf	Shear Strength, tsf
RESULTS:	**14.851**	**0.12**	**0.06**

FAILURE TYPE:

NOTE: _____



Tested By: RB

Computed By: RB

Reviewed By: _____

intertek psi

Jefferson, Louisiana

UNCONSOLIDATED UNDRAINED TRIAXIAL TEST
ASTM D 2850

Project Name:	Long Point Bayou Marsh Creation Proj.	**Date Tested:**	7/14/2020
Project No.:	02541211	**Scale:**	03ES254
Boring No.:	B-1	**Calipers:**	01CAL254
Samp. and Spec. No.:	S-4	**Oven:**	10OV251
Sample Depth:	6-8'	**GeoJac Station No.:**	02GJ254
Qp / Torvane (tsf):	TV = 0.20	**Loadcell:**	17COM254
Sample Description:	GR CH W/ SI	**Air Pressure (psi):**	2.8

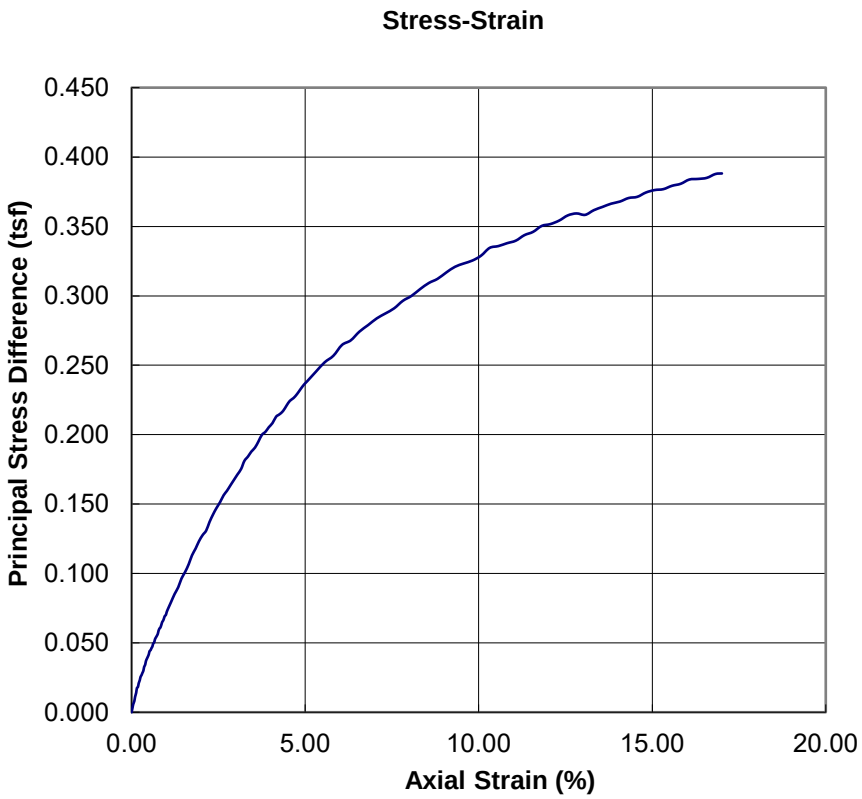
Sample Data:	1	2	3	Average	Height / Diameter Ratio (2 to 2.5)
Diameter (in)	2.881	2.820	2.823	2.841	1.99
Height (in)	5.667	5.659	5.663	5.663	
	Area, ft²:	0.044	Volume, ft³:	0.021	

Moisture Content (%)		**Unit Weight**	
Can Number:	L-33	Wet Weight of Sample (g):	1160.08
Wt. of Can (g):	31.33	Dry Weight of Sample (g):	919.31
Wt. of Wet Soil + Can (g):	83.80	Wet Unit Weight (pcf):	**123.1**
Wt. of Dry Soil + Can (g):	72.91	Dry Unit Weight (pcf):	**97.5**
Wt. of Dry Soil (g):	41.58		
Wt. of Water (g):	10.89		
Moisture Content (%):	**26.2**		

	Max Strain (≤ 15%)	Compressive Strength, tsf	Shear Strength, tsf
RESULTS:	**15.068**	**0.38**	**0.19**

FAILURE TYPE:

NOTE: _____



Tested By: RB
Computed By: RB
Reviewed By: _____

intertek psi

Jefferson, Louisiana

UNCONSOLIDATED UNDRAINED TRIAXIAL TEST
ASTM D 2850

Project Name:	Long Point Bayou Marsh Creation Proj.	**Date Tested:**	7/27/2020
Project No.:	02541211	**Scale:**	03ES254
Boring No.:	B-1	**Calipers:**	01CAL254
Samp. and Spec. No.:	S-7	**Oven:**	10OV251
Sample Depth:	12-14'	**GeoJac Station No.:**	02GJ254
Qp / Torvane (tsf):	TV = 0.375	**Loadcell:**	12COM254
Sample Description:	GR CH W/ SI	**Air Pressure (psi):**	5.2

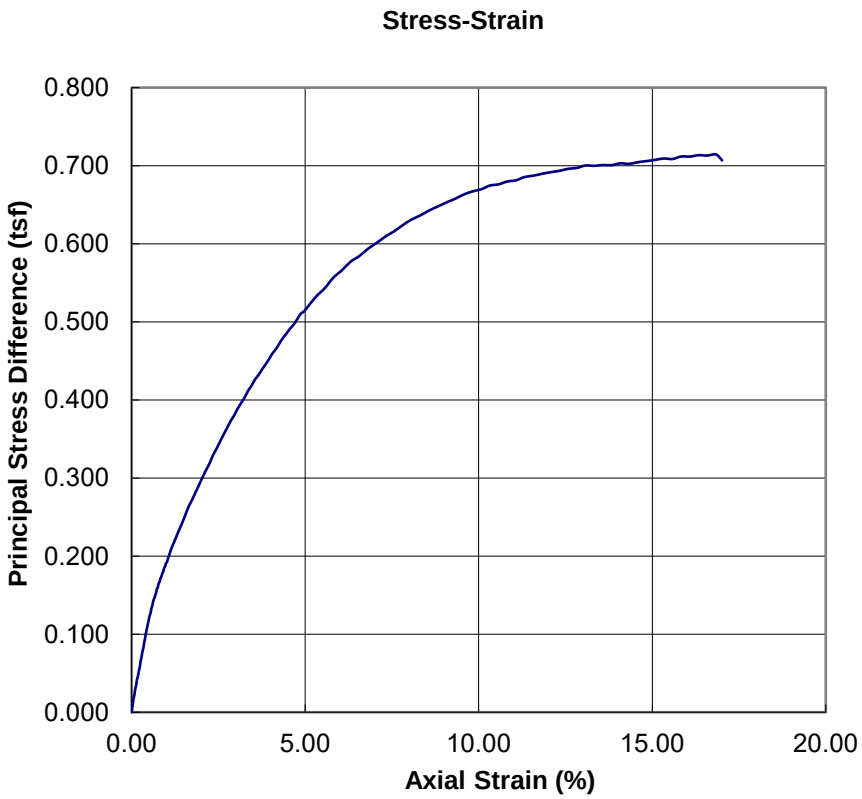
Sample Data:	1	2	3	Average	Height / Diameter Ratio (2 to 2.5)
Diameter (in)	2.795	2.806	2.836	2.812	2.05
Height (in)	5.757	5.765	5.766	5.763	
	Area, ft²:	0.043	Volume, ft³:	0.021	

Moisture Content (%)		**Unit Weight**	
Can Number:	DB-10	Wet Weight of Sample (g):	1169.76
Wt. of Can (g):	31.53	Dry Weight of Sample (g):	903.76
Wt. of Wet Soil + Can (g):	83.07	Wet Unit Weight (pcf):	**124.5**
Wt. of Dry Soil + Can (g):	71.35	Dry Unit Weight (pcf):	**96.2**
Wt. of Dry Soil (g):	39.82		
Wt. of Water (g):	11.72		
Moisture Content (%):	**29.4**		

	Max Strain (≤ 15%)	Compressive Strength, tsf	Shear Strength, tsf
RESULTS:	**15.082**	**0.71**	**0.35**

FAILURE TYPE:

NOTE: _____



Tested By: RB
Computed By: RB
Reviewed By: _____

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Jefferson, Louisiana

UNCONSOLIDATED UNDRAINED TRIAXIAL TEST
ASTM D 2850

Project Name:	Long Point Bayou Marsh Creation Proj.	**Date Tested:**	7/14/2020
Project No.:	02541211	**Scale:**	03ES254
Boring No.:	B-2	**Calipers:**	01CAL254
Samp. and Spec. No.:	S-1	**Oven:**	10OV251
Sample Depth:	0-2'	**GeoJac Station No.:**	02GJ254
Qp / Torvane (tsf):	TV = 0.20	**Loadcell:**	17COM254
Sample Description:	GR CH W/ SI & ORGANICS	**Air Pressure (psi):**	0.4

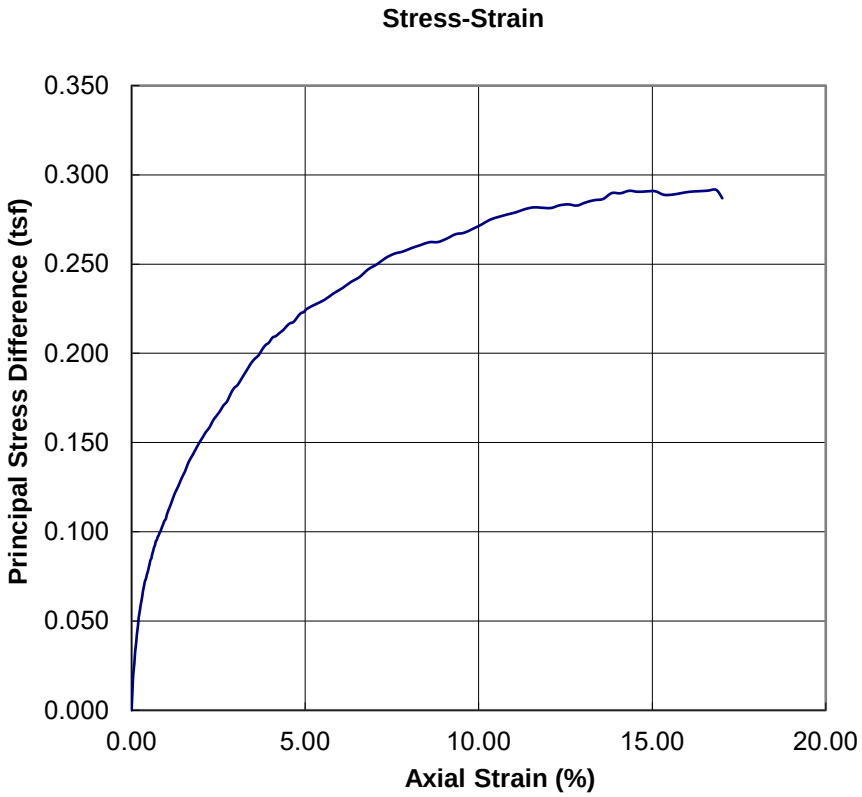
Sample Data:	1	2	3	Average	Height / Diameter Ratio (2 to 2.5)
Diameter (in)	2.829	2.824	2.750	2.801	2.04
Height (in)	5.720	5.720	5.724	5.721	
	Area, ft²:	0.043	Volume, ft³:	0.020	

	Moisture Content (%)		**Unit Weight**
Can Number:	53H	Wet Weight of Sample (g):	1031.51
Wt. of Can (g):	31.12	Dry Weight of Sample (g):	684.70
Wt. of Wet Soil + Can (g):	82.04	Wet Unit Weight (pcf):	**111.5**
Wt. of Dry Soil + Can (g):	64.92	Dry Unit Weight (pcf):	**74.0**
Wt. of Dry Soil (g):	33.80		
Wt. of Water (g):	17.12		
Moisture Content (%):	**50.7**		

	Max Strain (≤ 15%)	Compressive Strength, tsf	Shear Strength, tsf
RESULTS:	**15.085**	**0.29**	**0.15**

FAILURE TYPE:

NOTE: _____



Tested By: RB

Computed By: RB

Reviewed By: _____

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Jefferson, Louisiana

UNCONSOLIDATED UNDRAINED TRIAXIAL TEST
ASTM D 2850

Project Name:	Long Point Bayou Marsh Creation Proj.	**Date Tested:**	7/14/2020
Project No.:	02541211	**Scale:**	03ES254
Boring No.:	B-2	**Calipers:**	01CAL254
Samp. and Spec. No.:	S-4	**Oven:**	10OV251
Sample Depth:	6-8'	**GeoJac Station No.:**	02GJ254
Qp / Torvane (tsf):	TV = 0.55	**Loadcell:**	12COM254
Sample Description:	GR CH W/ SI & SA	**Air Pressure (psi):**	2.8

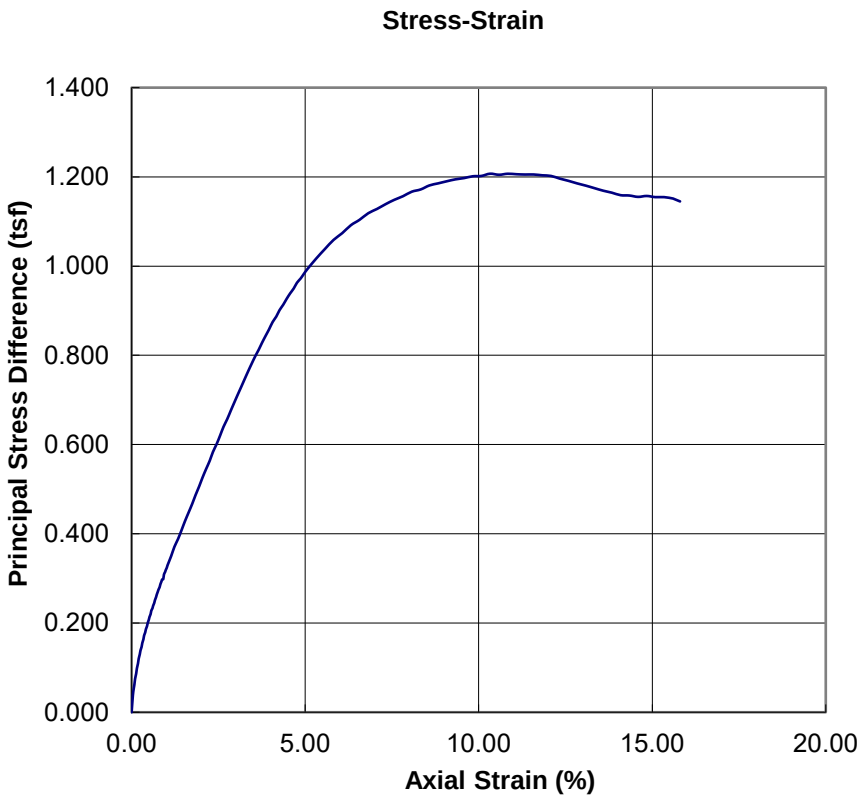
Sample Data:	1	2	3	Average	Height / Diameter Ratio (2 to 2.5)
Diameter (in)	2.836	2.854	2.847	2.846	2.01
Height (in)	5.708	5.719	5.712	5.713	
	Area, ft²:	0.044	Volume, ft³:	0.021	

	Moisture Content (%)		Unit Weight
Can Number:	DB-14	Wet Weight of Sample (g):	1196.56
Wt. of Can (g):	31.38	Dry Weight of Sample (g):	977.57
Wt. of Wet Soil + Can (g):	82.96	Wet Unit Weight (pcf):	125.5
Wt. of Dry Soil + Can (g):	73.52	Dry Unit Weight (pcf):	102.5
Wt. of Dry Soil (g):	42.14		
Wt. of Water (g):	9.44		
Moisture Content (%):	22.4		

	Max Strain (≤ 15%)	Compressive Strength, tsf	Shear Strength, tsf
RESULTS:	10.326	1.21	0.60

FAILURE TYPE:

NOTE: _____



Tested By: RB

Computed By: RB

Reviewed By: _____

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UNCONSOLIDATED UNDRAINED TRIAXIAL TEST
ASTM D 2850

Project Name:	Long Point Bayou Marsh Creation Proj.	**Date Tested:**	7/14/2020
Project No.:	02541211	**Scale:**	03ES254
Boring No.:	B-2	**Calipers:**	01CAL254
Samp. and Spec. No.:	S-6	**Oven:**	10OV251
Sample Depth:	10-12'	**GeoJac Station No.:**	02GJ254
Qp / Torvane (tsf):	TV = 0.15	**Loadcell:**	16COM254
Sample Description:	GR CH W/ SI & SA	**Air Pressure (psi):**	4.4

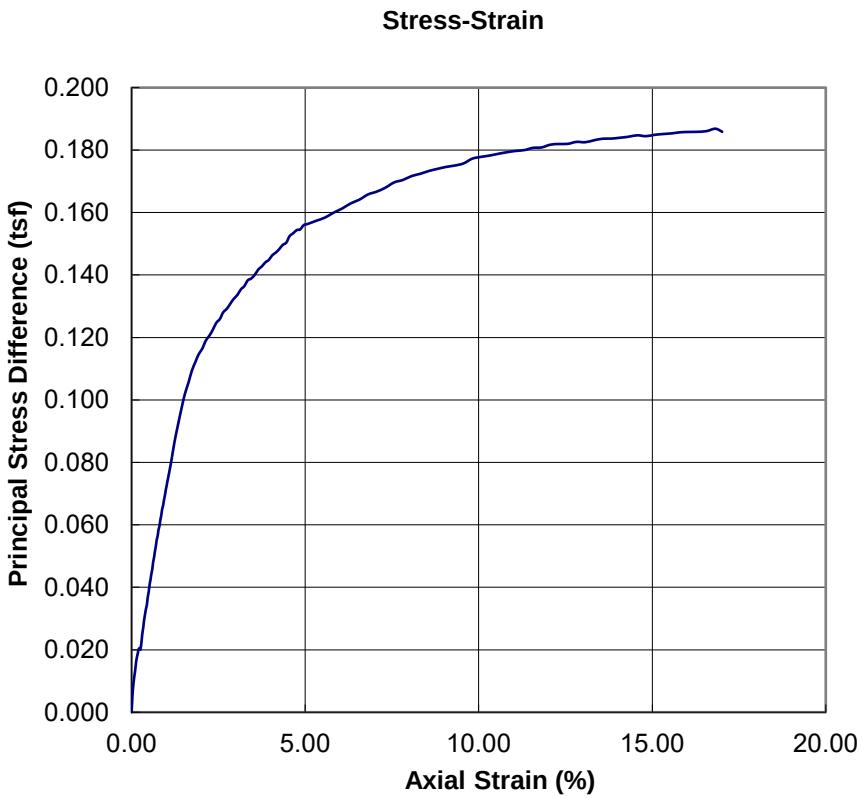
Sample Data:	1	2	3	Average	Height / Diameter Ratio (2 to 2.5)
Diameter (in)	2.853	2.799	2.864	2.839	2.01
Height (in)	5.695	5.701	5.687	5.694	
	Area, ft²:	0.044	Volume, ft³:	0.021	

Moisture Content (%)		**Unit Weight**	
Can Number:	DB-19	Wet Weight of Sample (g):	1090.79
Wt. of Can (g):	31.50	Dry Weight of Sample (g):	790.80
Wt. of Wet Soil + Can (g):	84.95	Wet Unit Weight (pcf):	**115.3**
Wt. of Dry Soil + Can (g):	70.25	Dry Unit Weight (pcf):	**83.6**
Wt. of Dry Soil (g):	38.75		
Wt. of Water (g):	14.70		
Moisture Content (%):	**37.9**		

	Max Strain (≤ 15%)	Compressive Strength, tsf	Shear Strength, tsf
RESULTS:	**15.068**	**0.18**	**0.09**

FAILURE TYPE:

NOTE: _____



Tested By: RB

Computed By: RB

Reviewed By: _____

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UNCONSOLIDATED UNDRAINED TRIAXIAL TEST
ASTM D 2850

Project Name:	Long Point Bayou Marsh Creation Proj.	**Date Tested:**	7/14/2020
Project No.:	02541211	**Scale:**	03ES254
Boring No.:	B-3	**Calipers:**	01CAL254
Samp. and Spec. No.:	S-2	**Oven:**	10OV251
Sample Depth:	2-4'	**GeoJac Station No.:**	02GJ254
Qp / Torvane (tsf):	0.5 / 3 TV = 0.40	**Loadcell:**	17COM254
Sample Description:	GR/OR CH W/ SA & SI	**Air Pressure (psi):**	1.2

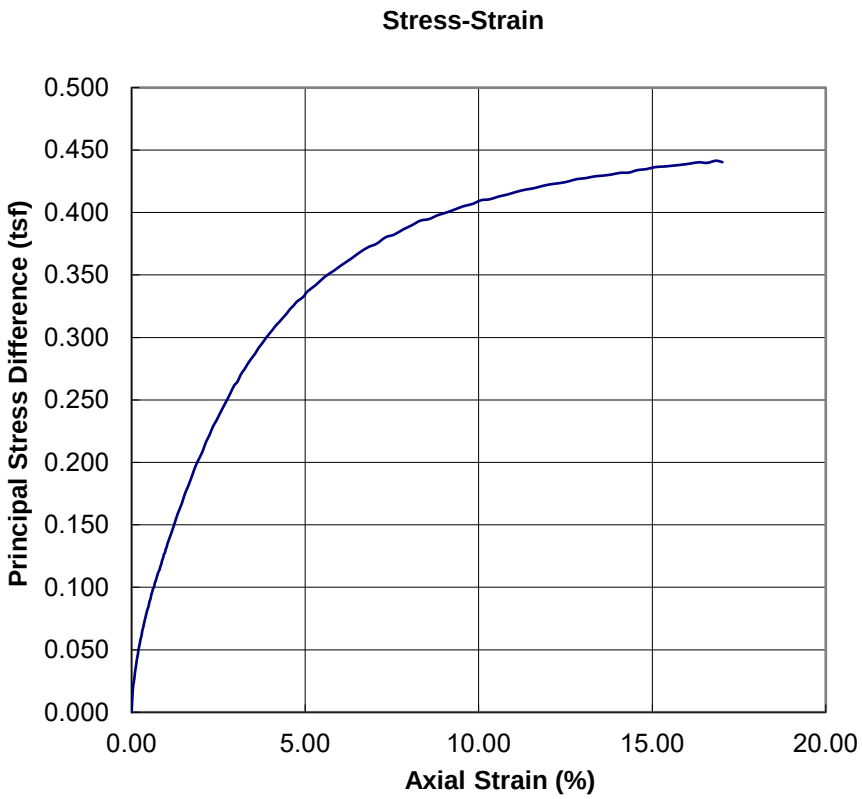
Sample Data:	1	2	3	Average	Height / Diameter Ratio (2 to 2.5)
Diameter (in)	2.813	2.835	2.844	2.831	2.04
Height (in)	5.760	5.762	5.760	5.761	
	Area, ft²:	0.044	Volume, ft³:	0.021	

Moisture Content (%)		**Unit Weight**	
Can Number:	5H	Wet Weight of Sample (g):	1162.65
Wt. of Can (g):	30.40	Dry Weight of Sample (g):	894.23
Wt. of Wet Soil + Can (g):	83.72	Wet Unit Weight (pcf):	**122.2**
Wt. of Dry Soil + Can (g):	71.41	Dry Unit Weight (pcf):	**94.0**
Wt. of Dry Soil (g):	41.01		
Wt. of Water (g):	12.31		
Moisture Content (%):	**30.0**		

	Max Strain (≤ 15%)	Compressive Strength, tsf	Shear Strength, tsf
RESULTS:	**15.081**	**0.44**	**0.22**

FAILURE TYPE:

NOTE: _____



Tested By: RB
Computed By: RB
Reviewed By: _____

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UNCONSOLIDATED UNDRAINED TRIAXIAL TEST
ASTM D 2850

Project Name:	Long Point Bayou Marsh Creation Proj.	**Date Tested:**	7/14/2020
Project No.:	02541211	**Scale:**	03ES254
Boring No.:	B-3	**Calipers:**	01CAL254
Samp. and Spec. No.:	S-5	**Oven:**	10OV251
Sample Depth:	8-10'	**GeoJac Station No.:**	02GJ254
Qp / Torvane (tsf):	3.5 / 3 TV = 1.0625	**Loadcell:**	12COM254
Sample Description:	GR CH W/ SA	**Air Pressure (psi):**	3.6

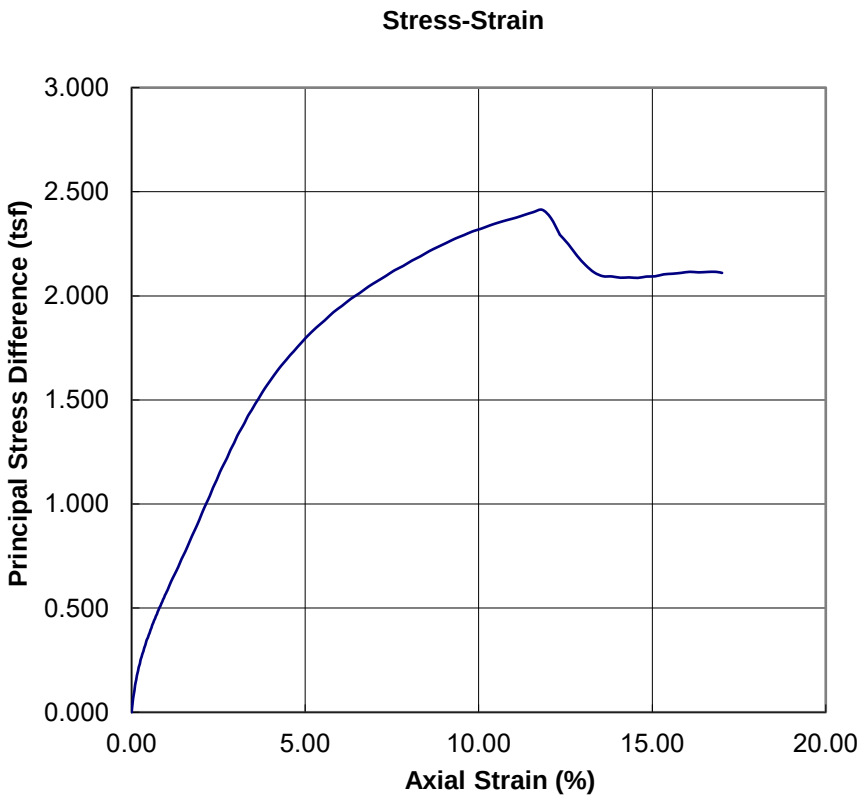
Sample Data:	1	2	3	Average	Height / Diameter Ratio (2 to 2.5)
Diameter (in)	2.862	2.845	2.827	2.845	2.02
Height (in)	5.740	5.735	5.733	5.736	
	Area, ft²:	0.044	Volume, ft³:	0.021	

	Moisture Content (%)		Unit Weight
Can Number:	DB-5	Wet Weight of Sample (g):	1248.07
Wt. of Can (g):	31.46	Dry Weight of Sample (g):	1053.10
Wt. of Wet Soil + Can (g):	84.08	Wet Unit Weight (pcf):	**130.4**
Wt. of Dry Soil + Can (g):	75.86	Dry Unit Weight (pcf):	**110.0**
Wt. of Dry Soil (g):	44.40		
Wt. of Water (g):	8.22		
Moisture Content (%):	**18.5**		

	Max Strain (≤ 15%)	Compressive Strength, tsf	Shear Strength, tsf
RESULTS:	**11.829**	**2.41**	**1.21**

FAILURE TYPE:

NOTE: _____



Tested By: RB
Computed By: RB
Reviewed By: _____

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UNCONSOLIDATED UNDRAINED TRIAXIAL TEST
ASTM D 2850

Project Name:	Long Point Bayou Marsh Creation Proj.	**Date Tested:**	7/14/2020
Project No.:	02541211	**Scale:**	03ES254
Boring No.:	B-4	**Calipers:**	01CAL254
Samp. and Spec. No.:	S-2	**Oven:**	10OV251
Sample Depth:	2-4'	**GeoJac Station No.:**	02GJ254
Qp / Torvane (tsf):	TV = 0.10	**Loadcell:**	16COM254
Sample Description:	GR CH W/ SI	**Air Pressure (psi):**	1.2

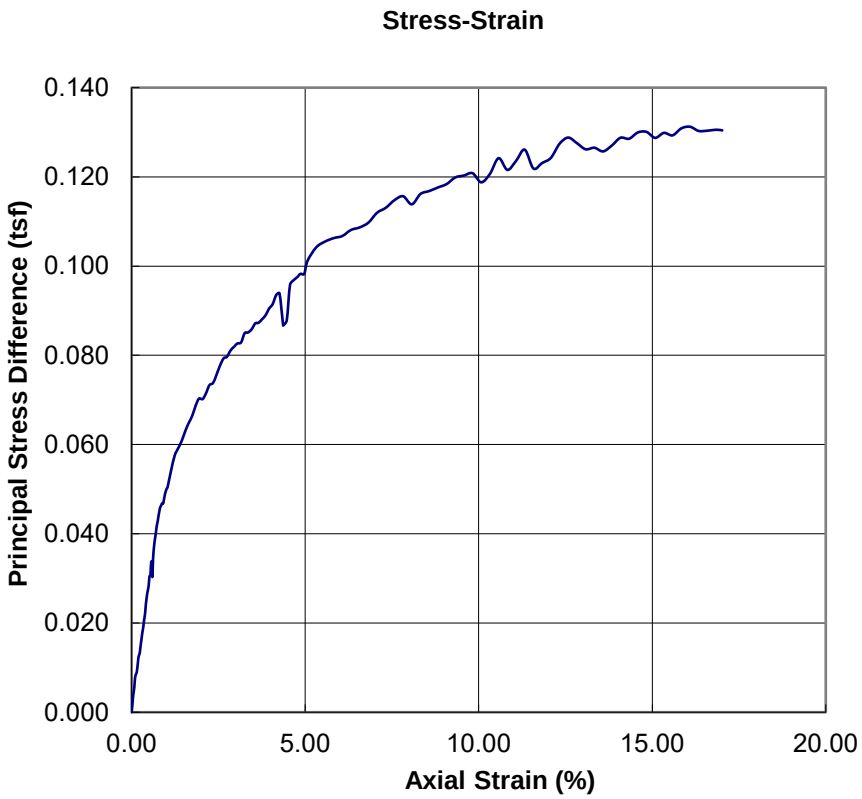
Sample Data:	1	2	3	Average	Height / Diameter Ratio (2 to 2.5)
Diameter (in)	2.822	2.837	2.739	2.799	1.93
Height (in)	5.402	5.379	5.389	5.390	
	Area, ft²:	0.043	Volume, ft³:	0.019	

Moisture Content (%)		**Unit Weight**	
Can Number:	S-28	Wet Weight of Sample (g):	943.72
Wt. of Can (g):	31.61	Dry Weight of Sample (g):	726.47
Wt. of Wet Soil + Can (g):	85.30	Wet Unit Weight (pcf):	**108.4**
Wt. of Dry Soil + Can (g):	72.94	Dry Unit Weight (pcf):	**83.4**
Wt. of Dry Soil (g):	41.33		
Wt. of Water (g):	12.36		
Moisture Content (%):	**29.9**		

	Max Strain (≤ 15%)	Compressive Strength, tsf	Shear Strength, tsf
RESULTS:	**15.086**	**0.13**	**0.06**

FAILURE TYPE:

NOTE: _____



Tested By: RB

Computed By: RB

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UNCONSOLIDATED UNDRAINED TRIAXIAL TEST
ASTM D 2850

Project Name:	Long Point Bayou Marsh Creation Proj.	**Date Tested:**	7/14/2020
Project No.:	02541211	**Scale:**	03ES254
Boring No.:	B-4	**Calipers:**	01CAL254
Samp. and Spec. No.:	S-5	**Oven:**	10OV251
Sample Depth:	8-10'	**GeoJac Station No.:**	02GJ254
Qp / Torvane (tsf):	TV = 0.65	**Loadcell:**	12COM254
Sample Description:	GR CH W/ SI & SA	**Air Pressure (psi):**	3.6

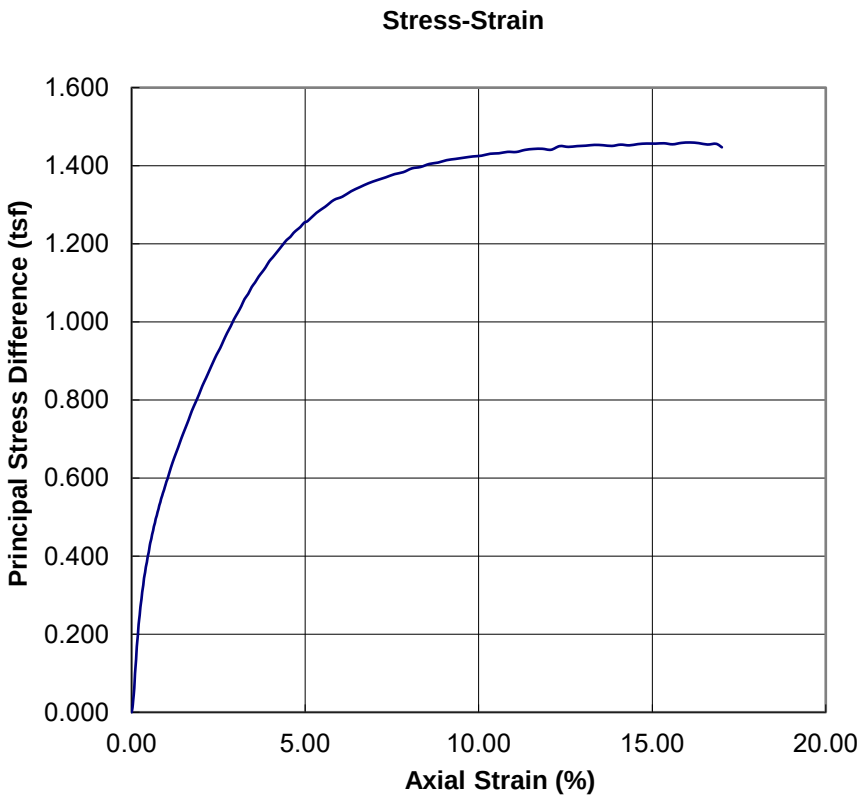
Sample Data:	1	2	3	Average	Height / Diameter Ratio (2 to 2.5)
Diameter (in)	2.860	2.862	2.859	2.860	2.03
Height (in)	5.807	5.799	5.801	5.802	
	Area, ft²:	0.045	Volume, ft³:	0.022	

	Moisture Content (%)		Unit Weight
Can Number:	302	Wet Weight of Sample (g):	1212.61
Wt. of Can (g):	29.81	Dry Weight of Sample (g):	976.48
Wt. of Wet Soil + Can (g):	82.19	Wet Unit Weight (pcf):	**123.9**
Wt. of Dry Soil + Can (g):	71.99	Dry Unit Weight (pcf):	**99.8**
Wt. of Dry Soil (g):	42.18		
Wt. of Water (g):	10.20		
Moisture Content (%):	**24.2**		

	Max Strain (≤ 15%)	Compressive Strength, tsf	Shear Strength, tsf
RESULTS:	**15.087**	**1.46**	**0.73**

FAILURE TYPE:

NOTE: _____



Tested By: RB
Computed By: RB
Reviewed By: _____

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UNCONSOLIDATED UNDRAINED TRIAXIAL TEST
ASTM D 2850

Project Name:	Long Point Bayou Marsh Creation Proj.	**Date Tested:**	7/14/2020
Project No.:	02541211	**Scale:**	03ES254
Boring No.:	B-5	**Calipers:**	01CAL254
Samp. and Spec. No.:	S-2	**Oven:**	10OV251
Sample Depth:	2-4'	**GeoJac Station No.:**	02GJ254
Qp / Torvane (tsf):	TV = 0.30	**Loadcell:**	17COM254
Sample Description:	GR CH W/ TR ORG	**Air Pressure (psi):**	1.2

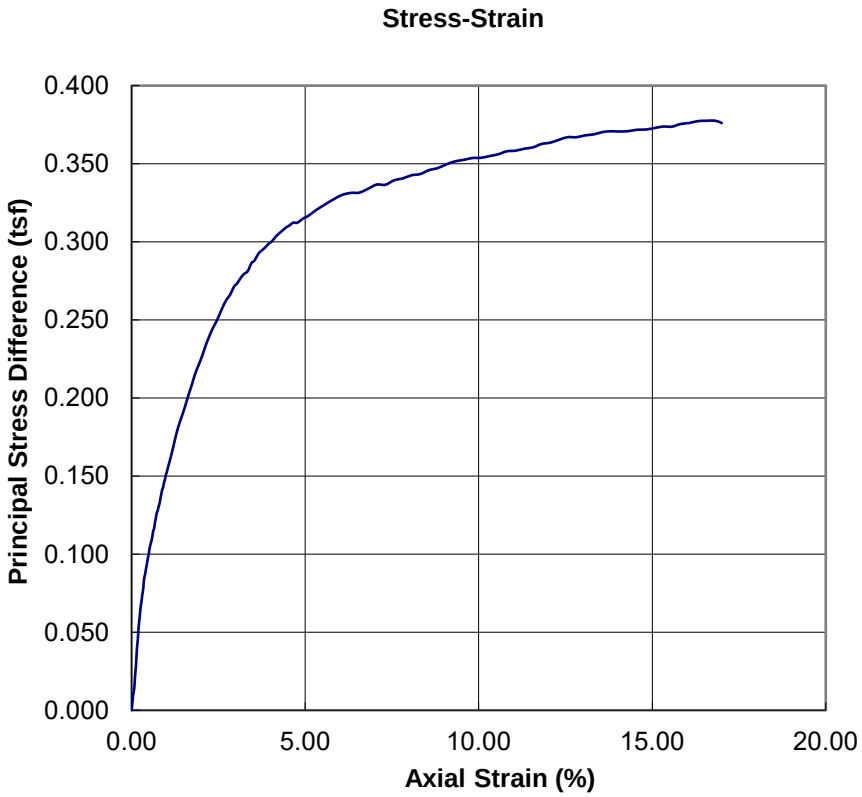
Sample Data:	1	2	3	Average	Height / Diameter Ratio (2 to 2.5)
Diameter (in)	2.852	2.804	2.835	2.830	2.05
Height (in)	5.803	5.812	5.807	5.807	
	Area, ft²:	0.044	Volume, ft³:	0.021	

	Moisture Content (%)		Unit Weight
Can Number:	246-21	Wet Weight of Sample (g):	1129.86
Wt. of Can (g):	29.75	Dry Weight of Sample (g):	834.41
Wt. of Wet Soil + Can (g):	82.41	Wet Unit Weight (pcf):	**117.8**
Wt. of Dry Soil + Can (g):	68.64	Dry Unit Weight (pcf):	**87.0**
Wt. of Dry Soil (g):	38.89		
Wt. of Water (g):	13.77		
Moisture Content (%):	**35.4**		

	Max Strain (≤ 15%)	Compressive Strength, tsf	Shear Strength, tsf
RESULTS:	**15.065**	**0.37**	**0.19**

FAILURE TYPE:

NOTE: _____



Tested By: RB
Computed By: RB
Reviewed By: _____

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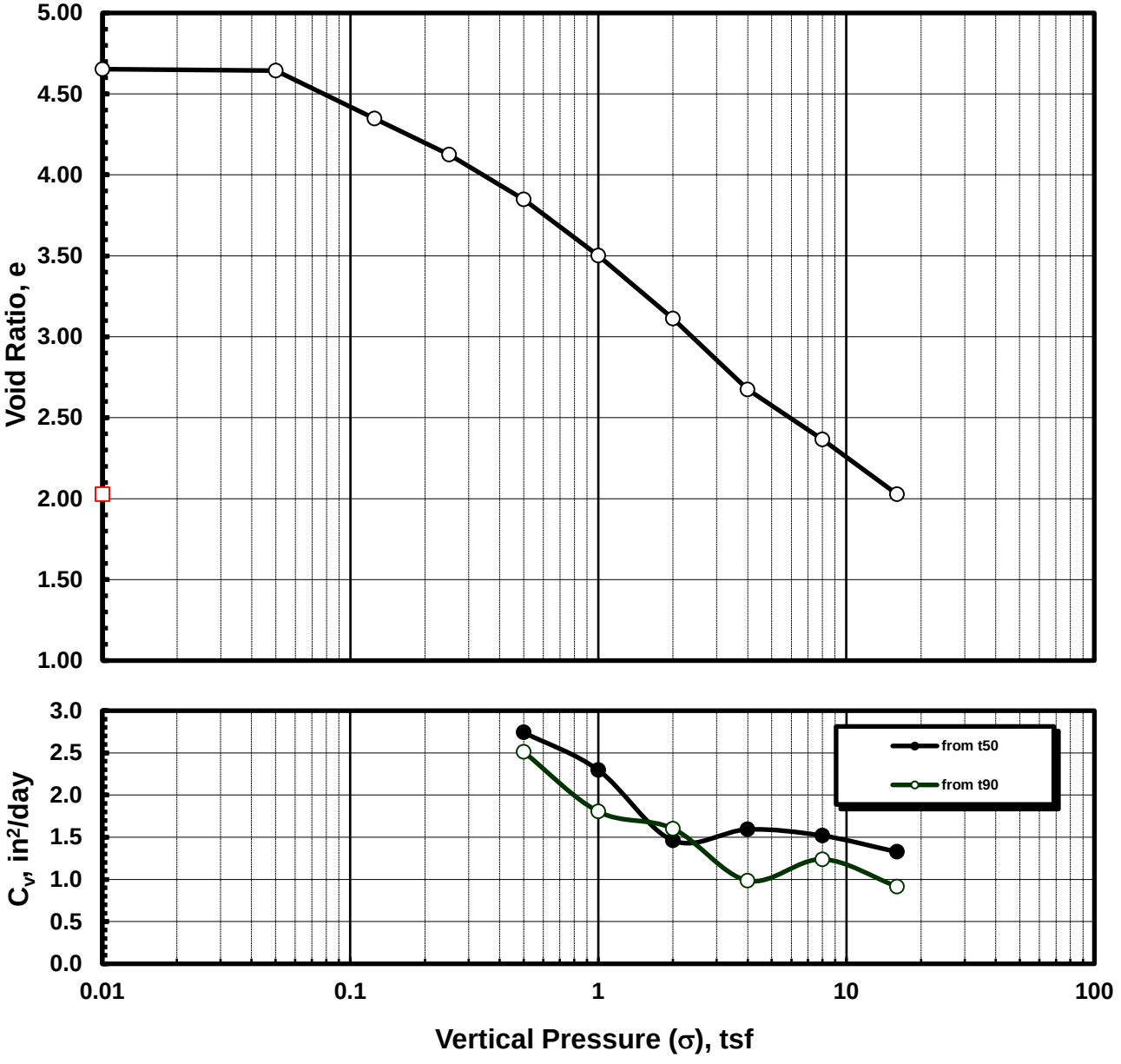
APPENDIX E

CONSOLIDATION TEST RESULTS
SETTLING COLUMN TEST AND SLURRY CONSOLIDATION TEST RESULTS

CONSOLIDATION TEST RESULTS - ASTM D 2435



Sample Condition	Before	After	Consolidation Parameters	
Moisture Content, %:	174.8%	79.4%	Overburden Pressure, tsf:	0.27
Sample Height, in.:	0.9970	0.5340	Preconsolidation Pressure, tsf:	0.20
Void Ratio, e:	4.6531	2.0277	Compression Index, (Cc):	1.224
Dry Unit Weight, pcf:	28.7	53.6	Re-Compression Index, (Cr)	
Degree of Saturation:	1.0	1.0	Swell Index, Cs:	-

Project Number:	02541211	Liquid Limit:	NA	Hand Pen:	0.05 tsf
Project Name	Long Point Bayou Marsh Creation	Plastic Limit:	NA	-200 %:	NA
Boring No.:	B-1	Plasticity Index:	NA	SPG:	2.6
Sample ID, Depth:	S-4, 6-8 ft	Classification:	Organic Clay (OH), Dark Gray		

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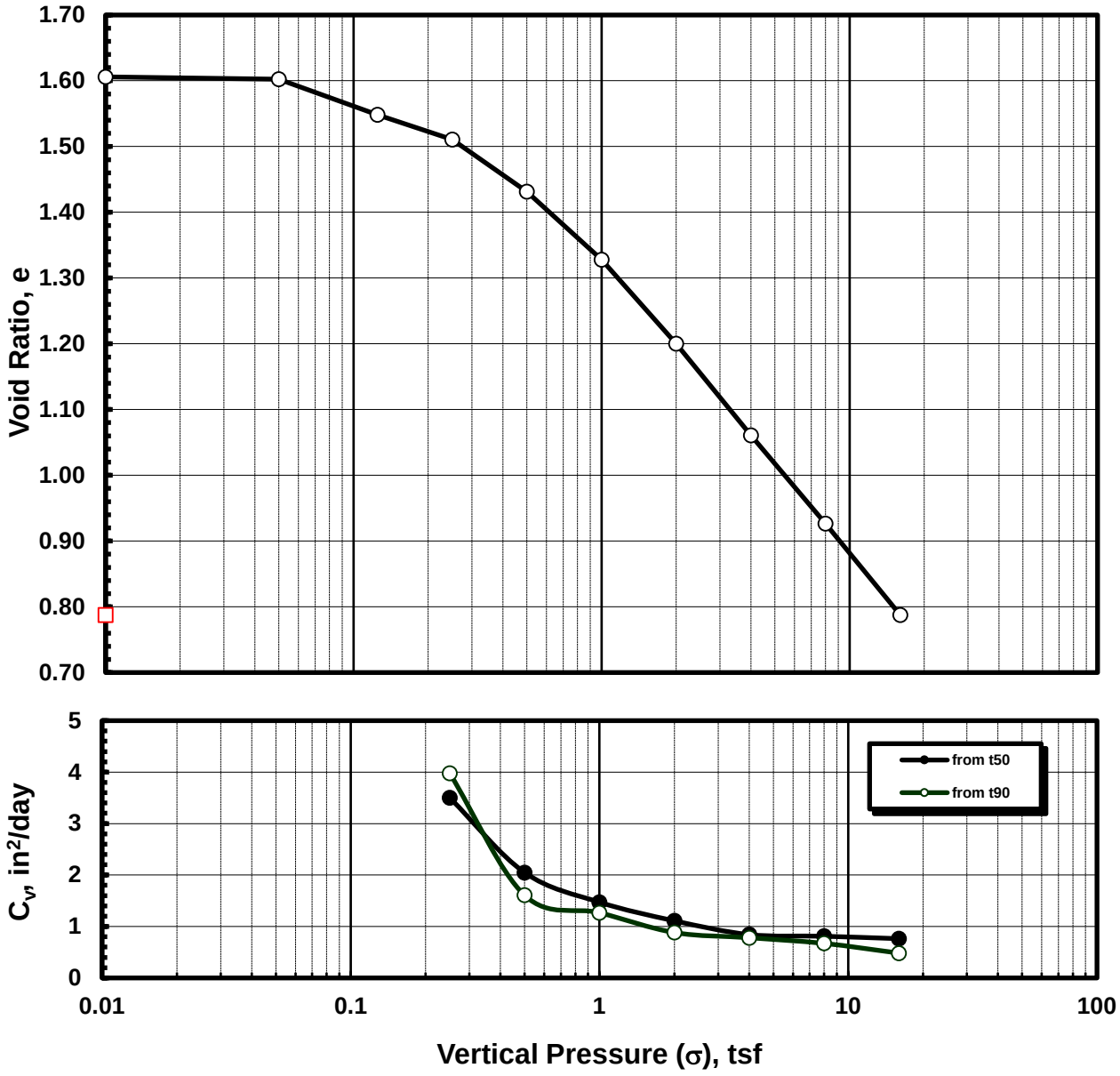
CONSOLIDATION TEST RESULTS - ASTM D 2435



Sample Condition	Before	After	Consolidation Parameters	
Moisture Content, %:	58.7%	29.8%	Overburden Pressure, tsf:	0.09
Sample Height, in.:	0.9980	0.6846	Preconsolidation Pressure, tsf:	0.35
Void Ratio, e:	1.6059	0.7876	Compression Index, (Cc):	0.457
Dry Unit Weight, pcf:	64.7	94.2	Re-Compression Index, (Cr)	-
Degree of Saturation:	1.0	1.0	Swell Index, Cs:	-

Project Number:	254-1211	Liquid Limit:	86	Torvane:	0.25 tsf
Project Name	Long Point Bayou Marsh Creation	Plastic Limit:	23	-200 %:	99
Boring No.:	B-2	Plasticity Index:	63	SPG:	2.7
Sample ID, Depth:	S-1, 0-2 ft	Classification:	Fat Clay (CH), Gray/ Brown		

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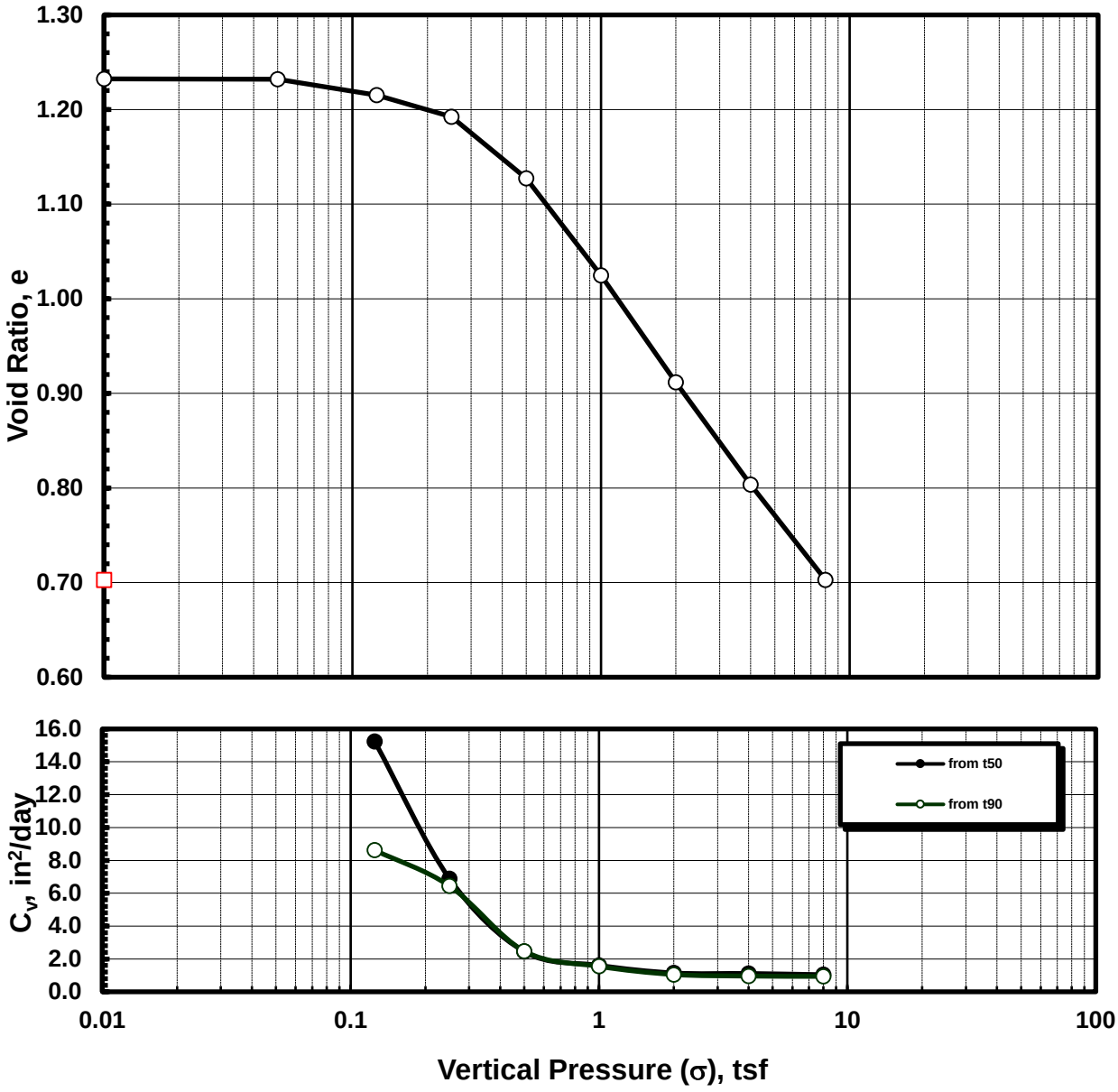
CONSOLIDATION TEST RESULTS - ASTM D 2435



Sample Condition	Before	After	Consolidation Parameters	
Moisture Content, %:	45.7%	26.0%	Overburden Pressure, tsf:	0.21
Sample Height, in.:	0.9980	0.7613	Preconsolidation Pressure, tsf:	0.30
Void Ratio, e:	1.2324	0.7029	Compression Index, (Cc):	0.356
Dry Unit Weight, pcf:	75.5	98.9	Re-Compression Index, (Cr)	
Degree of Saturation:	1.00	1.00	Swell Index, Cs:	-

Project Number:	02541211	Liquid Limit:	NA	Hand Pen:	0.10 tsf
Project Name	Long Point Bayou Marsh Creation	Plastic Limit:	NA	-200 %:	NA
Boring No.:	B-3	Plasticity Index:	NA	SPG:	2.7
Sample ID, Depth:	S-3, 4-6 ft	Classification:	Fat Clay (CH), Gray		

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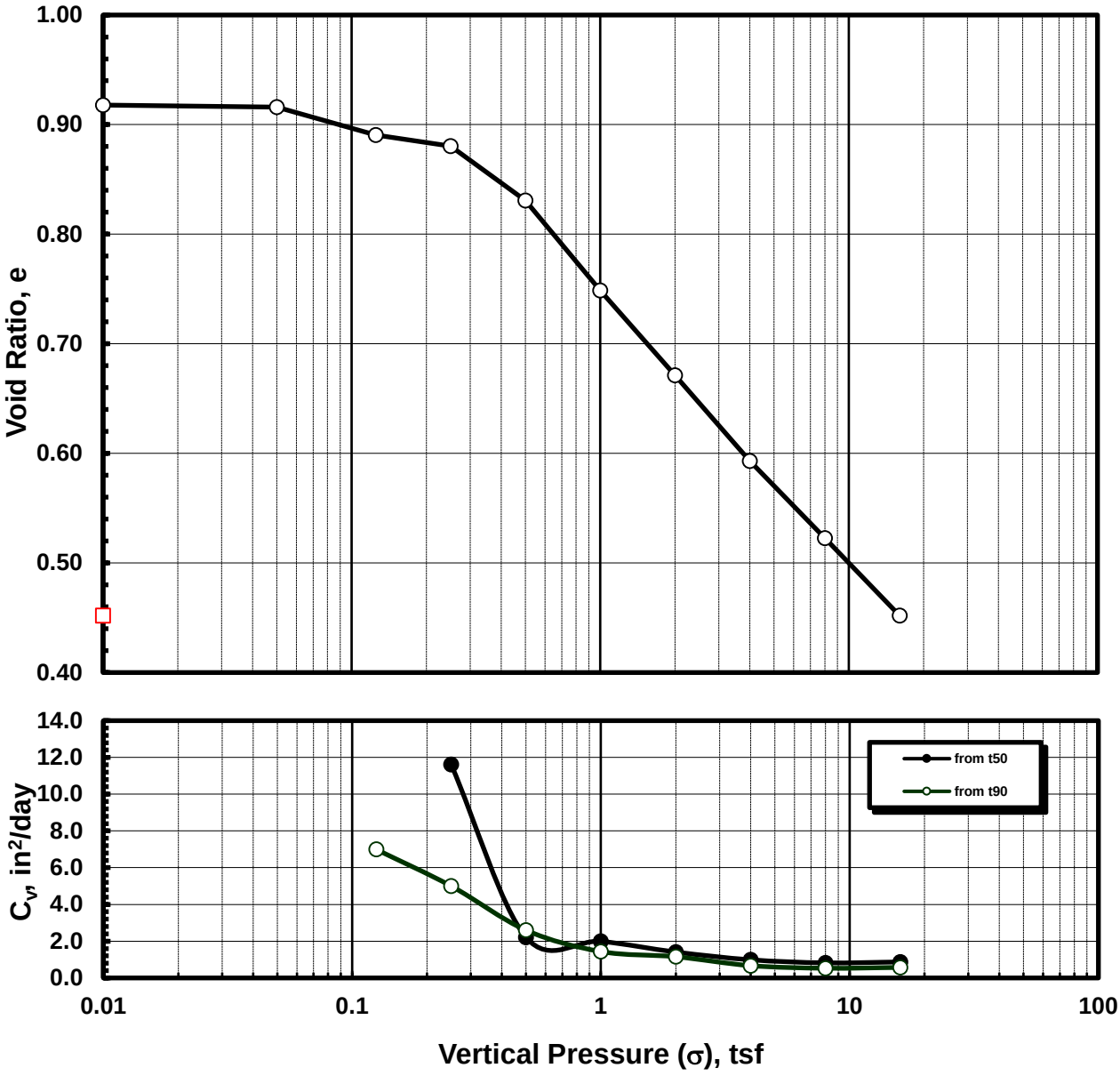
CONSOLIDATION TEST RESULTS - ASTM D 2435



Sample Condition	Before	After	Consolidation Parameters	
Moisture Content, %:	33.9%	16.7%	Overburden Pressure, tsf:	0.4
Sample Height, in.:	1.0000	0.7571	Preconsolidation Pressure, tsf:	0.30
Void Ratio, e:	0.9178	0.4519	Compression Index, (Cc):	0.246
Dry Unit Weight, pcf:	87.8	116.0	Re-Compression Index, (Cr)	-
Degree of Saturation:	1.00	1.00	Swell Index, Cs:	-

Project Number:	254-1211	Liquid Limit:	NA	Torvane:	0.1 tsf
Project Name	Long Point Bayou Marsh Creation	Plastic Limit:	NA	-200 %:	NA
Boring No.:	B-4	Plasticity Index:	NA	SPG:	2.7
Sample ID, Depth:	S-6, 10-12 ft	Classification:	Fat Clay with Sand (CH), Gray		

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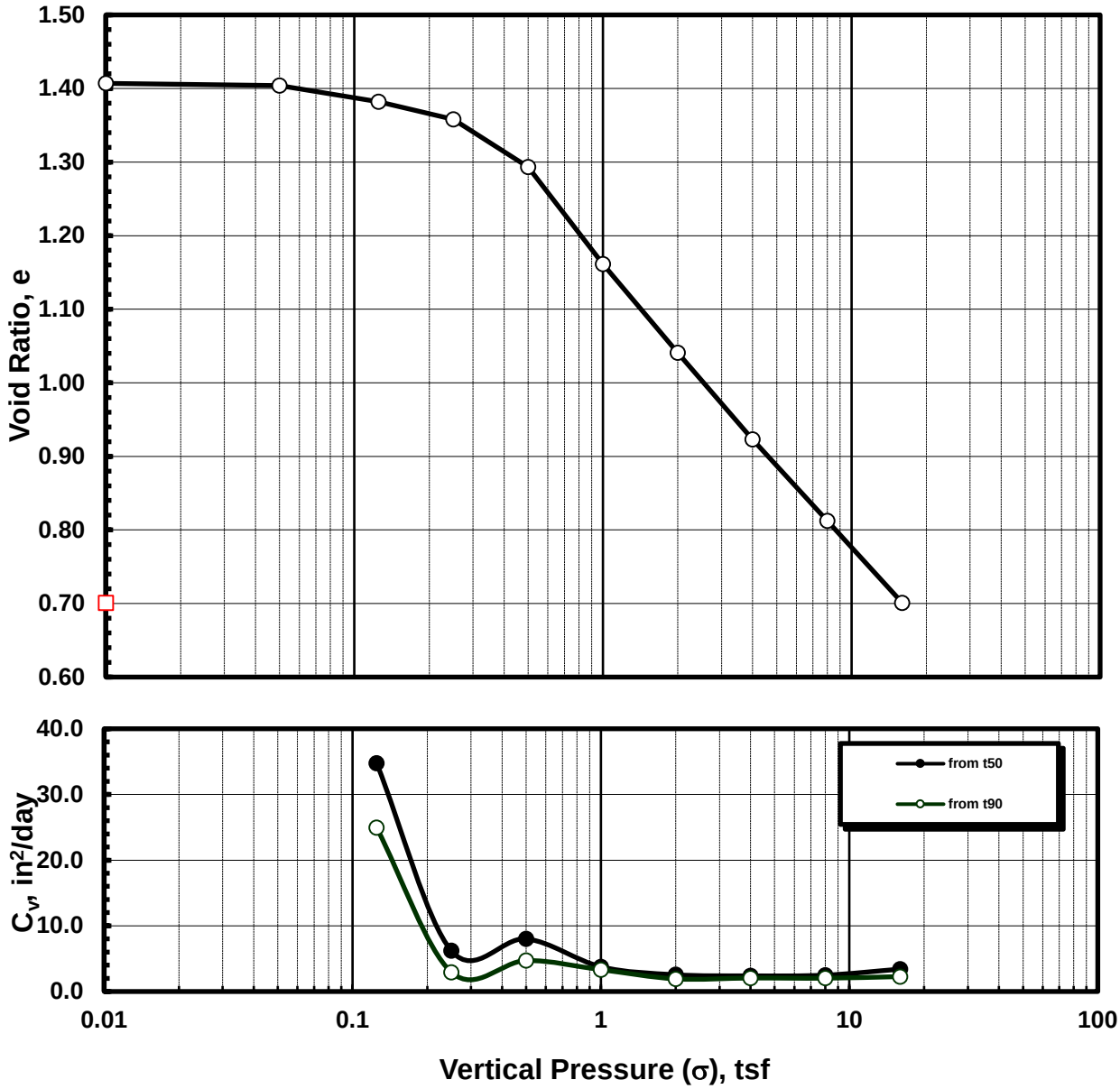
CONSOLIDATION TEST RESULTS - ASTM D 2435



Sample Condition	Before	After	Consolidation Parameters	
Moisture Content, %:	52.4%	26.0%	Overburden Pressure, tsf:	0.15
Sample Height, in.:	0.9960	0.7038	Preconsolidation Pressure, tsf:	0.30
Void Ratio, e:	1.4070	0.7009	Compression Index, (Cc):	0.393
Dry Unit Weight, pcf:	69.8	98.8	Re-Compression Index, (Cr)	-
Degree of Saturation:	1.00	1.00	Swell Index, Cs:	-

Project Number:	02541211	Liquid Limit:	53	Hand Pen:	0.15 tsf
Project Name	Long Point Bayou Marsh Creation	Plastic Limit:	15	-200 %:	94
Boring No.:	B-5	Plasticity Index:	38	SPG:	2.692
Sample ID, Depth:	S-2, 2-4 ft	Classification:	Fat Clay (CH); Dark Gray w/ organics		

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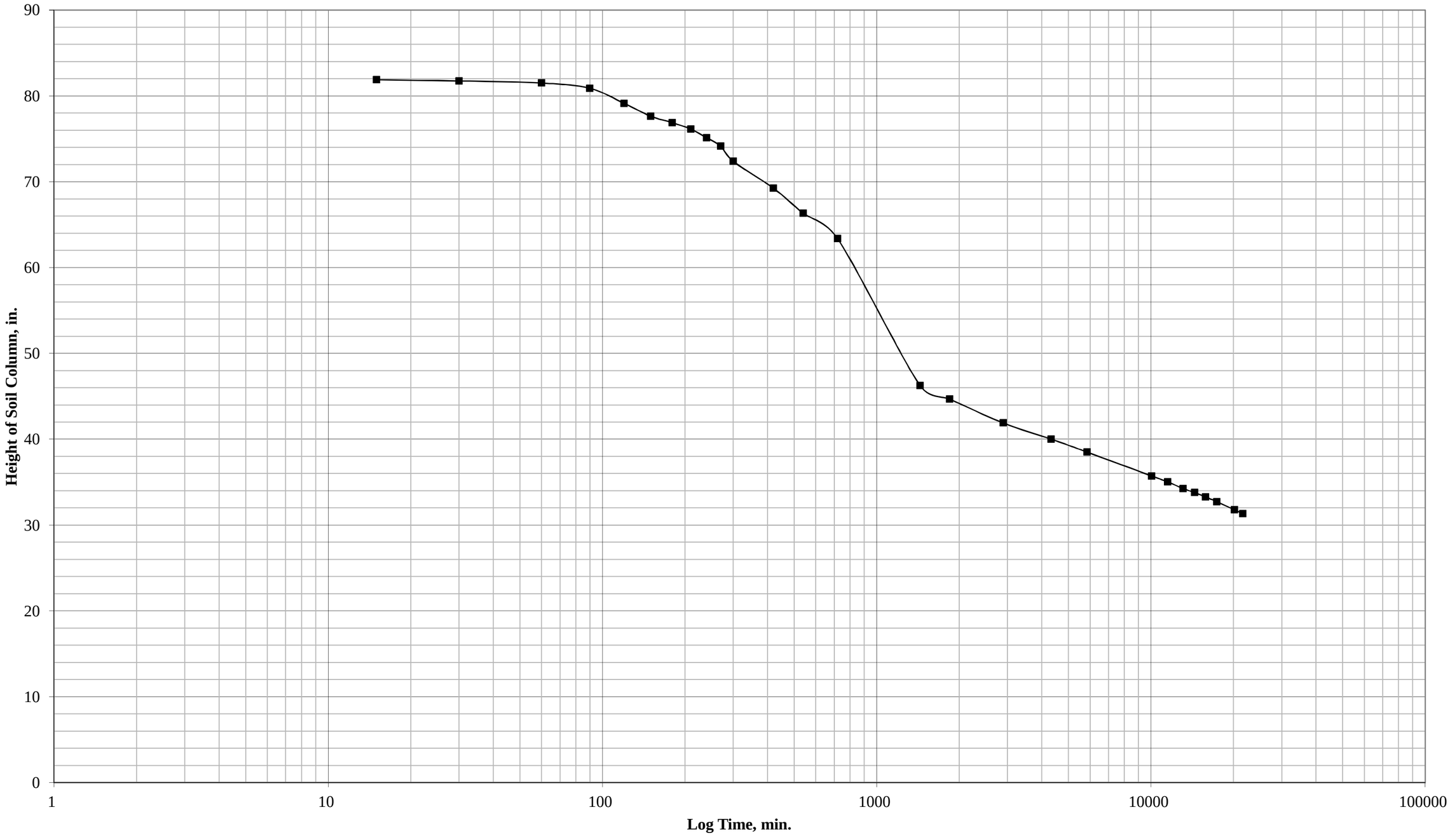
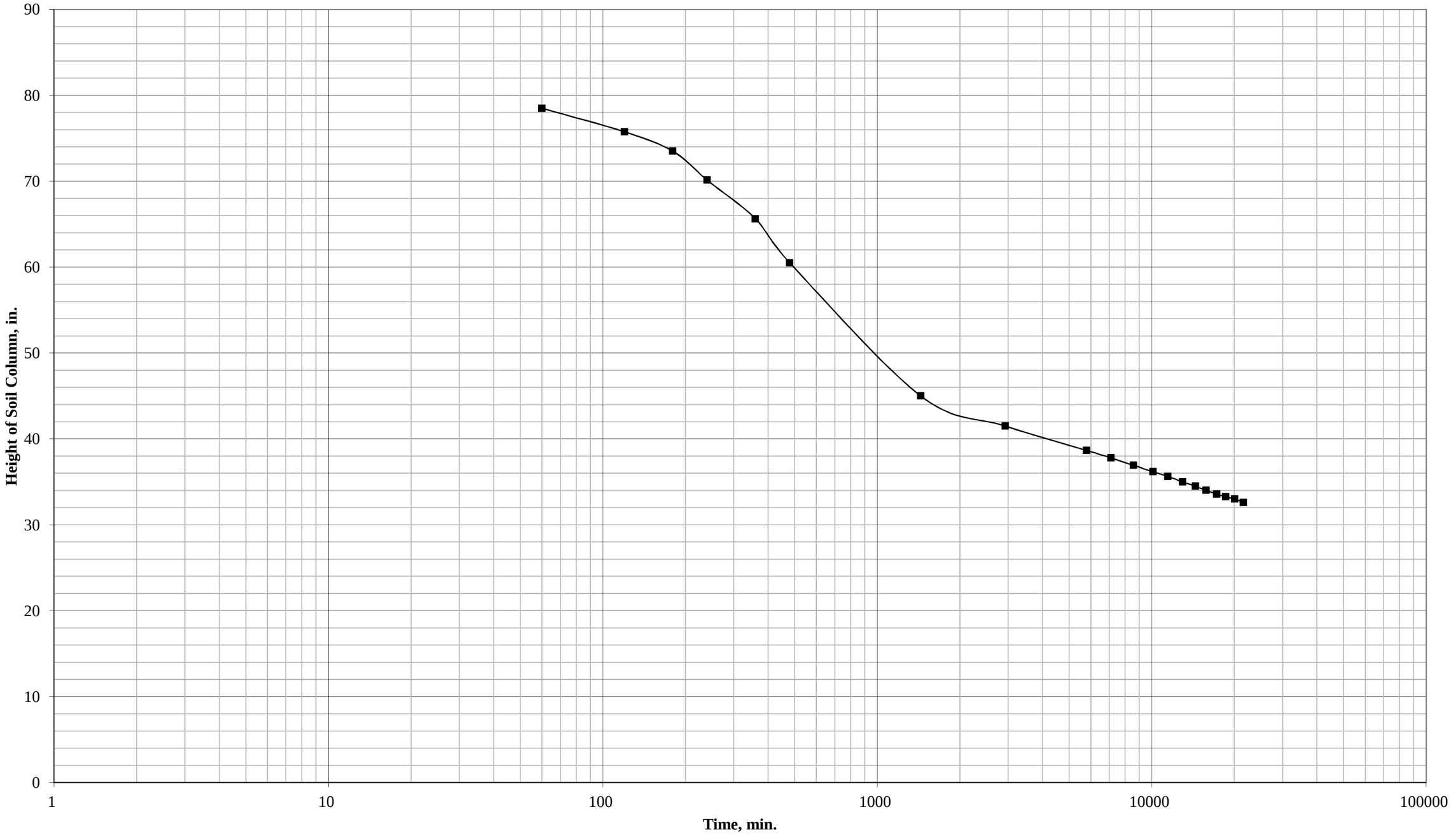
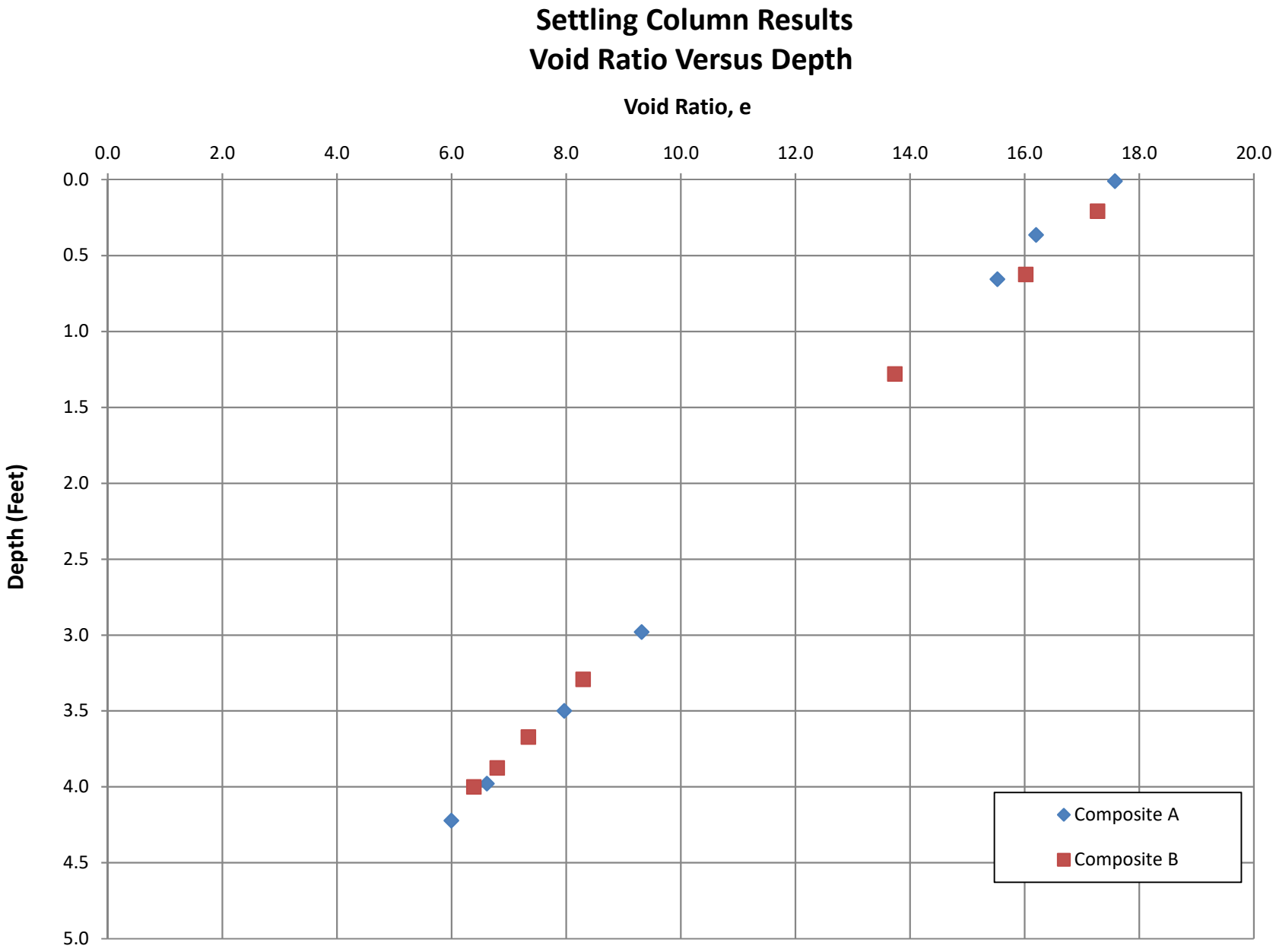
Settling Colum Test

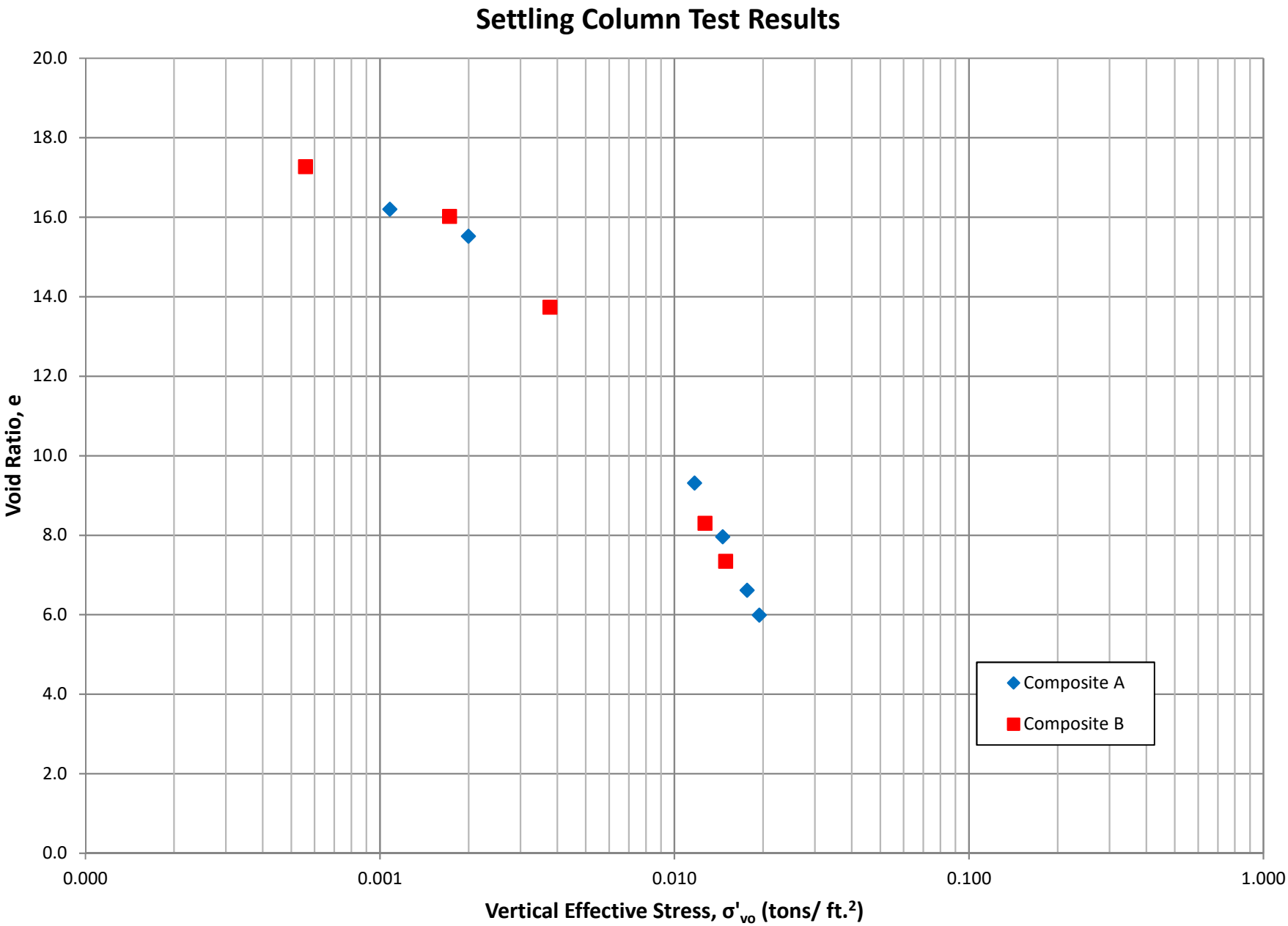
Composite A- Settling column



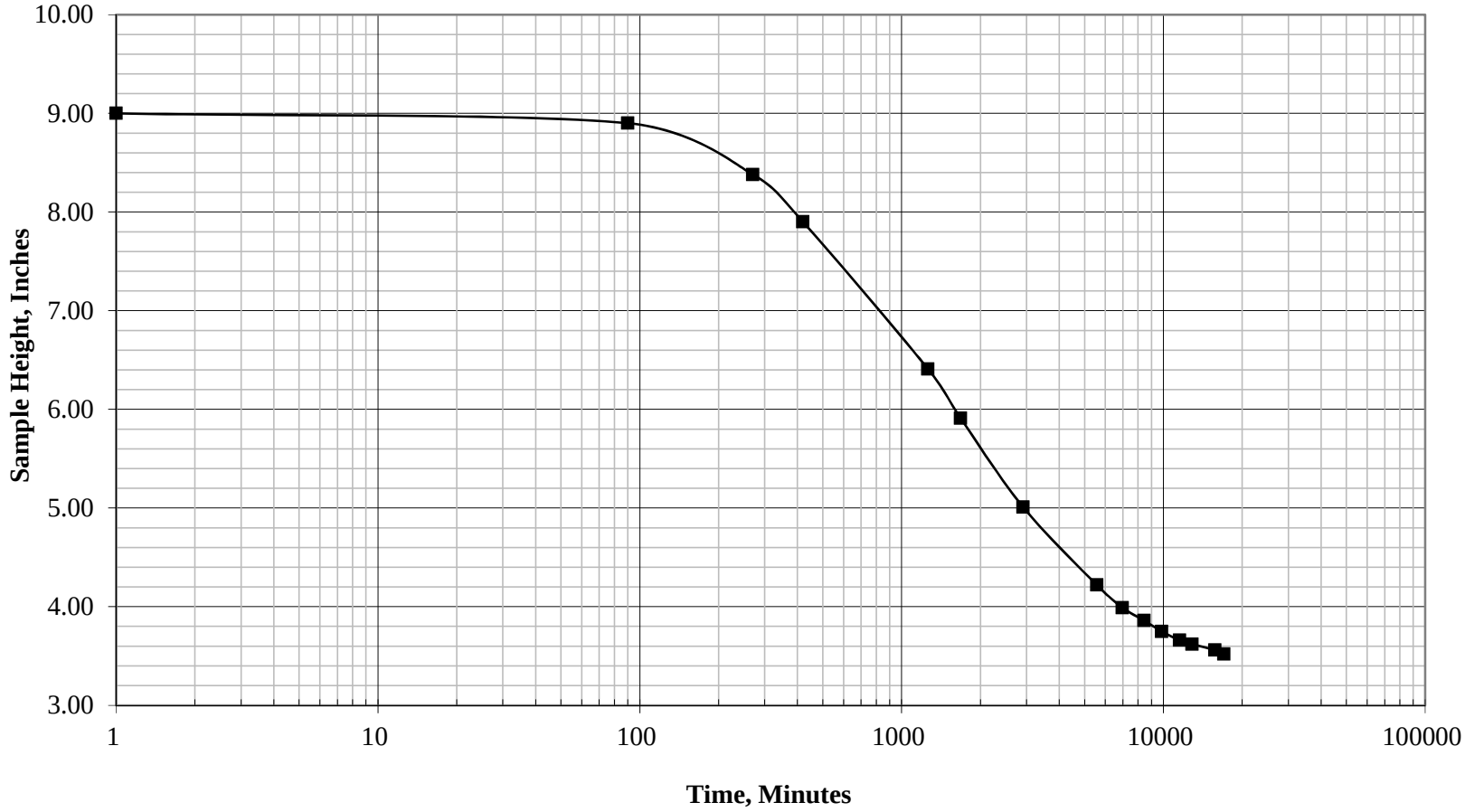
Composite B- Settling column



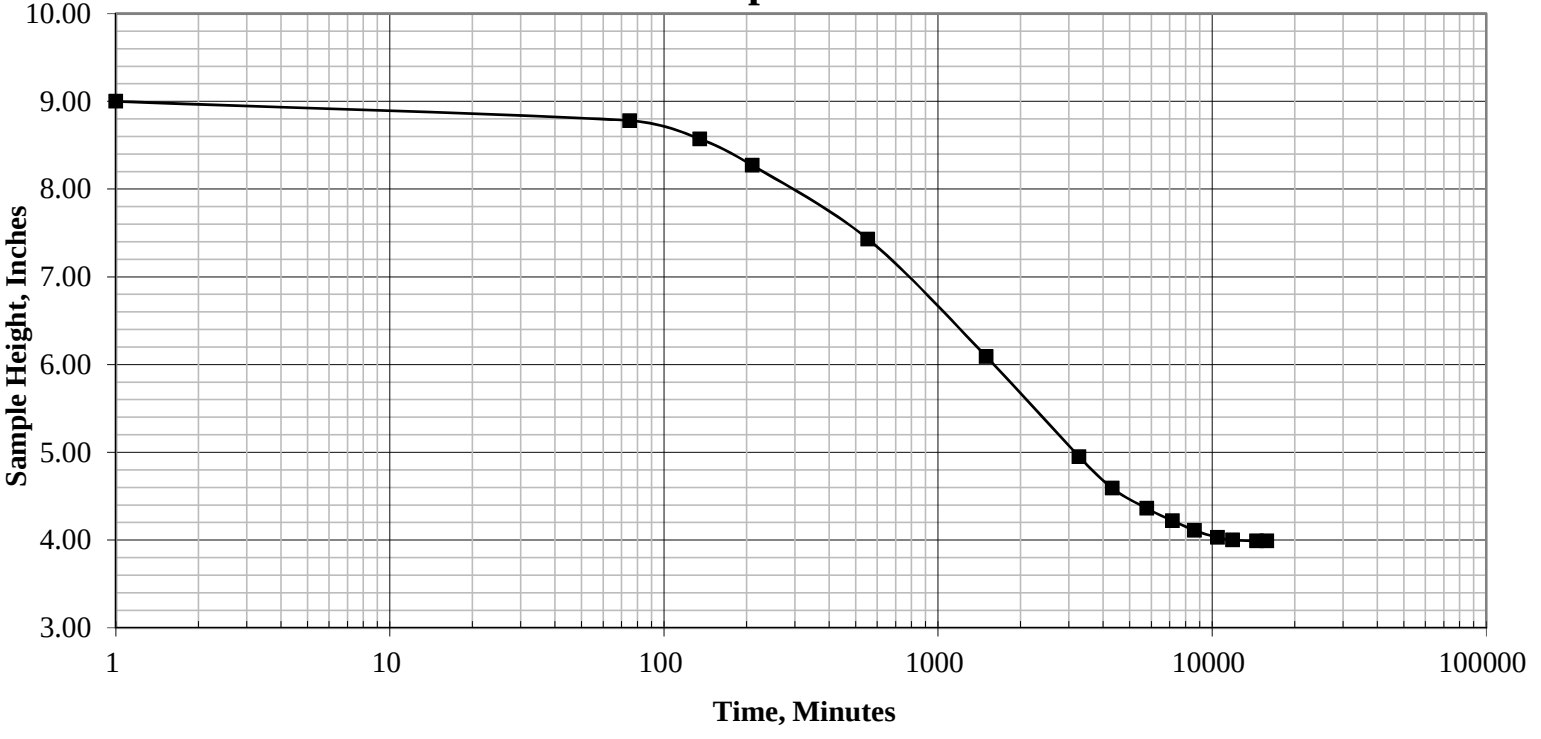

Settling Column Results
Void Ratio Versus Depth
Void Ratio, e
0.0
2.0
4.0
6.0
8.0
10.0
12.0
14.0
16.0
18.0
20.0
Depth (Feet)
0.0
0.5
1.0
1.5
2.0
2.5
3.0
3.5
4.0
4.5
5.0
Composite A
Composite B

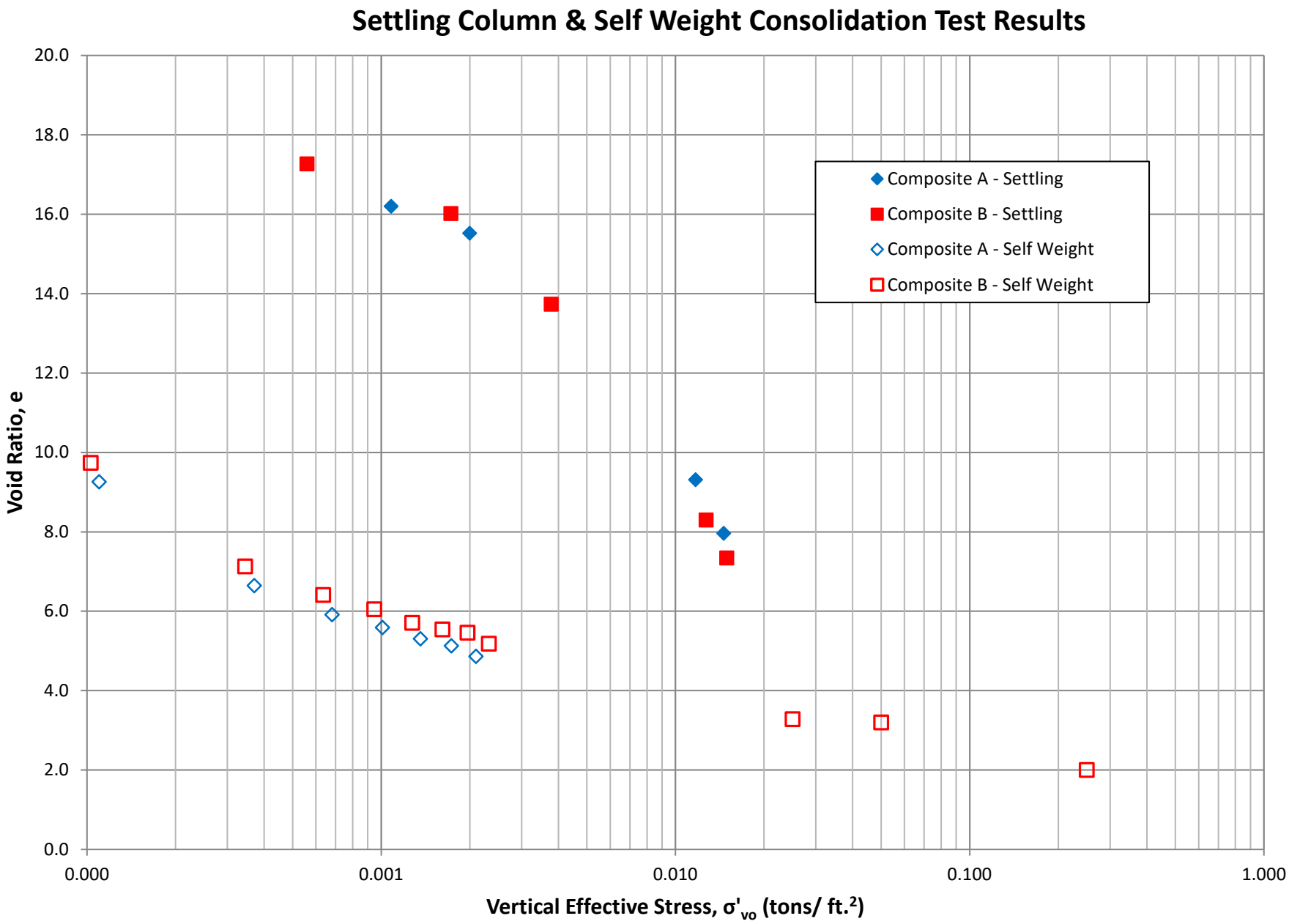

Settling Column Test Results
20.0
18.0
16.0
14.0
12.0
10.0
8.0
6.0
4.0
2.0
0.0
Void Ratio, e
0.000
0.001
0.010
0.100
1.000
Vertical Effective Stress, σ'vo (tons/ ft.2)
Composite A
Composite B

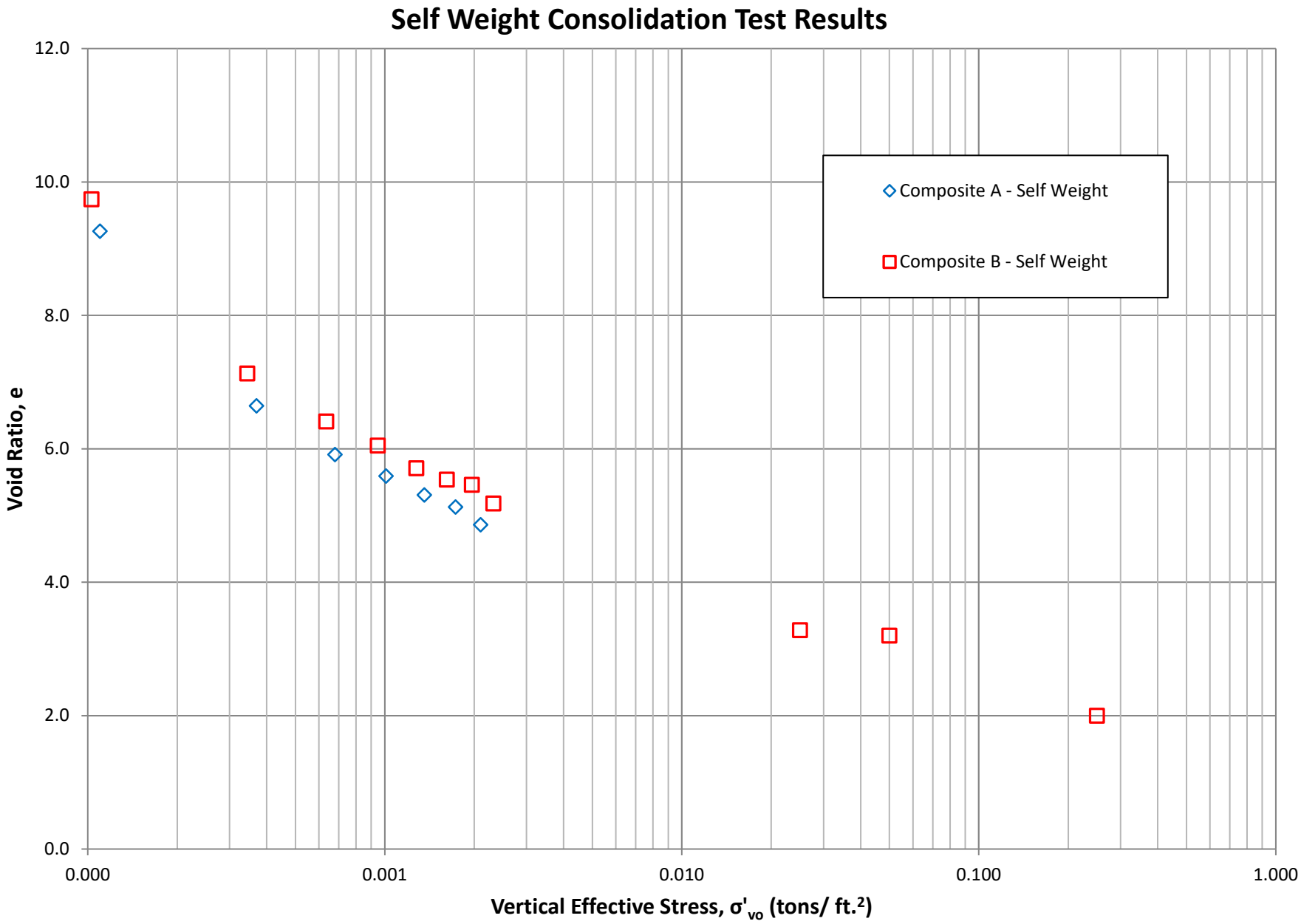
SELF-WEIGHT TEST
Composite A
Initial Sample Consolidation



SELF-WEIGHT TEST
Composite B
Initial Sample Consolidation




Settling Column & Self Weight Consolidation Test Results
Void Ratio, e
20.0
18.0
16.0
14.0
12.0
10.0
8.0
6.0
4.0
2.0
0.0
0.000
0.001
0.010
0.100
1.000
Vertical Effective Stress, σ'vo (tons/ ft.2)
Composite A - Settling
Composite B - Settling
Composite A - Self Weight
Composite B - Self Weight


Self Weight Consolidation Test Results
12.0
10.0
8.0
6.0
4.0
2.0
0.0
Void Ratio, e
0.000
0.001
0.010
0.100
1.000
Vertical Effective Stress, σ'vo (tons/ ft.²)
Composite A - Self Weight
Composite B - Self Weight