



**Geotechnical Data Report
Bayou De Cade Marsh Creation and
Ridge Restoration (TE-0138)
Terrebonne Parish, Louisiana**

**Fugro Project No. 04.55174066
June 2018**



Report No. 04.55174047
June 8, 2018

COASTAL PROTECTION AND RESTORATION AUTHORITY

8404 River Road
Geismar, Louisiana 70734

Attention: Ms. April Newman
CPRA Task Manager

**DRAFT Geotechnical Data Report
Bayou De Cade Marsh Creation and Ridge Restoration (TE-0138)
Terrebonne Parish, Louisiana**

Fugro USA Land, Inc. (Fugro) is pleased to submit this geotechnical data report for the referenced project. Fugro's services were authorized by the State of Louisiana Coastal Protection and Restoration Authority (CPRA) on March 5, 2018 under Contract No. 440010495. This study was performed in general accordance with Fugro's Proposal No. 04.55174066_rev2, dated December 19, 2017.

As of June 8, 2018, there are a few pending test results pertaining to the consolidation tests, i.e., Atterberg limits and specific gravities. They will be added to the final report.

We appreciate the opportunity to be of service to CPRA and look forward to working together on the next phase of the project. Please call if you have any questions about this report.

Sincerely,
FUGRO USA LAND, INC.

Samuel M. Bryant, P.E.
Vice President

Eric Marx, P.E.
Vice President

Copies Submitted: pdf to addressee



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1. INTRODUCTION

1.1 Project Description

The Louisiana Coastal Protection and Restoration Authority (CPRA) is planning to restore 11,276 linear feet of ridge habitat along the northern bank of Bayou De Cade and create/nourish approximately 504 acres of marsh by pumping hydraulically dredged material from Lake De Cade to the designated fill sites.

The site is located as shown on Plate 1. A site layout is presented as Plate 2. The project site is located in Terrebonne Parish, Louisiana, about 12 miles west of Dulac and immediately west of Lake De Cade. Approximate project area center coordinates are N29°22'37.23" and W90°55'00.39" (RE: NAD83). Elevations noted herein are based on the 1983 North American Vertical Datum (NAVD83). The land owner for the marsh creation area is Apache Louisiana Minerals LLC.

1.2 Purposes and Scope

The purpose of the geotechnical data study was to: 1) explore and evaluate subsurface soil conditions, and 2) perform laboratory testing to develop pertinent engineering parameters for marsh restoration.

1.3 Authorization and Personnel

Ms. April Newman is the CPRA task manager. Mr. Eric Marx, P.E., is the Fugro Project Manager, and Mr. Sam Bryant, P.E., is the Fugro technical lead. Mr. Ryan Fasone, with Fugro, coordinated field exploration. Exploration location and magnetometer survey services were provided by Fugro's survey group in Lafayette, Louisiana, with Mr. Jesse Kibodeaux, as the survey manager. Dr. William Moe, Ph.D, P.E., Principal/Manager, with SCTCS Group LLC, performed the column settling tests

1.4 Report Applicability

Explorations, laboratory testing, findings, and conclusions presented in this data report are based on the project description, as described herein, and the authorized scope of work.

If there are differences or changes in project location or design features from those described herein, Fugro should be authorized to review changes and propose additional exploration and laboratory testing, if deemed appropriate. Observations, conclusions, and recommendations may not apply to locations beyond explorations performed for this study and beyond project boundaries.

Fugro prepared this report exclusively for CPRA to guide geotechnical aspects of design and construction of proposed facilities. The study was conducted using the standard level of care and



diligence normally practiced by recognized engineering firms now performing similar services under similar circumstances in the area. This report, including all illustrations and appendices, should be used in its entirety. This report should be made available for information only and not as a warranty of subsurface conditions.

2. FIELD EXPLORATION

Field exploration, described in Appendix A, included fifteen (15) cone penetration test (CPT) soundings and fifteen (15) borings.

3. LABORATORY TESTING

Laboratory testing was performed to aid material classification, shear strength, compressibility and corrosion characteristics. Laboratory test results are presented in Appendix B. Column settling tests were performed on two selected composite samples. Test procedures and results are presented in Appendix B1.

4. GEOLOGY AND SUBSURFACE CONDITIONS

4.1 Site Description

Topographic and existing feature information is presented on Plate 2. Saucier (1994, Plate 14) indicate the site is underlain by Holocene Intertributary deposits. Surficial conditions range from over water to within the marsh area and out in Lake DeCade, to just above water land surfaces around the marsh perimeter.

4.2 Geographic Information System Database

Information developed or obtained for the project was included in a geographic information system (GIS) databased using ESRI (2018) ArcGIS, version 10.4. Data from explorations, i.e., field and laboratory data, was included in a GIS database using Bentley Systems (2018) gINT, version 10. The gINT database file is linked to ArcGIS for processing. CPT electronic data files are included in the ArcGIS database.

4.3 Subsurface Conditions

4.3.1 Cross-Sections

Example subsurface profiles, presented as Plates 3a to 3d, generally show the distribution of subsurface conditions across the section lines. Profile locations are shown on Plate 2.



4.3.2 Earth Materials

Earth materials encountered in explorations consist mostly of soft clay with interbedded sand and silt layers. Organic and peat layers are also present. Comparing to Profile A-A', Profile B-B seems to indicate a more continuous sandy zone following along the profile line between about El -13 and -5 ft or so.

4.3.3 Water Conditions

A nearby CRMS (2018) gauge CRMS0398-H01, located about 3/4-mile north of the marsh site center, indicates a mean water elevation of about El+0.65 ft, a range from about El-0.5 ft to as high as El+2.0 ft, and with a more typical range from about El+0.2 to El+1 ft for daily measurements between October 2016 to September/October 2017.

Wave action during field exploration was notable and affected water surface elevation measurements at exploration locations, see Table A-1 in Appendix A.

5. REFERENCES

Apache Louisiana Mineral LLC (2017) "Access Permit; Bayou Decade Ridge and Marsh Creation (TE-138), Terrebonne Parish, Louisiana," letter to Fugro USA Land, Inc., Attn: Mr. Mike Allen, P.G., November 10.

ASTM International (2017) "ASTM Compass, Section: 4 Construction," <https://compass.astm.org>.

Bentley Systems (2018) "gINT Professional, version 10," <https://www.bentley.com/en>.

Coastwide Reference Monitoring System (CRMS) (2018)
https://www.lacoast.gov/crms_viewer2/default.aspx

ESRI (2018) "ArcGIS, version 10.4," <https://www.esri.com/en-us/home>.

Olson, R.E., Rauch, A.F., Mecham, E.C., and Luke, A.M. (2003) "Self-Weight Consolidation of Large Laboratory Deposits of Clay," Proceedings 12th Pan American Conference on Soil Mechanics and Geotechnical Engineering, MIT, Vol 1, pp. 703-708/

Robertson, P.K. and Cabal, K.L. (2015) "Guide to Cone Penetration Testing for Geotechnical Engineering, 6th Edition," prepared for Gregg Drilling & Testing, Inc.

Saucier, R.T. (1994) "Geomorphology and Quaternary Geologic History of the Lower Mississippi River Valley, Volumes I and II," prepared for The President Mississippi River Commission Vicksburg, Mississippi and US Army of Corps of Engineers, December.



U.S. Army Corps of Engineers (USACE) (1987) "Confined Disposal of Dredged Material," EM 1110-2-5027, September 30, *column settling testing described in Section 3-3 and Appendix B, Plans and Specifications.*

U.S. Army Corps of Engineers (USACE) (2015) "Dredging and Dredged Material Management," EM 1110-2-5025, July 31, *supersedes EM 1110-2-5027, column settling testing described in Appendix G, Plans and Specifications and Appendix H, Column Settling Test Procedures.*



PLATES

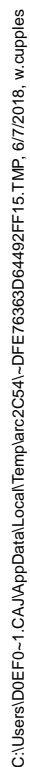
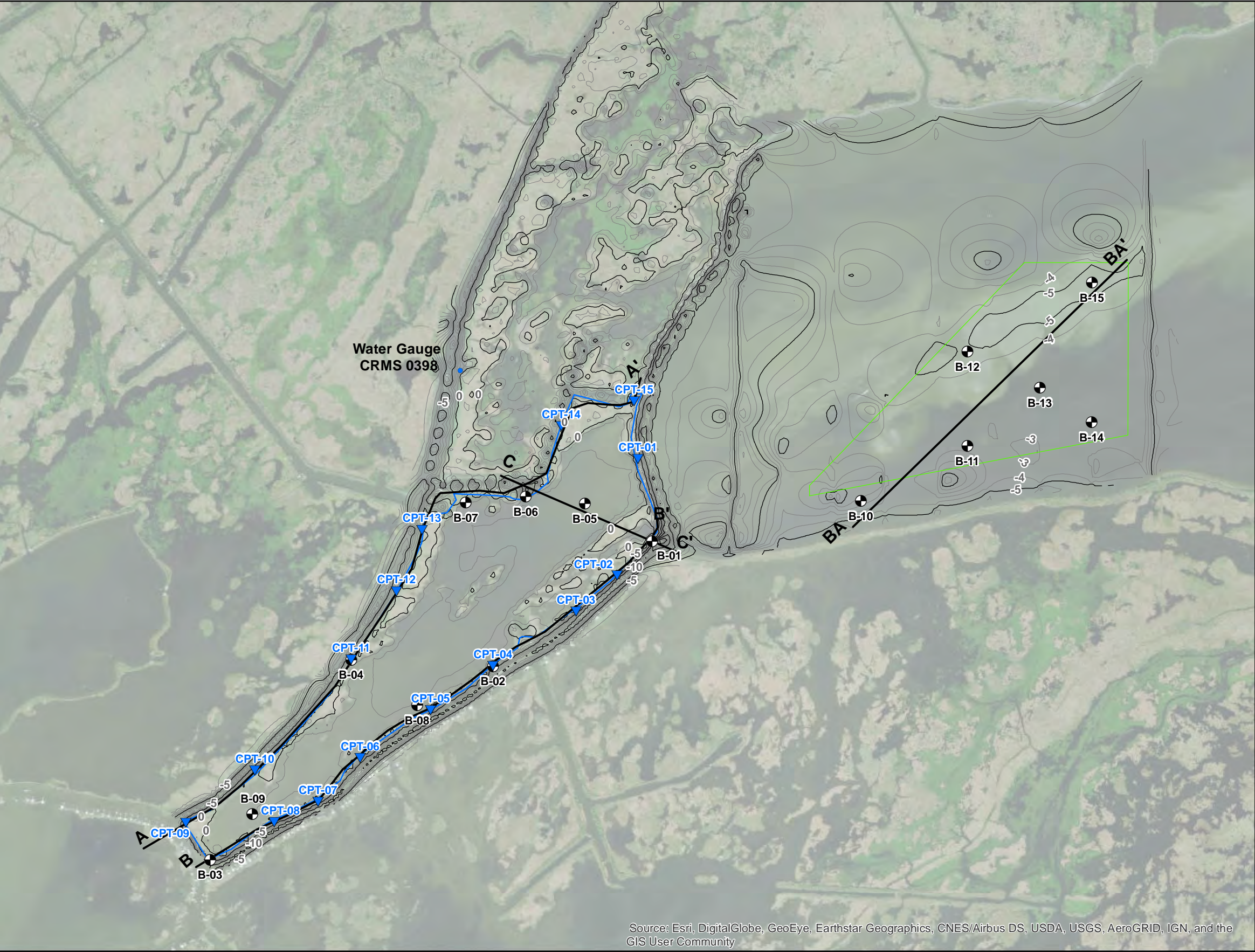


Plate 1

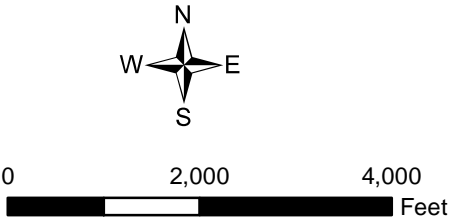


Legend

- Fugro CPT
- Fugro Boring
- Subsurface Profile Line Location
- Project Area
- Borrow Area

Topographic Survey Contours (Feet, NAVD88)

- (survey data provided by client)
- 5- Contour interval is 5 feet
- Contour interval is 1 foot

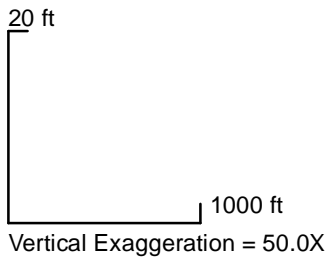
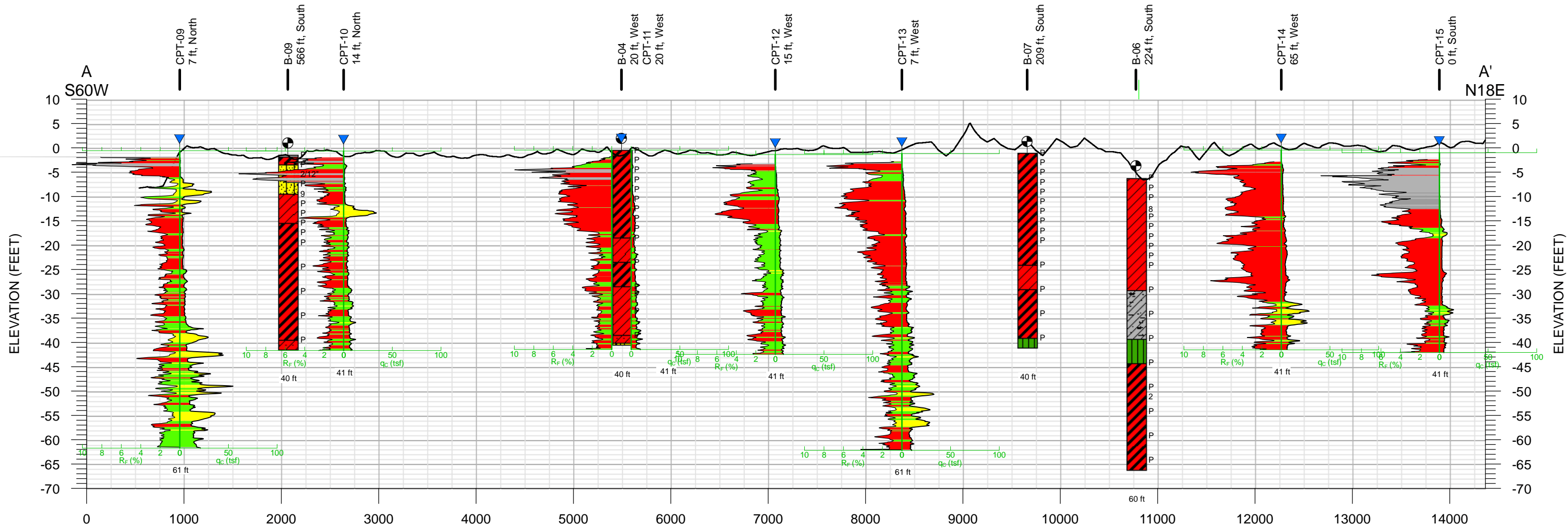


SITE LAYOUT AND EXPLORATION PLAN
Bayou Decade Marsh Creation
and Ridge Restoration
Terrebonne Parish, Louisiana

Source: Esri, DigitalGlobe, GeoEye, Earthstar Geographics, CNES/Airbus DS, USDA, USGS, AeroGRID, IGN, and the GIS User Community



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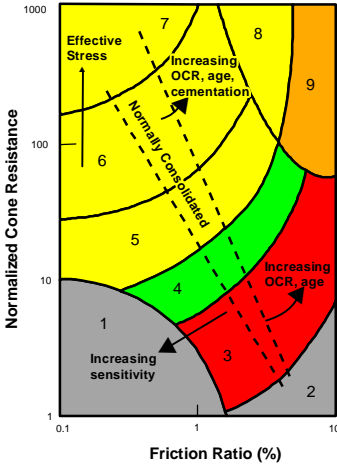


Legend

- Fugro Boring Location
- Fugro CPT
- 13 Field SPT N-Value
- P Push

Soil Descriptions

- High-Plasticity Organic (OH)
- Fat CLAY (CH)
- Peat
- Lean CLAY (CL)
- Sandy Lean Clay (CL)
- Silt (ML)
- Silty SAND (SM)

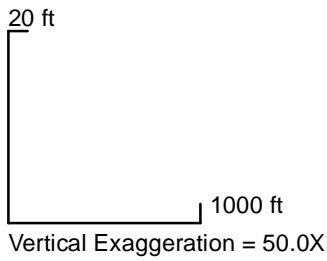
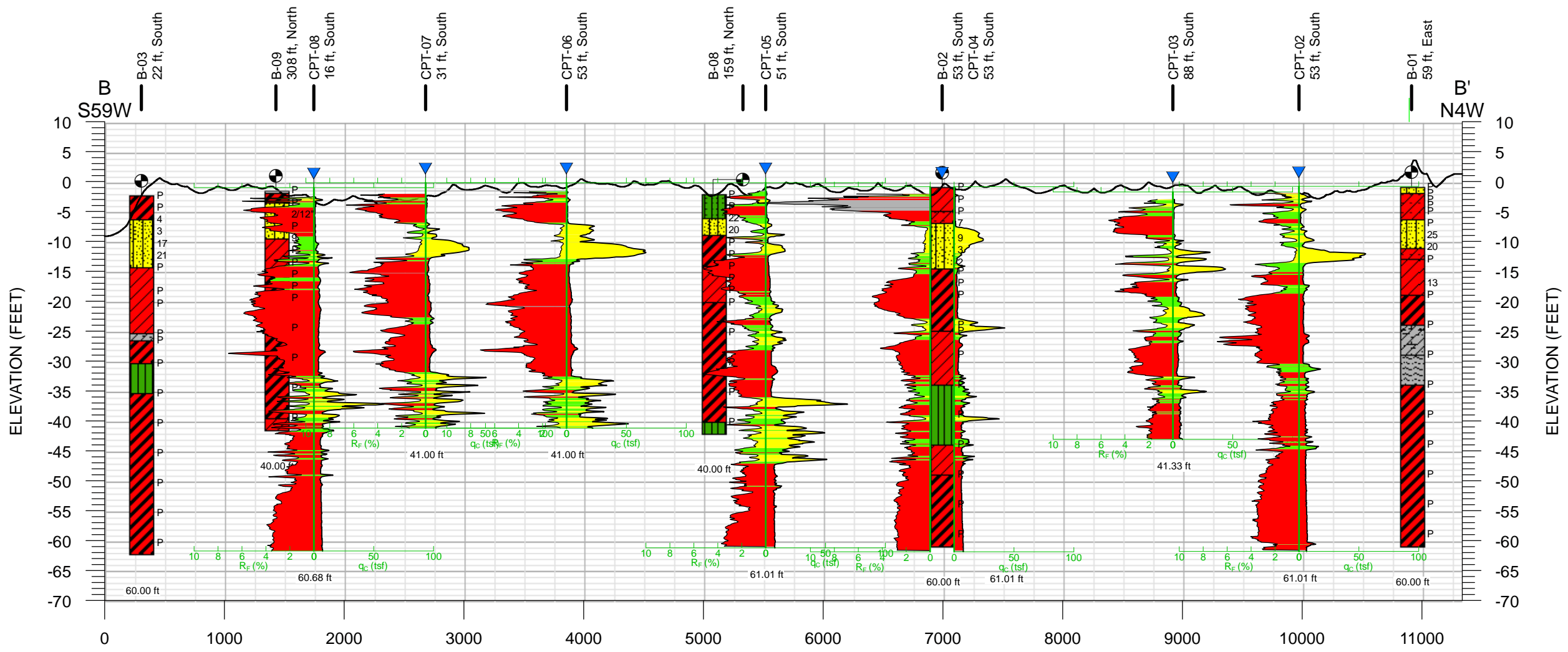


| Zone | Soil Behavior Type | U.S.C.S. |
|------|---------------------------|----------|
| 1 | Sensitive Fine-grained | OL-CH |
| 2 | Organic Material | OL-OH |
| 3 | Clay to Silty Clay | CL-CH |
| 4 | Clayey Silt to Silty Clay | MH-CL |
| 5 | Silty Sand to Sandy Silt | SM-ML |
| 6 | Sand to Silty Sand | SP-SM |
| 7 | Gravelly Sand to Sand | GP-SP |
| 8 | Sand to Clayey Sand | SP-SC |
| 9 | Very Stiff Fine-grained* | CH-CL |

*overconsolidated or cemented

**SBT CORRELATION CHART
ROBERTSON, 1990**

SUBSURFACE PROFILE A-A'
Bayou Decade Marsh Creation
and Ridge Restoration
Terrebonne Parish, Louisiana

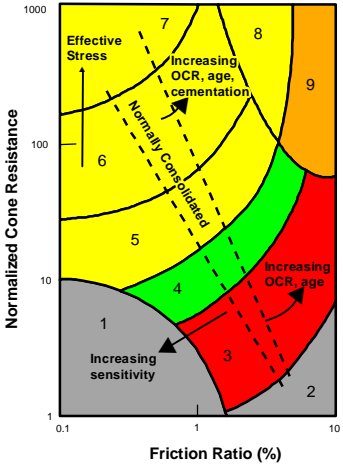


Legend

- Fugro Boring Location
- Fugro CPT
- 13 Field SPT N-Value
- P Push

Soil Descriptions

- High-Plasticity Organic (OH)
- Fat CLAY (CH)
- Peat
- Silt (ML)
- Lean CLAY (CL)
- Silty SAND (SM)
- Sandy Lean Clay (CL)



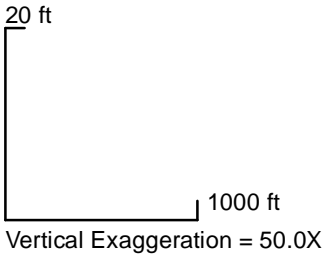
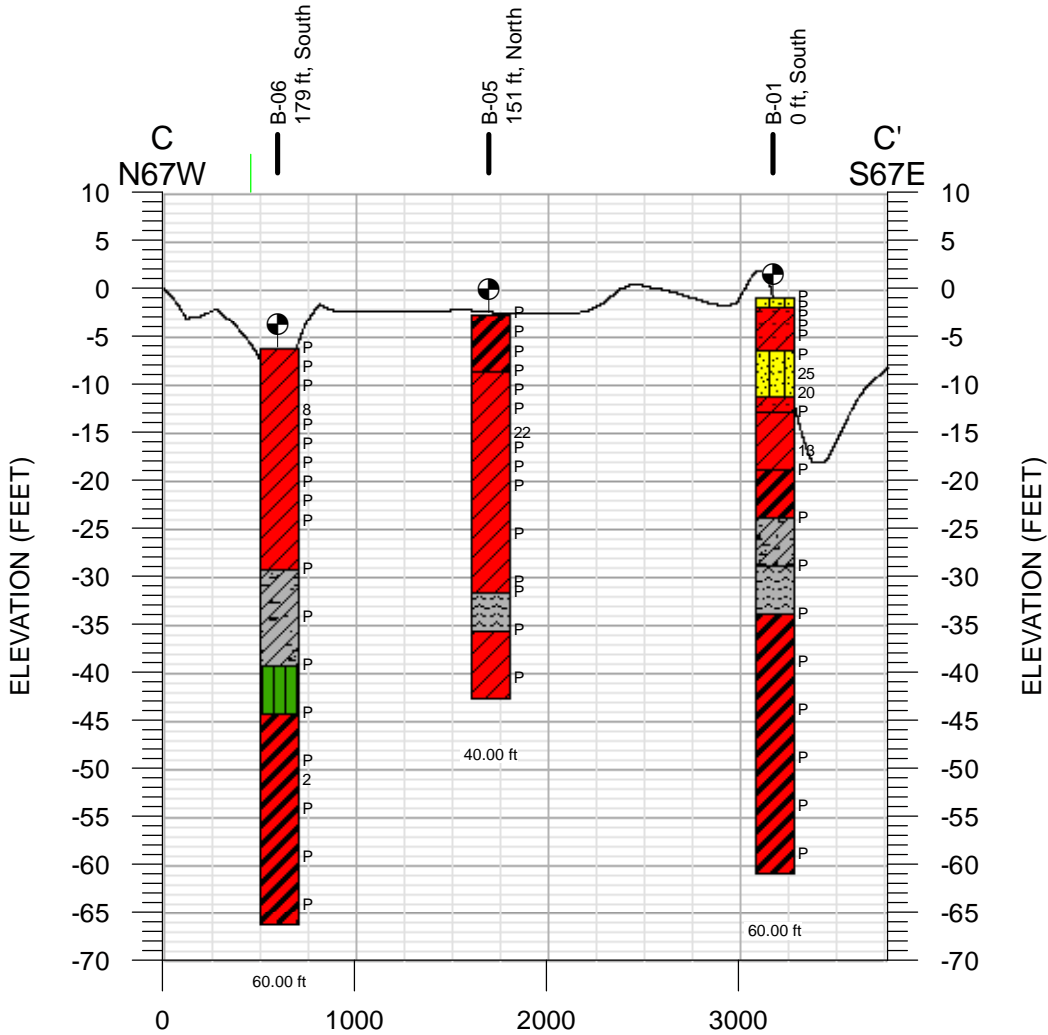
| Zone | Soil Behavior Type | U.S.C.S. |
|------|---------------------------|----------|
| 1 | Sensitive Fine-grained | OL-CH |
| 2 | Organic Material | OL-OH |
| 3 | Clay to Silty Clay | CL-CH |
| 4 | Clayey Silt to Silty Clay | MH-CL |
| 5 | Silty Sand to Sandy Silt | SM-ML |
| 6 | Sand to Silty Sand | SP-SM |
| 7 | Gravelly Sand to Sand | GP-SP |
| 8 | Sand to Clayey Sand | SP-SC |
| 9 | Very Stiff Fine-grained* | CH-CL |

*overconsolidated or cemented

**SBT CORRELATION CHART
ROBERTSON, 1990**

SUBSURFACE PROFILE B-B'
Bayou Decade Marsh Creation
and Ridge Restoration
Terrebonne Parish, Louisiana

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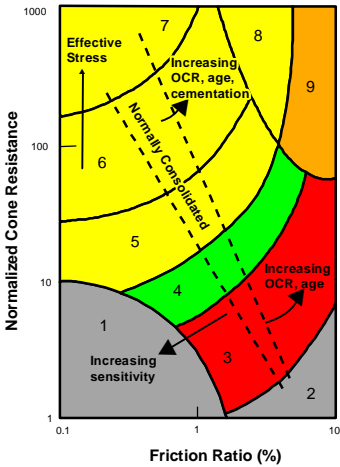


Legend

- Fugro Boring Location
- Fugro CPT
- 13 Field SPT N-Value
- P Push

Soil Descriptions

- High-Plasticity Organic (OH)
- Fat CLAY (CH)
- Peat
- Silt (ML)
- Lean CLAY (CL)
- Silty SAND (SM)
- Sandy Lean Clay (CL)

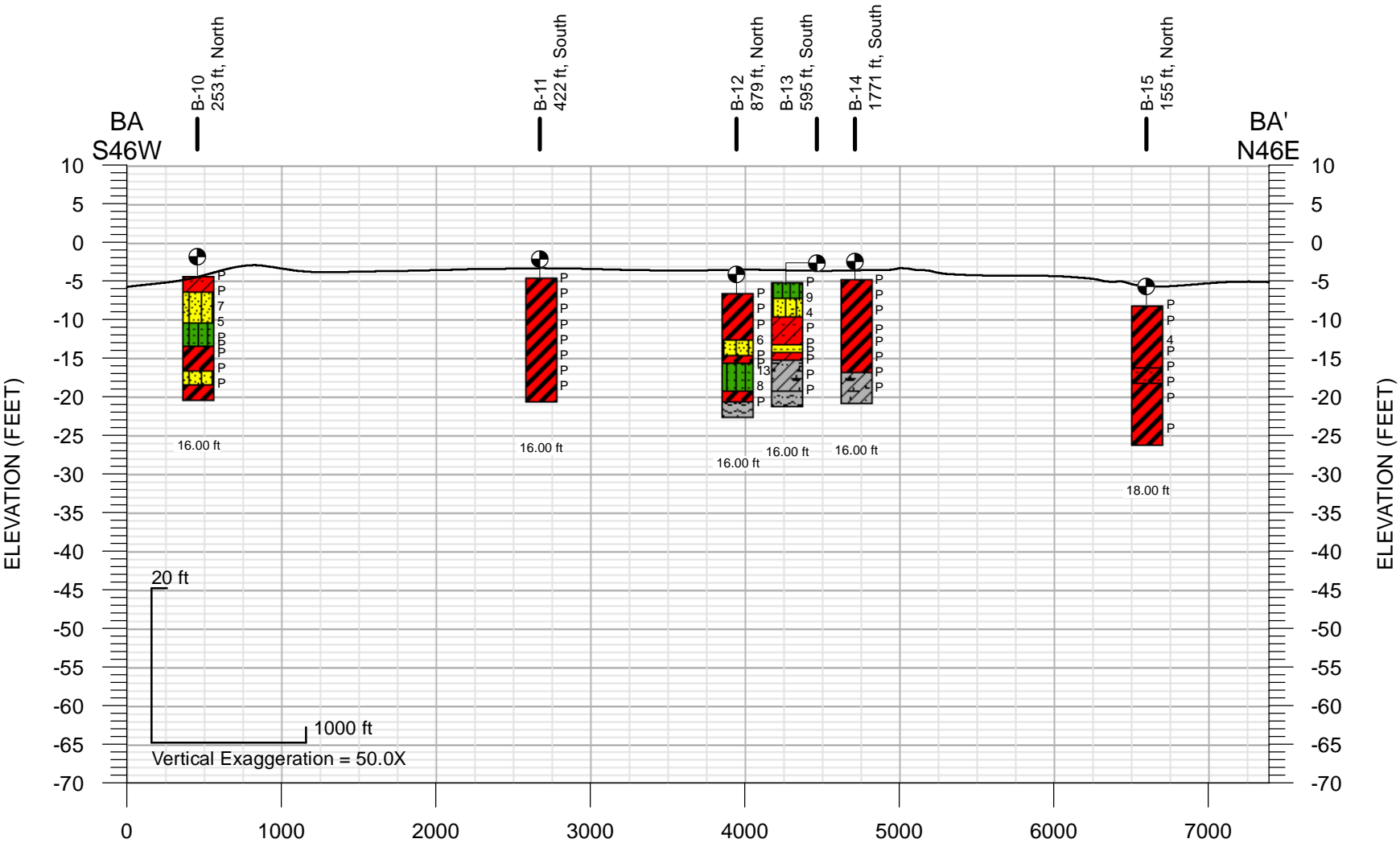


| Zone | Soil Behavior Type | U.S.C.S. |
|------|---------------------------|----------|
| 1 | Sensitive Fine-grained | OL-CH |
| 2 | Organic Material | OL-OH |
| 3 | Clay to Silty Clay | CL-CH |
| 4 | Clayey Silt to Silty Clay | MH-CL |
| 5 | Silty Sand to Sandy Silt | SM-ML |
| 6 | Sand to Silty Sand | SP-SM |
| 7 | Gravelly Sand to Sand | GP-SP |
| 8 | Sand to Clayey Sand | SP-SC |
| 9 | Very Stiff Fine-grained* | CH-CL |

*overconsolidated or cemented

SBT CORRELATION CHART
ROBERTSON, 1990

SUBSURFACE PROFILE C-C'
Bayou Decade Marsh Creation
and Ridge Restoration
Terrebonne Parish, Louisiana

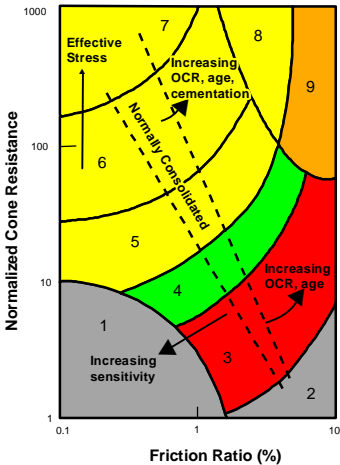


Legend

- Fugro Boring Location
- Fugro CPT
- Field SPT N-Value
- Push

Soil Descriptions

- High-Plasticity Organic (OH)
- Fat CLAY (CH)
- Peat
- Silt (ML)
- Lean CLAY (CL)
- Silty SAND (SM)
- Sandy Lean Clay (CL)



| Zone | Soil Behavior Type | U.S.C.S. |
|------|---------------------------|----------|
| 1 | Sensitive Fine-grained | OL-CH |
| 2 | Organic Material | OL-OH |
| 3 | Clay to Silty Clay | CL-CH |
| 4 | Clayey Silt to Silty Clay | MH-CL |
| 5 | Silty Sand to Sandy Silt | SM-ML |
| 6 | Sand to Silty Sand | SP-SM |
| 7 | Gravelly Sand to Sand | GP-SP |
| 8 | Sand to Clayey Sand | SP-SC |
| 9 | Very Stiff Fine-grained* | CH-CL |

*overconsolidated or cemented

SBT CORRELATION CHART
ROBERTSON, 1990

SUBSURFACE PROFILE Borrow Area A
Bayou Decade Marsh Creation
and Ridge Restoration
Terrebonne Parish, Louisiana



APPENDIX A

FIELD EXPLORATION

APPENDIX A - FIELD EXPLORATION

INTRODUCTION

This appendix provides information about field exploration, including drilling equipment and soil sampling methods. Field exploration was performed between March 26 and April 20, 2018.

Fugro performed 15 cone penetration test (CPT) soundings ranging in depth from 40 ft to 60 ft and 15 borings ranging in depth from 16 ft to 60 ft.

Table A-1 summarizes exploration locations, depths, ground surface elevations, and other information. Explorations are approximately located as shown on Plate 2. Explorations were located prior to commencement of the field exploration program.

As-drilled exploration locations and ground surface/mudline elevations were surveyed by Fugro's survey group.

FIELD COORDINATION

Exploration locations were cleared through Louisiana One Call. Apache Louisiana Minerals LLC (2017) provided access permission for Fugro exploration. Land owners were contacted prior to site mobilization, as necessary. The U.S. Army Corps of Engineers and U.S. Coast Guard were notified regarding field exploration.

Prior to drilling or CPT work, exploration locations were surveyed using a magnetometer assess the potential presence of pipelines or other magnetic-susceptible obstructions. A closed loop path was surveyed around each exploration location using a Geometrics 858 cesium vapor magnetometer. The loop path enclosed the exploration location and maintained a minimum 25-ft radius or a 25- by 25-foot rectangular cleared area. Cleared locations were marked with a cane pole or buoy with specific flagging.

Table A-1. Exploration Summary

| Exploration ID | LA State Plane South (NAD83) | | NAD83 Geographic | | Elevation (NAVD88) | Completion | | Depth to Mudline | Water Elevation |
|----------------|------------------------------|-----------|------------------|------------|--------------------|------------|-------|------------------|-----------------|
| | Easting | Northing | Latitude | Longitude | | Date | Depth | | |
| | ft | ft | deg | deg | | | ft | ft | ft |
| B-01 | 3,417,117.4 | 320,359.7 | 29.380211 | -90.905437 | -0.8 | 3/27/2018 | 60.0 | 1.3 | 0.5 |
| B-02 | 3,414,045.8 | 317,944.2 | 29.373600 | -90.915109 | -0.9 | 3/27/2018 | 60.0 | 2.2 | 1.3 |
| B-03 | 3,408,578.8 | 314,205.9 | 29.363374 | -90.932314 | -2.2 | 4/3/2018 | 60.0 | 3.2 | 1.0 |
| B-04 | 3,411,307.2 | 318,072.7 | 29.373980 | -90.923705 | -0.5 | 4/3/2018 | 40.0 | 1.4 | 0.9 |
| B-05 | 3,415,819.4 | 321,086.2 | 29.382222 | -90.909504 | -2.5 | 3/28/2018 | 40.0 | 3.0 | 0.5 |
| B-06 | 3,414,677.7 | 321,220.9 | 29.382604 | -90.913087 | -6.1 | 3/30/2018 | 60.0 | 7.0 | 0.9 |
| B-07 | 3,413,518.7 | 321,109.8 | 29.382310 | -90.916728 | -1.0 | 3/30/2018 | 40.0 | 1.9 | 0.9 |
| B-08 | 3,412,577.1 | 317,193.9 | 29.371551 | -90.919729 | -2.0 | 4/4/2018 | 40.0 | 2.5 | 0.5 |
| B-09 | 3,409,394.7 | 315,092.6 | 29.365804 | -90.929743 | -1.4 | 3/30/2018 | 40.0 | 2.0 | 0.6 |
| B-10 | 3,421,152.1 | 321,135.3 | 29.382302 | -90.892760 | -4.3 | 4/2/2018 | 16.0 | 6.0 | 1.7 |
| B-11 | 3,423,210.3 | 322,200.4 | 29.385209 | -90.886285 | -4.6 | 4/2/2018 | 16.0 | 6.0 | 1.4 |
| B-12 | 3,423,211.8 | 324,020.3 | 29.390213 | -90.886258 | -6.6 | 4/2/2018 | 16.0 | 8.0 | 1.4 |
| B-13 | 3,424,613.2 | 323,327.9 | 29.388294 | -90.881866 | -5.1 | 4/2/2018 | 16.0 | 6.5 | 1.4 |
| B-14 | 3,425,611.5 | 322,658.2 | 29.386442 | -90.878740 | -4.8 | 3/28/2018 | 16.0 | 6.5 | 1.7 |
| B-15 | 3,425,616.9 | 325,355.7 | 29.393859 | -90.878689 | -8.1 | 3/28/2018 | 18.0 | 9.0 | 0.9 |
| CPT-01 | 3,416,845.3 | 321,940.5 | 29.384561 | -90.906273 | -0.4 | 4/17/2018 | 40.0 | 1.0 | 0.6 |
| CPT-02 | 3,416,442.3 | 319,696.0 | 29.378393 | -90.907565 | -0.8 | 4/17/2018 | 60.0 | 1.5 | 0.7 |
| CPT-03 | 3,415,653.1 | 318,995.7 | 29.376475 | -90.910051 | -1.7 | 4/17/2018 | 40.0 | 2.0 | 0.3 |
| CPT-04 | 3,414,045.8 | 317,944.2 | 29.373600 | -90.915109 | -0.9 | 4/17/2018 | 60.0 | 2.2 | 1.3 |
| CPT-05 | 3,412,839.2 | 317,087.7 | 29.371257 | -90.918907 | -0.2 | 4/18/2018 | 60.0 | 1.0 | 0.8 |
| CPT-06 | 3,411,478.9 | 316,169.4 | 29.368745 | -90.923188 | -0.2 | 4/18/2018 | 40.0 | 1.0 | 0.8 |
| CPT-07 | 3,410,663.9 | 315,321.4 | 29.366421 | -90.925756 | -0.2 | 4/18/2018 | 40.0 | 1.0 | 0.8 |
| CPT-08 | 3,409,817.8 | 314,928.9 | 29.365350 | -90.928416 | -1.0 | 4/19/2018 | 60.0 | 1.5 | 0.5 |
| CPT-09 | 3,408,113.2 | 314,913.8 | 29.365325 | -90.933768 | -0.6 | 4/19/2018 | 60.0 | 1.5 | 0.9 |
| CPT-10 | 3,409,442.4 | 315,929.8 | 29.368106 | -90.929584 | -0.7 | 4/19/2018 | 40.0 | 1.5 | 0.8 |
| CPT-11 | 3,411,307.2 | 318,072.7 | 29.373980 | -90.923705 | -0.5 | 4/19/2018 | 40.0 | 1.4 | 0.9 |
| CPT-12 | 3,412,176.9 | 319,390.1 | 29.377594 | -90.920960 | -1.4 | 4/20/2018 | 40.0 | 1.5 | 0.1 |
| CPT-13 | 3,412,670.8 | 320,574.8 | 29.380848 | -90.919396 | -1.2 | 4/20/2018 | 60.0 | 1.5 | 0.3 |
| CPT-14 | 3,415,362.9 | 322,585.6 | 29.386350 | -90.910920 | -0.4 | 4/20/2018 | 40.0 | 1.2 | 0.8 |
| CPT-15 | 3,416,769.5 | 323,055.9 | 29.387629 | -90.906498 | -1.0 | 4/18/2018 | 40.0 | 2.0 | 1.0 |

CONE PENETRATION TEST SOUNDINGS

CPT Logs

CPT logs follow the appendix text, as Plates A-1 to A-15, along with a key for the CPT logs as Plate A-16. CPT logs present tip resistance, friction ratio (friction resistance/tip resistance), general soils type, pore pressure measured near by a transducer behind the cone tip, and interpreted strength properties.

Cone penetration test (CPT) soundings were conducted using an air boat mounted CPT rig. A CPT unit utilizes the self-weight of the equipment to push a cylindrical steel probe into the ground. CPT data is obtained by pushing a series of cylindrical rods, with an instrumented probe at the base, into the soil at a constant rate. The probe consists of a piezocone tip element and a side-friction sleeve element. Continuous measurements of penetration resistance at the cone tip, friction along the friction sleeve, and pore water pressure were recorded during the penetration tests. During testing, the results were saved electronically for further data reduction in our office.

CPT Hole Completion

CPTs were backfilled upon completion with cement-bentonite grout, using a tremie pipe and topped off at the surface.

BORINGS

Boring Logs

Boring logs are presented as Plates A-17 to A-32, with a key to terms and symbols presented as Plates A-32a and 32b. Boring logs present boring number, coordinates, ground surface/mudline elevation, completion date, logger's name, drilling method, drill rig type, backfill method, material descriptions, sampling method, and point-depth related laboratory test results.

Drilling Methods and Equipment

Borings were drilled with a Robicheaux Air Boat Drill Unit 38 (ABDU-38) drill rig, using wet rotary techniques.

Sampling Equipment and Methods

Cohesive soil samples were generally obtained at a maximum of 5-ft intervals. When sandy/cohesionless materials were encountered, samples were generally obtained at 3-ft-depth intervals for a depth interval of about 10 feet before proceeding with 5-ft-depth intervals. Sampling methods are described in Table A-2.

Table A-2. Sampling Methods

| Sampler Type | Dimensions | Description |
|---------------------------------|-----------------------------|--|
| Thin-wall Tubes | 3-inch-OD, 2-7/8-in-ID | Test procedure in general accordance with ASTM D1587. 30-inch-long, thin-wall tubes are attached to the drill string and hydraulically pushed into the borehole bottom about 24 inches (2 ft). |
| Standard Penetration Test (SPT) | 2-inch-OD, 1-3/8-inch-ID | Test procedure in general accordance with ASTM D1586. SPT split-spoon sampler, attached to drill pipe and lowered to borehole bottom, are driven with a cat head and 140-pound manual hammer attached to the top of the drill rod near the ground surface. |

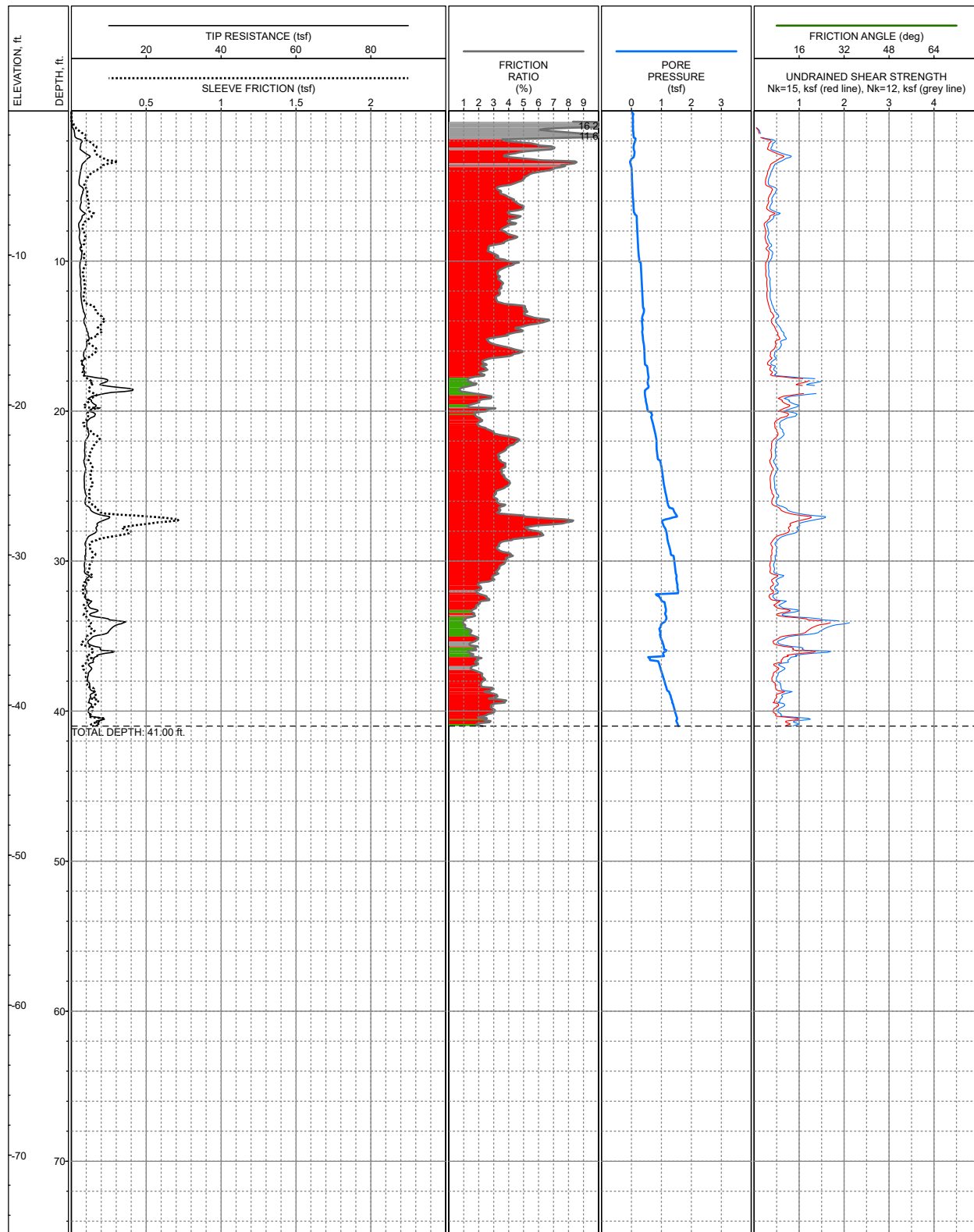
A field technician logged the borings and samples in general accordance with the ASTM D2488 for visual soil classification. Boundaries between soil types shown on the logs are approximate and the transition between different soil layers may be gradational.

Tube samples were extruded in the laboratory with a hydraulic ram. After extrusion, samples were identified according to project number, boring number and depth, then wrapped in aluminum foil and placed in plastic bags to protect against moisture loss.

SPT samples were identified in the same manner as tube samples but were placed in plastic bags in the field and transported to the laboratory. Field SPT blows are recorded as the split-barrel sampler is advanced 18 inches. Blow counts are recorded for three successive 6-inch-depth intervals. Field N-values are calculated by adding the second and third blow count numbers. Field SPT N-values suggest relative density of cohesionless soils and relative consistency of cohesive soils.

Borehole Completion

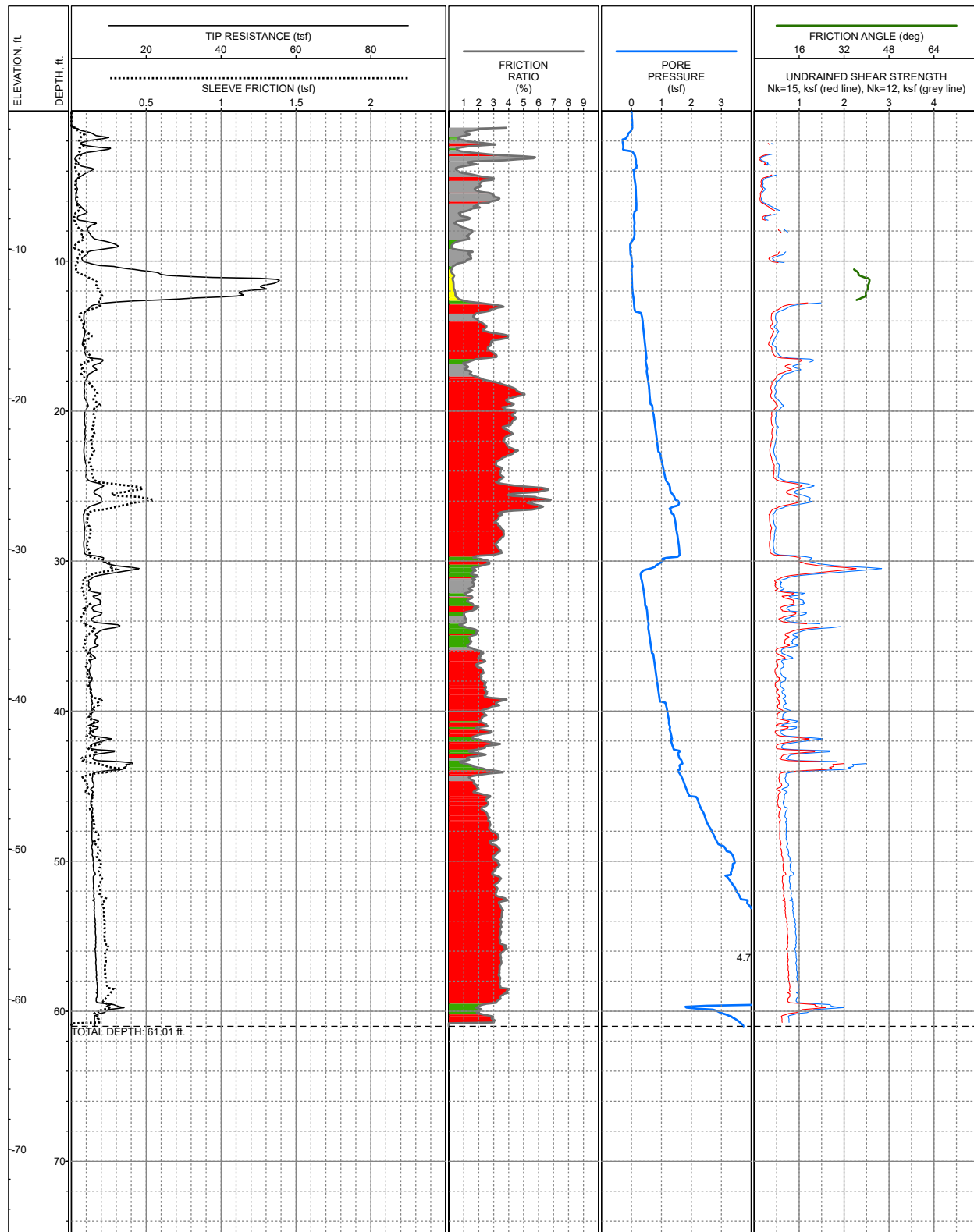
Borings were backfilled upon completion with cement-bentonite grout using a tremie and topped off at the surface. Cuttings were spread out as the site.



LOCATION: E: 3,416,845, N: 321,941, Louisiana State Plane South, NAD83, Feet
 SURFACE EL: -0.4ft +/- NAVD88
 COMPLETION DEPTH: 41.00ft
 TESTDATE: 4/17/2018

EXPLORATION METHOD: Cone Penetrometer
 PERFORMED BY: Fugro
 REVIEWED BY: S. Bryant
 CONE AREA RATIO: 0.59

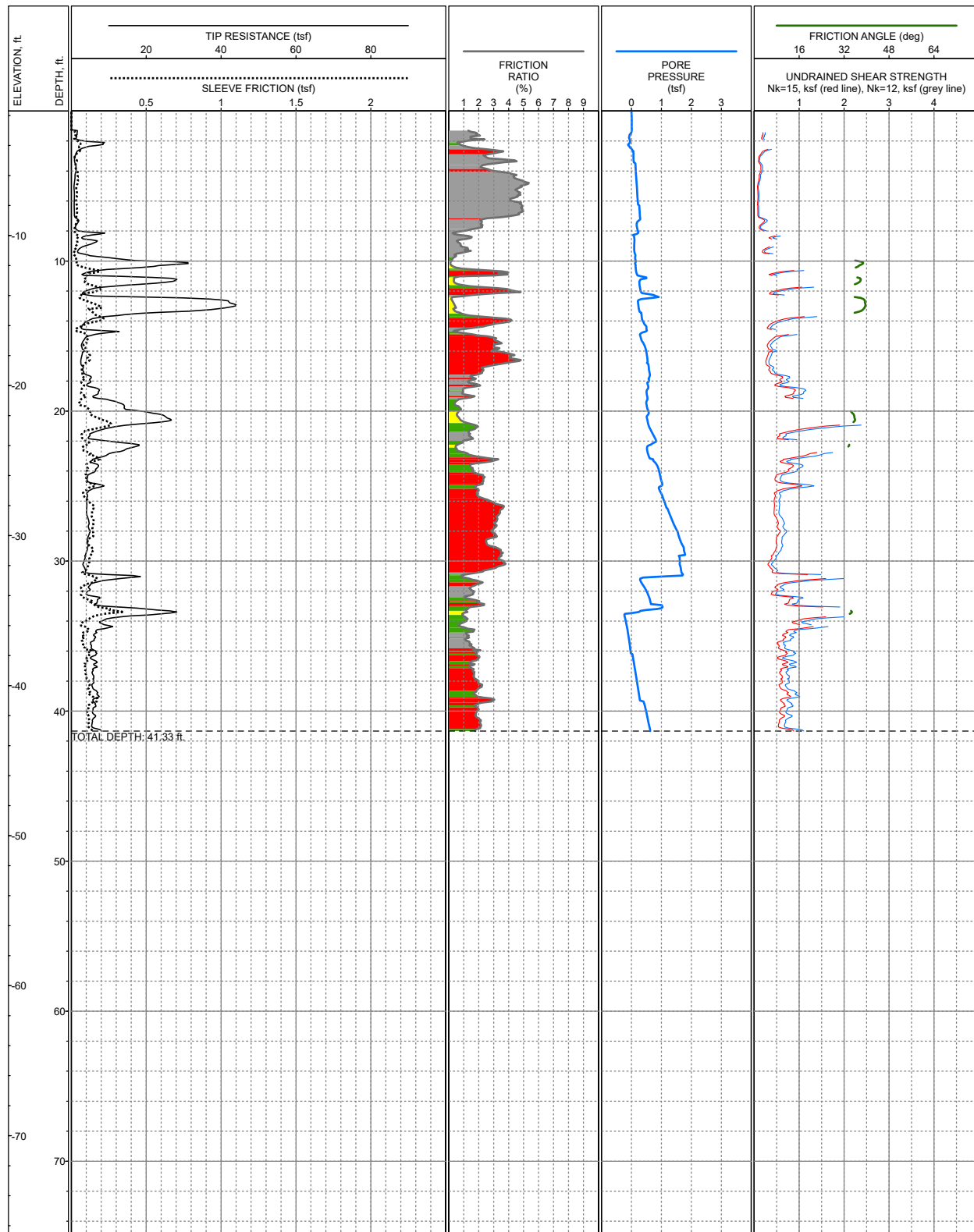
LOG OF: CPT-01
 Bayou Decade Marsh Creation
 and Ridge Restoration
 Terrebonne Parish, Louisiana



LOCATION: E: 3,416,442, N: 319,696, Louisiana State Plane South, NAD83, Feet
 SURFACE EL: -0.8ft +/- NAVD88
 COMPLETION DEPTH: 61.01ft
 TESTDATE: 4/17/2018

EXPLORATION METHOD: Cone Penetrometer
 PERFORMED BY: Fugro
 REVIEWED BY: S. Bryant
 CONE AREA RATIO: 0.59

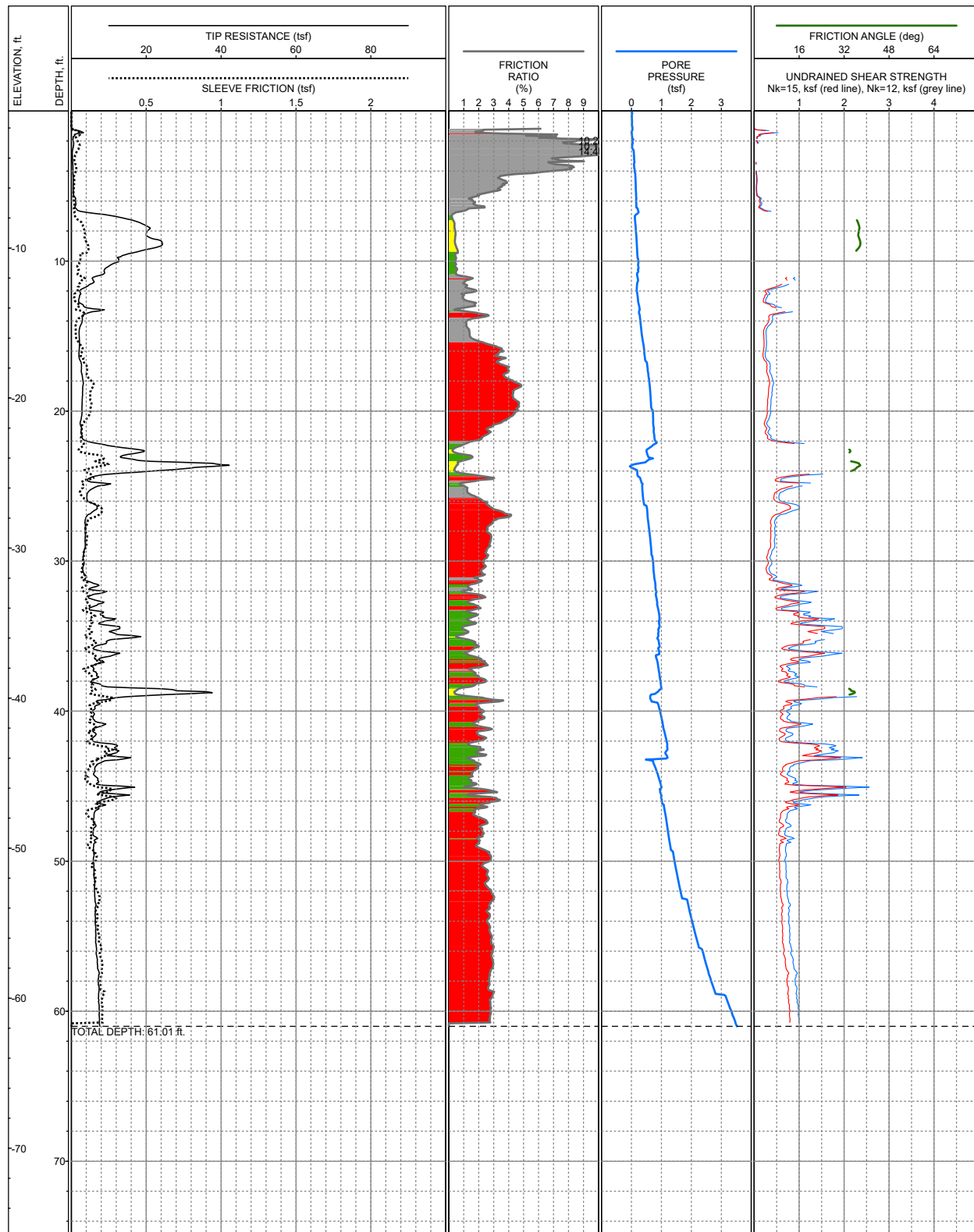
LOG OF: CPT-02
 Bayou Decade Marsh Creation
 and Ridge Restoration
 Terrebonne Parish, Louisiana



LOCATION: E: 3,415,653, N: 318,996, Louisiana State Plane South, NAD83, Feet
 SURFACE EL: -1.7ft +/- NAVD88
 COMPLETION DEPTH: 41.33ft
 TESTDATE: 4/17/2018

EXPLORATION METHOD: Cone Penetrometer
 PERFORMED BY: Fugro
 REVIEWED BY: S. Bryant
 CONE AREA RATIO: 0.59

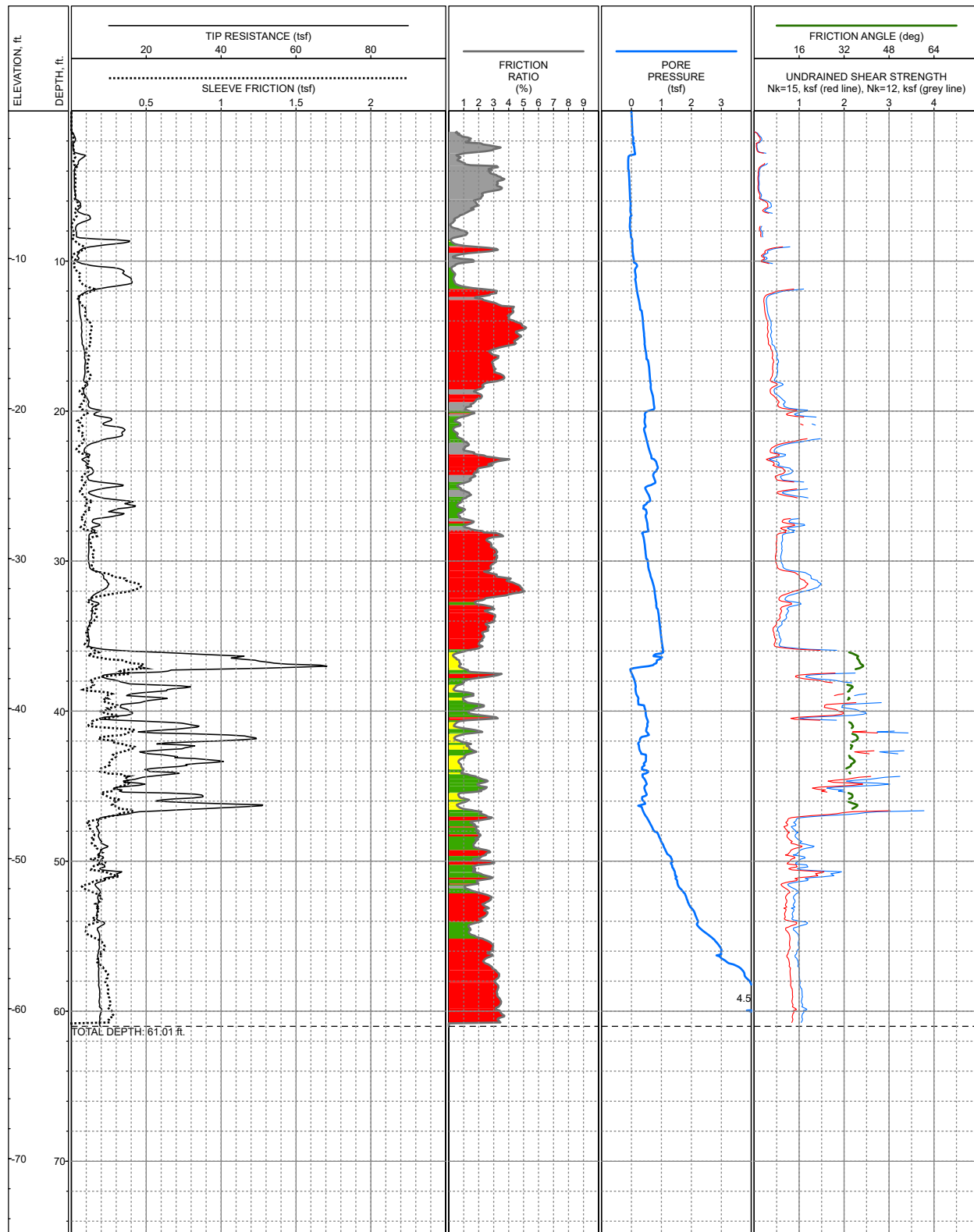
LOG OF: CPT-03
 Bayou Decade Marsh Creation
 and Ridge Restoration
 Terrebonne Parish, Louisiana



LOCATION: E: 3,414,046, N: 317,944, Louisiana State Plane South, NAD83, Feet
 SURFACE EL: -0.9ft +/- NAVD88
 COMPLETION DEPTH: 61.01ft
 TESTDATE: 4/17/2018

EXPLORATION METHOD: Cone Penetrometer
 PERFORMED BY: Fugro
 REVIEWED BY: S. Bryant
 CONE AREA RATIO: 0.59

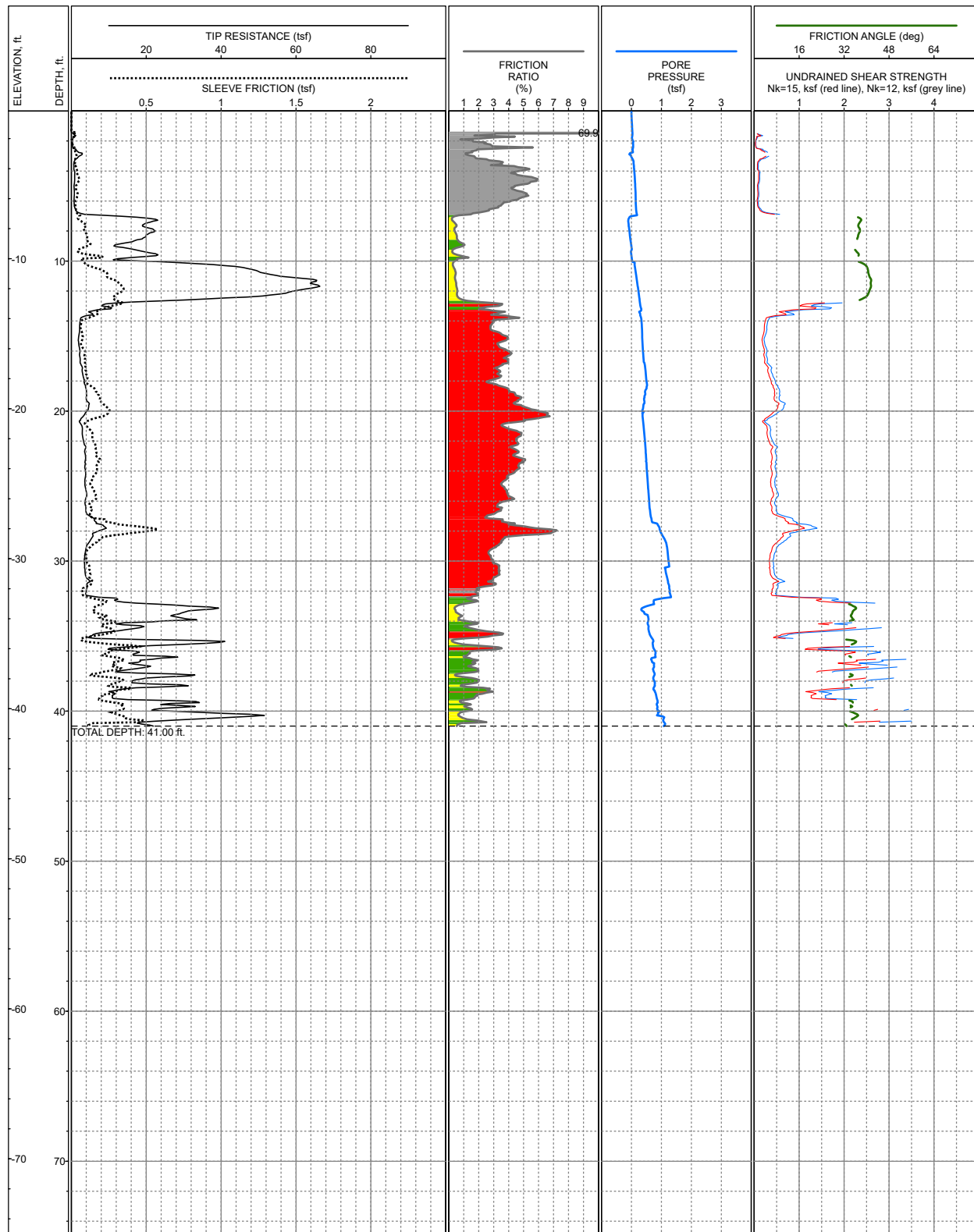
LOG OF: CPT-04
 Bayou Decade Marsh Creation
 and Ridge Restoration
 Terrebonne Parish, Louisiana



LOCATION: E: 3,412,839, N: 317,088, Louisiana State Plane South, NAD83, Feet
 SURFACE EL: -0.2ft +/- NAVD88
 COMPLETION DEPTH: 61.01ft
 TESTDATE: 4/18/2018

EXPLORATION METHOD: Cone Penetrometer
 PERFORMED BY: Fugro
 REVIEWED BY: S. Bryant
 CONE AREA RATIO: 0.59

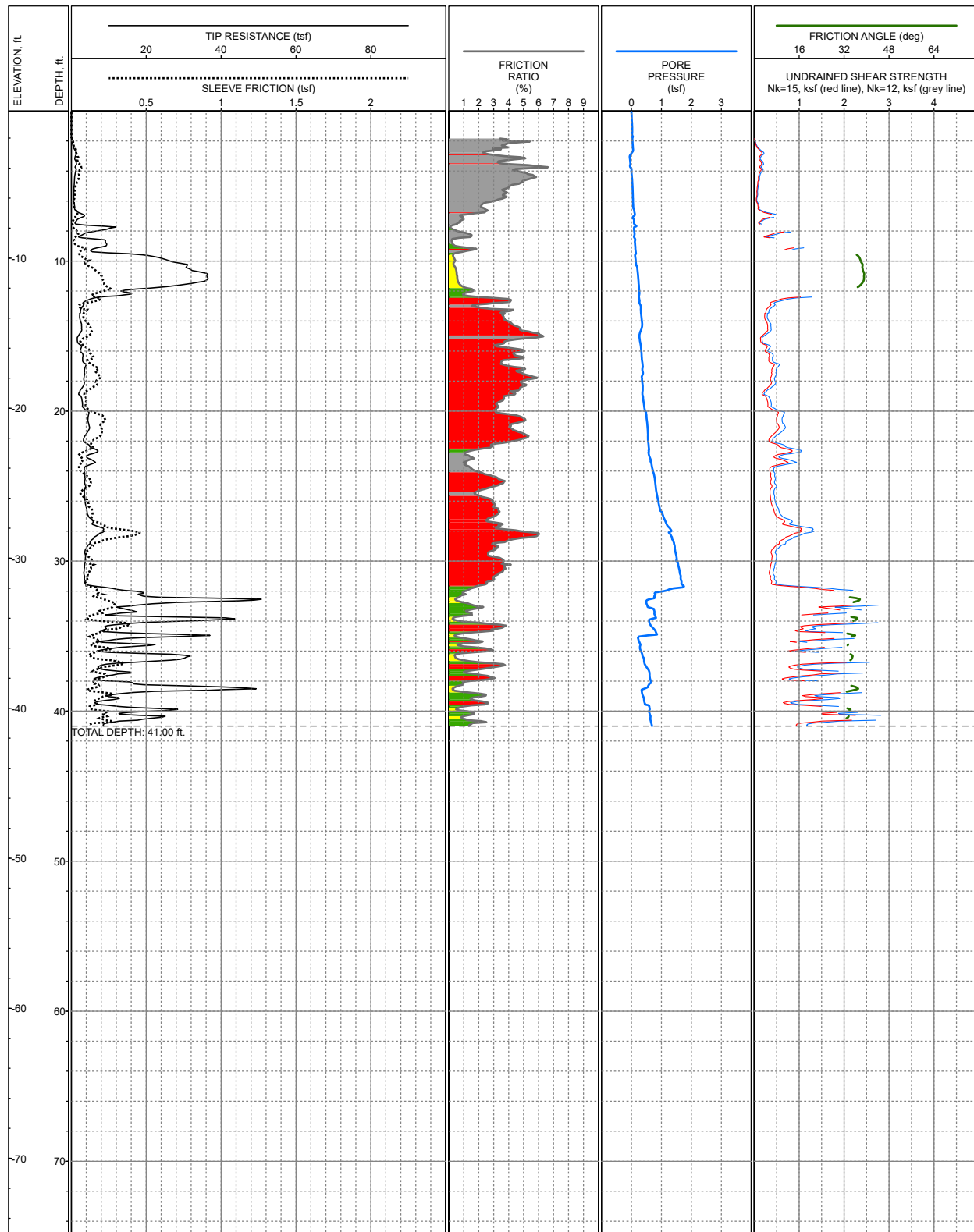
LOG OF: CPT-05
 Bayou Decade Marsh Creation
 and Ridge Restoration
 Terrebonne Parish, Louisiana



LOCATION: E: 3,411,479, N: 316,169, Louisiana State Plane South, NAD83, Feet
 SURFACE EL: -0.2ft +/- NAVD88
 COMPLETION DEPTH: 41.00ft
 TESTDATE: 4/18/2018

EXPLORATION METHOD: Cone Penetrometer
 PERFORMED BY: Fugro
 REVIEWED BY: S. Bryant
 CONE AREA RATIO: 0.59

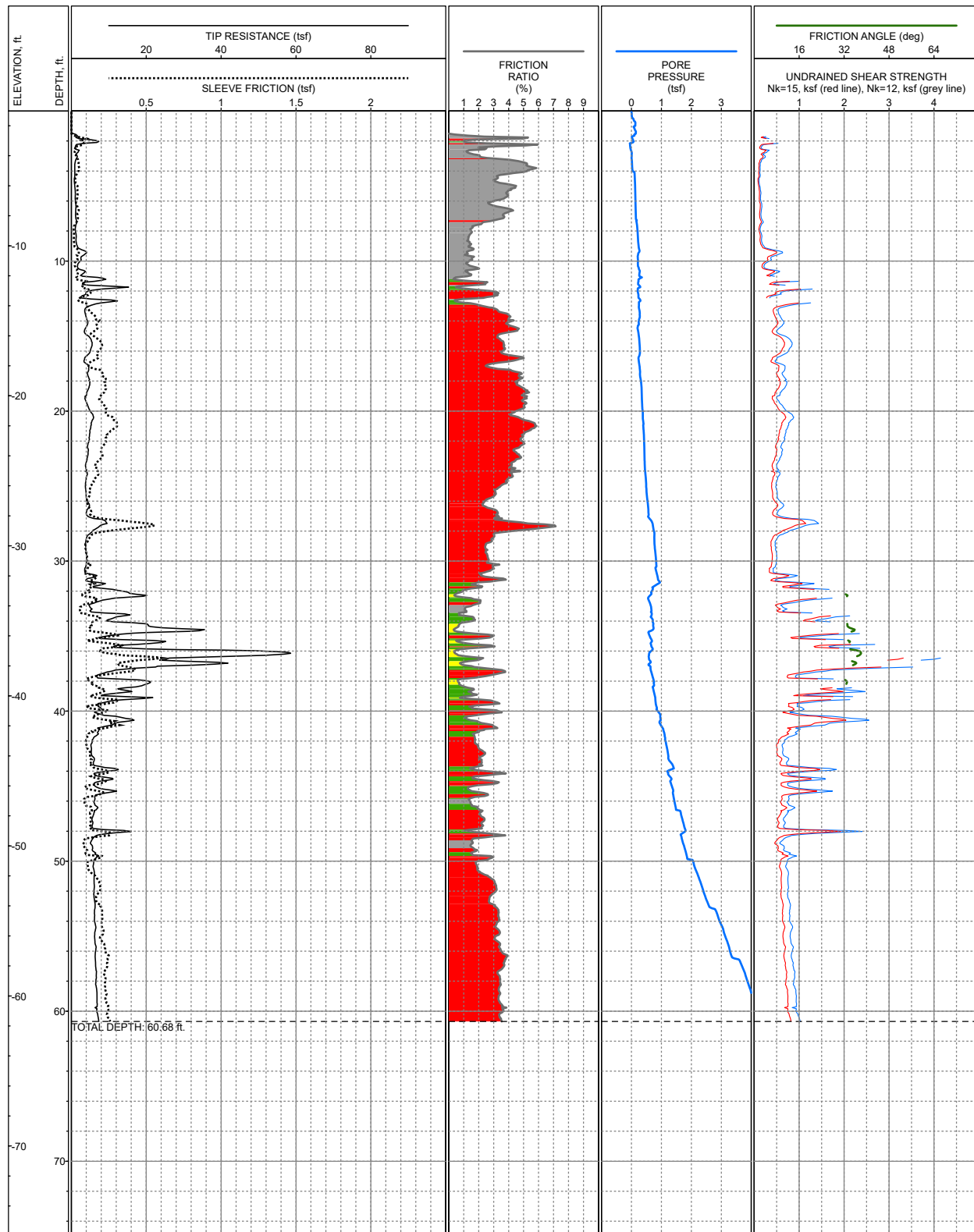
LOG OF: CPT-06
 Bayou Decade Marsh Creation
 and Ridge Restoration
 Terrebonne Parish, Louisiana



LOCATION: E: 3,410,664, N: 315,321, Louisiana State Plane South, NAD83, Feet
 SURFACE EL: -0.2ft +/- NAVD88
 COMPLETION DEPTH: 41.00ft
 TESTDATE: 4/18/2018

EXPLORATION METHOD: Cone Penetrometer
 PERFORMED BY: Fugro
 REVIEWED BY: S. Bryant
 CONE AREA RATIO: 0.59

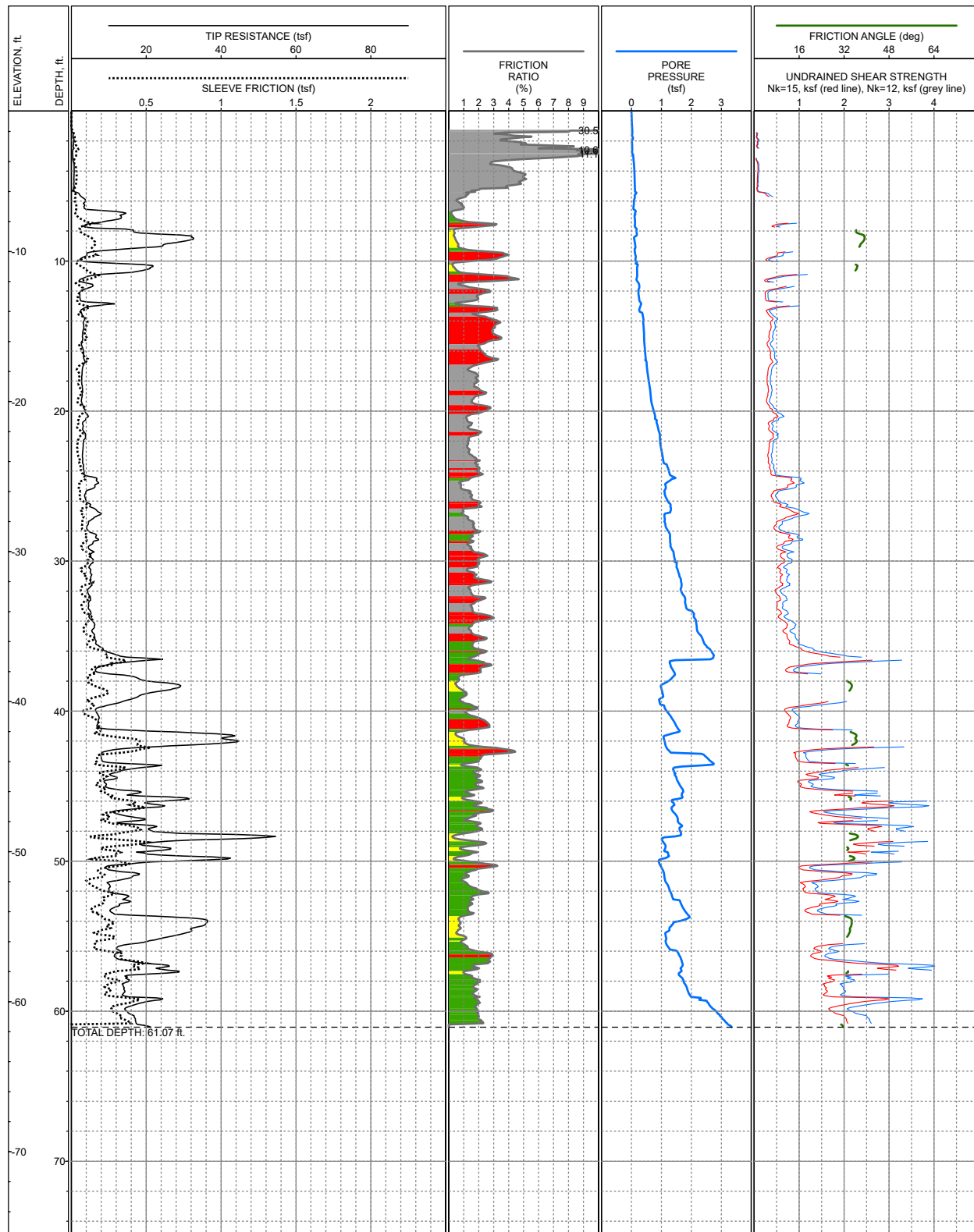
LOG OF: CPT-07
 Bayou Decade Marsh Creation
 and Ridge Restoration
 Terrebonne Parish, Louisiana



LOCATION: E: 3,409,818, N: 314,929, Louisiana State Plane South, NAD83, Feet
SURFACE EL: -1.0ft +/- NAVD88
COMPLETION DEPTH: 60.68ft
TESTDATE: 4/18/2018

EXPLORATION METHOD: Cone Penetrometer
PERFORMED BY: Fugro
REVIEWED BY: S. Bryant
CONE AREA RATIO: 0.59

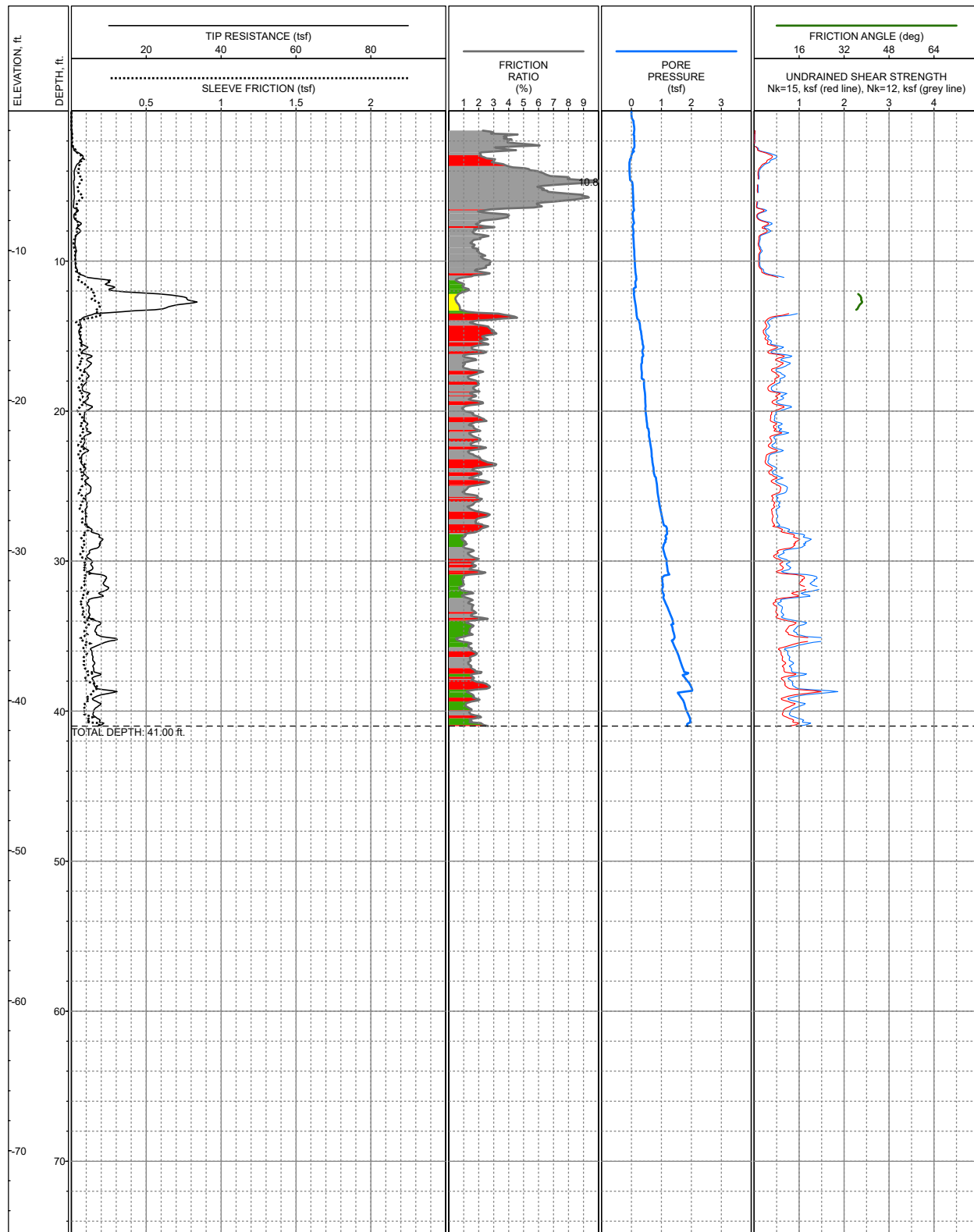
LOG OF: CPT-08
Bayou Decade Marsh Creation
and Ridge Restoration
Terrebonne Parish, Louisiana



LOCATION: E: 3,408,113, N: 314,914, Louisiana State Plane South, NAD83, Feet
 SURFACE EL: -0.6ft +/- NAVD88
 COMPLETION DEPTH: 61.07ft
 TESTDATE: 4/18/2018

EXPLORATION METHOD: Cone Penetrometer
 PERFORMED BY: Fugro
 REVIEWED BY: S. Bryant
 CONE AREA RATIO: 0.59

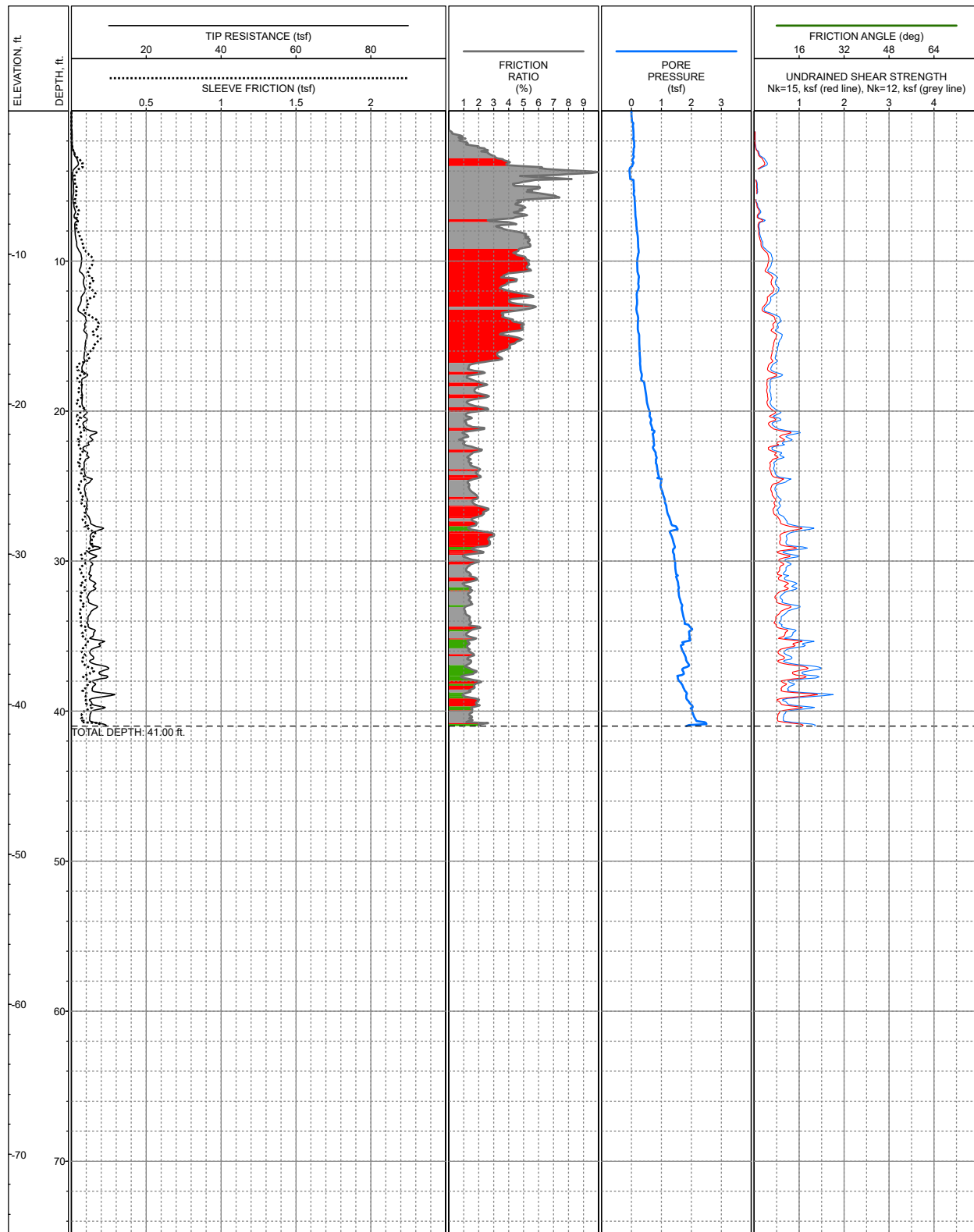
LOG OF: CPT-09
 Bayou Decade Marsh Creation
 and Ridge Restoration
 Terrebonne Parish, Louisiana



LOCATION: E: 3,409,442, N: 315,930, Louisiana State Plane South, NAD83, Feet
 SURFACE EL: -0.7ft +/- NAVD88
 COMPLETION DEPTH: 41.00ft
 TESTDATE: 4/18/2018

EXPLORATION METHOD: Cone Penetrometer
 PERFORMED BY: Fugro
 REVIEWED BY: S. Bryant
 CONE AREA RATIO: 0.59

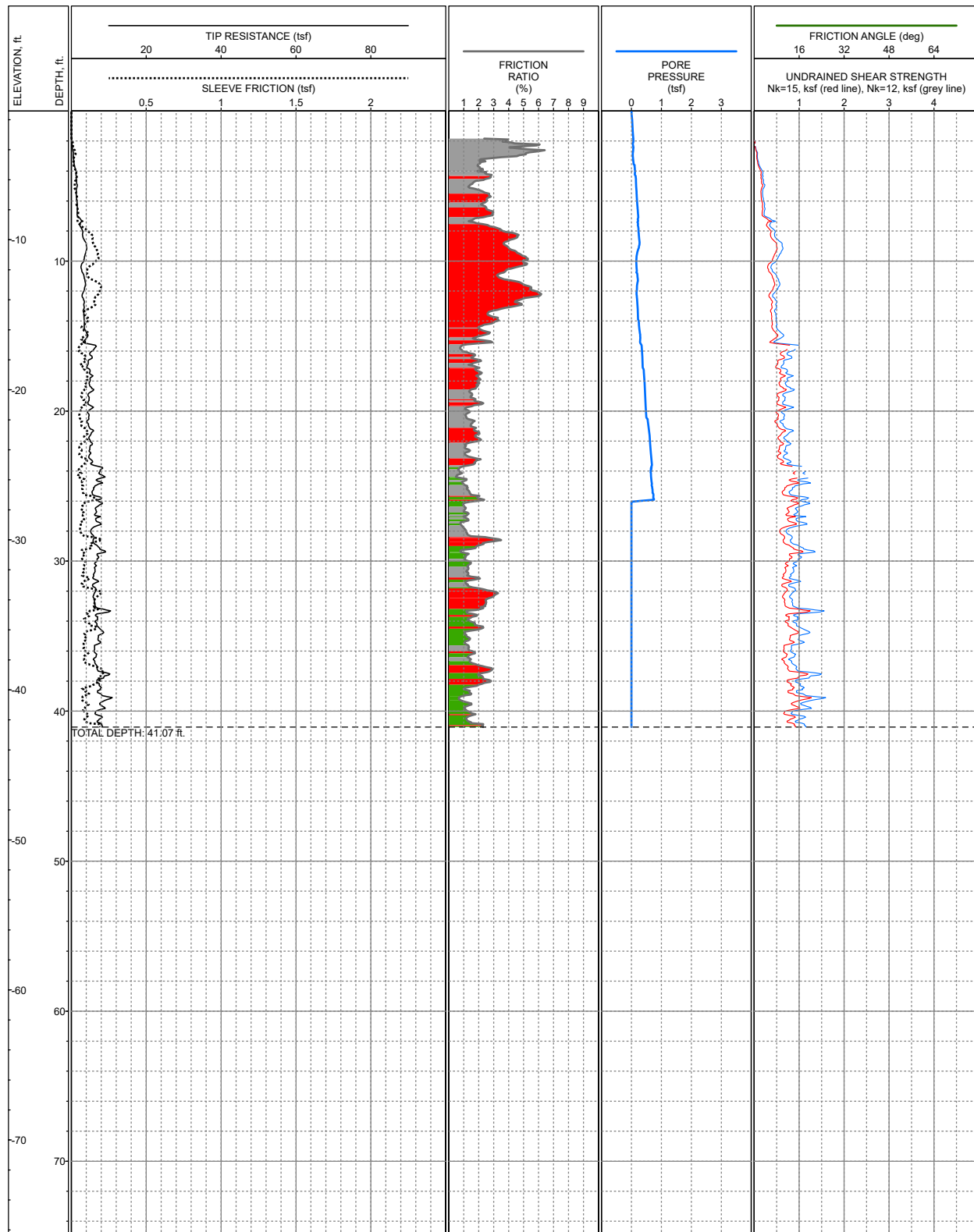
LOG OF: CPT-10
 Bayou Decade Marsh Creation
 and Ridge Restoration
 Terrebonne Parish, Louisiana



LOCATION: E: 3,411,307, N: 318,073, Louisiana State Plane South, NAD83, Feet
 SURFACE EL: -0.5ft +/- NAVD88
 COMPLETION DEPTH: 41.00ft
 TESTDATE: 4/18/2018

EXPLORATION METHOD: Cone Penetrometer
 PERFORMED BY: Fugro
 REVIEWED BY: S. Bryant
 CONE AREA RATIO: 0.59

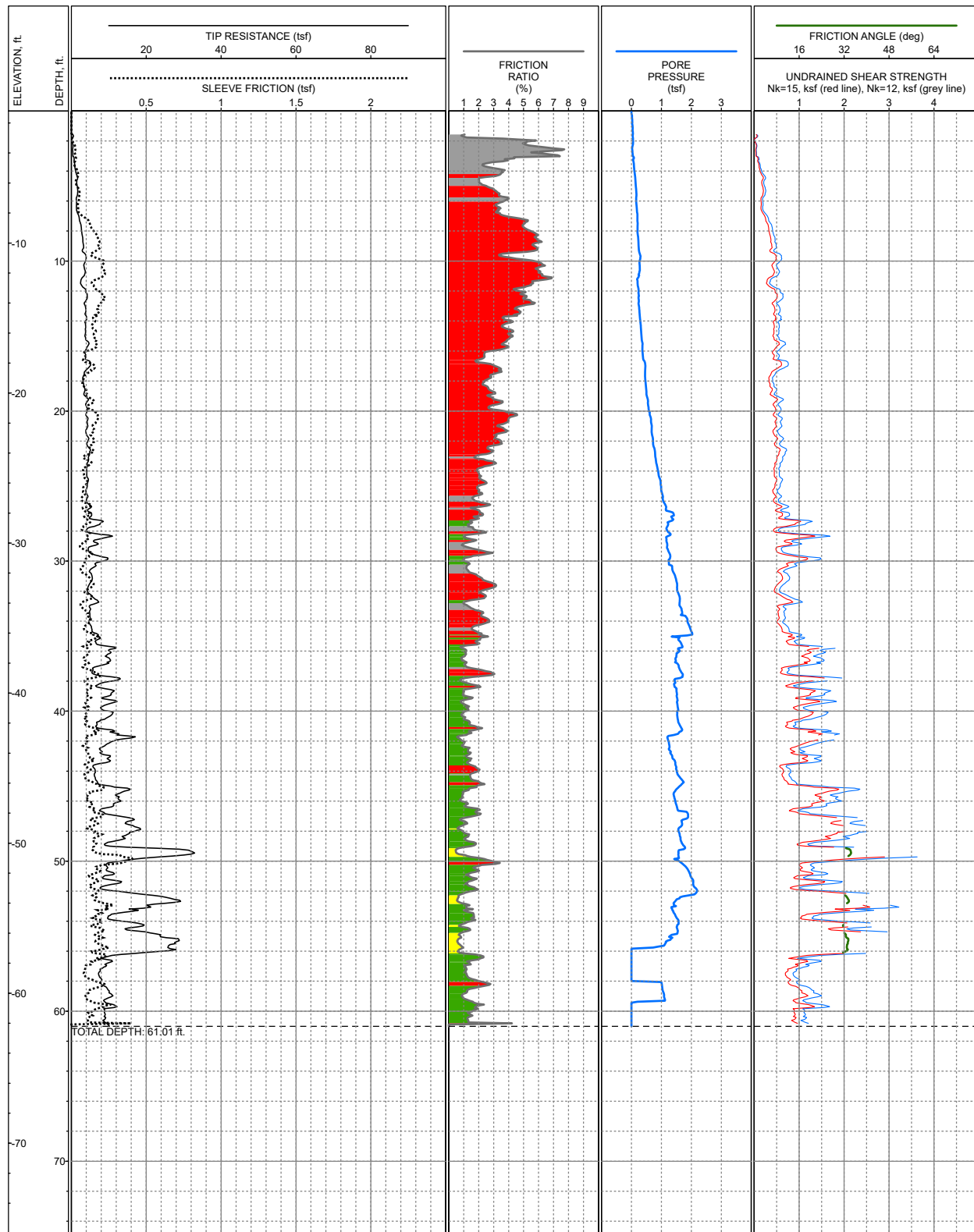
LOG OF: CPT-11
 Bayou Decade Marsh Creation
 and Ridge Restoration
 Terrebonne Parish, Louisiana



LOCATION: E: 3,412,177, N: 319,390, Louisiana State Plane South, NAD83, Feet
 SURFACE EL: -1.4ft +/- NAVD88
 COMPLETION DEPTH: 41.07ft
 TESTDATE: 4/20/2018

EXPLORATION METHOD: Cone Penetrometer
 PERFORMED BY: Fugro
 REVIEWED BY: S. Bryant
 CONE AREA RATIO: 0.59

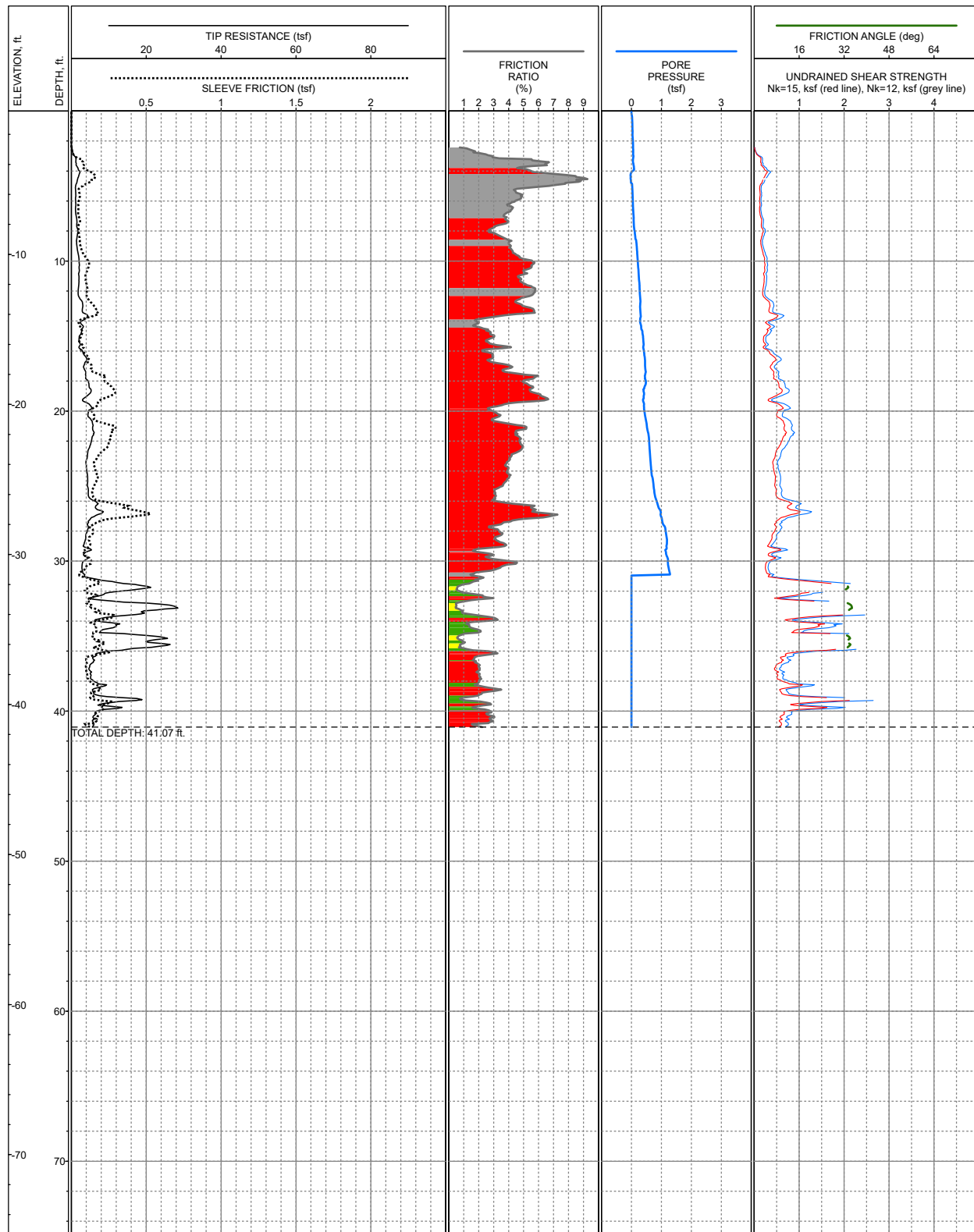
LOG OF: CPT-12
 Bayou Decade Marsh Creation
 and Ridge Restoration
 Terrebonne Parish, Louisiana



LOCATION: E: 3,412,671, N: 320,575, Louisiana State Plane South, NAD83, Feet
 SURFACE EL: -1.2ft +/- NAVD88
 COMPLETION DEPTH: 61.01ft
 TESTDATE: 4/20/2018

EXPLORATION METHOD: Cone Penetrometer
 PERFORMED BY: Fugro
 REVIEWED BY: S. Bryant
 CONE AREA RATIO: 0.59

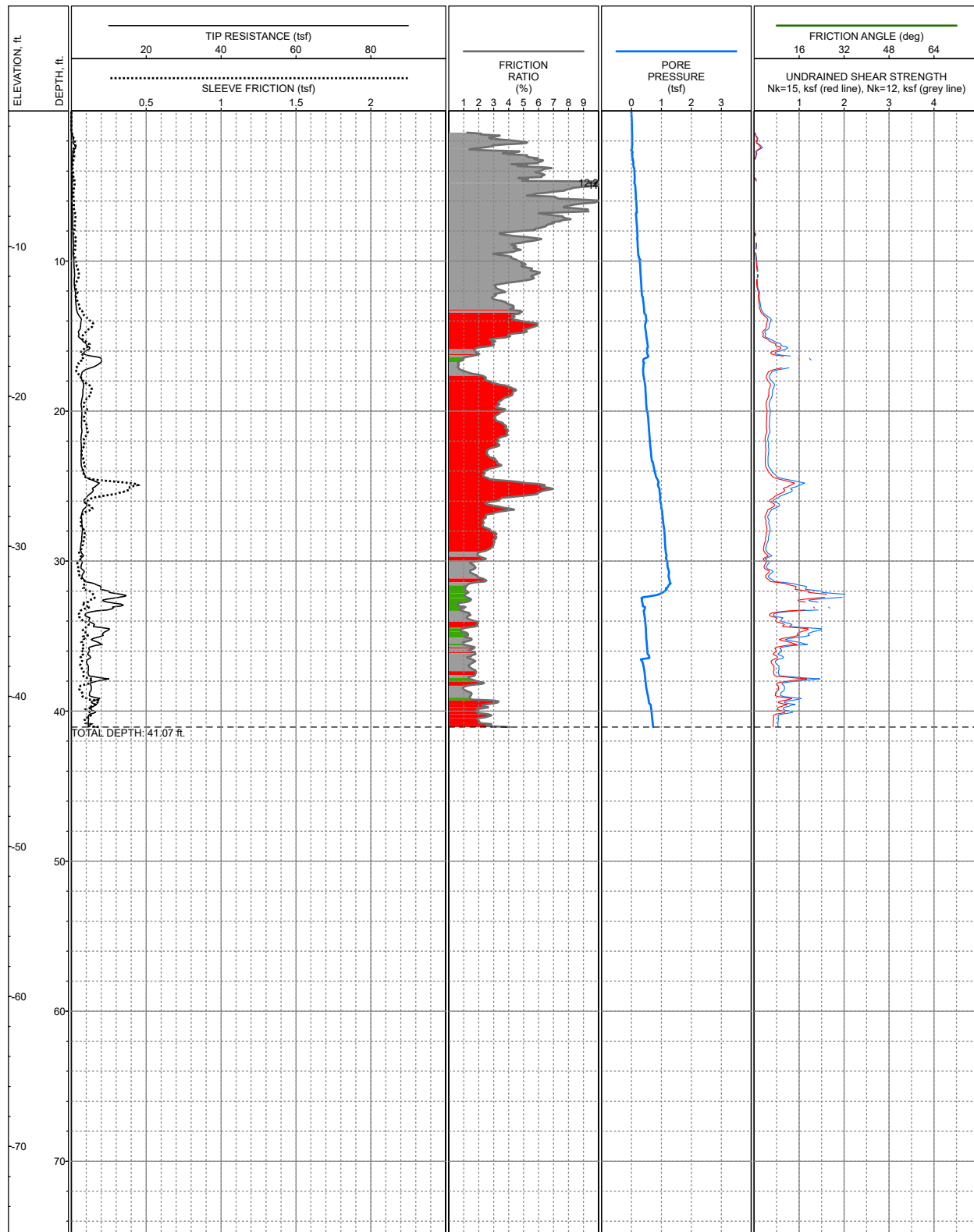
LOG OF: CPT-13
 Bayou Decade Marsh Creation
 and Ridge Restoration
 Terrebonne Parish, Louisiana



LOCATION: E: 3,415,363, N: 322,586, Louisiana State Plane South, NAD83, Feet
 SURFACE EL: -0.4ft +/- NAVD88
 COMPLETION DEPTH: 41.07ft
 TESTDATE: 4/20/2018

EXPLORATION METHOD: Cone Penetrometer
 PERFORMED BY: Fugro
 REVIEWED BY: S. Bryant
 CONE AREA RATIO: 0.59

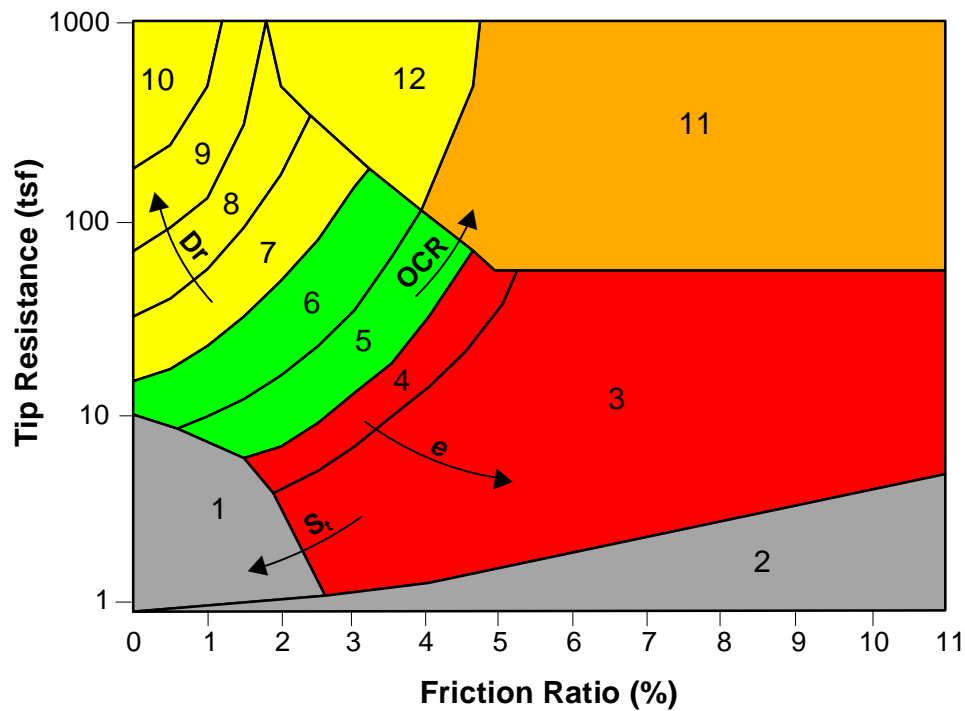
LOG OF: CPT-14
 Bayou Decade Marsh Creation
 and Ridge Restoration
 Terrebonne Parish, Louisiana



LOCATION: E: 3,416,770, N: 323,056, Louisiana State Plane South, NAD83, Feet
 SURFACE EL: -1.0ft +/- NAVD88
 COMPLETION DEPTH: 41.07ft
 TESTDATE: 4/18/2018

EXPLORATION METHOD: Cone Penetrometer
 PERFORMED BY: Fugro
 REVIEWED BY: S. Bryant
 CONE AREA RATIO: 0.59

LOG OF: CPT-15
 Bayou Decade Marsh Creation
 and Ridge Restoration
 Terrebonne Parish, Louisiana



| Zone | Soil Behavior Type | U.S.C.S. |
|------|---------------------------|----------|
| 1 | Sensitive Fine-grained | OL-CH |
| 2 | Organic Material | OL-OH |
| 3 | Clay | CH |
| 4 | Silty Clay to Clay | CL-CH |
| 5 | Clayey Silt to Silty Clay | MH-CL |
| 6 | Sandy Silt to Clayey Silt | ML-MH |
| 7 | Silty Sand to Sandy Silt | SM-ML |
| 8 | Sand to Silty Sand | SM-SP |
| 9 | Sand | SW-SP |
| 10 | Gravelly Sand to Sand | SW-GW |
| 11 | Very Stiff Fine-grained * | CH-CL |
| 12 | Sand to Clayey Sand * | SC-SM |

*overconsolidated or cemented

SBT CORRELATION CHART
(Robertson and Campanella, 1988)

KEY TO CPT LOGS
Bayou Decade Marsh Creation
and Ridge Restoration
Terrebonne Parish, Louisiana

| DEPTH, FT | WATER LEVEL | SYMBOL SAMPLES | BLOWS PER FOOT | LOCATION: See Plate 1 COORDINATES: N 29° 22' 48.77" W 90° 54' 19.56" SURFACE EL.: -0.8' | STRATUM DEPTH, FT | CLASSIFICATION | | | | | | SHEAR STRENGTH | | | | |
|-----------|-------------|----------------|----------------|---|-------------------|------------------|--------------------------|------------------|--------------|---------------|-----------------------|----------------|-----|-----|-----|-----|
| | | | | STRATUM DESCRIPTION | | UNIT DRY WT, PCF | PASSING NO. 200 SIEVE, % | WATER CONTENT, % | LIQUID LIMIT | PLASTIC LIMIT | PLASTICITY INDEX (PI) | KIPS PER SQ FT | | | | |
| | | | | | | | | | | | | 0.5 | 1.0 | 1.5 | 2.0 | 2.5 |
| | | | | SILTY SAND (SM) , dark gray, with clay seams and shells | 1.0 | | | | | | | | | | | |
| | | | | LEAN CLAY WITH SAND (CL) , soft, gray - very soft, with shells at 2' - with a 1" layer of SILTY SAND at 3' - with organics below 3' - firm below 4' | 5.5 | | 74 | 30 33 | 37 | 22 | 15 | | | | | |
| 5 | | | | | | | | 28 | 35 | 19 | 16 | | | | | |
| | | | N=25 | SILTY SAND (SM) , dark gray, with organics, and clay partings and pockets - with a 1" peat seam at 6' - medium-dense, gray below 8' | | | | 23 | | | | | | | | |
| 10 | | | N=20 | SANDY LEAN CLAY (CL) , very stiff, gray | 10.3 | | | 21 | | | | | | | | |
| | | | | LEAN CLAY (CL) , very soft, gray, with shells | 12.0 | | | 24 | | | | | | | | |
| 15 | | | | | | | | 26 | | | | | | | | |
| | | | N=13 | - stiff below 16' | | | | 27 | 43 | 21 | 22 | | | | | |
| 20 | | | | FAT CLAY (CH) , very soft to soft, gray, with sand pockets, organics, and shells | 18.0 | 79 | | 44 | | | | | | | | |
| | | | | ORGANIC CLAY (OH) , firm, black and gray, with few peat pockets and seams | 23.0 | | | 116 | 126 | 34 | 92 | | | | | |
| 25 | | | | | | | | | | | | | | | | |
| | | | | PEAT (PT) , firm, black | 28.0 | | | 321 | 473 | 321 | 152 | | | | | |
| 30 | | | | | | | | | | | | | | | | |
| | | | | FAT CLAY (CH) , soft to firm, gray - with sand lenses and pockets at 33' - with sand partings at 38' - with sand lenses at 43' | 33.0 | 80 | | 41 | | | | | | | | |
| 35 | | | | | | | | | | | | | | | | |
| 40 | | | | | | 69 | | 59 | | | | | | | | |
| | | | | | | | | 57 | | | | | | | | |

NOTES:

- Terms and symbols defined on Plates A-32a and A-32b.

COMPLETION DATE: March 26, 2018
TOTAL DEPTH: 60.0'
CAVED DEPTH: Not Applicable
DRY AUGER: Not Applicable
WET ROTARY: 0' to 60'
BACKFILL: Cement-Bentonite Grout
LOGGER: R. Fasone
DRILL RIG: ABDU-38
HAMMER TYPE: Manual



Bayou De Cade Marsh Creation and Ridge Restoration

(TE-0138, Task 1)

Terrebonne Parish, Louisiana

LOG OF BORING NO. B-01

Project No.

04.55174066

PLATE A-17a

| DEPTH, FT | WATER LEVEL | SYMBOL | SAMPLES | BLOWS PER FOOT | LOCATION: See Plate 1 COORDINATES: N 29° 22' 48.77" W 90° 54' 19.56" SURFACE EL.: -0.8' | STRATUM DEPTH, FT | CLASSIFICATION | | | | | | SHEAR STRENGTH | | | | |
|-----------|-------------|--------|---------|----------------|--|-------------------|------------------|--------------------------|------------------|--------------|---------------|-----------------------|----------------|-----|-----|-----|-----|
| | | | | | STRATUM DESCRIPTION | | UNIT DRY WT, PCF | PASSING NO. 200 SIEVE, % | WATER CONTENT, % | LIQUID LIMIT | PLASTIC LIMIT | PLASTICITY INDEX (PI) | KIPS PER SQ FT | | | | |
| | | | | | | | | | | | | | 0.5 | 1.0 | 1.5 | 2.0 | 2.5 |
| | | | | | FAT CLAY (CH) , soft to firm, gray | | | | | | | | | | | | |
| | | | | | - with few sand pockets at 48' | | | | 59 | 82 | 27 | 55 | □ | ◇ | ▲ | | |
| -50 | | | | | | | | | | | | | | | | | |
| | | | | | | | 60 | | 67 | | | | □ | ● | ▲ | | |
| -55 | | | | | | | | | | | | | | | | | |
| | | | | | - with shell traces and shell fragments below 58' | | | | 37 | 96 | 27 | 69 | □ | | ▲ | | |
| -60 | | | | | | 60.0 | | | | | | | | | | | |
| -65 | | | | | | | | | | | | | | | | | |
| -70 | | | | | | | | | | | | | | | | | |
| -75 | | | | | | | | | | | | | | | | | |
| -80 | | | | | | | | | | | | | | | | | |
| -85 | | | | | | | | | | | | | | | | | |

NOTES:

- Terms and symbols defined on Plates A-32a and A-32b.

COMPLETION DATE: March 26, 2018
TOTAL DEPTH: 60.0'
CAVED DEPTH: Not Applicable
DRY AUGER: Not Applicable
WET ROTARY: 0' to 60'
BACKFILL: Cement-Bentonite Grout
LOGGER: R. Fasone
DRILL RIG: ABDU-38
HAMMER TYPE: Manual



Bayou De Cade Marsh Creation and Ridge Restoration

LOG OF BORING NO. B-01

(TE-0138, Task 1)

Terrebonne Parish, Louisiana

Project No.

04.55174066

PLATE A-17b

| DEPTH, FT | WATER LEVEL | SYMBOL | SAMPLES | BLOWS PER FOOT | LOCATION: See Plate 1 COORDINATES: N 29° 22' 24.77" W 90° 54' 54.11" SURFACE EL.: -0.9' | STRATUM DEPTH, FT | CLASSIFICATION | | | | | | SHEAR STRENGTH | | | | |
|-----------|-------------|--------|---------|----------------|--|-------------------|------------------|--------------------------|------------------|--------------|---------------|-----------------------|----------------|--|--|--|--|
| | | | | | STRATUM DESCRIPTION | | UNIT DRY WT, PCF | PASSING NO. 200 SIEVE, % | WATER CONTENT, % | LIQUID LIMIT | PLASTIC LIMIT | PLASTICITY INDEX (PI) | KIPS PER SQ FT | | | | |
| | | | | | | | | | | | | | | | | | |
| | | | | | LEAN CLAY (CL) , very soft, dark gray, with peat pockets, sand pockets and roots | | | | 67 | | | | | | | | |
| | | | | | | 4.0 | | | 36 | 39 | 23 | 16 | | | | | |
| 5 | | | | | SANDY LEAN CLAY (CL) , soft to firm, dark gray, with roots | | | 60 | 28 | | | | | | | | |
| | | | | N=7 | SILTY SAND (SM) , loose, gray | 6.0 | | | | | | | | | | | |
| | | | | N=9 | | | | 33 | 34 | | | | | | | | |
| 10 | | | | N=3 | - very loose below 10.5' | | | | 32 | | | | | | | | |
| | | | | N=2 | - with clay pockets below 12' | | | | | | | | | | | | |
| | | | | | FAT CLAY (CH) , very soft, gray - gray and dark gray, with organics from 14' to 18' - firm at 16' - soft at 18' - with 2" sand layer at 18' | 13.5 | | | 74 | 121 | 36 | 85 | | | | | |
| 15 | | | | | | | | | 76 | | | | | | | | |
| | | | | | | | 59 | | 67 | | | | | | | | |
| 20 | | | | | | | | | | | | | | | | | |
| | | | | | LEAN CLAY (CL) , soft to very soft, gray -with an organic layer at 24' - with peat layers at 28' - with a 2" sand layer at 30' | 24.0 | | | 163 | 39 | 19 | 20 | | | | | |
| 25 | | | | | | | | | | | | | | | | | |
| | | | | | | | 75 | | 29 | | | | | | | | |
| 30 | | | | | | | | | | | | | | | | | |
| | | | | | SILT (ML) , gray, with clay seams | 33.0 | | | 34 | | | | | | | | |
| 35 | | | | | | | | | | | | | | | | | |
| | | | | | | | | 99 | 41 | | | | | | | | |
| 40 | | | | | | | | | | | | | | | | | |
| | | | | | LEAN CLAY (CL) , firm, gray, with sand layers | 43.0 | | | 48 | 34 | 20 | 14 | | | | | |

NOTES:

- Terms and symbols defined on Plates A-32a and A-32b.

COMPLETION DATE: March 27, 2018
TOTAL DEPTH: 60.0'
CAVED DEPTH: Not Applicable
DRY AUGER: Not Applicable
WET ROTARY: 0' to 60'
BACKFILL: Cement-Bentonite Grout
LOGGER: R. Fasone
DRILL RIG: ABDU-38
HAMMER TYPE: Manual



Bayou De Cade Marsh Creation and Ridge Restoration

(TE-0138, Task 1)

Terrebonne Parish, Louisiana

LOG OF BORING NO. B-02

Project No.

04.55174066

PLATE A-18a

| DEPTH, FT | WATER LEVEL | SYMBOL | SAMPLES | BLOWS PER FOOT | LOCATION: See Plate 1 COORDINATES: N 29° 22' 24.77" W 90° 54' 54.11" SURFACE EL.: -0.9' | STRATUM DEPTH, FT | CLASSIFICATION | | | | | | SHEAR STRENGTH | | | | |
|-----------|-------------|--------|---------|----------------|--|-------------------|------------------|--------------------------|------------------|--------------|---------------|-----------------------|----------------|--|--|--|--|
| | | | | | STRATUM DESCRIPTION | | UNIT DRY WT, PCF | PASSING NO. 200 SIEVE, % | WATER CONTENT, % | LIQUID LIMIT | PLASTIC LIMIT | PLASTICITY INDEX (PI) | KIPS PER SQ FT | | | | |
| | | | | | LEAN CLAY (CL) , firm, gray, with sand layers | | | | | | | | | | | | |
| | | | | | FAT CLAY (CH) , soft, gray - with some sand layers at 48' | 48.0 | 68 | | 57 | | | | ◆●▲ | | | | |
| -50 | | | | | - firm below 53' | | | | 66 | | | | ◆▲ | | | | |
| -55 | | | | | | | | | 73 | 100 | 28 | 72 | ◆▲ | | | | |
| -60 | | | | | | 60.0 | | | | | | | | | | | |
| -65 | | | | | | | | | | | | | | | | | |
| -70 | | | | | | | | | | | | | | | | | |
| -75 | | | | | | | | | | | | | | | | | |
| -80 | | | | | | | | | | | | | | | | | |
| -85 | | | | | | | | | | | | | | | | | |

NOTES:

- Terms and symbols defined on Plates A-32a and A-32b.

COMPLETION DATE: March 27, 2018
TOTAL DEPTH: 60.0'
CAVED DEPTH: Not Applicable
DRY AUGER: Not Applicable
WET ROTARY: 0' to 60'
BACKFILL: Cement-Bentonite Grout
LOGGER: R. Fasone
DRILL RIG: ABDU-38
HAMMER TYPE: Manual



Bayou De Cade Marsh Creation and Ridge Restoration

(TE-0138, Task 1)

Terrebonne Parish, Louisiana

LOG OF BORING NO. B-02

Project No.

04.55174066

PLATE A-18b

| DEPTH, FT | WATER LEVEL | SYMBOL | SAMPLES | BLOWS PER FOOT | LOCATION: See Plate 1 | STRATUM DEPTH, FT | CLASSIFICATION | | | | | | SHEAR STRENGTH | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
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| | | | | | STRATUM DESCRIPTION | | | | | | UNIT DRY WT., PCF | PASSING NO. 200 SIEVE, % | WATER CONTENT, % | LIQUID LIMIT | PLASTIC LIMIT | PLASTICITY INDEX (PI) | KIPS PER SQ FT | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | 0.5 | 1.0 | 1.5 | 2.0 | 2.5 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | | | | FAT CLAY (CH) , gray, with peat and organics - with shells at 0' | | | | 65 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |

NOTES:

- Terms and symbols defined on Plates A-32a and A-32b.

COMPLETION DATE: April 3, 2018
TOTAL DEPTH: 60.0'
CAVED DEPTH: Not Applicable
DRY AUGER: Not Applicable
WET ROTARY: 0' to 60'
BACKFILL: Cement-Bentonite Grout
LOGGER: R. Fasone
DRILL RIG: ABDU-38
HAMMER TYPE: Manual



Bayou De Cade Marsh Creation and Ridge Restoration

(TE-0138, Task 1)

Terrebonne Parish, Louisiana

LOG OF BORING NO. B-03

Project No.

04.55174066

PLATE A-19a

| DEPTH, FT | WATER LEVEL | SYMBOL | SAMPLES | BLOWS PER FOOT | LOCATION: See Plate 1 COORDINATES: N 29° 21' 48.14" W 90° 55' 56.36" SURFACE EL.: -2.2' | STRATUM DEPTH, FT | CLASSIFICATION | | | | | | SHEAR STRENGTH | | | | |
|-----------|-------------|--------|---------|----------------|--|-------------------|------------------|--------------------------|------------------|--------------|---------------|-----------------------|----------------|---|--|--|--|
| | | | | | STRATUM DESCRIPTION | | UNIT DRY WT, PCF | PASSING NO. 200 SIEVE, % | WATER CONTENT, % | LIQUID LIMIT | PLASTIC LIMIT | PLASTICITY INDEX (PI) | KIPS PER SQ FT | | | | |
| | | | | | FAT CLAY (CH) , very soft, gray | | | | | | | | | | | | |
| | | | | | - firm, with few sand partings and trace organics at 48' | | 69 | | 60 | | | | ◇ | ● | | | |
| -50 | | | | | | | | | | | | | | | | | |
| | | | | | - soft at 53' | | | | | 83 | 26 | 57 | ◇ | | | | |
| -55 | | | | | | | | | | | | | | | | | |
| | | | | | - firm below 58' | | 59 | | 70 | | | | ◇ | ● | | | |
| -60 | | | | | | 60.0 | | | | | | | | | | | |
| -65 | | | | | | | | | | | | | | | | | |
| -70 | | | | | | | | | | | | | | | | | |
| -75 | | | | | | | | | | | | | | | | | |
| -80 | | | | | | | | | | | | | | | | | |
| -85 | | | | | | | | | | | | | | | | | |

NOTES:

- Terms and symbols defined on Plates A-32a and A-32b.

COMPLETION DATE: April 3, 2018
TOTAL DEPTH: 60.0'
CAVED DEPTH: Not Applicable
DRY AUGER: Not Applicable
WET ROTARY: 0' to 60'
BACKFILL: Cement-Bentonite Grout
LOGGER: R. Fasone
DRILL RIG: ABDU-38
HAMMER TYPE: Manual



Bayou De Cade Marsh Creation and Ridge Restoration

LOG OF BORING NO. B-03

(TE-0138, Task 1)

Terrebonne Parish, Louisiana

Project No.

04.55174066

PLATE A-19b

| DEPTH, FT | WATER LEVEL | SYMBOL | SAMPLES | BLOWS PER FOOT | LOCATION: See Plate 1 COORDINATES: N 29° 22' 26.38" W 90° 55' 25.32" SURFACE EL.: -0.5' | STRATUM DEPTH, FT | CLASSIFICATION | | | | | | SHEAR STRENGTH | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
|-----------|-------------|--------|---------|----------------|--|-------------------|------------------|--------------------------|------------------|--------------|---------------|-----------------------|----------------|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|----|
| | | | | | STRATUM DESCRIPTION | | UNIT DRY WT, PCF | PASSING NO. 200 SIEVE, % | WATER CONTENT, % | LIQUID LIMIT | PLASTIC LIMIT | PLASTICITY INDEX (PI) | KIPS PER SQ FT | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
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NOTES:

- Terms and symbols defined on Plates A-32a and A-32b.

COMPLETION DATE: April 3, 2018
TOTAL DEPTH: 40.0'
CAVED DEPTH: Not Applicable
DRY AUGER: Not Applicable
WET ROTARY: 0' to 40'
BACKFILL: Cement-Bentonite Grout
LOGGER: R. Fasone
DRILL RIG: ABDU-38
HAMMER TYPE: Manual



Bayou De Cade Marsh Creation and Ridge Restoration

(TE-0138, Task 1)

Terrebonne Parish, Louisiana

LOG OF BORING NO. B-04

Project No.

04.55174066

PLATE A-20

| DEPTH, FT | WATER LEVEL | SYMBOL | SAMPLES | BLOWS PER FOOT | LOCATION: See Plate 1 COORDINATES: N 29° 22' 56" W 90° 54' 34.17" SURFACE EL.: -2.5' | STRATUM DEPTH, FT | CLASSIFICATION | | | | | | SHEAR STRENGTH | | | | |
|-----------|-------------|--------|---------|----------------|---|-------------------|------------------|--------------------------|------------------|--------------|---------------|-----------------------|----------------|-----|-----|-----|-----|
| | | | | | STRATUM DESCRIPTION | | UNIT DRY WT, PCF | PASSING NO. 200 SIEVE, % | WATER CONTENT, % | LIQUID LIMIT | PLASTIC LIMIT | PLASTICITY INDEX (PI) | KIPS PER SQ FT | | | | |
| | | | | | | | | | | | | | 0.5 | 1.0 | 1.5 | 2.0 | 2.5 |
| | | | | | FAT CLAY (CH) , very soft to firm, dark gray - with a 2" organic clay layer at 2' - with roots below 4' | | | | 60 | 55 | 18 | 37 | | | | | |
| 5 | | | | | | | 71 | | 52 | | | | | | | | |
| | | | | | | | | 45 | 65 | 20 | 45 | | | | | | |
| | | | | | LEAN CLAY (CL) , soft, gray - with roots at 6' - with sand pockets at 7' - firm at 8' - very soft, with sand layers and ferrous nodules at 10' | 6.0 | | | 32 | | | | | | | | |
| 10 | | | | | | | 87 | | 33 | | | | | | | | |
| | | | | | | | | 95 | 37 | | | | | | | | |
| | | | | N=22 | - very stiff, with organics at 12.5' - with silt pockets from 12.5' to 18' | | | | 46 | 36 | 20 | 16 | | | | | |
| 15 | | | | | | | 72 | | 52 | | | | | | | | |
| | | | | | - with wood at 16' | | | | 35 | | | | | | | | |
| | | | | N=Push | - very soft, with sand pockets at 18' | | | | 32 | 31 | 22 | 9 | | | | | |
| 20 | | | | | | | | | | | | | | | | | |
| | | | | | - firm, with wood and silt pockets below 23' | | 89 | | 33 | | | | | | | | |
| 25 | | | | | | | | | | | | | | | | | |
| 30 | | | | | PEAT (PT) , gray | 29.0 | | | 231 | | | | | | | | |
| | | | | | | | | | | | | | | | | | |
| | | | | | LEAN CLAY (CL) , soft, gray | 33.0 | | | 36 | 32 | 19 | 13 | | | | | |
| 35 | | | | N=Push | | | | | | | | | | | | | |
| | | | | | - soft, with silt pockets below 38' | | | | 42 | | | | | | | | |
| 40 | | | | | | 40.0 | | | | | | | | | | | |

NOTES:

- Terms and symbols defined on Plates A-32a and A-32b.

COMPLETION DATE: March 28, 2018
TOTAL DEPTH: 40.0'
CAVED DEPTH: Not Applicable
DRY AUGER: Not Applicable
WET ROTARY: 0' to 40'
BACKFILL: Cement-Bentonite Grout
LOGGER: R. Fasone
DRILL RIG: ABDU-38
HAMMER TYPE: Manual



Bayou De Cade Marsh Creation and Ridge Restoration

LOG OF BORING NO. B-05

(TE-0138, Task 1)

Terrebonne Parish, Louisiana

Project No.

04.55174066

PLATE A-21

| DEPTH, FT | WATER LEVEL | SYMBOL | SAMPLES | BLOWS PER FOOT | LOCATION: See Plate 1 COORDINATES: N 29° 22' 57.4" W 90° 54' 46.95" SURFACE EL.: -6.1' | STRATUM DEPTH, FT | CLASSIFICATION | | | | | | SHEAR STRENGTH | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
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| | | | | | STRATUM DESCRIPTION | | UNIT DRY WT, PCF | PASSING NO. 200 SIEVE, % | WATER CONTENT, % | LIQUID LIMIT | PLASTIC LIMIT | PLASTICITY INDEX (PI) | KIPS PER SQ FT | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
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NOTES:

- Terms and symbols defined on Plates A-32a and A-32b.

COMPLETION DATE: March 30, 2018
TOTAL DEPTH: 60.0'
CAVED DEPTH: Not Applicable
DRY AUGER: Not Applicable
WET ROTARY: 0' to 60'
BACKFILL: Cement-Bentonite Grout
LOGGER: R. Fasone
DRILL RIG: ABDU-38
HAMMER TYPE: Manual



Bayou De Cade Marsh Creation and Ridge Restoration

LOG OF BORING NO. B-06

(TE-0138, Task 1)

Terrebonne Parish, Louisiana

Project No.

04.55174066

PLATE A-22a

| DEPTH, FT | WATER LEVEL | SYMBOL | SAMPLES | BLOWS PER FOOT | LOCATION: See Plate 1 COORDINATES: N 29° 22' 57.4" W 90° 54' 46.95" SURFACE EL.: -6.1' | STRATUM DEPTH, FT | CLASSIFICATION | | | | | | SHEAR STRENGTH | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
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| | | | | | STRATUM DESCRIPTION | | UNIT DRY WT, PCF | PASSING NO. 200 SIEVE, % | WATER CONTENT, % | LIQUID LIMIT | PLASTIC LIMIT | PLASTICITY INDEX (PI) | KIPS PER SQ FT | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | | | N=2 | FAT CLAY (CH) , firm, gray, with silt - soft at 45' - soft to firm, with silt pockets at 48' - with shells below 58' | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |

NOTES:

- Terms and symbols defined on Plates A-32a and A-32b.

COMPLETION DATE: March 30, 2018
TOTAL DEPTH: 60.0'
CAVED DEPTH: Not Applicable
DRY AUGER: Not Applicable
WET ROTARY: 0' to 60'
BACKFILL: Cement-Bentonite Grout
LOGGER: R. Fasone
DRILL RIG: ABDU-38
HAMMER TYPE: Manual



Bayou De Cade Marsh Creation and Ridge Restoration

(TE-0138, Task 1)

Terrebonne Parish, Louisiana

LOG OF BORING NO. B-06

Project No.

04.55174066

PLATE A-22b

| DEPTH, FT | WATER LEVEL | SYMBOL | SAMPLES | BLOWS PER FOOT | LOCATION: See Plate 1 | STRATUM DEPTH, FT | CLASSIFICATION | | | | | | SHEAR STRENGTH | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
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| | | | | | SURFACE EL.: -1.0' | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
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| | | | | | FAT CLAY (CH) , very soft, gray, with silt pockets - with a 4" organic clay layer with peat at 0' - with organics from 0.25' to 12' - firm from 2' to 12' | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |

NOTES:

- Terms and symbols defined on Plates A-32a and A-32b.

COMPLETION DATE: March 30, 2018
TOTAL DEPTH: 40.0'
CAVED DEPTH: Not Applicable
DRY AUGER: Not Applicable
WET ROTARY: 0' to 40'
BACKFILL: Cement-Bentonite Grout
LOGGER: R. Fasone
DRILL RIG: ABDU-38
HAMMER TYPE: Manual



Bayou De Cade Marsh Creation and Ridge Restoration

(TE-0138, Task 1)

Terrebonne Parish, Louisiana

LOG OF BORING NO. B-07

Project No.

04.55174066

PLATE A-23

| DEPTH, FT | WATER LEVEL | SYMBOL | SAMPLES | BLOWS PER FOOT | LOCATION: See Plate 1 | STRATUM DEPTH, FT | CLASSIFICATION | | | | | | SHEAR STRENGTH | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
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| | | | | | STRATUM DESCRIPTION | | | | | | UNIT DRY WT., PCF | PASSING NO. 200 SIEVE, % | WATER CONTENT, % | LIQUID LIMIT | PLASTIC LIMIT | PLASTICITY INDEX (PI) | KIPS PER SQ FT | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | 0.5 | 1.0 | 1.5 | 2.0 | 2.5 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | | | | SANDY SILT (ML) , gray, with clay layers - with organics at 0' | | | 59 | 12 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | </ |

NOTES:

- Terms and symbols defined on Plates A-32a and A-32b.

COMPLETION DATE: April 4, 2018
TOTAL DEPTH: 40.0'
CAVED DEPTH: Not Applicable
DRY AUGER: Not Applicable
WET ROTARY: 0' to 40'
BACKFILL: Cement-Bentonite Grout
LOGGER: R. Fasone
DRILL RIG: ABDU-38
HAMMER TYPE: Manual



Bayou De Cade Marsh Creation and Ridge Restoration

(TE-0138, Task 1)

Terrebonne Parish, Louisiana

LOG OF BORING NO. B-08

Project No.

04.55174066

PLATE A-24

| DEPTH, FT | WATER LEVEL | SYMBOL | SAMPLES | BLOWS PER FOOT | LOCATION: See Plate 1 | STRATUM DEPTH, FT | CLASSIFICATION | | | | | | SHEAR STRENGTH | | | | | | |
|---------------------|-------------|--------|---------|----------------|--|-------------------|------------------|--------------------------|------------------|--------------|---------------|-----------------------|----------------|-----|-----|-----|-----|--|--|
| | | | | | COORDINATES: N 29° 21' 56.94" W 90° 55' 47.05" | | UNIT DRY WT, PCF | PASSING NO. 200 SIEVE, % | WATER CONTENT, % | LIQUID LIMIT | PLASTIC LIMIT | PLASTICITY INDEX (PI) | KIPS PER SQ FT | | | | | | |
| | | | | | SURFACE EL.: -1.4' | | | | | | | | 0.5 | 1.0 | 1.5 | 2.0 | 2.5 | | |
| STRATUM DESCRIPTION | | | | | | | | | | | | | | | | | | | |
| | | | | | PEAT (PT), gray | 0.5 | | | 44 | 82 | 24 | 58 | ▲ | | | | | | |
| | | | | | FAT CLAY (CH), very soft, gray, with organics | 2.0 | | | | | | | | | | | | | |
| | | | | | SILTY SAND (SM), very loose, gray, with clay pockets | | | | 20 | | | | | | | | | | |
| 5 | | | | N=2/12" | | | | 33 | 14 | | | | | | | | | | |
| | | | | N=Push | | | | | | | | | | | | | | | |
| | | | | N=9 | LEAN CLAY (CL), firm, gray | 8.0 | | | | 47 | 22 | 25 | | | | | | | |
| 10 | | | | | - very soft at 10' | | | | 31 | 46 | 21 | 25 | ▲ | | | | | | |
| | | | | | - soft below 12' | | | 88 | 39 | | | | ◆ | ● | | | | | |
| 15 | | | | | FAT CLAY (CH), firm, gray | 14.0 | | | 49 | | | | | ◆ | ▲ | | | | |
| | | | | | | | | | 53 | 62 | 24 | 38 | ◆ | | ▲ | | | | |
| | | | | | - soft below 18' | | | 75 | 48 | | | | ◆ | ● | ▲ | | | | |
| 20 | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | 65 | 60 | | | | | ● | ◆ | | | | |
| 25 | | | | | | | | | | | | | | | | | | | |
| | | | | | - with a 4" peat layer at 29.5' | | | | | | | | | ◆ | | | | | |
| 30 | | | | | | | | | | | | | | | | | | | |
| | | | | | - with a 1" peat layer at 33' | | | 91 | 35 | | | | | ◆ | ● | | | | |
| 35 | | | | | | | | | | | | | | | | | | | |
| 40 | | | | | SANDY LEAN CLAY (CL), soft, gray, with silt seams | 38.0 | | | | | | | | ◆ | | | | | |
| | | | | | | 40.0 | | | | | | | | | | | | | |

NOTES:

- Terms and symbols defined on Plates A-32a and A-32b.

COMPLETION DATE: March 30, 2018
TOTAL DEPTH: 40.0'
CAVED DEPTH: Not Applicable
DRY AUGER: Not Applicable
WET ROTARY: 0' to 40'
BACKFILL: Cement-Bentonite Grout
LOGGER: R. Fasone
DRILL RIG: ABDU-38
HAMMER TYPE: Manual



Bayou De Cade Marsh Creation and Ridge Restoration

(TE-0138, Task 1)

Terrebonne Parish, Louisiana

LOG OF BORING NO. B-09

Project No.

04.55174066

PLATE A-25

| DEPTH, FT | WATER LEVEL | SYMBOL | SAMPLES | BLOWS PER FOOT | LOCATION: See Plate 1 COORDINATES: N 29° 23' 01.59" W 90° 53' 33.96" SURFACE EL.: -4.3' | STRATUM DEPTH, FT | CLASSIFICATION | | | | | | SHEAR STRENGTH | | | | |
|-----------|-------------|--------|---------|----------------|--|-------------------|------------------|--------------------------|------------------|--------------|---------------|-----------------------|----------------|--|--|--|--|
| | | | | | STRATUM DESCRIPTION | | UNIT DRY WT, PCF | PASSING NO. 200 SIEVE, % | WATER CONTENT, % | LIQUID LIMIT | PLASTIC LIMIT | PLASTICITY INDEX (PI) | KIPS PER SQ FT | | | | |
| | | | | | | | | | | | | | | | | | |
| | | | | | LEAN CLAY WITH SAND (CL), very soft, gray | | | | 31 | | | | | | | | |
| | | | | | SILTY SAND (SM), gray, with clay pockets | 2.0 | | 50 | 28 | | | | | | | | |
| 5 | | | | N=7 | - loose below 4' | | | | | | | | | | | | |
| | | | | N=5 | SANDY SILT (ML), loose, gray, with clay pockets | 6.0 | | | | 25 | 24 | 1 | | | | | |
| | | | | | FAT CLAY (CH), soft, gray, with wood and organics | 9.0 | | | 61 | | | | | | | | |
| 10 | | | | | | | | 111 | 81 | 27 | 54 | | | | | | |
| | | | | | SILTY SAND (SM), gray, with clay pockets and shells | 12.3 | | | 30 | | | | | | | | |
| 15 | | | | | FAT CLAY (CH), soft, dark gray, with sand seams | 14.0 | | | 113 | | | | | | | | |
| | | | | | | 16.0 | | | | | | | | | | | |
| 20 | | | | | | | | | | | | | | | | | |
| 25 | | | | | | | | | | | | | | | | | |
| 30 | | | | | | | | | | | | | | | | | |
| 35 | | | | | | | | | | | | | | | | | |
| 40 | | | | | | | | | | | | | | | | | |

NOTES:

- Terms and symbols defined on Plates A-32a and A-32b.

COMPLETION DATE: April 2, 2018
TOTAL DEPTH: 16.0'
CAVED DEPTH: Not Applicable
DRY AUGER: Not Applicable
WET ROTARY: 0' to 16'
BACKFILL: Cement-Bentonite Grout
LOGGER: R. Fasone
DRILL RIG: ABDU-38
HAMMER TYPE: Manual



Bayou De Cade Marsh Creation and Ridge Restoration

(TE-0138, Task 1)


Terrebonne Parish, Louisiana

LOG OF BORING NO. B-10

Project No.

04.55174066

PLATE A-26

| DEPTH, FT | WATER LEVEL | SYMBOL | SAMPLES | BLOWS PER FOOT | LOCATION: See Plate 1 COORDINATES: N 29° 23' 06.77" W 90° 53' 10.61" SURFACE EL.: -4.6' | STRATUM DEPTH, FT | CLASSIFICATION | | | | | SHEAR STRENGTH | | | | | | | |
|---|-------------|--------|---------|----------------|---|-------------------|---|--------------------------|------------------|--------------|---------------|-----------------------|---------------------------------------|--|--|--|--|--|--|
| | | | | | | | UNIT DRY WT, PCF | PASSING NO. 200 SIEVE, % | WATER CONTENT, % | LIQUID LIMIT | PLASTIC LIMIT | PLASTICITY INDEX (PI) | KIPS PER SQ FT 0.5 1.0 1.5 2.0 2.5 | | | | | | |
| 5 | | | | | FAT CLAY (CH) , very soft to soft, gray - with shells from 0' to 0.5' - with wood from 0.5' to 1.2' - with sand from 1.2' to 1.8' - with 1' LEAN CLAY with SAND, gray at 3' - with peat at 4' - with sand traces at 6' - with wood and sand traces at 10' - with sand seams at 12' | | | 86 | | | | | | | | | | | |
| | | | | | | | | 83 | 26 | | | | | | | | | | |
| | | | | | | | | | 85 | 84 | 25 | 59 | | | | | | | |
| | | | | | | | | | 64 | | | | | | | | | | |
| 10 | | | | | | | | | 74 | | | | | | | | | | |
| | | | | | | | | | 63 | | | | | | | | | | |
| | | | | | | | | | 62 | 56 | 20 | 36 | | | | | | | |
| 15 | | | | | | | | | 61 | | | | | | | | | | |
| | | | | | | | 16.0 | | | | | | | | | | | | |
| 20 | | | | | | | | | | | | | | | | | | | |
| 25 | | | | | | | | | | | | | | | | | | | |
| 30 | | | | | | | | | | | | | | | | | | | |
| 35 | | | | | | | | | | | | | | | | | | | |
| 40 | | | | | | | | | | | | | | | | | | | |
| NOTES: 1. Terms and symbols defined on Plates A-32a and A-32b. | | | | | | | COMPLETION DATE: April 2, 2018 TOTAL DEPTH: 16.0' CAVED DEPTH: Not Applicable DRY AUGER: Not Applicable WET ROTARY: 0' to 16' BACKFILL: Cement-Bentonite Grout LOGGER: R. Fasone DRILL RIG: ABDU-38 HAMMER TYPE: Manual | | | | | | | | | | | | |
|  Bayou De Cade Marsh Creation and Ridge Restoration (TE-0138, Task 1) | | | | | | | LOG OF BORING NO. B-11 | | | | | | | | | | | | |
| Terrebonne Parish, Louisiana | | | | | | | Project No. 04.55174066 | | | | | PLATE A-27 | | | | | | | |

[illegible]

COMPLETION DATE: April 2, 2018
TOTAL DEPTH: 16.0'
CAVED DEPTH: Not Applicable
DRY AUGER: Not Applicable
WET ROTARY: 0' to 16'
BACKFILL: Cement-Bentonite Grout
LOGGER: R. Fasone
DRILL RIG: ABDU-38
HAMMER TYPE: Manual



Bayou De Cade Marsh Creation and Ridge Restoration

(TE-0138, Task 1)

Terrebonne Parish, Louisiana

LOG OF BORING NO. B-12

| |
|-------------|
| Project No. |
|-------------|

04.55174066

PLATE A-28

| DEPTH, FT | WATER LEVEL | SYMBOL | SAMPLES | BLOWS PER FOOT | LOCATION: See Plate 1 COORDINATES: N 29° 23' 17.88" W 90° 52' 54.71" SURFACE EL.: -5.1' | STRATUM DEPTH, FT | CLASSIFICATION | | | | | | SHEAR STRENGTH | | | | |
|-----------|-------------|--------|---------|----------------|--|-------------------|------------------|--------------------------|------------------|--------------|---------------|-----------------------|----------------|--|--|--|--|
| | | | | | STRATUM DESCRIPTION | | UNIT DRY WT, PCF | PASSING NO. 200 SIEVE, % | WATER CONTENT, % | LIQUID LIMIT | PLASTIC LIMIT | PLASTICITY INDEX (PI) | KIPS PER SQ FT | | | | |
| | | | | | | | | | | | | | | | | | |
| | | | | N=9 | SILT WITH SAND (ML) , stiff, gray, with clay lenses and organics | 2.0 | | 84 | 25 | | | | | | | | |
| | | | | | SILTY SAND (SM) , loose, gray | | | | | | | | | | | | |
| 5 | | | | N=4 | LEAN CLAY (CL) , very soft to soft, gray - with peat layers and sand layers at 5.5' | 4.5 | | | | | | | | | | | |
| | | | | | SHELLS | 8.0 | | | | | | | | | | | |
| | | | | | LEAN CLAY (CL) , soft, gray, with organics | 9.0 | | | | | | | | | | | |
| 10 | | | | | ORGANIC CLAY (OH) , soft, gray | 10.0 | | 52 | 28 | | | | ◆▲ | | | | |
| | | | | | - with wood below 12' | | | | | | | | | | | | |
| | | | | | PEAT (PT) , very soft to soft, black and brown, with clay layers, rootlets, and an organic odor | 14.0 | | | 82 | 123 | 38 | 85 | ▲ | | | | |
| 15 | | | | | | | | 162 | | | | | ▲ | | | | |
| | | | | | | 16.0 | | 206 | | | | | ◆▲ | | | | |
| 20 | | | | | | | | | | | | | | | | | |
| 25 | | | | | | | | | | | | | | | | | |
| 30 | | | | | | | | | | | | | | | | | |
| 35 | | | | | | | | | | | | | | | | | |
| 40 | | | | | | | | | | | | | | | | | |

NOTES:

- Terms and symbols defined on Plates A-32a and A-32b.

COMPLETION DATE: April 2, 2018
TOTAL DEPTH: 16.0'
CAVED DEPTH: Not Applicable
DRY AUGER: Not Applicable
WET ROTARY: 0' to 16'
BACKFILL: Cement-Bentonite Grout
LOGGER: R. Fasone
DRILL RIG: ABDU-38
HAMMER TYPE: Manual



Bayou De Cade Marsh Creation and Ridge Restoration

(TE-0138, Task 1)

Terrebonne Parish, Louisiana

LOG OF BORING NO. B-13

Project No.

04.55174066

PLATE A-29

| DEPTH, FT | WATER LEVEL | SYMBOL SAMPLES | BLOWS PER FOOT | LOCATION: See Plate 1 | STRATUM DEPTH, FT | CLASSIFICATION | | | | | | SHEAR STRENGTH | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
|-----------|-------------|-------------------|-------------------|-----------------------|----------------------|----------------|--|--|--|----------------------|-----------------------------|---------------------|-----------------|------------------|--------------------------|----------------|-----|-----|-----|-----|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|
| | | | | STRATUM DESCRIPTION | | | | | | UNIT DRY WT., PCF | PASSING NO. 200 SIEVE, % | WATER CONTENT, % | LIQUID LIMIT | PLASTIC LIMIT | PLASTICITY INDEX (PI) | KIPS PER SQ FT | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
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NOTES:

- Terms and symbols defined on Plates A-32a and A-32b.

COMPLETION DATE: March 28, 2018
TOTAL DEPTH: 16.0'
CAVED DEPTH: Not Applicable
DRY AUGER: Not Applicable
WET ROTARY: 0' to 16'
BACKFILL: Cement-Bentonite Grout
LOGGER: R. Fasone
DRILL RIG: ABDU-38
HAMMER TYPE: Manual



Bayou De Cade Marsh Creation and Ridge Restoration

(TE-0138, Task 1)


Terrebonne Parish, Louisiana

LOG OF BORING NO. B-14

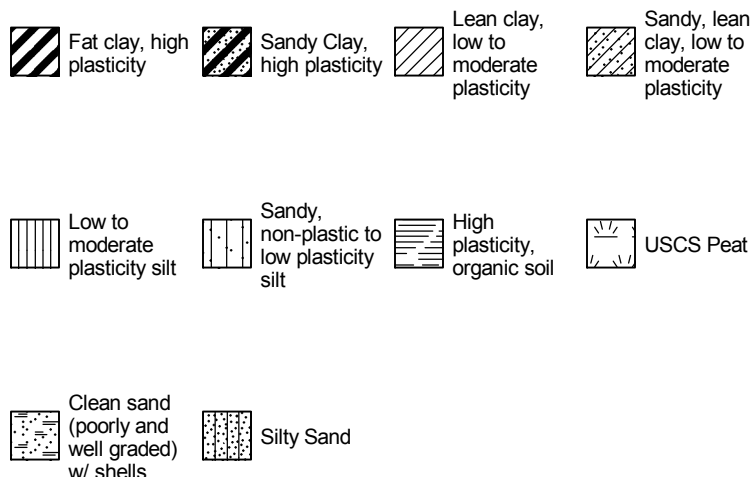
Project No.

04.55174066

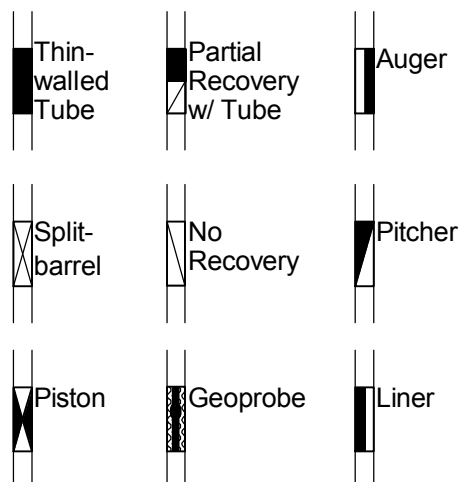
PLATE A-30

| DEPTH, FT | WATER LEVEL | SYMBOL | SAMPLES | BLOWS PER FOOT | LOCATION: See Plate 1 | STRATUM DEPTH, FT | CLASSIFICATION | | | | | | SHEAR STRENGTH | | | | | | |
|---|-------------|--------|---------|----------------|--|-------------------|--|--------------------------|------------------|--------------|---------------|-----------------------|---------------------|----|--|--|--|--|--|
| | | | | | COORDINATES: N 29° 23' 11.23" W 90° 52' 43.43" | | UNIT DRY WT., PCF | PASSING NO. 200 SIEVE, % | WATER CONTENT, % | LIQUID LIMIT | PLASTIC LIMIT | PLASTICITY INDEX (PI) | KIPS PER SQ FT | | | | | | |
| | | | | | SURFACE EL.: -8.1' | | | | | | | | 0.5 1.0 1.5 2.0 2.5 | | | | | | |
| | | | | | STRATUM DESCRIPTION | | | | | | | | | | | | | | |
| | | | | | FAT CLAY (CH) , very soft, gray, with silt layers and shells - with gravel and roots at 2' | | | | 71 | | | | | | | | | | |
| | | | | | - with a 4" silty sand layer at 4.5' | | | 93 | 40 | | | | | | | | | | |
| 5 | | | | N=4 | - with ferrous nodules below 6' | | | | 103 | | | | | | | | | | |
| | | | | | FAT CLAY WITH SAND (CH) , soft, gray | 8.0 | | 79 | 36 | | | | | ◆▲ | | | | | |
| 10 | | | | | FAT CLAY (CH) , very soft, gray | 10.0 | | | 102 | | | | | ▲ | | | | | |
| | | | | | | | | | 71 | 87 | 28 | 59 | | ▲ | | | | | |
| 15 | | | | | | | | | 64 | | | | | ◆ | | | | | |
| | | | | | | 18.0 | | | | | | | | | | | | | |
| 20 | | | | | | | | | | | | | | | | | | | |
| 25 | | | | | | | | | | | | | | | | | | | |
| 30 | | | | | | | | | | | | | | | | | | | |
| 35 | | | | | | | | | | | | | | | | | | | |
| 40 | | | | | | | | | | | | | | | | | | | |
| NOTES: 1. Terms and symbols defined on Plates A-32a and A-32b. | | | | | | | COMPLETION DATE: March 28, 2018 TOTAL DEPTH: 18.0' CAVED DEPTH: Not Applicable DRY AUGER: Not Applicable WET ROTARY: 0' to 18' BACKFILL: Cement-Bentonite Grout LOGGER: R. Fasone DRILL RIG: ABDU-38 HAMMER TYPE: Manual | | | | | | | | | | | | |
|  Bayou De Cade Marsh Creation and Ridge Restoration (TE-0138, Task 1) | | | | | | | LOG OF BORING NO. B-15 | | | | | | | | | | | | |
| Terrebonne Parish, Louisiana | | | | | | | Project No. | | | 04.55174066 | | | PLATE A-31 | | | | | | |

SOIL TYPES



SAMPLER TYPES

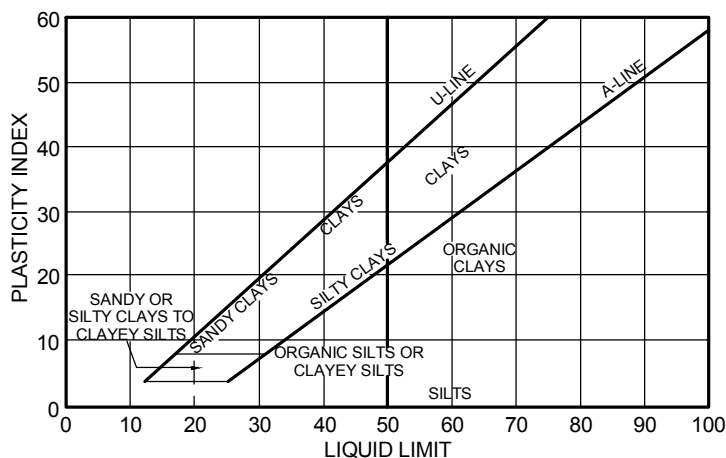


SOIL GRAIN SIZE

U.S. Standard Sieve

| 6" | 3" | 3/4" | 4 | 10 | 40 | 200 | | |
|----------|---------|--------|------|--------|--------|-------|-------|------|
| Boulders | Cobbles | Gravel | | Sand | | | Silt | Clay |
| | | Coarse | Fine | Coarse | Medium | Fine | | |
| 152 | 75.0 | 19.0 | 4.75 | 2.00 | 0.425 | 0.075 | 0.005 | (mm) |

PLASTICITY CHART



SOIL STRUCTURE

| | |
|--------------|--|
| Slickensided | Having planes of weakness that appear slick and glossy. |
| Fissured | Containing shrinkage or relief cracks, often filled with fine sand or silt; usually more or less vertical. |
| Pocket | Inclusion of material of different texture that is smaller than the diameter of the sample. |
| Parting | Inclusion less than 1/8 inch thick extending through the sample. |
| Seam | Inclusion 1/8 inch to 3 inches thick extending through the sample. |
| Layer | Inclusion greater than 3 inches thick extending through the sample. |
| Laminated | Soil sample composed of alternating partings or seams of different soil type. |
| Interlayered | Soil sample composed of alternating layers of different soil type. |
| Intermixed | Soil sample composed of pockets of different soil type and layered or laminated structure is not evident. |
| Calcareous | Having appreciable quantities of carbonate. |
| Carbonate | Having more than 50% carbonate content. |



TERMS AND SYMBOLS USED ON BORING LOGS

SOIL CLASSIFICATION (1 of 2)

Project No.
04.55174066

PLATE A-32a

STANDARD PENETRATION TEST (SPT)

A 2-in.-OD, 1-3/8-ID split spoon sampler is driven 1.5 ft into undisturbed soil with a 140-pound hammer free falling 30 in. After the sampler is seated 6 in. into undisturbed soil, the number of blows required to drive the sampler the last 12 in. is the Standard Penetration Resistance or "N" value, which is recorded as blows per foot as described below.

SPLIT-BARREL SAMPLER DRIVING RECORD

| Blows Per Foot | Description |
|----------------|---|
| 25 | 25 blows drove sampler 12 inches, after initial 6 inches of seating. |
| 50/7" | 50 blows drove sampler 7 inches, after initial 6 inches of seating. |
| Ref/3" | 50 blows drove sampler 3 inches during initial 6-inch seating interval. |

NOTE: To avoid damage to sampling tools, driving is limited to 50 blows during or after seating interval.

DENSITY OF GRANULAR SOILS

| Descriptive Term | *Relative Density, % | **Blows Per Foot (SPT) |
|--------------------|----------------------|------------------------|
| Very Loose | < 15 | 0 to 4 |
| Loose | 15 to 35 | 5 to 10 |
| Medium Dense | 35 to 65 | 11 to 30 |
| Dense | 65 to 85 | 31 to 50 |
| Very Dense | > 85 | > 50 |

*Estimated from sampler driving record.

**Requires correction for depth, groundwater level, and grain size.

STRENGTH OF COHESIVE SOILS

| Term | Undrained Shear Strength, ksf | Blows Per Foot (SPT) (approximate) |
|------------------|-------------------------------|------------------------------------|
| Very Soft | < 0.25 | 0 to 2 |
| Soft | 0.25 to 0.50 | 2 to 4 |
| Firm | 0.50 to 1.00 | 4 to 8 |
| Stiff | 1.00 to 2.00 | 8 to 16 |
| Very Stiff | 2.00 to 4.00 | 16 to 32 |
| Hard | > 4.00 | > 32 |

SHEAR STRENGTH TEST METHOD

U = Unconfined Q = Unconsolidated - Undrained Triaxial

P = Pocket Penetrometer T = Torvane V = Miniature Vane F = Hand Vane

HAND PENETROMETER CORRECTION

Our experience has shown that the hand penetrometer generally overestimates the in-situ undrained shear strength of over consolidated Pleistocene Gulf Coast clays. These strengths are partially controlled by the presence of macroscopic soil defects such as slickensides, which generally do not influence smaller scale tests like the hand penetrometer. Based on our experience, we have adjusted these field estimates of the undrained shear strength of natural, overconsolidated Pleistocene Gulf Coast soils by multiplying the measured penetrometer reading by a factor of 0.6. These adjusted strength estimates are recorded in the "Shear Strength" column on the boring logs. Except as described in the text, we have not adjusted estimates of the undrained shear strength for projects located outside of the Pleistocene Gulf Coast formations.

Information on each boring log is a compilation of subsurface conditions and soil or rock classifications obtained from the field as well as from laboratory testing of samples. Strata have been interpreted by commonly accepted procedures. The stratum lines on the logs may be transitional and approximate in nature. Water level measurements refer only to those observed at the time and places indicated, and can vary with time, geologic condition, or construction activity.



TERMS AND SYMBOLS USED ON BORING LOGS

SOIL CLASSIFICATION (2 of 2)

Project No.
04.55174066

PLATE A-32b



APPENDIX B

LABORATORY TESTING

| Sample No. | Depth (ft) | Identification Tests | | | | | | | | | Field Shear Strength Estimate | | Miniature Vane Tests | Compression Tests | | | | Other Tests |
|------------|------------|----------------------|-------------------|-----------------------|----------------------|-----------------------|-------------------------|------------------|---------------------|---------------------------|-------------------------------|---------------|----------------------|-------------------|--------------------------|----------------------|-----------------|-------------|
| | | Liquid Limit (%) | Plastic Limit (%) | Plasticity Index (PI) | Moisture Content (%) | Dry Unit Weight (pcf) | Total Unit Weight (pcf) | Specific Gravity | Organic Content (%) | Passing No. 200 Sieve (%) | Penetrometer (ksf) | Torvane (ksf) | Shear Strength (ksf) | Type Test | Confining Pressure (psi) | Shear Strength (ksf) | Type of Failure | |
| 1a | 1.0-2.0 | 37 | 22 | 15 | 30 | | | | | | 0.50 | 0.20 | 0.38 | | | | | |
| 2 | 2.0-3.0 | | | | 33 | | | | | 74 | | 0.20 | 0.22 | | | | | |
| 3 | 4.0-6.0 | 35 | 19 | 16 | 28 | | | | | | 1.00 | 0.30 | 0.82 | | | | | |
| 4 | 6.0-8.0 | | | | 23 | | | | | | 0.50 | 0.20 | 0.92 | | | | | |
| 5 | 8.0-9.5 | | | | 21 | | | | | | | | | | | | | |
| 6 | 10.0-11.5 | | | | 24 | | | | | | | | | | | | | |
| 7 | 12.0-14.0 | | | | 26 | | | | | | 0.25 | 0.15 | 0.13 | | | | | |
| 9 | 16.0-17.5 | 43 | 21 | 22 | 27 | | | | | | | | | | | | | |
| 10 | 18.0-20.0 | | | | 44 | 79 | 113 | | | | | 0.20 | 0.25 | UU | 5 | 0.26 | A | |
| 11 | 23.0-25.0 | 126 | 34 | 92 | 116 | | | 2.472 | | | 0.25 | 0.23 | 0.68 | | | | | C |
| 12 | 28.0-30.0 | 473 | 321 | 152 | 321 | | | | | | 1.25 | 0.53 | 2.58 | | | | | |
| 13 | 33.0-35.0 | | | | 41 | 80 | 114 | | | | 0.25 | 0.20 | 0.29 | UU | 9 | 0.29 | A | |
| 14 | 38.0-40.0 | | | | 59 | 69 | 109 | | | | 0.25 | 0.18 | 0.68 | UU | 11 | 0.45 | A | |
| 15 | 43.0-45.0 | | | | 57 | | | | | | 0.25 | 0.20 | 0.57 | | | | | |
| 16 | 48.0-50.0 | 82 | 27 | 55 | 59 | | | | | | 0.25 | 0.20 | 0.53 | | | | | |
| 17 | 53.0-55.0 | | | | 67 | 60 | 100 | | | | 0.25 | 0.20 | 0.57 | UU | 15 | 0.45 | C | |
| 18 | 58.0-60.0 | 96 | 27 | 69 | 37 | | | | | | 0.25 | 0.43 | 0.91 | | | | | |
| | | | | | | | | | | | | | | | | | | |
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Notes:

NP = Non-Plastic Material

TYPE OF TEST

U - Unconfined Compression
 UU - Unconsolidated - Undrained Triaxial
 CU - Consolidated - Undrained Triaxial

TYPE OF FAILURE

A - Bulge
 B - Single Shear Plane
 C - Multiple Shear Plane
 D - Vertical Fracture

OTHER TEST TYPES

C = Consolidation SO = Sulfates
 pH = pH
 R = Resistivity
 Cl = Chlorides



Bayou De Cade Marsh Creation and Ridge Restoration

(TE-0138, Task 1)

Terrebonne Parish, Louisiana

SUMMARY OF TEST RESULTS - BORING B-01

LELAP Lab ID #10001

Project No.

04.55174066

PLATE B-1a

| Sample No. | Depth (ft) | Identification Tests | | | | | | | | | Field Shear Strength Estimate | | Miniature Vane Tests | Compression Tests | | | | Other Tests |
|------------|------------|----------------------|-------------------|-----------------------|----------------------|-----------------------|-------------------------|------------------|---------------------|---------------------------|-------------------------------|---------------|----------------------|-------------------|--------------------------|----------------------|-----------------|-------------|
| | | Liquid Limit (%) | Plastic Limit (%) | Plasticity Index (PI) | Moisture Content (%) | Dry Unit Weight (pcf) | Total Unit Weight (pcf) | Specific Gravity | Organic Content (%) | Passing No. 200 Sieve (%) | Penetrometer (ksf) | Torvane (ksf) | Shear Strength (ksf) | Type Test | Confining Pressure (psi) | Shear Strength (ksf) | Type of Failure | |
| 1 | 0.0-2.0 | | | | 67 | | | | | | | 0.05 | 0.08 | | | | | |
| 2 | 2.0-4.0 | 39 | 23 | 16 | 36 | | | | | | | 0.20 | 0.09 | | | | | |
| 3 | 4.0-6.0 | | | | 28 | | | | | 60 | 0.50 | 0.10 | | | | | | |
| 4 | 6.0-7.5 | | | | 32 | | | | | | | | | | | | | |
| 5 | 8.5-10.0 | | | | 34 | | | | | 33 | | | | | | | | |
| 6 | 10.5-12.0 | | | | 32 | | | | | | | | | | | | | |
| 7 | 12.0-14.0 | | | | 44 | | | | | | | | 0.26 | | | | | |
| 8 | 14.0-16.0 | 121 | 36 | 85 | 74 | | | | | | | 0.10 | 0.14 | | | | | |
| 9 | 16.0-18.0 | | | | 76 | | | 2.689 | | | 0.25 | 0.18 | 0.57 | | | | | C |
| 10 | 18.0-20.0 | | | | 67 | 59 | 99 | | | | | 0.18 | 0.34 | UU | 5 | 0.32 | A,C | |
| | 24.0-25.0 | 39 | 19 | 20 | 163 | | | | | | 0.75 | 0.18 | 0.45 | | | | | |
| 12 | 28.0-30.0 | | | | 29 | 75 | 97 | | | | | 0.40 | 0.40 | UU | 8 | 0.20 | C | |
| 13 | 33.0-35.0 | | | | 34 | | | | | | 0.25 | 0.28 | | | | | | |
| 14 | 38.0-40.0 | | | | 41 | | | | | 99 | 0.25 | 0.11 | 0.29 | | | | | |
| 15 | 43.0-45.0 | 34 | 20 | 14 | 48 | | | | | | 0.25 | 0.20 | 0.55 | | | | | |
| 16 | 48.0-50.0 | | | | 57 | 68 | 106 | | | | 0.25 | 0.10 | 0.54 | UU | 13 | 0.40 | A | |
| 17 | 53.0-55.0 | | | | 66 | | | | | | 0.25 | 0.15 | 0.59 | | | | | |
| 18 | 58.0-60.0 | 100 | 28 | 72 | 73 | | | | | | 0.75 | 0.20 | 0.73 | | | | | |
| | | | | | | | | | | | | | | | | | | |
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Notes:

NP = Non-Plastic Material

TYPE OF TEST

U - Unconfined Compression
 UU - Unconsolidated - Undrained Triaxial
 CU - Consolidated - Undrained Triaxial

TYPE OF FAILURE

A - Bulge
 B - Single Shear Plane
 C - Multiple Shear Plane
 D - Vertical Fracture

OTHER TEST TYPES

C = Consolidation SO = Sulfates
 pH = pH
 R = Resistivity
 Cl = Chlorides



Bayou De Cade Marsh Creation and Ridge Restoration

SUMMARY OF TEST RESULTS - BORING B-02

(TE-0138, Task 1)

LELAP Lab ID #10001

Terrebonne Parish, Louisiana

Project No.

04.55174066

PLATE B-1b

| Sample No. | Depth (ft) | Identification Tests | | | | | | | | | Field Shear Strength Estimate | | Miniature Vane Tests | Compression Tests | | | | Other Tests |
|------------|------------|----------------------|-------------------|-----------------------|----------------------|-----------------------|-------------------------|------------------|---------------------|---------------------------|-------------------------------|---------------|----------------------|-------------------|--------------------------|----------------------|-----------------|-------------|
| | | Liquid Limit (%) | Plastic Limit (%) | Plasticity Index (PI) | Moisture Content (%) | Dry Unit Weight (pcf) | Total Unit Weight (pcf) | Specific Gravity | Organic Content (%) | Passing No. 200 Sieve (%) | Penetrometer (ksf) | Torvane (ksf) | Shear Strength (ksf) | Type Test | Confining Pressure (psi) | Shear Strength (ksf) | Type of Failure | |
| 1 | 0.0-2.0 | | | | 65 | | | | | | | 0.30 | 0.11 | | | | | |
| 2 | 2.0-4.0 | | | | 31 | | | | | | | 0.30 | 0.19 | | | | | C |
| 4 | 6.0-7.5 | | | | 11 | | | | | 19 | | | | | | | | |
| 6 | 10.0-11.5 | | | | 29 | | | | | 17 | | | | | | | | |
| 7 | 12.0-14.0 | | | | 39 | 86 | 120 | | | | | | 0.57 | UU | 5 | 0.34 | A | |
| 8 | 14.0-16.0 | 39 | 18 | 21 | 86 | | | | | | | | 0.50 | | | | | |
| 9 | 16.0-18.0 | | | | 81 | 54 | 98 | | | | | 0.20 | 1.12 | UU | 6 | 0.39 | C | |
| 10 | 18.0-20.0 | | | | 65 | | | | | | | 0.25 | 0.40 | | | | | |
| 11 | 23.0-24.2 | | | | | | | | 38.94 | | | | | | | | | |
| | 24.2-25.0 | | | | 69 | 58 | 98 | | 6.28 | | | 0.30 | | UU | 9 | 0.30 | A | |
| 12 | 28.0-30.0 | | | | 28 | | | | | 87 | | 0.10 | | | | | | |
| 13 | 33.0-35.0 | | | | 39 | | | | | 91 | | 0.10 | | | | | | |
| 14 | 38.0-40.0 | | | | 53 | 71 | 108 | | | | | 0.10 | | UU | 14 | 0.47 | A | |
| 15 | 43.0-45.0 | | | | | | | | | | | 0.45 | | | | | | |
| 16 | 48.0-50.0 | | | | 60 | 69 | 110 | | | | | 0.15 | | UU | 17 | 0.57 | A,B | |
| 17 | 53.0-55.0 | 83 | 26 | 57 | | | | | | | | 0.15 | | | | | | |
| 18 | 58.0-60.0 | | | | 70 | 59 | 100 | | | | | 0.20 | | UU | 21 | 0.59 | | |
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Notes:

NP = Non-Plastic Material

TYPE OF TEST

U - Unconfined Compression
 UU - Unconsolidated - Undrained Triaxial
 CU - Consolidated - Undrained Triaxial

TYPE OF FAILURE

A - Bulge
 B - Single Shear Plane
 C - Multiple Shear Plane
 D - Vertical Fracture

OTHER TEST TYPES

C = Consolidation SO = Sulfates
 pH = pH
 R = Resistivity
 Cl = Chlorides



Bayou De Cade Marsh Creation and Ridge Restoration

SUMMARY OF TEST RESULTS - BORING B-03

(TE-0138, Task 1)

LELAP Lab ID #10001

Terrebonne Parish, Louisiana

Project No.

04.55174066

PLATE B-1c

[illegible]

Notes:

NP = Non-Plastic Material

TYPE OF TEST

U - Unconfined Compression

UU - Unconsolidated - Undrained Triaxial

CU - Consolidated - Undrained Triaxial

TYPE OF FAILURE

A - Bulge

B - Single Shear Plane

C - Multiple Shear Plane

D - Vertical Fracture

OTHER TEST TYPES

C = Consolidation SO = Sulfates

$\text{pH} = \text{pH}$

R = Resistivity

Cl = Chlorides



Bayou De Cade Marsh Creation and Ridge Restoration

(TE-0138, Task 1)

Terrebonne Parish, Louisiana

SUMMARY OF TEST RESULTS - BORING B-04

LELAP Lab ID #10001

| |
|-------------|
| Project No. |
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04.55174066

PLATE B-1d

[illegible]

Notes:

NP = Non-Plastic Material

TYPE OF TEST

U - Unconfined Compression

UU - Unconsolidated - Undrained Triaxial

CU - Consolidated - Undrained Triaxial

TYPE OF FAILURE

A - Bulge

B - Single Shear Plane

C - Multiple Shear Plane

D - Vertical Fracture

OTHER TEST TYPES

C = Consolidation SO = Sulfates

pH = pH

R = Resistivity

Cl = Chlorides



Bayou De Cade Marsh Creation and Ridge Restoration

(TE-0138, Task 1)

Terrebonne Parish, Louisiana

SUMMARY OF TEST RESULTS - BORING B-05

LELAP Lab ID #10001

| | |
|-------------|--|
| Project No. | |
|-------------|--|

04.55174066

PLATE B-1e

| Sample No. | Depth (ft) | Identification Tests | | | | | | | | | Field Shear Strength Estimate | | Miniature Vane Tests | Compression Tests | | | | Other Tests |
|------------|------------|----------------------|-------------------|-----------------------|----------------------|-----------------------|-------------------------|------------------|---------------------|---------------------------|-------------------------------|---------------|----------------------|-------------------|--------------------------|----------------------|-----------------|-------------|
| | | Liquid Limit (%) | Plastic Limit (%) | Plasticity Index (PI) | Moisture Content (%) | Dry Unit Weight (pcf) | Total Unit Weight (pcf) | Specific Gravity | Organic Content (%) | Passing No. 200 Sieve (%) | Penetrometer (ksf) | Torvane (ksf) | Shear Strength (ksf) | Type Test | Confining Pressure (psi) | Shear Strength (ksf) | Type of Failure | |
| 1 | 0.0-2.0 | 42 | 23 | 19 | 36 | | | | | | | 0.15 | 0.14 | | | | | |
| 2 | 2.0-4.0 | | | | 47 | | | 2.533 | | | | 0.05 | 0.14 | | | | | C |
| 3 | 4.0-6.0 | | | | 35 | 88 | 119 | | | | | 0.10 | 2.17 | UU | 3 | 0.33 | A | |
| 4 | 6.5-8.0 | 41 | 17 | 24 | | | | | | | | | | | | | | |
| 5 | 8.0-10.0 | | | | 43 | 81 | 115 | | | | | | 0.47 | UU | 3 | 0.60 | C | |
| 6 | 10.0-12.0 | | | | 40 | | | | | | | 0.20 | 0.43 | | | | | |
| 7 | 12.0-14.0 | 47 | 18 | 29 | 66 | | | | | | | 0.20 | 0.14 | | | | | |
| 8 | 14.0-16.0 | | | | 66 | 63 | 104 | | | | | 0.25 | 0.18 | UU | 5 | 0.30 | A | |
| 9 | 16.0-18.0 | | | | 52 | | | | | | | 0.25 | 0.21 | | | | | |
| 10 | 18.0-20.0 | 36 | 19 | 17 | 62 | | | | | | | 0.25 | 0.54 | | | | | |
| 11 | 23.0-25.0 | | | | 111 | | | | | | | 0.20 | 0.58 | | | | | |
| 12 | 28.0-30.0 | 216 | 49 | 167 | 31 | | | | | | | | 0.61 | | | | | |
| 13 | 33.0-35.0 | | | | 38 | | | | | | | 0.15 | 0.18 | | | | | |
| 14 | 38.0-40.0 | | | | 52 | 73 | 110 | | | | | 0.20 | 0.51 | UU | 11 | 0.54 | C | |
| 15 | 43.0-45.0 | | | | 53 | | | | | | | 0.20 | 0.66 | | | | | |
| 17 | 48.0-50.0 | | | | 67 | 61 | 101 | | | | | 0.20 | 0.72 | UU | 14 | 0.47 | C | |
| 18 | 53.0-55.0 | 98 | 30 | 68 | | | | | | | | 0.25 | 0.99 | | | | | |
| 19 | 58.0-60.0 | | | | 52 | | | | | | | 0.20 | 0.75 | | | | | |
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Notes:

NP = Non-Plastic Material

TYPE OF TEST

U - Unconfined Compression
 UU - Unconsolidated - Undrained Triaxial
 CU - Consolidated - Undrained Triaxial

TYPE OF FAILURE

A - Bulge
 B - Single Shear Plane
 C - Multiple Shear Plane
 D - Vertical Fracture

OTHER TEST TYPES

C = Consolidation SO = Sulfates
 pH = pH
 R = Resistivity
 Cl = Chlorides



Bayou De Cade Marsh Creation and Ridge Restoration

SUMMARY OF TEST RESULTS - BORING B-06

(TE-0138, Task 1)

LELAP Lab ID #10001

Terrebonne Parish, Louisiana

 Project No.
04.55174066

PLATE B-1f

[illegible]

Notes:

NP = Non-Plastic Material

TYPE OF TEST

U - Unconfined Compression
UU - Unconsolidated - Undrained Triaxial
CU - Consolidated - Undrained Triaxial

TYPE OF FAILURE

A - Bulge
B - Single Shear Plane
C - Multiple Shear Plane
D - Vertical Fracture

OTHER TEST TYPES

C = Consolidation SO = Sulfates
pH = pH
R = Resistivity
Cl = Chlorides



Bayou De Cade Marsh Creation and Ridge Restoration

(TE-0138, Task 1)

Terrebonne Parish, Louisiana

SUMMARY OF TEST RESULTS - BORING B-07

LELAP Lab ID #10001

| | |
|-------------|-------------|
| Project No. | 04.55174066 |
|-------------|-------------|

PLATE B-1g

[illegible]

Notes:

NP = Non-Plastic Material

TYPE OF TEST

U - Unconfined Compression

UU - Unconsolidated - Undrained Triaxial

CU - Consolidated - Undrained Triaxial

TYPE OF FAILURE

A - Bulge

B - Single Shear Plane

C - Multiple Shear Plane

D - Vertical Fracture

OTHER TEST TYPES

C = Consolidation SO = Sulfates

pH = pH

R = Resistivity

Cl = Chlorides



Bayou De Cade Marsh Creation and Ridge Restoration

(TE-0138, Task 1)

Terrebonne Parish, Louisiana

SUMMARY OF TEST RESULTS - BORING B-08

LELAP Lab ID #10001

| | |
|-------------|--|
| Project No. | |
|-------------|--|

04.55174066

PLATE B-1h

[illegible]

Notes:

NP = Non-Plastic Material

TYPE OF TEST

U - Unconfined Compression

UU - Unconsolidated - Undrained Triaxial

CU - Consolidated - Undrained Triaxial

TYPE OF FAILURE

A - Bulge

B - Single Shear Plane

C - Multiple Shear Plane

D - Vertical Fracture

OTHER TEST TYPES

C = Consolidation SO = Sulfates

pH = pH

R = Resistivity

Cl = Chlorides



Bayou De Cade Marsh Creation and Ridge Restoration

(TE-0138, Task 1)

Terrebonne Parish, Louisiana

SUMMARY OF TEST RESULTS - BORING B-09

LELAP Lab ID #10001

| | |
|-------------|--|
| Project No. | |
|-------------|--|

04.55174066

PLATE B-1i

[illegible]

Notes:

NP = Non-Plastic Material

TYPE OF TEST

U - Unconfined Compression
UU - Unconsolidated - Undrained Triaxial
CU - Consolidated - Undrained Triaxial

TYPE OF FAILURE

A - Bulge
B - Single Shear Plane
C - Multiple Shear Plane
D - Vertical Fracture

OTHER TEST TYPES

C = Consolidation SO = Sulfates
pH = pH
R = Resistivity
Cl = Chlorides



Bayou De Cade Marsh Creation and Ridge Restoration

(TE-0138, Task 1)

Terrebonne Parish, Louisiana

SUMMARY OF TEST RESULTS - BORING B-10

LELAP Lab ID #10001

| | |
|-------------|-------------|
| Project No. | 04.55174066 |
|-------------|-------------|

PLATE B-1j

[illegible]

Notes:

NP = Non-Plastic Material

TYPE OF TEST

U - Unconfined Compression
UU - Unconsolidated - Undrained Triaxial
CU - Consolidated - Undrained Triaxial

TYPE OF FAILURE

A - Bulge
B - Single Shear Plane
C - Multiple Shear Plane
D - Vertical Fracture

OTHER TEST TYPES

C = Consolidation SO = Sulfates
pH = pH
R = Resistivity
Cl = Chlorides



Bayou De Cade Marsh Creation and Ridge Restoration

(TE-0138, Task 1)

Terrebonne Parish, Louisiana

SUMMARY OF TEST RESULTS - BORING B-11

LELAP Lab ID #10001

| | |
|-------------|-------------|
| Project No. | 04.55174066 |
|-------------|-------------|

PLATE B-1k

| | | | |
|---------------------------|--|--------------------------|---------------------------------|
| Notes: | TYPE OF TEST | TYPE OF FAILURE | OTHER TEST TYPES |
| NP = Non-Plastic Material | U - Unconfined Compression | A - Bulge | C = Consolidation SO = Sulfates |
| | UU - Unconsolidated - Undrained Triaxial | B - Single Shear Plane | pH = pH |
| | CU - Consolidated - Undrained Triaxial | C - Multiple Shear Plane | R = Resistivity |
| | | D - Vertical Fracture | Cl = Chlorides |

PLATE B-11

[illegible]

(TE-0138, Task 1)

Terrebonne Parish, Louisiana

PLATE B-1m

[illegible]

[illegible]

Notes:

NP = Non-Plastic Material

TYPE OF TEST

U - Unconfined Compression
UU - Unconsolidated - Undrained Triaxial
CU - Consolidated - Undrained Triaxial

TYPE OF FAILURE

A - Bulge
B - Single Shear Plane
C - Multiple Shear Plane
D - Vertical Fracture

OTHER TEST TYPES

C = Consolidation SO = Sulfates
pH = pH
R = Resistivity
Cl = Chlorides



Bayou De Cade Marsh Creation and Ridge Restoration

(TE-0138, Task 1)

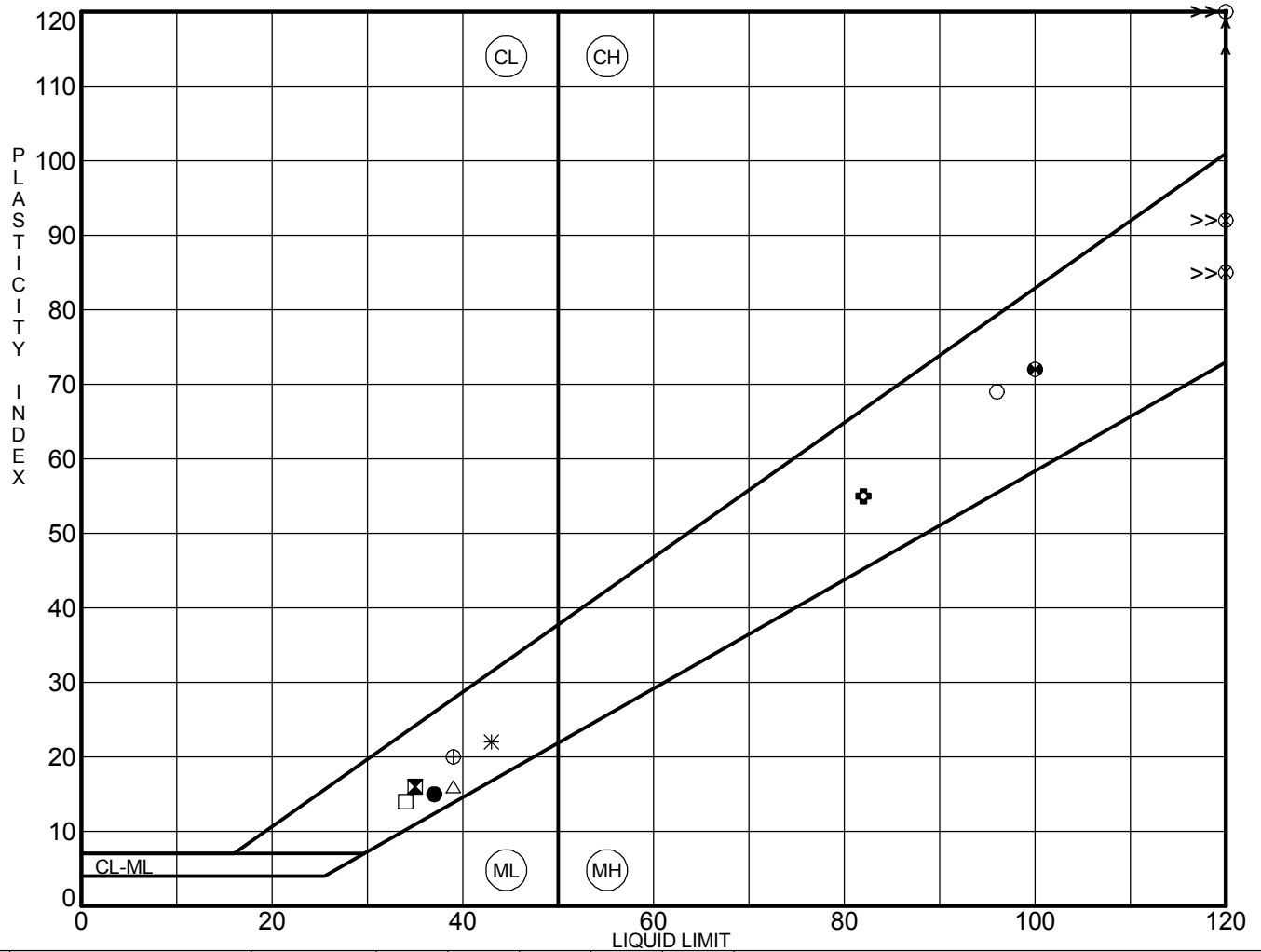
Terrebonne Parish, Louisiana

SUMMARY OF TEST RESULTS - BORING B-15

LELAP Lab ID #10001

| | |
|-------------|-------------|
| Project No. | 04.55174066 |
|-------------|-------------|

PLATE B-1o



| | Sample Source | Sample ID | Depth (ft) | LL | PL | PI | Fines | Visual Classification |
|---|---------------|-----------|------------|-----|-----|-----|-------|--|
| ● | B-01 | 1a | 1.00 | 37 | 22 | 15 | | LEAN CLAY WITH SAND, gray, with silt pockets |
| ⊠ | B-01 | 3 | 4.00 | 35 | 19 | 16 | | |
| * | B-01 | 9 | 16.00 | 43 | 21 | 22 | | SILTY, SANDY CLAY, gray |
| ⊗ | B-01 | 11 | 23.00 | 126 | 34 | 92 | | ORGANIC CLAY, black and gray |
| ⊙ | B-01 | 12 | 28.00 | 473 | 321 | 152 | | |
| ⊕ | B-01 | 16 | 48.00 | 82 | 27 | 55 | | |
| ○ | B-01 | 18 | 58.00 | 96 | 27 | 69 | | |
| △ | B-02 | 2 | 2.00 | 39 | 23 | 16 | | LEAN CLAY, gray |
| ⊗ | B-02 | 8 | 14.00 | 121 | 36 | 85 | | ORGANIC CLAY, black |
| ⊕ | B-02 | | 24.00 | 39 | 19 | 20 | | LEAN CLAY, gray |
| □ | B-02 | 15 | 43.00 | 34 | 20 | 14 | | LEAN CLAY, gray |
| ⊙ | B-02 | 18 | 58.00 | 100 | 28 | 72 | | FAT CLAY, gray |

Remarks: All tests were performed in general accordance with ASTM Standards D4318, D421, D2217, and D1140. Fines column represent % passing No. 200 sieve.

Note:



Bayou De Cade Marsh Creation and Ridge Restoration

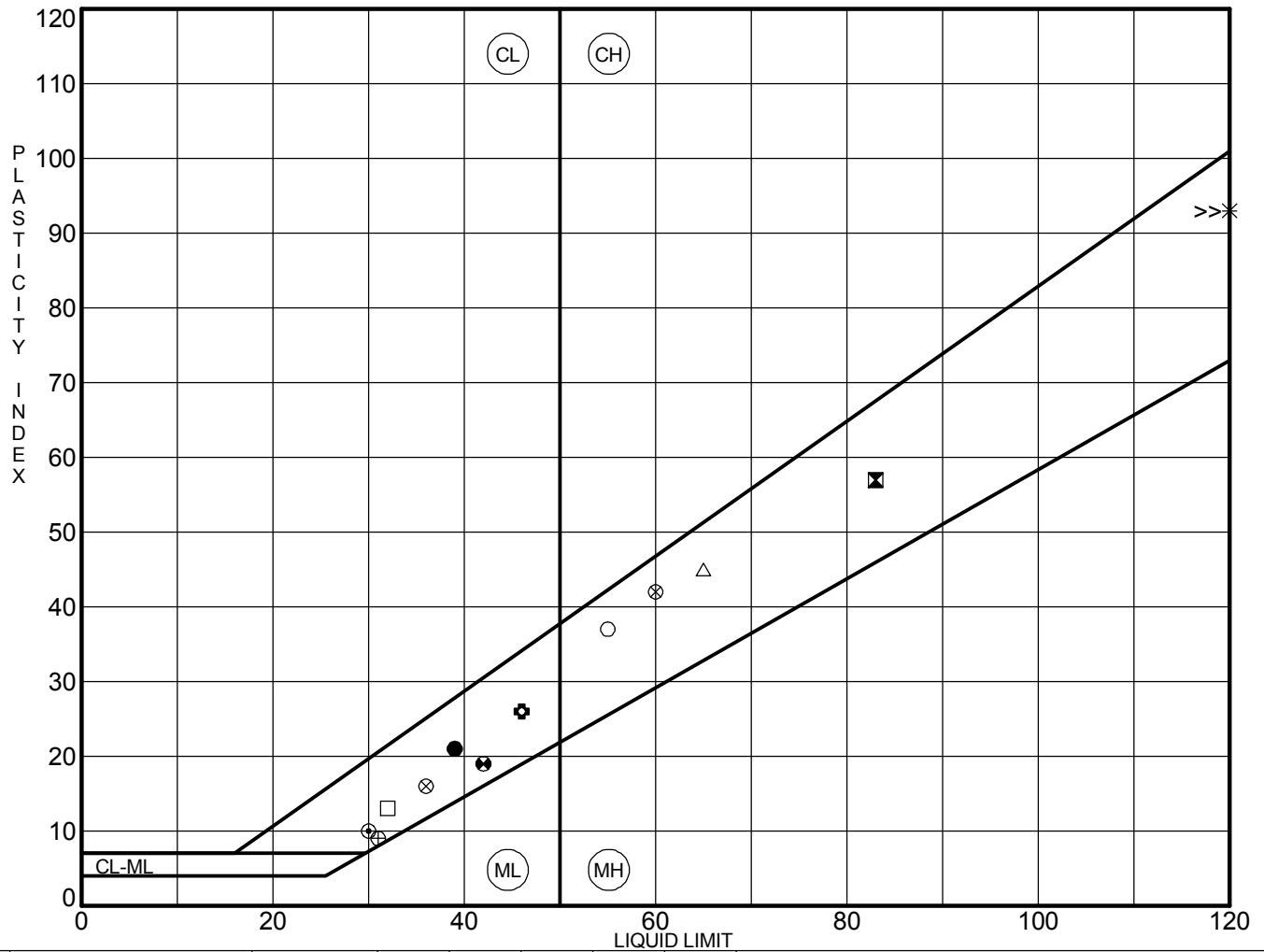
(TE-0138, Task 1)

Terrebonne Parish, Louisiana

ATTERBERG LIMITS' RESULTS

Project No.
04.55174066

PLATE B-2a



| | Sample Source | Sample ID | Depth (ft) | LL | PL | PI | Fines | Visual Classification |
|---|---------------|-----------|------------|-----|----|----|-------|---|
| ● | B-03 | 8 | 14.00 | 39 | 18 | 21 | | LEAN CLAY, gray |
| ⊠ | B-03 | 17 | 53.00 | 83 | 26 | 57 | | FAT CLAY, dark gray |
| ✱ | B-04 | 1 | 0.00 | 127 | 34 | 93 | | ORGANIC CLAY, black |
| ⊗ | B-04 | 3 | 4.00 | 60 | 18 | 42 | | FAT CLAY, gray |
| ⊙ | B-04 | 12 | 28.00 | 30 | 20 | 10 | | LEAN CLAY, gray, with silt |
| ⊕ | B-04 | 14 | 48.00 | 46 | 20 | 26 | | LEAN CLAY, gray |
| ○ | B-05 | 1 | 0.00 | 55 | 18 | 37 | | FAT CLAY, dark gray |
| △ | B-05 | 3 | 4.00 | 65 | 20 | 45 | | FAT CLAY, dark gray |
| ⊗ | B-05 | 7 | 12.50 | 36 | 20 | 16 | | LEAN CLAY, gray, with silt pockets and organics |
| ⊕ | B-05 | 10 | 18.00 | 31 | 22 | 9 | | SILT, gray, with clay pockets |
| □ | B-05 | 13 | 33.00 | 32 | 19 | 13 | | SILT, gray, with clay pockets |
| ⊙ | B-06 | 1 | 0.00 | 42 | 23 | 19 | | LEAN CLAY, gray with sand |

Remarks: All tests were performed in general accordance with ASTM Standards D4318, D421, D2217, and D1140. Fines column represent % passing No. 200 sieve.

Note:



Bayou De Cade Marsh Creation and Ridge Restoration

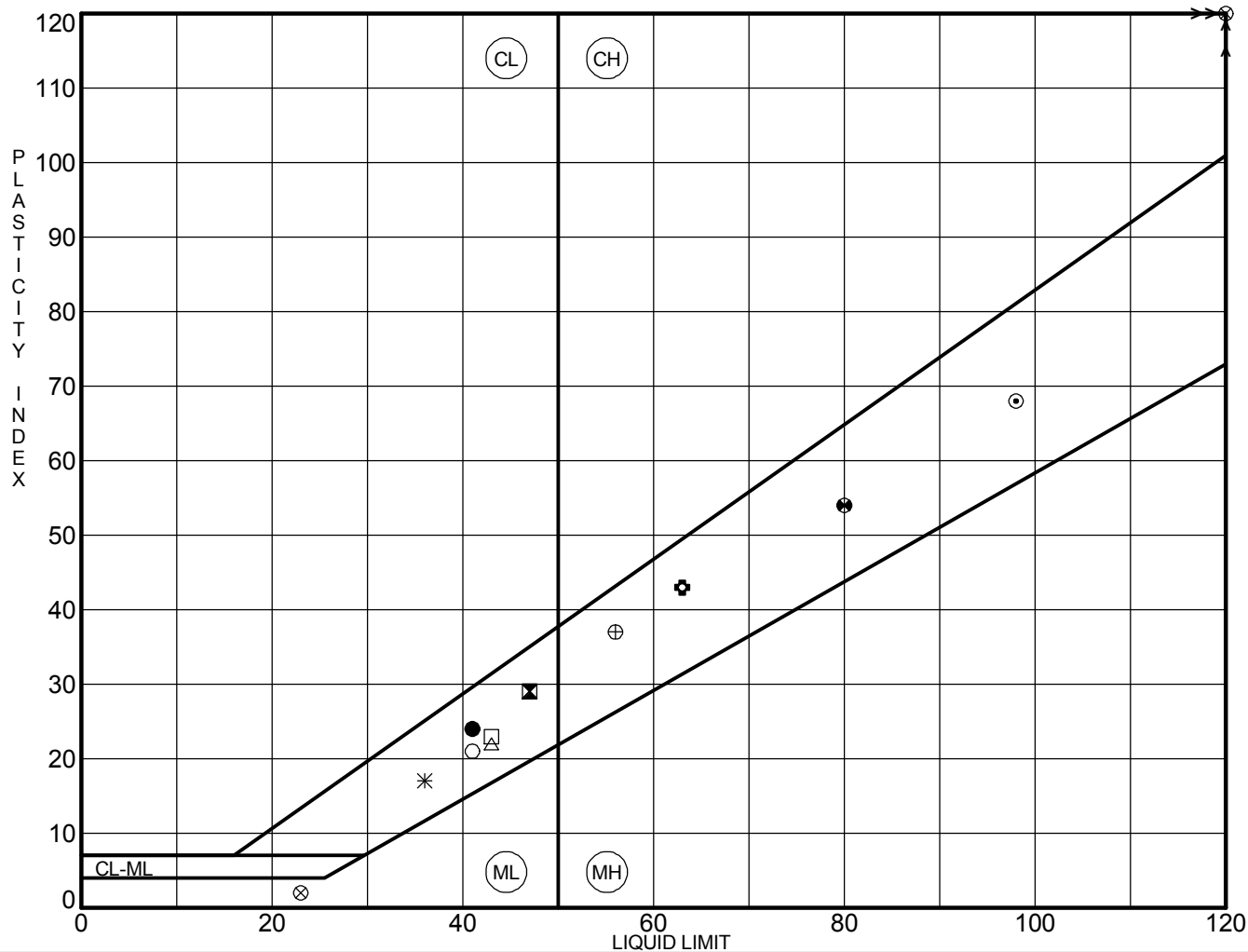
(TE-0138, Task 1)

Terrebonne Parish, Louisiana

ATTERBERG LIMITS' RESULTS

Project No.
04.55174066

PLATE B-2b



| | Sample Source | Sample ID | Depth (ft) | LL | PL | PI | Fines | Visual Classification |
|---|---------------|-----------|------------|-----|----|-----|-------|----------------------------|
| ● | B-06 | 4 | 6.50 | 41 | 17 | 24 | | LEAN CLAY, gray |
| ⊗ | B-06 | 7 | 12.00 | 47 | 18 | 29 | | |
| * | B-06 | 10 | 18.00 | 36 | 19 | 17 | | LEAN CLAY, gray, with silt |
| ⊗ | B-06 | 12 | 28.00 | 216 | 49 | 167 | | PEAT, black |
| ⊙ | B-06 | 18 | 53.00 | 98 | 30 | 68 | | FAT CLAY, gray |
| ⊕ | B-07 | 3 | 4.00 | 63 | 20 | 43 | | FAT CLAY, gray |
| ○ | B-07 | 6 | 10.00 | 41 | 20 | 21 | | LEAN CLAY, gray, with silt |
| △ | B-07 | 11 | 23.00 | 43 | 21 | 22 | | LEAN CLAY, gray |
| ⊗ | B-08 | 2 | 2.00 | 23 | 21 | 2 | | SILT, gray, with clay |
| ⊕ | B-08 | 5 | 8.00 | 56 | 19 | 37 | | FAT CLAY, gray |
| □ | B-08 | 8 | 14.00 | 43 | 20 | 23 | | LEAN CLAY, gray |
| ⊕ | B-08 | 11 | 23.00 | 80 | 26 | 54 | | FAT CLAY, gray |

Remarks: All tests were performed in general accordance with ASTM Standards D4318, D421, D2217, and D1140. Fines column represent % passing No. 200 sieve.

Note:



Bayou De Cade Marsh Creation and Ridge Restoration

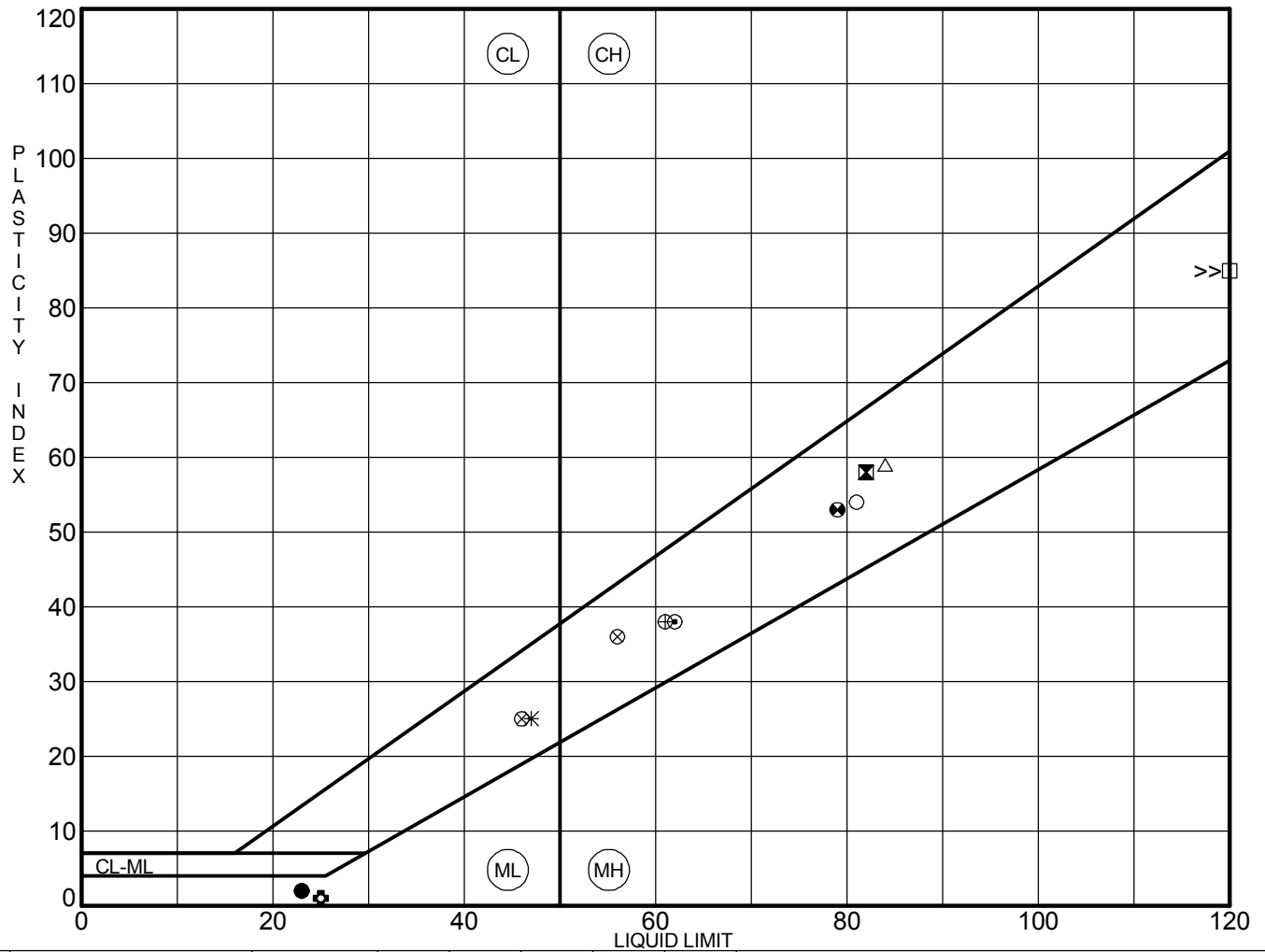
(TE-0138, Task 1)

Terrebonne Parish, Louisiana

ATTERBERG LIMITS' RESULTS

Project No.
04.55174066

PLATE B-2c



| | Sample Source | Sample ID | Depth (ft) | LL | PL | PI | Fines | Visual Classification |
|---|---------------|-----------|------------|-----|----|----|-------|------------------------------------|
| ● | B-08 | 14 | 38.00 | 23 | 21 | 2 | | SILT, gray, with some clay |
| ⊠ | B-09 | 1 | 0.00 | 82 | 24 | 58 | | FAT CLAY, black, with organics |
| ✱ | B-09 | 5 | 8.00 | 47 | 22 | 25 | | LEAN CLAY, gray |
| ⊗ | B-09 | 6 | 10.00 | 46 | 21 | 25 | | |
| ⊙ | B-09 | 9 | 16.00 | 62 | 24 | 38 | | FAT CLAY, gray |
| ⊕ | B-10 | 4 | 6.00 | 25 | 24 | 1 | | SILT, gray, with clay |
| ○ | B-10 | 6 | 10.00 | 81 | 27 | 54 | | FAT CLAY, gray, with organics |
| △ | B-11 | 3 | 4.00 | 84 | 25 | 59 | | FAT CLAY, gray, with sand |
| ⊗ | B-11 | 7 | 12.00 | 56 | 20 | 36 | | FAT CLAY, gray |
| ⊕ | B-12 | 2 | 2.00 | 61 | 23 | 38 | | FAT CLAY, gray |
| □ | B-13 | 6 | 10.00 | 123 | 38 | 85 | | FAT CLAY, dark gray, with organics |
| ⊕ | B-14 | 2 | 2.00 | 79 | 26 | 53 | | FAT CLAY, gray |

Remarks: All tests were performed in general accordance with ASTM Standards D4318, D421, D2217, and D1140. Fines column represent % passing No. 200 sieve.

Note:



Bayou De Cade Marsh Creation and Ridge Restoration

(TE-0138, Task 1)

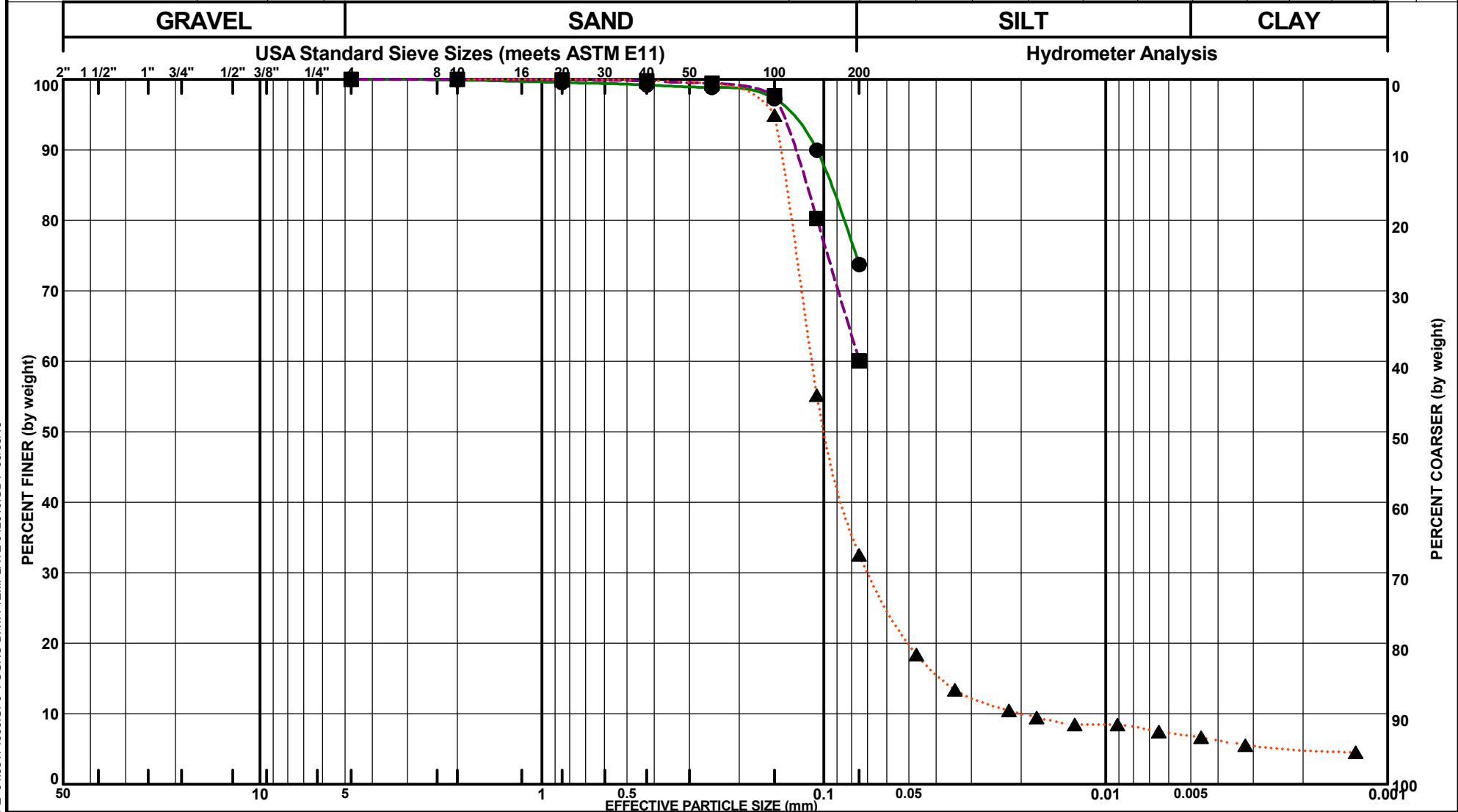
Terrebonne Parish, Louisiana

ATTERBERG LIMITS' RESULTS

Project No.
04.55174066

PLATE B-2d

| Boring Number | Sample Number | Depth (ft) | Material Description | %Gravel | %Sand | %Silt | %Clay | D100 | D60 | D30 | D10 | Cc | Cu | LL | PL | PI |
|---------------|---------------|------------|---|---------|-------|-------|-------|------|-------|-------|------|------|------|----|----|----|
| ● B-01 | 2a | 2-3 | LEAN CLAY WITH SAND (CL), gray, with silt pockets | 0.0 | 26.3 | | | 4.75 | | | | | | | | |
| ■ B-02 | 3 | 4-6 | SANDY LEAN CLAY (CL), dark gray | 0.0 | 39.9 | | | 4.75 | | | | | | | | |
| ▲ B-02 | 5 | 8.5-10 | SILTY SAND (SM), gray | 0.0 | 67.4 | 25.7 | 6.8 | 2 | 0.111 | 0.069 | 0.02 | 2.15 | 5.53 | | | |



Bayou De Cade Marsh Creation and Ridge Restoration

Terrebonne Parish, Louisiana

Tested By:

Allen Bentley

Date Tested:

4/23/2018

Reviewed By:

Adam Linson

Date Reviewed:

4/26/2018

Project No.

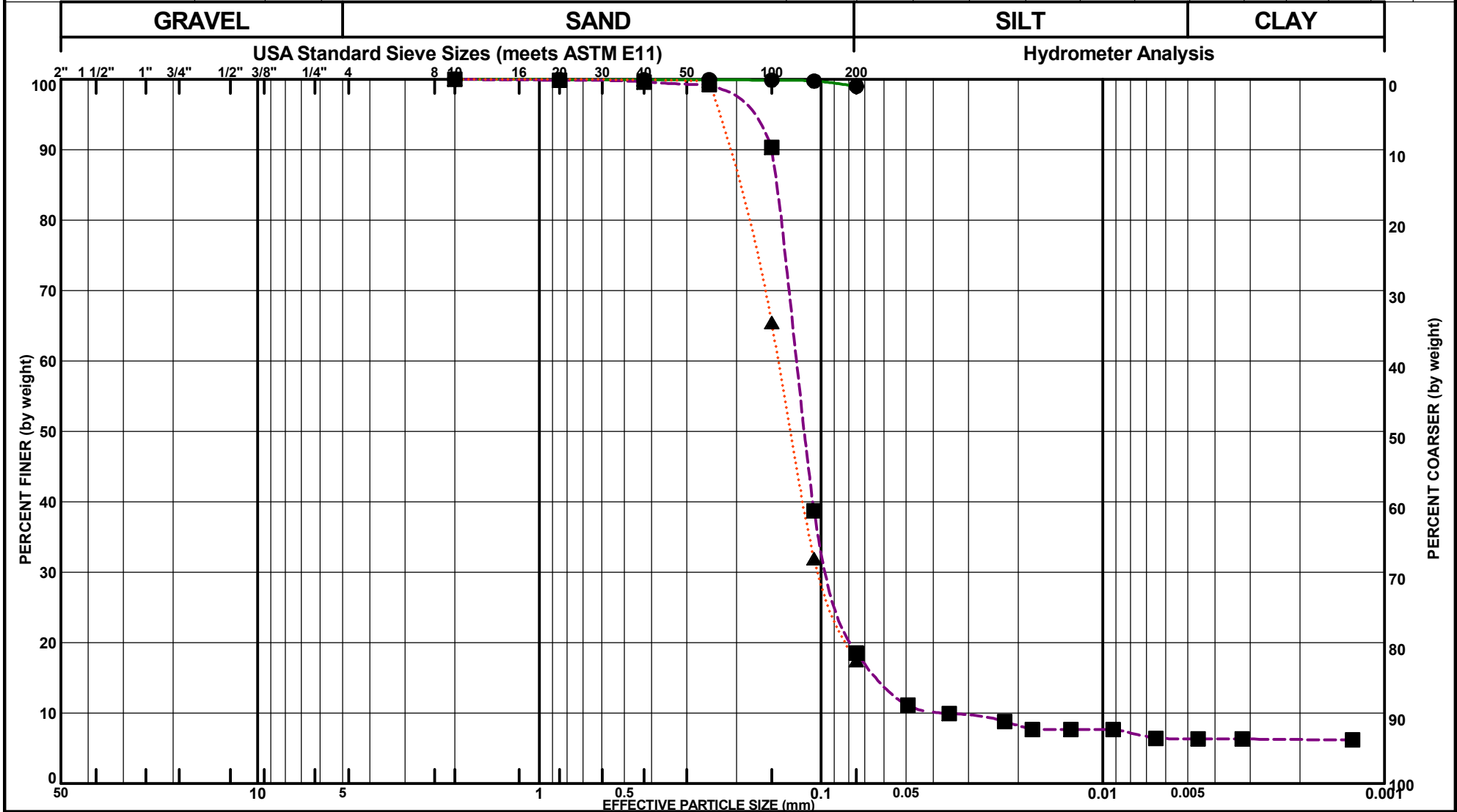
04.55174066

PARTICLE-SIZE ANALYSIS

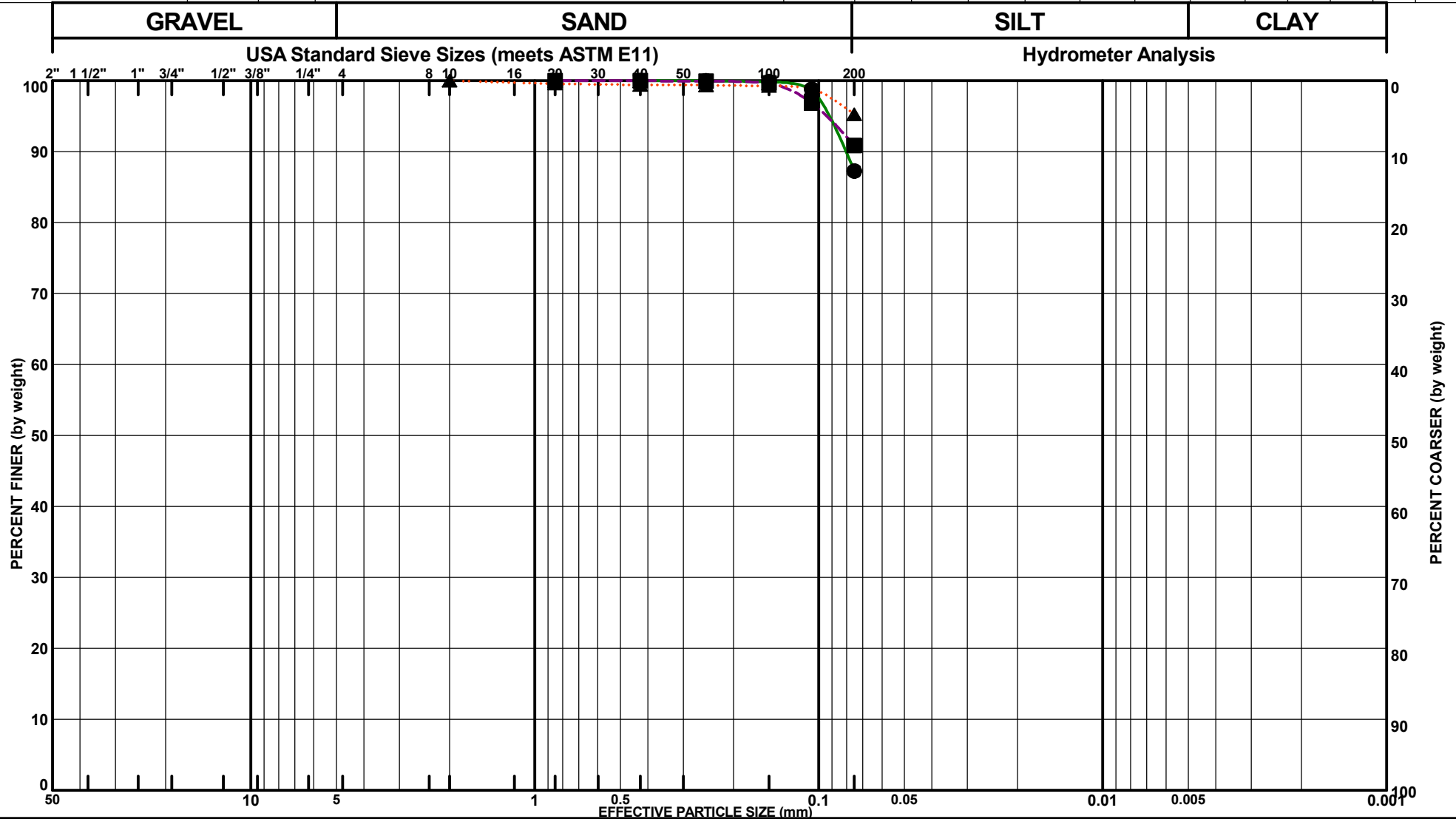
ASTM D422/D6913/C136

PLATE B-3a

| Boring Number | Sample Number | Depth (ft) | Material Description | %Gravel | %Sand | %Silt | %Clay | D100 | D60 | D30 | D10 | Cc | Cu | LL | PL | PI |
|---------------|---------------|------------|--|---------|-------|-------|-------|------|-------|-------|-------|------|------|----|----|----|
| ● B-02 | 14 | 38-40 | SILT (ML), gray, with clay laminations | 0.0 | 1.0 | | | 2 | | | | | | | | |
| ■ B-03 | 4 | 6-7.5 | SILTY SAND (SM), gray | 0.0 | 81.5 | 12.2 | 6.3 | 2 | 0.122 | 0.091 | 0.035 | 1.92 | 3.45 | | | |
| ▲ B-03 | 6 | 10-11.5 | SILTY SAND (SM), gray | 0.0 | 82.5 | | | 2 | 0.142 | 0.101 | | | | | | |

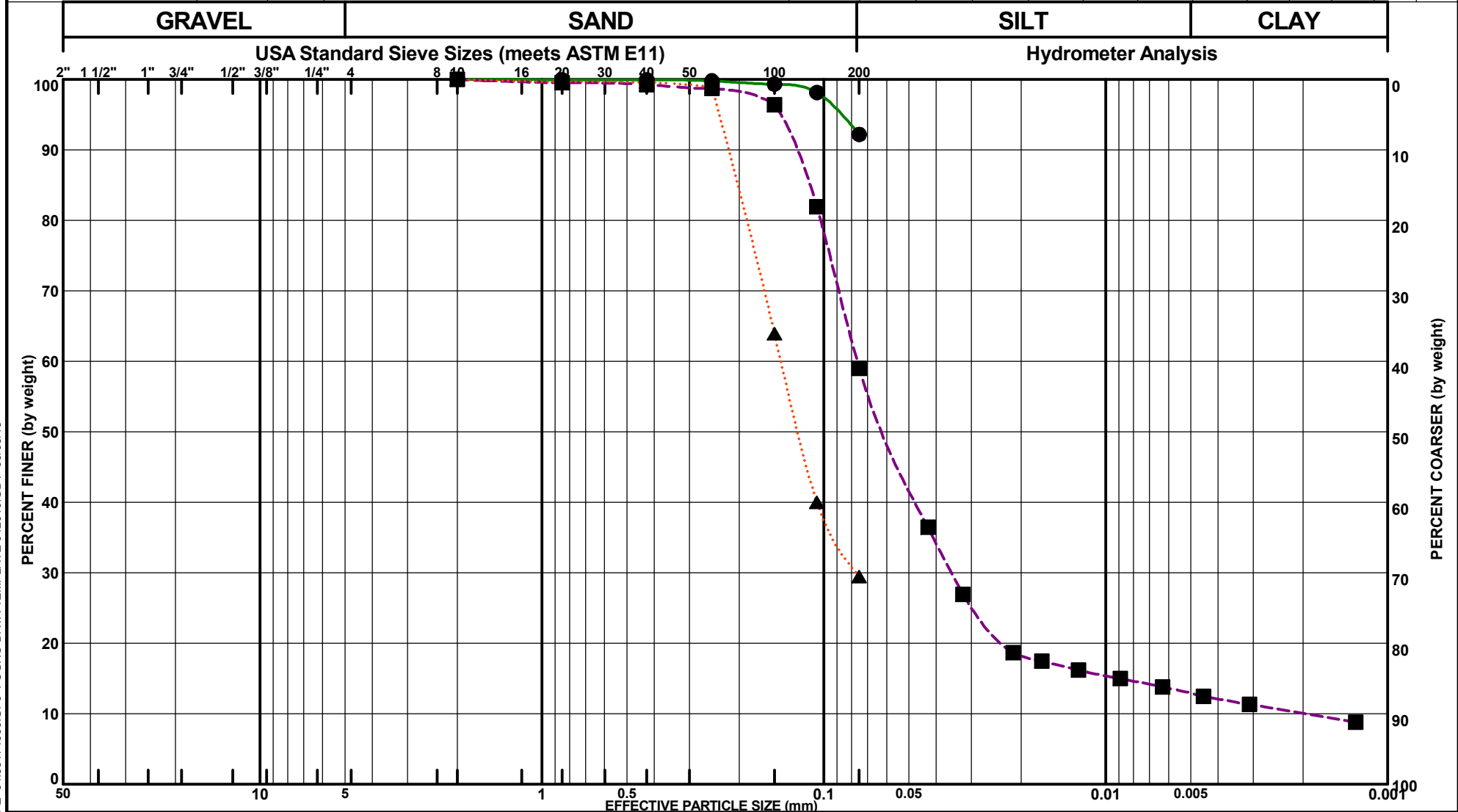


| Boring Number | Sample Number | Depth (ft) | Material Description | %Gravel | %Sand | %Silt | %Clay | D100 | D60 | D30 | D10 | Cc | Cu | LL | PL | PI |
|---------------|---------------|------------|--|---------|-------|-------|-------|-------|-----|-----|-----|----|----|----|----|----|
| ● B-03 | 12 | 28-30 | SILT (ML), gray, with clay and sand seams | 0.0 | 12.7 | | | 0.425 | | | | | | | | |
| ■ B-03 | 13 | 33-35 | FAT CLAY (CH), gray | 0.0 | 9.1 | | | 0.85 | | | | | | | | |
| ▲ B-05 | 6 | 10-12 | LEAN CLAY (CL), gray, with sand layers and ferrous nodules | 0.0 | 4.7 | | | 2 | | | | | | | | |



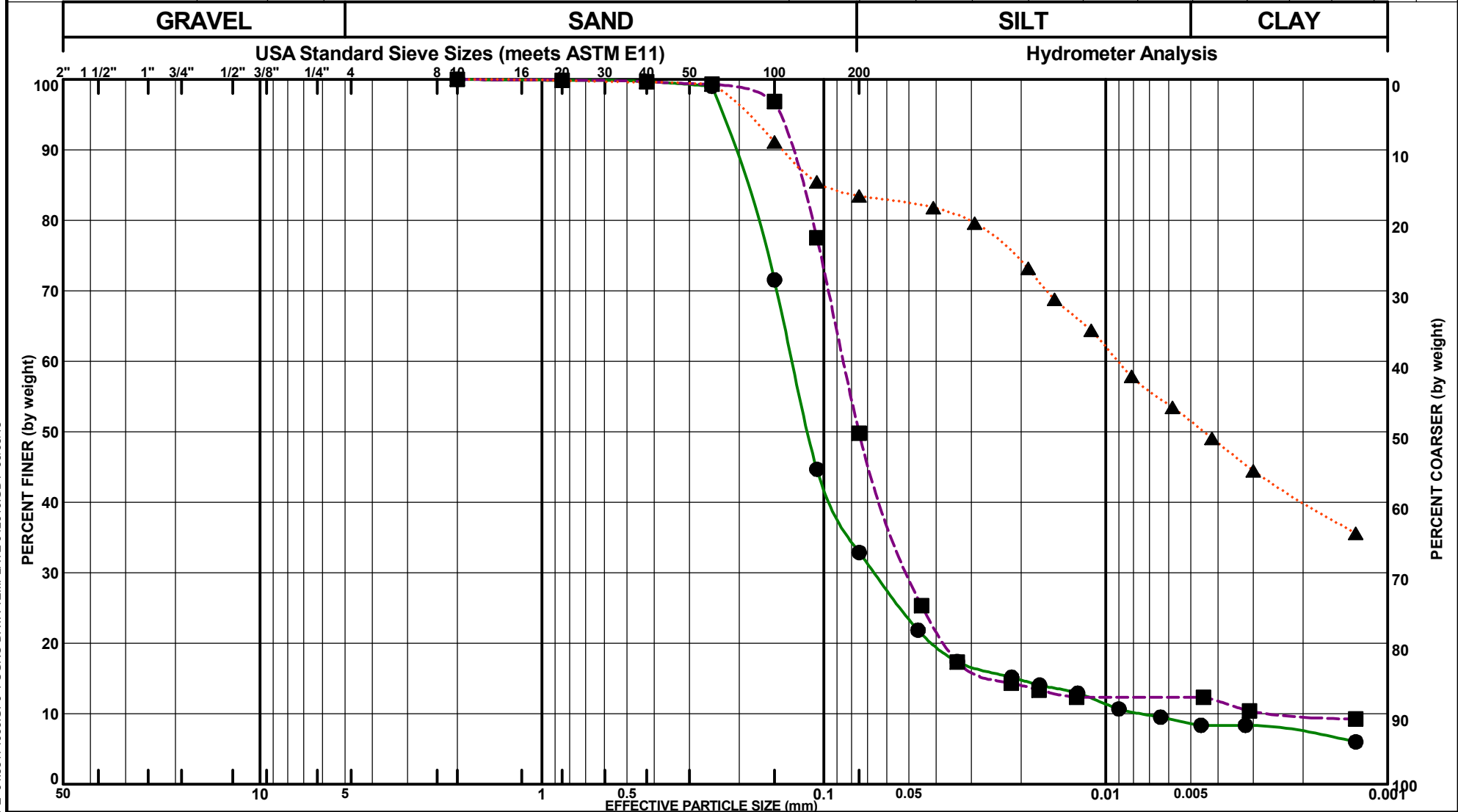
Bayou De Cade Marsh Creation and Ridge Restoration

| Boring Number | Sample Number | Depth (ft) | Material Description | %Gravel | %Sand | %Silt | %Clay | D100 | D60 | D30 | D10 | Cc | Cu | LL | PL | PI |
|---------------|---------------|------------|---|---------|-------|-------|-------|------|-------|-------|-------|------|-------|----|----|----|
| ● B-07 | 14 | 38-40 | SILT (ML), gray, with sand pockets and clay seams | 0.0 | 7.8 | | | 2 | | | | | | | | |
| ■ B-08 | 1 | 0-2 | SANDY SILT (ML), gray, with clay traces | 0.0 | 41.0 | 46.1 | 12.9 | 2 | 0.076 | 0.035 | 0.002 | 8.25 | 38.58 | | | |
| ▲ B-08 | 4 | 5.99-6 | SILTY SAND (SM), gray, with clay pockets | 0.0 | 70.5 | | | 2 | 0.142 | 0.076 | | | | | | |



| | | | | | | |
|--|--|--------------|--------------|----------------|-------------------------------|------------|
| | Bayou De Cade Marsh Creation and Ridge Restoration | | | | PARTICLE-SIZE ANALYSIS | |
| | Terrebonne Parish, Louisiana | | | | ASTM D422/D6913/C136 | |
| | Tested By: | Date Tested: | Reviewed By: | Date Reviewed: | Project No. | PLATE B-3d |
| | Allen Bentley | 5/3/2018 | Adam Linson | 5/7/2018 | 04.55174066 | |

| Boring Number | Sample Number | Depth (ft) | Material Description | %Gravel | %Sand | %Silt | %Clay | D100 | D60 | D30 | D10 | Cc | Cu | LL | PL | PI |
|---------------|---------------|------------|--|---------|-------|-------|-------|------|-------|-------|-------|-------|-------|----|----|----|
| ● B-09 | 3 | 4-5.5 | SILTY SAND (SM), gray, with clay pockets | 0.0 | 67.1 | 24.2 | 8.6 | 2 | 0.129 | 0.066 | 0.007 | 4.59 | 17.50 | | | |
| ■ B-10 | 2 | 2-4 | SILTY SAND (SM), gray, with clay pockets | 0.0 | 50.2 | 37.5 | 12.3 | 2 | 0.085 | 0.05 | 0.002 | 12.46 | 36.62 | | | |
| ▲ B-11 | 2 | 2-4 | FAT CLAY (CH), gray | 0.0 | 16.5 | 32.0 | 51.4 | 2 | 0.009 | | | | | | | |



Bayou De Cade Marsh Creation and Ridge Restoration

Terrebonne Parish, Louisiana

PARTICLE-SIZE ANALYSIS

ASTM D422/D6913/C136

Tested By:

Shamira Serf

Date Tested:

4/14/2018

Reviewed By:

Adam Linson

Date Reviewed:

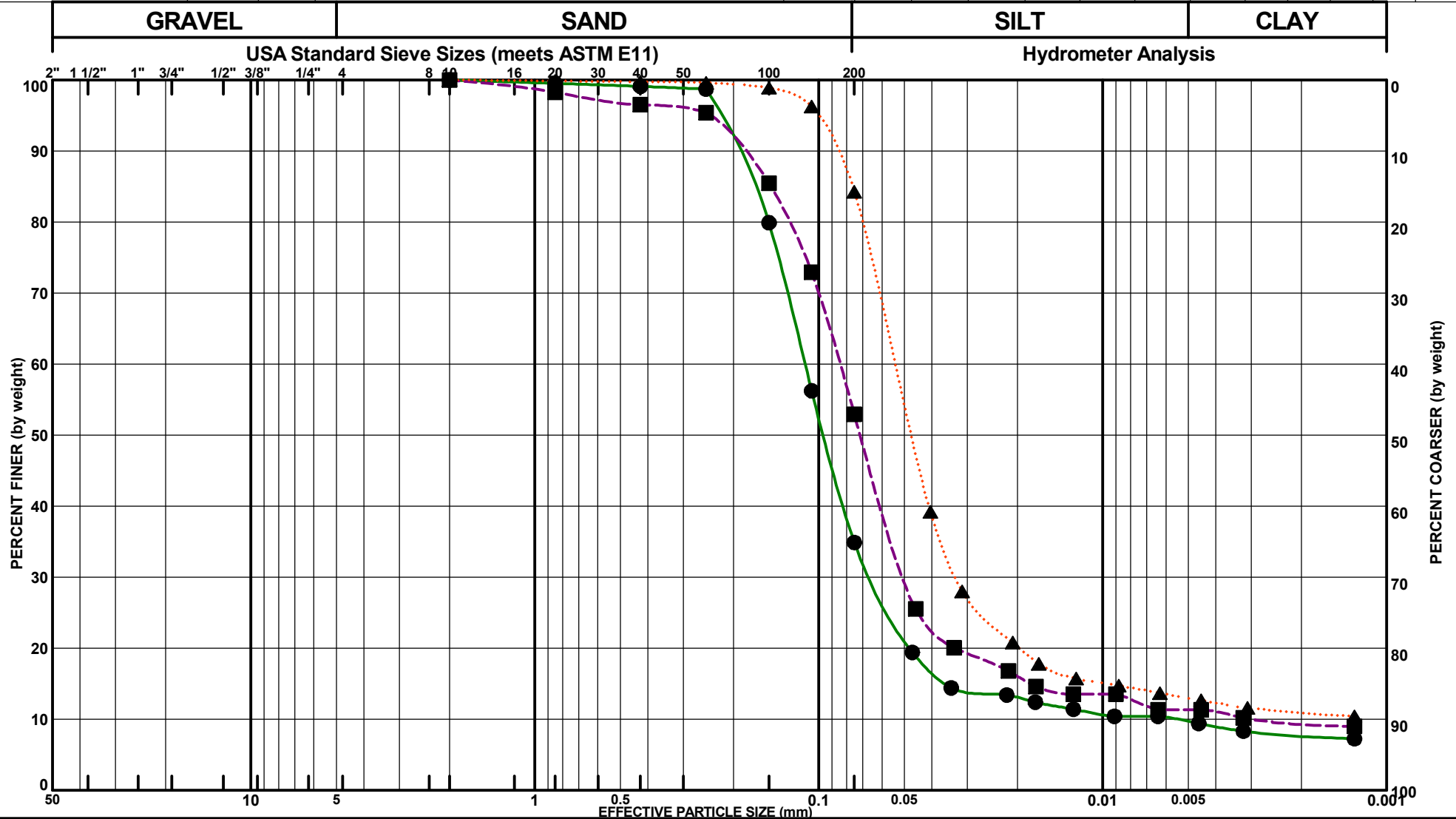
4/20/2018

Project No.

04.55174066

PLATE B-3e

| Boring Number | Sample Number | Depth (ft) | Material Description | %Gravel | %Sand | %Silt | %Clay | D100 | D60 | D30 | D10 | Cc | Cu | LL | PL | PI |
|---------------|---------------|------------|--|---------|-------|-------|-------|------|-------|-------|-------|-------|-------|----|----|----|
| ● B-12 | 4 | 6-7.5 | SILTY SAND (SM), gray, with clay and wood | 0.0 | 65.1 | 25.2 | 9.7 | 2 | 0.112 | 0.065 | 0.006 | 6.67 | 20.02 | | | |
| ■ B-12 | 6 | 10-11.5 | SANDY SILT (ML), gray, with clay pockets and peat layers | 0.0 | 47.1 | 41.6 | 11.3 | 2 | 0.085 | 0.049 | 0.003 | 10.34 | 30.37 | | | |
| ▲ B-13 | 1 | 0-2 | SILT WITH SAND (ML), gray, with clay lenses and organics | 0.0 | 15.7 | 71.3 | 13.0 | 2 | 0.054 | 0.033 | | | | | | |



Bayou De Cade Marsh Creation and Ridge Restoration

Terrebonne Parish, Louisiana

Tested By:

Shamira Serf

Date Tested:

4/16/2018

Reviewed By:

Adam Linson

Date Reviewed:

4/20/2018

Project No.

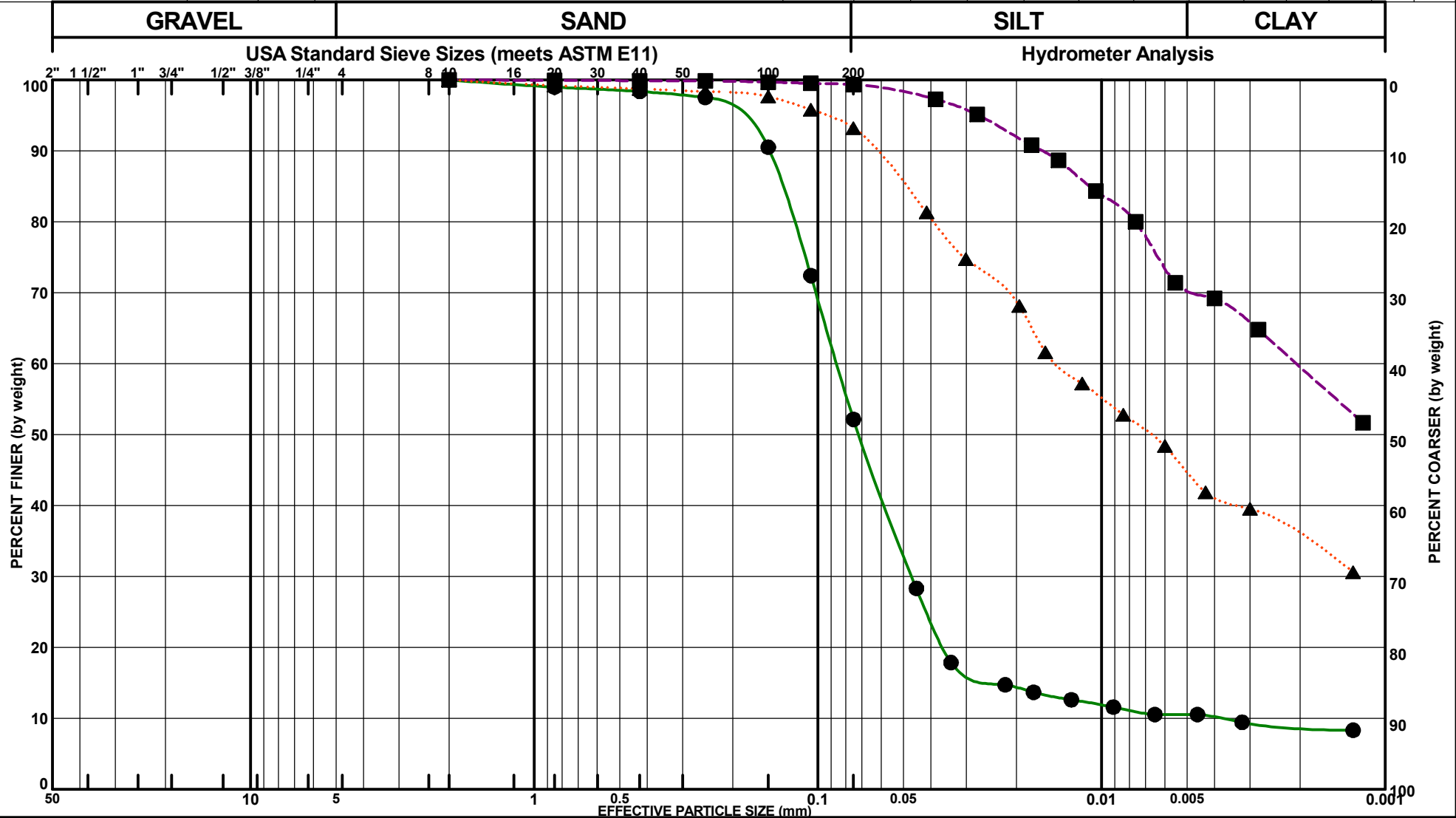
04.55174066

PARTICLE-SIZE ANALYSIS

ASTM D422/D6913/C136

PLATE B-3f

| Boring Number | Sample Number | Depth (ft) | Material Description | %Gravel | %Sand | %Silt | %Clay | D100 | D60 | D30 | D10 | Cc | Cu | LL | PL | PI |
|---------------|---------------|------------|--|---------|-------|-------|-------|------|-------|-------|-------|------|-------|----|----|----|
| ● B-13 | 4 | 6-8 | LEAN CLAY (CL), gray | 0.0 | 47.9 | 41.6 | 10.5 | 2 | 0.086 | 0.047 | 0.004 | 6.59 | 22.25 | | | |
| ■ B-14 | 3 | 4-6 | FAT CLAY (CH), gray | 0.0 | 0.7 | 28.6 | 70.7 | 2 | 0.002 | | | | | | | |
| ▲ B-15 | 2 | 2-4 | FAT CLAY (CH), gray, with gravel and roots | 0.0 | 6.8 | 48.4 | 44.8 | 2 | 0.014 | | | | | | | |



Bayou De Cade Marsh Creation and Ridge Restoration

Terrebonne Parish, Louisiana

Tested By:

Shamira Serf

Date Tested:

4/16/2018

Reviewed By:

Adam Linson

Date Reviewed:

4/20/2018

Project No.

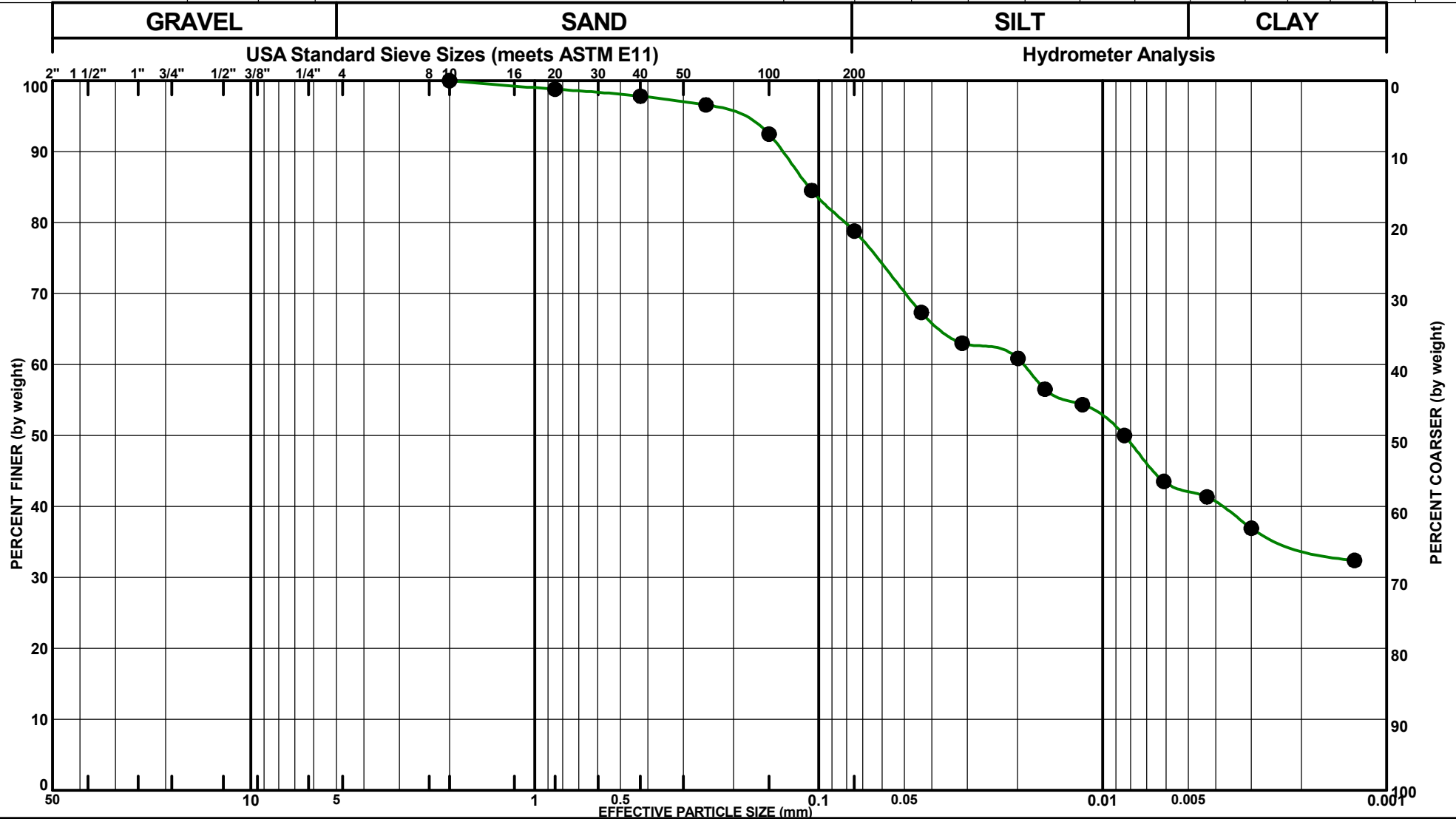
04.55174066

PARTICLE-SIZE ANALYSIS

ASTM D422/D6913/C136

PLATE B-3g

| Boring Number | Sample Number | Depth (ft) | Material Description | %Gravel | %Sand | %Silt | %Clay | D100 | D60 | D30 | D10 | Cc | Cu | LL | PL | PI |
|---------------|---------------|------------|-------------------------------|---------|-------|-------|-------|------|-------|-----|-----|----|----|----|----|----|
| ● B-15 | 5 | 8-10 | FAT CLAY WITH SAND (CH), gray | 0.0 | 21.2 | 36.5 | 42.3 | 2 | 0.019 | | | | | | | |
| ■ | | | | | | | | | | | | | | | | |
| ▲ | | | | | | | | | | | | | | | | |



Bayou De Cade Marsh Creation and Ridge Restoration

Terrebonne Parish, Louisiana

PARTICLE-SIZE ANALYSIS

ASTM D422/D6913/C136

Tested By:

Shamira Serf

Date Tested:

4/16/2018

Reviewed By:

Adam Linson

Date Reviewed:

4/20/2018

Project No.

04.55174066

PLATE B-3h



Project Name: Bayou De Cade Marsh Creation and Ridge Restoration
Terrebonne Parish, Louisiana

Type of Test:
Unconsolidated Undrained ASTM D 2850

Source of Sample: B-01 Depth: 38-40 ft.

Visual Classification:
FAT CLAY (CH), gray, with sand lenses and pockets

Sample Number: 14

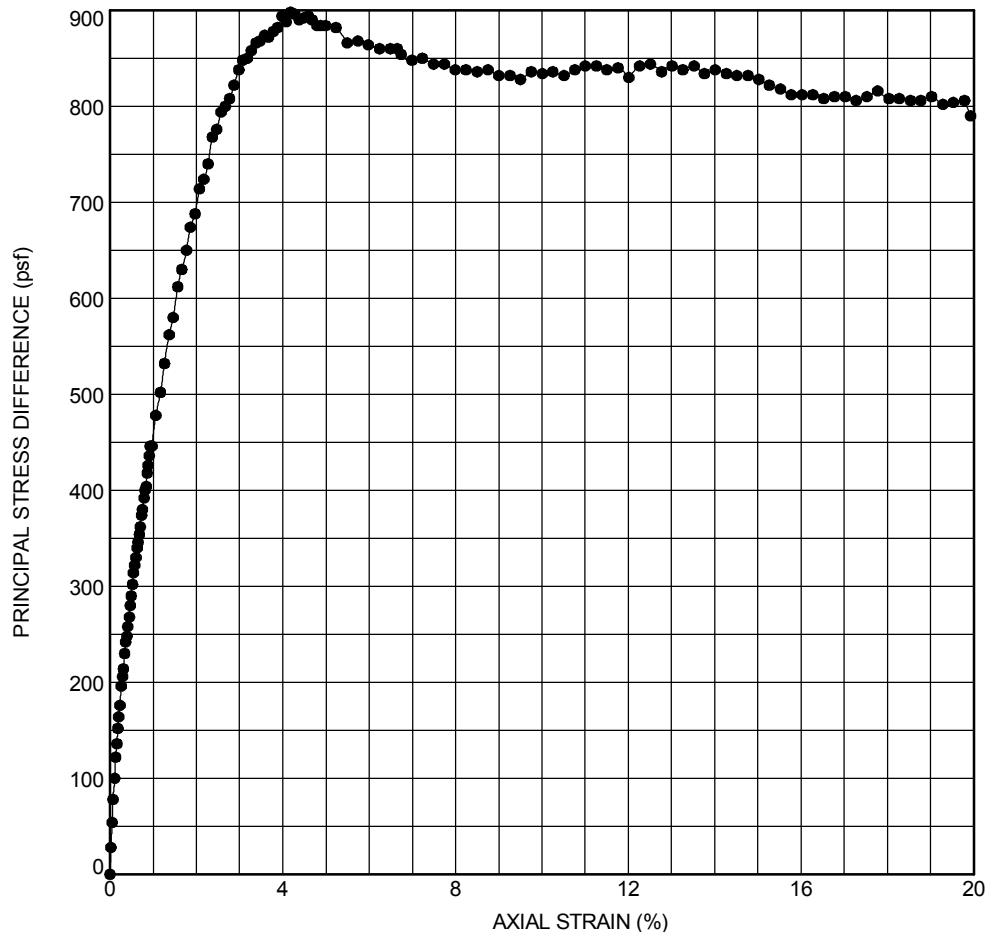
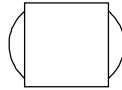
Project No.: 04.55174066 Test Date.: 4/20/2018

Organic Content (%) ASTM D2974: N/A

| Sample No. | 1 ● | 2 ■ | 3 ▲ |
|----------------------------|-------|-----|-----|
| Water Content (%) | 58.9 | | |
| Dry Density (pcf) | 68.9 | | |
| Saturation (%) | 100.0 | | |
| Void Ratio | 1.45 | | |
| Diameter (inches) | 1.41 | | |
| Height (inches) | 2.96 | | |
| % Passing #200 Sieve | | | |
| Specific Gravity (assumed) | 2.70 | | |

Remarks:
Visual classification in general accordance with ASTM Standard D2487.

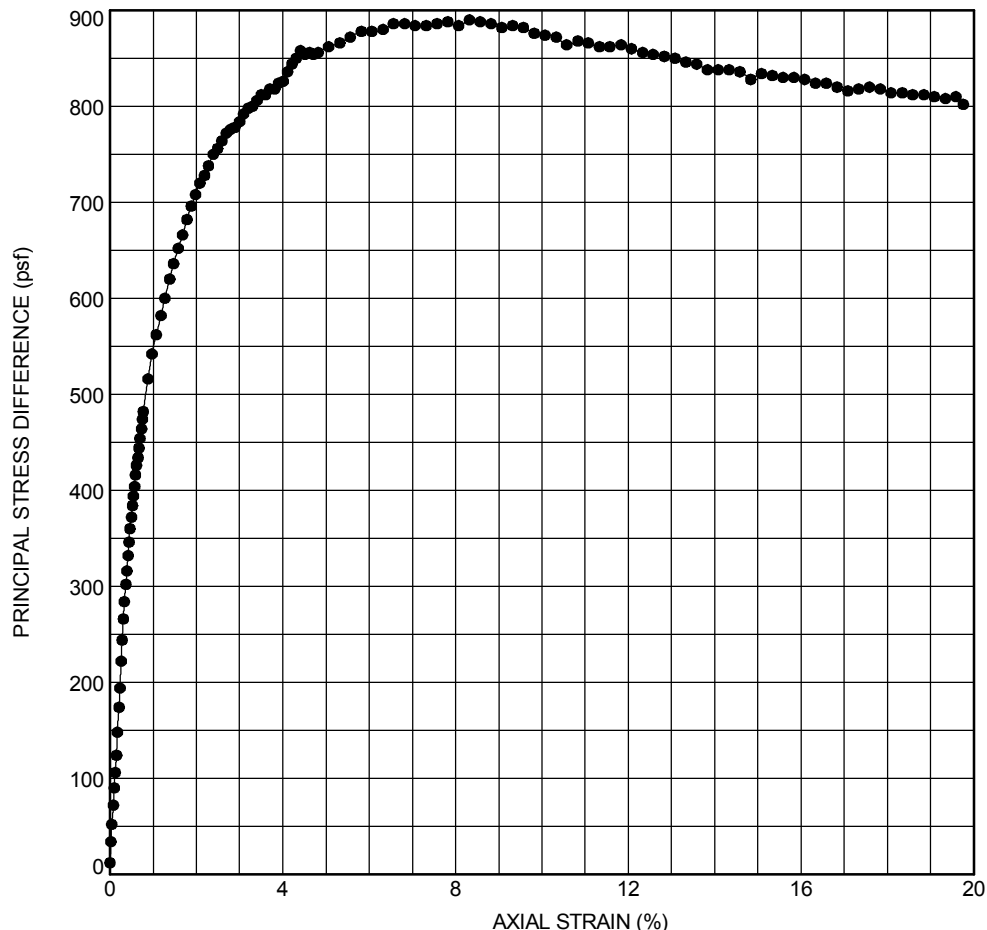
| | | |
|---------------------------|---------|----------------|
| Strain Rate (%/min.) | 1.0 | |
| Cell Pressure (psi) | 11.00 | |
| Deviator Stress (psf) | 898 | |
| Shear Strength (psf) | 449 | |
| Failure Strain (%) | 4.2 | |
| σ_1 Failure (psf): | 2482 | |
| σ_3 Failure (psf): | 1584 | |
| Failure Type: | Bulging | Failure Sketch |



STRESS STRAIN CURVE



| | | | | | |
|--|----------------------------|-------------|---|-----|--|
| Project Name: Bayou De Cade Marsh Creation and Ridge Restoration Terrebonne Parish, Louisiana | | | Type of Test: Unconsolidated Undrained ASTM D 2850 | | |
| Source of Sample: B-01 | | | Depth: 53-55 ft. | | |
| Sample Number: 17 | | | Visual Classification: FAT CLAY (CH), gray | | |
| Project No.: 04.55174066 | | | Test Date.: 4/20/2018 | | |
| Organic Content (%) ASTM D2974: | | | N/A | | |
| Sample No. | | 1 ● | 2 ■ | 3 ▲ | |
| INITIAL | Water Content (%) | 67.3 | | | |
| | Dry Density (pcf) | 59.5 | | | |
| | Saturation (%) | 99.2 | | | |
| | Void Ratio | 1.83 | | | |
| | Diameter (inches) | 2.84 | | | |
| | Height (inches) | 5.58 | | | |
| | % Passing #200 Sieve | | | | |
| | Specific Gravity (assumed) | 2.70 | | | |
| Strain Rate (%/min.) | | 1.0 | | | |
| Cell Pressure (psi) | | 15.00 | | | |
| Deviator Stress (psf) | | 890 | | | |
| Shear Strength (psf) | | 445 | | | |
| Failure Strain (%) | | 8.3 | | | |
| σ ₁ Failure (psf): | | 3050 | | | |
| σ ₃ Failure (psf): | | 2160 | | | |
| Failure Type: | | Multi Shear | Failure Sketch | | |



STRESS STRAIN CURVE

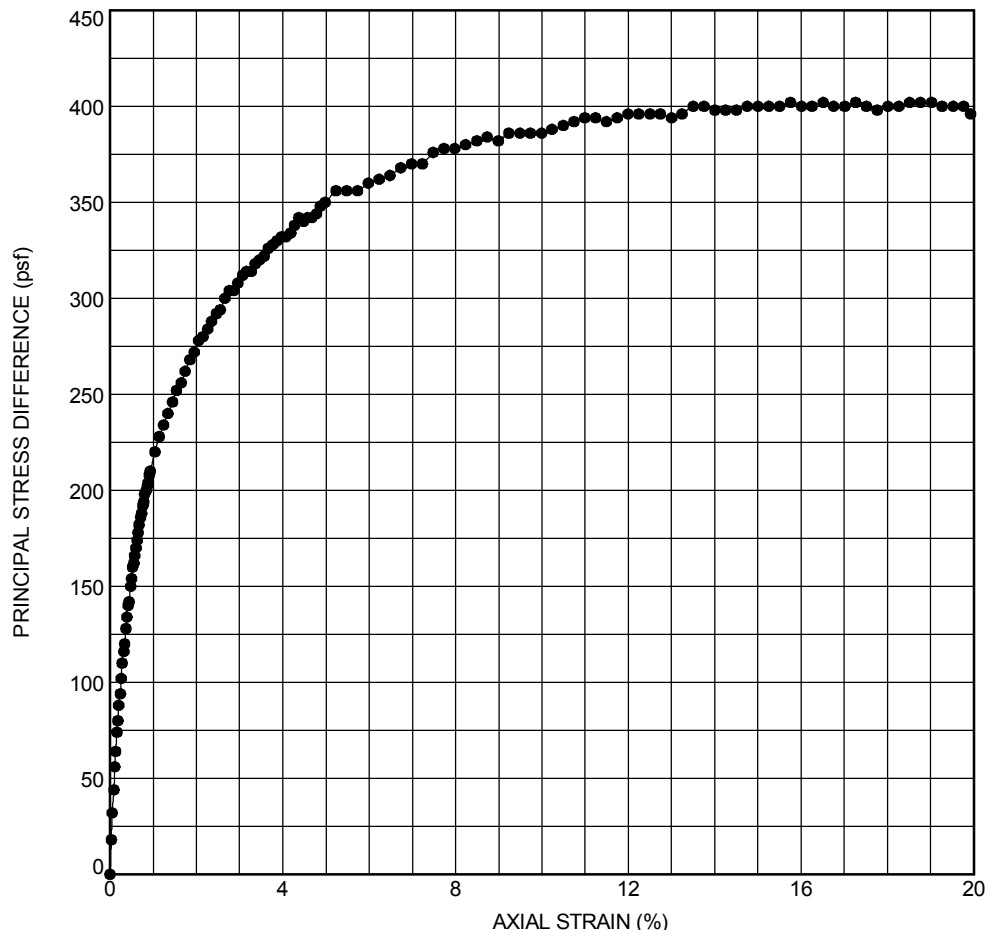


Multi Shear Failure Sketch





| | | | | | |
|--|----------------------------|----------------------------|--|-----|--|
| Project Name: Bayou De Cade Marsh Creation and Ridge Restoration Terrebonne Parish, Louisiana | | | Type of Test: Unconsolidated Undrained ASTM D 2850 | | |
| Source of Sample: B-02 | | | Depth: 28-30 ft. | | |
| Sample Number: 12 | | | Visual Classification: LEAN CLAY (CL), gray, with peat layers | | |
| Project No.: 04.55174066 | | | Test Date.: 4/25/2018 | | |
| Organic Content (%) ASTM D2974: | | | N/A | | |
| Sample No. | | 1 ● | 2 ■ | 3 ▲ | |
| INITIAL | Water Content (%) | 29.3 | | | |
| | Dry Density (pcf) | 74.9 | | | |
| | Saturation (%) | 63.3 | | | |
| | Void Ratio | 1.25 | | | |
| | Diameter (inches) | 2.84 | | | |
| | Height (inches) | 5.55 | | | |
| | % Passing #200 Sieve | | | | |
| | Specific Gravity (assumed) | 2.70 | | | |
| Strain Rate (%/min.) | | 1.0 | | | |
| Cell Pressure (psi) | | 8.00 | | | |
| Deviator Stress (psf) | | 400 | | | |
| Shear Strength (psf) | | 200 | | | |
| Failure Strain (%) | | 13.5 | | | |
| σ ₁ Failure (psf): | | 1552 | | | |
| σ ₃ Failure (psf): | | 1152 | | | |
| Failure Type: | | Multi Shear Failure Sketch | | | |



STRESS STRAIN CURVE



TRIAXIAL SHEAR TEST

Project Name: Bayou De Cade Marsh Creation and Ridge Restoration
Terrebonne Parish, Louisiana

Type of Test:
Unconsolidated Undrained ASTM D 2850

Source of Sample: B-03 Depth: 12-14 ft.

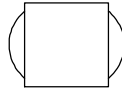
Visual Classification:
LEAN CLAY (CL), gray

Sample Number: 7

Project No.: 04.55174066 Test Date.: 4/27/2018

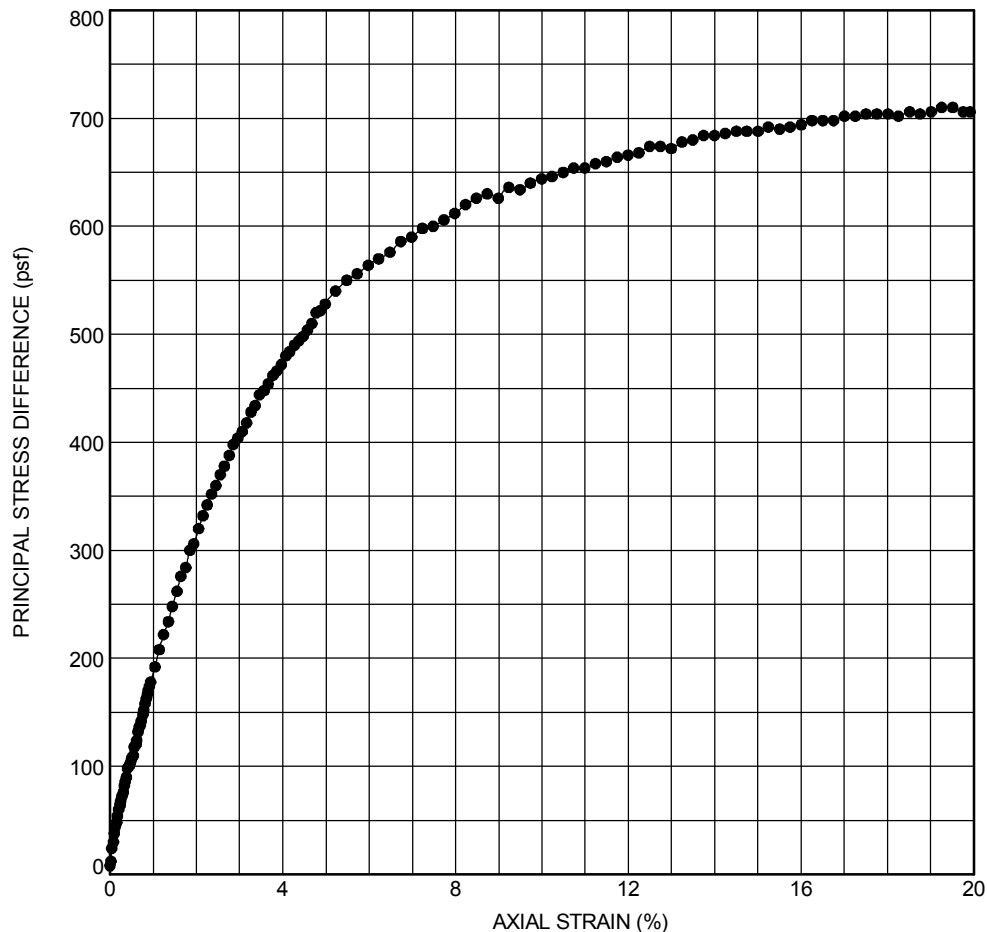
Organic Content (%) ASTM D2974: N/A

| Sample No. | 1 ● | 2 ■ | 3 ▲ |
|----------------------------|---------|-----|-----|
| Water Content (%) | 39.4 | | |
| Dry Density (pcf) | 86.1 | | |
| Saturation (%) | 100.0 | | |
| Void Ratio | 0.96 | | |
| Diameter (inches) | 2.83 | | |
| Height (inches) | 5.40 | | |
| % Passing #200 Sieve | | | |
| Specific Gravity (assumed) | 2.70 | | |
| Strain Rate (%/min.) | 1.0 | | |
| Cell Pressure (psi) | 5.00 | | |
| Deviator Stress (psf) | 688 | | |
| Shear Strength (psf) | 344 | | |
| Failure Strain (%) | 14.5 | | |
| σ_1 Failure (psf): | 1408 | | |
| σ_3 Failure (psf): | 720 | | |
| Failure Type: | Bulging | | |



Failure Sketch

Remarks:
Visual classification in general accordance with ASTM Standard D2487.



STRESS STRAIN CURVE



Project Name: Bayou De Cade Marsh Creation and Ridge Restoration
Terrebonne Parish, Louisiana

Type of Test:
Unconsolidated Undrained ASTM D 2850

Source of Sample: B-03 Depth: 16-18 ft.

Visual Classification:
LEAN CLAY (CL), gray, with organic traces

Sample Number: 9

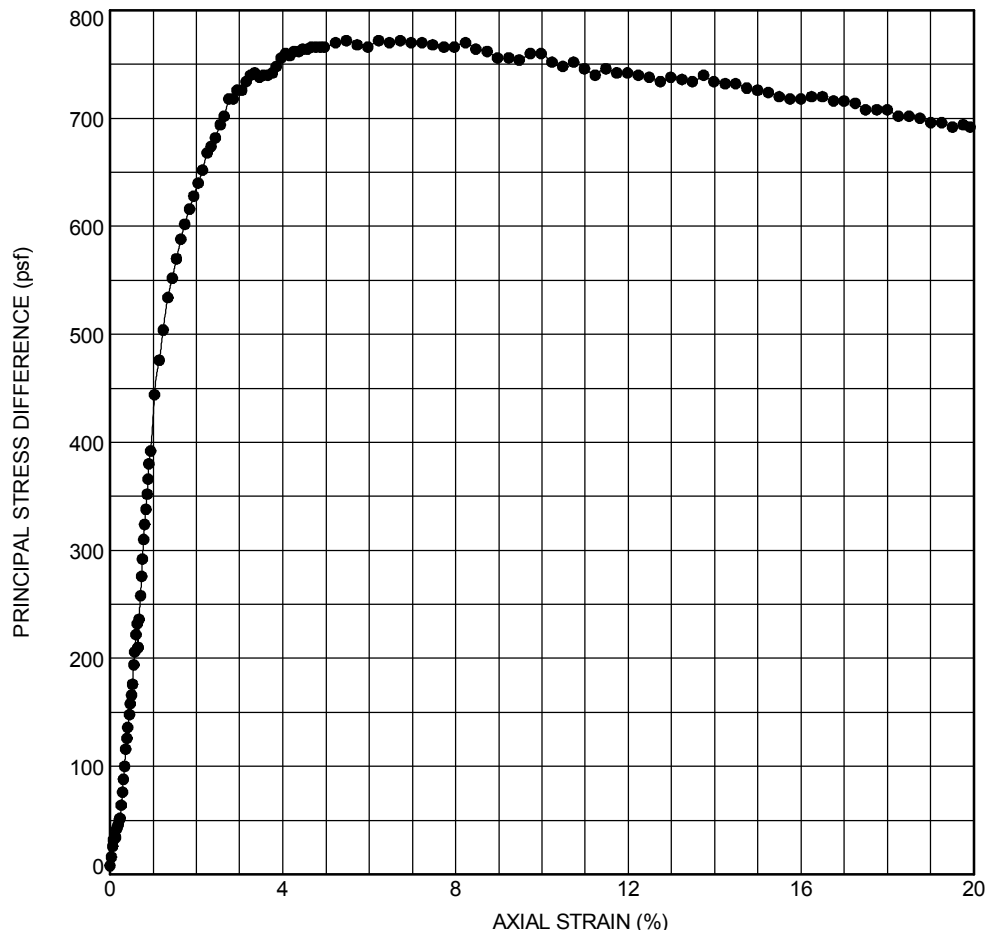
Project No.: 04.55174066 Test Date.: 4/27/2018

Organic Content (%) ASTM D2974: N/A

| Sample No. | 1 ● | 2 ■ | 3 ▲ |
|----------------------------|-------|-----|-----|
| Water Content (%) | 80.7 | | |
| Dry Density (pcf) | 54.3 | | |
| Saturation (%) | 100.0 | | |
| Void Ratio | 2.11 | | |
| Diameter (inches) | 2.82 | | |
| Height (inches) | 5.61 | | |
| % Passing #200 Sieve | | | |
| Specific Gravity (assumed) | 2.70 | | |

Remarks:
Visual classification in general accordance with ASTM Standard D2487.

| | | |
|---------------------------|-------------|----------------|
| Strain Rate (%/min.) | 1.0 | |
| Cell Pressure (psi) | 6.00 | |
| Deviator Stress (psf) | 772 | |
| Shear Strength (psf) | 386 | |
| Failure Strain (%) | 5.5 | |
| σ_1 Failure (psf): | 1636 | |
| σ_3 Failure (psf): | 864 | |
| Failure Type: | Multi Shear | Failure Sketch |



STRESS STRAIN CURVE



Project Name: Bayou De Cade Marsh Creation and Ridge Restoration
Terrebonne Parish, Louisiana

Type of Test:
Unconsolidated Undrained ASTM D 2850

Source of Sample: B-03 Depth: 38-40 ft.

Visual Classification:
FAT CLAY (CH), gray, with sand layers

Sample Number: 14

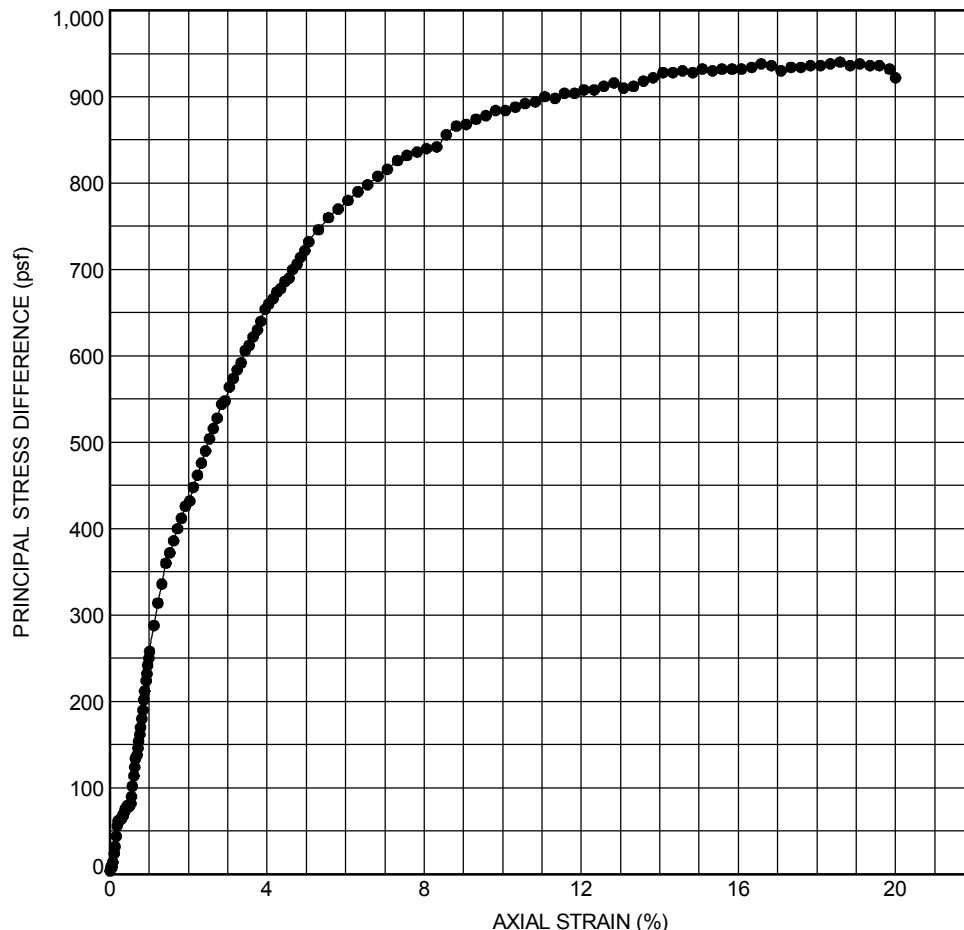
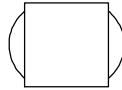
Project No.: 04.55174066 Test Date.: 4/27/2018

Organic Content (%) ASTM D2974: N/A

| Sample No. | 1 ● | 2 ■ | 3 ▲ |
|----------------------------|-------|-----|-----|
| Water Content (%) | 52.8 | | |
| Dry Density (pcf) | 70.6 | | |
| Saturation (%) | 100.0 | | |
| Void Ratio | 1.39 | | |
| Diameter (inches) | 2.80 | | |
| Height (inches) | 5.59 | | |
| % Passing #200 Sieve | | | |
| Specific Gravity (assumed) | 2.70 | | |

Remarks:
Visual classification in general accordance with ASTM Standard D2487.

| | | |
|---------------------------|---------|----------------|
| Strain Rate (%/min.) | 1.0 | |
| Cell Pressure (psi) | 14.00 | |
| Deviator Stress (psf) | 931 | |
| Shear Strength (psf) | 465 | |
| Failure Strain (%) | 15.0 | |
| σ_1 Failure (psf): | 2947 | |
| σ_3 Failure (psf): | 2016 | |
| Failure Type: | Bulging | Failure Sketch |



STRESS STRAIN CURVE



Project Name: Bayou De Cade Marsh Creation and Ridge Restoration
Terrebonne Parish, Louisiana

Type of Test:
Unconsolidated Undrained ASTM D 2850

Source of Sample: B-03 Depth: 48-50 ft.

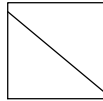
Visual Classification:
FAT CLAY (CH), gray, with organic traces

Sample Number: 16

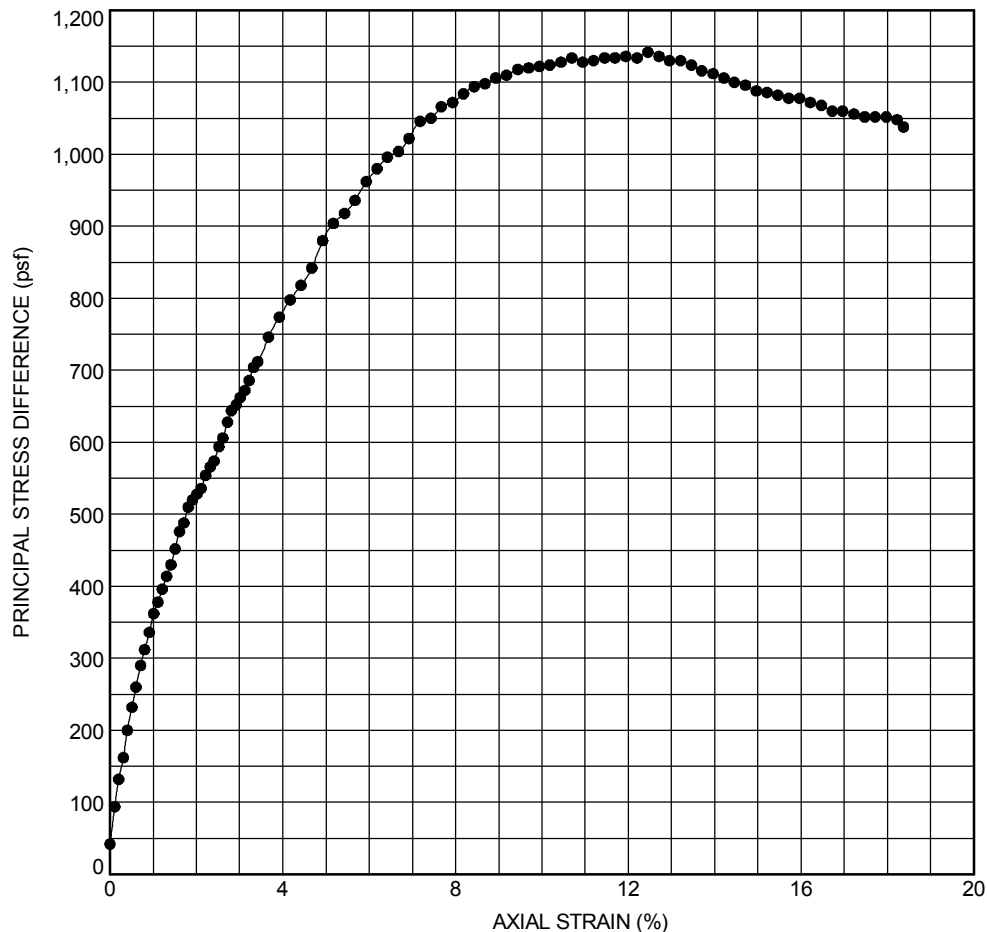
Project No.: 04.55174066 Test Date.: 5/3/2018

Organic Content (%) ASTM D2974: N/A

| Sample No. | 1 ● | 2 ■ | 3 ▲ |
|----------------------------|-----------|-----|-----|
| Water Content (%) | 59.7 | | |
| Dry Density (pcf) | 68.9 | | |
| Saturation (%) | 100.0 | | |
| Void Ratio | 1.45 | | |
| Diameter (inches) | 1.46 | | |
| Height (inches) | 2.83 | | |
| % Passing #200 Sieve | | | |
| Specific Gravity (assumed) | 2.70 | | |
| Strain Rate (%/min.) | 1.0 | | |
| Cell Pressure (psi) | 17.00 | | |
| Deviator Stress (psf) | 1142 | | |
| Shear Strength (psf) | 571 | | |
| Failure Strain (%) | 12.5 | | |
| σ_1 Failure (psf): | 3590 | | |
| σ_3 Failure (psf): | 2448 | | |
| Failure Type: | 45° Shear | | |



Remarks:
Visual classification in general accordance with ASTM Standard D2487.



STRESS STRAIN CURVE



TRIAXIAL SHEAR TEST

Project Name: Bayou De Cade Marsh Creation and
Ridge Restoration
Terrebonne Parish, Louisiana

Type of Test:
Unconsolidated Undrained ASTM D 2850

Source of Sample: B-04 Depth: 12-14 ft.

Sample Number: 7

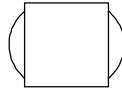
Visual Classification:
FAT CLAY (CH), gray

Project No.: 04.55174066

Test Date.: 5/4/2018

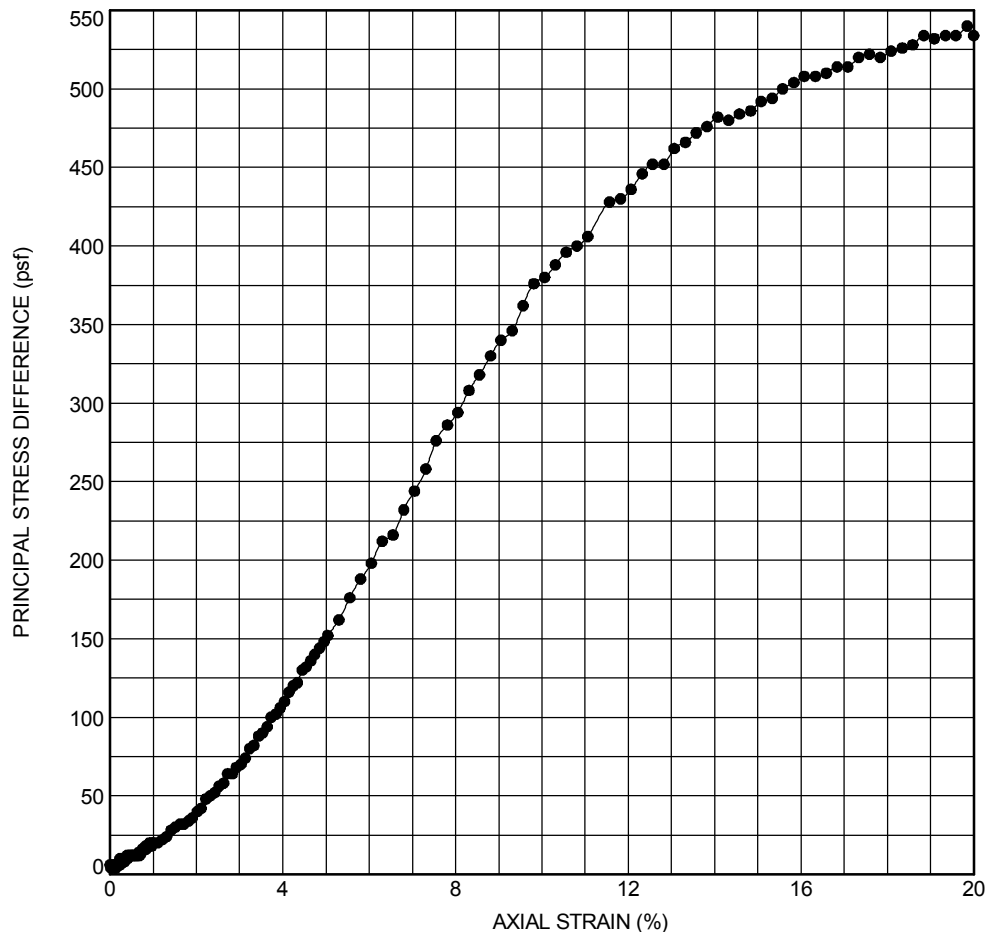
Organic Content (%) ASTM D2974: N/A

| Sample No. | 1 ● | 2 ■ | 3 ▲ |
|----------------------------|---------|-----|-----|
| Water Content (%) | 33.0 | | |
| Dry Density (pcf) | 87.2 | | |
| Saturation (%) | 95.6 | | |
| Void Ratio | 0.93 | | |
| Diameter (inches) | 2.87 | | |
| Height (inches) | 5.16 | | |
| % Passing #200 Sieve | | | |
| Specific Gravity (assumed) | 2.70 | | |
| Strain Rate (%/min.) | 1.0 | | |
| Cell Pressure (psi) | 5.00 | | |
| Deviator Stress (psf) | 490 | | |
| Shear Strength (psf) | 245 | | |
| Failure Strain (%) | 15.0 | | |
| σ_1 Failure (psf): | 1210 | | |
| σ_3 Failure (psf): | 720 | | |
| Failure Type: | Bulging | | |



Failure Sketch

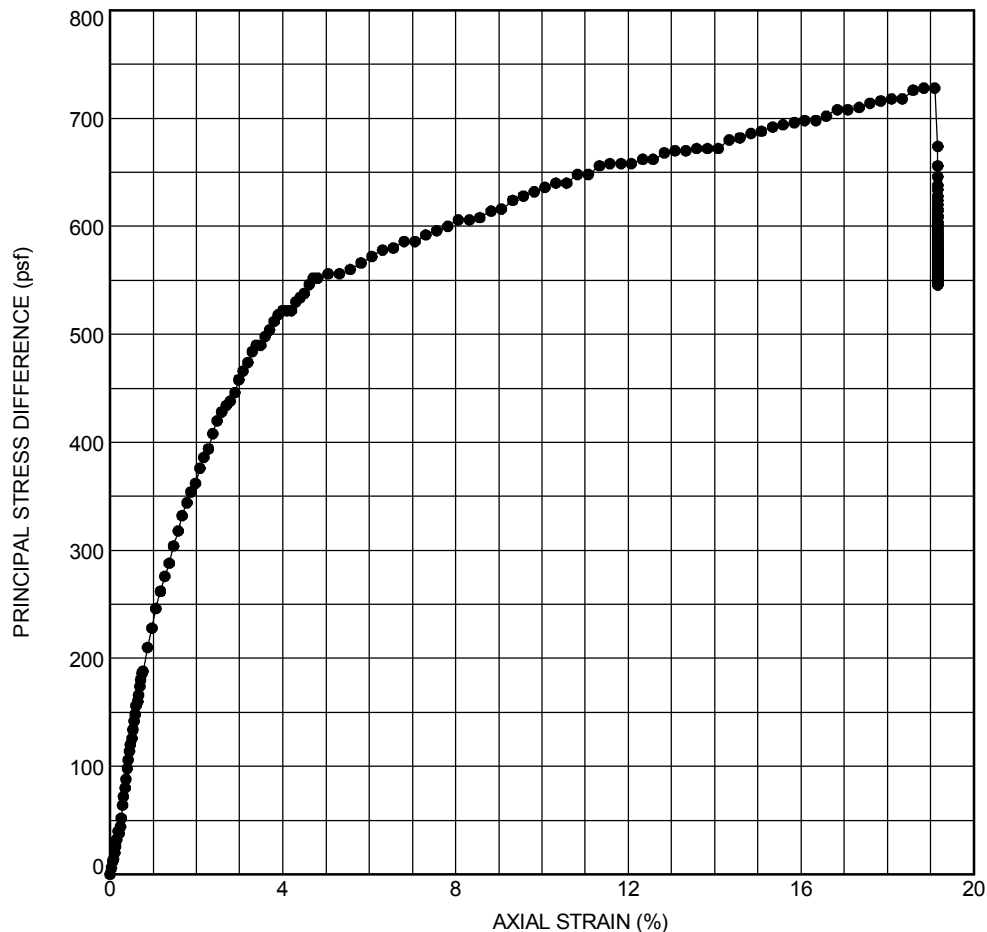
Remarks:
Visual classification in general accordance with ASTM Standard D2487.



STRESS STRAIN CURVE

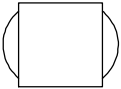


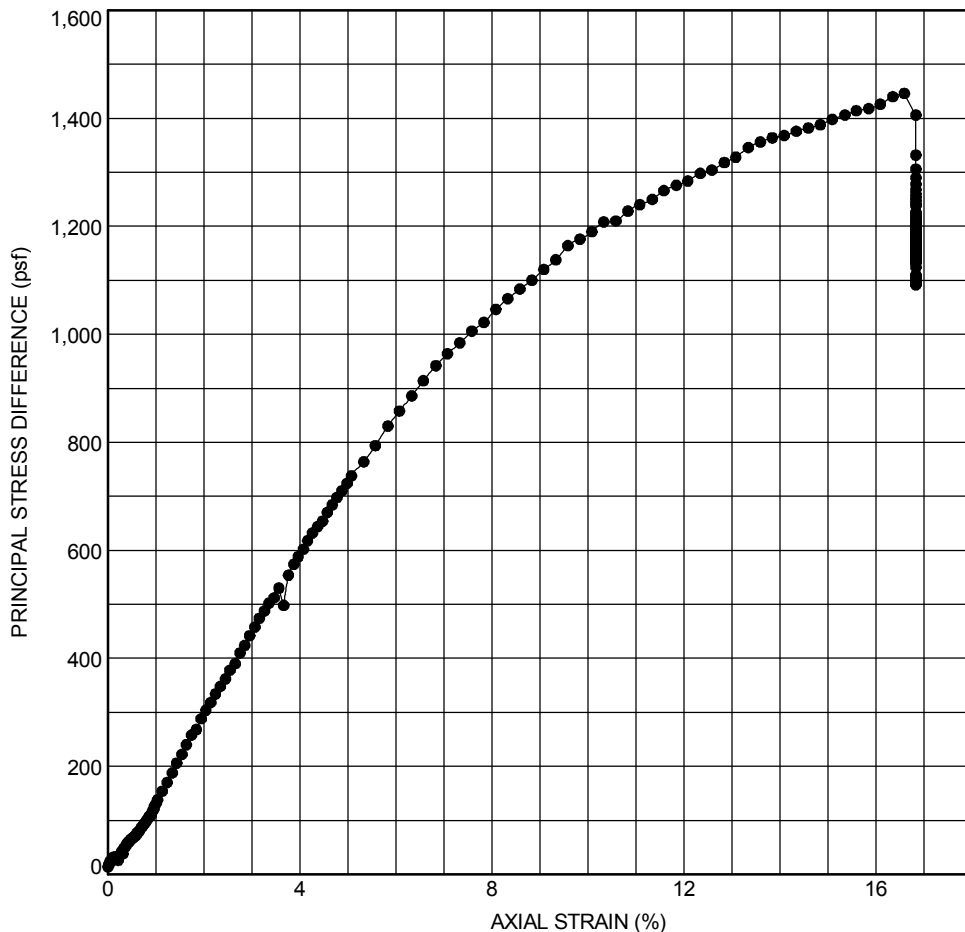
| | | | | | |
|--|----------------------------|---------------------------------|--|--|--|
| Project Name: Bayou De Cade Marsh Creation and Ridge Restoration Terrebonne Parish, Louisiana | | | Type of Test: Unconsolidated Undrained ASTM D 2850 | | |
| Source of Sample: B-04 | | | Depth: 33-35 ft. | | |
| Sample Number: 13 | | | Visual Classification: LEAN CLAY (CL), gray, with silt and sand pockets | | |
| Project No.: 04.55174066 | | | Test Date.: 5/7/2018 | | |
| Organic Content (%) ASTM D2974: | | | N/A | | |
| Sample No. | | | 1 ● 2 ■ 3 ▲ | | |
| INITIAL | Water Content (%) | | 45.2 | | |
| | Dry Density (pcf) | | 79.0 | | |
| | Saturation (%) | | 100.0 | | |
| | Void Ratio | | 1.13 | | |
| | Diameter (inches) | | 2.79 | | |
| | Height (inches) | | 5.52 | | |
| | % Passing #200 Sieve | | | | |
| | Specific Gravity (assumed) | | 2.70 | | |
| Strain Rate (%/min.) | | 1.0 | | | |
| Cell Pressure (psi) | | 12.00 | | | |
| Deviator Stress (psf) | | 687 | | | |
| Shear Strength (psf) | | 344 | | | |
| Failure Strain (%) | | 15.0 | | | |
| σ ₁ Failure (psf): | | 2415 | | | |
| σ ₃ Failure (psf): | | 1728 | | | |
| Failure Type: | | Multi Shear Failure Sketch | | | |



STRESS STRAIN CURVE



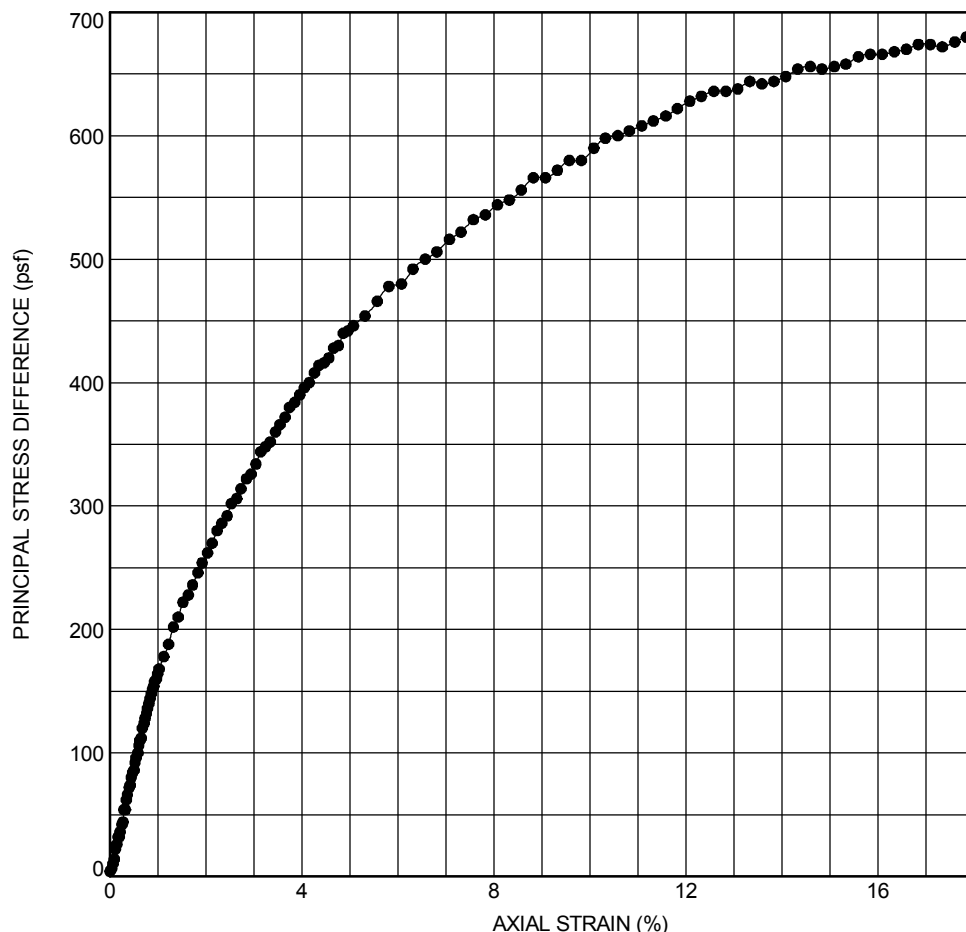
| | | | |
|--|---------|---|-----|
| Project Name: Bayou De Cade Marsh Creation and Ridge Restoration Terrebonne Parish, Louisiana | | Type of Test: Unconsolidated Undrained ASTM D 2850 | |
| Source of Sample: B-05 | | Depth: 8-10 ft. | |
| Sample Number: 5 | | Visual Classification: LEAN CLAY (CL), gray | |
| Project No.: 04.55174066 | | Test Date.: 4/24/2018 | |
| Organic Content (%) ASTM D2974: | | N/A | |
| Sample No. | 1 ● | 2 ■ | 3 ▲ |
| Water Content (%) | 33.3 | | |
| Dry Density (pcf) | 87.5 | | |
| Saturation (%) | 97.1 | | |
| Void Ratio | 0.93 | | |
| Diameter (inches) | 2.81 | | |
| Height (inches) | 5.58 | | |
| % Passing #200 Sieve | | | |
| Specific Gravity (assumed) | 2.70 | | |
| Strain Rate (%/min.) | 1.0 | | |
| Cell Pressure (psi) | 3.00 | | |
| Deviator Stress (psf) | 1394 | | |
| Shear Strength (psf) | 697 | | |
| Failure Strain (%) | 15.0 | | |
| σ_1 Failure (psf): | 1826 | | |
| σ_3 Failure (psf): | 432 | | |
| Failure Type: | Bulging | | |
| <div style="text-align: center;">  <p>Failure Sketch</p> </div> | | | |
| Remarks: | | Visual classification in general accordance with ASTM Standard D2487. | |



STRESS STRAIN CURVE



| | | | |
|--|---------|---|-----|
| Project Name: Bayou De Cade Marsh Creation and Ridge Restoration Terrebonne Parish, Louisiana | | Type of Test: Unconsolidated Undrained ASTM D 2850 | |
| Source of Sample: B-06 | | Depth: 4-6 ft. | |
| Sample Number: 3 | | Visual Classification: LEAN CLAY (CL), gray, with silt pockets and roots | |
| Project No.: 04.55174066 | | Test Date.: 4/25/2018 | |
| Organic Content (%) ASTM D2974: | | N/A | |
| Sample No. | 1 ● | 2 ■ | 3 ▲ |
| Water Content (%) | 35.4 | | |
| Dry Density (pcf) | 87.5 | | |
| Saturation (%) | 100.0 | | |
| Void Ratio | 0.92 | | |
| Diameter (inches) | 2.84 | | |
| Height (inches) | 5.56 | | |
| % Passing #200 Sieve | | | |
| Specific Gravity (assumed) | 2.70 | | |
| Strain Rate (%/min.) | 1.0 | | |
| Cell Pressure (psi) | 3.00 | | |
| Deviator Stress (psf) | 656 | | |
| Shear Strength (psf) | 328 | | |
| Failure Strain (%) | 14.6 | | |
| σ_1 Failure (psf): | 1088 | | |
| σ_3 Failure (psf): | 432 | | |
| Failure Type: | Bulging | | |
| Failure Sketch | | | |
| Remarks: | | Visual classification in general accordance with ASTM Standard D2487. | |



STRESS STRAIN CURVE



TRIAXIAL SHEAR TEST

Project Name: Bayou De Cade Marsh Creation and
Ridge Restoration
Terrebonne Parish, Louisiana

Type of Test:
Unconsolidated Undrained ASTM D 2850

Source of Sample: B-06 Depth: 8-10 ft.

Sample Number: 5

Visual Classification:
LEAN CLAY (CL), gray, with silt pockets

Project No.: 04.55174066

Test Date.: 4/26/2018

Organic Content (%) ASTM D2974: N/A

Sample No.

1 ●

2 ■

3 ▲

INITIAL

Water Content (%)

42.7

Dry Density (pcf)

80.7

Saturation (%)

100.0

Void Ratio

1.09

Diameter (inches)

2.81

Height (inches)

5.56

% Passing #200 Sieve

Specific Gravity (assumed)

2.70

Remarks:

Visual classification in general accordance with ASTM Standard D2487.

Strain Rate (%/min.)

1.0

Cell Pressure (psi)

3.00

Deviator Stress (psf)

1196

Shear Strength (psf)

598

Failure Strain (%)

8.0

σ_1 Failure (psf):

1628

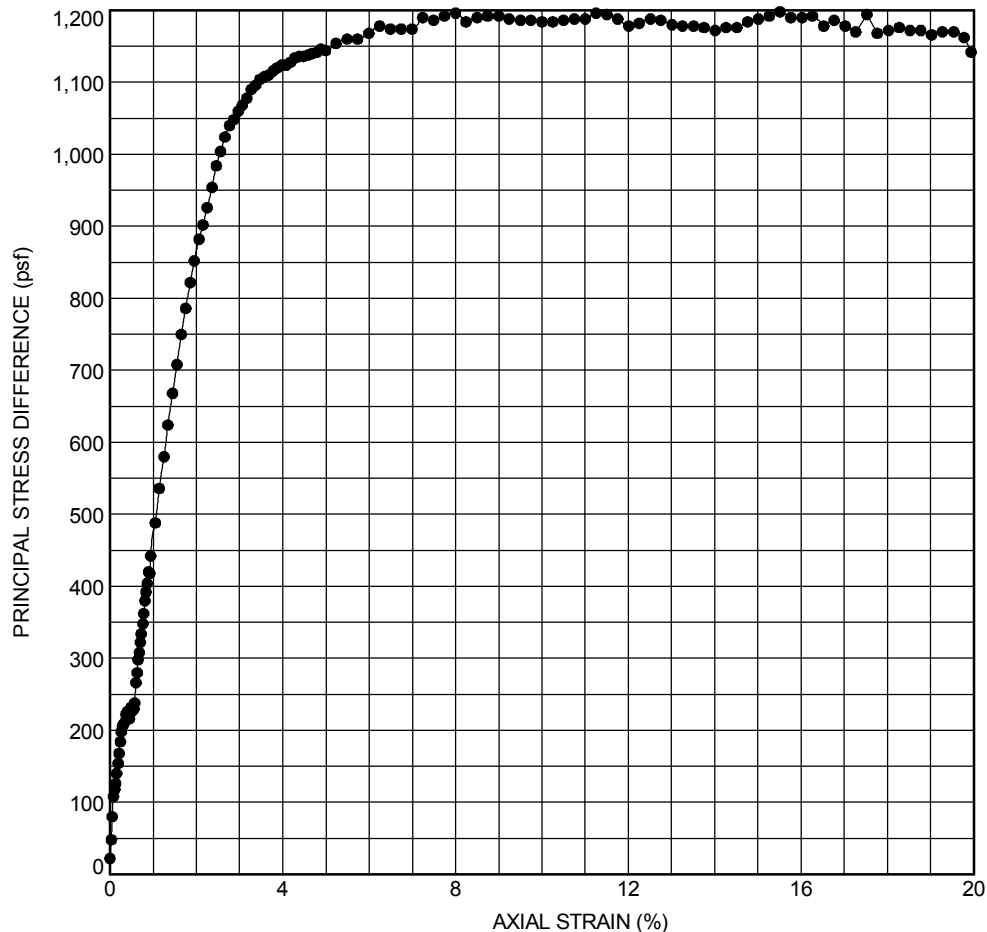
σ_3 Failure (psf):

432

Failure Type:

Multi Shear

Failure Sketch



STRESS STRAIN CURVE

PLATE B-4w



PLATE B-4x



TRIAXIAL SHEAR TEST

Project Name: Bayou De Cade Marsh Creation and
Ridge Restoration
Terrebonne Parish, Louisiana

Type of Test:
Unconsolidated Undrained ASTM D 2850

Source of Sample: B-06 Depth: 38-40 ft.

Visual Classification:
FAT CLAY (CH), gray, with silt pockets

Sample Number: 14

Project No.: 04.55174066

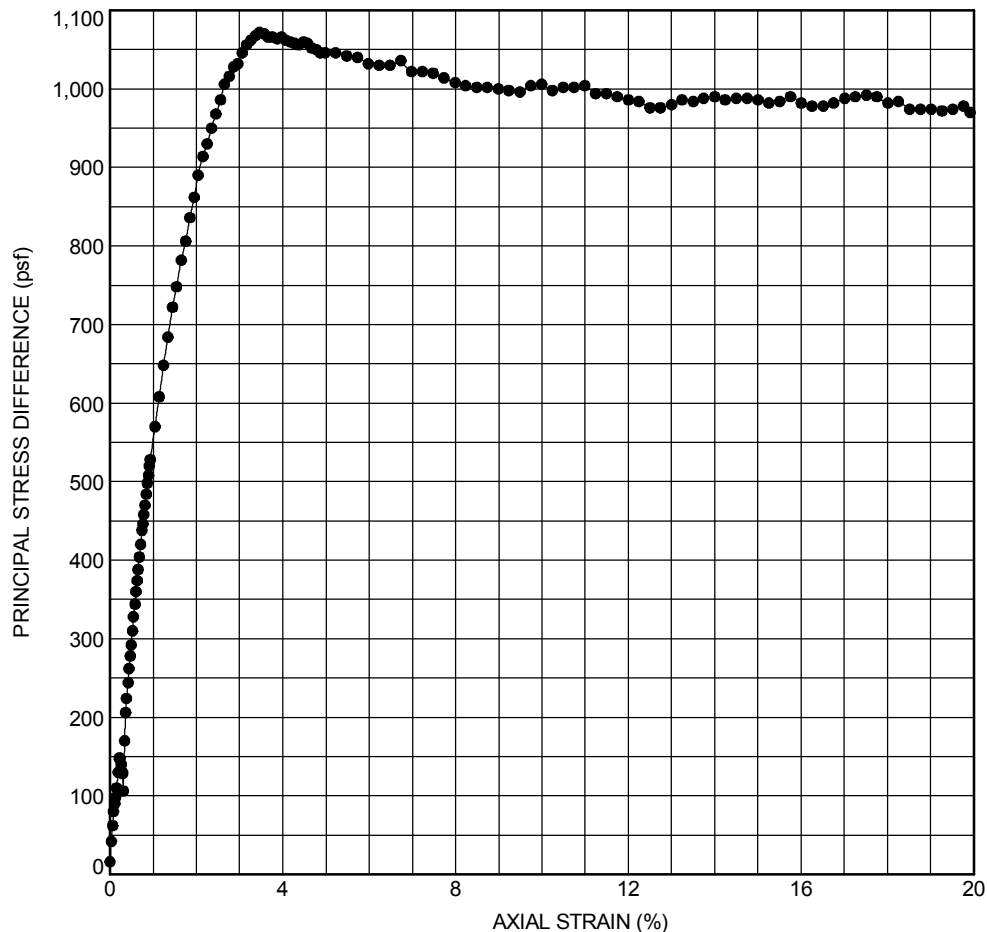
Test Date.: 4/26/2018

Organic Content (%) ASTM D2974: N/A

| Sample No. | 1 ● | 2 ■ | 3 ▲ |
|----------------------------|-------------|-----|-----|
| Water Content (%) | 51.7 | | |
| Dry Density (pcf) | 72.5 | | |
| Saturation (%) | 100.0 | | |
| Void Ratio | 1.32 | | |
| Diameter (inches) | 2.81 | | |
| Height (inches) | 5.62 | | |
| % Passing #200 Sieve | | | |
| Specific Gravity (assumed) | 2.70 | | |
| Strain Rate (%/min.) | 1.0 | | |
| Cell Pressure (psi) | 11.00 | | |
| Deviator Stress (psf) | 1072 | | |
| Shear Strength (psf) | 536 | | |
| Failure Strain (%) | 3.5 | | |
| σ_1 Failure (psf): | 2656 | | |
| σ_3 Failure (psf): | 1584 | | |
| Failure Type: | Multi Shear | | |




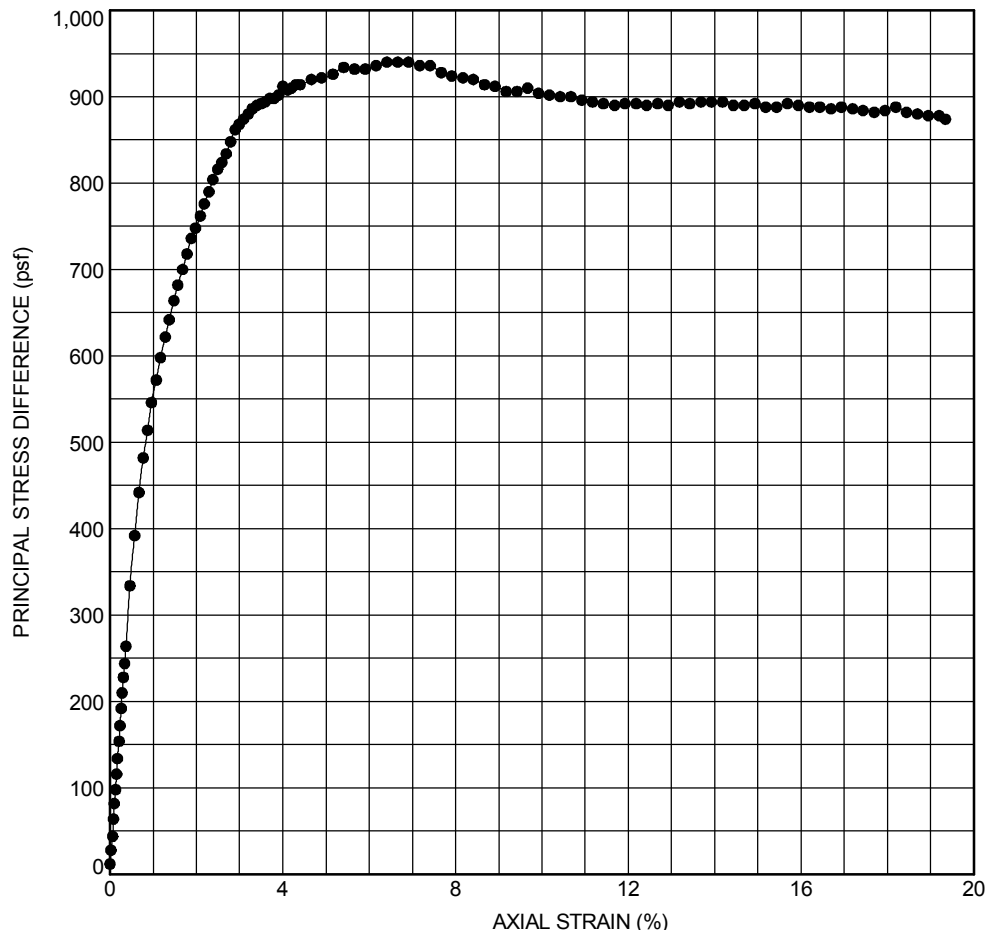
Remarks:
Visual classification in general accordance with ASTM Standard D2487.



STRESS STRAIN CURVE




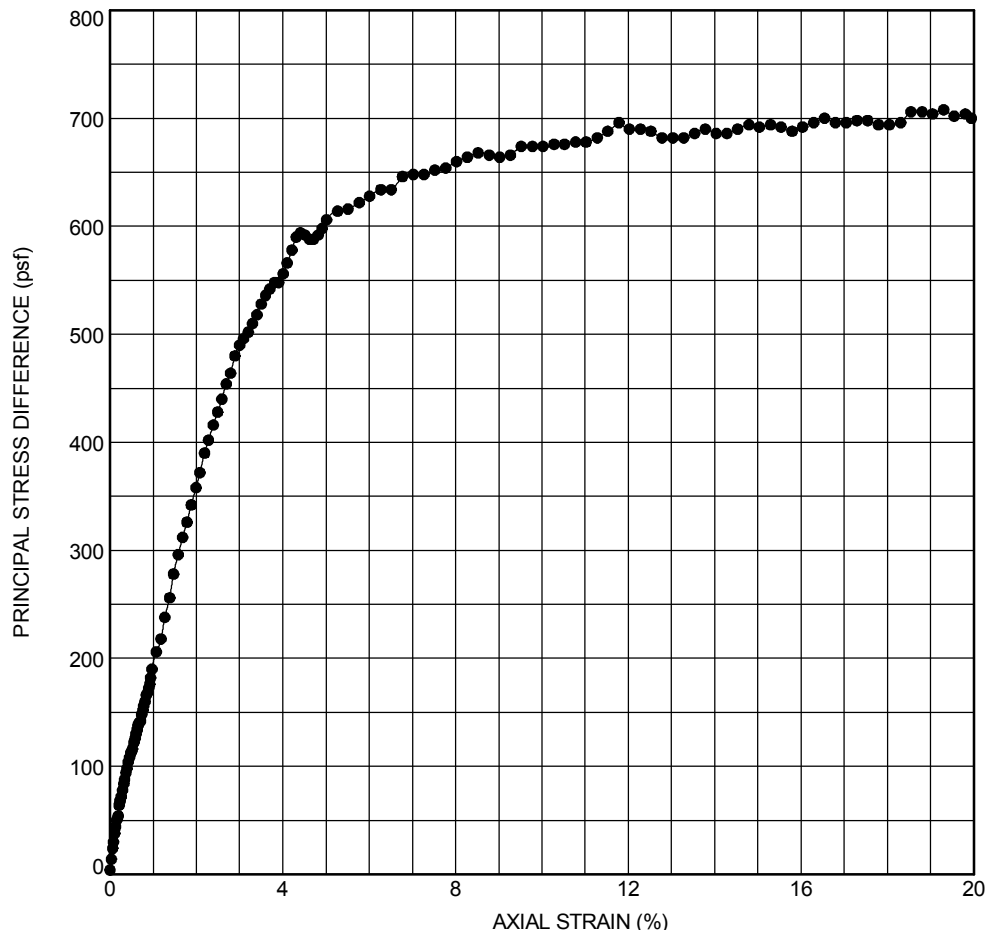
| | | | | | |
|--|----------------------------|---|---|-----|----------------|
| Project Name: Bayou De Cade Marsh Creation and Ridge Restoration Terrebonne Parish, Louisiana | | | Type of Test: Unconsolidated Undrained ASTM D 2850 | | |
| Source of Sample: B-06 | | | Depth: 48-50 ft. | | |
| Sample Number: 17 | | | Visual Classification: FAT CLAY (CH), gray, with silt pockets | | |
| Project No.: 04.55174066 | | | Test Date.: 4/26/2018 | | |
| Organic Content (%) ASTM D2974: | | | N/A | | |
| Sample No. | | 1 ● | 2 ■ | 3 ▲ | |
| INITIAL | Water Content (%) | 66.7 | Remarks: Visual classification in general accordance with ASTM Standard D2487. | | |
| | Dry Density (pcf) | 60.8 | | | |
| | Saturation (%) | 100.0 | | | |
| | Void Ratio | 1.77 | | | |
| | Diameter (inches) | 2.83 | | | |
| | Height (inches) | 5.62 | | | |
| | % Passing #200 Sieve | | | | |
| | Specific Gravity (assumed) | 2.70 | | | |
| Strain Rate (%/min.) | 1.0 |  | | | |
| Cell Pressure (psi) | 14.00 | | | | |
| Deviator Stress (psf) | 940 | | | | |
| Shear Strength (psf) | 470 | | | | |
| Failure Strain (%) | 6.4 | | | | |
| σ ₁ Failure (psf): | 2956 | | | | |
| σ ₃ Failure (psf): | 2016 | | | | |
| Failure Type: | Multi Shear | | | | Failure Sketch |



STRESS STRAIN CURVE



| | | | | | |
|--|----------------------------|---|---|-----|--|
| Project Name: Bayou De Cade Marsh Creation and Ridge Restoration Terrebonne Parish, Louisiana | | | Type of Test: Unconsolidated Undrained ASTM D 2850 | | |
| Source of Sample: B-08 | | | Depth: 18-20 ft. | | |
| Sample Number: 10 | | | Visual Classification: FAT CLAY (CH), gray, with organics | | |
| Project No.: 04.55174066 | | | Test Date.: 5/8/2018 | | |
| Organic Content (%) ASTM D2974: | | | N/A | | |
| Sample No. | | 1 ● | 2 ■ | 3 ▲ | |
| INITIAL | Water Content (%) | 43.1 | Remarks: Visual classification in general accordance with ASTM Standard D2487. | | |
| | Dry Density (pcf) | 80.1 | | | |
| | Saturation (%) | 100.0 | | | |
| | Void Ratio | 1.10 | | | |
| | Diameter (inches) | 2.80 | | | |
| | Height (inches) | 5.59 | | | |
| | % Passing #200 Sieve | | | | |
| | Specific Gravity (assumed) | 2.70 | | | |
| Strain Rate (%/min.) | 1.0 |  | | | |
| Cell Pressure (psi) | 7.00 | | | | |
| Deviator Stress (psf) | 696 | | | | |
| Shear Strength (psf) | 348 | | | | |
| Failure Strain (%) | 11.8 | | | | |
| σ ₁ Failure (psf): | 1704 | | | | |
| σ ₃ Failure (psf): | 1008 | | | | |
| Failure Type: | Bulging | | | | |
| Failure Sketch | | | | | |



STRESS STRAIN CURVE



Project Name: Bayou De Cade Marsh Creation and Ridge Restoration
Terrebonne Parish, Louisiana

Type of Test:
Unconsolidated Undrained ASTM D 2850

Source of Sample: B-09 Depth: 23-25 ft.

Visual Classification:
FAT CLAY (CH), gray

Sample Number:

Project No.: 04.55174066

Test Date.: 5/8/2018

Organic Content (%) ASTM D2974: N/A

Sample No.

1 ●

2 ■

3 ▲

Remarks:
Visual classification in general accordance with ASTM Standard D2487.

INITIAL

Water Content (%)

59.9

Dry Density (pcf)

65.3

Saturation (%)

100.0

Void Ratio

1.58

Diameter (inches)

2.84

Height (inches)

5.59

% Passing #200 Sieve

Specific Gravity (assumed)

2.70

Strain Rate (%/min.)

1.0

Cell Pressure (psi)

9.00

Deviator Stress (psf)

617

Shear Strength (psf)

309

Failure Strain (%)

15.0

σ_1 Failure (psf):

1913

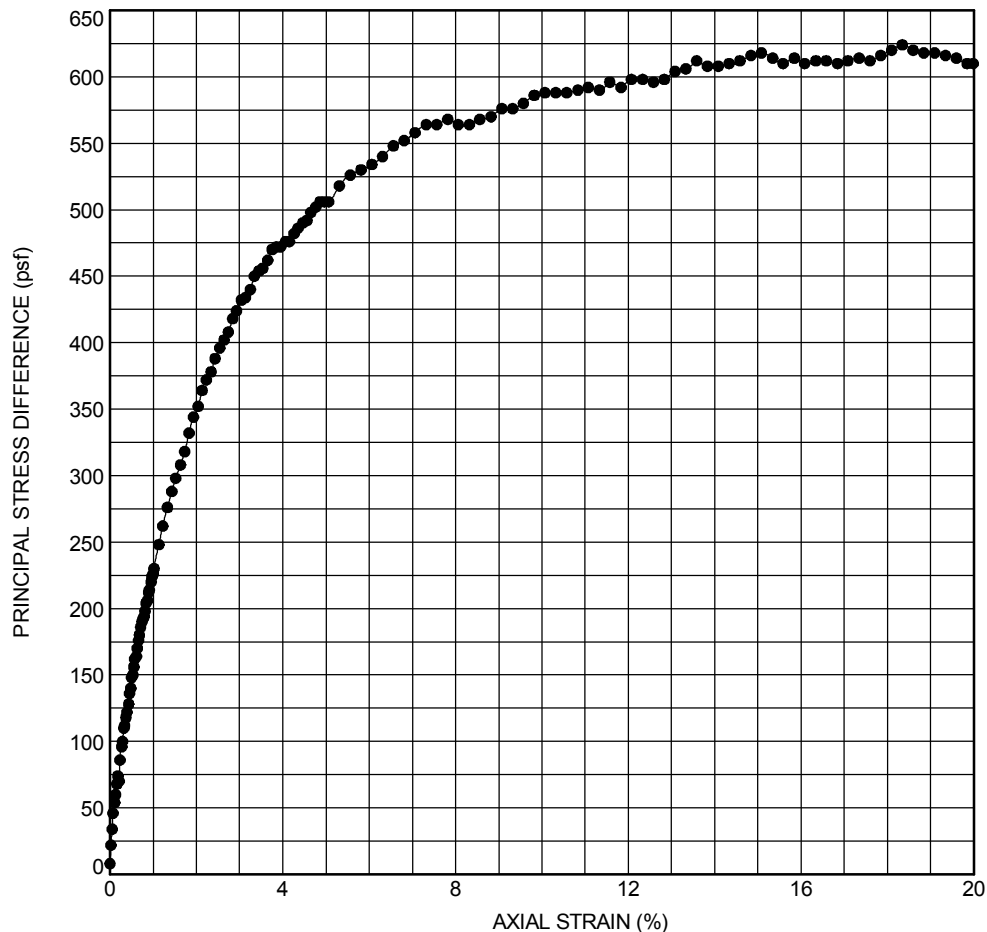
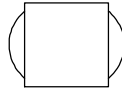
σ_3 Failure (psf):

1296

Failure Type:

Bulging

Failure Sketch

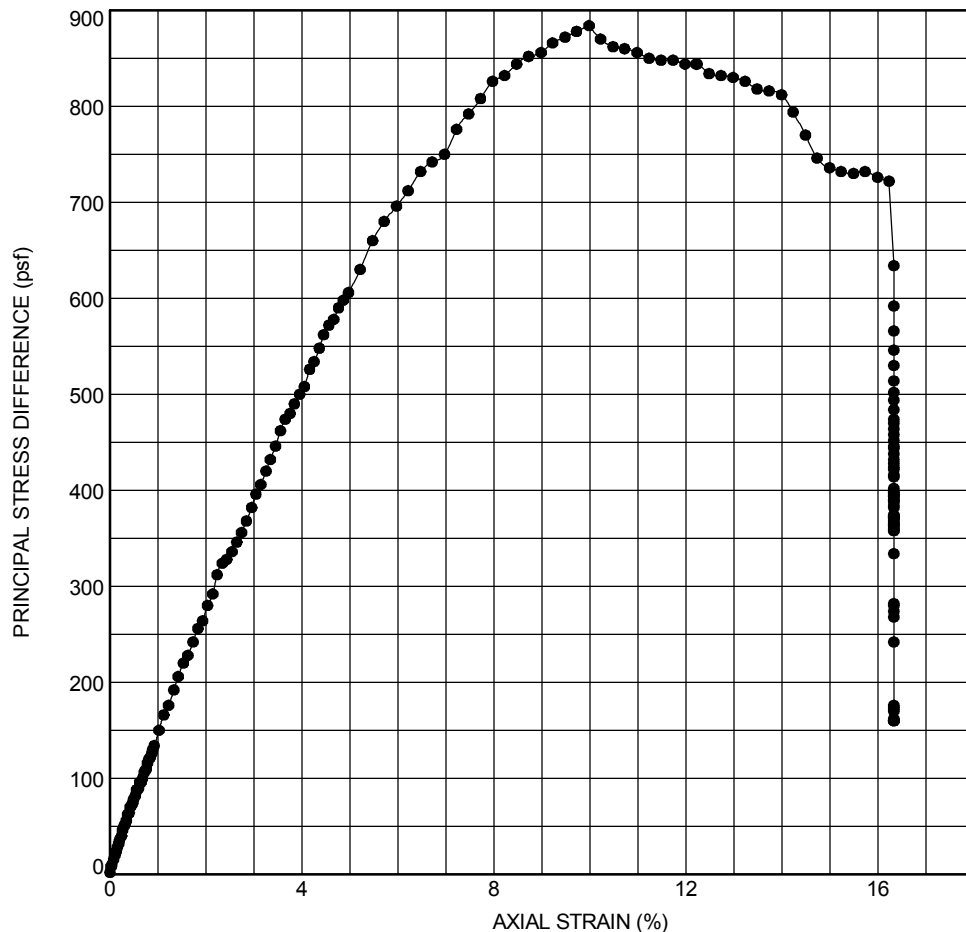


STRESS STRAIN CURVE

PLATE B-4aj

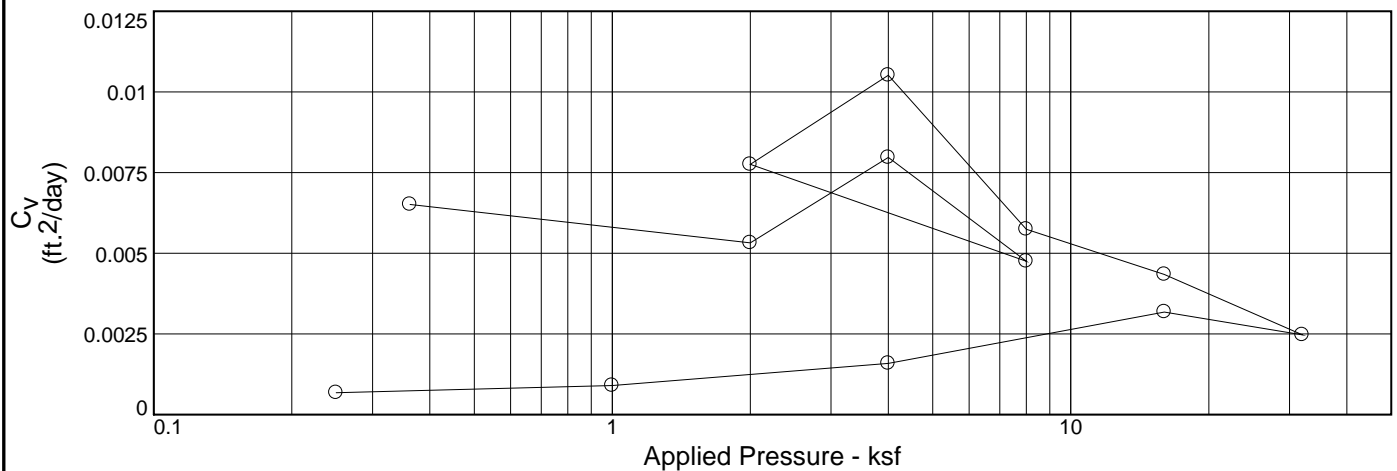
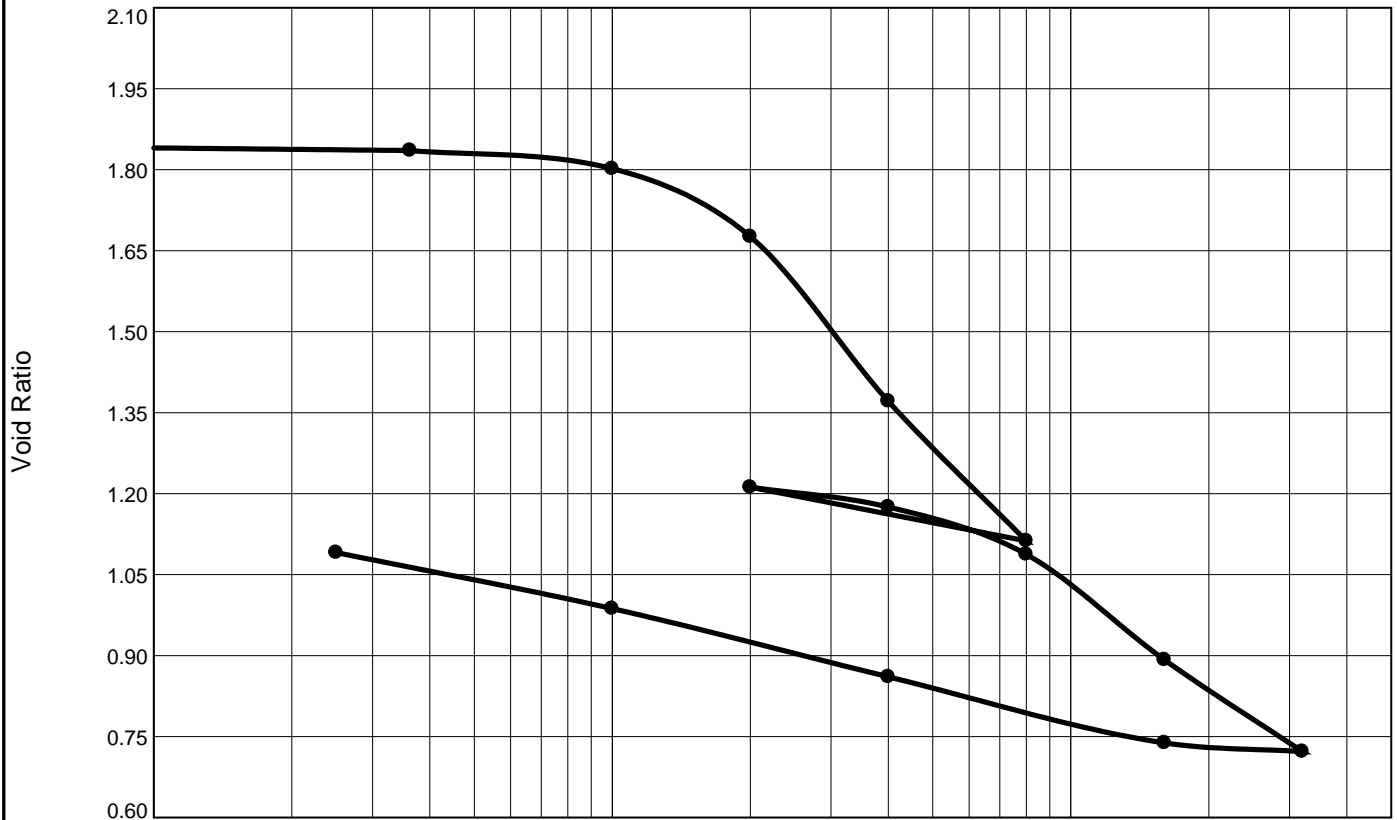


| | | | | | |
|--|----------------------------|---------|---|-----|--|
| Project Name: Bayou De Cade Marsh Creation and Ridge Restoration Terrebonne Parish, Louisiana | | | Type of Test: Unconsolidated Undrained ASTM D 2850 | | |
| Source of Sample: B-09 | | | Depth: 33-35 ft. | | |
| Sample Number: 13 | | | Visual Classification: FAT CLAY (CH), gray | | |
| Project No.: 04.55174066 | | | Test Date.: 5/8/2018 | | |
| Organic Content (%) ASTM D2974: | | | N/A | | |
| Sample No. | | 1 ● | 2 ■ | 3 ▲ | |
| INITIAL | Water Content (%) | 35.4 | | | |
| | Dry Density (pcf) | 90.9 | | | |
| | Saturation (%) | 100.0 | | | |
| | Void Ratio | 0.85 | | | |
| | Diameter (inches) | 2.75 | | | |
| | Height (inches) | 5.53 | | | |
| | % Passing #200 Sieve | | | | |
| | Specific Gravity (assumed) | 2.70 | | | |
| Strain Rate (%/min.) | | 1.0 | | | |
| Cell Pressure (psi) | | 12.00 | | | |
| Deviator Stress (psf) | | 884 | | | |
| Shear Strength (psf) | | 442 | | | |
| Failure Strain (%) | | 10.0 | | | |
| σ ₁ Failure (psf): | | 2612 | | | |
| σ ₃ Failure (psf): | | 1728 | | | |
| Failure Type: | | Bulging | Failure Sketch | | |
| Remarks: Visual classification in general accordance with ASTM Standard D2487. | | | | | |



STRESS STRAIN CURVE

CONSOLIDATION TEST REPORT

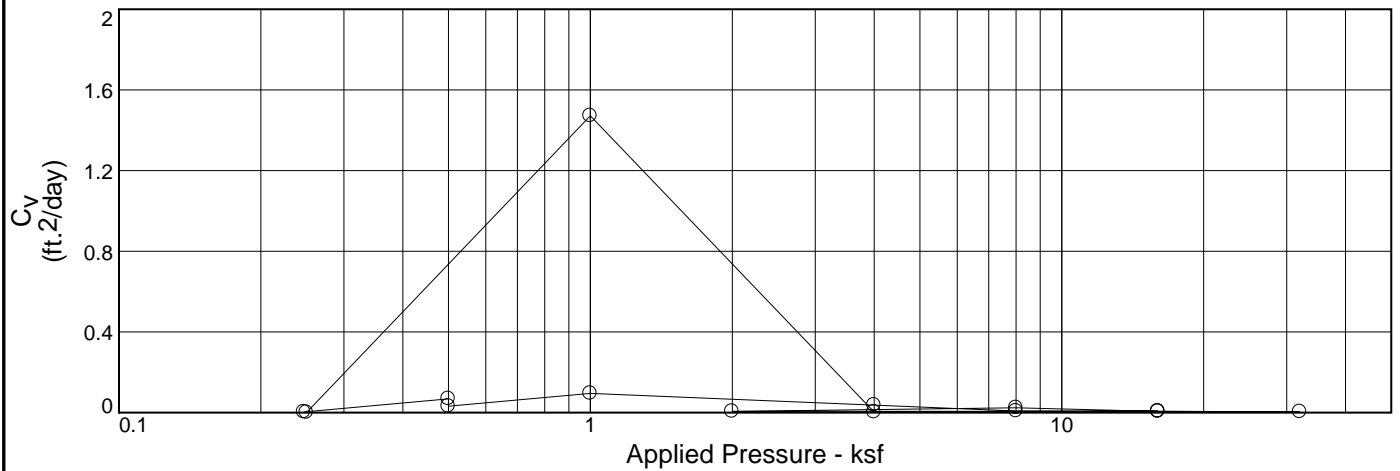
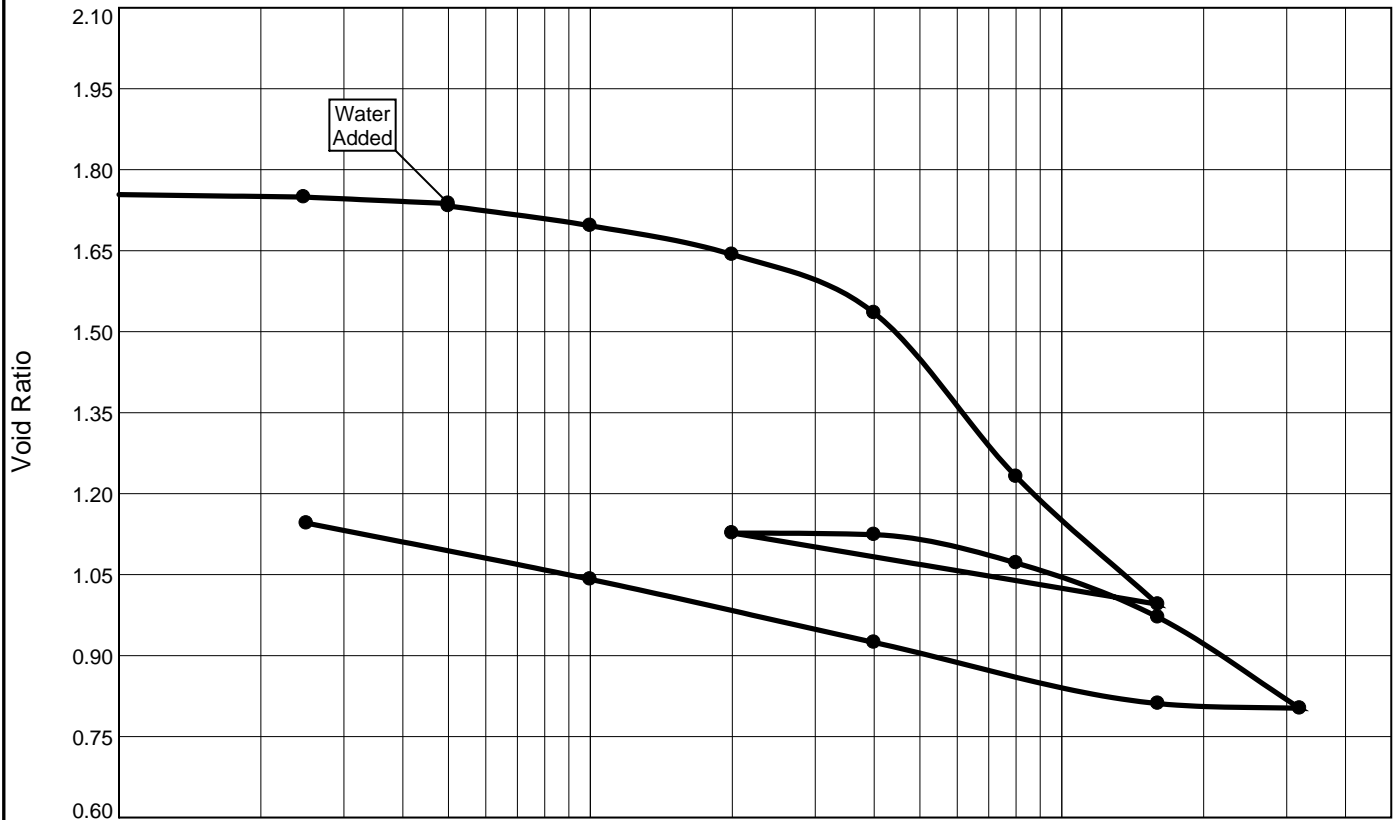


| Natural | | Dry Dens. (pcf) | LL | PI | Sp. Gr. | Overburden (ksf) | P_c (ksf) | C_c | C_r | Initial Void Ratio |
|------------|----------|--------------------|-----|----|---------|---------------------|----------------|-------|-------|-----------------------|
| Saturation | Moisture | | | | | | | | | |
| 102.6 % | 76.4 % | 54.3 | 126 | 92 | 2.472 | 1.25 | 1.9 | 0.93 | 0.10 | 1.840 |

| MATERIAL DESCRIPTION | | | | | | | | USCS | AASHTO |
|---|--|--|--|--|--|--|--|------|--------|
| ORGANIC CLAY, black and gray, with few peat pockets and seams | | | | | | | | OH | |

| | | | | | | | | | |
|---|--|--|--|--|--|---|--|--|--|
| Project No. 04.55174066 Client: CPRA Project: BAYOU DE CADE MARSH CREATION AND RIDGE RESTORATION Source of Sample: B-01 Depth: 23.0 Sample Number: 11 Fugro USA Land, Inc. Baton Rouge, LA | | | | | | Remarks: Date Tested: 05/24/2018 Tested by: JK Reviewed by: ERM | | | |
| | | | | | | Plate B-5a | | | |

CONSOLIDATION TEST REPORT

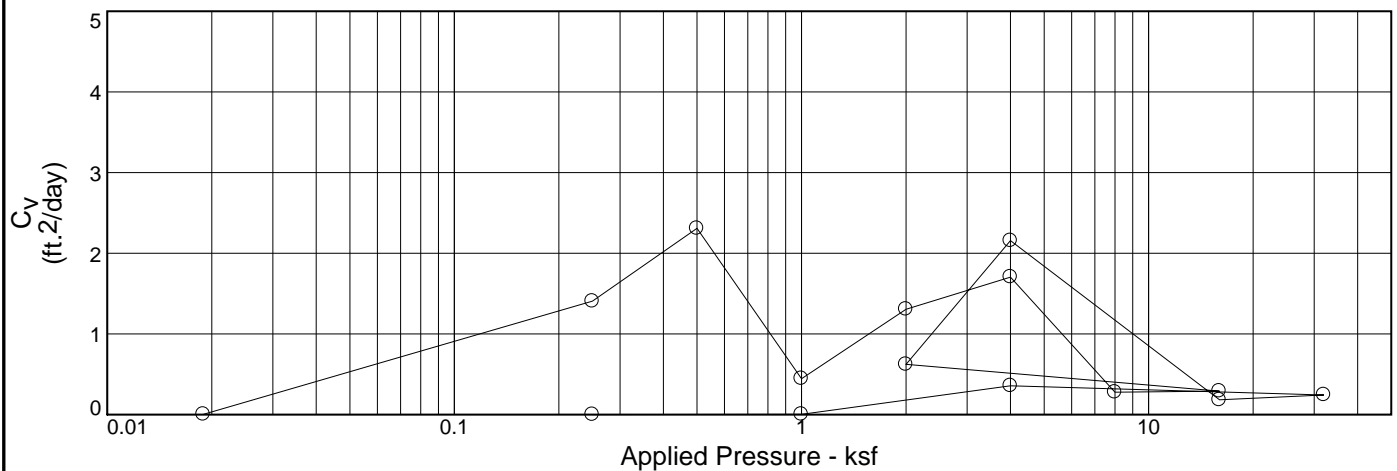


| Natural | | Dry Dens. (pcf) | LL | PI | Sp. Gr. | Overburden (ksf) | P_c (ksf) | C_c | C_r | Initial Void Ratio |
|------------|----------|--------------------|-----|----|---------|---------------------|----------------|-------|-------|--------------------|
| Saturation | Moisture | | | | | | | | | |
| 98.8 % | 64.5 % | 61.0 | 121 | 85 | 2.689 | 0.76 | 3.5 | 0.90 | 0.08 | 1.754 |

| MATERIAL DESCRIPTION | | | | | | | | USCS | AASHTO |
|---|--|--|--|--|--|--|--|------|--------|
| FAT CLAY, gray and dark gray, with organics | | | | | | | | CH | |

| | | | | | |
|---|--|--|--|---|--|
| Project No. 04.55174066 Client: CPRA Project: BAYOU DE CADE MARSH CREATION AND RIDGE RESTORATION Source of Sample: B-02 Depth: 16.0 Sample Number: 9 Fugro USA Land, Inc. Baton Rouge, LA | | | | Remarks: Date Tested: 05/07/2018 Tested by: JK Reviewed by: ERM | |
| | | | | Plate B-5b | |

CONSOLIDATION TEST REPORT

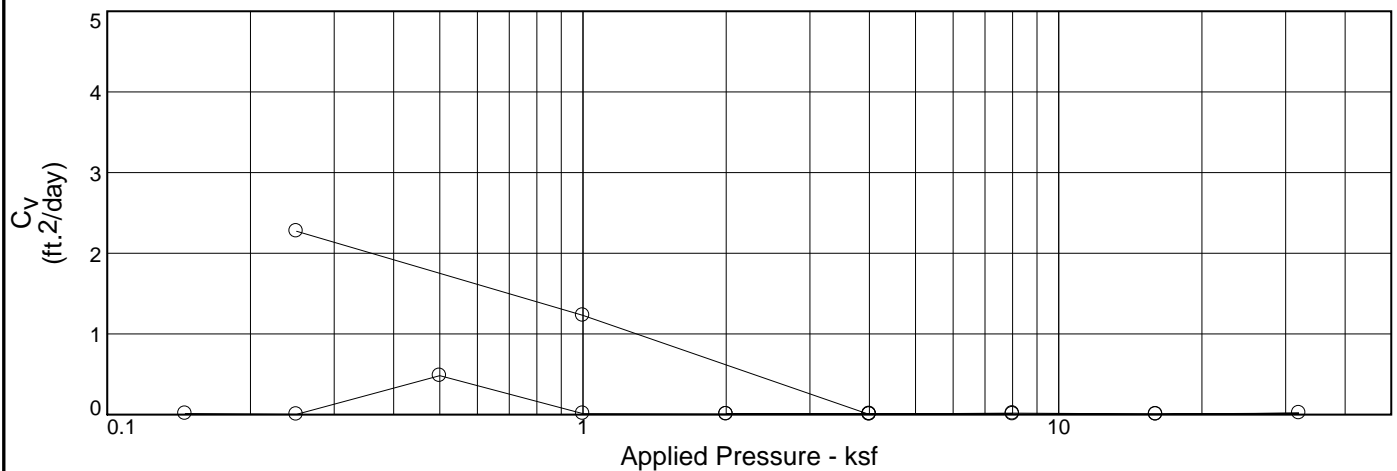
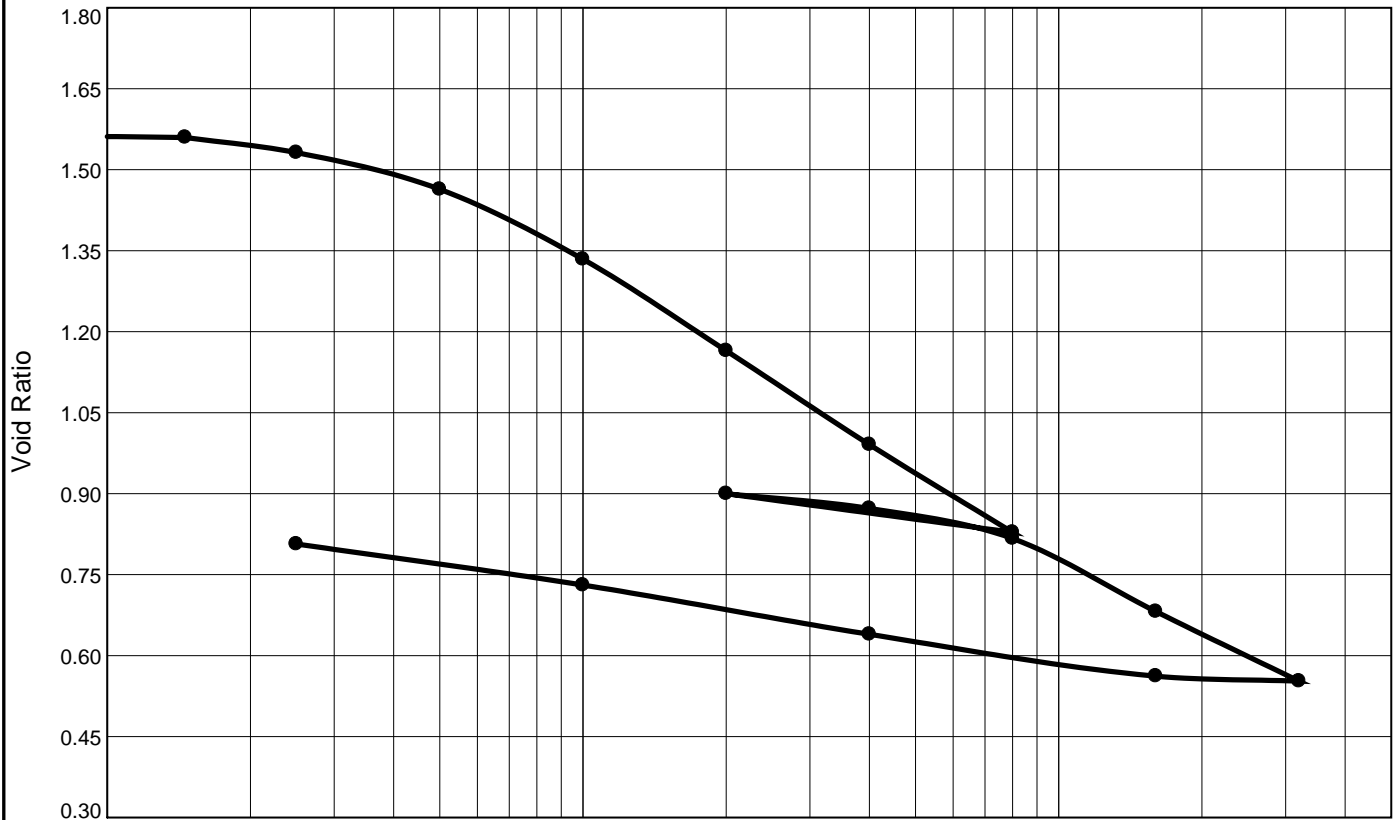


| Natural | | Dry Dens. (pcf) | LL | PI | Sp. Gr. | Overburden (ksf) | P _c (ksf) | C _c | C _r | Initial Void Ratio |
|------------|----------|--------------------|----|----|---------|---------------------|-------------------------|----------------|----------------|-----------------------|
| Saturation | Moisture | | | | | | | | | |
| 97.3 % | 71.8 % | 56.3 | | | 2.70 | 0.10 | 0.3 | 0.61 | 0.06 | 1.992 |

| MATERIAL DESCRIPTION | | | | | | | | USCS | AASHTO |
|--|--|--|--|--|--|--|--|------|--------|
| FAT CLAY, gray, with peat and organics | | | | | | | | CH | |

| | | |
|---|---|---|
| Project No. 04.55174066 | Client: CPRA | Remarks: Date Tested: 06/04/2018 Tested by: JK Reviewed by: ERM Atterber Limit and Specific Gravity test pending. Plate B-5c |
| Project: BAYOU DE CADE MARSH CREATION AND RIDGE RESTORATION | | |
| Source of Sample: B-03 | Depth: 2.0 Sample Number: 2 | |
| Fugro USA Land, Inc. Baton Rouge, LA | | |

CONSOLIDATION TEST REPORT

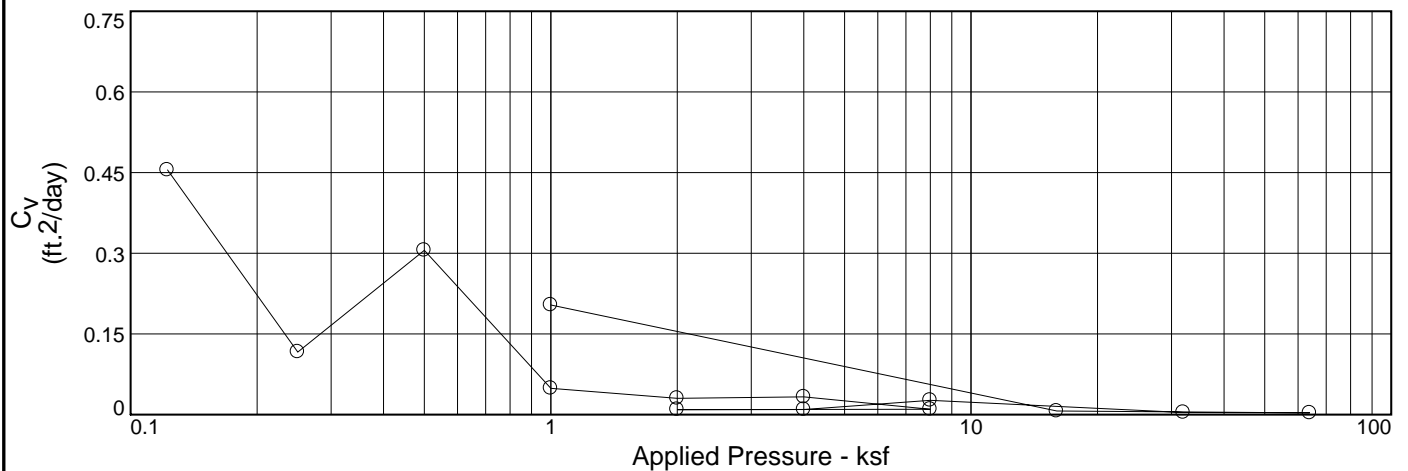
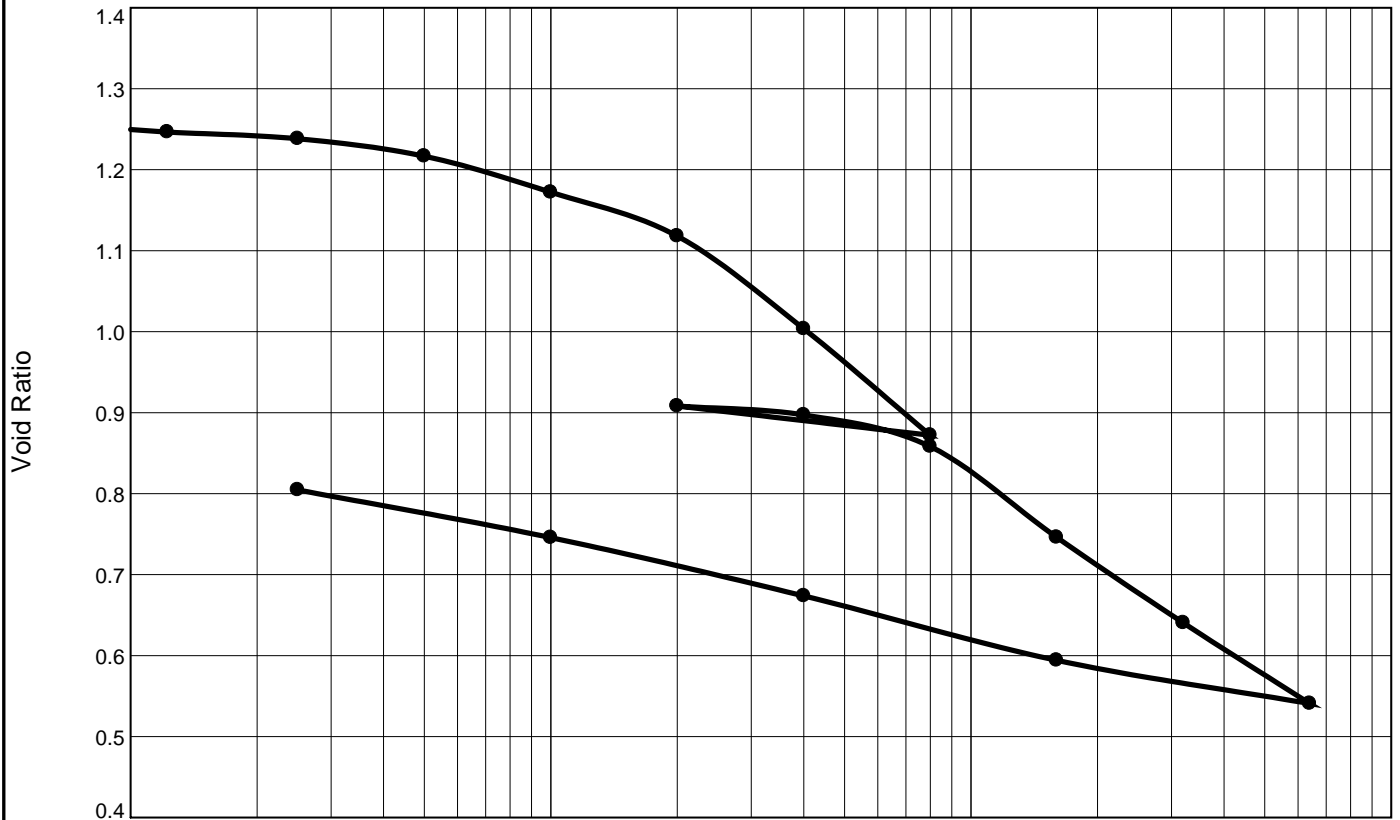


| Natural | | Dry Dens. (pcf) | LL | PI | Sp. Gr. | Overburden (ksf) | P_c (ksf) | C_c | C_r | Initial Void Ratio |
|------------|----------|--------------------|----|----|---------|---------------------|----------------|-------|-------|--------------------|
| Saturation | Moisture | | | | | | | | | |
| 105.5 % | 64.1 % | 62.6 | 60 | 42 | 2.569 | 0.21 | 0.52 | 0.53 | 0.06 | 1.561 |

| MATERIAL DESCRIPTION | | | | | | | | USCS | AASHTO |
|----------------------------------|--|--|--|--|--|--|--|------|--------|
| FAT CLAY, gray, with peat layers | | | | | | | | CH | |

| | | | | | |
|--|--|--|--|---|--|
| Project No. 04.55174066 Client: CPRA Project: BAYOU DE CADE MARSH CREATION AND RIDGE RESTORATION Source of Sample: B-04 Depth: 4.0 Sample Number: 3 Fugro USA Land, Inc. Baton Rouge, LA | | | | Remarks: Date Tested: 05/24/2018 Tested by: JK Reviewed by: ERM | |
| | | | | Plate B-5d | |

CONSOLIDATION TEST REPORT

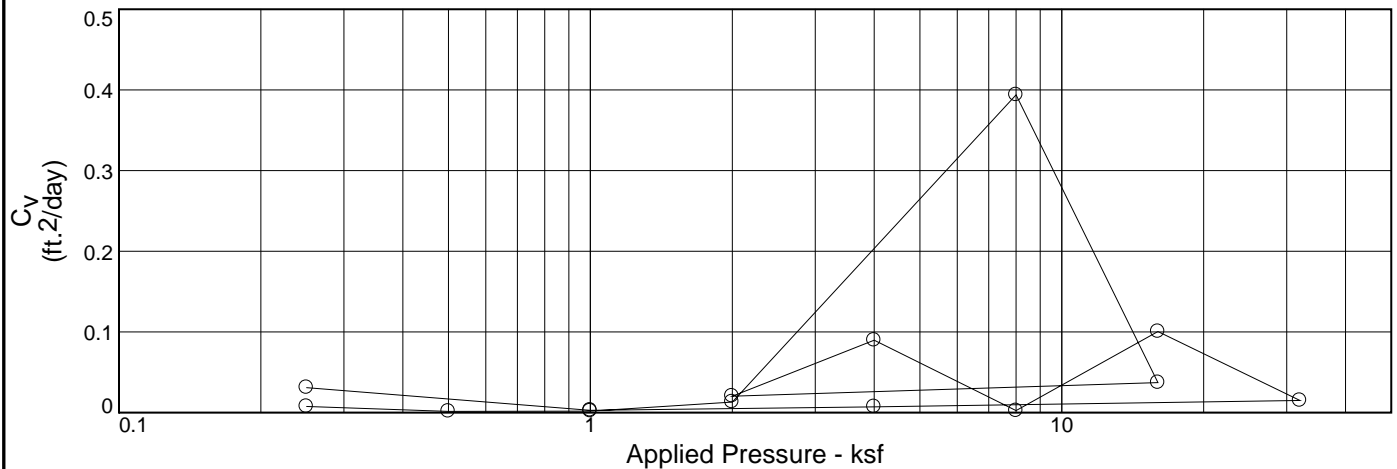
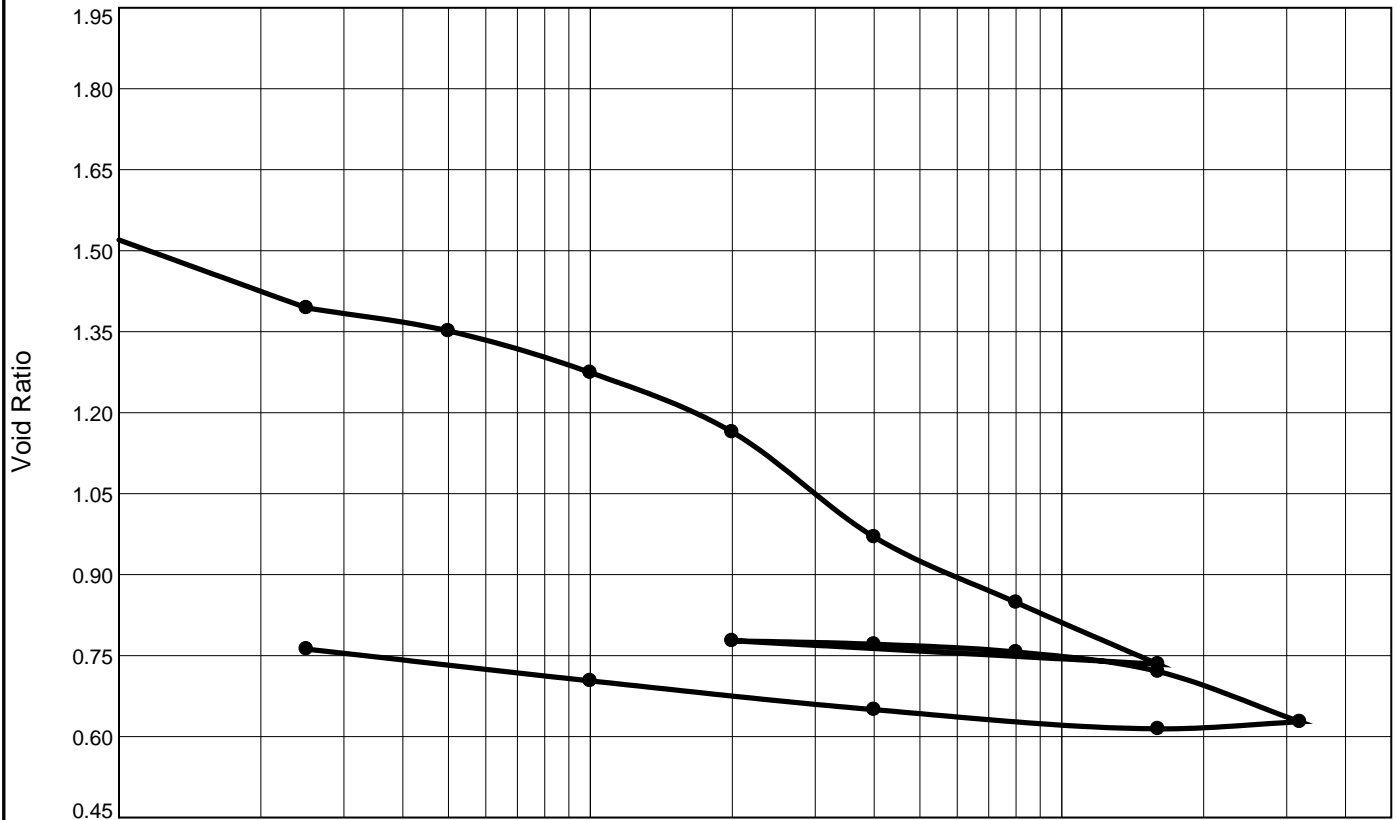


| Natural | | Dry Dens. (pcf) | LL | PI | Sp. Gr. | Overburden (ksf) | P _c (ksf) | C _c | C _r | Initial Void Ratio |
|------------|----------|--------------------|----|----|---------|---------------------|-------------------------|----------------|----------------|--------------------|
| Saturation | Moisture | | | | | | | | | |
| 102.7 % | 49.2 % | 72.3 | 65 | 45 | 2.606 | 0.18 | 1.5 | 0.38 | 0.04 | 1.250 |

| MATERIAL DESCRIPTION | | | | | | | | USCS | AASHTO |
|---------------------------------|--|--|--|--|--|--|--|------|--------|
| FAT CLAY, dark gray, with roots | | | | | | | | CH | |

| | | |
|---|---|---|
| Project No. 04.55174066 | Client: CPRA | Remarks: Date Tested: 05/07/2018 Tested by: JK Reviewed by: ERM |
| Project: BAYOU DE CADE MARSH CREATION AND RIDGE RESTORATION | | |
| Source of Sample: B-05 | Depth: 4.0 Sample Number: 3 | |
| Fugro USA Land, Inc. Baton Rouge, LA | | |
| | | Plate B-5e |

CONSOLIDATION TEST REPORT

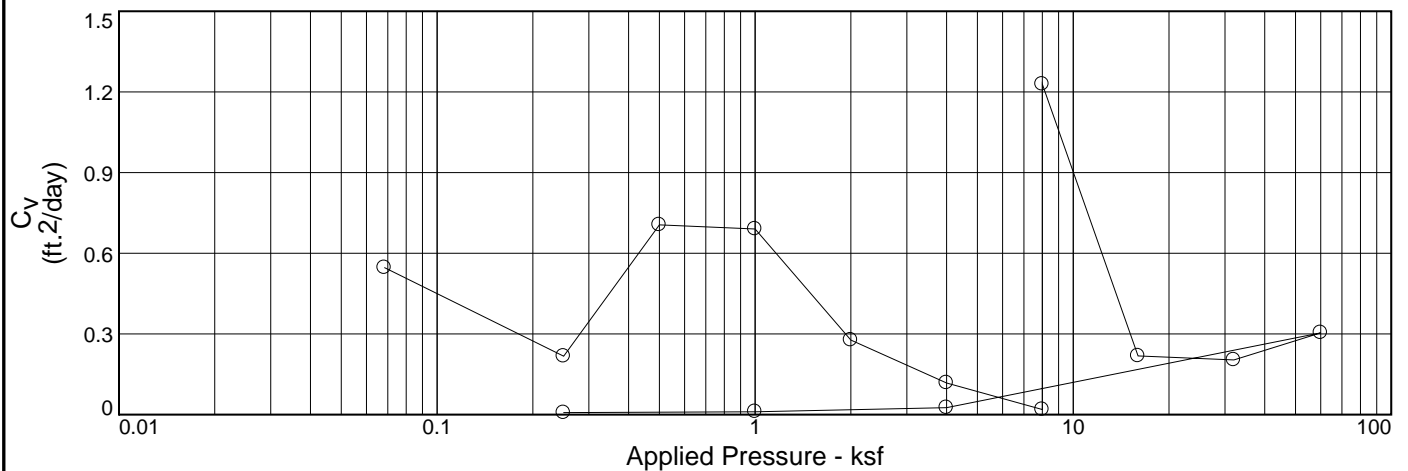
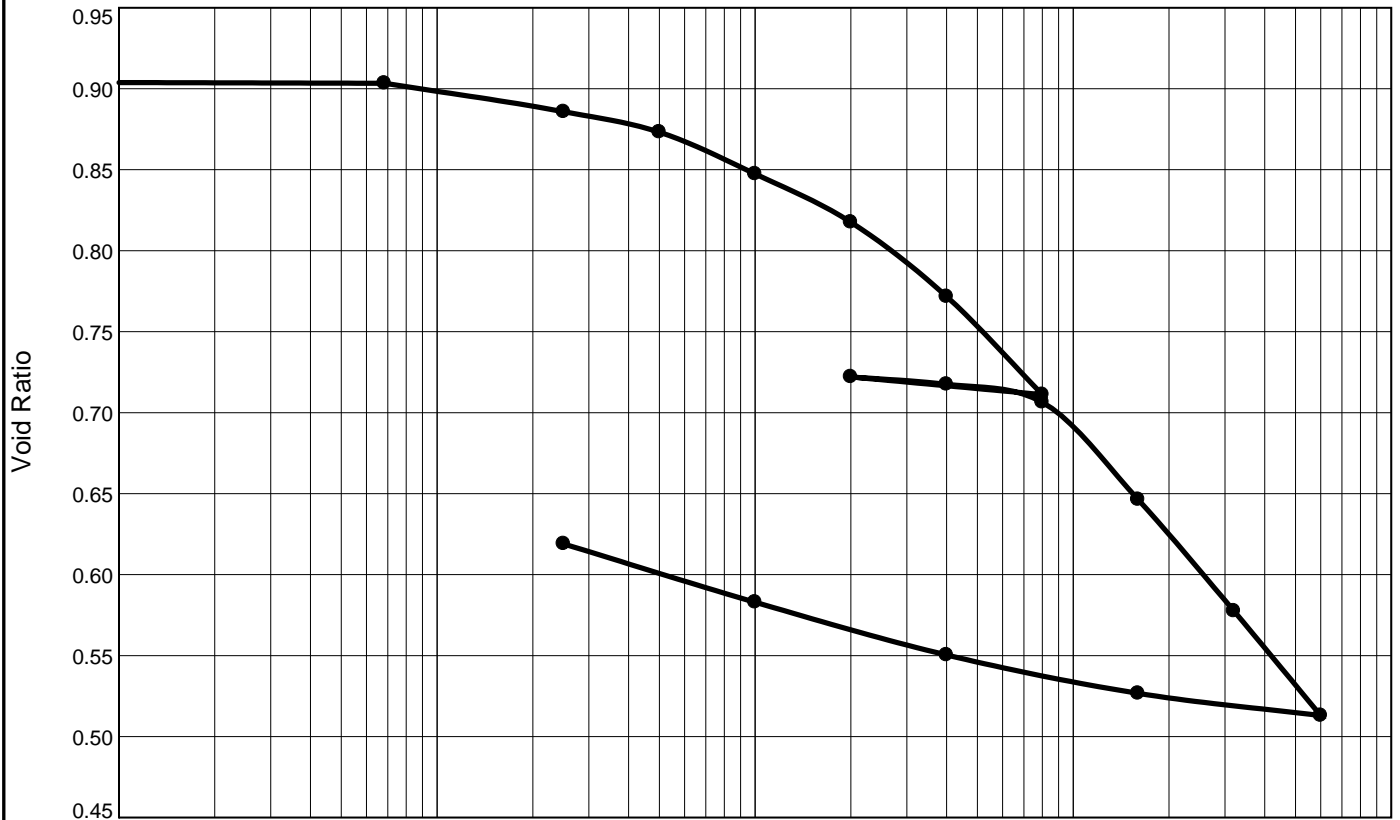


| Natural | | Dry Dens. (pcf) | LL | PI | Sp. Gr. | Overburden (ksf) | P _c (ksf) | C _c | C _r | Initial Void Ratio |
|------------|----------|--------------------|----|----|---------|---------------------|-------------------------|----------------|----------------|--------------------|
| Saturation | Moisture | | | | | | | | | |
| 111.5 % | 66.9 % | 62.8 | 42 | 19 | 2.533 | 0.10 | 1.0 | 0.50 | 0.05 | 1.520 |

| MATERIAL DESCRIPTION | | | | | | | | USCS | AASHTO |
|----------------------|--|--|--|--|--|--|--|------|--------|
| LEAN CLAY, gray | | | | | | | | CL | |

| | | | | | |
|--|--|--|--|---|--|
| Project No. 04.55174066 Client: CPRA Project: BAYOU DE CADE MARSH CREATION AND RIDGE RESTORATION Source of Sample: B-06 Depth: 2.0 Sample Number: 2 Fugro USA Land, Inc. Baton Rouge, LA | | | | Remarks: Date Tested: 06/04/2018 Tested by: JK Reviewed by: ERM | |
| | | | | Plate B-5f | |

CONSOLIDATION TEST REPORT

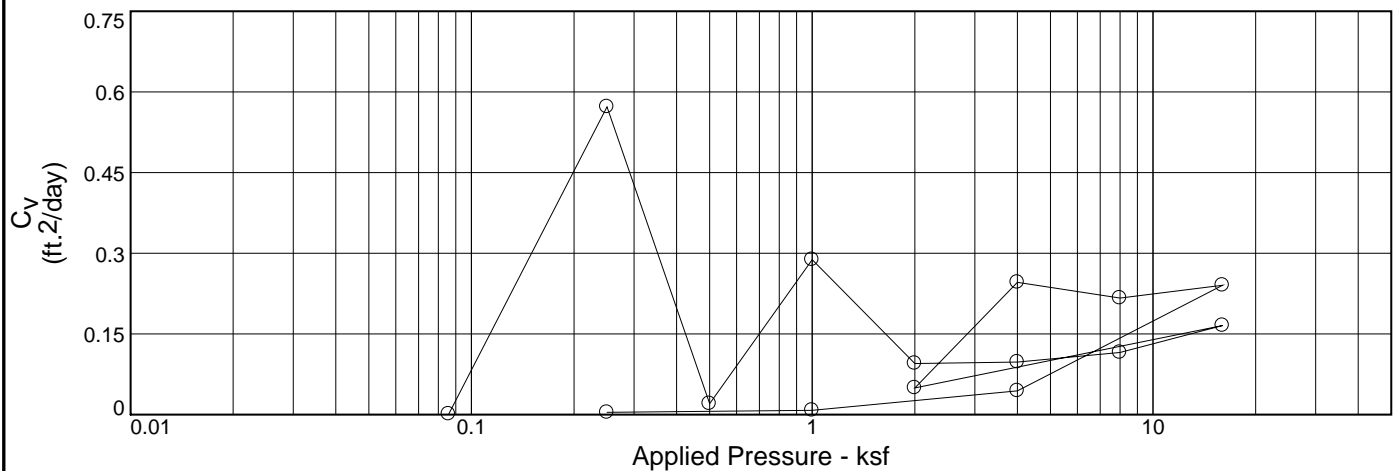
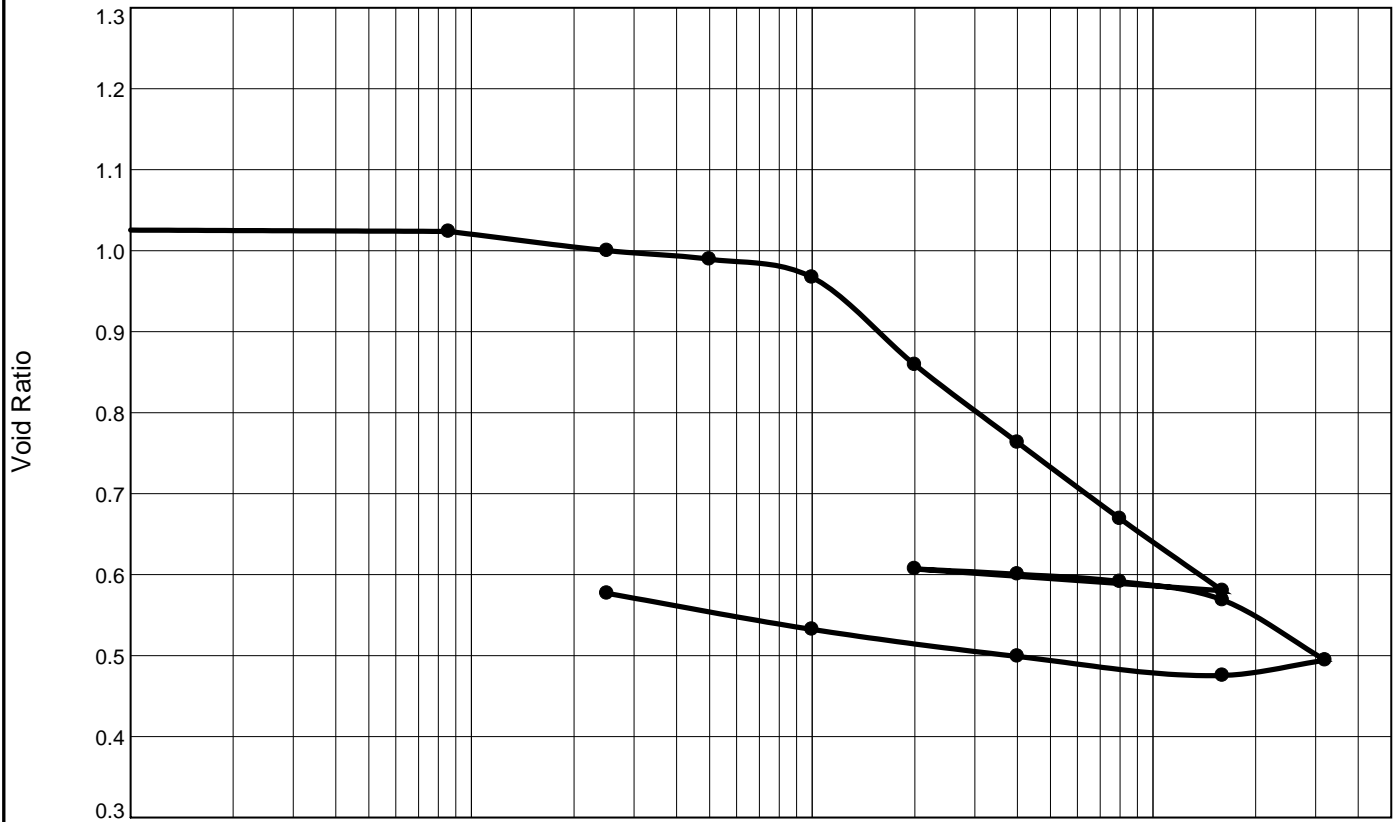


| Natural | | Dry Dens. (pcf) | LL | PI | Sp. Gr. | Overburden (ksf) | P _c (ksf) | C _c | C _r | Initial Void Ratio |
|------------|----------|--------------------|----|----|---------|---------------------|-------------------------|----------------|----------------|--------------------|
| Saturation | Moisture | | | | | | | | | |
| 102.0 % | 35.2 % | 85.8 | 41 | 21 | 2.617 | 0.53 | 2.0 | 0.24 | 0.05 | 0.904 |

| MATERIAL DESCRIPTION | | | | | | | | USCS | AASHTO |
|--|--|--|--|--|--|--|--|------|--------|
| FAT CLAY, gray, with silt pockets and organics | | | | | | | | CH | |

| | | | | | |
|---|--|--|--|---|--|
| Project No. 04.55174066 Client: CPRA Project: BAYOU DE CADE MARSH CREATION AND RIDGE RESTORATION Source of Sample: B-07 Depth: 10.0 Sample Number: 6 Fugro USA Land, Inc. Baton Rouge, LA | | | | Remarks: Date Tested: 05/24/2018 Tested by: JK Reviewed by: ERM | |
| | | | | Plate B-5g | |

CONSOLIDATION TEST REPORT

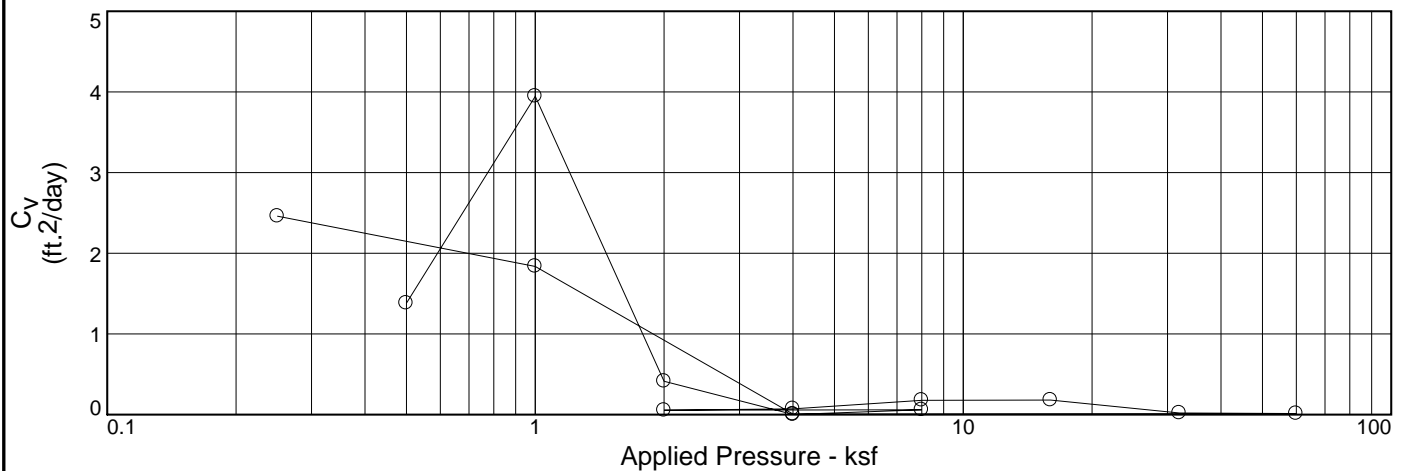
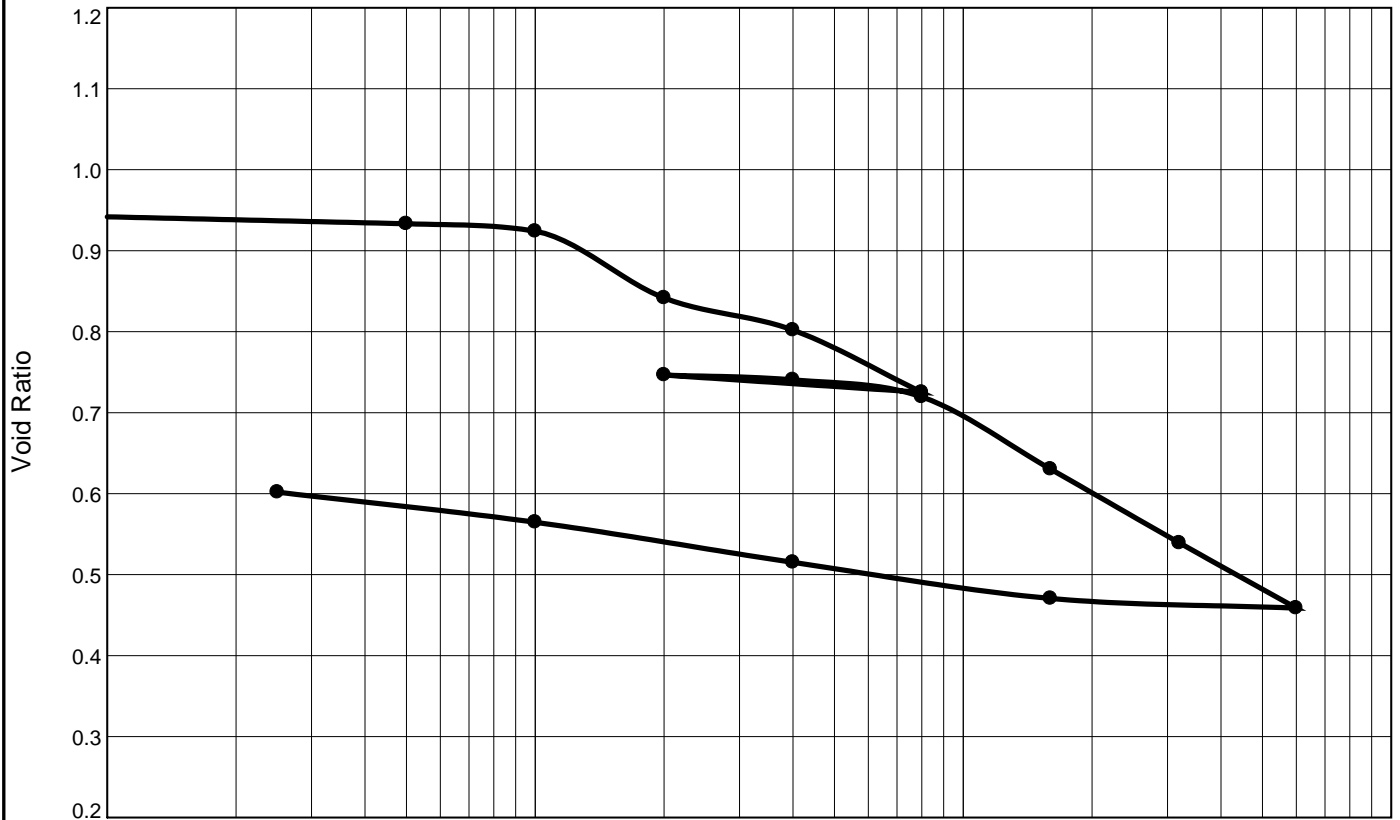


| Natural | | Dry Dens. (pcf) | LL | PI | Sp. Gr. | Overburden (ksf) | P _c (ksf) | C _c | C _r | Initial Void Ratio |
|------------|----------|--------------------|----|----|---------|---------------------|-------------------------|----------------|----------------|--------------------|
| Saturation | Moisture | | | | | | | | | |
| 99.4 % | 39.2 % | 80.1 | 43 | 23 | 2.599 | 0.74 | 1.0 | 0.33 | 0.03 | 1.025 |

| MATERIAL DESCRIPTION | | | | | | | | USCS | AASHTO |
|----------------------|--|--|--|--|--|--|--|------|--------|
| LEAN CLAY, gray | | | | | | | | CL | |

| | | | | | | | | | |
|---|--|--|--|--|--|---|--|--|--|
| Project No. 04.55174066 Client: CPRA Project: BAYOU DE CADE MARSH CREATION AND RIDGE RESTORATION Source of Sample: B-08 Depth: 14.0 Sample Number: 8 Fugro USA Land, Inc. Baton Rouge, LA | | | | | | Remarks: Date Tested: 05/25/2018 Tested by: JK Reviewed by: ERM | | | |
| | | | | | | Plate B-5h | | | |

CONSOLIDATION TEST REPORT

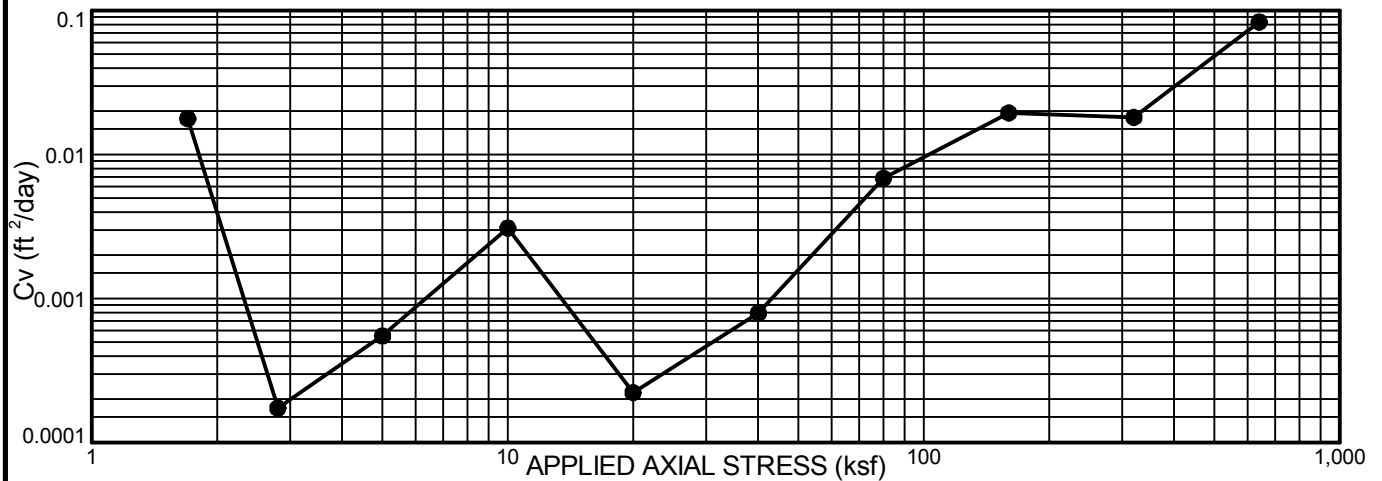
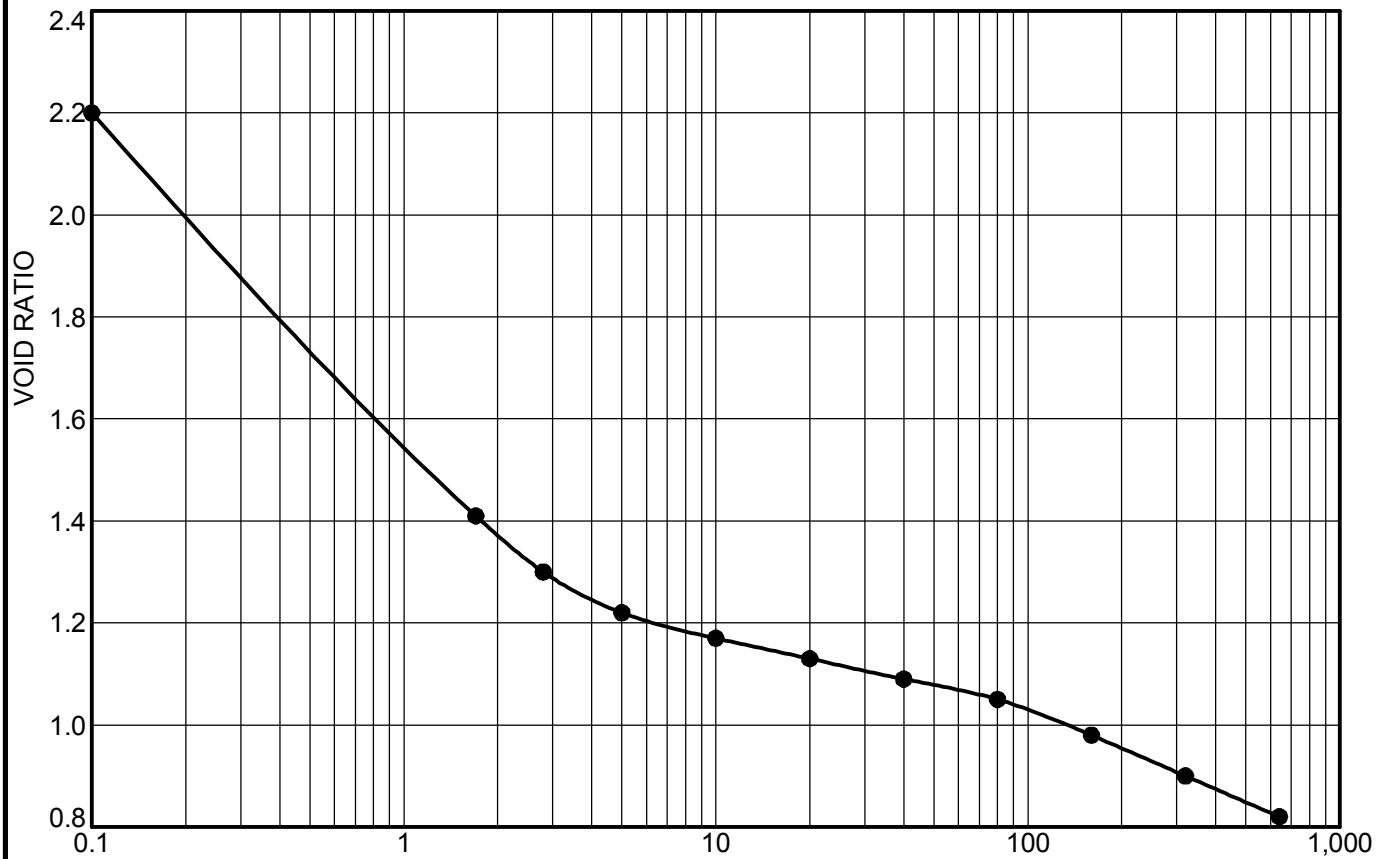


| Natural | | Dry Dens. (pcf) | LL | PI | Sp. Gr. | Overburden (ksf) | P _c (ksf) | C _c | C _r | Initial Void Ratio |
|------------|----------|--------------------|----|----|---------|---------------------|-------------------------|----------------|----------------|--------------------|
| Saturation | Moisture | | | | | | | | | |
| 98.6 % | 35.0 % | 85.2 | 46 | 25 | 2.65 | 0.50 | 2.0 | 0.32 | 0.08 | 0.942 |

| MATERIAL DESCRIPTION | | | | | | | | USCS | AASHTO |
|----------------------|--|--|--|--|--|--|--|------|--------|
| LEAN CLAY, gray | | | | | | | | CL | |

| | | | | | | | | | |
|---|--|--|--|--|--|---|--|--|--|
| Project No. 04.55174066 Client: CPRA Project: BAYOU DE CADE MARSH CREATION AND RIDGE RESTORATION Source of Sample: B-09 Depth: 10.0 Sample Number: 6 Fugro USA Land, Inc. Baton Rouge, LA | | | | | | Remarks: Date Tested: 06/04/2018 Tested by: JK Reviewed by: ERM Specific Gravity test pending. | | | |
| | | | | | | Plate B-5i | | | |

SELF-WEIGHT CONSOLIDATION TEST REPORT



| Initial | | | LL | PI | Sp. Gr. | Pc (ksf) | Cc | Initial Void Ratio |
|--------------|------------|----------------|----|----|---------|----------|-----|--------------------|
| Saturation % | Moisture % | Dry Dens.(pcf) | | | | | | |
| 100.0 | 93.7% | 46.2 | | | 2.35 | N/A | N/A | 2.202 |

MATERIAL DESCRIPTION

FAT CLAY (CH)



Project No. 04.55174066 Client: CPRA

Project: Bayou De Cade Marsh Creation and Ridge Restoration

Source of Sample: Composite B-10 B-12 B-13 from mudline to depth of 10 ft

Remarks:

Test Date: 6/5/2018

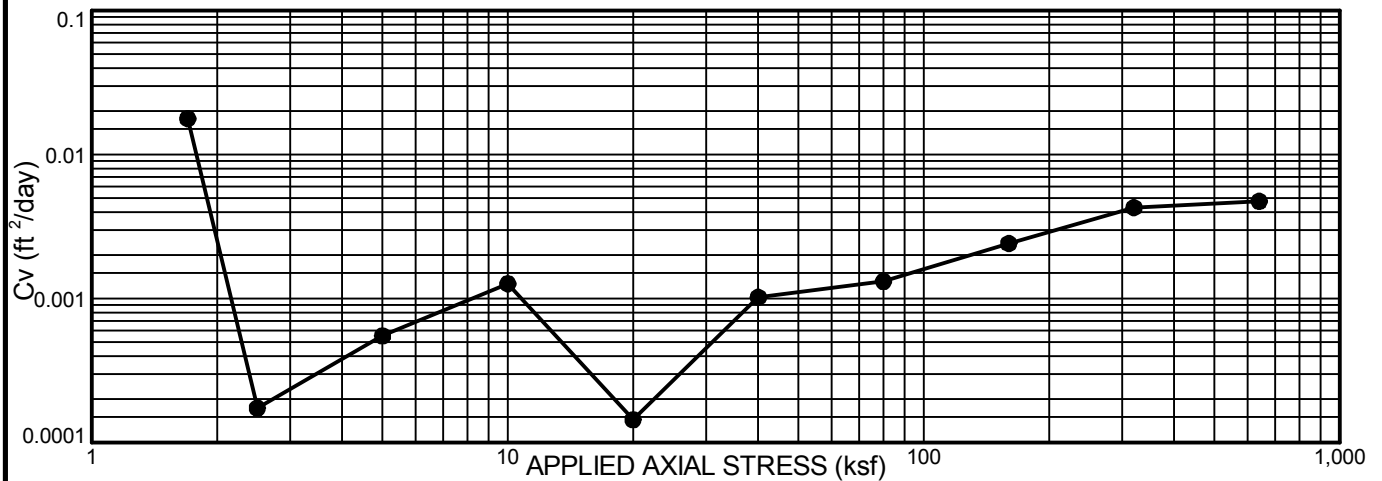
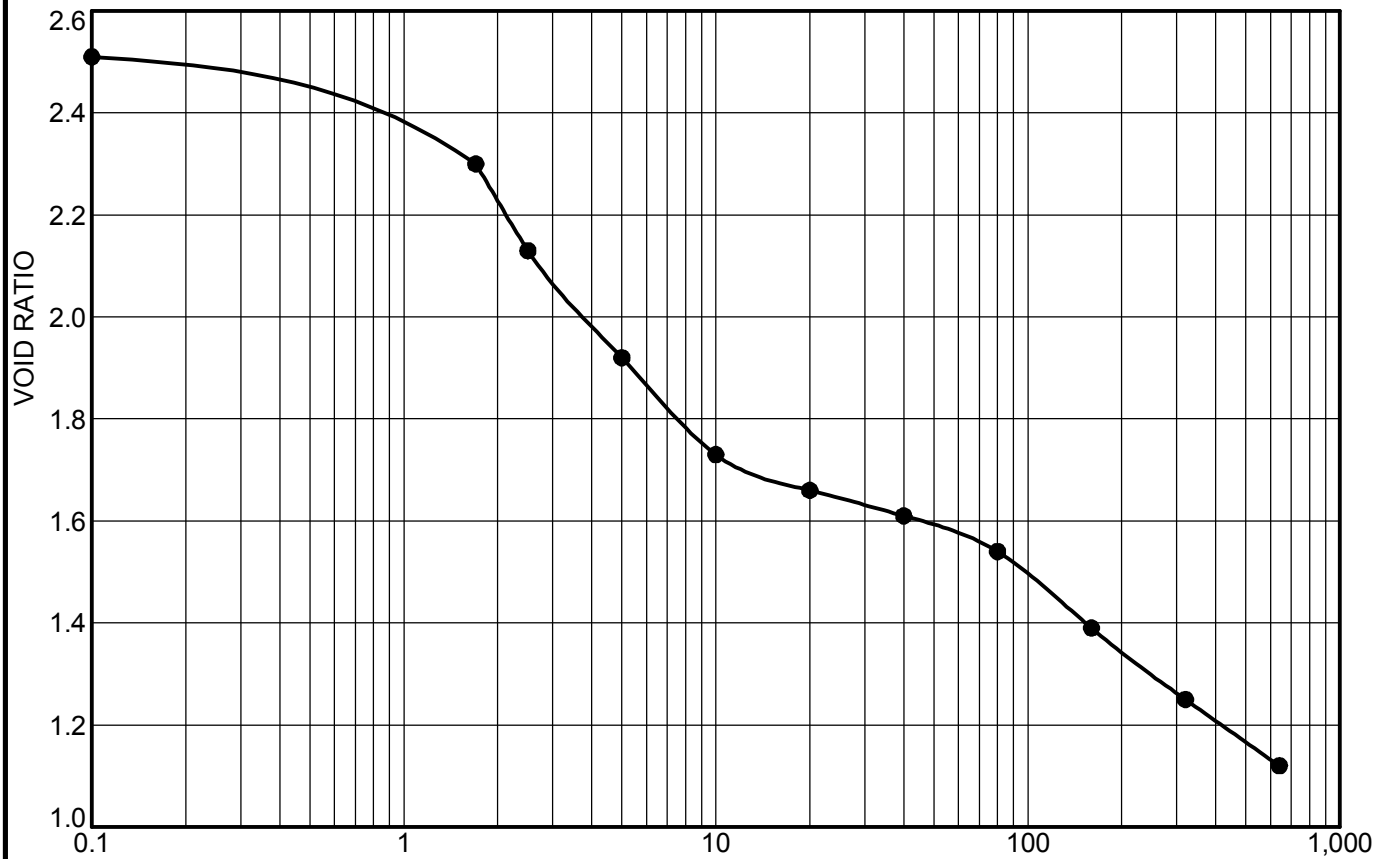
Tested by: Jack Koban

Reviewed by: Sam Bryant

Specific Gravity test pending.

PLATE B-6a

SELF-WEIGHT CONSOLIDATION TEST REPORT



| Initial | | | LL | PI | Sp. Gr. | Pc (ksf) | Cc | Initial Void Ratio |
|--------------|------------|----------------|----|----|---------|----------|-----|--------------------|
| Saturation % | Moisture % | Dry Dens.(pcf) | | | | | | |
| 86.0 | 107.0% | 37.4 | | | 2.35 | N/A | N/A | 2.515 |

MATERIAL DESCRIPTION

FAT CLAY (CH)



Project No. 04.55174066 Client: CPRA

Project: Bayou De Cade Marsh Creation and Ridge Restoration

Source of Sample: Composite B-11 B-14 B-15 from mudline to depth of 10 ft

Remarks:

Test Date: 6/5/2018

Tested by: Jack Koban

Reviewed by: Sam Bryant

Specific Gravity test pending.

PLATE B-6b



APPENDIX B1

COLUMN SETTLING TESTS

Final Report:

**Settling Properties of Fine-Grained Sediments:
Bayou De Cade Marsh Creation and Ridge Restoration (TE-0138)
(Fugro Project No. 04.55174066)**

Submitted to:

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Vice President
Fugro USA Land, Inc.
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June 6, 2018



1.0 Introduction, Scope, and Objectives

The objective of the testing reported here was to evaluate the settling properties of fine-grained sediments which may be hydraulically dredged in support of the Bayou De Cade Marsh Creation and Ridge Restoration (TE-0138) project (Fugro Project No. 04.55174066).

2.0 Experimental Procedures and Results

2.1 Materials Provided for Testing

Two composited sediment samples, each comprised of sediment from three separate borings in the proposed dredging area, were provided by Fugro USA Land, Inc. for pilot-scale settling column testing (see Appendix A for chain of custody forms).

Table 1. Sediment core samples used to prepare fine-grained sediment slurry for pilot-scale settling column testing

| Composited Sediment Boring IDs |
|---|
| B-10, B-12, B-13 |
| B-11, B-14, B-15 |

A five-gallon bucket of water from the proposed dredging area was also provided by Fugro USA Land, Inc. for laboratory testing. The salinity of the water sample, measured gravimetrically with drying at 180 °C¹, was 0.39 parts per thousand (ppt) indicative of a freshwater environment.

As requested by Fugro USA Land, Inc., a separate settling column test was conducted using each of the composited sediment samples. Testing procedures and results from each of the two tests are presented in the following sections.

2.2 Pilot-Scale Settling Column Test Results for Composite of Sediment from Boring ID Numbers B-10, B-12, and B-13

The first settling column test utilized sediment composited from boring ID numbers B-10, B-12, and B-13. Slurry was prepared by mixing homogenized sediment from the three borings with tap water supplemented with a small amount of synthetic sea salts (Instant Ocean) to match the average salinity of the site water sample [salinity of 0.39 parts per thousand (ppt)]. Slurry containing the fine-grained fraction of sediments was obtained by thoroughly mixing the slurry and then allowing coarse grained materials (e.g., sand and shells), to separate by differential settling as described in the US Army Corps of Engineers Manual No. 1110-2-5027¹. Preliminary solids concentrations measured in the fine-grained sediment slurry revealed that the particulate concentration was below the initial target concentration of 150 g/L. In consultation with Fugro, a decision was made to proceed with testing at the highest fine-grained particulate concentration that could be achieved with the materials provided.

The fine-grained sediment slurry was transferred to a second mixing barrel, thoroughly mixed, and then loaded into a large-scale (8.0 inch ID) column while mixing with air sparging as described in the US Army Corps of Engineers Manual No. 1110-2-5027¹. Solids concentrations in the slurry at the start of the settling test were measured in samples collected along the height of the column at one foot intervals (see Table B1 in Appendix B for tabulated data). The average particulate concentration at the start of the settling test was 71.0 g/L.

A readily visible sediment-water interface was observed less than one hour after the start of the settling test, indicating zone settling. The height of the sediment-water interface above the bottom of the column was measured and recorded over a period lasting more than 30 days as depicted in Figure 1 (see Table C1 in Appendix C for tabulated data). As shown in Figure 1, zone settling was observed during the first portion of the settling test, followed by compression settling thereafter.

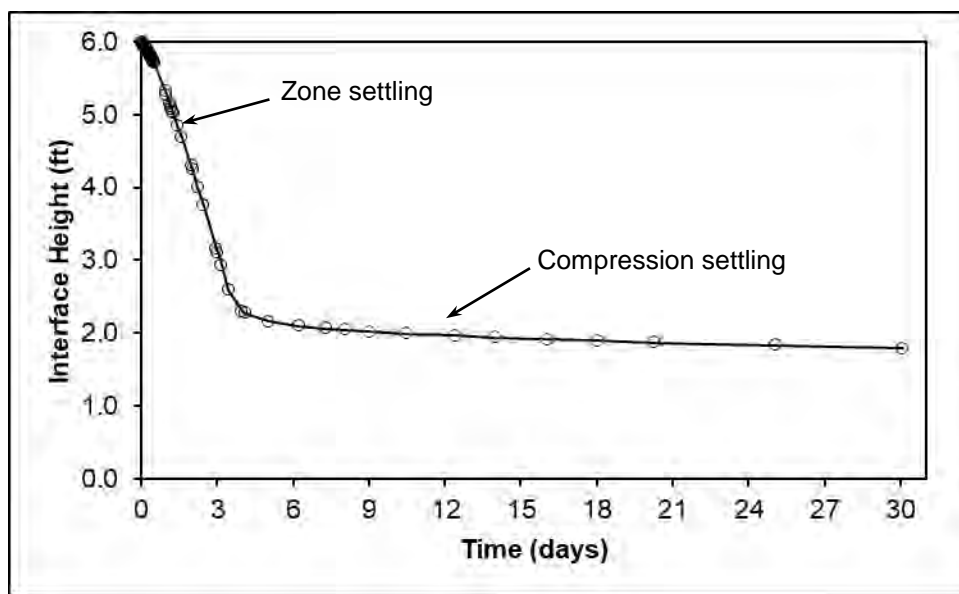


Figure 1. Interface height as a function of time during the pilot-scale settling test with composite of sediment from borings B-10, B-12, and B-13.

Interface heights from the first 90 hours of the settling test, during which zone settling was observed, are depicted separately in Figure 2. A linear regression was performed for settling data in this time interval with the resulting equation and correlation coefficient shown on the graph. The slope of the regression line, which corresponds to the zone settling velocity, was 0.0406 ft/hr (0.97 ft/day).

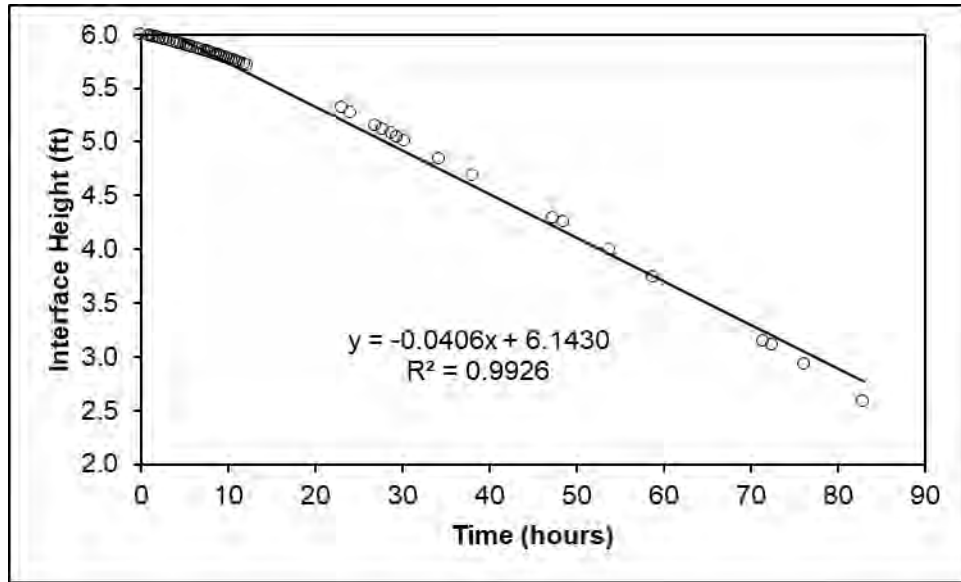


Figure 2. Interface height as a function of time during the zone settling portion of the pilot-scale settling test with composite of borings B-10, B-12, and B-13.

For the portion of the settling test during which compression settling was observed, the concentration in the settled solids at each time interval was calculated using the following equation (equation 3-11 in ref. 1).

$$C = \frac{C_o H_i}{H_t}$$

Where:

C = slurry suspended solids concentration at time t (g/L)

C_o = initial slurry suspended solids concentration (g/L)

H_i = initial slurry height (ft)

H_t = height of the interface at time t (ft)

The corresponding particulate concentration in the settled sediment as a function of time during compression settling is depicted in Figure 3.

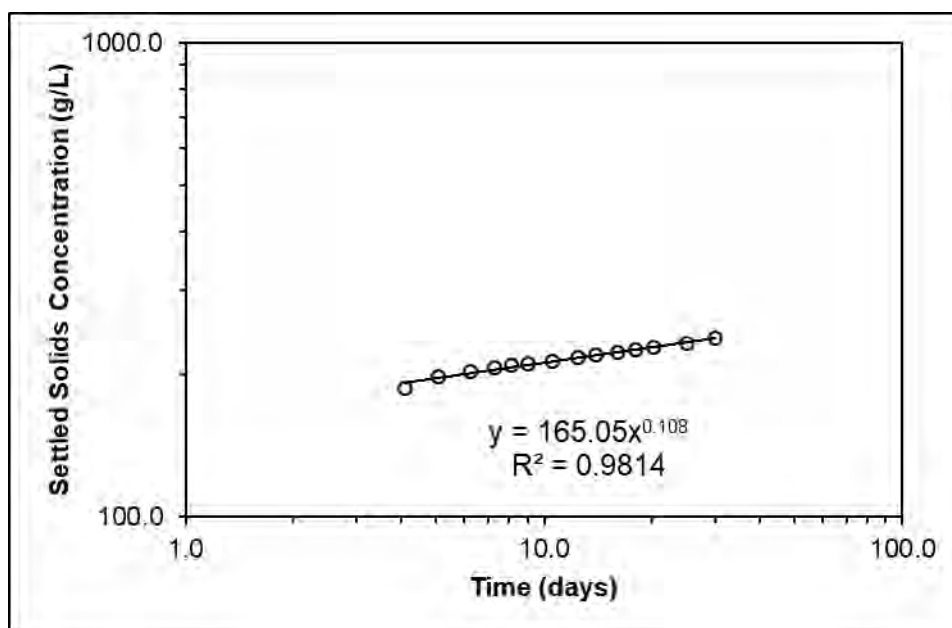


Figure 3. Concentration of settled solids as a function of time during the compression settling portion of the pilot-scale settling test with composite of borings B-10, B-12, and B-13.

For analysis of flocculent settling as described in the US Army Corps of Engineers Manual No. 1110-2-5027¹, water samples were collected from the clarified layer above the sediment-water interface for measurement of total suspended (TSS) following Standard Method 2450D². The first of these samples, collected 24 hours after the start of settling when the sediment-water interface was sufficiently below the uppermost sample port (height of 5.5 ft) to allow sample collection, had a TSS concentration of 740 mg/L. TSS concentrations decreased over time but remained above 100 mg/L after 176 hours (7.3 days) and above 50 mg/L even after 434 hours (18.1 days) settling. Tabulated data are provided in Table D1 in Appendix D.

2.3 Pilot-Scale Settling Column Test using Composite of Sediment from Boring ID Numbers B-11, B-14, and B-15

The second pilot-scale settling column test utilized sediment composited from boring ID numbers B-11, B-14, and B-15. Slurry was prepared by mixing homogenized sediment from the three borings with tap water supplemented with a small amount of synthetic sea salts (Instant Ocean) to match the average salinity of the site water sample [salinity of 0.39 parts per thousand (ppt)]. Slurry containing the fine-grained fraction of sediments was obtained by thoroughly mixing the slurry and then allowing coarse grained materials (e.g., sand and shells), to separate by differential settling as described in the US Army Corps of Engineers Manual No. 1110-2-5027¹. The fine-grained sediment slurry was transferred to a second mixing barrel, thoroughly mixed, and then loaded into a large-scale (8.0 inch ID) column while mixing with air sparging as described in the US Army Corps of Engineers Manual No. 1110-2-5027¹. Solids concentrations in the slurry at the start of the settling test were measured in samples collected along the height of the column at one foot intervals (see Table B2 in Appendix B for tabulated data). The average particulate concentration at the start of the settling test was 139.5 g/L.

A readily visible sediment-water interface was observed shortly (<2 hours) after the start of the settling test, indicating zone settling. The height of the sediment-water interface above the bottom of the column was measured and recorded over a period lasting more than 30 days as depicted in Figure 4 (see Table C2 in Appendix C for tabulated data). As shown in Figure 4, zone settling was observed during the initial portion of the settling test, followed by compression settling.

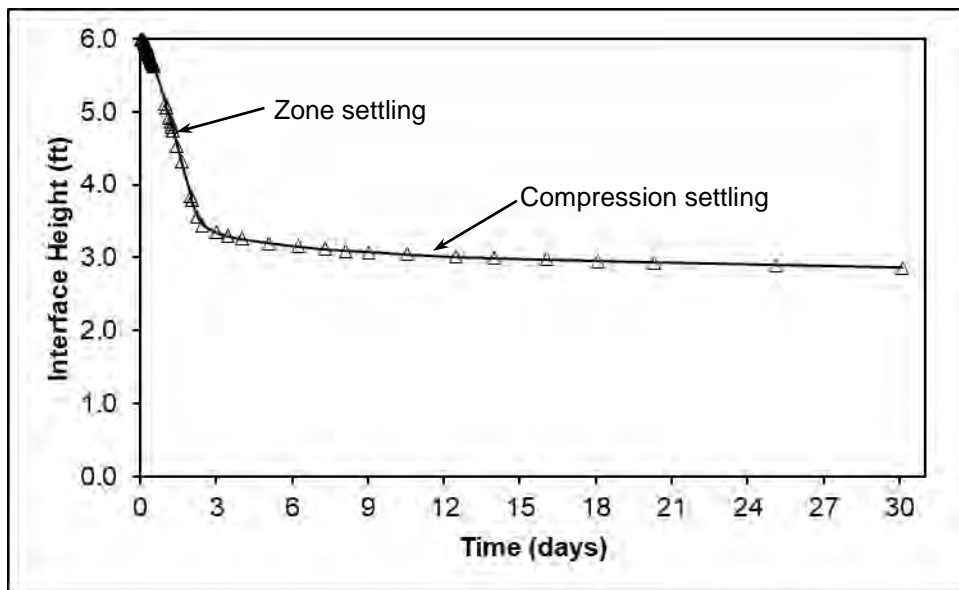


Figure 4. Interface height as a function of time during the pilot-scale settling test with fine grained sediment prepared using a composite of sediment from borings B-11, B-14, and B-15.

Data from the first 60 hours of the settling test are depicted separately in Figure 5. A linear regression was performed for settling data in the time interval of 3 to 60 hours (during which zone settling was observed) with the resulting equation and correlation coefficient shown on the graph. The slope of the regression line, which corresponds to the zone settling velocity, was 0.047 ft/hr (1.13 ft/day).

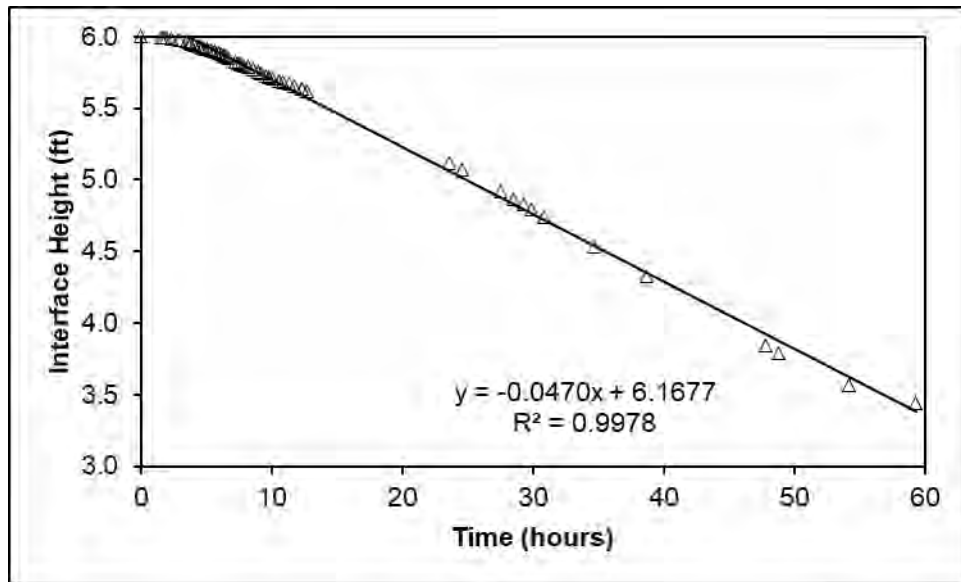


Figure 5. Interface height as a function of time during the zone settling portion of the pilot-scale settling test with composite of borings B-11, B-14, and B-15.

For the portion of the settling test during which compression settling was observed, the concentration in the settled solids at each time interval was calculated as described previously (using equation 3-11 in ref. 1). The corresponding suspended solids concentration as a function of time during compression settling is depicted in Figure 6.

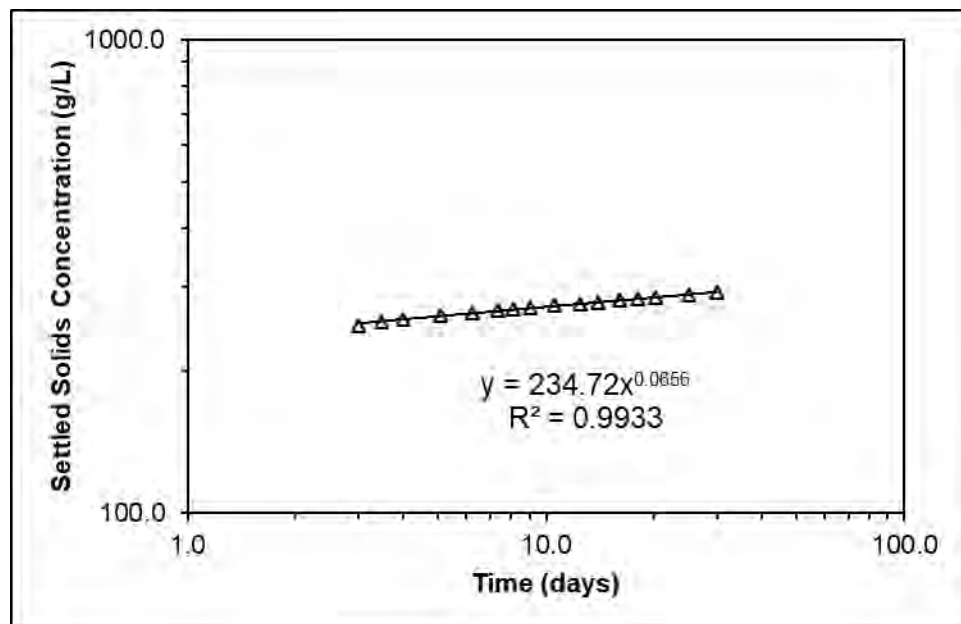


Figure 6: Concentration of settled solids as a function of time during the compression settling portion of the pilot-scale settling test with composite of borings B-11, B-14, and B-15.

For analysis of flocculent settling as described in the US Army Corps of Engineers Manual No. 1110-2-5027¹, water samples were collected from the clarified layer above the sediment-water interface for measurement of total suspended (TSS) following Standard Method 2450D². The first of these samples, collected 24 hours after the start of settling, had a TSS concentration of 180 mg/L. Concentrations decreased over time, and all elevations sampled (i.e., water from all ports above the sediment-water interface) had TSS concentrations <100 mg/L after 96 hours (4 days) and <50 mg/L after 336 hours (14 days) settling time. Tabulated data are provided in Table D2 in Appendix D.

2.4 Data Comparisons

For comparison purposes, the settling behavior observed during the zone settling interval for composited sediment from borings B-10, B-12, and B-13 ($C_o=71.0$ g/L) is shown along with zone settling data collected during testing of composited sediment from borings B-11, B-14, and B-15 ($C_o= 139.5$ g/L). As shown in Figure 7, the zone settling behavior was similar for both samples but with slightly faster zone settling with the B-11, B-14, and B-15 composite (0.0470 ft/hr, 1.13 ft/day) than the B-10, B-12, and B-13 composite (0.0406 ft/hr, 0.97 ft/day).

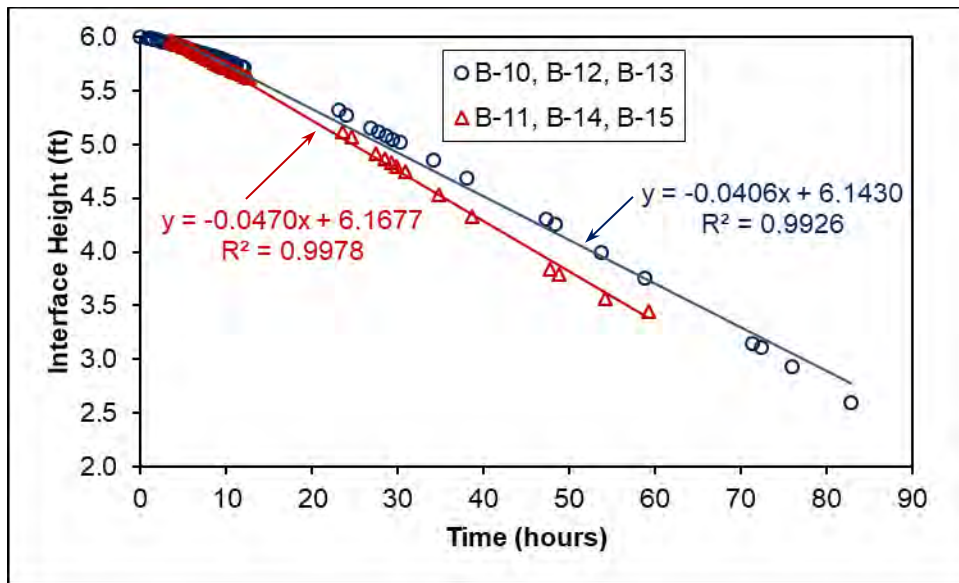


Figure 7: Interface height as a function of time during the zone settling portion of the two pilot-scale settling column tests.

Also for comparison purposes, the compression settling behavior of the settled solids in the two pilot-scale settling column tests is shown below in Figure 8. As shown in the figure, the two composited sediment samples exhibited markedly different compression settling, with the fine-grained sediments from the B-11, B-14, and B-15 composite compacting to a much higher solids concentration than the B-10, B-12, and B-13 composite.

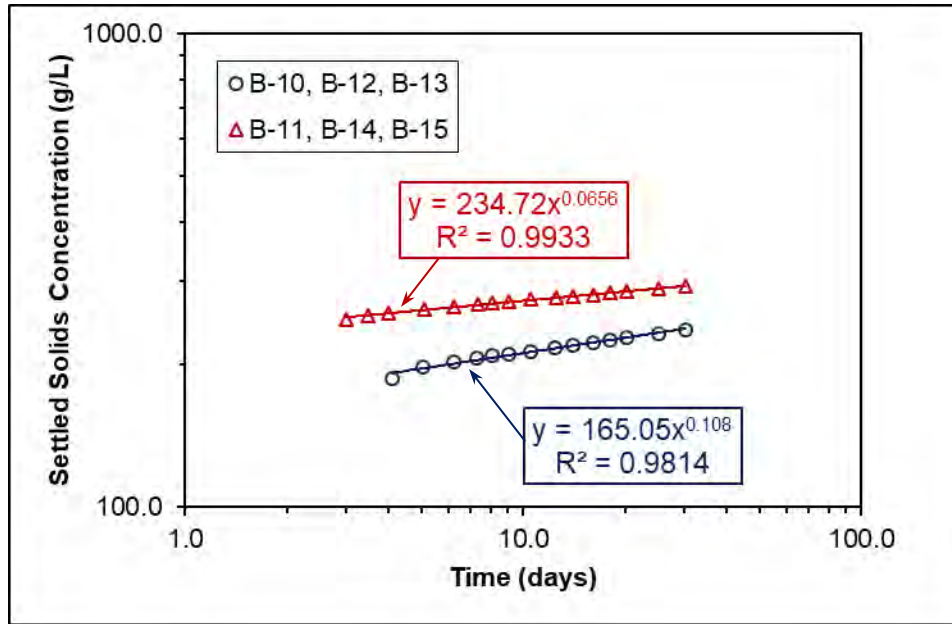


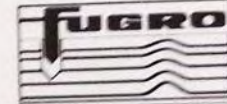
Figure 8: Concentration of settled solids as a function of time during the compression settling portion of the pilot-scale settling tests conducted with fine-grained sediment slurry.

3.0 References

- [1] US Army Corps of Engineers (1987) *Engineering and Design - Confined Disposal of Dredged Material*, Engineer Manual No. 1110-2-5027.
- [2] American Public Health Association (1998) *Standard Methods for the Examination of Water and Wastewater*, 20th Edition, American Water Works Association, Water Pollution Control Federation, Washington, DC.

Appendix A

Fugro Consultants, Inc.
4233 Rhoda Dr., Baton Rouge, LA 70816
Telephone 225.292.5084
Fax 225.292.8084



CHAIN OF CUSTODY

| Project No. 55174066 | | Project Name BDC | | | Location | | | | | | | | | |
|---|------|---------------------|---------------------------------|----------------------------------|--------------|--------------------|---|---|---|---|---|---|----------|--|
| Sample ID (Fugro Lab/Client Sample ID) | Date | Time | Sample Container (Size/Type) | Sample Type (liquid, Soil, etc.) | Preservative | Analyses Requested | | | | | | | Comments | |
| | | | | | | A | B | C | D | E | F | G | | |
| B-10 | 4/27 | | | Soil | | X | | | | | | | | |
| Q | | | | | | | | | | | | | | |
| B | | | | | | | | | | | | | | |
| 0-2 | | | | | | | | | | | | | | |
| 2-4 | | | | | | | | | | | | | | |
| 4-5.5 | | | | | | | | | | | | | | |
| 6-7.5 | | | | | | | | | | | | | | |
| B-10 | | | | | | | | | | | | | | |
| B-10(2) | | | | | | | | | | | | | | |
| — | | | | | | | | | | | | | | |
| B-12 | | | | | | | | | | | | | | |
| Q | | | | | | | | | | | | | | |
| B | | | | | | | | | | | | | | |
| 0-2 | | | | | | | | | | | | | | |
| 2-4 | | | | | | | | | | | | | | |
| 4-6 | | | | | | | | | | | | | | |
| 6-7.5 | | | | | | | | | | | | | | |
| B-10 | | | | | | | | | | | | | | |
| B-10 | | | | | | | | | | | | | | |

| | | | |
|------------------|---------|-------|--------------|
| Relinquished By: | Date | Time | Received By: |
| | 4/26/18 | 10:45 | William Mae |
| Remarks | | | |
| 1 of 3 | | | |

| | |
|-----------|-----------------|
| Analyses: | |
| A | Col. J. H. King |
| B | |
| C | |
| D | |
| E | |
| F | |
| G | |

Fugro Consultants, Inc.
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CHAIN OF CUSTODY

| Project No. 55174066 | | Project Name BDC | | | Location | | | | | | | | |
|---|-------------|-------------------------|---------------------------------|-------------------------------------|--------------|--------------------|---|---|---|---|---|---|----------|
| Sample ID (Fugro Lab/Client Sample ID) | Date | Time | Sample Container (Size/Type) | Sample Type (liquid, Soil, etc.) | Preservative | Analyses Requested | | | | | | | Comments |
| | | | | | | A | B | C | D | E | F | G | |
| B-13 | 4/27 | | | Soil | | X | | | | | | | |
| Q-2 | | | | | | | | | | | | | |
| B | | | | | | | | | | | | | |
| 0-2 | | | | | | | | | | | | | |
| 2-3.5 | | | | | | | | | | | | | |
| 4-4.5 | | | | | | | | | | | | | |
| 4-5.5 | | | | | | | | | | | | | |
| G-8 | | | | | | | | | | | | | |
| 8-10 | | | | | | | | | | | | | |
| B-14 | | | | | | | | | | | | | |
| Q | | | | | | | | | | | | | |
| 2-4 | | | | | | | | | | | | | |
| 2-4 | | | | | | | | | | | | | |
| 4-6 (2) | | | | | | | | | | | | | |
| 6-8 | | | | | | | | | | | | | |
| 8-10 | | | | | | | | | | | | | |
| 8-10 | | | | | | | | | | | | | |

| | | | |
|-----------------------|----------------|--------------|--------------------|
| Relinquished By: | Date | Time | Received By: |
| | 4/30/16 | 10:45 | William Mae |
| Remarks 2 of 3 | | | |

| | |
|-----------|---------------------|
| Analyses: | |
| A | Cal Settling |
| B | |
| C | |
| D | |
| E | |
| F | |
| G | |

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CHAIN OF CUSTODY

| Project No. 55174066 | | Project Name BDC | | | | Location | | | | | | | |
|---|------|----------------------------|---------------------------------|----------------------------------|--------------|--------------------|---|---|---|---|---|---|----------|
| Sample ID (Fugro Lab/Client Sample ID) | Date | Time | Sample Container (Size/Type) | Sample Type (liquid, Soil, etc.) | Preservative | Analyses Requested | | | | | | | Comments |
| | | | | | | A | B | C | D | E | F | G | |
| B-15 Q | 4/27 | | | Soil | | X | | | | | | | |
| B 0-2 | | | | | | | | | | | | | |
| 2-4 (2) | | | | | | | | | | | | | |
| 4-6 | | | | | | | | | | | | | |
| 4-5-6 | | | | | | | | | | | | | |
| 6-8 | | | | | | | | | | | | | |
| 8-10 | | | | | | | | | | | | | |
| B-11 Q | | | | | | | | | | | | | |
| B 0-2 (A,B,C,D) | | | | | | | | | | | | | |
| 2-4 (A,E) | | | | | | | | | | | | | |
| 4-6 | | | | | | | | | | | | | |
| 6-8 | | | | | | | | | | | | | |
| 8-10 | | | | | | | | | | | | | |

| | | | |
|--|-----------------|---------------|-----------------------------|
| Relinquished By: <i>[Signature]</i> | Date 4/30/12 | Time 10:45 | Received By: William Mae |
| Remarks 3 of 3 | | | |

| | |
|-----------|---------------|
| Analyses: | |
| A | Col. Settling |
| B | |
| C | |
| D | |
| E | |
| F | |
| G | |

Print 4492

White - Original Yellow - DFR Pink - Lab Binder Gold - Deliverer

Appendix B

Table B1. Particulate concentrations measured in samples collected from side ports at the start (t=0) of the pilot-scale settling column test using composited sediment from borings B-10, B-12, and B-13.

| Port height (ft) ^a | Particulate Conc. (g/L) |
|-------------------------------|-------------------------|
| 1.0 | 72.1 |
| 2.0 | 70.5 |
| 3.0 | 70.5 |
| 4.0 | 70.7 |
| 5.0 | 71.1 |
| 6.0 | 71.4 |
| Average | 71.0 |

^a As measured from the bottom of the column

Table B2. Particulate concentrations measured in samples collected from side ports at the start (t=0) of the pilot-scale settling column test using composited sediment from borings B-11, B-14, and B-15.

| Port height (ft) ^a | Particulate Conc. (g/L) |
|-------------------------------|-------------------------|
| 1.0 | 140.0 |
| 2.0 | 140.0 |
| 3.0 | 139.3 |
| 4.0 | 139.6 |
| 5.0 | 138.7 |
| 6.0 | 139.1 |
| Average | 139.5 |

^a As measured from the bottom of the column

Appendix C

Table C1. Interface height as a function of time during the pilot-scale column settling test using composited sediment from B-10, B-12, and B-13.

The height of the sediment-water interface above the bottom of the column was recorded as a function of time as summarized in the table below.

| Elapsed Time (hr) | Elapsed Time (days) | Solids Interface Height (ft) | Head height (ft) | Settled Solids Conc. (g/L) ^a |
|-------------------|---------------------|------------------------------|------------------|---|
| 0.00 | 0.000 | 6.000 | 6.000 | 71.0 |
| 0.88 | 0.037 | 5.992 | 6.000 | 71.1 |
| 1.15 | 0.048 | 5.988 | 6.000 | 71.1 |
| 1.45 | 0.060 | 5.979 | 6.000 | 71.2 |
| 1.90 | 0.079 | 5.975 | 6.000 | 71.3 |
| 2.18 | 0.091 | 5.967 | 6.000 | 71.4 |
| 2.55 | 0.106 | 5.958 | 6.000 | 71.5 |
| 2.93 | 0.122 | 5.950 | 6.000 | 71.6 |
| 3.33 | 0.139 | 5.942 | 6.000 | 71.7 |
| 3.73 | 0.156 | 5.933 | 6.000 | 71.8 |
| 4.17 | 0.174 | 5.925 | 6.000 | 71.9 |
| 4.48 | 0.187 | 5.917 | 6.000 | 72.0 |
| 4.92 | 0.205 | 5.908 | 6.000 | 72.1 |
| 5.22 | 0.217 | 5.900 | 6.000 | 72.2 |
| 5.57 | 0.232 | 5.892 | 6.000 | 72.3 |
| 5.85 | 0.244 | 5.883 | 6.000 | 72.4 |
| 6.57 | 0.274 | 5.867 | 6.000 | 72.6 |
| 6.88 | 0.287 | 5.858 | 6.000 | 72.7 |
| 7.25 | 0.302 | 5.850 | 6.000 | 72.8 |
| 7.60 | 0.317 | 5.842 | 6.000 | 72.9 |
| 7.93 | 0.331 | 5.833 | 6.000 | 73.0 |
| 8.32 | 0.347 | 5.825 | 6.000 | 73.1 |
| 8.60 | 0.358 | 5.817 | 6.000 | 73.2 |
| 8.93 | 0.372 | 5.808 | 6.000 | 73.3 |
| 9.23 | 0.385 | 5.800 | 6.000 | 73.4 |
| 9.50 | 0.396 | 5.792 | 6.000 | 73.6 |
| 9.78 | 0.408 | 5.783 | 6.000 | 73.7 |
| 10.05 | 0.419 | 5.775 | 6.000 | 73.8 |

^a Calculated using equation 3-11 in ref. 1 based on the measured particulate concentrations at t=0 and the height of the sediment-water interface at each time interval.

Table C1. Continued from previous page

| Elapsed Time (hr) | Elapsed Time (days) | Solids Interface Height (ft) | Head height (ft) | Settled Solids Conc. (g/L)^a |
|--------------------------|----------------------------|-------------------------------------|-------------------------|---|
| 10.33 | 0.431 | 5.767 | 6.000 | 73.9 |
| 10.67 | 0.444 | 5.758 | 6.000 | 74.0 |
| 10.95 | 0.456 | 5.750 | 6.000 | 74.1 |
| 11.23 | 0.468 | 5.742 | 6.000 | 74.2 |
| 11.83 | 0.493 | 5.725 | 6.000 | 74.4 |
| 12.10 | 0.504 | 5.717 | 6.000 | 74.5 |
| 23.08 | 0.962 | 5.317 | 6.000 | 80.1 |
| 24.05 | 1.002 | 5.275 | 5.983 | 80.8 |
| 26.92 | 1.122 | 5.154 | 5.983 | 82.7 |
| 27.80 | 1.158 | 5.117 | 5.983 | 83.3 |
| 28.70 | 1.196 | 5.079 | 5.983 | 83.9 |
| 29.42 | 1.226 | 5.050 | 5.983 | 84.4 |
| 30.23 | 1.260 | 5.017 | 5.975 | 84.9 |
| 34.18 | 1.424 | 4.850 | 5.975 | 87.8 |
| 38.10 | 1.588 | 4.688 | 5.975 | 90.9 |
| 47.33 | 1.972 | 4.300 | 5.975 | 99.1 |
| 48.43 | 2.018 | 4.254 | 5.975 | 100.1 |
| 53.70 | 2.238 | 4.000 | 5.975 | 106.5 |
| 58.78 | 2.449 | 3.750 | 5.975 | 113.6 |
| 71.43 | 2.976 | 3.150 | 5.975 | 135.2 |
| 72.45 | 3.019 | 3.108 | 5.867 | 137.1 |
| 76.07 | 3.169 | 2.933 | 5.867 | 145.2 |
| 82.95 | 3.456 | 2.592 | 5.867 | 164.4 |
| 95.45 | 3.977 | 2.304 | 5.867 | 184.9 |
| 98.47 | 4.103 | 2.275 | 5.783 | 187.3 |
| 121.22 | 5.051 | 2.158 | 5.783 | 197.4 |
| 149.42 | 6.226 | 2.100 | 5.704 | 202.9 |
| 175.32 | 7.305 | 2.063 | 5.621 | 206.5 |
| 193.88 | 8.078 | 2.042 | 5.529 | 208.7 |
| 216.43 | 9.018 | 2.023 | 5.529 | 210.6 |
| 252.28 | 10.51 | 1.996 | 5.442 | 213.4 |
| 298.33 | 12.43 | 1.963 | 5.442 | 217.1 |
| 335.43 | 13.98 | 1.942 | 5.442 | 219.4 |

^a Calculated using equation 3-11 in ref. 1 based on the measured particulate concentrations at t=0 and the height of the sediment-water interface at each time interval.

Table C1. Continued from previous page

| Elapsed Time (hr) | Elapsed Time (days) | Solids Interface Height (ft) | Head height (ft) | Settled Solids Conc. (g/L)^a |
|--------------------------|----------------------------|-------------------------------------|-------------------------|---|
| 385.38 | 16.06 | 1.917 | 5.338 | 222.3 |
| 433.43 | 18.06 | 1.893 | 5.338 | 225.0 |
| 486.50 | 20.27 | 1.871 | 5.258 | 227.7 |
| 602.10 | 25.09 | 1.829 | 5.258 | 232.9 |
| 722.22 | 30.09 | 1.792 | 5.258 | 237.8 |

^a Calculated using equation 3-11 in ref. 1 based on the measured particulate concentrations at t=0 and the height of the sediment-water interface at each time interval.

Table C2. Interface height as a function of time during the pilot-scale column settling test using composited sediment from borings B-11, B-14, and B-15.

The height of the sediment-water interface above the bottom of the column was recorded as a function of time as summarized in the table below.

| Elapsed Time (hr) | Elapsed Time (days) | Solids Interface Height (ft) | Head height (ft) | Settled Solids Conc. (g/L) ^a |
|-------------------|---------------------|------------------------------|------------------|---|
| 0.00 | 0.000 | 6.000 | 6.000 | 139.5 |
| 1.52 | 0.063 | 5.996 | 6.000 | 139.6 |
| 1.72 | 0.072 | 5.996 | 6.000 | 139.6 |
| 1.93 | 0.081 | 5.992 | 6.000 | 139.7 |
| 2.33 | 0.097 | 5.983 | 6.000 | 139.9 |
| 2.87 | 0.119 | 5.975 | 6.000 | 140.1 |
| 3.45 | 0.144 | 5.967 | 6.000 | 140.3 |
| 3.65 | 0.152 | 5.958 | 6.000 | 140.5 |
| 3.82 | 0.159 | 5.950 | 6.000 | 140.7 |
| 4.12 | 0.172 | 5.942 | 6.000 | 140.9 |
| 4.50 | 0.188 | 5.933 | 6.000 | 141.1 |
| 4.67 | 0.194 | 5.925 | 6.000 | 141.3 |
| 4.87 | 0.203 | 5.917 | 6.000 | 141.5 |
| 5.07 | 0.211 | 5.908 | 6.000 | 141.7 |
| 5.32 | 0.222 | 5.900 | 6.000 | 141.9 |
| 5.60 | 0.233 | 5.892 | 6.000 | 142.1 |
| 5.90 | 0.246 | 5.883 | 6.000 | 142.3 |
| 6.12 | 0.255 | 5.875 | 6.000 | 142.5 |
| 6.28 | 0.262 | 5.867 | 6.000 | 142.7 |
| 6.42 | 0.267 | 5.858 | 6.000 | 142.9 |
| 6.60 | 0.275 | 5.850 | 6.000 | 143.1 |
| 7.17 | 0.299 | 5.825 | 6.000 | 143.7 |
| 7.40 | 0.308 | 5.817 | 6.000 | 143.9 |
| 7.58 | 0.316 | 5.808 | 6.000 | 144.1 |
| 7.78 | 0.324 | 5.800 | 6.000 | 144.3 |
| 8.15 | 0.340 | 5.783 | 6.000 | 144.7 |
| 8.58 | 0.358 | 5.767 | 6.000 | 145.1 |
| 8.98 | 0.374 | 5.750 | 6.000 | 145.6 |
| 9.17 | 0.382 | 5.742 | 6.000 | 145.8 |
| 9.60 | 0.400 | 5.725 | 6.000 | 146.2 |

^a Calculated using equation 3-11 in ref. 1 based on the measured particulate concentrations at t=0 and the height of the sediment-water interface at each time interval.

Table C2. Continued from previous page.

| Elapsed Time (hr) | Elapsed Time (days) | Solids Interface Height (ft) | Head height (ft) | Settled Solids Conc. (g/L)^a |
|--------------------------|----------------------------|-------------------------------------|-------------------------|---|
| 9.78 | 0.408 | 5.717 | 6.000 | 146.4 |
| 10.07 | 0.419 | 5.708 | 6.000 | 146.6 |
| 10.52 | 0.438 | 5.692 | 6.000 | 147.1 |
| 10.83 | 0.451 | 5.683 | 6.000 | 147.3 |
| 11.30 | 0.471 | 5.667 | 6.000 | 147.7 |
| 11.75 | 0.490 | 5.650 | 6.000 | 148.1 |
| 12.28 | 0.512 | 5.633 | 6.000 | 148.6 |
| 12.68 | 0.528 | 5.617 | 6.000 | 149.0 |
| 23.62 | 0.984 | 5.117 | 6.000 | 163.6 |
| 24.55 | 1.023 | 5.067 | 5.983 | 165.2 |
| 27.48 | 1.145 | 4.917 | 5.983 | 170.2 |
| 28.45 | 1.185 | 4.867 | 5.983 | 172.0 |
| 29.28 | 1.220 | 4.825 | 5.983 | 173.5 |
| 29.90 | 1.246 | 4.792 | 5.983 | 174.7 |
| 30.87 | 1.286 | 4.742 | 5.958 | 176.5 |
| 34.72 | 1.447 | 4.538 | 5.958 | 184.5 |
| 38.67 | 1.611 | 4.325 | 5.958 | 193.5 |
| 47.83 | 1.993 | 3.842 | 5.958 | 217.9 |
| 48.83 | 2.035 | 3.792 | 5.892 | 220.7 |
| 54.17 | 2.257 | 3.563 | 5.892 | 234.9 |
| 59.30 | 2.471 | 3.442 | 5.892 | 243.2 |
| 71.93 | 2.997 | 3.350 | 5.892 | 249.9 |
| 83.50 | 3.479 | 3.296 | 5.817 | 254.0 |
| 95.98 | 3.999 | 3.258 | 5.817 | 256.9 |
| 121.78 | 5.074 | 3.196 | 5.754 | 261.9 |
| 149.93 | 6.247 | 3.150 | 5.692 | 265.7 |
| 175.88 | 7.328 | 3.117 | 5.629 | 268.6 |
| 194.42 | 8.101 | 3.096 | 5.567 | 270.4 |
| 216.98 | 9.041 | 3.075 | 5.567 | 272.2 |
| 252.82 | 10.53 | 3.046 | 5.492 | 274.8 |
| 298.87 | 12.45 | 3.017 | 5.492 | 277.5 |
| 335.98 | 14.00 | 2.996 | 5.492 | 279.4 |
| 385.88 | 16.08 | 2.974 | 5.442 | 281.4 |

^a Calculated using equation 3-11 in ref. 1 based on the measured particulate concentrations at t=0 and the height of the sediment-water interface at each time interval.

Table C2. Continued from previous page.

| Elapsed Time (hr) | Elapsed Time (days) | Solids Interface Height (ft) | Head height (ft) | Settled Solids Conc. (g/L)^a |
|--------------------------|----------------------------|-------------------------------------|-------------------------|---|
| 433.93 | 18.08 | 2.954 | 5.442 | 283.3 |
| 487.00 | 20.29 | 2.933 | 5.363 | 285.3 |
| 602.65 | 25.11 | 2.896 | 5.363 | 289.0 |
| 722.77 | 30.12 | 2.863 | 5.363 | 292.4 |

^a Calculated using equation 3-11 in ref. 1 based on the measured particulate concentrations at t=0 and the height of the sediment-water interface at each time interval.

Appendix D

Table D1. Total suspended solids (TSS) concentrations measured above the sediment-water interface for characterization of flocculent settling during the pilot-scale column settling test using composited sediment from borings B-10, B-12, and B-13.

| Sample Extraction Time (hr) | Port Height (ft) ^a | Head Height (ft) ^a | Depth of Sample Extraction (ft) ^b | TSS (mg/L) |
|-----------------------------|-------------------------------|-------------------------------|--|------------|
| 24 | 5.50 | 6.00 | 0.50 | 740 |
| 30 | 5.50 | 5.98 | 0.48 | 662 |
| 48 | 5.50 | 5.98 | 0.48 | 364 |
| 48 | 5.00 | 5.98 | 0.98 | 420 |
| 48 | 4.50 | 5.98 | 1.48 | 731 |
| 72 | 5.50 | 5.98 | 0.48 | 252 |
| 72 | 5.00 | 5.98 | 0.98 | 258 |
| 72 | 4.50 | 5.98 | 1.48 | 276 |
| 72 | 4.00 | 5.98 | 1.98 | 366 |
| 72 | 3.50 | 5.98 | 2.48 | 531 |
| 96 | 5.50 | 5.87 | 0.37 | 148 |
| 96 | 5.00 | 5.87 | 0.87 | 200 |
| 96 | 4.50 | 5.87 | 1.37 | 210 |
| 96 | 4.00 | 5.87 | 1.87 | 234 |
| 96 | 3.50 | 5.87 | 2.37 | 240 |
| 96 | 3.00 | 5.87 | 2.87 | 264 |
| 96 | 2.50 | 5.87 | 3.37 | 338 |
| 122 | 5.50 | 5.78 | 0.28 | 89 |
| 122 | 5.00 | 5.78 | 0.78 | 171 |
| 122 | 4.50 | 5.78 | 1.28 | 179 |
| 122 | 4.00 | 5.78 | 1.78 | 180 |
| 122 | 3.50 | 5.78 | 2.28 | 180 |
| 122 | 3.00 | 5.78 | 2.78 | 188 |
| 122 | 2.50 | 5.78 | 3.28 | 196 |
| 150 | 5.50 | 5.70 | 0.20 | 59 |
| 150 | 5.00 | 5.70 | 0.70 | 112 |
| 150 | 4.50 | 5.70 | 1.20 | 137 |
| 150 | 4.00 | 5.70 | 1.70 | 142 |
| 150 | 3.50 | 5.70 | 2.20 | 143 |
| 150 | 3.00 | 5.70 | 2.70 | 143 |
| 150 | 2.50 | 5.70 | 3.20 | 147 |

^a As measured from the bottom of the column; ^b Relative to the top liquid level

Table D1. Continued from previous page

| Sample Extraction Time (hr) | Port Height (ft) ^a | Head Height (ft) ^a | Depth of Sample Extraction (ft) ^b | TSS (mg/L) |
|-----------------------------------|-------------------------------------|-------------------------------------|---|---------------|
| 176 | 5.50 | 5.62 | 0.12 | 29 |
| 176 | 5.00 | 5.62 | 0.62 | 101 |
| 176 | 4.50 | 5.62 | 1.12 | 108 |
| 176 | 4.00 | 5.62 | 1.62 | 109 |
| 176 | 3.50 | 5.62 | 2.12 | 113 |
| 176 | 3.00 | 5.62 | 2.62 | 117 |
| 176 | 2.50 | 5.62 | 3.12 | 119 |
| 217 | 5.50 | 5.53 | 0.03 | 27 |
| 217 | 5.00 | 5.53 | 0.53 | 77 |
| 217 | 4.50 | 5.53 | 1.03 | 78 |
| 217 | 4.00 | 5.53 | 1.53 | 86 |
| 217 | 3.50 | 5.53 | 2.03 | 93 |
| 217 | 3.00 | 5.53 | 2.53 | 95 |
| 217 | 2.50 | 5.53 | 3.03 | 94 |
| 336 | 5.00 | 5.44 | 0.44 | 28 |
| 336 | 4.50 | 5.44 | 0.94 | 60 |
| 336 | 4.00 | 5.44 | 1.44 | 65 |
| 336 | 3.50 | 5.44 | 1.94 | 65 |
| 336 | 3.00 | 5.44 | 2.44 | 69 |
| 336 | 2.67 | 5.44 | 2.78 | 70 |
| 336 | 2.00 | 5.44 | 3.44 | 72 |
| 434 | 5.00 | 5.34 | 0.34 | 26 |
| 434 | 4.50 | 5.34 | 0.84 | 35 |
| 434 | 4.00 | 5.34 | 1.34 | 54 |
| 434 | 3.50 | 5.34 | 1.84 | 59 |
| 434 | 3.00 | 5.34 | 2.34 | 60 |
| 434 | 2.50 | 5.34 | 2.84 | 62 |
| 434 | 2.00 | 5.34 | 3.34 | 63 |

^a As measured from the bottom of the column

^b Relative to the top liquid level

Table D2. Total suspended solids (TSS) concentrations measured above the sediment-water interface for characterization of flocculent settling during pilot-scale column settling test using composited sediment from borings B-11, B-14, and B-15.

| Sample Extraction Time (hr) | Port Height (ft) ^a | Head Height (ft) ^a | Depth of Sample Extraction (ft) ^b | TSS (mg/L) |
|-----------------------------|-------------------------------|-------------------------------|--|------------------|
| 24 | 5.50 | 6.00 | 0.50 | 188 |
| 30 | 5.50 | 5.98 | 0.48 | 116 |
| 30 | 5.00 | 5.98 | 0.98 | 182 |
| 48 | 5.50 | 5.96 | 0.46 | 68 |
| 48 | 5.00 | 5.96 | 0.96 | 80 |
| 48 | 4.50 | 5.96 | 1.46 | 116 |
| 48 | 4.00 | 5.96 | 1.96 | 283 |
| 72 | 5.50 | 5.89 | 0.39 | 67 |
| 72 | 5.00 | 5.89 | 0.89 | 73 |
| 72 | 4.50 | 5.89 | 1.39 | 75 |
| 72 | 4.00 | 5.89 | 1.89 | 88 |
| 72 | 3.50 | 5.89 | 2.39 | 124 |
| 96 | 5.50 | 5.82 | 0.32 | 51 |
| 96 | 5.00 | 5.82 | 0.82 | 69 |
| 96 | 4.50 | 5.82 | 1.32 | 72 |
| 96 | 4.00 | 5.82 | 1.82 | 73 |
| 96 | 3.50 | 5.82 | 2.32 | 89 |
| 122 | 5.50 | 5.75 | 0.25 | 26 |
| 122 | 5.00 | 5.75 | 0.75 | 54 |
| 122 | 4.50 | 5.75 | 1.25 | 60 |
| 122 | 4.00 | 5.75 | 1.75 | 61 |
| 122 | 3.50 | 5.75 | 2.25 | 75 |
| 150 | 5.50 | 5.69 | 0.19 | <25 ^c |
| 150 | 5.00 | 5.69 | 0.69 | 50 |
| 150 | 4.50 | 5.69 | 1.19 | 52 |
| 150 | 4.00 | 5.69 | 1.69 | 53 |
| 150 | 3.50 | 5.69 | 2.19 | 59 |

^a As measured from the bottom of the column

^b Relative to the top liquid level

^c The mass of dry residue retained on the filter was less than 2.5 mg (the minimum required for an acceptable analysis). The result is reported here as <25 mg/L [calculated as the minimum residue mass required for acceptable analysis, 2.5 mg, divided by the sample volume filtered (0.10 L)].

Table D2. Continued from previous page

| Sample Extraction Time (hr) | Port Height (ft)^a | Head Height (ft)^a | Depth of Sample Extraction (ft)^b | TSS (mg/L) |
|--|---|---|--|-----------------------|
| 176 | 5.50 | 5.63 | 0.13 | <25 ^c |
| 176 | 5.00 | 5.63 | 0.63 | 32 |
| 176 | 4.50 | 5.63 | 1.13 | 52 |
| 176 | 4.00 | 5.63 | 1.63 | 56 |
| 176 | 3.50 | 5.63 | 2.13 | 57 |
| 217 | 5.50 | 5.57 | 0.07 | <25 ^c |
| 217 | 5.00 | 5.57 | 0.57 | 34 |
| 217 | 4.50 | 5.57 | 1.07 | 54 |
| 217 | 4.00 | 5.57 | 1.57 | 55 |
| 217 | 3.50 | 5.57 | 2.07 | 54 |
| 336 | 5.00 | 5.49 | 0.49 | <25 ^c |
| 336 | 4.50 | 5.49 | 0.99 | 33 |
| 336 | 4.00 | 5.49 | 1.49 | 37 |
| 336 | 3.50 | 5.49 | 1.99 | 47 |
| 434 | 5.00 | 5.44 | 0.44 | <25 ^c |
| 434 | 4.50 | 5.44 | 0.94 | 27 |
| 434 | 4.00 | 5.44 | 1.44 | 28 |
| 434 | 3.50 | 5.44 | 1.94 | 31 |
| 434 | 3.00 | 5.44 | 2.44 | 32 |

^a As measured from the bottom of the column

^b Relative to the top liquid level

^c The mass of dry residue retained on the filter was less than 2.5 mg (the minimum required for an acceptable analysis). The result is reported here as <25 mg/L [calculated as the minimum residue mass required for acceptable analysis, 2.5 mg, divided by the sample volume filtered (0.10 L)].